ANEJO Nº 6. ESTRUCTURAS

4. Cálculos

4. CALCULOS

A continuación se adjuntan los cálculos correspondientes al Viaducto del Bò:

SUBANEJOS

ESFUERZOS EN ESTADOS INDIVIDUALES

PRETENSADOS EN ESTRUCTURA IDEAL (Fase 4)

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEI.FAM1.ISO + [1; 1]ej1preEI.FAM2.ISO + [1; 1]ej1preEI.FAM3.ISO + [1; 1]ej1preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-1201.76	0.00	-1538.71
27	27	30.40	-1533.28	0.00	-1982.61
27	28	31.80	-1533.28	0.00	-1982.61
28	28	31.80	-1533.28	0.00	-1982.61
28	29	33.20	-1533.28	0.00	-1982.61
29	29	33.20	-1533.28	0.00	-1982.61
29	30	34.60	-1533.28	0.00	-1982.61
30	30	34.60	-1533.28	0.00	-1982.61
30	31	36.00	-1533.28	0.00	-1982.61
31	31	36.00	-1533.28	0.00	-1982.61
31	32	37.40	-1533.28	0.00	-1982.61
32	32	37.40	-1533.28	0.00	-1982.61
32	33	38.80	-1533.28	0.00	-1982.61
33	33	38.80	-1533.28	0.00	-1982.61
33	34	40.20	-1533.28	0.00	-1982.61
34	34	40.20	-1533.28	0.00	-1982.61
34	35	41.60	-1533.28	0.00	-1982.61
35	35	41.60	-1201.76	0.00	-1538.71
35	36	43.00	-1201.76	0.00	-1538.71
36	36	43.00	-1201.76	0.00	-1538.71
36	37	44.40	-1201.76	0.00	-1538.71
37	37	44.40	-828.80	0.00	-1031.86
37	38	45.80	-828.80	0.00	-1031.86
38	38	45.80	-828.80	0.00	-1031.86
38	39	47.20	-828.80	0.00	-1031.86
39	39	47.20	-538.72	0.00	-628.93
39	40	48.60	-538.72	0.00	-628.93
40	40	48.60	-538.72	0.00	-628.93
40	41	50.00	-538.72	0.00	-628.93
41	1041	50.00	-538.72	0.00	-628.93
41	42	51.40	-538.72	0.00	-628.93
42	42	51.40	-538.72	0.00	-628.93
42	43	52.80	-538.72	0.00	-628.93
43	43	52.80	-828.80	0.00	-1031.86
43	44	54.20	-828.80	0.00	-1031.86
44	44	54.20	-828.80	0.00	-1031.86
44	45	55.60	-828.80	0.00	-1031.86
45	45	55.60	-1201.76	0.00	-1538.71
45	46	57.00	-1201.76	0.00	-1538.71
46	46	57.00	-1201.76	0.00	-1538.71
46	47	58.40	-1201.76	0.00	-1538.71
47	47	58.40	-1533.28	0.00	-1982.61
47	48	59.80	-1533.28	0.00	-1982.61
48	48	59.80	-1533.28	0.00	-1982.61
48	49	61.20	-1533.28	0.00	-1982.61
49	49	61.20	-1533.28	0.00	-1982.61
49	50	62.60	-1533.28	0.00	-1982.61
50	50	62.60	-1533.28	0.00	-1982.61
50	51	64.00	-1533.28	0.00	-1982.61
51	51	64.00	-1533.28	0.00	-1982.61
51	52	65.40	-1533.28	0.00	-1982.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1)ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	1.04	-77.41	-568.17
1	2	1.10	1.04	-77.41	-483.02
2	2	1.10	-288.46	-79.38	-885.99
2	3	2.20	-288.46	-79.38	-798.67
3	3	2.20	-287.64	-80.23	-796.22
3	4	3.30	-287.64	-80.23	-707.97
4	4	3.30	-493.79	-80.12	-991.60
4	5	4.40	-493.79	-80.12	-903.47
5	5	4.40	-492.73	-79.23	-901.82
5	6	5.50	-492.73	-79.23	-814.66
6	6	5.50	-698.86	-77.73	-1097.06
6	7	6.60	-698.86	-77.73	-1011.55
7	7	6.60	-698.00	-75.80	-1010.78
7	8	7.70	-698.00	-75.80	-927.40
8	8	7.70	-697.34	-73.63	-927.04
8	9	8.80	-697.34	-73.63	-846.05
9	9	8.80	-696.89	-71.36	-846.08
9	10	9.90	-696.89	-71.36	-767.58
10	10	9.90	-696.63	-69.14	-767.95
10	11	11.00	-696.63	-69.14	-691.90
11	11	11.00	-696.58	-67.09	-692.58
11	12	12.10	-696.58	-67.09	-618.78
12	12	12.10	-696.74	-65.33	-619.74
12	13	13.20	-696.74	-65.33	-547.88
13	13	13.20	-697.12	-63.94	-549.10
13	14	14.30	-697.12	-63.94	-478.76
14	14	14.30	-490.52	-63.03	-196.54
14	15	15.40	-490.52	-63.03	-127.21
15	15	15.40	-491.14	-62.64	-128.71
15	16	16.50	-491.14	-62.64	-59.81
16	16	16.50	-491.78	-62.80	-61.35
16	17	17.60	-491.78	-62.80	7.31
17	17	17.60	-285.26	-63.51	291.90
17	18	18.70	-285.26	-63.51	361.76
18	18	18.70	-285.76	-64.76	360.36
18	19	19.80	-285.76	-64.76	431.60
19	19	19.80	3.99	-66.49	836.20
19	20	20.90	3.99	-66.49	909.34
20	20	20.90	4.12	-68.58	908.52
20	21	22.00	4.12	-68.58	983.95
21	1021	22.00	-36.43	11.25	924.30
21	22	23.40	-36.43	11.25	908.55
22	22	23.40	-34.06	8.33	908.74
22	23	24.80	-34.06	8.33	897.07
23	23	24.80	-320.59	5.73	495.01
23	24	26.20	-320.59	5.73	486.99
24	24	26.20	-316.59	3.70	488.20
24	25	27.60	-316.59	3.70	483.02
25	25	27.60	-685.01	2.40	-22.27
25	26	29.00	-685.01	2.40	-25.63
26	26	29.00	-680.87	1.90	-24.10

F4.pret.esf.xls Programa DINTEL PACADAR S.A. 11/09/03
ej1preEl.TOT.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1)ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-680.87	1.90	-26.76
27	27	30.40	-1008.54	2.17	-469.16
27	28	31.80	-1008.54	2.17	-472.20
28	28	31.80	-1005.84	3.12	-471.05
28	29	33.20	-1005.84	3.12	-475.42
29	29	33.20	-1004.22	4.55	-474.62
29	30	34.60	-1004.22	4.55	-481.00
30	30	34.60	-1003.63	6.31	-480.54
30	31	36.00	-1003.63	6.31	-489.38
31	31	36.00	-1004.07	8.22	-489.27
31	32	37.40	-1004.07	8.22	-500.78
32	32	37.40	-1005.56	10.12	-501.02
32	33	38.80	-1005.56	10.12	-515.18
33	33	38.80	-1008.13	11.83	-515.79
33	34	40.20	-1008.13	11.83	-532.35
34	34	40.20	-1011.86	13.18	-533.33
34	35	41.60	-1011.86	13.18	-551.78
35	35	41.60	-685.34	13.97	-109.25
35	36	43.00	-685.34	13.97	-128.80
36	36	43.00	-690.79	14.07	-130.26
36	37	44.40	-690.79	14.07	-149.96
37	37	44.40	-323.88	13.45	355.32
37	38	45.80	-323.88	13.45	336.49
38	38	45.80	-329.63	12.12	335.18
38	39	47.20	-329.63	12.12	318.22
39	39	47.20	-45.16	10.21	720.08
39	40	48.60	-45.16	10.21	705.79
40	40	48.60	-49.95	7.90	705.26
40	41	50.00	-49.95	7.90	694.20
41	1041	50.00	-54.06	-7.90	694.20
41	42	51.40	-54.06	-7.90	705.26
42	42	51.40	-57.50	-10.20	705.79
42	43	52.80	-57.50	-10.20	720.07
43	43	52.80	-350.24	-12.12	318.22
43	44	54.20	-350.24	-12.12	335.18
44	44	54.20	-352.80	-13.45	336.49
44	45	55.60	-352.80	-13.45	355.31
45	45	55.60	-728.11	-14.07	-149.97
45	46	57.00	-728.11	-14.07	-130.26
46	46	57.00	-731.16	-13.96	-128.80
46	47	58.40	-731.16	-13.96	-109.25
47	47	58.40	-1066.33	-13.18	-551.78
47	48	59.80	-1066.33	-13.18	-533.33
48	48	59.80	-1071.41	-11.83	-532.35
48	49	61.20	-1071.41	-11.83	-515.79
49	49	61.20	-1077.84	-10.12	-515.19
49	50	62.60	-1077.84	-10.12	-501.02
50	50	62.60	-1085.62	-8.22	-500.78
50	51	64.00	-1085.62	-8.22	-489.27
51	51	64.00	-1094.73	-6.31	-489.38
51	52	65.40	-1094.73	-6.31	-480.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-1105.22	-4.55	-481.00
52	53	66.80	-1105.22	-4.55	-474.63
53	53	66.80	-1117.16	-3.12	-475.43
53	54	68.20	-1117.16	-3.12	-471.06
54	54	68.20	-1130.68	-2.17	-472.21
54	55	69.60	-1130.68	-2.17	-469.17
55	55	69.60	-814.41	-1.90	-26.76
55	56	71.00	-814.41	-1.90	-24.10
56	56	71.00	-830.65	-2.40	-25.63
56	57	72.40	-830.65	-2.40	-22.27
57	57	72.40	-475.15	-3.70	483.02
57	58	73.80	-475.15	-3.70	488.20
58	58	73.80	-493.01	-5.73	486.99
58	59	75.20	-493.01	-5.73	495.01
59	59	75.20	-221.47	-8.33	897.08
59	60	76.60	-221.47	-8.33	908.74
60	60	76.60	-240.16	-11.25	908.55
60	61	78.00	-240.16	-11.25	924.31
61	1061	78.00	-212.32	68.58	983.96
61	62	79.10	-212.32	68.58	908.52
62	62	79.10	-221.75	66.49	909.34
62	63	80.20	-221.75	66.49	836.20
63	63	80.20	-521.38	64.77	431.60
63	64	81.30	-521.38	64.77	360.36
64	64	81.30	-531.35	63.52	361.76
64	65	82.40	-531.35	63.52	291.89
65	65	82.40	-748.89	62.80	7.72
65	66	83.50	-748.89	62.80	-61.36
66	66	83.50	-759.81	62.64	-59.82
66	67	84.60	-759.81	62.64	-128.73
67	67	84.60	-771.30	63.03	-127.23
67	68	85.70	-771.30	63.03	-196.56
68	68	85.70	-990.54	63.94	-478.78
68	69	86.80	-990.54	63.94	-549.12
69	69	86.80	-1003.37	65.33	-547.91
69	70	87.90	-1003.37	65.33	-619.77
70	70	87.90	-1016.96	67.10	-618.81
70	71	89.00	-1016.96	67.10	-692.61
71	71	89.00	-1031.34	69.14	-691.93
71	72	90.10	-1031.34	69.14	-767.98
72	72	90.10	-1046.52	71.36	-767.61
72	73	91.20	-1046.52	71.36	-846.11
73	73	91.20	-1062.53	73.62	-846.08
73	74	92.30	-1062.53	73.62	-927.07
74	74	92.30	-1079.40	75.80	-927.42
74	75	93.40	-1079.40	75.80	-1010.80
75	75	93.40	-1097.17	77.73	-1011.58
75	76	94.50	-1097.17	77.73	-1097.08
76	76	94.50	-908.71	79.23	-814.68
76	77	95.60	-908.71	79.23	-901.83
77	77	95.60	-928.25	80.12	-903.49

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-928.25	80.12	-991.61
78	78	96.70	-741.47	80.23	-707.98
78	79	97.80	-741.47	80.23	-796.23
79	79	97.80	-762.60	79.38	-798.68
79	80	98.90	-762.60	79.38	-885.99
80	80	98.90	-494.46	77.41	-483.02
80	81	100.00	-494.46	77.41	-568.17
101	101	0.00	-498.32	5.00	-1.55
101	102	1.10	-498.32	5.00	-7.05
102	102	1.10	-498.91	6.97	-9.89
102	103	2.20	-498.91	6.97	-17.56
103	103	2.20	-499.72	7.82	-20.01
103	104	3.30	-499.72	7.82	-28.61
104	104	3.30	-500.77	7.71	-30.70
104	105	4.40	-500.77	7.71	-39.18
105	105	4.40	-501.83	6.81	-40.83
105	106	5.50	-501.83	6.81	-48.33
106	106	5.50	-502.90	5.32	-49.59
106	107	6.60	-502.90	5.32	-55.44
107	107	6.60	-503.76	3.39	-56.22
107	108	7.70	-503.76	3.39	-59.95
108	108	7.70	-504.42	1.22	-60.30
108	109	8.80	-504.42	1.22	-61.64
109	109	8.80	-504.88	-1.05	-61.62
109	110	9.90	-504.88	-1.05	-60.46
110	110	9.90	-505.13	-3.26	-60.09
110	111	11.00	-505.13	-3.26	-56.50
111	111	11.00	-505.18	-5.31	-55.82
111	112	12.10	-505.18	-5.31	-49.98
112	112	12.10	-505.02	-7.07	-49.01
112	113	13.20	-505.02	-7.07	-41.23
113	113	13.20	-504.64	-8.46	-40.02
113	114	14.30	-504.64	-8.46	-30.71
114	114	14.30	-504.04	-9.37	-29.28
114	115	15.40	-504.04	-9.37	-18.97
115	115	15.40	-503.42	-9.76	-17.47
115	116	16.50	-503.42	-9.76	-6.73
116	116	16.50	-502.78	-9.60	-5.19
116	117	17.60	-502.78	-9.60	5.37
117	117	17.60	-502.10	-8.88	6.92
117	118	18.70	-502.10	-8.88	16.70
118	118	18.70	-501.60	-7.63	18.10
118	119	19.80	-501.60	-7.63	26.50
119	119	19.80	-501.27	-5.91	27.72
119	120	20.90	-501.27	-5.91	34.22
120	120	20.90	-501.40	-3.82	35.04
120	121	22.00	-501.40	-3.82	39.24
121	1121	22.00	-502.29	-2.31	39.68
121	122	23.40	-502.29	-2.31	42.92
122	122	23.40	-504.66	0.61	42.73
122	123	24.80	-504.66	0.61	41.88

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-508.21	3.20	41.02
123	124	26.20	-508.21	3.20	36.53
124	124	26.20	-512.21	5.24	35.32
124	125	27.60	-512.21	5.24	27.99
125	125	27.60	-516.75	6.54	26.42
125	126	29.00	-516.75	6.54	17.26
126	126	29.00	-520.90	7.04	15.73
126	127	30.40	-520.90	7.04	5.87
127	127	30.40	-524.74	6.77	4.37
127	128	31.80	-524.74	6.77	-5.11
128	128	31.80	-527.44	5.83	-6.25
128	129	33.20	-527.44	5.83	-14.41
129	129	33.20	-529.06	4.39	-15.21
129	130	34.60	-529.06	4.39	-21.36
130	130	34.60	-529.65	2.64	-21.82
130	131	36.00	-529.65	2.64	-25.51
131	131	36.00	-529.21	0.73	-25.62
131	132	37.40	-529.21	0.73	-26.65
132	132	37.40	-527.72	-1.16	-26.41
132	133	38.80	-527.72	-1.16	-24.78
133	133	38.80	-525.15	-2.87	-24.18
133	134	40.20	-525.15	-2.87	-20.16
134	134	40.20	-521.42	-4.22	-19.18
134	135	41.60	-521.42	-4.22	-13.28
135	135	41.60	-516.42	-5.00	-11.90
135	136	43.00	-516.42	-5.00	-4.90
136	136	43.00	-510.97	-5.11	-3.43
136	137	44.40	-510.97	-5.11	3.72
137	137	44.40	-504.92	-4.48	5.29
137	138	45.80	-504.92	-4.48	11.56
138	138	45.80	-499.17	-3.15	12.87
138	139	47.20	-499.17	-3.15	17.28
139	139	47.20	-493.56	-1.24	18.34
139	140	48.60	-493.56	-1.24	20.08
140	140	48.60	-488.77	1.07	20.60
140	141	50.00	-488.77	1.07	19.11
141	1141	50.00	-484.65	-1.07	19.11
141	142	51.40	-484.65	-1.07	20.60
142	142	51.40	-481.22	1.24	20.07
142	143	52.80	-481.22	1.24	18.34
143	143	52.80	-478.56	3.15	17.28
143	144	54.20	-478.56	3.15	12.87
144	144	54.20	-476.00	4.48	11.56
144	145	55.60	-476.00	4.48	5.29
145	145	55.60	-473.65	5.11	3.71
145	146	57.00	-473.65	5.11	-3.44
146	146	57.00	-470.60	5.00	-4.90
146	147	58.40	-470.60	5.00	-11.90
147	147	58.40	-466.95	4.22	-13.28
147	148	59.80	-466.95	4.22	-19.18
148	148	59.80	-461.88	2.87	-20.16

CÁLCULO TENSIONAL

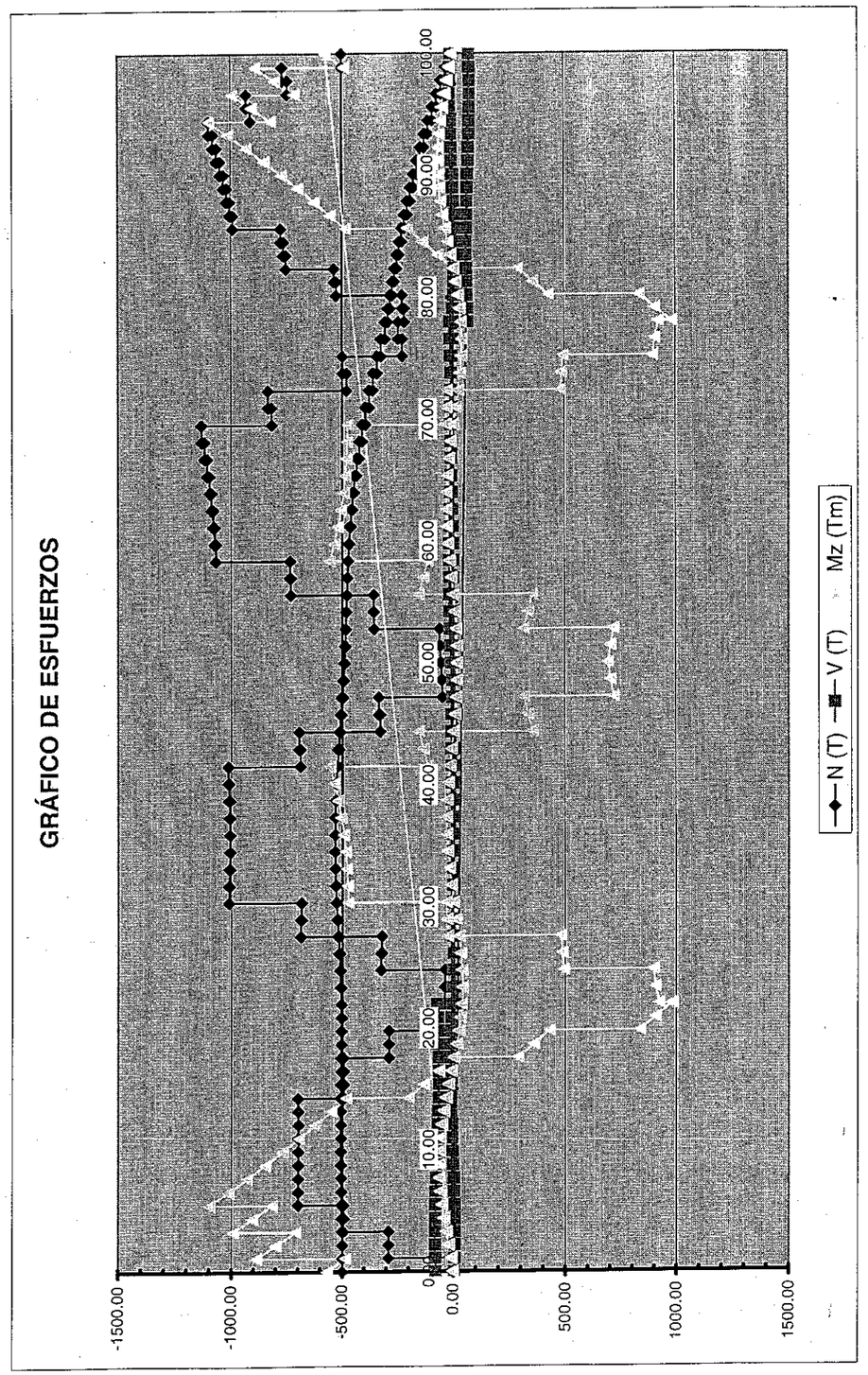
Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-461.88	2.87	-24.18
149	149	61.20	-455.44	1.16	-24.79
149	150	62.60	-455.44	1.16	-26.41
150	150	62.60	-447.66	-0.73	-26.65
150	151	64.00	-447.66	-0.73	-25.63
151	151	64.00	-438.55	-2.64	-25.52
151	152	65.40	-438.55	-2.64	-21.82
152	152	65.40	-428.06	-4.39	-21.37
152	153	66.80	-428.06	-4.39	-15.21
153	153	66.80	-416.12	-5.83	-14.41
153	154	68.20	-416.12	-5.83	-6.26
154	154	68.20	-402.60	-6.77	-5.11
154	155	69.60	-402.60	-6.77	4.37
155	155	69.60	-387.35	-7.04	5.87
155	156	71.00	-387.35	-7.04	15.73
156	156	71.00	-371.11	-6.54	17.26
156	157	72.40	-371.11	-6.54	26.42
157	157	72.40	-353.65	-5.24	27.99
157	158	73.80	-353.65	-5.24	35.32
158	158	73.80	-335.79	-3.21	36.53
158	159	75.20	-335.79	-3.21	41.02
159	159	75.20	-317.25	-0.61	41.88
159	160	76.60	-317.25	-0.61	42.73
160	160	76.60	-298.56	2.31	42.92
160	161	78.00	-298.56	2.31	39.68
161	1161	78.00	-284.96	3.82	39.25
161	162	79.10	-284.96	3.82	35.04
162	162	79.10	-275.53	5.91	34.22
162	163	80.20	-275.53	5.91	27.72
163	163	80.20	-265.97	7.63	26.50
163	164	81.30	-265.97	7.63	18.10
164	164	81.30	-256.01	8.89	16.70
164	165	82.40	-256.01	8.89	6.92
165	165	82.40	-245.67	9.60	5.37
165	166	83.50	-245.67	9.60	-5.19
166	166	83.50	-234.75	9.76	-6.73
166	167	84.60	-234.75	9.76	-17.47
167	167	84.60	-223.26	9.37	-18.97
167	168	85.70	-223.26	9.37	-29.28
168	168	85.70	-211.21	8.46	-30.71
168	169	86.80	-211.21	8.46	-40.02
169	169	86.80	-198.39	7.07	-41.23
169	170	87.90	-198.39	7.07	-49.02
170	170	87.90	-184.80	5.31	-49.98
170	171	89.00	-184.80	5.31	-55.82
171	171	89.00	-170.42	3.26	-56.50
171	172	90.10	-170.42	3.26	-60.09
172	172	90.10	-155.24	1.05	-60.47
172	173	91.20	-155.24	1.05	-61.62
173	173	91.20	-139.23	-1.22	-61.65
173	174	92.30	-139.23	-1.22	-60.31



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	1.04	-77.41	-568.17
1	2	1.10	1.04	-77.41	-483.02
2	2	1.10	-288.46	-79.38	-885.99
2	3	2.20	-288.46	-79.38	-798.67
3	3	2.20	-287.64	-80.23	-796.22
3	4	3.30	-287.64	-80.23	-707.97
4	4	3.30	-493.79	-80.12	-991.60
4	5	4.40	-493.79	-80.12	-903.47
5	5	4.40	-492.73	-79.23	-901.82
5	6	5.50	-492.73	-79.23	-814.66
6	6	5.50	-698.86	-77.73	-1097.06
6	7	6.60	-698.86	-77.73	-1011.55
7	7	6.60	-698.00	-75.80	-1010.78
7	8	7.70	-698.00	-75.80	-927.40
8	8	7.70	-697.34	-73.63	-927.04
8	9	8.80	-697.34	-73.63	-846.05
9	9	8.80	-696.89	-71.36	-846.08
9	10	9.90	-696.89	-71.36	-767.58
10	10	9.90	-696.63	-69.14	-767.95
10	11	11.00	-696.63	-69.14	-691.90
11	11	11.00	-696.58	-67.09	-692.58
11	12	12.10	-696.58	-67.09	-618.78
12	12	12.10	-696.74	-65.33	-619.74
12	13	13.20	-696.74	-65.33	-547.88
13	13	13.20	-697.12	-63.94	-549.10
13	14	14.30	-697.12	-63.94	-478.76
14	14	14.30	-490.52	-63.03	-196.54
14	15	15.40	-490.52	-63.03	-127.21
15	15	15.40	-491.14	-62.64	-128.71
15	16	16.50	-491.14	-62.64	-59.81
16	16	16.50	-491.78	-62.80	-61.35
16	17	17.60	-491.78	-62.80	7.31
17	17	17.60	-285.26	-63.51	291.90
17	18	18.70	-285.26	-63.51	361.76
18	18	18.70	-285.76	-64.76	360.36
18	19	19.80	-285.76	-64.76	431.60
19	19	19.80	3.99	-66.49	836.20
19	20	20.90	3.99	-66.49	909.34
20	20	20.90	4.12	-68.58	908.52
20	21	22.00	4.12	-68.58	983.95
21	1021	22.00	-36.43	11.25	924.30
21	22	23.40	-36.43	11.25	908.55
22	22	23.40	-34.06	8.33	908.74
22	23	24.80	-34.06	8.33	897.07
23	23	24.80	-320.59	5.73	495.01
23	24	26.20	-320.59	5.73	486.99
24	24	26.20	-316.59	3.70	488.20
24	25	27.60	-316.59	3.70	483.02
25	25	27.60	-685.01	2.40	-22.27
25	26	29.00	-685.01	2.40	-25.63
26	26	29.00	-680.87	1.90	-24.10

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAI

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-680.87	1.90	-26.76
27	27	30.40	-1008.54	2.17	-469.16
27	28	31.80	-1008.54	2.17	-472.20
28	28	31.80	-1005.84	3.12	-471.05
28	29	33.20	-1005.84	3.12	-475.42
29	29	33.20	-1004.22	4.55	-474.62
29	30	34.60	-1004.22	4.55	-481.00
30	30	34.60	-1003.63	6.31	-480.54
30	31	36.00	-1003.63	6.31	-489.38
31	31	36.00	-1004.07	8.22	-489.27
31	32	37.40	-1004.07	8.22	-500.78
32	32	37.40	-1005.56	10.12	-501.02
32	33	38.80	-1005.56	10.12	-515.18
33	33	38.80	-1008.13	11.83	-515.79
33	34	40.20	-1008.13	11.83	-532.35
34	34	40.20	-1011.86	13.18	-533.33
34	35	41.60	-1011.86	13.18	-551.78
35	35	41.60	-685.34	13.97	-109.25
35	36	43.00	-685.34	13.97	-128.80
36	36	43.00	-690.79	14.07	-130.26
36	37	44.40	-690.79	14.07	-149.96
37	37	44.40	-323.88	13.45	355.32
37	38	45.80	-323.88	13.45	336.49
38	38	45.80	-329.63	12.12	335.18
38	39	47.20	-329.63	12.12	318.22
39	39	47.20	-45.16	10.21	720.08
39	40	48.60	-45.16	10.21	705.79
40	40	48.60	-49.95	7.90	705.26
40	41	50.00	-49.95	7.90	694.20
41	1041	50.00	-54.06	-7.90	694.20
41	42	51.40	-54.06	-7.90	705.26
42	42	51.40	-57.50	-10.20	705.79
42	43	52.80	-57.50	-10.20	720.07
43	43	52.80	-350.24	-12.12	318.22
43	44	54.20	-350.24	-12.12	335.18
44	44	54.20	-352.80	-13.45	336.49
44	45	55.60	-352.80	-13.45	355.31
45	45	55.60	-728.11	-14.07	-149.97
45	46	57.00	-728.11	-14.07	-130.26
46	46	57.00	-731.16	-13.96	-128.80
46	47	58.40	-731.16	-13.96	-109.25
47	47	58.40	-1066.33	-13.18	-551.78
47	48	59.80	-1066.33	-13.18	-533.33
48	48	59.80	-1071.41	-11.83	-532.35
48	49	61.20	-1071.41	-11.83	-515.79
49	49	61.20	-1077.84	-10.12	-515.19
49	50	62.60	-1077.84	-10.12	-501.02
50	50	62.60	-1085.62	-8.22	-500.78
50	51	64.00	-1085.62	-8.22	-489.27
51	51	64.00	-1094.73	-6.31	-489.38
51	52	65.40	-1094.73	-6.31	-480.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAI

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-1105.22	-4.55	-481.00
52	53	66.80	-1105.22	-4.55	-474.63
53	53	66.80	-1117.16	-3.12	-475.43
53	54	68.20	-1117.16	-3.12	-471.06
54	54	68.20	-1130.68	-2.17	-472.21
54	55	69.60	-1130.68	-2.17	-469.17
55	55	69.60	-814.41	-1.90	-26.76
55	56	71.00	-814.41	-1.90	-24.10
56	56	71.00	-830.65	-2.40	-25.63
56	57	72.40	-830.65	-2.40	-22.27
57	57	72.40	-475.15	-3.70	483.02
57	58	73.80	-475.15	-3.70	488.20
58	58	73.80	-493.01	-5.73	486.99
58	59	75.20	-493.01	-5.73	495.01
59	59	75.20	-221.47	-8.33	897.08
59	60	76.60	-221.47	-8.33	908.74
60	60	76.60	-240.16	-11.25	908.55
60	61	78.00	-240.16	-11.25	924.31
61	1061	78.00	-212.32	68.58	983.96
61	62	79.10	-212.32	68.58	908.52
62	62	79.10	-221.75	66.49	909.34
62	63	80.20	-221.75	66.49	836.20
63	63	80.20	-521.38	64.77	431.60
63	64	81.30	-521.38	64.77	360.36
64	64	81.30	-531.35	63.52	361.76
64	65	82.40	-531.35	63.52	291.89
65	65	82.40	-748.89	62.80	7.72
65	66	83.50	-748.89	62.80	-61.36
66	66	83.50	-759.81	62.64	-59.82
66	67	84.60	-759.81	62.64	-128.73
67	67	84.60	-771.30	63.03	-127.23
67	68	85.70	-771.30	63.03	-196.56
68	68	85.70	-990.54	63.94	-478.78
68	69	86.80	-990.54	63.94	-549.12
69	69	86.80	-1003.37	65.33	-547.91
69	70	87.90	-1003.37	65.33	-619.77
70	70	87.90	-1016.96	67.10	-618.81
70	71	89.00	-1016.96	67.10	-692.61
71	71	89.00	-1031.34	69.14	-691.93
71	72	90.10	-1031.34	69.14	-767.98
72	72	90.10	-1046.52	71.36	-767.61
72	73	91.20	-1046.52	71.36	-846.11
73	73	91.20	-1062.53	73.62	-846.08
73	74	92.30	-1062.53	73.62	-927.07
74	74	92.30	-1079.40	75.80	-927.42
74	75	93.40	-1079.40	75.80	-1010.80
75	75	93.40	-1097.17	77.73	-1011.58
75	76	94.50	-1097.17	77.73	-1097.08
76	76	94.50	-908.71	79.23	-814.68
76	77	95.60	-908.71	79.23	-901.83
77	77	95.60	-928.25	80.12	-903.49

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-928.25	80.12	-991.61
78	78	96.70	-741.47	80.23	-707.98
78	79	97.80	-741.47	80.23	-796.23
79	79	97.80	-762.60	79.38	-798.68
79	80	98.90	-762.60	79.38	-885.99
80	80	98.90	-494.46	77.41	-483.02
80	81	100.00	-494.46	77.41	-568.17
101	101	0.00	-498.32	5.00	-1.55
101	102	1.10	-498.32	5.00	-7.05
102	102	1.10	-498.91	6.97	-9.89
102	103	2.20	-498.91	6.97	-17.56
103	103	2.20	-499.72	7.82	-20.01
103	104	3.30	-499.72	7.82	-28.61
104	104	3.30	-500.77	7.71	-30.70
104	105	4.40	-500.77	7.71	-39.18
105	105	4.40	-501.83	6.81	-40.83
105	106	5.50	-501.83	6.81	-48.33
106	106	5.50	-502.90	5.32	-49.59
106	107	6.60	-502.90	5.32	-55.44
107	107	6.60	-503.76	3.39	-56.22
107	108	7.70	-503.76	3.39	-59.95
108	108	7.70	-504.42	1.22	-60.30
108	109	8.80	-504.42	1.22	-61.64
109	109	8.80	-504.88	-1.05	-61.62
109	110	9.90	-504.88	-1.05	-60.46
110	110	9.90	-505.13	-3.26	-60.09
110	111	11.00	-505.13	-3.26	-56.50
111	111	11.00	-505.18	-5.31	-55.82
111	112	12.10	-505.18	-5.31	-49.98
112	112	12.10	-505.02	-7.07	-49.01
112	113	13.20	-505.02	-7.07	-41.23
113	113	13.20	-504.64	-8.46	-40.02
113	114	14.30	-504.64	-8.46	-30.71
114	114	14.30	-504.04	-9.37	-29.28
114	115	15.40	-504.04	-9.37	-18.97
115	115	15.40	-503.42	-9.76	-17.47
115	116	16.50	-503.42	-9.76	-6.73
116	116	16.50	-502.78	-9.60	-5.19
116	117	17.60	-502.78	-9.60	5.37
117	117	17.60	-502.10	-8.88	6.92
117	118	18.70	-502.10	-8.88	16.70
118	118	18.70	-501.60	-7.63	18.10
118	119	19.80	-501.60	-7.63	26.50
119	119	19.80	-501.27	-5.91	27.72
119	120	20.90	-501.27	-5.91	34.22
120	120	20.90	-501.40	-3.82	35.04
120	121	22.00	-501.40	-3.82	39.24
121	1121	22.00	-502.29	-2.31	39.68
121	122	23.40	-502.29	-2.31	42.92
122	122	23.40	-504.66	0.61	42.73
122	123	24.80	-504.66	0.61	41.88

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-508.21	3.20	41.02
123	124	26.20	-508.21	3.20	36.53
124	124	26.20	-512.21	5.24	35.32
124	125	27.60	-512.21	5.24	27.99
125	125	27.60	-516.75	6.54	26.42
125	126	29.00	-516.75	6.54	17.26
126	126	29.00	-520.90	7.04	15.73
126	127	30.40	-520.90	7.04	5.87
127	127	30.40	-524.74	6.77	4.37
127	128	31.80	-524.74	6.77	-5.11
128	128	31.80	-527.44	5.83	-6.25
128	129	33.20	-527.44	5.83	-14.41
129	129	33.20	-529.06	4.39	-15.21
129	130	34.60	-529.06	4.39	-21.36
130	130	34.60	-529.65	2.64	-21.82
130	131	36.00	-529.65	2.64	-25.51
131	131	36.00	-529.21	0.73	-25.62
131	132	37.40	-529.21	0.73	-26.65
132	132	37.40	-527.72	-1.16	-26.41
132	133	38.80	-527.72	-1.16	-24.78
133	133	38.80	-525.15	-2.87	-24.18
133	134	40.20	-525.15	-2.87	-20.16
134	134	40.20	-521.42	-4.22	-19.18
134	135	41.60	-521.42	-4.22	-13.28
135	135	41.60	-516.42	-5.00	-11.90
135	136	43.00	-516.42	-5.00	-4.90
136	136	43.00	-510.97	-5.11	-3.43
136	137	44.40	-510.97	-5.11	3.72
137	137	44.40	-504.92	-4.48	5.29
137	138	45.80	-504.92	-4.48	11.56
138	138	45.80	-499.17	-3.15	12.87
138	139	47.20	-499.17	-3.15	17.28
139	139	47.20	-493.56	-1.24	18.34
139	140	48.60	-493.56	-1.24	20.08
140	140	48.60	-488.77	1.07	20.60
140	141	50.00	-488.77	1.07	19.11
141	1141	50.00	-484.65	-1.07	19.11
141	142	51.40	-484.65	-1.07	20.60
142	142	51.40	-481.22	1.24	20.07
142	143	52.80	-481.22	1.24	18.34
143	143	52.80	-478.56	3.15	17.28
143	144	54.20	-478.56	3.15	12.87
144	144	54.20	-476.00	4.48	11.56
144	145	55.60	-476.00	4.48	5.29
145	145	55.60	-473.65	5.11	3.71
145	146	57.00	-473.65	5.11	-3.44
146	146	57.00	-470.60	5.00	-4.90
146	147	58.40	-470.60	5.00	-11.90
147	147	58.40	-466.95	4.22	-13.28
147	148	59.80	-466.95	4.22	-19.18
148	148	59.80	-461.88	2.87	-20.16

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1)ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-461.88	2.87	-24.18
149	149	61.20	-455.44	1.16	-24.79
149	150	62.60	-455.44	1.16	-26.41
150	150	62.60	-447.66	-0.73	-26.65
150	151	64.00	-447.66	-0.73	-25.63
151	151	64.00	-438.55	-2.64	-25.52
151	152	65.40	-438.55	-2.64	-21.82
152	152	65.40	-428.06	-4.39	-21.37
152	153	66.80	-428.06	-4.39	-15.21
153	153	66.80	-416.12	-5.83	-14.41
153	154	68.20	-416.12	-5.83	-6.26
154	154	68.20	-402.60	-6.77	-5.11
154	155	69.60	-402.60	-6.77	4.37
155	155	69.60	-387.35	-7.04	5.87
155	156	71.00	-387.35	-7.04	15.73
156	156	71.00	-371.11	-6.54	17.26
156	157	72.40	-371.11	-6.54	26.42
157	157	72.40	-353.65	-5.24	27.99
157	158	73.80	-353.65	-5.24	35.32
158	158	73.80	-335.79	-3.21	36.53
158	159	75.20	-335.79	-3.21	41.02
159	159	75.20	-317.25	-0.61	41.88
159	160	76.60	-317.25	-0.61	42.73
160	160	76.60	-298.56	2.31	42.92
160	161	78.00	-298.56	2.31	39.68
161	1161	78.00	-284.96	3.82	39.25
161	162	79.10	-284.96	3.82	35.04
162	162	79.10	-275.53	5.91	34.22
162	163	80.20	-275.53	5.91	27.72
163	163	80.20	-265.97	7.63	26.50
163	164	81.30	-265.97	7.63	18.10
164	164	81.30	-256.01	8.89	16.70
164	165	82.40	-256.01	8.89	6.92
165	165	82.40	-245.67	9.60	5.37
165	166	83.50	-245.67	9.60	-5.19
166	166	83.50	-234.75	9.76	-6.73
166	167	84.60	-234.75	9.76	-17.47
167	167	84.60	-223.26	9.37	-18.97
167	168	85.70	-223.26	9.37	-29.28
168	168	85.70	-211.21	8.46	-30.71
168	169	86.80	-211.21	8.46	-40.02
169	169	86.80	-198.39	7.07	-41.23
169	170	87.90	-198.39	7.07	-49.02
170	170	87.90	-184.80	5.31	-49.98
170	171	89.00	-184.80	5.31	-55.82
171	171	89.00	-170.42	3.26	-56.50
171	172	90.10	-170.42	3.26	-60.09
172	172	90.10	-155.24	1.05	-60.47
172	173	91.20	-155.24	1.05	-61.62
173	173	91.20	-139.23	-1.22	-61.65
173	174	92.30	-139.23	-1.22	-60.31

CÁLCULO TENSIONAL

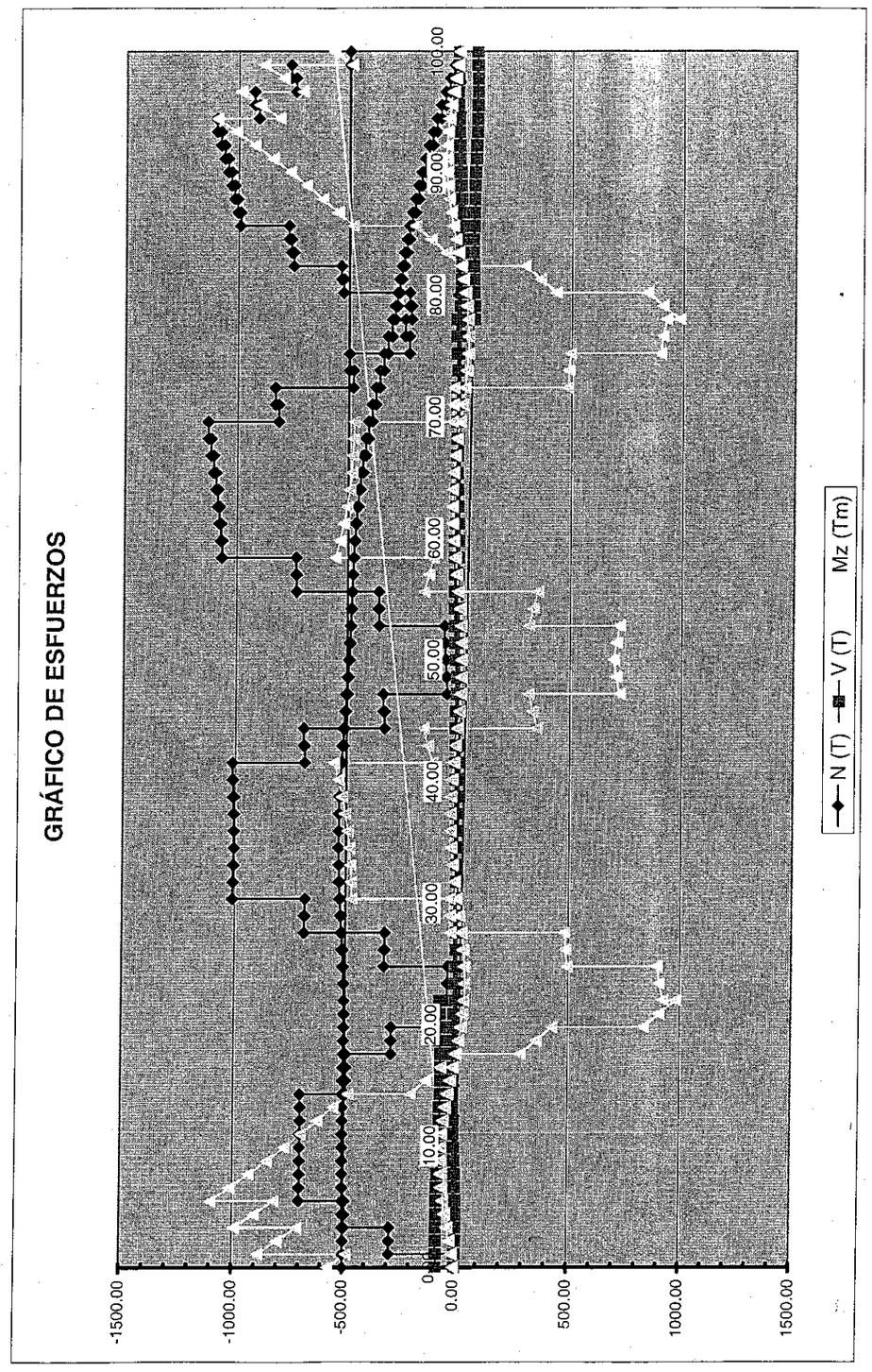
Hipótesis de cálculo:
ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1)ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-122.36	-3.39	-59.95
174	175	93.40	-122.36	-3.39	-56.22
175	175	93.40	-104.59	-5.32	-55.44
175	176	94.50	-104.59	-5.32	-49.60
176	176	94.50	-85.85	-6.82	-48.33
176	177	95.60	-85.85	-6.82	-40.84
177	177	95.60	-66.31	-7.71	-39.18
177	178	96.70	-66.31	-7.71	-30.71
178	178	96.70	-45.89	-7.82	-28.61
178	179	97.80	-45.89	-7.82	-20.01
179	179	97.80	-24.76	-6.97	-17.56
179	180	98.90	-24.76	-6.97	-9.90
180	180	98.90	-2.82	-5.00	-7.05
180	181	100.00	-2.82	-5.00	-1.55



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	498.32	-77.41	1.55
1	2	1.10	498.32	-77.41	86.70
2	2	1.10	498.90	-79.38	89.55
2	3	2.20	498.90	-79.38	176.87
3	3	2.20	499.72	-80.23	179.32
3	4	3.30	499.72	-80.23	267.57
4	4	3.30	500.77	-80.12	269.66
4	5	4.40	500.77	-80.12	357.80
5	5	4.40	501.83	-79.23	359.45
5	6	5.50	501.83	-79.23	446.60
6	6	5.50	502.90	-77.73	447.87
6	7	6.60	502.90	-77.73	533.37
7	7	6.60	503.76	-75.80	534.15
7	8	7.70	503.76	-75.80	617.53
8	8	7.70	504.42	-73.63	617.88
8	9	8.80	504.42	-73.63	698.88
9	9	8.80	504.87	-71.36	698.85
9	10	9.90	504.87	-71.36	777.35
10	10	9.90	505.13	-69.14	776.97
10	11	11.00	505.13	-69.14	853.03
11	11	11.00	505.18	-67.09	852.34
11	12	12.10	505.18	-67.09	926.15
12	12	12.10	505.02	-65.33	925.18
12	13	13.20	505.02	-65.33	997.04
13	13	13.20	504.64	-63.94	995.83
13	14	14.30	504.64	-63.94	1066.17
14	14	14.30	504.04	-63.03	1064.73
14	15	15.40	504.04	-63.03	1134.06
15	15	15.40	503.42	-62.64	1132.56
15	16	16.50	503.42	-62.64	1201.46
16	16	16.50	502.78	-62.80	1199.92
16	17	17.60	502.78	-62.80	1268.99
17	17	17.60	502.10	-63.51	1267.44
17	18	18.70	502.10	-63.51	1337.30
18	18	18.70	501.60	-64.76	1335.90
18	19	19.80	501.60	-64.76	1407.14
19	19	19.80	501.27	-66.49	1405.92
19	20	20.90	501.27	-66.49	1479.06
20	20	20.90	501.40	-68.58	1478.24
20	21	22.00	501.40	-68.58	1553.67
21	1021	22.00	502.29	11.25	1553.24
21	22	23.40	502.29	11.25	1537.48
22	22	23.40	504.66	8.33	1537.67
22	23	24.80	504.66	8.33	1526.01
23	23	24.80	508.21	5.73	1526.87
23	24	26.20	508.21	5.73	1518.84
24	24	26.20	512.21	3.70	1520.05
24	25	27.60	512.21	3.70	1514.88
25	25	27.60	516.75	2.40	1516.44
25	26	29.00	516.75	2.40	1513.08
26	26	29.00	520.90	1.90	1514.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	520.90	1.90	1511.95
27	27	30.40	524.74	2.17	1513.45
27	28	31.80	524.74	2.17	1510.41
28	28	31.80	527.44	3.12	1511.56
28	29	33.20	527.44	3.12	1507.20
29	29	33.20	529.06	4.55	1508.00
29	30	34.60	529.06	4.55	1501.62
30	30	34.60	529.65	6.31	1502.08
30	31	36.00	529.65	6.31	1493.24
31	31	36.00	529.21	8.22	1493.35
31	32	37.40	529.21	8.22	1481.84
32	32	37.40	527.72	10.12	1481.60
32	33	38.80	527.72	10.12	1467.43
33	33	38.80	525.15	11.83	1466.83
33	34	40.20	525.15	11.83	1450.27
34	34	40.20	521.42	13.18	1449.29
34	35	41.60	521.42	13.18	1430.84
35	35	41.60	516.42	13.97	1429.46
35	36	43.00	516.42	13.97	1409.91
36	36	43.00	510.97	14.07	1408.45
36	37	44.40	510.97	14.07	1388.75
37	37	44.40	504.92	13.45	1387.17
37	38	45.80	504.92	13.45	1368.35
38	38	45.80	499.17	12.12	1367.04
38	39	47.20	499.17	12.12	1350.08
39	39	47.20	493.56	10.21	1349.01
39	40	48.60	493.56	10.21	1334.72
40	40	48.60	488.77	7.90	1334.20
40	41	50.00	488.77	7.90	1323.13
41	1041	50.00	484.66	-7.90	1323.13
41	42	51.40	484.66	-7.90	1334.19
42	42	51.40	481.22	-10.20	1334.72
42	43	52.80	481.22	-10.20	1349.01
43	43	52.80	478.56	-12.12	1350.08
43	44	54.20	478.56	-12.12	1367.04
44	44	54.20	476.00	-13.45	1368.35
44	45	55.60	476.00	-13.45	1387.17
45	45	55.60	473.65	-14.07	1388.74
45	46	57.00	473.65	-14.07	1408.45
46	46	57.00	470.60	-13.96	1409.91
46	47	58.40	470.60	-13.96	1429.46
47	47	58.40	466.95	-13.18	1430.83
47	48	59.80	466.95	-13.18	1449.28
48	48	59.80	461.88	-11.83	1450.26
48	49	61.20	461.88	-11.83	1466.82
49	49	61.20	455.44	-10.12	1467.43
49	50	62.60	455.44	-10.12	1481.59
50	50	62.60	447.66	-8.22	1481.83
50	51	64.00	447.66	-8.22	1493.34
51	51	64.00	438.55	-6.31	1493.23
51	52	65.40	438.55	-6.31	1502.07

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	428.06	-4.55	1501.61
52	53	66.80	428.06	-4.55	1507.99
53	53	66.80	416.12	-3.12	1507.19
53	54	68.20	416.12	-3.12	1511.55
54	54	68.20	402.60	-2.17	1510.41
54	55	69.60	402.60	-2.17	1513.45
55	55	69.60	387.35	-1.90	1511.95
55	56	71.00	387.35	-1.90	1514.61
56	56	71.00	371.11	-2.40	1513.08
56	57	72.40	371.11	-2.40	1516.44
57	57	72.40	353.65	-3.70	1514.87
57	58	73.80	353.65	-3.70	1520.05
58	58	73.80	335.79	-5.73	1518.84
58	59	75.20	335.79	-5.73	1526.87
59	59	75.20	317.25	-8.33	1526.01
59	60	76.60	317.25	-8.33	1537.68
60	60	76.60	298.56	-11.25	1537.49
60	61	78.00	298.56	-11.25	1553.24
61	1061	78.00	284.96	68.58	1553.68
61	62	79.10	284.96	68.58	1478.24
62	62	79.10	275.53	66.49	1479.06
62	63	80.20	275.53	66.49	1405.92
63	63	80.20	265.98	64.77	1407.14
63	64	81.30	265.98	64.77	1335.90
64	64	81.30	256.01	63.52	1337.30
64	65	82.40	256.01	63.52	1267.43
65	65	82.40	245.67	62.80	1268.99
65	66	83.50	245.67	62.80	1199.91
66	66	83.50	234.75	62.64	1201.45
66	67	84.60	234.75	62.64	1132.54
67	67	84.60	223.26	63.03	1134.04
67	68	85.70	223.26	63.03	1064.71
68	68	85.70	211.22	63.94	1066.14
68	69	86.80	211.22	63.94	995.80
69	69	86.80	198.39	65.33	997.02
69	70	87.90	198.39	65.33	925.15
70	70	87.90	184.80	67.10	926.12
70	71	89.00	184.80	67.10	852.31
71	71	89.00	170.42	69.14	853.00
71	72	90.10	170.42	69.14	776.94
72	72	90.10	155.24	71.36	777.31
72	73	91.20	155.24	71.36	698.82
73	73	91.20	139.23	73.62	698.85
73	74	92.30	139.23	73.62	617.86
74	74	92.30	122.36	75.80	617.50
74	75	93.40	122.36	75.80	534.12
75	75	93.40	104.59	77.73	533.35
75	76	94.50	104.59	77.73	447.84
76	76	94.50	85.85	79.23	446.58
76	77	95.60	85.85	79.23	359.43
77	77	95.60	66.31	80.12	357.78

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	66.31	80.12	269.65
78	78	96.70	45.89	80.23	267.56
78	79	97.80	45.89	80.23	179.31
79	79	97.80	24.76	79.38	176.86
79	80	98.90	24.76	79.38	89.54
80	80	98.90	2.82	77.41	86.70
80	81	100.00	2.82	77.41	1.55
101	101	0.00	-498.32	5.00	-1.55
101	102	1.10	-498.32	5.00	-7.05
102	102	1.10	-498.91	6.97	-9.89
102	103	2.20	-498.91	6.97	-17.56
103	103	2.20	-499.72	7.82	-20.01
103	104	3.30	-499.72	7.82	-28.61
104	104	3.30	-500.77	7.71	-30.70
104	105	4.40	-500.77	7.71	-39.18
105	105	4.40	-501.83	6.81	-40.83
105	106	5.50	-501.83	6.81	-48.33
106	106	5.50	-502.90	5.32	-49.59
106	107	6.60	-502.90	5.32	-55.44
107	107	6.60	-503.76	3.39	-56.22
107	108	7.70	-503.76	3.39	-59.95
108	108	7.70	-504.42	1.22	-60.30
108	109	8.80	-504.42	1.22	-61.64
109	109	8.80	-504.88	-1.05	-61.62
109	110	9.90	-504.88	-1.05	-60.46
110	110	9.90	-505.13	-3.26	-60.09
110	111	11.00	-505.13	-3.26	-56.50
111	111	11.00	-505.18	-5.31	-55.82
111	112	12.10	-505.18	-5.31	-49.98
112	112	12.10	-505.02	-7.07	-49.01
112	113	13.20	-505.02	-7.07	-41.23
113	113	13.20	-504.64	-8.46	-40.02
113	114	14.30	-504.64	-8.46	-30.71
114	114	14.30	-504.04	-9.37	-29.28
114	115	15.40	-504.04	-9.37	-18.97
115	115	15.40	-503.42	-9.76	-17.47
115	116	16.50	-503.42	-9.76	-6.73
116	116	16.50	-502.78	-9.60	-5.19
116	117	17.60	-502.78	-9.60	5.37
117	117	17.60	-502.10	-8.88	6.92
117	118	18.70	-502.10	-8.88	16.70
118	118	18.70	-501.60	-7.63	18.10
118	119	19.80	-501.60	-7.63	26.50
119	119	19.80	-501.27	-5.91	27.72
119	120	20.90	-501.27	-5.91	34.22
120	120	20.90	-501.40	-3.82	35.04
120	121	22.00	-501.40	-3.82	39.24
121	1121	22.00	-502.29	-2.31	39.68
121	122	23.40	-502.29	-2.31	42.92
122	122	23.40	-504.66	0.61	42.73
122	123	24.80	-504.66	0.61	41.88

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-508.21	3.20	41.02
123	124	26.20	-508.21	3.20	36.53
124	124	26.20	-512.21	5.24	35.32
124	125	27.60	-512.21	5.24	27.99
125	125	27.60	-516.75	6.54	26.42
125	126	29.00	-516.75	6.54	17.26
126	126	29.00	-520.90	7.04	15.73
126	127	30.40	-520.90	7.04	5.87
127	127	30.40	-524.74	6.77	4.37
127	128	31.80	-524.74	6.77	-5.11
128	128	31.80	-527.44	5.83	-6.25
128	129	33.20	-527.44	5.83	-14.41
129	129	33.20	-529.06	4.39	-15.21
129	130	34.60	-529.06	4.39	-21.36
130	130	34.60	-529.65	2.64	-21.82
130	131	36.00	-529.65	2.64	-25.51
131	131	36.00	-529.21	0.73	-25.62
131	132	37.40	-529.21	0.73	-26.65
132	132	37.40	-527.72	-1.16	-26.41
132	133	38.80	-527.72	-1.16	-24.78
133	133	38.80	-525.15	-2.87	-24.18
133	134	40.20	-525.15	-2.87	-20.16
134	134	40.20	-521.42	-4.22	-19.18
134	135	41.60	-521.42	-4.22	-13.28
135	135	41.60	-516.42	-5.00	-11.90
135	136	43.00	-516.42	-5.00	-4.90
136	136	43.00	-510.97	-5.11	-3.43
136	137	44.40	-510.97	-5.11	3.72
137	137	44.40	-504.92	-4.48	5.29
137	138	45.80	-504.92	-4.48	11.56
138	138	45.80	-499.17	-3.15	12.87
138	139	47.20	-499.17	-3.15	17.28
139	139	47.20	-493.56	-1.24	18.34
139	140	48.60	-493.56	-1.24	20.08
140	140	48.60	-488.77	1.07	20.60
140	141	50.00	-488.77	1.07	19.11
141	1141	50.00	-484.65	-1.07	19.11
141	142	51.40	-484.65	-1.07	20.60
142	142	51.40	-481.22	1.24	20.07
142	143	52.80	-481.22	1.24	18.34
143	143	52.80	-478.56	3.15	17.28
143	144	54.20	-478.56	3.15	12.87
144	144	54.20	-476.00	4.48	11.56
144	145	55.60	-476.00	4.48	5.29
145	145	55.60	-473.65	5.11	3.71
145	146	57.00	-473.65	5.11	-3.44
146	146	57.00	-470.60	5.00	-4.90
146	147	58.40	-470.60	5.00	-11.90
147	147	58.40	-466.95	4.22	-13.28
147	148	59.80	-466.95	4.22	-19.18
148	148	59.80	-461.88	2.87	-20.16

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-461.88	2.87	-24.18
149	149	61.20	-455.44	1.16	-24.79
149	150	62.60	-455.44	1.16	-26.41
150	150	62.60	-447.66	-0.73	-26.65
150	151	64.00	-447.66	-0.73	-25.63
151	151	64.00	-438.55	-2.64	-25.52
151	152	65.40	-438.55	-2.64	-21.82
152	152	65.40	-428.06	-4.39	-21.37
152	153	66.80	-428.06	-4.39	-15.21
153	153	66.80	-416.12	-5.83	-14.41
153	154	68.20	-416.12	-5.83	-6.26
154	154	68.20	-402.60	-6.77	-5.11
154	155	69.60	-402.60	-6.77	4.37
155	155	69.60	-387.35	-7.04	5.87
155	156	71.00	-387.35	-7.04	15.73
156	156	71.00	-371.11	-6.54	17.26
156	157	72.40	-371.11	-6.54	26.42
157	157	72.40	-353.65	-5.24	27.99
157	158	73.80	-353.65	-5.24	35.32
158	158	73.80	-335.79	-3.21	36.53
158	159	75.20	-335.79	-3.21	41.02
159	159	75.20	-317.25	-0.61	41.88
159	160	76.60	-317.25	-0.61	42.73
160	160	76.60	-298.56	2.31	42.92
160	161	78.00	-298.56	2.31	39.68
161	1161	78.00	-284.96	3.82	39.25
161	162	79.10	-284.96	3.82	35.04
162	162	79.10	-275.53	5.91	34.22
162	163	80.20	-275.53	5.91	27.72
163	163	80.20	-265.97	7.63	26.50
163	164	81.30	-265.97	7.63	18.10
164	164	81.30	-256.01	8.89	16.70
164	165	82.40	-256.01	8.89	6.92
165	165	82.40	-245.67	9.60	5.37
165	166	83.50	-245.67	9.60	-5.19
166	166	83.50	-234.75	9.76	-6.73
166	167	84.60	-234.75	9.76	-17.47
167	167	84.60	-223.26	9.37	-18.97
167	168	85.70	-223.26	9.37	-29.28
168	168	85.70	-211.21	8.46	-30.71
168	169	86.80	-211.21	8.46	-40.02
169	169	86.80	-198.39	7.07	-41.23
169	170	87.90	-198.39	7.07	-49.02
170	170	87.90	-184.80	5.31	-49.98
170	171	89.00	-184.80	5.31	-55.82
171	171	89.00	-170.42	3.26	-56.50
171	172	90.10	-170.42	3.26	-60.09
172	172	90.10	-155.24	1.05	-60.47
172	173	91.20	-155.24	1.05	-61.62
173	173	91.20	-139.23	-1.22	-61.65
173	174	92.30	-139.23	-1.22	-60.31

CÁLCULO TENSIONAL

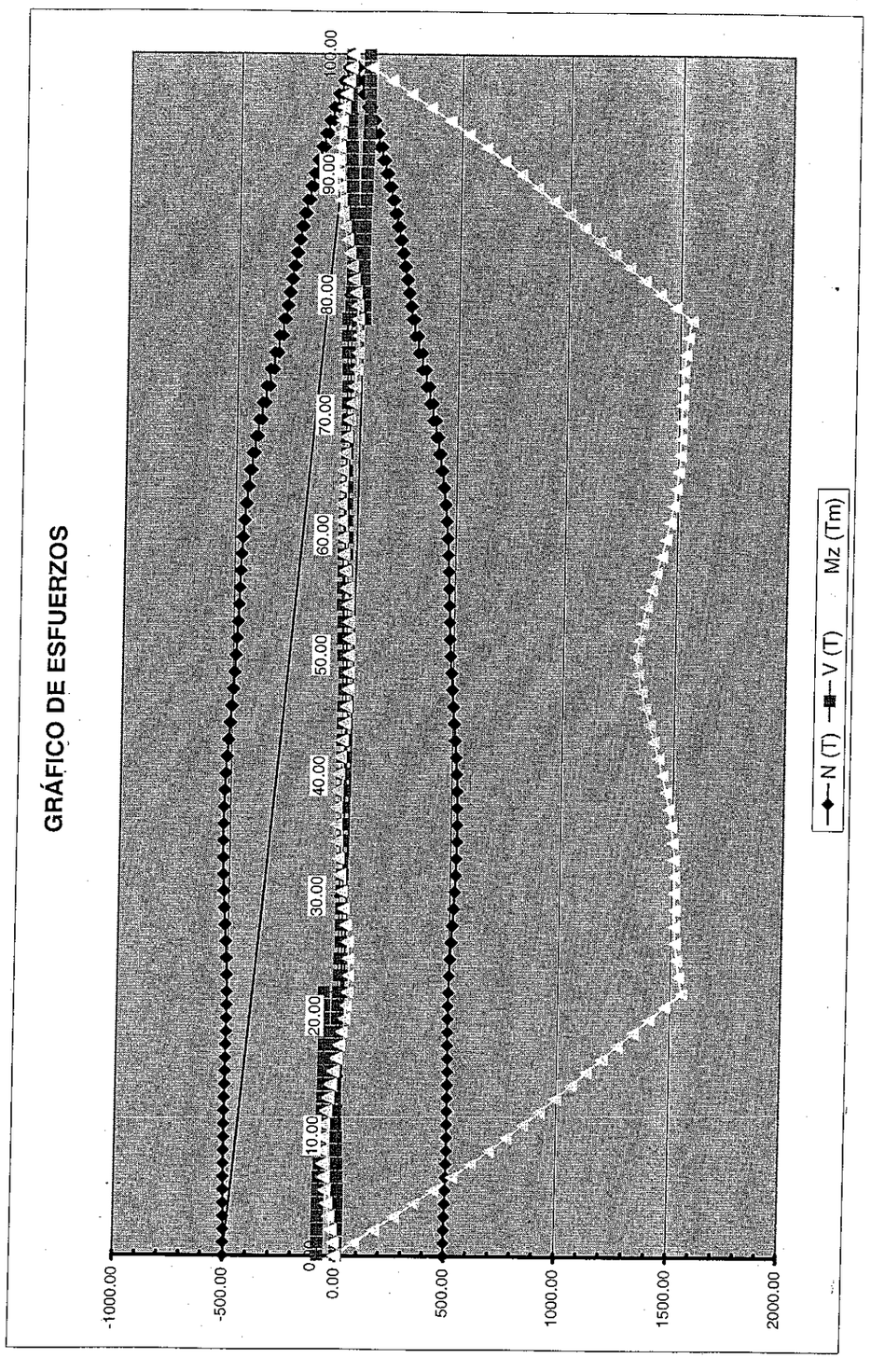
Hipótesis de cálculo:
ej1preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-122.36	-3.39	-59.95
174	175	93.40	-122.36	-3.39	-56.22
175	175	93.40	-104.59	-5.32	-55.44
175	176	94.50	-104.59	-5.32	-49.60
176	176	94.50	-85.85	-6.82	-48.33
176	177	95.60	-85.85	-6.82	-40.84
177	177	95.60	-66.31	-7.71	-39.18
177	178	96.70	-66.31	-7.71	-30.71
178	178	96.70	-45.89	-7.82	-28.61
178	179	97.80	-45.89	-7.82	-20.01
179	179	97.80	-24.76	-6.97	-17.56
179	180	98.90	-24.76	-6.97	-9.90
180	180	98.90	-2.82	-5.00	-7.05
180	181	100.00	-2.82	-5.00	-1.55



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	498.32	-77.41	1.55
1	2	1.10	498.32	-77.41	86.70
2	2	1.10	498.90	-79.38	89.55
2	3	2.20	498.90	-79.38	176.87
3	3	2.20	499.72	-80.23	179.32
3	4	3.30	499.72	-80.23	267.57
4	4	3.30	500.77	-80.12	269.66
4	5	4.40	500.77	-80.12	357.80
5	5	4.40	501.83	-79.23	359.45
5	6	5.50	501.83	-79.23	446.60
6	6	5.50	502.90	-77.73	447.87
6	7	6.60	502.90	-77.73	533.37
7	7	6.60	503.76	-75.80	534.15
7	8	7.70	503.76	-75.80	617.53
8	8	7.70	504.42	-73.63	617.88
8	9	8.80	504.42	-73.63	698.88
9	9	8.80	504.87	-71.36	698.85
9	10	9.90	504.87	-71.36	777.35
10	10	9.90	505.13	-69.14	776.97
10	11	11.00	505.13	-69.14	853.03
11	11	11.00	505.18	-67.09	852.34
11	12	12.10	505.18	-67.09	926.15
12	12	12.10	505.02	-65.33	925.18
12	13	13.20	505.02	-65.33	997.04
13	13	13.20	504.64	-63.94	995.83
13	14	14.30	504.64	-63.94	1066.17
14	14	14.30	504.04	-63.03	1064.73
14	15	15.40	504.04	-63.03	1134.06
15	15	15.40	503.42	-62.64	1132.56
15	16	16.50	503.42	-62.64	1201.46
16	16	16.50	502.78	-62.80	1199.92
16	17	17.60	502.78	-62.80	1268.99
17	17	17.60	502.10	-63.51	1267.44
17	18	18.70	502.10	-63.51	1337.30
18	18	18.70	501.60	-64.76	1335.90
18	19	19.80	501.60	-64.76	1407.14
19	19	19.80	501.27	-66.49	1405.92
19	20	20.90	501.27	-66.49	1479.06
20	20	20.90	501.40	-68.58	1478.24
20	21	22.00	501.40	-68.58	1553.67
21	1021	22.00	502.29	11.25	1553.24
21	22	23.40	502.29	11.25	1537.48
22	22	23.40	504.66	8.33	1537.67
22	23	24.80	504.66	8.33	1526.01
23	23	24.80	508.21	5.73	1526.87
23	24	26.20	508.21	5.73	1518.84
24	24	26.20	512.21	3.70	1520.05
24	25	27.60	512.21	3.70	1514.88
25	25	27.60	516.75	2.40	1516.44
25	26	29.00	516.75	2.40	1513.08
26	26	29.00	520.90	1.90	1514.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	520.90	1.90	1511.95
27	27	30.40	524.74	2.17	1513.45
27	28	31.80	524.74	2.17	1510.41
28	28	31.80	527.44	3.12	1511.56
28	29	33.20	527.44	3.12	1507.20
29	29	33.20	529.06	4.55	1508.00
29	30	34.60	529.06	4.55	1501.62
30	30	34.60	529.65	6.31	1502.08
30	31	36.00	529.65	6.31	1493.24
31	31	36.00	529.21	8.22	1493.35
31	32	37.40	529.21	8.22	1481.84
32	32	37.40	527.72	10.12	1481.60
32	33	38.80	527.72	10.12	1467.43
33	33	38.80	525.15	11.83	1466.83
33	34	40.20	525.15	11.83	1450.27
34	34	40.20	521.42	13.18	1449.29
34	35	41.60	521.42	13.18	1430.84
35	35	41.60	516.42	13.97	1429.46
35	36	43.00	516.42	13.97	1409.91
36	36	43.00	510.97	14.07	1408.45
36	37	44.40	510.97	14.07	1388.75
37	37	44.40	504.92	13.45	1387.17
37	38	45.80	504.92	13.45	1368.35
38	38	45.80	499.17	12.12	1367.04
38	39	47.20	499.17	12.12	1350.08
39	39	47.20	493.56	10.21	1349.01
39	40	48.60	493.56	10.21	1334.72
40	40	48.60	488.77	7.90	1334.20
40	41	50.00	488.77	7.90	1323.13
41	1041	50.00	484.66	-7.90	1323.13
41	42	51.40	484.66	-7.90	1334.19
42	42	51.40	481.22	-10.20	1334.72
42	43	52.80	481.22	-10.20	1349.01
43	43	52.80	478.56	-12.12	1350.08
43	44	54.20	478.56	-12.12	1367.04
44	44	54.20	476.00	-13.45	1368.35
44	45	55.60	476.00	-13.45	1387.17
45	45	55.60	473.65	-14.07	1388.74
45	46	57.00	473.65	-14.07	1408.45
46	46	57.00	470.60	-13.96	1409.91
46	47	58.40	470.60	-13.96	1429.46
47	47	58.40	466.95	-13.18	1430.83
47	48	59.80	466.95	-13.18	1449.28
48	48	59.80	461.88	-11.83	1450.26
48	49	61.20	461.88	-11.83	1466.82
49	49	61.20	455.44	-10.12	1467.43
49	50	62.60	455.44	-10.12	1481.59
50	50	62.60	447.66	-8.22	1481.83
50	51	64.00	447.66	-8.22	1493.34
51	51	64.00	438.55	-6.31	1493.23
51	52	65.40	438.55	-6.31	1502.07

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	428.06	-4.55	1501.61
52	53	66.80	428.06	-4.55	1507.99
53	53	66.80	416.12	-3.12	1507.19
53	54	68.20	416.12	-3.12	1511.55
54	54	68.20	402.60	-2.17	1510.41
54	55	69.60	402.60	-2.17	1513.45
55	55	69.60	387.35	-1.90	1511.95
55	56	71.00	387.35	-1.90	1514.61
56	56	71.00	371.11	-2.40	1513.08
56	57	72.40	371.11	-2.40	1516.44
57	57	72.40	353.65	-3.70	1514.87
57	58	73.80	353.65	-3.70	1520.05
58	58	73.80	335.79	-5.73	1518.84
58	59	75.20	335.79	-5.73	1526.87
59	59	75.20	317.25	-8.33	1526.01
59	60	76.60	317.25	-8.33	1537.68
60	60	76.60	298.56	-11.25	1537.49
60	61	78.00	298.56	-11.25	1553.24
61	1061	78.00	284.96	68.58	1553.68
61	62	79.10	284.96	68.58	1478.24
62	62	79.10	275.53	66.49	1479.06
62	63	80.20	275.53	66.49	1405.92
63	63	80.20	265.98	64.77	1407.14
63	64	81.30	265.98	64.77	1335.90
64	64	81.30	256.01	63.52	1337.30
64	65	82.40	256.01	63.52	1267.43
65	65	82.40	245.67	62.80	1268.99
65	66	83.50	245.67	62.80	1199.91
66	66	83.50	234.75	62.64	1201.45
66	67	84.60	234.75	62.64	1132.54
67	67	84.60	223.26	63.03	1134.04
67	68	85.70	223.26	63.03	1064.71
68	68	85.70	211.22	63.94	1066.14
68	69	86.80	211.22	63.94	995.80
69	69	86.80	198.39	65.33	997.02
69	70	87.90	198.39	65.33	925.15
70	70	87.90	184.80	67.10	926.12
70	71	89.00	184.80	67.10	852.31
71	71	89.00	170.42	69.14	853.00
71	72	90.10	170.42	69.14	776.94
72	72	90.10	155.24	71.36	777.31
72	73	91.20	155.24	71.36	698.82
73	73	91.20	139.23	73.62	698.85
73	74	92.30	139.23	73.62	617.86
74	74	92.30	122.36	75.80	617.50
74	75	93.40	122.36	75.80	534.12
75	75	93.40	104.59	77.73	533.35
75	76	94.50	104.59	77.73	447.84
76	76	94.50	85.85	79.23	446.58
76	77	95.60	85.85	79.23	359.43
77	77	95.60	66.31	80.12	357.78

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	66.31	80.12	269.65
78	78	96.70	45.89	80.23	267.56
78	79	97.80	45.89	80.23	179.31
79	79	97.80	24.76	79.38	176.86
79	80	98.90	24.76	79.38	89.54
80	80	98.90	2.82	77.41	86.70
80	81	100.00	2.82	77.41	1.55
101	101	0.00	-498.32	5.00	-1.55
101	102	1.10	-498.32	5.00	-7.05
102	102	1.10	-498.91	6.97	-9.89
102	103	2.20	-498.91	6.97	-17.56
103	103	2.20	-499.72	7.82	-20.01
103	104	3.30	-499.72	7.82	-28.61
104	104	3.30	-500.77	7.71	-30.70
104	105	4.40	-500.77	7.71	-39.18
105	105	4.40	-501.83	6.81	-40.83
105	106	5.50	-501.83	6.81	-48.33
106	106	5.50	-502.90	5.32	-49.59
106	107	6.60	-502.90	5.32	-55.44
107	107	6.60	-503.76	3.39	-56.22
107	108	7.70	-503.76	3.39	-59.95
108	108	7.70	-504.42	1.22	-60.30
108	109	8.80	-504.42	1.22	-61.64
109	109	8.80	-504.88	-1.05	-61.62
109	110	9.90	-504.88	-1.05	-60.46
110	110	9.90	-505.13	-3.26	-60.09
110	111	11.00	-505.13	-3.26	-56.50
111	111	11.00	-505.18	-5.31	-55.82
111	112	12.10	-505.18	-5.31	-49.98
112	112	12.10	-505.02	-7.07	-49.01
112	113	13.20	-505.02	-7.07	-41.23
113	113	13.20	-504.64	-8.46	-40.02
113	114	14.30	-504.64	-8.46	-30.71
114	114	14.30	-504.04	-9.37	-29.28
114	115	15.40	-504.04	-9.37	-18.97
115	115	15.40	-503.42	-9.76	-17.47
115	116	16.50	-503.42	-9.76	-6.73
116	116	16.50	-502.78	-9.60	-5.19
116	117	17.60	-502.78	-9.60	5.37
117	117	17.60	-502.10	-8.88	6.92
117	118	18.70	-502.10	-8.88	16.70
118	118	18.70	-501.60	-7.63	18.10
118	119	19.80	-501.60	-7.63	26.50
119	119	19.80	-501.27	-5.91	27.72
119	120	20.90	-501.27	-5.91	34.22
120	120	20.90	-501.40	-3.82	35.04
120	121	22.00	-501.40	-3.82	39.24
121	1121	22.00	-502.29	-2.31	39.68
121	122	23.40	-502.29	-2.31	42.92
122	122	23.40	-504.66	0.61	42.73
122	123	24.80	-504.66	0.61	41.88

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej1preEl.HIP.Tinf

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-508.21	3.20	41.02
123	124	26.20	-508.21	3.20	36.53
124	124	26.20	-512.21	5.24	35.32
124	125	27.60	-512.21	5.24	27.99
125	125	27.60	-516.75	6.54	26.42
125	126	29.00	-516.75	6.54	17.26
126	126	29.00	-520.90	7.04	15.73
126	127	30.40	-520.90	7.04	5.87
127	127	30.40	-524.74	6.77	4.37
127	128	31.80	-524.74	6.77	-5.11
128	128	31.80	-527.44	5.83	-6.25
128	129	33.20	-527.44	5.83	-14.41
129	129	33.20	-529.06	4.39	-15.21
129	130	34.60	-529.06	4.39	-21.36
130	130	34.60	-529.65	2.64	-21.82
130	131	36.00	-529.65	2.64	-25.51
131	131	36.00	-529.21	0.73	-25.62
131	132	37.40	-529.21	0.73	-26.65
132	132	37.40	-527.72	-1.16	-26.41
132	133	38.80	-527.72	-1.16	-24.78
133	133	38.80	-525.15	-2.87	-24.18
133	134	40.20	-525.15	-2.87	-20.16
134	134	40.20	-521.42	-4.22	-19.18
134	135	41.60	-521.42	-4.22	-13.28
135	135	41.60	-516.42	-5.00	-11.90
135	136	43.00	-516.42	-5.00	-4.90
136	136	43.00	-510.97	-5.11	-3.43
136	137	44.40	-510.97	-5.11	3.72
137	137	44.40	-504.92	-4.48	5.29
137	138	45.80	-504.92	-4.48	11.56
138	138	45.80	-499.17	-3.15	12.87
138	139	47.20	-499.17	-3.15	17.28
139	139	47.20	-493.56	-1.24	18.34
139	140	48.60	-493.56	-1.24	20.08
140	140	48.60	-488.77	1.07	20.60
140	141	50.00	-488.77	1.07	19.11
141	1141	50.00	-484.65	-1.07	19.11
141	142	51.40	-484.65	-1.07	20.60
142	142	51.40	-481.22	1.24	20.07
142	143	52.80	-481.22	1.24	18.34
143	143	52.80	-478.56	3.15	17.28
143	144	54.20	-478.56	3.15	12.87
144	144	54.20	-476.00	4.48	11.56
144	145	55.60	-476.00	4.48	5.29
145	145	55.60	-473.65	5.11	3.71
145	146	57.00	-473.65	5.11	-3.44
146	146	57.00	-470.60	5.00	-4.90
146	147	58.40	-470.60	5.00	-11.90
147	147	58.40	-466.95	4.22	-13.28
147	148	59.80	-466.95	4.22	-19.18
148	148	59.80	-461.88	2.87	-20.16

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-461.88	2.87	-24.18
149	149	61.20	-455.44	1.16	-24.79
149	150	62.60	-455.44	1.16	-26.41
150	150	62.60	-447.66	-0.73	-26.65
150	151	64.00	-447.66	-0.73	-25.63
151	151	64.00	-438.55	-2.64	-25.52
151	152	65.40	-438.55	-2.64	-21.82
152	152	65.40	-428.06	-4.39	-21.37
152	153	66.80	-428.06	-4.39	-15.21
153	153	66.80	-416.12	-5.83	-14.41
153	154	68.20	-416.12	-5.83	-6.26
154	154	68.20	-402.60	-6.77	-5.11
154	155	69.60	-402.60	-6.77	4.37
155	155	69.60	-387.35	-7.04	5.87
155	156	71.00	-387.35	-7.04	15.73
156	156	71.00	-371.11	-6.54	17.26
156	157	72.40	-371.11	-6.54	26.42
157	157	72.40	-353.65	-5.24	27.99
157	158	73.80	-353.65	-5.24	35.32
158	158	73.80	-335.79	-3.21	36.53
158	159	75.20	-335.79	-3.21	41.02
159	159	75.20	-317.25	-0.61	41.88
159	160	76.60	-317.25	-0.61	42.73
160	160	76.60	-298.56	2.31	42.92
160	161	78.00	-298.56	2.31	39.68
161	1161	78.00	-284.96	3.82	39.25
161	162	79.10	-284.96	3.82	35.04
162	162	79.10	-275.53	5.91	34.22
162	163	80.20	-275.53	5.91	27.72
163	163	80.20	-265.97	7.63	26.50
163	164	81.30	-265.97	7.63	18.10
164	164	81.30	-256.01	8.89	16.70
164	165	82.40	-256.01	8.89	6.92
165	165	82.40	-245.67	9.60	5.37
165	166	83.50	-245.67	9.60	-5.19
166	166	83.50	-234.75	9.76	-6.73
166	167	84.60	-234.75	9.76	-17.47
167	167	84.60	-223.26	9.37	-18.97
167	168	85.70	-223.26	9.37	-29.28
168	168	85.70	-211.21	8.46	-30.71
168	169	86.80	-211.21	8.46	-40.02
169	169	86.80	-198.39	7.07	-41.23
169	170	87.90	-198.39	7.07	-49.02
170	170	87.90	-184.80	5.31	-49.98
170	171	89.00	-184.80	5.31	-55.82
171	171	89.00	-170.42	3.26	-56.50
171	172	90.10	-170.42	3.26	-60.09
172	172	90.10	-155.24	1.05	-60.47
172	173	91.20	-155.24	1.05	-61.62
173	173	91.20	-139.23	-1.22	-61.65
173	174	92.30	-139.23	-1.22	-60.31

CÁLCULO TENSIONAL

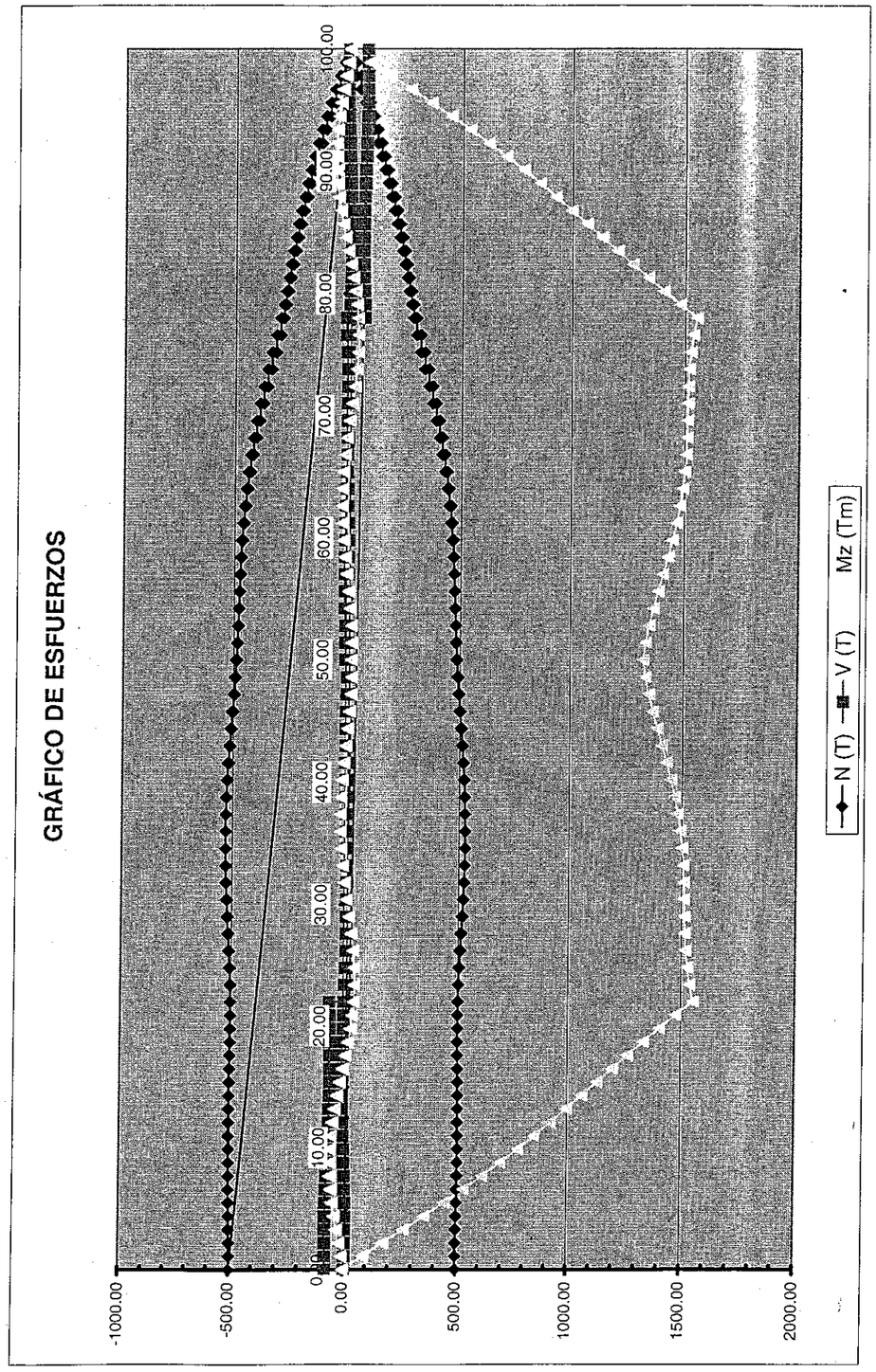
Hipótesis de cálculo:
ej1preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [-1;-1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.TOT + [-1;-1]ej1preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-122.36	-3.39	-59.95
174	175	93.40	-122.36	-3.39	-56.22
175	175	93.40	-104.59	-5.32	-55.44
175	176	94.50	-104.59	-5.32	-49.60
176	176	94.50	-85.85	-6.82	-48.33
176	177	95.60	-85.85	-6.82	-40.84
177	177	95.60	-66.31	-7.71	-39.18
177	178	96.70	-66.31	-7.71	-30.71
178	178	96.70	-45.89	-7.82	-28.61
178	179	97.80	-45.89	-7.82	-20.01
179	179	97.80	-24.76	-6.97	-17.56
179	180	98.90	-24.76	-6.97	-9.90
180	180	98.90	-2.82	-5.00	-7.05
180	181	100.00	-2.82	-5.00	-1.55



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEI.FAM1.ISO + [1; 1]ej1preEI.FAM2.ISO + [1; 1]ej1preEI.FAM3.ISO + [1; 1]ej1preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-497.28	0.00	-569.72
1	2	1.10	-497.28	0.00	-569.72
2	2	1.10	-787.36	0.00	-975.54
2	3	2.20	-787.36	0.00	-975.54
3	3	2.20	-787.36	0.00	-975.54
3	4	3.30	-787.36	0.00	-975.54
4	4	3.30	-994.56	0.00	-1261.27
4	5	4.40	-994.56	0.00	-1261.27
5	5	4.40	-994.56	0.00	-1261.27
5	6	5.50	-994.56	0.00	-1261.27
6	6	5.50	-1201.76	0.00	-1544.93
6	7	6.60	-1201.76	0.00	-1544.93
7	7	6.60	-1201.76	0.00	-1544.93
7	8	7.70	-1201.76	0.00	-1544.93
8	8	7.70	-1201.76	0.00	-1544.93
8	9	8.80	-1201.76	0.00	-1544.93
9	9	8.80	-1201.76	0.00	-1544.93
9	10	9.90	-1201.76	0.00	-1544.93
10	10	9.90	-1201.76	0.00	-1544.93
10	11	11.00	-1201.76	0.00	-1544.93
11	11	11.00	-1201.76	0.00	-1544.93
11	12	12.10	-1201.76	0.00	-1544.93
12	12	12.10	-1201.76	0.00	-1544.93
12	13	13.20	-1201.76	0.00	-1544.93
13	13	13.20	-1201.76	0.00	-1544.93
13	14	14.30	-1201.76	0.00	-1544.93
14	14	14.30	-994.56	0.00	-1261.27
14	15	15.40	-994.56	0.00	-1261.27
15	15	15.40	-994.56	0.00	-1261.27
15	16	16.50	-994.56	0.00	-1261.27
16	16	16.50	-994.56	0.00	-1261.27
16	17	17.60	-994.56	0.00	-1261.68
17	17	17.60	-787.36	0.00	-975.54
17	18	18.70	-787.36	0.00	-975.54
18	18	18.70	-787.36	0.00	-975.54
18	19	19.80	-787.36	0.00	-975.54
19	19	19.80	-497.28	0.00	-569.72
19	20	20.90	-497.28	0.00	-569.72
20	20	20.90	-497.28	0.00	-569.72
20	21	22.00	-497.28	0.00	-569.72
21	1021	22.00	-538.72	0.00	-628.93
21	22	23.40	-538.72	0.00	-628.93
22	22	23.40	-538.72	0.00	-628.93
22	23	24.80	-538.72	0.00	-628.93
23	23	24.80	-828.80	0.00	-1031.86
23	24	26.20	-828.80	0.00	-1031.86
24	24	26.20	-828.80	0.00	-1031.86
24	25	27.60	-828.80	0.00	-1031.86
25	25	27.60	-1201.76	0.00	-1538.71
25	26	29.00	-1201.76	0.00	-1538.71
26	26	29.00	-1201.76	0.00	-1538.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-1533.28	0.00	-1982.61
52	53	66.80	-1533.28	0.00	-1982.61
53	53	66.80	-1533.28	0.00	-1982.61
53	54	68.20	-1533.28	0.00	-1982.61
54	54	68.20	-1533.28	0.00	-1982.61
54	55	69.60	-1533.28	0.00	-1982.61
55	55	69.60	-1201.76	0.00	-1538.71
55	56	71.00	-1201.76	0.00	-1538.71
56	56	71.00	-1201.76	0.00	-1538.71
56	57	72.40	-1201.76	0.00	-1538.71
57	57	72.40	-828.80	0.00	-1031.86
57	58	73.80	-828.80	0.00	-1031.86
58	58	73.80	-828.80	0.00	-1031.86
58	59	75.20	-828.80	0.00	-1031.86
59	59	75.20	-538.72	0.00	-628.93
59	60	76.60	-538.72	0.00	-628.93
60	60	76.60	-538.72	0.00	-628.93
60	61	78.00	-538.72	0.00	-628.93
61	1061	78.00	-497.28	0.00	-569.72
61	62	79.10	-497.28	0.00	-569.72
62	62	79.10	-497.28	0.00	-569.72
62	63	80.20	-497.28	0.00	-569.72
63	63	80.20	-787.36	0.00	-975.54
63	64	81.30	-787.36	0.00	-975.54
64	64	81.30	-787.36	0.00	-975.54
64	65	82.40	-787.36	0.00	-975.54
65	65	82.40	-994.56	0.00	-1261.27
65	66	83.50	-994.56	0.00	-1261.27
66	66	83.50	-994.56	0.00	-1261.27
66	67	84.60	-994.56	0.00	-1261.27
67	67	84.60	-994.56	0.00	-1261.27
67	68	85.70	-994.56	0.00	-1261.27
68	68	85.70	-1201.76	0.00	-1544.93
68	69	86.80	-1201.76	0.00	-1544.93
69	69	86.80	-1201.76	0.00	-1544.93
69	70	87.90	-1201.76	0.00	-1544.93
70	70	87.90	-1201.76	0.00	-1544.93
70	71	89.00	-1201.76	0.00	-1544.93
71	71	89.00	-1201.76	0.00	-1544.93
71	72	90.10	-1201.76	0.00	-1544.93
72	72	90.10	-1201.76	0.00	-1544.93
72	73	91.20	-1201.76	0.00	-1544.93
73	73	91.20	-1201.76	0.00	-1544.93
73	74	92.30	-1201.76	0.00	-1544.93
74	74	92.30	-1201.76	0.00	-1544.93
74	75	93.40	-1201.76	0.00	-1544.93
75	75	93.40	-1201.76	0.00	-1544.93
75	76	94.50	-1201.76	0.00	-1544.93
76	76	94.50	-994.56	0.00	-1261.27
76	77	95.60	-994.56	0.00	-1261.27
77	77	95.60	-994.56	0.00	-1261.27

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-994.56	0.00	-1261.27
78	78	96.70	-787.36	0.00	-975.54
78	79	97.80	-787.36	0.00	-975.54
79	79	97.80	-787.36	0.00	-975.54
79	80	98.90	-787.36	0.00	-975.54
80	80	98.90	-497.28	0.00	-569.72
80	81	100.00	-497.28	0.00	-569.72
101	101	0.00	0.00	0.00	0.00
101	102	0.00	0.00	0.00	0.00
102	102	0.00	0.00	0.00	0.00
102	103	0.00	0.00	0.00	0.00
103	103	0.00	0.00	0.00	0.00
103	104	0.00	0.00	0.00	0.00
104	104	0.00	0.00	0.00	0.00
104	105	0.00	0.00	0.00	0.00
105	105	0.00	0.00	0.00	0.00
105	106	0.00	0.00	0.00	0.00
106	106	0.00	0.00	0.00	0.00
106	107	0.00	0.00	0.00	0.00
107	107	0.00	0.00	0.00	0.00
107	108	0.00	0.00	0.00	0.00
108	108	0.00	0.00	0.00	0.00
108	109	0.00	0.00	0.00	0.00
109	109	0.00	0.00	0.00	0.00
109	110	0.00	0.00	0.00	0.00
110	110	0.00	0.00	0.00	0.00
110	111	0.00	0.00	0.00	0.00
111	111	0.00	0.00	0.00	0.00
111	112	0.00	0.00	0.00	0.00
112	112	0.00	0.00	0.00	0.00
112	113	0.00	0.00	0.00	0.00
113	113	0.00	0.00	0.00	0.00
113	114	0.00	0.00	0.00	0.00
114	114	0.00	0.00	0.00	0.00
114	115	0.00	0.00	0.00	0.00
115	115	0.00	0.00	0.00	0.00
115	116	0.00	0.00	0.00	0.00
116	116	0.00	0.00	0.00	0.00
116	117	0.00	0.00	0.00	0.00
117	117	0.00	0.00	0.00	0.00
117	118	0.00	0.00	0.00	0.00
118	118	0.00	0.00	0.00	0.00
118	119	0.00	0.00	0.00	0.00
119	119	0.00	0.00	0.00	0.00
119	120	0.00	0.00	0.00	0.00
120	120	0.00	0.00	0.00	0.00
120	121	0.00	0.00	0.00	0.00
121	1121	0.00	0.00	0.00	0.00
121	122	0.00	0.00	0.00	0.00
122	122	0.00	0.00	0.00	0.00
122	123	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	0.00	0.00	0.00	0.00
123	124	0.00	0.00	0.00	0.00
124	124	0.00	0.00	0.00	0.00
124	125	0.00	0.00	0.00	0.00
125	125	0.00	0.00	0.00	0.00
125	126	0.00	0.00	0.00	0.00
126	126	0.00	0.00	0.00	0.00
126	127	0.00	0.00	0.00	0.00
127	127	0.00	0.00	0.00	0.00
127	128	0.00	0.00	0.00	0.00
128	128	0.00	0.00	0.00	0.00
128	129	0.00	0.00	0.00	0.00
129	129	0.00	0.00	0.00	0.00
129	130	0.00	0.00	0.00	0.00
130	130	0.00	0.00	0.00	0.00
130	131	0.00	0.00	0.00	0.00
131	131	0.00	0.00	0.00	0.00
131	132	0.00	0.00	0.00	0.00
132	132	0.00	0.00	0.00	0.00
132	133	0.00	0.00	0.00	0.00
133	133	0.00	0.00	0.00	0.00
133	134	0.00	0.00	0.00	0.00
134	134	0.00	0.00	0.00	0.00
134	135	0.00	0.00	0.00	0.00
135	135	0.00	0.00	0.00	0.00
135	136	0.00	0.00	0.00	0.00
136	136	0.00	0.00	0.00	0.00
136	137	0.00	0.00	0.00	0.00
137	137	0.00	0.00	0.00	0.00
137	138	0.00	0.00	0.00	0.00
138	138	0.00	0.00	0.00	0.00
138	139	0.00	0.00	0.00	0.00
139	139	0.00	0.00	0.00	0.00
139	140	0.00	0.00	0.00	0.00
140	140	0.00	0.00	0.00	0.00
140	141	0.00	0.00	0.00	0.00
141	1141	0.00	0.00	0.00	0.00
141	142	0.00	0.00	0.00	0.00
142	142	0.00	0.00	0.00	0.00
142	143	0.00	0.00	0.00	0.00
143	143	0.00	0.00	0.00	0.00
143	144	0.00	0.00	0.00	0.00
144	144	0.00	0.00	0.00	0.00
144	145	0.00	0.00	0.00	0.00
145	145	0.00	0.00	0.00	0.00
145	146	0.00	0.00	0.00	0.00
146	146	0.00	0.00	0.00	0.00
146	147	0.00	0.00	0.00	0.00
147	147	0.00	0.00	0.00	0.00
147	148	0.00	0.00	0.00	0.00
148	148	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	0.00	0.00	0.00	0.00
149	149	0.00	0.00	0.00	0.00
149	150	0.00	0.00	0.00	0.00
150	150	0.00	0.00	0.00	0.00
150	151	0.00	0.00	0.00	0.00
151	151	0.00	0.00	0.00	0.00
151	152	0.00	0.00	0.00	0.00
152	152	0.00	0.00	0.00	0.00
152	153	0.00	0.00	0.00	0.00
153	153	0.00	0.00	0.00	0.00
153	154	0.00	0.00	0.00	0.00
154	154	0.00	0.00	0.00	0.00
154	155	0.00	0.00	0.00	0.00
155	155	0.00	0.00	0.00	0.00
155	156	0.00	0.00	0.00	0.00
156	156	0.00	0.00	0.00	0.00
156	157	0.00	0.00	0.00	0.00
157	157	0.00	0.00	0.00	0.00
157	158	0.00	0.00	0.00	0.00
158	158	0.00	0.00	0.00	0.00
157	158	0.00	0.00	0.00	0.00
158	158	0.00	0.00	0.00	0.00
158	159	0.00	0.00	0.00	0.00
159	159	0.00	0.00	0.00	0.00
159	160	0.00	0.00	0.00	0.00
160	160	0.00	0.00	0.00	0.00
160	161	0.00	0.00	0.00	0.00
161	1161	0.00	0.00	0.00	0.00
161	162	0.00	0.00	0.00	0.00
162	162	0.00	0.00	0.00	0.00
162	163	0.00	0.00	0.00	0.00
163	163	0.00	0.00	0.00	0.00
163	164	0.00	0.00	0.00	0.00
164	164	0.00	0.00	0.00	0.00
164	165	0.00	0.00	0.00	0.00
165	165	0.00	0.00	0.00	0.00
165	166	0.00	0.00	0.00	0.00
166	166	0.00	0.00	0.00	0.00
166	167	0.00	0.00	0.00	0.00
167	167	0.00	0.00	0.00	0.00
167	168	0.00	0.00	0.00	0.00
168	168	0.00	0.00	0.00	0.00
168	169	0.00	0.00	0.00	0.00
169	169	0.00	0.00	0.00	0.00
169	170	0.00	0.00	0.00	0.00
170	170	0.00	0.00	0.00	0.00
170	171	0.00	0.00	0.00	0.00
171	171	0.00	0.00	0.00	0.00
171	172	0.00	0.00	0.00	0.00
172	172	0.00	0.00	0.00	0.00
172	173	0.00	0.00	0.00	0.00
173	173	0.00	0.00	0.00	0.00
173	174	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

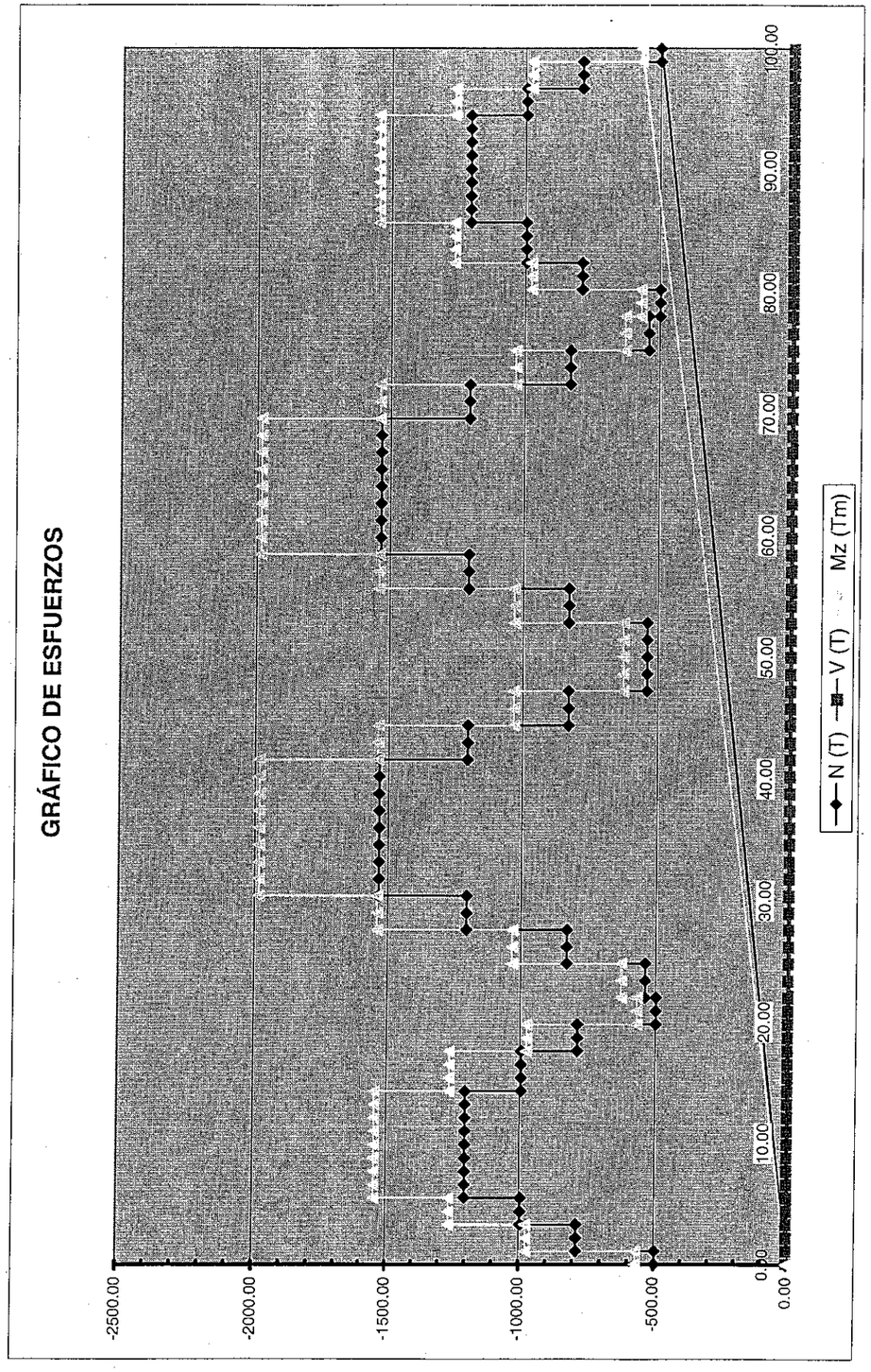
Hipótesis de cálculo:
ej1preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	0.00	0.00	0.00	0.00
174	175	0.00	0.00	0.00	0.00
175	175	0.00	0.00	0.00	0.00
175	176	0.00	0.00	0.00	0.00
176	176	0.00	0.00	0.00	0.00
176	177	0.00	0.00	0.00	0.00
177	177	0.00	0.00	0.00	0.00
177	178	0.00	0.00	0.00	0.00
178	178	0.00	0.00	0.00	0.00
178	179	0.00	0.00	0.00	0.00
179	179	0.00	0.00	0.00	0.00
179	180	0.00	0.00	0.00	0.00
180	180	0.00	0.00	0.00	0.00
180	181	0.00	0.00	0.00	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-497.28	0.00	-569.72
1	2	1.10	-497.28	0.00	-569.72
2	2	1.10	-787.36	0.00	-975.54
2	3	2.20	-787.36	0.00	-975.54
3	3	2.20	-787.36	0.00	-975.54
3	4	3.30	-787.36	0.00	-975.54
4	4	3.30	-994.56	0.00	-1261.27
4	5	4.40	-994.56	0.00	-1261.27
5	5	4.40	-994.56	0.00	-1261.27
5	6	5.50	-994.56	0.00	-1261.27
6	6	5.50	-1201.76	0.00	-1544.93
6	7	6.60	-1201.76	0.00	-1544.93
7	7	6.60	-1201.76	0.00	-1544.93
7	8	7.70	-1201.76	0.00	-1544.93
8	8	7.70	-1201.76	0.00	-1544.93
8	9	8.80	-1201.76	0.00	-1544.93
9	9	8.80	-1201.76	0.00	-1544.93
9	10	9.90	-1201.76	0.00	-1544.93
10	10	9.90	-1201.76	0.00	-1544.93
10	11	11.00	-1201.76	0.00	-1544.93
11	11	11.00	-1201.76	0.00	-1544.93
11	12	12.10	-1201.76	0.00	-1544.93
12	12	12.10	-1201.76	0.00	-1544.93
12	13	13.20	-1201.76	0.00	-1544.93
13	13	13.20	-1201.76	0.00	-1544.93
13	14	14.30	-1201.76	0.00	-1544.93
14	14	14.30	-994.56	0.00	-1261.27
14	15	15.40	-994.56	0.00	-1261.27
15	15	15.40	-994.56	0.00	-1261.27
15	16	16.50	-994.56	0.00	-1261.27
16	16	16.50	-994.56	0.00	-1261.27
16	17	17.60	-994.56	0.00	-1261.68
17	17	17.60	-787.36	0.00	-975.54
17	18	18.70	-787.36	0.00	-975.54
18	18	18.70	-787.36	0.00	-975.54
18	19	19.80	-787.36	0.00	-975.54
19	19	19.80	-497.28	0.00	-569.72
19	20	20.90	-497.28	0.00	-569.72
20	20	20.90	-497.28	0.00	-569.72
20	21	22.00	-497.28	0.00	-569.72
21	1021	22.00	-538.72	0.00	-628.93
21	22	23.40	-538.72	0.00	-628.93
22	22	23.40	-538.72	0.00	-628.93
22	23	24.80	-538.72	0.00	-628.93
23	23	24.80	-828.80	0.00	-1031.86
23	24	26.20	-828.80	0.00	-1031.86
24	24	26.20	-828.80	0.00	-1031.86
24	25	27.60	-828.80	0.00	-1031.86
25	25	27.60	-1201.76	0.00	-1538.71
25	26	29.00	-1201.76	0.00	-1538.71
26	26	29.00	-1201.76	0.00	-1538.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-1201.76	0.00	-1538.71
27	27	30.40	-1533.28	0.00	-1982.61
27	28	31.80	-1533.28	0.00	-1982.61
28	28	31.80	-1533.28	0.00	-1982.61
28	29	33.20	-1533.28	0.00	-1982.61
29	29	33.20	-1533.28	0.00	-1982.61
29	30	34.60	-1533.28	0.00	-1982.61
30	30	34.60	-1533.28	0.00	-1982.61
30	31	36.00	-1533.28	0.00	-1982.61
31	31	36.00	-1533.28	0.00	-1982.61
31	32	37.40	-1533.28	0.00	-1982.61
32	32	37.40	-1533.28	0.00	-1982.61
32	33	38.80	-1533.28	0.00	-1982.61
33	33	38.80	-1533.28	0.00	-1982.61
33	34	40.20	-1533.28	0.00	-1982.61
34	34	40.20	-1533.28	0.00	-1982.61
34	35	41.60	-1533.28	0.00	-1982.61
35	35	41.60	-1201.76	0.00	-1538.71
35	36	43.00	-1201.76	0.00	-1538.71
36	36	43.00	-1201.76	0.00	-1538.71
36	37	44.40	-1201.76	0.00	-1538.71
37	37	44.40	-828.80	0.00	-1031.86
37	38	45.80	-828.80	0.00	-1031.86
38	38	45.80	-828.80	0.00	-1031.86
38	39	47.20	-828.80	0.00	-1031.86
39	39	47.20	-538.72	0.00	-628.93
39	40	48.60	-538.72	0.00	-628.93
40	40	48.60	-538.72	0.00	-628.93
40	41	50.00	-538.72	0.00	-628.93
41	1041	50.00	-538.72	0.00	-628.93
41	42	51.40	-538.72	0.00	-628.93
42	42	51.40	-538.72	0.00	-628.93
42	43	52.80	-538.72	0.00	-628.93
43	43	52.80	-828.80	0.00	-1031.86
43	44	54.20	-828.80	0.00	-1031.86
44	44	54.20	-828.80	0.00	-1031.86
44	45	55.60	-828.80	0.00	-1031.86
45	45	55.60	-1201.76	0.00	-1538.71
45	46	57.00	-1201.76	0.00	-1538.71
46	46	57.00	-1201.76	0.00	-1538.71
46	47	58.40	-1201.76	0.00	-1538.71
47	47	58.40	-1533.28	0.00	-1982.61
47	48	59.80	-1533.28	0.00	-1982.61
48	48	59.80	-1533.28	0.00	-1982.61
48	49	61.20	-1533.28	0.00	-1982.61
49	49	61.20	-1533.28	0.00	-1982.61
49	50	62.60	-1533.28	0.00	-1982.61
50	50	62.60	-1533.28	0.00	-1982.61
50	51	64.00	-1533.28	0.00	-1982.61
51	51	64.00	-1533.28	0.00	-1982.61
51	52	65.40	-1533.28	0.00	-1982.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-1533.28	0.00	-1982.61
52	53	66.80	-1533.28	0.00	-1982.61
53	53	66.80	-1533.28	0.00	-1982.61
53	54	68.20	-1533.28	0.00	-1982.61
54	54	68.20	-1533.28	0.00	-1982.61
54	55	69.60	-1533.28	0.00	-1982.61
55	55	69.60	-1201.76	0.00	-1538.71
55	56	71.00	-1201.76	0.00	-1538.71
56	56	71.00	-1201.76	0.00	-1538.71
56	57	72.40	-1201.76	0.00	-1538.71
57	57	72.40	-828.80	0.00	-1031.86
57	58	73.80	-828.80	0.00	-1031.86
58	58	73.80	-828.80	0.00	-1031.86
58	59	75.20	-828.80	0.00	-1031.86
59	59	75.20	-538.72	0.00	-628.93
59	60	76.60	-538.72	0.00	-628.93
60	60	76.60	-538.72	0.00	-628.93
60	61	78.00	-538.72	0.00	-628.93
61	1061	78.00	-497.28	0.00	-569.72
61	62	79.10	-497.28	0.00	-569.72
62	62	79.10	-497.28	0.00	-569.72
62	63	80.20	-497.28	0.00	-569.72
63	63	80.20	-787.36	0.00	-975.54
63	64	81.30	-787.36	0.00	-975.54
64	64	81.30	-787.36	0.00	-975.54
64	65	82.40	-787.36	0.00	-975.54
65	65	82.40	-994.56	0.00	-1261.27
65	66	83.50	-994.56	0.00	-1261.27
66	66	83.50	-994.56	0.00	-1261.27
66	67	84.60	-994.56	0.00	-1261.27
67	67	84.60	-994.56	0.00	-1261.27
67	68	85.70	-994.56	0.00	-1261.27
68	68	85.70	-1201.76	0.00	-1544.93
68	69	86.80	-1201.76	0.00	-1544.93
69	69	86.80	-1201.76	0.00	-1544.93
69	70	87.90	-1201.76	0.00	-1544.93
70	70	87.90	-1201.76	0.00	-1544.93
70	71	89.00	-1201.76	0.00	-1544.93
71	71	89.00	-1201.76	0.00	-1544.93
71	72	90.10	-1201.76	0.00	-1544.93
72	72	90.10	-1201.76	0.00	-1544.93
72	73	91.20	-1201.76	0.00	-1544.93
73	73	91.20	-1201.76	0.00	-1544.93
73	74	92.30	-1201.76	0.00	-1544.93
74	74	92.30	-1201.76	0.00	-1544.93
74	75	93.40	-1201.76	0.00	-1544.93
75	75	93.40	-1201.76	0.00	-1544.93
75	76	94.50	-1201.76	0.00	-1544.93
76	76	94.50	-994.56	0.00	-1261.27
76	77	95.60	-994.56	0.00	-1261.27
77	77	95.60	-994.56	0.00	-1261.27

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-994.56	0.00	-1261.27
78	78	96.70	-787.36	0.00	-975.54
78	79	97.80	-787.36	0.00	-975.54
79	79	97.80	-787.36	0.00	-975.54
79	80	98.90	-787.36	0.00	-975.54
80	80	98.90	-497.28	0.00	-569.72
80	81	100.00	-497.28	0.00	-569.72
101	101	0.00	0.00	0.00	0.00
101	102	0.00	0.00	0.00	0.00
102	102	0.00	0.00	0.00	0.00
102	103	0.00	0.00	0.00	0.00
103	103	0.00	0.00	0.00	0.00
103	104	0.00	0.00	0.00	0.00
104	104	0.00	0.00	0.00	0.00
104	105	0.00	0.00	0.00	0.00
105	105	0.00	0.00	0.00	0.00
105	106	0.00	0.00	0.00	0.00
106	106	0.00	0.00	0.00	0.00
106	107	0.00	0.00	0.00	0.00
107	107	0.00	0.00	0.00	0.00
107	108	0.00	0.00	0.00	0.00
108	108	0.00	0.00	0.00	0.00
108	109	0.00	0.00	0.00	0.00
109	109	0.00	0.00	0.00	0.00
109	110	0.00	0.00	0.00	0.00
110	110	0.00	0.00	0.00	0.00
110	111	0.00	0.00	0.00	0.00
111	111	0.00	0.00	0.00	0.00
111	112	0.00	0.00	0.00	0.00
112	112	0.00	0.00	0.00	0.00
112	113	0.00	0.00	0.00	0.00
113	113	0.00	0.00	0.00	0.00
113	114	0.00	0.00	0.00	0.00
114	114	0.00	0.00	0.00	0.00
114	115	0.00	0.00	0.00	0.00
115	115	0.00	0.00	0.00	0.00
115	116	0.00	0.00	0.00	0.00
116	116	0.00	0.00	0.00	0.00
116	117	0.00	0.00	0.00	0.00
117	117	0.00	0.00	0.00	0.00
117	118	0.00	0.00	0.00	0.00
118	118	0.00	0.00	0.00	0.00
118	119	0.00	0.00	0.00	0.00
119	119	0.00	0.00	0.00	0.00
119	120	0.00	0.00	0.00	0.00
120	120	0.00	0.00	0.00	0.00
120	121	0.00	0.00	0.00	0.00
121	1121	0.00	0.00	0.00	0.00
121	122	0.00	0.00	0.00	0.00
122	122	0.00	0.00	0.00	0.00
122	123	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEI.FAM1.ISO + [1; 1]ej1preEI.FAM2.ISO + [1; 1]ej1preEI.FAM3.ISO + [1; 1]ej1preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	0.00	0.00	0.00	0.00
123	124	0.00	0.00	0.00	0.00
124	124	0.00	0.00	0.00	0.00
124	125	0.00	0.00	0.00	0.00
125	125	0.00	0.00	0.00	0.00
125	126	0.00	0.00	0.00	0.00
126	126	0.00	0.00	0.00	0.00
126	127	0.00	0.00	0.00	0.00
127	127	0.00	0.00	0.00	0.00
127	128	0.00	0.00	0.00	0.00
128	128	0.00	0.00	0.00	0.00
128	129	0.00	0.00	0.00	0.00
129	129	0.00	0.00	0.00	0.00
129	130	0.00	0.00	0.00	0.00
130	130	0.00	0.00	0.00	0.00
130	131	0.00	0.00	0.00	0.00
131	131	0.00	0.00	0.00	0.00
131	132	0.00	0.00	0.00	0.00
132	132	0.00	0.00	0.00	0.00
132	133	0.00	0.00	0.00	0.00
133	133	0.00	0.00	0.00	0.00
133	134	0.00	0.00	0.00	0.00
134	134	0.00	0.00	0.00	0.00
134	135	0.00	0.00	0.00	0.00
135	135	0.00	0.00	0.00	0.00
135	136	0.00	0.00	0.00	0.00
136	136	0.00	0.00	0.00	0.00
136	137	0.00	0.00	0.00	0.00
137	137	0.00	0.00	0.00	0.00
137	138	0.00	0.00	0.00	0.00
138	138	0.00	0.00	0.00	0.00
138	139	0.00	0.00	0.00	0.00
139	139	0.00	0.00	0.00	0.00
139	140	0.00	0.00	0.00	0.00
140	140	0.00	0.00	0.00	0.00
140	141	0.00	0.00	0.00	0.00
141	1141	0.00	0.00	0.00	0.00
141	142	0.00	0.00	0.00	0.00
142	142	0.00	0.00	0.00	0.00
142	143	0.00	0.00	0.00	0.00
143	143	0.00	0.00	0.00	0.00
143	144	0.00	0.00	0.00	0.00
144	144	0.00	0.00	0.00	0.00
144	145	0.00	0.00	0.00	0.00
145	145	0.00	0.00	0.00	0.00
145	146	0.00	0.00	0.00	0.00
146	146	0.00	0.00	0.00	0.00
146	147	0.00	0.00	0.00	0.00
147	147	0.00	0.00	0.00	0.00
147	148	0.00	0.00	0.00	0.00
148	148	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1preEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEI.FAM1.ISO + [1; 1]ej1preEI.FAM2.ISO + [1; 1]ej1preEI.FAM3.ISO + [1; 1]ej1preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	0.00	0.00	0.00	0.00
149	149	0.00	0.00	0.00	0.00
149	150	0.00	0.00	0.00	0.00
150	150	0.00	0.00	0.00	0.00
150	151	0.00	0.00	0.00	0.00
151	151	0.00	0.00	0.00	0.00
151	152	0.00	0.00	0.00	0.00
152	152	0.00	0.00	0.00	0.00
152	153	0.00	0.00	0.00	0.00
153	153	0.00	0.00	0.00	0.00
153	154	0.00	0.00	0.00	0.00
154	154	0.00	0.00	0.00	0.00
154	155	0.00	0.00	0.00	0.00
155	155	0.00	0.00	0.00	0.00
155	156	0.00	0.00	0.00	0.00
156	156	0.00	0.00	0.00	0.00
156	157	0.00	0.00	0.00	0.00
157	157	0.00	0.00	0.00	0.00
157	158	0.00	0.00	0.00	0.00
158	158	0.00	0.00	0.00	0.00
158	159	0.00	0.00	0.00	0.00
159	159	0.00	0.00	0.00	0.00
159	160	0.00	0.00	0.00	0.00
160	160	0.00	0.00	0.00	0.00
160	161	0.00	0.00	0.00	0.00
161	1161	0.00	0.00	0.00	0.00
161	162	0.00	0.00	0.00	0.00
162	162	0.00	0.00	0.00	0.00
162	163	0.00	0.00	0.00	0.00
163	163	0.00	0.00	0.00	0.00
163	164	0.00	0.00	0.00	0.00
164	164	0.00	0.00	0.00	0.00
164	165	0.00	0.00	0.00	0.00
165	165	0.00	0.00	0.00	0.00
165	166	0.00	0.00	0.00	0.00
166	166	0.00	0.00	0.00	0.00
166	167	0.00	0.00	0.00	0.00
167	167	0.00	0.00	0.00	0.00
167	168	0.00	0.00	0.00	0.00
168	168	0.00	0.00	0.00	0.00
168	169	0.00	0.00	0.00	0.00
169	169	0.00	0.00	0.00	0.00
169	170	0.00	0.00	0.00	0.00
170	170	0.00	0.00	0.00	0.00
170	171	0.00	0.00	0.00	0.00
171	171	0.00	0.00	0.00	0.00
171	172	0.00	0.00	0.00	0.00
172	172	0.00	0.00	0.00	0.00
172	173	0.00	0.00	0.00	0.00
173	173	0.00	0.00	0.00	0.00
173	174	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

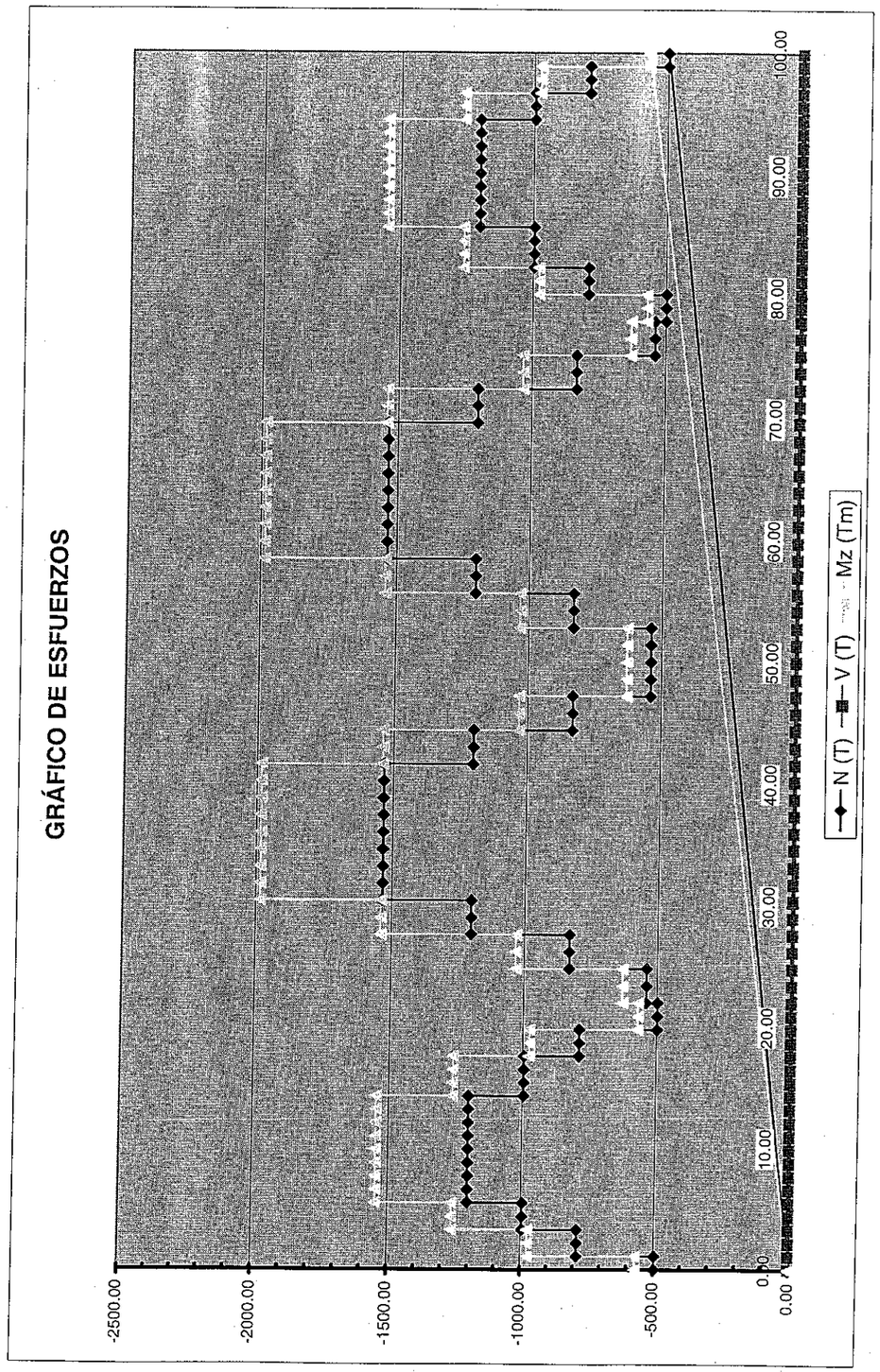
ej1preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1preEl.FAM1.ISO + [1; 1]ej1preEl.FAM2.ISO + [1; 1]ej1preEl.FAM3.ISO + [1; 1]ej1preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	0.00	0.00	0.00	0.00
174	175	0.00	0.00	0.00	0.00
175	175	0.00	0.00	0.00	0.00
175	176	0.00	0.00	0.00	0.00
176	176	0.00	0.00	0.00	0.00
176	177	0.00	0.00	0.00	0.00
177	177	0.00	0.00	0.00	0.00
177	178	0.00	0.00	0.00	0.00
178	178	0.00	0.00	0.00	0.00
178	179	0.00	0.00	0.00	0.00
179	179	0.00	0.00	0.00	0.00
179	180	0.00	0.00	0.00	0.00
180	180	0.00	0.00	0.00	0.00
180	181	0.00	0.00	0.00	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	225.60	21.91	0.24
1	2	1.10	225.60	21.91	-23.86
2	2	1.10	226.45	21.27	-23.37
2	3	2.20	226.45	21.27	-46.77
3	3	2.20	227.77	20.83	-46.31
3	4	3.30	227.77	20.83	-69.23
4	4	3.30	229.54	20.58	-68.79
4	5	4.40	229.54	20.58	-91.43
5	5	4.40	231.75	20.49	-91.04
5	6	5.50	231.75	20.49	-113.58
6	6	5.50	234.40	20.55	-113.24
6	7	6.60	234.40	20.55	-135.84
7	7	6.60	237.48	20.73	-135.56
7	8	7.70	237.48	20.73	-158.36
8	8	7.70	241.01	21.01	-158.15
8	9	8.80	241.01	21.01	-181.25
9	9	8.80	244.98	21.35	-181.12
9	10	9.90	244.98	21.35	-204.60
10	10	9.90	249.41	21.72	-204.56
10	11	11.00	249.41	21.72	-228.44
11	11	11.00	254.31	22.08	-228.50
11	12	12.10	254.31	22.08	-252.79
12	12	12.10	259.71	22.39	-252.96
12	13	13.20	259.71	22.39	-277.59
13	13	13.20	265.64	22.60	-277.89
13	14	14.30	265.64	22.60	-302.75
14	14	14.30	272.13	22.65	-303.18
14	15	15.40	272.13	22.65	-328.10
15	15	15.40	-591.02	22.47	89.89
15	16	16.50	-591.02	22.47	65.17
16	16	16.50	-584.23	22.04	64.61
16	17	17.60	-584.23	22.04	40.36
17	17	17.60	-1447.94	21.36	458.39
17	18	18.70	-1447.94	21.36	434.89
18	18	18.70	-1442.58	20.48	434.54
18	19	19.80	-1442.58	20.48	412.02
19	19	19.80	-1438.35	19.47	411.86
19	20	20.90	-1438.35	19.47	390.45
20	20	20.90	-1435.25	18.40	390.47
20	21	22.00	-1435.25	18.40	370.23
21	1021	22.00	-1432.33	-8.75	370.46
21	22	23.40	-1432.33	-8.75	382.70
22	22	23.40	-1431.14	-9.95	383.24
22	23	24.80	-1431.14	-9.95	397.17
23	23	24.80	-1432.82	-10.87	397.99
23	24	26.20	-1432.82	-10.87	413.21
24	24	26.20	-567.21	-11.36	-4.24
24	25	27.60	-567.21	-11.36	11.66
25	25	27.60	-572.44	-11.32	12.80
25	26	29.00	-572.44	-11.32	28.65
26	26	29.00	291.80	-10.76	-388.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	291.80	-10.76	-373.70
27	27	30.40	287.37	-9.73	-372.82
27	28	31.80	287.37	-9.73	-359.19
28	28	31.80	284.35	-8.37	-358.56
28	29	33.20	284.35	-8.37	-346.84
29	29	33.20	282.66	-6.80	-346.45
29	30	34.60	282.66	-6.80	-336.93
30	30	34.60	282.21	-5.11	-336.77
30	31	36.00	282.21	-5.11	-329.61
31	31	36.00	283.01	-3.43	-329.66
31	32	37.40	283.01	-3.43	-324.87
32	32	37.40	285.03	-1.83	-325.14
32	33	38.80	285.03	-1.83	-322.59
33	33	38.80	288.33	-0.41	-323.08
33	34	40.20	288.33	-0.41	-322.50
34	34	40.20	292.98	0.71	-323.22
34	35	41.60	292.98	0.71	-324.21
35	35	41.60	299.08	1.42	-325.16
35	36	43.00	299.08	1.42	-327.15
36	36	43.00	-563.45	1.62	90.23
36	37	44.40	-563.45	1.62	87.97
37	37	44.40	-556.43	1.23	86.83
37	38	45.80	-556.43	1.23	85.10
38	38	45.80	-1420.17	0.30	502.60
38	39	47.20	-1420.17	0.30	502.18
39	39	47.20	-1416.51	-1.08	501.46
39	40	48.60	-1416.51	-1.08	502.97
40	40	48.60	-1415.62	-2.72	502.61
40	41	50.00	-1415.62	-2.72	506.43
41	1041	50.00	-1417.48	2.72	506.43
41	42	51.40	-1417.48	2.72	502.61
42	42	51.40	-1422.10	1.08	502.97
42	43	52.80	-1422.10	1.08	501.46
43	43	52.80	-1429.50	-0.30	502.18
43	44	54.20	-1429.50	-0.30	502.60
44	44	54.20	-569.52	-1.23	85.10
44	45	55.60	-569.52	-1.23	86.82
45	45	55.60	-580.34	-1.62	87.97
45	46	57.00	-580.34	-1.62	90.23
46	46	57.00	278.33	-1.42	-327.15
46	47	58.40	278.33	-1.42	-325.16
47	47	58.40	268.33	-0.70	-324.21
47	48	59.80	268.33	-0.70	-323.22
48	48	59.80	259.69	0.41	-322.50
48	49	61.20	259.69	0.41	-323.09
49	49	61.20	252.31	1.83	-322.59
49	50	62.60	252.31	1.83	-325.15
50	50	62.60	246.10	3.42	-324.87
50	51	64.00	246.10	3.42	-329.67
51	51	64.00	240.98	5.12	-329.61
51	52	65.40	240.98	5.12	-336.77

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1; 1]ej1posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	236.94	6.80	-336.94
52	53	66.80	236.94	6.80	-346.45
53	53	66.80	233.96	8.37	-346.85
53	54	68.20	233.96	8.37	-358.57
54	54	68.20	232.09	9.73	-359.20
54	55	69.60	232.09	9.73	-372.82
55	55	69.60	231.35	10.76	-373.71
55	56	71.00	231.35	10.76	-388.77
56	56	71.00	-638.37	11.32	28.65
56	57	72.40	-638.37	11.32	12.80
57	57	72.40	-638.98	11.35	11.66
57	58	73.80	-638.98	11.35	-4.24
58	58	73.80	-1510.87	10.87	413.21
58	59	75.20	-1510.87	10.87	398.00
59	59	75.20	-1515.96	9.95	397.17
59	60	76.60	-1515.96	9.95	383.24
60	60	76.60	-1524.55	8.74	382.71
60	61	78.00	-1524.55	8.74	370.47
61	1061	78.00	-1533.22	-18.40	370.24
61	62	79.10	-1533.22	-18.40	390.48
62	62	79.10	-1540.53	-19.47	390.45
62	63	80.20	-1540.53	-19.47	411.87
63	63	80.20	-1549.23	-20.48	412.02
63	64	81.30	-1549.23	-20.48	434.55
64	64	81.30	-1559.33	-21.36	434.90
64	65	82.40	-1559.33	-21.36	458.40
65	65	82.40	-700.60	-22.04	40.36
65	66	83.50	-700.60	-22.04	64.61
66	66	83.50	-712.63	-22.47	65.18
66	67	84.60	-712.63	-22.47	89.89
67	67	84.60	145.04	-22.65	-328.09
67	68	85.70	145.04	-22.65	-303.18
68	68	85.70	132.83	-22.60	-302.75
68	69	86.80	132.83	-22.60	-277.89
69	69	86.80	120.92	-22.39	-277.59
69	70	87.90	120.92	-22.39	-252.96
70	70	87.90	109.29	-22.08	-252.79
70	71	89.00	109.29	-22.08	-228.50
71	71	89.00	97.90	-21.72	-228.45
71	72	90.10	97.90	-21.72	-204.56
72	72	90.10	86.72	-21.35	-204.60
72	73	91.20	86.72	-21.35	-181.12
73	73	91.20	75.71	-21.01	-181.26
73	74	92.30	75.71	-21.01	-158.15
74	74	92.30	64.85	-20.73	-158.37
74	75	93.40	64.85	-20.73	-135.56
75	75	93.40	54.11	-20.55	-135.84
75	76	94.50	54.11	-20.55	-113.24
76	76	94.50	43.46	-20.49	-113.58
76	77	95.60	43.46	-20.49	-91.04
77	77	95.60	32.88	-20.58	-91.44

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1; 1]ej1posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	32.88	-20.58	-68.80
78	78	96.70	22.35	-20.84	-69.23
78	79	97.80	22.35	-20.84	-46.31
79	79	97.80	11.84	-21.27	-46.78
79	80	98.90	11.84	-21.27	-23.37
80	80	98.90	1.32	-21.91	-23.86
80	81	100.00	1.32	-21.91	0.24
101	101	0.00	-225.60	-1.58	-0.24
101	102	1.10	-225.60	-1.58	1.50
102	102	1.10	-226.45	-0.95	1.01
102	103	2.20	-226.45	-0.95	2.05
103	103	2.20	-227.77	-0.51	1.59
103	104	3.30	-227.77	-0.51	2.15
104	104	3.30	-229.54	-0.25	1.72
104	105	4.40	-229.54	-0.25	2.00
105	105	4.40	-231.75	-0.17	1.60
105	106	5.50	-231.75	-0.17	1.78
106	106	5.50	-234.40	-0.22	1.44
106	107	6.60	-234.40	-0.22	1.69
107	107	6.60	-237.48	-0.40	1.40
107	108	7.70	-237.48	-0.40	1.85
108	108	7.70	-241.01	-0.68	1.63
108	109	8.80	-241.01	-0.68	2.38
109	109	8.80	-244.98	-1.02	2.24
109	110	9.90	-244.98	-1.02	3.36
110	110	9.90	-249.41	-1.39	3.32
110	111	11.00	-249.41	-1.39	4.85
111	111	11.00	-254.31	-1.75	4.90
111	112	12.10	-254.31	-1.75	6.83
112	112	12.10	-259.71	-2.06	7.00
112	113	13.20	-259.71	-2.06	9.27
113	113	13.20	-265.64	-2.27	9.57
113	114	14.30	-265.64	-2.27	12.06
114	114	14.30	-272.13	-2.32	12.50
114	115	15.40	-272.13	-2.32	15.05
115	115	15.40	-279.22	-2.14	15.64
115	116	16.50	-279.22	-2.14	18.00
116	116	16.50	-286.01	-1.71	18.57
116	117	17.60	-286.01	-1.71	20.45
117	117	17.60	-292.54	-1.03	21.00
117	118	18.70	-292.54	-1.03	22.14
118	118	18.70	-297.91	-0.15	22.49
118	119	19.80	-297.91	-0.15	22.65
119	119	19.80	-302.13	0.86	22.81
119	120	20.90	-302.13	0.86	21.86
120	120	20.90	-305.24	1.93	21.83
120	121	22.00	-305.24	1.93	19.71
121	1121	22.00	-308.15	2.97	19.48
121	122	23.40	-308.15	2.97	15.33
122	122	23.40	-309.35	4.17	14.80
122	123	24.80	-309.35	4.17	8.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1; 1]ej1posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-307.66	5.09	8.13
123	124	26.20	-307.66	5.09	1.00
124	124	26.20	-303.03	5.58	-0.13
124	125	27.60	-303.03	5.58	-7.94
125	125	27.60	-297.80	5.55	-9.09
125	126	29.00	-297.80	5.55	-16.85
126	126	29.00	-291.80	4.98	-18.02
126	127	30.40	-291.80	4.98	-25.00
127	127	30.40	-287.37	3.96	-25.88
127	128	31.80	-287.37	3.96	-31.43
128	128	31.80	-284.35	2.60	-32.06
128	129	33.20	-284.35	2.60	-35.70
129	129	33.20	-282.66	1.03	-36.10
129	130	34.60	-282.66	1.03	-37.54
130	130	34.60	-282.21	-0.65	-37.71
130	131	36.00	-282.21	-0.65	-36.80
131	131	36.00	-283.01	-2.34	-36.74
131	132	37.40	-283.01	-2.34	-33.47
132	132	37.40	-285.03	-3.93	-33.19
132	133	38.80	-285.03	-3.93	-27.69
133	133	38.80	-288.33	-5.34	-27.19
133	134	40.20	-288.33	-5.34	-19.71
134	134	40.20	-292.98	-6.46	-18.99
134	135	41.60	-292.98	-6.46	-9.95
135	135	41.60	-299.08	-7.18	-9.00
135	136	43.00	-299.08	-7.18	1.05
136	136	43.00	-306.79	-7.37	2.25
136	137	44.40	-306.79	-7.37	12.57
137	137	44.40	-313.81	-6.98	13.71
137	138	45.80	-313.81	-6.98	23.49
138	138	45.80	-320.31	-6.05	24.58
138	139	47.20	-320.31	-6.05	33.04
139	139	47.20	-323.97	-4.67	33.76
139	140	48.60	-323.97	-4.67	40.30
140	140	48.60	-324.86	-3.03	40.66
140	141	50.00	-324.86	-3.03	44.90
141	1141	50.00	-323.00	3.03	44.90
141	142	51.40	-323.00	3.03	40.66
142	142	51.40	-318.38	4.67	40.30
142	143	52.80	-318.38	4.67	33.76
143	143	52.80	-310.98	6.05	33.04
143	144	54.20	-310.98	6.05	24.57
144	144	54.20	-300.72	6.98	23.48
144	145	55.60	-300.72	6.98	13.71
145	145	55.60	-289.90	7.37	12.57
145	146	57.00	-289.90	7.37	2.25
146	146	57.00	-278.33	7.18	1.05
146	147	58.40	-278.33	7.18	-9.00
147	147	58.40	-268.33	6.46	-9.95
147	148	59.80	-268.33	6.46	-19.00
148	148	59.80	-259.69	5.34	-19.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1; 1]ej1posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-259.69	5.34	-27.20
149	149	61.20	-252.31	3.93	-27.69
149	150	62.60	-252.31	3.93	-33.20
150	150	62.60	-246.10	2.34	-33.47
150	151	64.00	-246.10	2.34	-36.74
151	151	64.00	-240.98	0.65	-36.80
151	152	65.40	-240.98	0.65	-37.71
152	152	65.40	-236.94	-1.03	-37.54
152	153	66.80	-236.94	-1.03	-36.10
153	153	66.80	-233.96	-2.60	-35.71
153	154	68.20	-233.96	-2.60	-32.06
154	154	68.20	-232.09	-3.96	-31.43
154	155	69.60	-232.09	-3.96	-25.89
155	155	69.60	-231.35	-4.98	-25.00
155	156	71.00	-231.35	-4.98	-18.02
156	156	71.00	-231.87	-5.55	-16.85
156	157	72.40	-231.87	-5.55	-9.09
157	157	72.40	-231.26	-5.58	-7.95
157	158	73.80	-231.26	-5.58	-0.13
158	158	73.80	-229.62	-5.09	1.00
158	159	75.20	-229.62	-5.09	8.13
159	159	75.20	-224.52	-4.17	8.96
159	160	76.60	-224.52	-4.17	14.80
160	160	76.60	-215.93	-2.97	15.33
160	161	78.00	-215.93	-2.97	19.49
161	1161	78.00	-207.27	-1.93	19.71
161	162	79.10	-207.27	-1.93	21.84
162	162	79.10	-199.95	-0.86	21.86
162	163	80.20	-199.95	-0.86	22.81
163	163	80.20	-191.25	0.15	22.66
163	164	81.30	-191.25	0.15	22.49
164	164	81.30	-181.15	1.03	22.14
164	165	82.40	-181.15	1.03	21.01
165	165	82.40	-169.64	1.71	20.45
165	166	83.50	-169.64	1.71	18.57
166	166	83.50	-157.61	2.14	18.00
166	167	84.60	-157.61	2.14	15.65
167	167	84.60	-145.04	2.32	15.05
167	168	85.70	-145.04	2.32	12.50
168	168	85.70	-132.83	2.27	12.06
168	169	86.80	-132.83	2.27	9.57
169	169	86.80	-120.92	2.06	9.27
169	170	87.90	-120.92	2.06	7.00
170	170	87.90	-109.29	1.75	6.83
170	171	89.00	-109.29	1.75	4.90
171	171	89.00	-97.90	1.39	4.85
171	172	90.10	-97.90	1.39	3.32
172	172	90.10	-86.72	1.02	3.36
172	173	91.20	-86.72	1.02	2.24
173	173	91.20	-75.71	0.68	2.38
173	174	92.30	-75.71	0.68	1.63

CÁLCULO TENSIONAL

Hipótesis de cálculo:

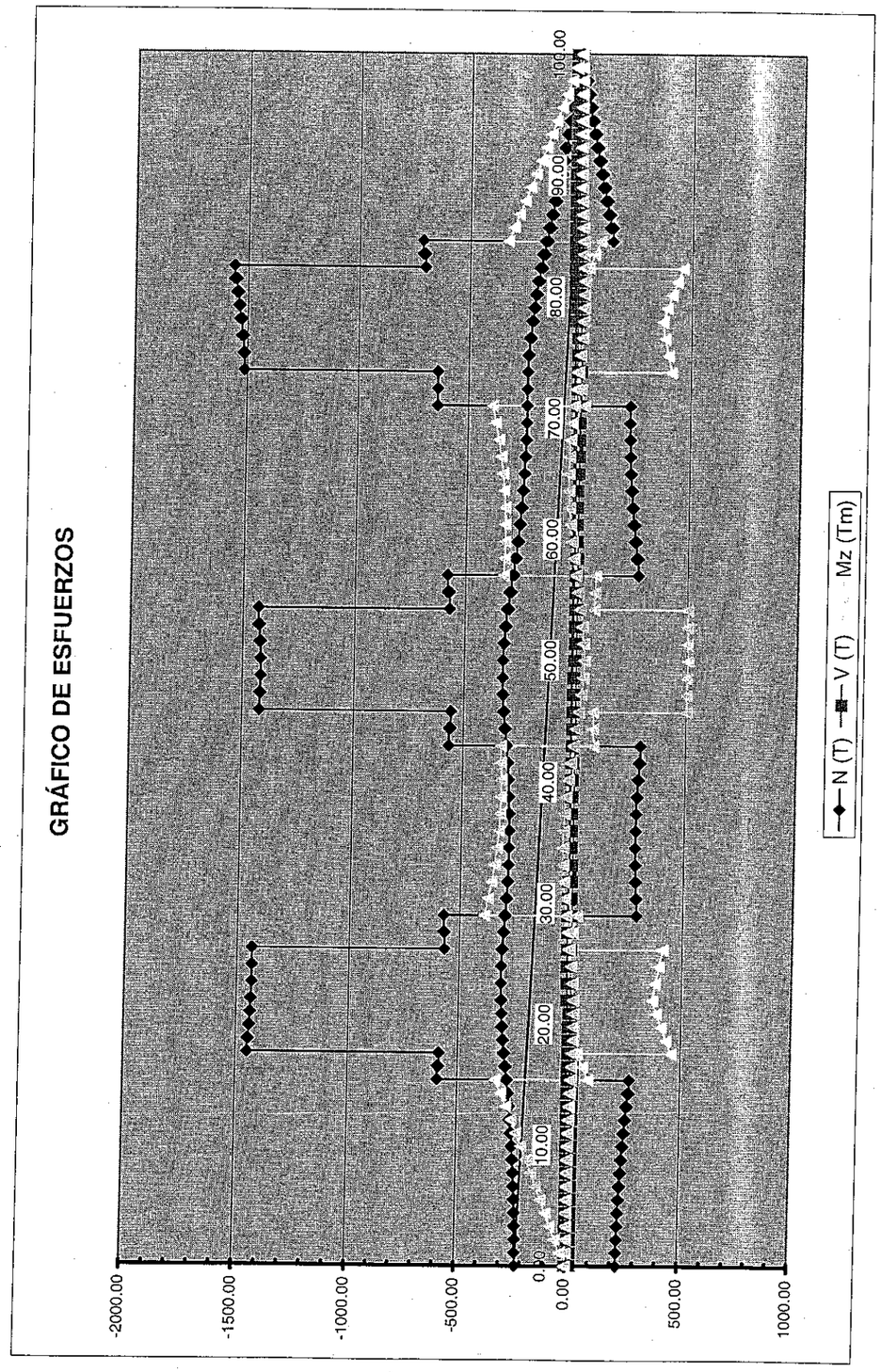
ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1; 1]ej1posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-64.85	0.40	1.85
174	175	93.40	-64.85	0.40	1.40
175	175	93.40	-54.11	0.22	1.69
175	176	94.50	-54.11	0.22	1.44
176	176	94.50	-43.46	0.17	1.78
176	177	95.60	-43.46	0.17	1.60
177	177	95.60	-32.88	0.25	2.00
177	178	96.70	-32.88	0.25	1.72
178	178	96.70	-22.35	0.51	2.15
178	179	97.80	-22.35	0.51	1.59
179	179	97.80	-11.84	0.95	2.05
179	180	98.90	-11.84	0.95	1.01
180	180	98.90	-1.32	1.58	1.50
180	181	100.00	-1.32	1.58	-0.24



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	225.60	21.91	0.24
1	2	1.10	225.60	21.91	-23.86
2	2	1.10	226.45	21.27	-23.37
2	3	2.20	226.45	21.27	-46.77
3	3	2.20	227.77	20.83	-46.31
3	4	3.30	227.77	20.83	-69.23
4	4	3.30	229.54	20.58	-68.79
4	5	4.40	229.54	20.58	-91.43
5	5	4.40	231.75	20.49	-91.04
5	6	5.50	231.75	20.49	-113.58
6	6	5.50	234.40	20.55	-113.24
6	7	6.60	234.40	20.55	-135.84
7	7	6.60	237.48	20.73	-135.56
7	8	7.70	237.48	20.73	-158.36
8	8	7.70	241.01	21.01	-158.15
8	9	8.80	241.01	21.01	-181.25
9	9	8.80	244.98	21.35	-181.12
9	10	9.90	244.98	21.35	-204.60
10	10	9.90	249.41	21.72	-204.56
10	11	11.00	249.41	21.72	-228.44
11	11	11.00	254.31	22.08	-228.50
11	12	12.10	254.31	22.08	-252.79
12	12	12.10	259.71	22.39	-252.96
12	13	13.20	259.71	22.39	-277.59
13	13	13.20	265.64	22.60	-277.89
13	14	14.30	265.64	22.60	-302.75
14	14	14.30	272.13	22.65	-303.18
14	15	15.40	272.13	22.65	-328.10
15	15	15.40	-591.02	22.47	89.89
15	16	16.50	-591.02	22.47	65.17
16	16	16.50	-584.23	22.04	64.61
16	17	17.60	-584.23	22.04	40.36
17	17	17.60	-1447.94	21.36	458.39
17	18	18.70	-1447.94	21.36	434.89
18	18	18.70	-1442.58	20.48	434.54
18	19	19.80	-1442.58	20.48	412.02
19	19	19.80	-1438.35	19.47	411.86
19	20	20.90	-1438.35	19.47	390.45
20	20	20.90	-1435.25	18.40	390.47
20	21	22.00	-1435.25	18.40	370.23
21	1021	22.00	-1432.33	-8.75	370.46
21	22	23.40	-1432.33	-8.75	382.70
22	22	23.40	-1431.14	-9.95	383.24
22	23	24.80	-1431.14	-9.95	397.17
23	23	24.80	-1432.82	-10.87	397.99
23	24	26.20	-1432.82	-10.87	413.21
24	24	26.20	-567.21	-11.36	-4.24
24	25	27.60	-567.21	-11.36	11.66
25	25	27.60	-572.44	-11.32	12.80
25	26	29.00	-572.44	-11.32	28.65
26	26	29.00	291.80	-10.76	-388.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	291.80	-10.76	-373.70
27	27	30.40	287.37	-9.73	-372.82
27	28	31.80	287.37	-9.73	-359.19
28	28	31.80	284.35	-8.37	-358.56
28	29	33.20	284.35	-8.37	-346.84
29	29	33.20	282.66	-6.80	-346.45
29	30	34.60	282.66	-6.80	-336.93
30	30	34.60	282.21	-5.11	-336.77
30	31	36.00	282.21	-5.11	-329.61
31	31	36.00	283.01	-3.43	-329.66
31	32	37.40	283.01	-3.43	-324.87
32	32	37.40	285.03	-1.83	-325.14
32	33	38.80	285.03	-1.83	-322.59
33	33	38.80	288.33	-0.41	-323.08
33	34	40.20	288.33	-0.41	-322.50
34	34	40.20	292.98	0.71	-323.22
34	35	41.60	292.98	0.71	-324.21
35	35	41.60	299.08	1.42	-325.16
35	36	43.00	299.08	1.42	-327.15
36	36	43.00	-563.45	1.62	90.23
36	37	44.40	-563.45	1.62	87.97
37	37	44.40	-556.43	1.23	86.83
37	38	45.80	-556.43	1.23	85.10
38	38	45.80	-1420.17	0.30	502.60
38	39	47.20	-1420.17	0.30	502.18
39	39	47.20	-1416.51	-1.08	501.46
39	40	48.60	-1416.51	-1.08	502.97
40	40	48.60	-1415.62	-2.72	502.61
40	41	50.00	-1415.62	-2.72	506.43
41	1041	50.00	-1417.48	2.72	506.43
41	42	51.40	-1417.48	2.72	502.61
42	42	51.40	-1422.10	1.08	502.97
42	43	52.80	-1422.10	1.08	501.46
43	43	52.80	-1429.50	-0.30	502.18
43	44	54.20	-1429.50	-0.30	502.60
44	44	54.20	-569.52	-1.23	85.10
44	45	55.60	-569.52	-1.23	86.82
45	45	55.60	-580.34	-1.62	87.97
45	46	57.00	-580.34	-1.62	90.23
46	46	57.00	278.33	-1.42	-327.15
46	47	58.40	278.33	-1.42	-325.16
47	47	58.40	268.33	-0.70	-324.21
47	48	59.80	268.33	-0.70	-323.22
48	48	59.80	259.69	0.41	-322.50
48	49	61.20	259.69	0.41	-323.09
49	49	61.20	252.31	1.83	-322.59
49	50	62.60	252.31	1.83	-325.15
50	50	62.60	246.10	3.42	-324.87
50	51	64.00	246.10	3.42	-329.67
51	51	64.00	240.98	5.12	-329.61
51	52	65.40	240.98	5.12	-336.77

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	236.94	6.80	-336.94
52	53	66.80	236.94	6.80	-346.45
53	53	66.80	233.96	8.37	-346.85
53	54	68.20	233.96	8.37	-358.57
54	54	68.20	232.09	9.73	-359.20
54	55	69.60	232.09	9.73	-372.82
55	55	69.60	231.35	10.76	-373.71
55	56	71.00	231.35	10.76	-388.77
56	56	71.00	-638.37	11.32	28.65
56	57	72.40	-638.37	11.32	12.80
57	57	72.40	-638.98	11.35	11.66
57	58	73.80	-638.98	11.35	-4.24
58	58	73.80	-1510.87	10.87	413.21
58	59	75.20	-1510.87	10.87	398.00
59	59	75.20	-1515.96	9.95	397.17
59	60	76.60	-1515.96	9.95	383.24
60	60	76.60	-1524.55	8.74	382.71
60	61	78.00	-1524.55	8.74	370.47
61	1061	78.00	-1533.22	-18.40	370.24
61	62	79.10	-1533.22	-18.40	390.48
62	62	79.10	-1540.53	-19.47	390.45
62	63	80.20	-1540.53	-19.47	411.87
63	63	80.20	-1549.23	-20.48	412.02
63	64	81.30	-1549.23	-20.48	434.55
64	64	81.30	-1559.33	-21.36	434.90
64	65	82.40	-1559.33	-21.36	458.40
65	65	82.40	-700.60	-22.04	40.36
65	66	83.50	-700.60	-22.04	64.61
66	66	83.50	-712.63	-22.47	65.18
66	67	84.60	-712.63	-22.47	89.89
67	67	84.60	145.04	-22.65	-328.09
67	68	85.70	145.04	-22.65	-303.18
68	68	85.70	132.83	-22.60	-302.75
68	69	86.80	132.83	-22.60	-277.89
69	69	86.80	120.92	-22.39	-277.59
69	70	87.90	120.92	-22.39	-252.96
70	70	87.90	109.29	-22.08	-252.79
70	71	89.00	109.29	-22.08	-228.50
71	71	89.00	97.90	-21.72	-228.45
71	72	90.10	97.90	-21.72	-204.56
72	72	90.10	86.72	-21.35	-204.60
72	73	91.20	86.72	-21.35	-181.12
73	73	91.20	75.71	-21.01	-181.26
73	74	92.30	75.71	-21.01	-158.15
74	74	92.30	64.85	-20.73	-158.37
74	75	93.40	64.85	-20.73	-135.56
75	75	93.40	54.11	-20.55	-135.84
75	76	94.50	54.11	-20.55	-113.24
76	76	94.50	43.46	-20.49	-113.58
76	77	95.60	43.46	-20.49	-91.04
77	77	95.60	32.88	-20.58	-91.44

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	32.88	-20.58	-68.80
78	78	96.70	22.35	-20.84	-69.23
78	79	97.80	22.35	-20.84	-46.31
79	79	97.80	11.84	-21.27	-46.78
79	80	98.90	11.84	-21.27	-23.37
80	80	98.90	1.32	-21.91	-23.86
80	81	100.00	1.32	-21.91	0.24
101	101	0.00	-225.60	-1.58	-0.24
101	102	1.10	-225.60	-1.58	1.50
102	102	1.10	-226.45	-0.95	1.01
102	103	2.20	-226.45	-0.95	2.05
103	103	2.20	-227.77	-0.51	1.59
103	104	3.30	-227.77	-0.51	2.15
104	104	3.30	-229.54	-0.25	1.72
104	105	4.40	-229.54	-0.25	2.00
105	105	4.40	-231.75	-0.17	1.60
105	106	5.50	-231.75	-0.17	1.78
106	106	5.50	-234.40	-0.22	1.44
106	107	6.60	-234.40	-0.22	1.69
107	107	6.60	-237.48	-0.40	1.40
107	108	7.70	-237.48	-0.40	1.85
108	108	7.70	-241.01	-0.68	1.63
108	109	8.80	-241.01	-0.68	2.38
109	109	8.80	-244.98	-1.02	2.24
109	110	9.90	-244.98	-1.02	3.36
110	110	9.90	-249.41	-1.39	3.32
110	111	11.00	-249.41	-1.39	4.85
111	111	11.00	-254.31	-1.75	4.90
111	112	12.10	-254.31	-1.75	6.83
112	112	12.10	-259.71	-2.06	7.00
112	113	13.20	-259.71	-2.06	9.27
113	113	13.20	-265.64	-2.27	9.57
113	114	14.30	-265.64	-2.27	12.06
114	114	14.30	-272.13	-2.32	12.50
114	115	15.40	-272.13	-2.32	15.05
115	115	15.40	-279.22	-2.14	15.64
115	116	16.50	-279.22	-2.14	18.00
116	116	16.50	-286.01	-1.71	18.57
116	117	17.60	-286.01	-1.71	20.45
117	117	17.60	-292.54	-1.03	21.00
117	118	18.70	-292.54	-1.03	22.14
118	118	18.70	-297.91	-0.15	22.49
118	119	19.80	-297.91	-0.15	22.65
119	119	19.80	-302.13	0.86	22.81
119	120	20.90	-302.13	0.86	21.86
120	120	20.90	-305.24	1.93	21.83
120	121	22.00	-305.24	1.93	19.71
121	1121	22.00	-308.15	2.97	19.48
121	122	23.40	-308.15	2.97	15.33
122	122	23.40	-309.35	4.17	14.80
122	123	24.80	-309.35	4.17	8.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-307.66	5.09	8.13
123	124	26.20	-307.66	5.09	1.00
124	124	26.20	-303.03	5.58	-0.13
124	125	27.60	-303.03	5.58	-7.94
125	125	27.60	-297.80	5.55	-9.09
125	126	29.00	-297.80	5.55	-16.85
126	126	29.00	-291.80	4.98	-18.02
126	127	30.40	-291.80	4.98	-25.00
127	127	30.40	-287.37	3.96	-25.88
127	128	31.80	-287.37	3.96	-31.43
128	128	31.80	-284.35	2.60	-32.06
128	129	33.20	-284.35	2.60	-35.70
129	129	33.20	-282.66	1.03	-36.10
129	130	34.60	-282.66	1.03	-37.54
130	130	34.60	-282.21	-0.65	-37.71
130	131	36.00	-282.21	-0.65	-36.80
131	131	36.00	-283.01	-2.34	-36.74
131	132	37.40	-283.01	-2.34	-33.47
132	132	37.40	-285.03	-3.93	-33.19
132	133	38.80	-285.03	-3.93	-27.69
133	133	38.80	-288.33	-5.34	-27.19
133	134	40.20	-288.33	-5.34	-19.71
134	134	40.20	-292.98	-6.46	-18.99
134	135	41.60	-292.98	-6.46	-9.95
135	135	41.60	-299.08	-7.18	-9.00
135	136	43.00	-299.08	-7.18	1.05
136	136	43.00	-306.79	-7.37	2.25
136	137	44.40	-306.79	-7.37	12.57
137	137	44.40	-313.81	-6.98	13.71
137	138	45.80	-313.81	-6.98	23.49
138	138	45.80	-320.31	-6.05	24.58
138	139	47.20	-320.31	-6.05	33.04
139	139	47.20	-323.97	-4.67	33.76
139	140	48.60	-323.97	-4.67	40.30
140	140	48.60	-324.86	-3.03	40.66
140	141	50.00	-324.86	-3.03	44.90
141	1141	50.00	-323.00	3.03	44.90
141	142	51.40	-323.00	3.03	40.66
142	142	51.40	-318.38	4.67	40.30
142	143	52.80	-318.38	4.67	33.76
143	143	52.80	-310.98	6.05	33.04
143	144	54.20	-310.98	6.05	24.57
144	144	54.20	-300.72	6.98	23.48
144	145	55.60	-300.72	6.98	13.71
145	145	55.60	-289.90	7.37	12.57
145	146	57.00	-289.90	7.37	2.25
146	146	57.00	-278.33	7.18	1.05
146	147	58.40	-278.33	7.18	-9.00
147	147	58.40	-268.33	6.46	-9.95
147	148	59.80	-268.33	6.46	-19.00
148	148	59.80	-259.69	5.34	-19.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-259.69	5.34	-27.20
149	149	61.20	-252.31	3.93	-27.69
149	150	62.60	-252.31	3.93	-33.20
150	150	62.60	-246.10	2.34	-33.47
150	151	64.00	-246.10	2.34	-36.74
151	151	64.00	-240.98	0.65	-36.80
151	152	65.40	-240.98	0.65	-37.71
152	152	65.40	-236.94	-1.03	-37.54
152	153	66.80	-236.94	-1.03	-36.10
153	153	66.80	-233.96	-2.60	-35.71
153	154	68.20	-233.96	-2.60	-32.06
154	154	68.20	-232.09	-3.96	-31.43
154	155	69.60	-232.09	-3.96	-25.89
155	155	69.60	-231.35	-4.98	-25.00
155	156	71.00	-231.35	-4.98	-18.02
156	156	71.00	-231.87	-5.55	-16.85
156	157	72.40	-231.87	-5.55	-9.09
157	157	72.40	-231.26	-5.58	-7.95
157	158	73.80	-231.26	-5.58	-0.13
158	158	73.80	-229.62	-5.09	1.00
158	159	75.20	-229.62	-5.09	8.13
159	159	75.20	-224.52	-4.17	8.96
159	160	76.60	-224.52	-4.17	14.80
160	160	76.60	-215.93	-2.97	15.33
160	161	78.00	-215.93	-2.97	19.49
161	1161	78.00	-207.27	-1.93	19.71
161	162	79.10	-207.27	-1.93	21.84
162	162	79.10	-199.95	-0.86	21.86
162	163	80.20	-199.95	-0.86	22.81
163	163	80.20	-191.25	0.15	22.66
163	164	81.30	-191.25	0.15	22.49
164	164	81.30	-181.15	1.03	22.14
164	165	82.40	-181.15	1.03	21.01
165	165	82.40	-169.64	1.71	20.45
165	166	83.50	-169.64	1.71	18.57
166	166	83.50	-157.61	2.14	18.00
166	167	84.60	-157.61	2.14	15.65
167	167	84.60	-145.04	2.32	15.05
167	168	85.70	-145.04	2.32	12.50
168	168	85.70	-132.83	2.27	12.06
168	169	86.80	-132.83	2.27	9.57
169	169	86.80	-120.92	2.06	9.27
169	170	87.90	-120.92	2.06	7.00
170	170	87.90	-109.29	1.75	6.83
170	171	89.00	-109.29	1.75	4.90
171	171	89.00	-97.90	1.39	4.85
171	172	90.10	-97.90	1.39	3.32
172	172	90.10	-86.72	1.02	3.36
172	173	91.20	-86.72	1.02	2.24
173	173	91.20	-75.71	0.68	2.38
173	174	92.30	-75.71	0.68	1.63

CÁLCULO TENSIONAL

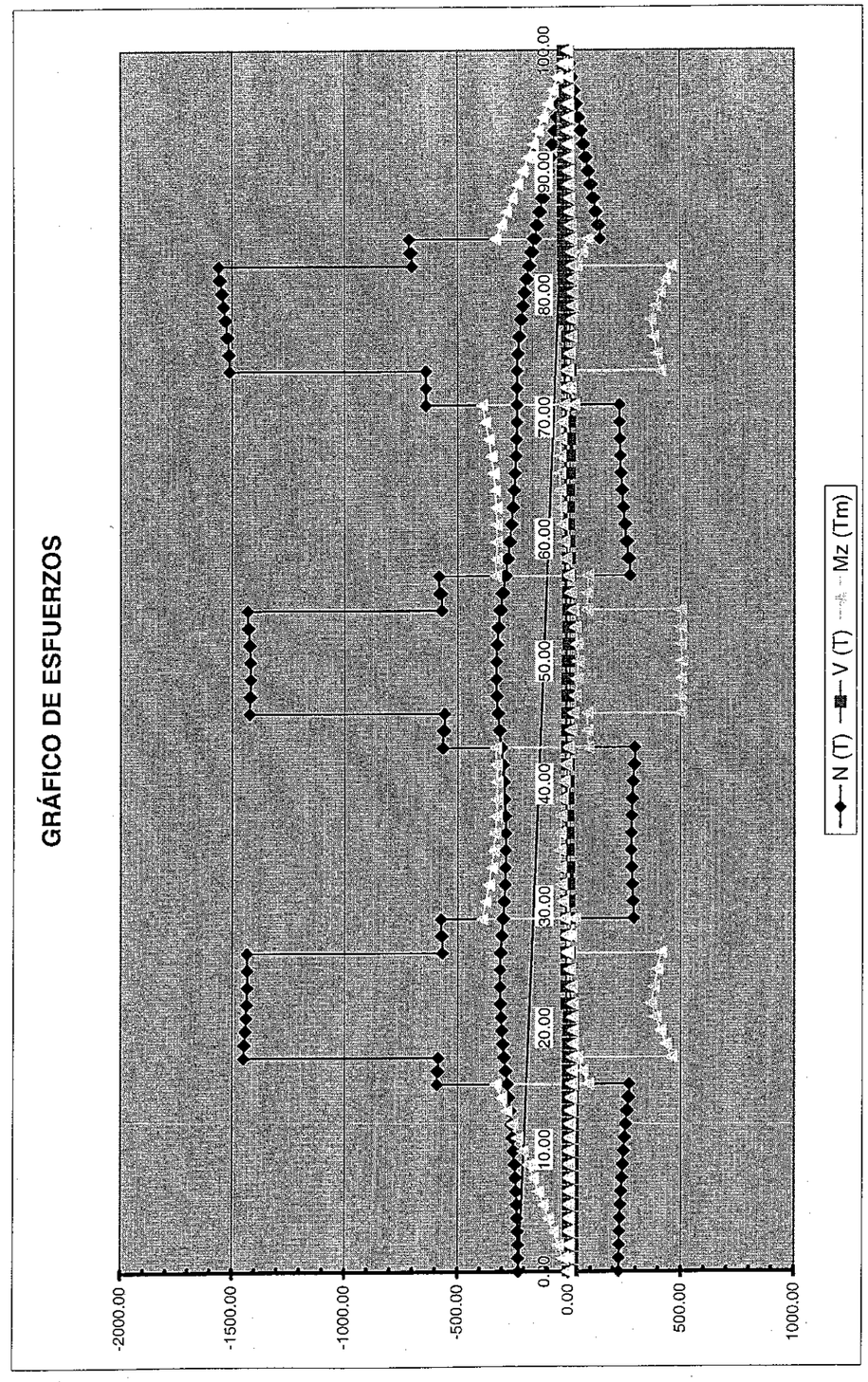
Hipótesis de cálculo:
ej1posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [1; 1]ej1posEI.FAM2.TOT + [1; 1]ej1posEI.FAM3.TOT + [1; 1]ej1posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-64.85	0.40	1.85
174	175	93.40	-64.85	0.40	1.40
175	175	93.40	-54.11	0.22	1.69
175	176	94.50	-54.11	0.22	1.44
176	176	94.50	-43.46	0.17	1.78
176	177	95.60	-43.46	0.17	1.60
177	177	95.60	-32.88	0.25	2.00
177	178	96.70	-32.88	0.25	1.72
178	178	96.70	-22.35	0.51	2.15
178	179	97.80	-22.35	0.51	1.59
179	179	97.80	-11.84	0.95	2.05
179	180	98.90	-11.84	0.95	1.01
180	180	98.90	-1.32	1.58	1.50
180	181	100.00	-1.32	1.58	-0.24



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	225.60	21.91	0.24
1	2	1.10	225.60	21.91	-23.86
2	2	1.10	226.45	21.27	-23.37
2	3	2.20	226.45	21.27	-46.77
3	3	2.20	227.77	20.83	-46.31
3	4	3.30	227.77	20.83	-69.23
4	4	3.30	229.54	20.58	-68.79
4	5	4.40	229.54	20.58	-91.43
5	5	4.40	231.75	20.49	-91.04
5	6	5.50	231.75	20.49	-113.58
6	6	5.50	234.40	20.55	-113.24
6	7	6.60	234.40	20.55	-135.84
7	7	6.60	237.48	20.73	-135.56
7	8	7.70	237.48	20.73	-158.36
8	8	7.70	241.01	21.01	-158.15
8	9	8.80	241.01	21.01	-181.25
9	9	8.80	244.98	21.35	-181.12
9	10	9.90	244.98	21.35	-204.60
10	10	9.90	249.41	21.72	-204.56
10	11	11.00	249.41	21.72	-228.44
11	11	11.00	254.31	22.08	-228.50
11	12	12.10	254.31	22.08	-252.79
12	12	12.10	259.71	22.39	-252.96
12	13	13.20	259.71	22.39	-277.59
13	13	13.20	265.64	22.60	-277.89
13	14	14.30	265.64	22.60	-302.75
14	14	14.30	272.13	22.65	-303.18
14	15	15.40	272.13	22.65	-328.10
15	15	15.40	279.22	22.47	-328.69
15	16	16.50	279.22	22.47	-353.41
16	16	16.50	286.01	22.04	-353.98
16	17	17.60	286.01	22.04	-378.23
17	17	17.60	292.54	21.36	-378.78
17	18	18.70	292.54	21.36	-402.28
18	18	18.70	297.91	20.48	-402.63
18	19	19.80	297.91	20.48	-425.15
19	19	19.80	302.13	19.47	-425.31
19	20	20.90	302.13	19.47	-446.72
20	20	20.90	305.24	18.40	-446.70
20	21	22.00	305.24	18.40	-466.94
21	1021	22.00	308.15	-8.75	-466.71
21	22	23.40	308.15	-8.75	-454.47
22	22	23.40	309.35	-9.95	-453.93
22	23	24.80	309.35	-9.95	-440.00
23	23	24.80	307.66	-10.87	-439.18
23	24	26.20	307.66	-10.87	-423.96
24	24	26.20	303.03	-11.36	-422.82
24	25	27.60	303.03	-11.36	-406.92
25	25	27.60	297.80	-11.32	-405.78
25	26	29.00	297.80	-11.32	-389.93
26	26	29.00	291.80	-10.76	-388.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	291.80	-10.76	-373.70
27	27	30.40	287.37	-9.73	-372.82
27	28	31.80	287.37	-9.73	-359.19
28	28	31.80	284.35	-8.37	-358.56
28	29	33.20	284.35	-8.37	-346.84
29	29	33.20	282.66	-6.80	-346.45
29	30	34.60	282.66	-6.80	-336.93
30	30	34.60	282.21	-5.11	-336.77
30	31	36.00	282.21	-5.11	-329.61
31	31	36.00	283.01	-3.43	-329.66
31	32	37.40	283.01	-3.43	-324.87
32	32	37.40	285.03	-1.83	-325.14
32	33	38.80	285.03	-1.83	-322.59
33	33	38.80	288.33	-0.41	-323.08
33	34	40.20	288.33	-0.41	-322.50
34	34	40.20	292.98	0.71	-323.22
34	35	41.60	292.98	0.71	-324.21
35	35	41.60	299.08	1.42	-325.16
35	36	43.00	299.08	1.42	-327.15
36	36	43.00	306.79	1.62	-328.35
36	37	44.40	306.79	1.62	-330.62
37	37	44.40	313.81	1.23	-331.76
37	38	45.80	313.81	1.23	-333.48
38	38	45.80	320.31	0.30	-334.57
38	39	47.20	320.31	0.30	-334.99
39	39	47.20	323.97	-1.08	-335.71
39	40	48.60	323.97	-1.08	-334.20
40	40	48.60	324.86	-2.72	-334.56
40	41	50.00	324.86	-2.72	-330.74
41	1041	50.00	323.00	2.72	-330.74
41	42	51.40	323.00	2.72	-334.56
42	42	51.40	318.38	1.08	-334.20
42	43	52.80	318.38	1.08	-335.71
43	43	52.80	310.98	-0.30	-334.99
43	44	54.20	310.98	-0.30	-334.57
44	44	54.20	300.72	-1.23	-333.49
44	45	55.60	300.72	-1.23	-331.76
45	45	55.60	289.90	-1.62	-330.62
45	46	57.00	289.90	-1.62	-328.36
46	46	57.00	278.33	-1.42	-327.15
46	47	58.40	278.33	-1.42	-325.16
47	47	58.40	268.33	-0.70	-324.21
47	48	59.80	268.33	-0.70	-323.22
48	48	59.80	259.69	0.41	-322.50
48	49	61.20	259.69	0.41	-323.09
49	49	61.20	252.31	1.83	-322.59
49	50	62.60	252.31	1.83	-325.15
50	50	62.60	246.10	3.42	-324.87
50	51	64.00	246.10	3.42	-329.67
51	51	64.00	240.98	5.12	-329.61
51	52	65.40	240.98	5.12	-336.77

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	236.94	6.80	-336.94
52	53	66.80	236.94	6.80	-346.45
53	53	66.80	233.96	8.37	-346.85
53	54	68.20	233.96	8.37	-358.57
54	54	68.20	232.09	9.73	-359.20
54	55	69.60	232.09	9.73	-372.82
55	55	69.60	231.35	10.76	-373.71
55	56	71.00	231.35	10.76	-388.77
56	56	71.00	231.87	11.32	-389.94
56	57	72.40	231.87	11.32	-405.78
57	57	72.40	231.26	11.35	-406.93
57	58	73.80	231.26	11.35	-422.82
58	58	73.80	229.61	10.87	-423.96
58	59	75.20	229.61	10.87	-439.18
59	59	75.20	224.52	9.95	-440.00
59	60	76.60	224.52	9.95	-453.93
60	60	76.60	215.93	8.74	-454.46
60	61	78.00	215.93	8.74	-466.70
61	1061	78.00	207.27	-18.40	-466.93
61	62	79.10	207.27	-18.40	-446.69
62	62	79.10	199.95	-19.47	-446.72
62	63	80.20	199.95	-19.47	-425.30
63	63	80.20	191.25	-20.48	-425.15
63	64	81.30	191.25	-20.48	-402.62
64	64	81.30	181.15	-21.36	-402.27
64	65	82.40	181.15	-21.36	-378.77
65	65	82.40	169.64	-22.04	-378.22
65	66	83.50	169.64	-22.04	-353.98
66	66	83.50	157.61	-22.47	-353.41
66	67	84.60	157.61	-22.47	-328.69
67	67	84.60	145.04	-22.65	-328.09
67	68	85.70	145.04	-22.65	-303.18
68	68	85.70	132.83	-22.60	-302.75
68	69	86.80	132.83	-22.60	-277.89
69	69	86.80	120.92	-22.39	-277.59
69	70	87.90	120.92	-22.39	-252.96
70	70	87.90	109.29	-22.08	-252.79
70	71	89.00	109.29	-22.08	-228.50
71	71	89.00	97.90	-21.72	-228.45
71	72	90.10	97.90	-21.72	-204.56
72	72	90.10	86.72	-21.35	-204.60
72	73	91.20	86.72	-21.35	-181.12
73	73	91.20	75.71	-21.01	-181.26
73	74	92.30	75.71	-21.01	-158.15
74	74	92.30	64.85	-20.73	-158.37
74	75	93.40	64.85	-20.73	-135.56
75	75	93.40	54.11	-20.55	-135.84
75	76	94.50	54.11	-20.55	-113.24
76	76	94.50	43.46	-20.49	-113.58
76	77	95.60	43.46	-20.49	-91.04
77	77	95.60	32.88	-20.58	-91.44

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	32.88	-20.58	-68.80
78	78	96.70	22.35	-20.84	-69.23
78	79	97.80	22.35	-20.84	-46.31
79	79	97.80	11.84	-21.27	-46.78
79	80	98.90	11.84	-21.27	-23.37
80	80	98.90	1.32	-21.91	-23.86
80	81	100.00	1.32	-21.91	0.24
101	101	0.00	-225.60	-1.58	-0.24
101	102	1.10	-225.60	-1.58	1.50
102	102	1.10	-226.45	-0.95	1.01
102	103	2.20	-226.45	-0.95	2.05
103	103	2.20	-227.77	-0.51	1.59
103	104	3.30	-227.77	-0.51	2.15
104	104	3.30	-229.54	-0.25	1.72
104	105	4.40	-229.54	-0.25	2.00
105	105	4.40	-231.75	-0.17	1.60
105	106	5.50	-231.75	-0.17	1.78
106	106	5.50	-234.40	-0.22	1.44
106	107	6.60	-234.40	-0.22	1.69
107	107	6.60	-237.48	-0.40	1.40
107	108	7.70	-237.48	-0.40	1.85
108	108	7.70	-241.01	-0.68	1.63
108	109	8.80	-241.01	-0.68	2.38
109	109	8.80	-244.98	-1.02	2.24
109	110	9.90	-244.98	-1.02	3.36
110	110	9.90	-249.41	-1.39	3.32
110	111	11.00	-249.41	-1.39	4.85
111	111	11.00	-254.31	-1.75	4.90
111	112	12.10	-254.31	-1.75	6.83
112	112	12.10	-259.71	-2.06	7.00
112	113	13.20	-259.71	-2.06	9.27
113	113	13.20	-265.64	-2.27	9.57
113	114	14.30	-265.64	-2.27	12.06
114	114	14.30	-272.13	-2.32	12.50
114	115	15.40	-272.13	-2.32	15.05
115	115	15.40	-279.22	-2.14	15.64
115	116	16.50	-279.22	-2.14	18.00
116	116	16.50	-286.01	-1.71	18.57
116	117	17.60	-286.01	-1.71	20.45
117	117	17.60	-292.54	-1.03	21.00
117	118	18.70	-292.54	-1.03	22.14
118	118	18.70	-297.91	-0.15	22.49
118	119	19.80	-297.91	-0.15	22.65
119	119	19.80	-302.13	0.86	22.81
119	120	20.90	-302.13	0.86	21.86
120	120	20.90	-305.24	1.93	21.83
120	121	22.00	-305.24	1.93	19.71
121	1121	22.00	-308.15	2.97	19.48
121	122	23.40	-308.15	2.97	15.33
122	122	23.40	-309.35	4.17	14.80
122	123	24.80	-309.35	4.17	8.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-307.66	5.09	8.13
123	124	26.20	-307.66	5.09	1.00
124	124	26.20	-303.03	5.58	-0.13
124	125	27.60	-303.03	5.58	-7.94
125	125	27.60	-297.80	5.55	-9.09
125	126	29.00	-297.80	5.55	-16.85
126	126	29.00	-291.80	4.98	-18.02
126	127	30.40	-291.80	4.98	-25.00
127	127	30.40	-287.37	3.96	-25.88
127	128	31.80	-287.37	3.96	-31.43
128	128	31.80	-284.35	2.60	-32.06
128	129	33.20	-284.35	2.60	-35.70
129	129	33.20	-282.66	1.03	-36.10
129	130	34.60	-282.66	1.03	-37.54
130	130	34.60	-282.21	-0.65	-37.71
130	131	36.00	-282.21	-0.65	-36.80
131	131	36.00	-283.01	-2.34	-36.74
131	132	37.40	-283.01	-2.34	-33.47
132	132	37.40	-285.03	-3.93	-33.19
132	133	38.80	-285.03	-3.93	-27.69
133	133	38.80	-288.33	-5.34	-27.19
133	134	40.20	-288.33	-5.34	-19.71
134	134	40.20	-292.98	-6.46	-18.99
134	135	41.60	-292.98	-6.46	-9.95
135	135	41.60	-299.08	-7.18	-9.00
135	136	43.00	-299.08	-7.18	1.05
136	136	43.00	-306.79	-7.37	2.25
136	137	44.40	-306.79	-7.37	12.57
137	137	44.40	-313.81	-6.98	13.71
137	138	45.80	-313.81	-6.98	23.49
138	138	45.80	-320.31	-6.05	24.58
138	139	47.20	-320.31	-6.05	33.04
139	139	47.20	-323.97	-4.67	33.76
139	140	48.60	-323.97	-4.67	40.30
140	140	48.60	-324.86	-3.03	40.66
140	141	50.00	-324.86	-3.03	44.90
141	1141	50.00	-323.00	3.03	44.90
141	142	51.40	-323.00	3.03	40.66
142	142	51.40	-318.38	4.67	40.30
142	143	52.80	-318.38	4.67	33.76
143	143	52.80	-310.98	6.05	33.04
143	144	54.20	-310.98	6.05	24.57
144	144	54.20	-300.72	6.98	23.48
144	145	55.60	-300.72	6.98	13.71
145	145	55.60	-289.90	7.37	12.57
145	146	57.00	-289.90	7.37	2.25
146	146	57.00	-278.33	7.18	1.05
146	147	58.40	-278.33	7.18	-9.00
147	147	58.40	-268.33	6.46	-9.95
147	148	59.80	-268.33	6.46	-19.00
148	148	59.80	-259.69	5.34	-19.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-259.69	5.34	-27.20
149	149	61.20	-252.31	3.93	-27.69
149	150	62.60	-252.31	3.93	-33.20
150	150	62.60	-246.10	2.34	-33.47
150	151	64.00	-246.10	2.34	-36.74
151	151	64.00	-240.98	0.65	-36.80
151	152	65.40	-240.98	0.65	-37.71
152	152	65.40	-236.94	-1.03	-37.54
152	153	66.80	-236.94	-1.03	-36.10
153	153	66.80	-233.96	-2.60	-35.71
153	154	68.20	-233.96	-2.60	-32.06
154	154	68.20	-232.09	-3.96	-31.43
154	155	69.60	-232.09	-3.96	-25.89
155	155	69.60	-231.35	-4.98	-25.00
155	156	71.00	-231.35	-4.98	-18.02
156	156	71.00	-231.87	-5.55	-16.85
156	157	72.40	-231.87	-5.55	-9.09
157	157	72.40	-231.26	-5.58	-7.95
157	158	73.80	-231.26	-5.58	-0.13
158	158	73.80	-229.62	-5.09	1.00
158	159	75.20	-229.62	-5.09	8.13
159	159	75.20	-224.52	-4.17	8.96
159	160	76.60	-224.52	-4.17	14.80
160	160	76.60	-215.93	-2.97	15.33
160	161	78.00	-215.93	-2.97	19.49
161	1161	78.00	-207.27	-1.93	19.71
161	162	79.10	-207.27	-1.93	21.84
162	162	79.10	-199.95	-0.86	21.86
162	163	80.20	-199.95	-0.86	22.81
163	163	80.20	-191.25	0.15	22.66
163	164	81.30	-191.25	0.15	22.49
164	164	81.30	-181.15	1.03	22.14
164	165	82.40	-181.15	1.03	21.01
165	165	82.40	-169.64	1.71	20.45
165	166	83.50	-169.64	1.71	18.57
166	166	83.50	-157.61	2.14	18.00
166	167	84.60	-157.61	2.14	15.65
167	167	84.60	-145.04	2.32	15.05
167	168	85.70	-145.04	2.32	12.50
168	168	85.70	-132.83	2.27	12.06
168	169	86.80	-132.83	2.27	9.57
169	169	86.80	-120.92	2.06	9.27
169	170	87.90	-120.92	2.06	7.00
170	170	87.90	-109.29	1.75	6.83
170	171	89.00	-109.29	1.75	4.90
171	171	89.00	-97.90	1.39	4.85
171	172	90.10	-97.90	1.39	3.32
172	172	90.10	-86.72	1.02	3.36
172	173	91.20	-86.72	1.02	2.24
173	173	91.20	-75.71	0.68	2.38
173	174	92.30	-75.71	0.68	1.63

CÁLCULO TENSIONAL

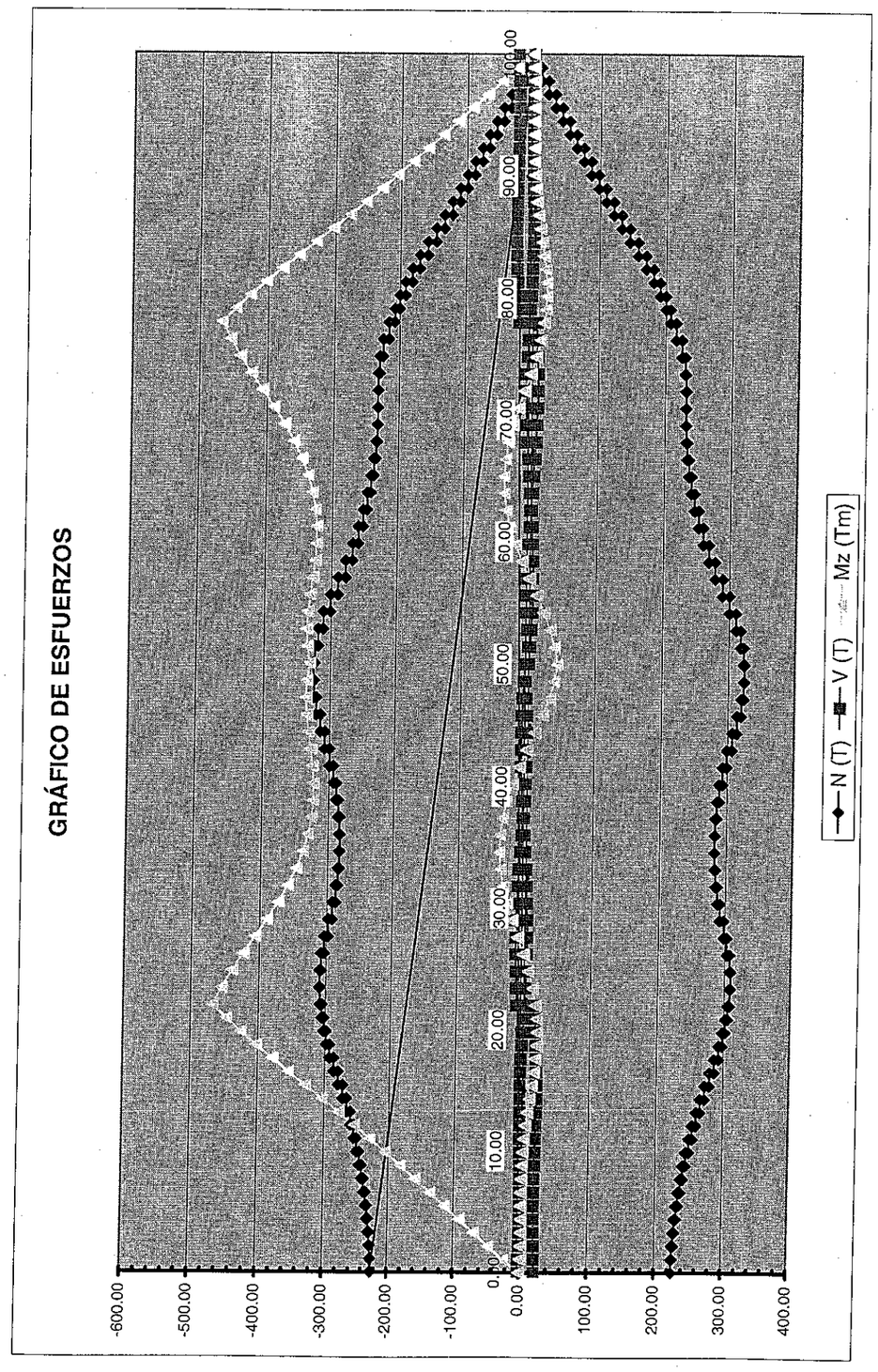
Hipótesis de cálculo:
ej1posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-64.85	0.40	1.85
174	175	93.40	-64.85	0.40	1.40
175	175	93.40	-54.11	0.22	1.69
175	176	94.50	-54.11	0.22	1.44
176	176	94.50	-43.46	0.17	1.78
176	177	95.60	-43.46	0.17	1.60
177	177	95.60	-32.88	0.25	2.00
177	178	96.70	-32.88	0.25	1.72
178	178	96.70	-22.35	0.51	2.15
178	179	97.80	-22.35	0.51	1.59
179	179	97.80	-11.84	0.95	2.05
179	180	98.90	-11.84	0.95	1.01
180	180	98.90	-1.32	1.58	1.50
180	181	100.00	-1.32	1.58	-0.24



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	225.60	21.91	0.24
1	2	1.10	225.60	21.91	-23.86
2	2	1.10	226.45	21.27	-23.37
2	3	2.20	226.45	21.27	-46.77
3	3	2.20	227.77	20.83	-46.31
3	4	3.30	227.77	20.83	-69.23
4	4	3.30	229.54	20.58	-68.79
4	5	4.40	229.54	20.58	-91.43
5	5	4.40	231.75	20.49	-91.04
5	6	5.50	231.75	20.49	-113.58
6	6	5.50	234.40	20.55	-113.24
6	7	6.60	234.40	20.55	-135.84
7	7	6.60	237.48	20.73	-135.56
7	8	7.70	237.48	20.73	-158.36
8	8	7.70	241.01	21.01	-158.15
8	9	8.80	241.01	21.01	-181.25
9	9	8.80	244.98	21.35	-181.12
9	10	9.90	244.98	21.35	-204.60
10	10	9.90	249.41	21.72	-204.56
10	11	11.00	249.41	21.72	-228.44
11	11	11.00	254.31	22.08	-228.50
11	12	12.10	254.31	22.08	-252.79
12	12	12.10	259.71	22.39	-252.96
12	13	13.20	259.71	22.39	-277.59
13	13	13.20	265.64	22.60	-277.89
13	14	14.30	265.64	22.60	-302.75
14	14	14.30	272.13	22.65	-303.18
14	15	15.40	272.13	22.65	-328.10
15	15	15.40	279.22	22.47	-328.69
15	16	16.50	279.22	22.47	-353.41
16	16	16.50	286.01	22.04	-353.98
16	17	17.60	286.01	22.04	-378.23
17	17	17.60	292.54	21.36	-378.78
17	18	18.70	292.54	21.36	-402.28
18	18	18.70	297.91	20.48	-402.63
18	19	19.80	297.91	20.48	-425.15
19	19	19.80	302.13	19.47	-425.31
19	20	20.90	302.13	19.47	-446.72
20	20	20.90	305.24	18.40	-446.70
20	21	22.00	305.24	18.40	-466.94
21	1021	22.00	308.15	-8.75	-466.71
21	22	23.40	308.15	-8.75	-454.47
22	22	23.40	309.35	-9.95	-453.93
22	23	24.80	309.35	-9.95	-440.00
23	23	24.80	307.66	-10.87	-439.18
23	24	26.20	307.66	-10.87	-423.96
24	24	26.20	303.03	-11.36	-422.82
24	25	27.60	303.03	-11.36	-406.92
25	25	27.60	297.80	-11.32	-405.78
25	26	29.00	297.80	-11.32	-389.93
26	26	29.00	291.80	-10.76	-388.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEI.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	291.80	-10.76	-373.70
27	27	30.40	287.37	-9.73	-372.82
27	28	31.80	287.37	-9.73	-359.19
28	28	31.80	284.35	-8.37	-358.56
28	29	33.20	284.35	-8.37	-346.84
29	29	33.20	282.66	-6.80	-346.45
29	30	34.60	282.66	-6.80	-336.93
30	30	34.60	282.21	-5.11	-336.77
30	31	36.00	282.21	-5.11	-329.61
31	31	36.00	283.01	-3.43	-329.66
31	32	37.40	283.01	-3.43	-324.87
32	32	37.40	285.03	-1.83	-325.14
32	33	38.80	285.03	-1.83	-322.59
33	33	38.80	288.33	-0.41	-323.08
33	34	40.20	288.33	-0.41	-322.50
34	34	40.20	292.98	0.71	-323.22
34	35	41.60	292.98	0.71	-324.21
35	35	41.60	299.08	1.42	-325.16
35	36	43.00	299.08	1.42	-327.15
36	36	43.00	306.79	1.62	-328.35
36	37	44.40	306.79	1.62	-330.62
37	37	44.40	313.81	1.23	-331.76
37	38	45.80	313.81	1.23	-333.48
38	38	45.80	320.31	0.30	-334.57
38	39	47.20	320.31	0.30	-334.99
39	39	47.20	323.97	-1.08	-335.71
39	40	48.60	323.97	-1.08	-334.20
40	40	48.60	324.86	-2.72	-334.56
40	41	50.00	324.86	-2.72	-330.74
41	1041	50.00	323.00	2.72	-330.74
41	42	51.40	323.00	2.72	-334.56
42	42	51.40	318.38	1.08	-334.20
42	43	52.80	318.38	1.08	-335.71
43	43	52.80	310.98	-0.30	-334.99
43	44	54.20	310.98	-0.30	-334.57
44	44	54.20	300.72	-1.23	-333.49
44	45	55.60	300.72	-1.23	-331.76
45	45	55.60	289.90	-1.62	-330.62
45	46	57.00	289.90	-1.62	-328.36
46	46	57.00	278.33	-1.42	-327.15
46	47	58.40	278.33	-1.42	-325.16
47	47	58.40	268.33	-0.70	-324.21
47	48	59.80	268.33	-0.70	-323.22
48	48	59.80	259.69	0.41	-322.50
48	49	61.20	259.69	0.41	-323.09
49	49	61.20	252.31	1.83	-322.59
49	50	62.60	252.31	1.83	-325.15
50	50	62.60	246.10	3.42	-324.87
50	51	64.00	246.10	3.42	-329.67
51	51	64.00	240.98	5.12	-329.61
51	52	65.40	240.98	5.12	-336.77

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEl.FAM1.TOT + [-1;-1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.TOT + [-1;-1]ej1posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	236.94	6.80	-336.94
52	53	66.80	236.94	6.80	-346.45
53	53	66.80	233.96	8.37	-346.85
53	54	68.20	233.96	8.37	-358.57
54	54	68.20	232.09	9.73	-359.20
54	55	69.60	232.09	9.73	-372.82
55	55	69.60	231.35	10.76	-373.71
55	56	71.00	231.35	10.76	-388.77
56	56	71.00	231.87	11.32	-389.94
56	57	72.40	231.87	11.32	-405.78
57	57	72.40	231.26	11.35	-406.93
57	58	73.80	231.26	11.35	-422.82
58	58	73.80	229.61	10.87	-423.96
58	59	75.20	229.61	10.87	-439.18
59	59	75.20	224.52	9.95	-440.00
59	60	76.60	224.52	9.95	-453.93
60	60	76.60	215.93	8.74	-454.46
60	61	78.00	215.93	8.74	-466.70
61	1061	78.00	207.27	-18.40	-466.93
61	62	79.10	207.27	-18.40	-446.69
62	62	79.10	199.95	-19.47	-446.72
62	63	80.20	199.95	-19.47	-425.30
63	63	80.20	191.25	-20.48	-425.15
63	64	81.30	191.25	-20.48	-402.62
64	64	81.30	181.15	-21.36	-402.27
64	65	82.40	181.15	-21.36	-378.77
65	65	82.40	169.64	-22.04	-378.22
65	66	83.50	169.64	-22.04	-353.98
66	66	83.50	157.61	-22.47	-353.41
66	67	84.60	157.61	-22.47	-328.69
67	67	84.60	145.04	-22.65	-328.09
67	68	85.70	145.04	-22.65	-303.18
68	68	85.70	132.83	-22.60	-302.75
68	69	86.80	132.83	-22.60	-277.89
69	69	86.80	120.92	-22.39	-277.59
69	70	87.90	120.92	-22.39	-252.96
70	70	87.90	109.29	-22.08	-252.79
70	71	89.00	109.29	-22.08	-228.50
71	71	89.00	97.90	-21.72	-228.45
71	72	90.10	97.90	-21.72	-204.56
72	72	90.10	86.72	-21.35	-204.60
72	73	91.20	86.72	-21.35	-181.12
73	73	91.20	75.71	-21.01	-181.26
73	74	92.30	75.71	-21.01	-158.15
74	74	92.30	64.85	-20.73	-158.37
74	75	93.40	64.85	-20.73	-135.56
75	75	93.40	54.11	-20.55	-135.84
75	76	94.50	54.11	-20.55	-113.24
76	76	94.50	43.46	-20.49	-113.58
76	77	95.60	43.46	-20.49	-91.04
77	77	95.60	32.88	-20.58	-91.44

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEl.FAM1.TOT + [-1;-1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.TOT + [-1;-1]ej1posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	32.88	-20.58	-68.80
78	78	96.70	22.35	-20.84	-69.23
78	79	97.80	22.35	-20.84	-46.31
79	79	97.80	11.84	-21.27	-46.78
79	80	98.90	11.84	-21.27	-23.37
80	80	98.90	1.32	-21.91	-23.86
80	81	100.00	1.32	-21.91	0.24
101	101	0.00	-225.60	-1.58	-0.24
101	102	1.10	-225.60	-1.58	1.50
102	102	1.10	-226.45	-0.95	1.01
102	103	2.20	-226.45	-0.95	2.05
103	103	2.20	-227.77	-0.51	1.59
103	104	3.30	-227.77	-0.51	2.15
104	104	3.30	-229.54	-0.25	1.72
104	105	4.40	-229.54	-0.25	2.00
105	105	4.40	-231.75	-0.17	1.60
105	106	5.50	-231.75	-0.17	1.78
106	106	5.50	-234.40	-0.22	1.44
106	107	6.60	-234.40	-0.22	1.69
107	107	6.60	-237.48	-0.40	1.40
107	108	7.70	-237.48	-0.40	1.85
108	108	7.70	-241.01	-0.68	1.63
108	109	8.80	-241.01	-0.68	2.38
109	109	8.80	-244.98	-1.02	2.24
109	110	9.90	-244.98	-1.02	3.36
110	110	9.90	-249.41	-1.39	3.32
110	111	11.00	-249.41	-1.39	4.85
111	111	11.00	-254.31	-1.75	4.90
111	112	12.10	-254.31	-1.75	6.83
112	112	12.10	-259.71	-2.06	7.00
112	113	13.20	-259.71	-2.06	9.27
113	113	13.20	-265.64	-2.27	9.57
113	114	14.30	-265.64	-2.27	12.06
114	114	14.30	-272.13	-2.32	12.50
114	115	15.40	-272.13	-2.32	15.05
115	115	15.40	-279.22	-2.14	15.64
115	116	16.50	-279.22	-2.14	18.00
116	116	16.50	-286.01	-1.71	18.57
116	117	17.60	-286.01	-1.71	20.45
117	117	17.60	-292.54	-1.03	21.00
117	118	18.70	-292.54	-1.03	22.14
118	118	18.70	-297.91	-0.15	22.49
118	119	19.80	-297.91	-0.15	22.65
119	119	19.80	-302.13	0.86	22.81
119	120	20.90	-302.13	0.86	21.86
120	120	20.90	-305.24	1.93	21.83
120	121	22.00	-305.24	1.93	19.71
121	1121	22.00	-308.15	2.97	19.48
121	122	23.40	-308.15	2.97	15.33
122	122	23.40	-309.35	4.17	14.80
122	123	24.80	-309.35	4.17	8.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEl.FAM1.TOT + [-1;-1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.TOT + [-1;-1]ej1posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-307.66	5.09	8.13
123	124	26.20	-307.66	5.09	1.00
124	124	26.20	-303.03	5.58	-0.13
124	125	27.60	-303.03	5.58	-7.94
125	125	27.60	-297.80	5.55	-9.09
125	126	29.00	-297.80	5.55	-16.85
126	126	29.00	-291.80	4.98	-18.02
126	127	30.40	-291.80	4.98	-25.00
127	127	30.40	-287.37	3.96	-25.88
127	128	31.80	-287.37	3.96	-31.43
128	128	31.80	-284.35	2.60	-32.06
128	129	33.20	-284.35	2.60	-35.70
129	129	33.20	-282.66	1.03	-36.10
129	130	34.60	-282.66	1.03	-37.54
130	130	34.60	-282.21	-0.65	-37.71
130	131	36.00	-282.21	-0.65	-36.80
131	131	36.00	-283.01	-2.34	-36.74
131	132	37.40	-283.01	-2.34	-33.47
132	132	37.40	-285.03	-3.93	-33.19
132	133	38.80	-285.03	-3.93	-27.69
133	133	38.80	-288.33	-5.34	-27.19
133	134	40.20	-288.33	-5.34	-19.71
134	134	40.20	-292.98	-6.46	-18.99
134	135	41.60	-292.98	-6.46	-9.95
135	135	41.60	-299.08	-7.18	-9.00
135	136	43.00	-299.08	-7.18	1.05
136	136	43.00	-306.79	-7.37	2.25
136	137	44.40	-306.79	-7.37	12.57
137	137	44.40	-313.81	-6.98	13.71
137	138	45.80	-313.81	-6.98	23.49
138	138	45.80	-320.31	-6.05	24.58
138	139	47.20	-320.31	-6.05	33.04
139	139	47.20	-323.97	-4.67	33.76
139	140	48.60	-323.97	-4.67	40.30
140	140	48.60	-324.86	-3.03	40.66
140	141	50.00	-324.86	-3.03	44.90
141	1141	50.00	-323.00	3.03	44.90
141	142	51.40	-323.00	3.03	40.66
142	142	51.40	-318.38	4.67	40.30
142	143	52.80	-318.38	4.67	33.76
143	143	52.80	-310.98	6.05	33.04
143	144	54.20	-310.98	6.05	24.57
144	144	54.20	-300.72	6.98	23.48
144	145	55.60	-300.72	6.98	13.71
145	145	55.60	-289.90	7.37	12.57
145	146	57.00	-289.90	7.37	2.25
146	146	57.00	-278.33	7.18	1.05
146	147	58.40	-278.33	7.18	-9.00
147	147	58.40	-268.33	6.46	-9.95
147	148	59.80	-268.33	6.46	-19.00
148	148	59.80	-259.69	5.34	-19.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEl.FAM1.TOT + [-1;-1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.TOT + [-1;-1]ej1posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-259.69	5.34	-27.20
149	149	61.20	-252.31	3.93	-27.69
149	150	62.60	-252.31	3.93	-33.20
150	150	62.60	-246.10	2.34	-33.47
150	151	64.00	-246.10	2.34	-36.74
151	151	64.00	-240.98	0.65	-36.80
151	152	65.40	-240.98	0.65	-37.71
152	152	65.40	-236.94	-1.03	-37.54
152	153	66.80	-236.94	-1.03	-36.10
153	153	66.80	-233.96	-2.60	-35.71
153	154	68.20	-233.96	-2.60	-32.06
154	154	68.20	-232.09	-3.96	-31.43
154	155	69.60	-232.09	-3.96	-25.89
155	155	69.60	-231.35	-4.98	-25.00
155	156	71.00	-231.35	-4.98	-18.02
156	156	71.00	-231.87	-5.55	-16.85
156	157	72.40	-231.87	-5.55	-9.09
157	157	72.40	-231.26	-5.58	-7.95
157	158	73.80	-231.26	-5.58	-0.13
158	158	73.80	-229.62	-5.09	1.00
158	159	75.20	-229.62	-5.09	8.13
159	159	75.20	-224.52	-4.17	8.96
159	160	76.60	-224.52	-4.17	14.80
160	160	76.60	-215.93	-2.97	15.33
160	161	78.00	-215.93	-2.97	19.49
161	1161	78.00	-207.27	-1.93	19.71
161	162	79.10	-207.27	-1.93	21.84
162	162	79.10	-199.95	-0.86	21.86
162	163	80.20	-199.95	-0.86	22.81
163	163	80.20	-191.25	0.15	22.66
163	164	81.30	-191.25	0.15	22.49
164	164	81.30	-181.15	1.03	22.14
164	165	82.40	-181.15	1.03	21.01
165	165	82.40	-169.64	1.71	20.45
165	166	83.50	-169.64	1.71	18.57
166	166	83.50	-157.61	2.14	18.00
166	167	84.60	-157.61	2.14	15.65
167	167	84.60	-145.04	2.32	15.05
167	168	85.70	-145.04	2.32	12.50
168	168	85.70	-132.83	2.27	12.06
168	169	86.80	-132.83	2.27	9.57
169	169	86.80	-120.92	2.06	9.27
169	170	87.90	-120.92	2.06	7.00
170	170	87.90	-109.29	1.75	6.83
170	171	89.00	-109.29	1.75	4.90
171	171	89.00	-97.90	1.39	4.85
171	172	90.10	-97.90	1.39	3.32
172	172	90.10	-86.72	1.02	3.36
172	173	91.20	-86.72	1.02	2.24
173	173	91.20	-75.71	0.68	2.38
173	174	92.30	-75.71	0.68	1.63

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej1posEI.FAM1.TOT + [-1;-1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.TOT + [-1;-1]ej1posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-64.85	0.40	1.85
174	175	93.40	-64.85	0.40	1.40
175	175	93.40	-54.11	0.22	1.69
175	176	94.50	-54.11	0.22	1.44
176	176	94.50	-43.46	0.17	1.78
176	177	95.60	-43.46	0.17	1.60
177	177	95.60	-32.88	0.25	2.00
177	178	96.70	-32.88	0.25	1.72
178	178	96.70	-22.35	0.51	2.15
178	179	97.80	-22.35	0.51	1.59
179	179	97.80	-11.84	0.95	2.05
179	180	98.90	-11.84	0.95	1.01
180	180	98.90	-1.32	1.58	1.50
180	181	100.00	-1.32	1.58	-0.24

11/09/03

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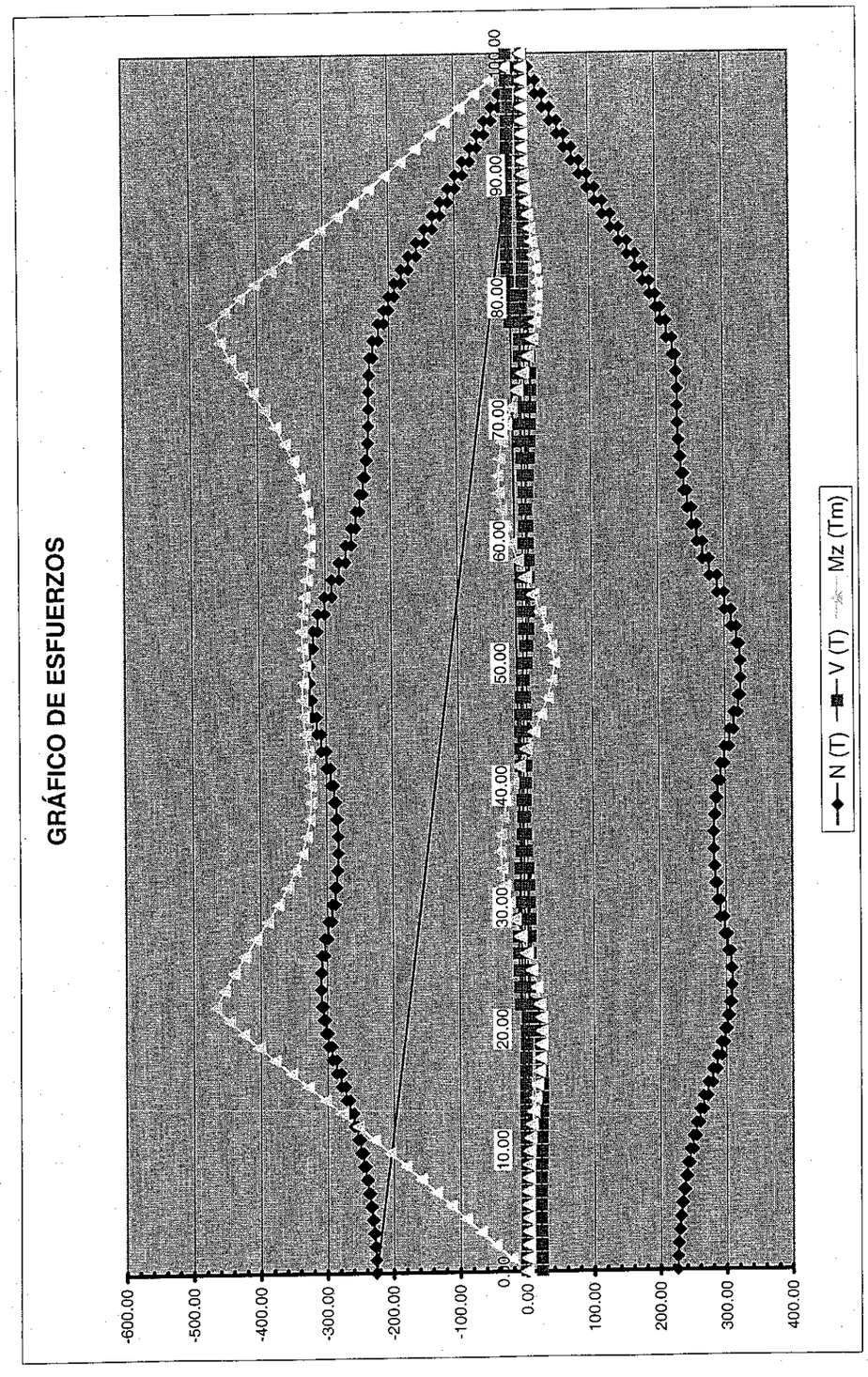
ej1posEI.HIP.Tinf

F4.pret.esf.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAN

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	1.10	0.00	0.00	0.00
2	2	1.10	0.00	0.00	0.00
2	3	2.20	0.00	0.00	0.00
3	3	2.20	0.00	0.00	0.00
3	4	3.30	0.00	0.00	0.00
4	4	3.30	0.00	0.00	0.00
4	5	4.40	0.00	0.00	0.00
5	5	4.40	0.00	0.00	0.00
5	6	5.50	0.00	0.00	0.00
6	6	5.50	0.00	0.00	0.00
6	7	6.60	0.00	0.00	0.00
7	7	6.60	0.00	0.00	0.00
7	8	7.70	0.00	0.00	0.00
8	8	7.70	0.00	0.00	0.00
8	9	8.80	0.00	0.00	0.00
9	9	8.80	0.00	0.00	0.00
9	10	9.90	0.00	0.00	0.00
10	10	9.90	0.00	0.00	0.00
10	11	11.00	0.00	0.00	0.00
11	11	11.00	0.00	0.00	0.00
11	12	12.10	0.00	0.00	0.00
12	12	12.10	0.00	0.00	0.00
12	13	13.20	0.00	0.00	0.00
13	13	13.20	0.00	0.00	0.00
13	14	14.30	0.00	0.00	0.00
14	14	14.30	0.00	0.00	0.00
14	15	15.40	0.00	0.00	0.00
15	15	15.40	-870.24	0.00	418.59
15	16	16.50	-870.24	0.00	418.59
16	16	16.50	-870.24	0.00	418.59
16	17	17.60	-870.24	0.00	418.59
17	17	17.60	-1740.48	0.00	837.17
17	18	18.70	-1740.48	0.00	837.17
18	18	18.70	-1740.48	0.00	837.17
18	19	19.80	-1740.48	0.00	837.17
19	19	19.80	-1740.48	0.00	837.17
19	20	20.90	-1740.48	0.00	837.17
20	20	20.90	-1740.48	0.00	837.17
20	21	22.00	-1740.48	0.00	837.17
21	1021	22.00	-1740.48	0.00	837.17
21	22	23.40	-1740.48	0.00	837.17
22	22	23.40	-1740.48	0.00	837.17
22	23	24.80	-1740.48	0.00	837.17
23	23	24.80	-1740.48	0.00	837.17
23	24	26.20	-1740.48	0.00	837.17
24	24	26.20	-870.24	0.00	418.59
24	25	27.60	-870.24	0.00	418.59
25	25	27.60	-870.24	0.00	418.59
25	26	29.00	-870.24	0.00	418.59
26	26	29.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAN

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	0.00	0.00
27	27	30.40	0.00	0.00	0.00
27	28	31.80	0.00	0.00	0.00
28	28	31.80	0.00	0.00	0.00
28	29	33.20	0.00	0.00	0.00
29	29	33.20	0.00	0.00	0.00
29	30	34.60	0.00	0.00	0.00
30	30	34.60	0.00	0.00	0.00
30	31	36.00	0.00	0.00	0.00
31	31	36.00	0.00	0.00	0.00
31	32	37.40	0.00	0.00	0.00
32	32	37.40	0.00	0.00	0.00
32	33	38.80	0.00	0.00	0.00
33	33	38.80	0.00	0.00	0.00
33	34	40.20	0.00	0.00	0.00
34	34	40.20	0.00	0.00	0.00
34	35	41.60	0.00	0.00	0.00
35	35	41.60	0.00	0.00	0.00
35	36	43.00	0.00	0.00	0.00
36	36	43.00	-870.24	0.00	418.59
36	37	44.40	-870.24	0.00	418.59
37	37	44.40	-870.24	0.00	418.59
37	38	45.80	-870.24	0.00	418.59
38	38	45.80	-1740.48	0.00	837.17
38	39	47.20	-1740.48	0.00	837.17
39	39	47.20	-1740.48	0.00	837.17
39	40	48.60	-1740.48	0.00	837.17
40	40	48.60	-1740.48	0.00	837.17
40	41	50.00	-1740.48	0.00	837.17
41	1041	50.00	-1740.48	0.00	837.17
41	42	51.40	-1740.48	0.00	837.17
42	42	51.40	-1740.48	0.00	837.17
42	43	52.80	-1740.48	0.00	837.17
43	43	52.80	-1740.48	0.00	837.17
43	44	54.20	-1740.48	0.00	837.17
44	44	54.20	-870.24	0.00	418.59
44	45	55.60	-870.24	0.00	418.59
45	45	55.60	-870.24	0.00	418.59
45	46	57.00	-870.24	0.00	418.59
46	46	57.00	0.00	0.00	0.00
46	47	58.40	0.00	0.00	0.00
47	47	58.40	0.00	0.00	0.00
47	48	59.80	0.00	0.00	0.00
48	48	59.80	0.00	0.00	0.00
48	49	61.20	0.00	0.00	0.00
49	49	61.20	0.00	0.00	0.00
49	50	62.60	0.00	0.00	0.00
50	50	62.60	0.00	0.00	0.00
50	51	64.00	0.00	0.00	0.00
51	51	64.00	0.00	0.00	0.00
51	52	65.40	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	0.00	0.00
52	53	66.80	0.00	0.00	0.00
53	53	66.80	0.00	0.00	0.00
53	54	68.20	0.00	0.00	0.00
54	54	68.20	0.00	0.00	0.00
54	55	69.60	0.00	0.00	0.00
55	55	69.60	0.00	0.00	0.00
55	56	71.00	0.00	0.00	0.00
56	56	71.00	-870.24	0.00	418.59
56	57	72.40	-870.24	0.00	418.59
57	57	72.40	-870.24	0.00	418.59
57	58	73.80	-870.24	0.00	418.59
58	58	73.80	-1740.48	0.00	837.17
58	59	75.20	-1740.48	0.00	837.17
59	59	75.20	-1740.48	0.00	837.17
59	60	76.60	-1740.48	0.00	837.17
60	60	76.60	-1740.48	0.00	837.17
60	61	78.00	-1740.48	0.00	837.17
61	1061	78.00	-1740.48	0.00	837.17
61	62	79.10	-1740.48	0.00	837.17
62	62	79.10	-1740.48	0.00	837.17
62	63	80.20	-1740.48	0.00	837.17
63	63	80.20	-1740.48	0.00	837.17
63	64	81.30	-1740.48	0.00	837.17
64	64	81.30	-1740.48	0.00	837.17
64	65	82.40	-1740.48	0.00	837.17
65	65	82.40	-870.24	0.00	418.59
65	66	83.50	-870.24	0.00	418.59
66	66	83.50	-870.24	0.00	418.59
66	67	84.60	-870.24	0.00	418.59
67	67	84.60	0.00	0.00	0.00
67	68	85.70	0.00	0.00	0.00
68	68	85.70	0.00	0.00	0.00
68	69	86.80	0.00	0.00	0.00
69	69	86.80	0.00	0.00	0.00
69	70	87.90	0.00	0.00	0.00
70	70	87.90	0.00	0.00	0.00
70	71	89.00	0.00	0.00	0.00
71	71	89.00	0.00	0.00	0.00
71	72	90.10	0.00	0.00	0.00
72	72	90.10	0.00	0.00	0.00
72	73	91.20	0.00	0.00	0.00
73	73	91.20	0.00	0.00	0.00
73	74	92.30	0.00	0.00	0.00
74	74	92.30	0.00	0.00	0.00
74	75	93.40	0.00	0.00	0.00
75	75	93.40	0.00	0.00	0.00
75	76	94.50	0.00	0.00	0.00
76	76	94.50	0.00	0.00	0.00
76	77	95.60	0.00	0.00	0.00
77	77	95.60	0.00	0.00	0.00

F4.pret.esf.xls

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CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	0.00	0.00
78	78	96.70	0.00	0.00	0.00
78	79	97.80	0.00	0.00	0.00
79	79	97.80	0.00	0.00	0.00
79	80	98.90	0.00	0.00	0.00
80	80	98.90	0.00	0.00	0.00
80	81	100.00	0.00	0.00	0.00
101	101	0.00	0.00	0.00	0.00
101	102	0.00	0.00	0.00	0.00
102	102	0.00	0.00	0.00	0.00
102	103	0.00	0.00	0.00	0.00
103	103	0.00	0.00	0.00	0.00
103	104	0.00	0.00	0.00	0.00
104	104	0.00	0.00	0.00	0.00
104	105	0.00	0.00	0.00	0.00
105	105	0.00	0.00	0.00	0.00
105	106	0.00	0.00	0.00	0.00
106	106	0.00	0.00	0.00	0.00
106	107	0.00	0.00	0.00	0.00
107	107	0.00	0.00	0.00	0.00
107	108	0.00	0.00	0.00	0.00
108	108	0.00	0.00	0.00	0.00
108	109	0.00	0.00	0.00	0.00
109	109	0.00	0.00	0.00	0.00
109	110	0.00	0.00	0.00	0.00
110	110	0.00	0.00	0.00	0.00
110	111	0.00	0.00	0.00	0.00
111	111	0.00	0.00	0.00	0.00
111	112	0.00	0.00	0.00	0.00
112	112	0.00	0.00	0.00	0.00
112	113	0.00	0.00	0.00	0.00
113	113	0.00	0.00	0.00	0.00
113	114	0.00	0.00	0.00	0.00
114	114	0.00	0.00	0.00	0.00
114	115	0.00	0.00	0.00	0.00
115	115	0.00	0.00	0.00	0.00
115	116	0.00	0.00	0.00	0.00
116	116	0.00	0.00	0.00	0.00
116	117	0.00	0.00	0.00	0.00
117	117	0.00	0.00	0.00	0.00
117	118	0.00	0.00	0.00	0.00
118	118	0.00	0.00	0.00	0.00
118	119	0.00	0.00	0.00	0.00
119	119	0.00	0.00	0.00	0.00
119	120	0.00	0.00	0.00	0.00
120	120	0.00	0.00	0.00	0.00
120	121	0.00	0.00	0.00	0.00
121	1121	0.00	0.00	0.00	0.00
121	122	0.00	0.00	0.00	0.00
122	122	0.00	0.00	0.00	0.00
122	123	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	0.00	0.00	0.00	0.00
123	124	0.00	0.00	0.00	0.00
124	124	0.00	0.00	0.00	0.00
124	125	0.00	0.00	0.00	0.00
125	125	0.00	0.00	0.00	0.00
125	126	0.00	0.00	0.00	0.00
126	126	0.00	0.00	0.00	0.00
126	127	0.00	0.00	0.00	0.00
127	127	0.00	0.00	0.00	0.00
127	128	0.00	0.00	0.00	0.00
128	128	0.00	0.00	0.00	0.00
128	129	0.00	0.00	0.00	0.00
129	129	0.00	0.00	0.00	0.00
129	130	0.00	0.00	0.00	0.00
130	130	0.00	0.00	0.00	0.00
130	131	0.00	0.00	0.00	0.00
131	131	0.00	0.00	0.00	0.00
131	132	0.00	0.00	0.00	0.00
132	132	0.00	0.00	0.00	0.00
132	133	0.00	0.00	0.00	0.00
133	133	0.00	0.00	0.00	0.00
133	134	0.00	0.00	0.00	0.00
134	134	0.00	0.00	0.00	0.00
134	135	0.00	0.00	0.00	0.00
135	135	0.00	0.00	0.00	0.00
135	136	0.00	0.00	0.00	0.00
136	136	0.00	0.00	0.00	0.00
136	137	0.00	0.00	0.00	0.00
137	137	0.00	0.00	0.00	0.00
137	138	0.00	0.00	0.00	0.00
138	138	0.00	0.00	0.00	0.00
138	139	0.00	0.00	0.00	0.00
139	139	0.00	0.00	0.00	0.00
139	140	0.00	0.00	0.00	0.00
140	140	0.00	0.00	0.00	0.00
140	141	0.00	0.00	0.00	0.00
141	1141	0.00	0.00	0.00	0.00
141	142	0.00	0.00	0.00	0.00
142	142	0.00	0.00	0.00	0.00
142	143	0.00	0.00	0.00	0.00
143	143	0.00	0.00	0.00	0.00
143	144	0.00	0.00	0.00	0.00
144	144	0.00	0.00	0.00	0.00
144	145	0.00	0.00	0.00	0.00
145	145	0.00	0.00	0.00	0.00
145	146	0.00	0.00	0.00	0.00
146	146	0.00	0.00	0.00	0.00
146	147	0.00	0.00	0.00	0.00
147	147	0.00	0.00	0.00	0.00
147	148	0.00	0.00	0.00	0.00
148	148	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	0.00	0.00	0.00	0.00
149	149	0.00	0.00	0.00	0.00
149	150	0.00	0.00	0.00	0.00
150	150	0.00	0.00	0.00	0.00
150	151	0.00	0.00	0.00	0.00
151	151	0.00	0.00	0.00	0.00
151	152	0.00	0.00	0.00	0.00
152	152	0.00	0.00	0.00	0.00
152	153	0.00	0.00	0.00	0.00
153	153	0.00	0.00	0.00	0.00
153	154	0.00	0.00	0.00	0.00
154	154	0.00	0.00	0.00	0.00
154	155	0.00	0.00	0.00	0.00
155	155	0.00	0.00	0.00	0.00
155	156	0.00	0.00	0.00	0.00
156	156	0.00	0.00	0.00	0.00
156	157	0.00	0.00	0.00	0.00
157	157	0.00	0.00	0.00	0.00
157	158	0.00	0.00	0.00	0.00
158	158	0.00	0.00	0.00	0.00
158	159	0.00	0.00	0.00	0.00
159	159	0.00	0.00	0.00	0.00
159	160	0.00	0.00	0.00	0.00
160	160	0.00	0.00	0.00	0.00
160	161	0.00	0.00	0.00	0.00
161	1161	0.00	0.00	0.00	0.00
161	162	0.00	0.00	0.00	0.00
162	162	0.00	0.00	0.00	0.00
162	163	0.00	0.00	0.00	0.00
163	163	0.00	0.00	0.00	0.00
163	164	0.00	0.00	0.00	0.00
164	164	0.00	0.00	0.00	0.00
164	165	0.00	0.00	0.00	0.00
165	165	0.00	0.00	0.00	0.00
165	166	0.00	0.00	0.00	0.00
166	166	0.00	0.00	0.00	0.00
166	167	0.00	0.00	0.00	0.00
167	167	0.00	0.00	0.00	0.00
167	168	0.00	0.00	0.00	0.00
168	168	0.00	0.00	0.00	0.00
168	169	0.00	0.00	0.00	0.00
169	169	0.00	0.00	0.00	0.00
169	170	0.00	0.00	0.00	0.00
170	170	0.00	0.00	0.00	0.00
170	171	0.00	0.00	0.00	0.00
171	171	0.00	0.00	0.00	0.00
171	172	0.00	0.00	0.00	0.00
172	172	0.00	0.00	0.00	0.00
172	173	0.00	0.00	0.00	0.00
173	173	0.00	0.00	0.00	0.00
173	174	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

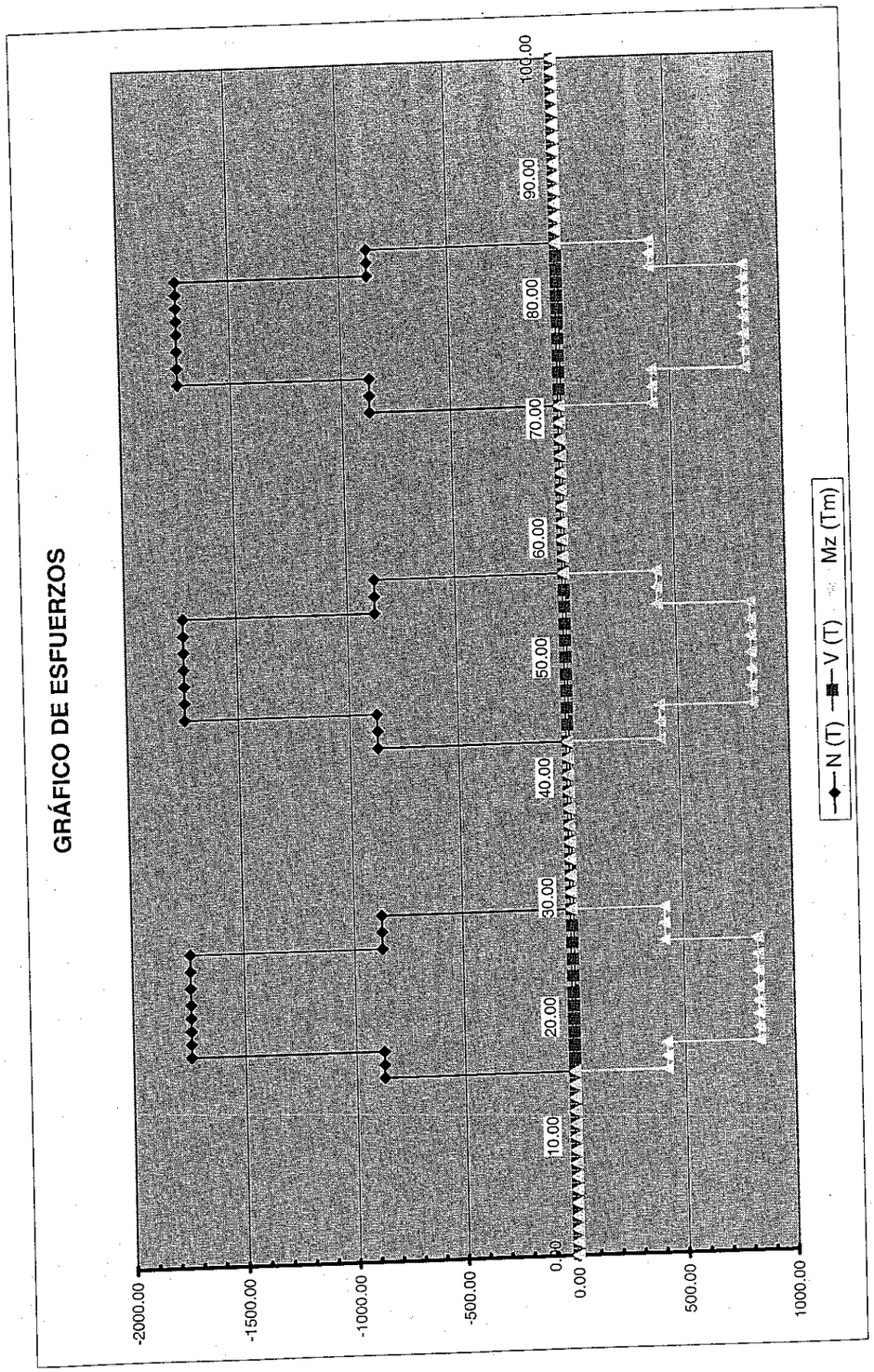
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	0.00	0.00	0.00	0.00
174	175	0.00	0.00	0.00	0.00
175	175	0.00	0.00	0.00	0.00
175	176	0.00	0.00	0.00	0.00
176	176	0.00	0.00	0.00	0.00
176	177	0.00	0.00	0.00	0.00
177	177	0.00	0.00	0.00	0.00
177	178	0.00	0.00	0.00	0.00
178	178	0.00	0.00	0.00	0.00
178	179	0.00	0.00	0.00	0.00
179	179	0.00	0.00	0.00	0.00
179	180	0.00	0.00	0.00	0.00
180	180	0.00	0.00	0.00	0.00
180	181	0.00	0.00	0.00	0.00

11/09/03

Programa DINTEL PACADAR S.A.
ej1posEI.ISO.To

F4.pret.esf.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	1.10	0.00	0.00	0.00
2	2	1.10	0.00	0.00	0.00
2	3	2.20	0.00	0.00	0.00
3	3	2.20	0.00	0.00	0.00
3	4	3.30	0.00	0.00	0.00
4	4	3.30	0.00	0.00	0.00
4	5	4.40	0.00	0.00	0.00
5	5	4.40	0.00	0.00	0.00
5	6	5.50	0.00	0.00	0.00
6	6	5.50	0.00	0.00	0.00
6	7	6.60	0.00	0.00	0.00
7	7	6.60	0.00	0.00	0.00
7	8	7.70	0.00	0.00	0.00
8	8	7.70	0.00	0.00	0.00
8	9	8.80	0.00	0.00	0.00
9	9	8.80	0.00	0.00	0.00
9	10	9.90	0.00	0.00	0.00
10	10	9.90	0.00	0.00	0.00
10	11	11.00	0.00	0.00	0.00
11	11	11.00	0.00	0.00	0.00
11	12	12.10	0.00	0.00	0.00
12	12	12.10	0.00	0.00	0.00
12	13	13.20	0.00	0.00	0.00
13	13	13.20	0.00	0.00	0.00
13	14	14.30	0.00	0.00	0.00
14	14	14.30	0.00	0.00	0.00
14	15	15.40	0.00	0.00	0.00
15	15	15.40	-870.24	0.00	418.59
15	16	16.50	-870.24	0.00	418.59
16	16	16.50	-870.24	0.00	418.59
16	17	17.60	-870.24	0.00	418.59
17	17	17.60	-1740.48	0.00	837.17
17	18	18.70	-1740.48	0.00	837.17
18	18	18.70	-1740.48	0.00	837.17
18	19	19.80	-1740.48	0.00	837.17
19	19	19.80	-1740.48	0.00	837.17
19	20	20.90	-1740.48	0.00	837.17
20	20	20.90	-1740.48	0.00	837.17
20	21	22.00	-1740.48	0.00	837.17
21	1021	22.00	-1740.48	0.00	837.17
21	22	23.40	-1740.48	0.00	837.17
22	22	23.40	-1740.48	0.00	837.17
22	23	24.80	-1740.48	0.00	837.17
23	23	24.80	-1740.48	0.00	837.17
23	24	26.20	-1740.48	0.00	837.17
24	24	26.20	-870.24	0.00	418.59
24	25	27.60	-870.24	0.00	418.59
25	25	27.60	-870.24	0.00	418.59
25	26	29.00	-870.24	0.00	418.59
26	26	29.00	0.00	0.00	0.00

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej1posEl.ISO.Tinf

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej1posEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEl.FAM1.ISO + [1; 1]ej1posEl.FAM2.ISO + [1; 1]ej1posEl.FAM3.ISO + [1; 1]ej1posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	0.00	0.00
27	27	30.40	0.00	0.00	0.00
27	28	31.80	0.00	0.00	0.00
28	28	31.80	0.00	0.00	0.00
28	29	33.20	0.00	0.00	0.00
29	29	33.20	0.00	0.00	0.00
29	30	34.60	0.00	0.00	0.00
30	30	34.60	0.00	0.00	0.00
30	31	36.00	0.00	0.00	0.00
31	31	36.00	0.00	0.00	0.00
31	32	37.40	0.00	0.00	0.00
32	32	37.40	0.00	0.00	0.00
32	33	38.80	0.00	0.00	0.00
33	33	38.80	0.00	0.00	0.00
33	34	40.20	0.00	0.00	0.00
34	34	40.20	0.00	0.00	0.00
34	35	41.60	0.00	0.00	0.00
35	35	41.60	0.00	0.00	0.00
35	36	43.00	0.00	0.00	0.00
36	36	43.00	-870.24	0.00	418.59
36	37	44.40	-870.24	0.00	418.59
37	37	44.40	-870.24	0.00	418.59
37	38	45.80	-870.24	0.00	418.59
38	38	45.80	-1740.48	0.00	837.17
38	39	47.20	-1740.48	0.00	837.17
39	39	47.20	-1740.48	0.00	837.17
39	40	48.60	-1740.48	0.00	837.17
40	40	48.60	-1740.48	0.00	837.17
40	41	50.00	-1740.48	0.00	837.17
41	1041	50.00	-1740.48	0.00	837.17
41	42	51.40	-1740.48	0.00	837.17
42	42	51.40	-1740.48	0.00	837.17
42	43	52.80	-1740.48	0.00	837.17
43	43	52.80	-1740.48	0.00	837.17
43	44	54.20	-1740.48	0.00	837.17
44	44	54.20	-870.24	0.00	418.59
44	45	55.60	-870.24	0.00	418.59
45	45	55.60	-870.24	0.00	418.59
45	46	57.00	-870.24	0.00	418.59
46	46	57.00	0.00	0.00	0.00
46	47	58.40	0.00	0.00	0.00
47	47	58.40	0.00	0.00	0.00
47	48	59.80	0.00	0.00	0.00
48	48	59.80	0.00	0.00	0.00
48	49	61.20	0.00	0.00	0.00
49	49	61.20	0.00	0.00	0.00
49	50	62.60	0.00	0.00	0.00
50	50	62.60	0.00	0.00	0.00
50	51	64.00	0.00	0.00	0.00
51	51	64.00	0.00	0.00	0.00
51	52	65.40	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	0.00	0.00
52	53	66.80	0.00	0.00	0.00
53	53	66.80	0.00	0.00	0.00
53	54	68.20	0.00	0.00	0.00
54	54	68.20	0.00	0.00	0.00
54	55	69.60	0.00	0.00	0.00
55	55	69.60	0.00	0.00	0.00
55	56	71.00	0.00	0.00	0.00
56	56	71.00	-870.24	0.00	418.59
56	57	72.40	-870.24	0.00	418.59
57	57	72.40	-870.24	0.00	418.59
57	58	73.80	-870.24	0.00	418.59
58	58	73.80	-1740.48	0.00	837.17
58	59	75.20	-1740.48	0.00	837.17
59	59	75.20	-1740.48	0.00	837.17
59	60	76.60	-1740.48	0.00	837.17
60	60	76.60	-1740.48	0.00	837.17
60	61	78.00	-1740.48	0.00	837.17
61	1061	78.00	-1740.48	0.00	837.17
61	62	79.10	-1740.48	0.00	837.17
62	62	79.10	-1740.48	0.00	837.17
62	63	80.20	-1740.48	0.00	837.17
63	63	80.20	-1740.48	0.00	837.17
63	64	81.30	-1740.48	0.00	837.17
64	64	81.30	-1740.48	0.00	837.17
64	65	82.40	-1740.48	0.00	837.17
65	65	82.40	-870.24	0.00	418.59
65	66	83.50	-870.24	0.00	418.59
66	66	83.50	-870.24	0.00	418.59
66	67	84.60	-870.24	0.00	418.59
67	67	84.60	0.00	0.00	0.00
67	68	85.70	0.00	0.00	0.00
68	68	85.70	0.00	0.00	0.00
68	69	86.80	0.00	0.00	0.00
69	69	86.80	0.00	0.00	0.00
69	70	87.90	0.00	0.00	0.00
70	70	87.90	0.00	0.00	0.00
70	71	89.00	0.00	0.00	0.00
71	71	89.00	0.00	0.00	0.00
71	72	90.10	0.00	0.00	0.00
72	72	90.10	0.00	0.00	0.00
72	73	91.20	0.00	0.00	0.00
73	73	91.20	0.00	0.00	0.00
73	74	92.30	0.00	0.00	0.00
74	74	92.30	0.00	0.00	0.00
74	75	93.40	0.00	0.00	0.00
75	75	93.40	0.00	0.00	0.00
75	76	94.50	0.00	0.00	0.00
76	76	94.50	0.00	0.00	0.00
76	77	95.60	0.00	0.00	0.00
77	77	95.60	0.00	0.00	0.00

F4.pret.esf.xls Programa DINTEL PACADAR S.A. 11/09/03
ej1posEI.ISO.Tinf

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	0.00	0.00
78	78	96.70	0.00	0.00	0.00
78	79	97.80	0.00	0.00	0.00
79	79	97.80	0.00	0.00	0.00
79	80	98.90	0.00	0.00	0.00
80	80	98.90	0.00	0.00	0.00
80	81	100.00	0.00	0.00	0.00
101	101	0.00	0.00	0.00	0.00
101	102	0.00	0.00	0.00	0.00
102	102	0.00	0.00	0.00	0.00
102	103	0.00	0.00	0.00	0.00
103	103	0.00	0.00	0.00	0.00
103	104	0.00	0.00	0.00	0.00
104	104	0.00	0.00	0.00	0.00
104	105	0.00	0.00	0.00	0.00
105	105	0.00	0.00	0.00	0.00
105	106	0.00	0.00	0.00	0.00
106	106	0.00	0.00	0.00	0.00
106	107	0.00	0.00	0.00	0.00
107	107	0.00	0.00	0.00	0.00
107	108	0.00	0.00	0.00	0.00
108	108	0.00	0.00	0.00	0.00
108	109	0.00	0.00	0.00	0.00
109	109	0.00	0.00	0.00	0.00
109	110	0.00	0.00	0.00	0.00
110	110	0.00	0.00	0.00	0.00
110	111	0.00	0.00	0.00	0.00
111	111	0.00	0.00	0.00	0.00
111	112	0.00	0.00	0.00	0.00
112	112	0.00	0.00	0.00	0.00
112	113	0.00	0.00	0.00	0.00
113	113	0.00	0.00	0.00	0.00
113	114	0.00	0.00	0.00	0.00
114	114	0.00	0.00	0.00	0.00
114	115	0.00	0.00	0.00	0.00
115	115	0.00	0.00	0.00	0.00
115	116	0.00	0.00	0.00	0.00
116	116	0.00	0.00	0.00	0.00
116	117	0.00	0.00	0.00	0.00
117	117	0.00	0.00	0.00	0.00
117	118	0.00	0.00	0.00	0.00
118	118	0.00	0.00	0.00	0.00
118	119	0.00	0.00	0.00	0.00
119	119	0.00	0.00	0.00	0.00
119	120	0.00	0.00	0.00	0.00
120	120	0.00	0.00	0.00	0.00
120	121	0.00	0.00	0.00	0.00
121	1121	0.00	0.00	0.00	0.00
121	122	0.00	0.00	0.00	0.00
122	122	0.00	0.00	0.00	0.00
122	123	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	0.00	0.00	0.00	0.00
123	124	0.00	0.00	0.00	0.00
124	124	0.00	0.00	0.00	0.00
124	125	0.00	0.00	0.00	0.00
125	125	0.00	0.00	0.00	0.00
125	126	0.00	0.00	0.00	0.00
126	126	0.00	0.00	0.00	0.00
126	127	0.00	0.00	0.00	0.00
127	127	0.00	0.00	0.00	0.00
127	128	0.00	0.00	0.00	0.00
128	128	0.00	0.00	0.00	0.00
128	129	0.00	0.00	0.00	0.00
129	129	0.00	0.00	0.00	0.00
129	130	0.00	0.00	0.00	0.00
130	130	0.00	0.00	0.00	0.00
130	131	0.00	0.00	0.00	0.00
131	131	0.00	0.00	0.00	0.00
131	132	0.00	0.00	0.00	0.00
132	132	0.00	0.00	0.00	0.00
132	133	0.00	0.00	0.00	0.00
133	133	0.00	0.00	0.00	0.00
133	134	0.00	0.00	0.00	0.00
134	134	0.00	0.00	0.00	0.00
134	135	0.00	0.00	0.00	0.00
135	135	0.00	0.00	0.00	0.00
135	136	0.00	0.00	0.00	0.00
136	136	0.00	0.00	0.00	0.00
136	137	0.00	0.00	0.00	0.00
137	137	0.00	0.00	0.00	0.00
137	138	0.00	0.00	0.00	0.00
138	138	0.00	0.00	0.00	0.00
138	139	0.00	0.00	0.00	0.00
139	139	0.00	0.00	0.00	0.00
139	140	0.00	0.00	0.00	0.00
140	140	0.00	0.00	0.00	0.00
140	141	0.00	0.00	0.00	0.00
141	1141	0.00	0.00	0.00	0.00
141	142	0.00	0.00	0.00	0.00
142	142	0.00	0.00	0.00	0.00
142	143	0.00	0.00	0.00	0.00
143	143	0.00	0.00	0.00	0.00
143	144	0.00	0.00	0.00	0.00
144	144	0.00	0.00	0.00	0.00
144	145	0.00	0.00	0.00	0.00
145	145	0.00	0.00	0.00	0.00
145	146	0.00	0.00	0.00	0.00
146	146	0.00	0.00	0.00	0.00
146	147	0.00	0.00	0.00	0.00
147	147	0.00	0.00	0.00	0.00
147	148	0.00	0.00	0.00	0.00
148	148	0.00	0.00	0.00	0.00

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej1posEI.ISO.Tinf

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej1posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	0.00	0.00	0.00	0.00
149	149	0.00	0.00	0.00	0.00
149	150	0.00	0.00	0.00	0.00
150	150	0.00	0.00	0.00	0.00
150	151	0.00	0.00	0.00	0.00
151	151	0.00	0.00	0.00	0.00
151	152	0.00	0.00	0.00	0.00
152	152	0.00	0.00	0.00	0.00
152	153	0.00	0.00	0.00	0.00
153	153	0.00	0.00	0.00	0.00
153	154	0.00	0.00	0.00	0.00
154	154	0.00	0.00	0.00	0.00
154	155	0.00	0.00	0.00	0.00
155	155	0.00	0.00	0.00	0.00
155	156	0.00	0.00	0.00	0.00
156	156	0.00	0.00	0.00	0.00
156	157	0.00	0.00	0.00	0.00
157	157	0.00	0.00	0.00	0.00
157	158	0.00	0.00	0.00	0.00
158	158	0.00	0.00	0.00	0.00
158	159	0.00	0.00	0.00	0.00
159	159	0.00	0.00	0.00	0.00
159	160	0.00	0.00	0.00	0.00
160	160	0.00	0.00	0.00	0.00
160	161	0.00	0.00	0.00	0.00
161	1161	0.00	0.00	0.00	0.00
161	162	0.00	0.00	0.00	0.00
162	162	0.00	0.00	0.00	0.00
162	163	0.00	0.00	0.00	0.00
163	163	0.00	0.00	0.00	0.00
163	164	0.00	0.00	0.00	0.00
164	164	0.00	0.00	0.00	0.00
164	165	0.00	0.00	0.00	0.00
165	165	0.00	0.00	0.00	0.00
165	166	0.00	0.00	0.00	0.00
166	166	0.00	0.00	0.00	0.00
166	167	0.00	0.00	0.00	0.00
167	167	0.00	0.00	0.00	0.00
167	168	0.00	0.00	0.00	0.00
168	168	0.00	0.00	0.00	0.00
168	169	0.00	0.00	0.00	0.00
169	169	0.00	0.00	0.00	0.00
169	170	0.00	0.00	0.00	0.00
170	170	0.00	0.00	0.00	0.00
170	171	0.00	0.00	0.00	0.00
171	171	0.00	0.00	0.00	0.00
171	172	0.00	0.00	0.00	0.00
172	172	0.00	0.00	0.00	0.00
172	173	0.00	0.00	0.00	0.00
173	173	0.00	0.00	0.00	0.00
173	174	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

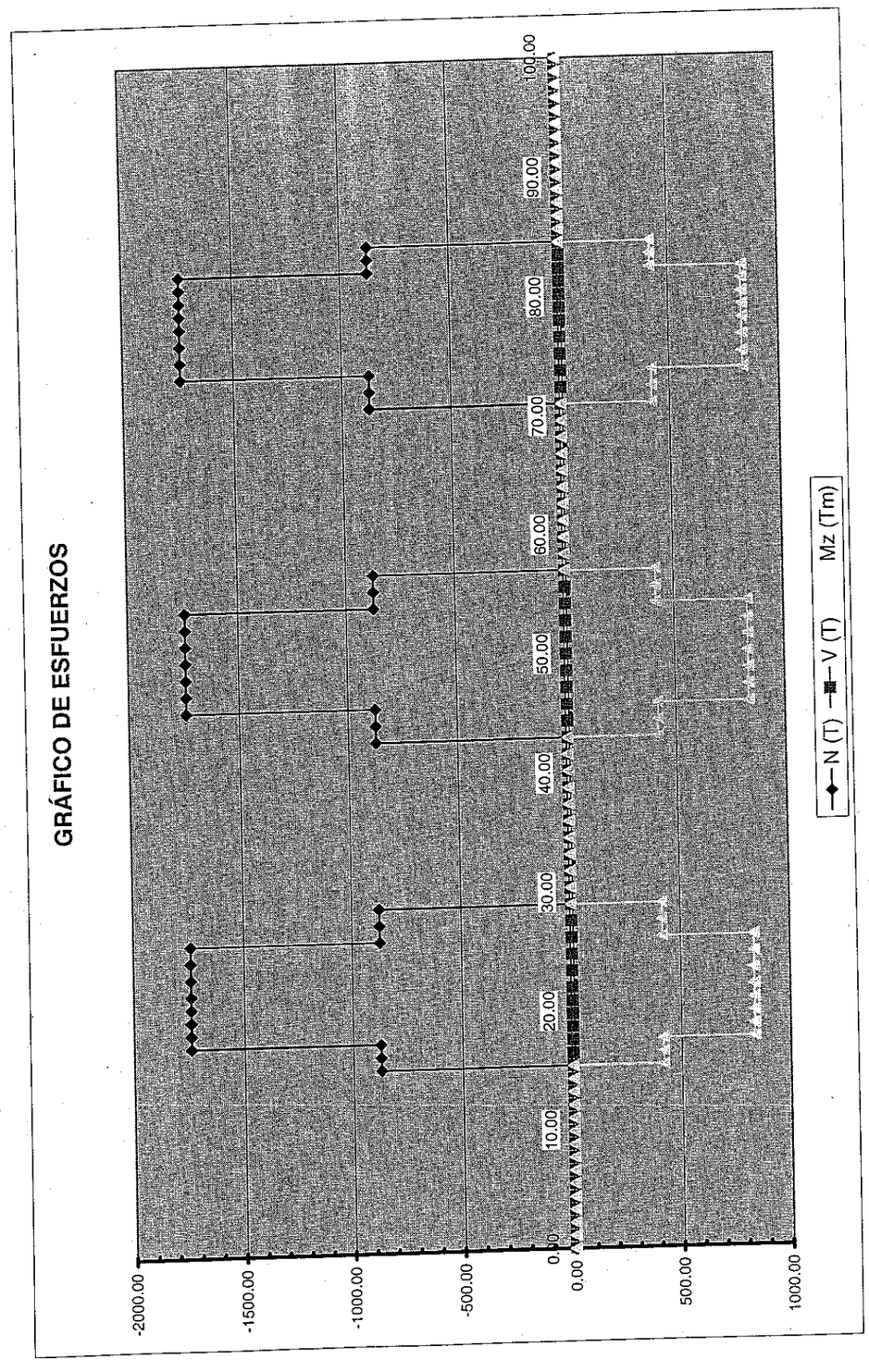
Hipótesis de cálculo:
ej1posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej1posEI.FAM1.ISO + [1; 1]ej1posEI.FAM2.ISO + [1; 1]ej1posEI.FAM3.ISO + [1; 1]ej1posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	0.00	0.00	0.00	0.00
174	175	0.00	0.00	0.00	0.00
175	175	0.00	0.00	0.00	0.00
175	176	0.00	0.00	0.00	0.00
176	176	0.00	0.00	0.00	0.00
176	177	0.00	0.00	0.00	0.00
177	177	0.00	0.00	0.00	0.00
177	178	0.00	0.00	0.00	0.00
178	178	0.00	0.00	0.00	0.00
178	179	0.00	0.00	0.00	0.00
179	179	0.00	0.00	0.00	0.00
179	180	0.00	0.00	0.00	0.00
180	180	0.00	0.00	0.00	0.00
180	181	0.00	0.00	0.00	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-498.32	5.00	-1.55
1	2	1.10	-498.32	5.00	-7.05
2	2	1.10	-498.91	6.97	-9.89
2	3	2.20	-498.91	6.97	-17.56
3	3	2.20	-499.72	7.82	-20.01
3	4	3.30	-499.72	7.82	-28.61
4	4	3.30	-500.77	7.71	-30.70
4	5	4.40	-500.77	7.71	-39.18
5	5	4.40	-501.83	6.81	-40.84
5	6	5.50	-501.83	6.81	-48.33
6	6	5.50	-502.90	5.32	-49.59
6	7	6.60	-502.90	5.32	-55.44
7	7	6.60	-503.76	3.39	-56.22
7	8	7.70	-503.76	3.39	-59.95
8	8	7.70	-504.42	1.22	-60.30
8	9	8.80	-504.42	1.22	-61.64
9	9	8.80	-504.88	-1.05	-61.62
9	10	9.90	-504.88	-1.05	-60.46
10	10	9.90	-505.13	-3.26	-60.09
10	11	11.00	-505.13	-3.26	-56.50
11	11	11.00	-505.18	-5.31	-55.82
11	12	12.10	-505.18	-5.31	-49.98
12	12	12.10	-505.02	-7.07	-49.01
12	13	13.20	-505.02	-7.07	-41.23
13	13	13.20	-504.64	-8.46	-40.02
13	14	14.30	-504.64	-8.46	-30.71
14	14	14.30	-504.04	-9.37	-29.28
14	15	15.40	-504.04	-9.37	-18.97
15	15	15.40	-503.42	-9.76	-17.47
15	16	16.50	-503.42	-9.76	-6.73
16	16	16.50	-502.78	-9.60	-5.19
16	17	17.60	-502.78	-9.60	5.37
17	17	17.60	-502.10	-8.88	6.92
17	18	18.70	-502.10	-8.88	16.69
18	18	18.70	-501.60	-7.63	18.10
18	19	19.80	-501.60	-7.63	26.49
19	19	19.80	-501.27	-5.91	27.72
19	20	20.90	-501.27	-5.91	34.22
20	20	20.90	-501.40	-3.82	35.04
20	21	22.00	-501.40	-3.82	39.24
21	1021	22.00	-502.29	-2.32	39.68
21	22	23.40	-502.29	-2.32	42.92
22	22	23.40	-504.66	0.60	42.73
22	23	24.80	-504.66	0.60	41.88
23	23	24.80	-508.21	3.20	41.02
23	24	26.20	-508.21	3.20	36.53
24	24	26.20	-512.21	5.24	35.32
24	25	27.60	-512.21	5.24	27.99
25	25	27.60	-516.75	6.54	26.42
25	26	29.00	-516.75	6.54	17.27
26	26	29.00	-520.90	7.04	15.74

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej2preEl.TOT.To

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-520.90	7.04	5.88
27	27	30.40	-524.74	6.77	4.38
27	28	31.80	-524.74	6.77	-5.10
28	28	31.80	-527.44	5.83	-6.25
28	29	33.20	-527.44	5.83	-14.41
29	29	33.20	-529.06	4.39	-15.21
29	30	34.60	-529.06	4.39	-21.36
30	30	34.60	-529.65	2.64	-21.82
30	31	36.00	-529.65	2.64	-25.51
31	31	36.00	-529.21	0.73	-25.62
31	32	37.40	-529.21	0.73	-26.65
32	32	37.40	-527.72	-1.16	-26.41
32	33	38.80	-527.72	-1.16	-24.78
33	33	38.80	-525.15	-2.87	-24.18
33	34	40.20	-525.15	-2.87	-20.16
34	34	40.20	-521.42	-4.22	-19.18
34	35	41.60	-521.42	-4.22	-13.28
35	35	41.60	-516.42	-5.00	-11.90
35	36	43.00	-516.42	-5.00	-4.90
36	36	43.00	-510.97	-5.11	-3.43
36	37	44.40	-510.97	-5.11	3.72
37	37	44.40	-504.92	-4.48	5.29
37	38	45.80	-504.92	-4.48	11.56
38	38	45.80	-499.17	-3.15	12.87
38	39	47.20	-499.17	-3.15	17.28
39	39	47.20	-493.56	-1.24	18.34
39	40	48.60	-493.56	-1.24	20.08
40	40	48.60	-488.77	1.07	20.60
40	41	50.00	-488.77	1.07	19.11
41	1041	50.00	-484.66	-1.07	19.11
41	42	51.40	-484.66	-1.07	20.60
42	42	51.40	-481.22	1.24	20.07
42	43	52.80	-481.22	1.24	18.34
43	43	52.80	-478.56	3.15	17.27
43	44	54.20	-478.56	3.15	12.87
44	44	54.20	-476.00	4.48	11.56
44	45	55.60	-476.00	4.48	5.29
45	45	55.60	-473.65	5.11	3.71
45	46	57.00	-473.65	5.11	-3.44
46	46	57.00	-470.60	5.00	-4.90
46	47	58.40	-470.60	5.00	-11.91
47	47	58.40	-466.95	4.22	-13.28
47	48	59.80	-466.95	4.22	-19.18
48	48	59.80	-461.87	2.87	-20.16
48	49	61.20	-461.87	2.87	-24.18
49	49	61.20	-455.44	1.16	-24.79
49	50	62.60	-455.44	1.16	-26.41
50	50	62.60	-447.66	-0.73	-26.65
50	51	64.00	-447.66	-0.73	-25.63
51	51	64.00	-438.55	-2.64	-25.52
51	52	65.40	-438.55	-2.64	-21.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-428.06	-4.39	-21.37
52	53	66.80	-428.06	-4.39	-15.22
53	53	66.80	-416.12	-5.83	-14.42
53	54	68.20	-416.12	-5.83	-6.26
54	54	68.20	-402.60	-6.77	-5.11
54	55	69.60	-402.60	-6.77	4.37
55	55	69.60	-387.35	-7.04	5.87
55	56	71.00	-387.35	-7.04	15.73
56	56	71.00	-371.11	-6.54	17.26
56	57	72.40	-371.11	-6.54	26.42
57	57	72.40	-353.65	-5.24	27.99
57	58	73.80	-353.65	-5.24	35.32
58	58	73.80	-335.79	-3.21	36.53
58	59	75.20	-335.79	-3.21	41.02
59	59	75.20	-317.25	-0.61	41.88
59	60	76.60	-317.25	-0.61	42.73
60	60	76.60	-298.56	2.31	42.92
60	61	78.00	-298.56	2.31	39.68
61	1061	78.00	-284.96	3.82	39.25
61	62	79.10	-284.96	3.82	35.04
62	62	79.10	-275.53	5.91	34.22
62	63	80.20	-275.53	5.91	27.72
63	63	80.20	-265.98	7.63	26.50
63	64	81.30	-265.98	7.63	18.10
64	64	81.30	-256.01	8.89	16.70
64	65	82.40	-256.01	8.89	6.93
65	65	82.40	-245.67	9.60	5.37
65	66	83.50	-245.67	9.60	-5.19
66	66	83.50	-234.75	9.76	-6.73
66	67	84.60	-234.75	9.76	-17.47
67	67	84.60	-223.26	9.37	-18.97
67	68	85.70	-223.26	9.37	-29.28
68	68	85.70	-211.21	8.46	-30.71
68	69	86.80	-211.21	8.46	-40.02
69	69	86.80	-198.39	7.08	-41.23
69	70	87.90	-198.39	7.08	-49.01
70	70	87.90	-184.80	5.31	-49.98
70	71	89.00	-184.80	5.31	-55.82
71	71	89.00	-170.42	3.26	-56.50
71	72	90.10	-170.42	3.26	-60.09
72	72	90.10	-155.24	1.05	-60.47
72	73	91.20	-155.24	1.05	-61.62
73	73	91.20	-139.23	-1.22	-61.64
73	74	92.30	-139.23	-1.22	-60.31
74	74	92.30	-122.36	-3.39	-59.95
74	75	93.40	-122.36	-3.39	-56.22
75	75	93.40	-104.59	-5.32	-55.44
75	76	94.50	-104.59	-5.32	-49.59
76	76	94.50	-85.85	-6.81	-48.33
76	77	95.60	-85.85	-6.81	-40.84
77	77	95.60	-66.31	-7.71	-39.18

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej2preEl.TOT.To

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-66.31	-7.71	-30.71
78	78	96.70	-45.89	-7.82	-28.61
78	79	97.80	-45.89	-7.82	-20.01
79	79	97.80	-24.76	-6.97	-17.56
79	80	98.90	-24.76	-6.97	-9.89
80	80	98.90	-2.82	-5.00	-7.05
80	81	100.00	-2.82	-5.00	-1.55
101	101	0.00	1.04	-77.41	-568.17
101	102	1.10	1.04	-77.41	-483.02
102	102	1.10	-288.46	-79.38	-885.99
102	103	2.20	-288.46	-79.38	-798.67
103	103	2.20	-287.64	-80.23	-796.22
103	104	3.30	-287.64	-80.23	-707.97
104	104	3.30	-493.79	-80.12	-991.61
104	105	4.40	-493.79	-80.12	-903.48
105	105	4.40	-492.73	-79.23	-901.82
105	106	5.50	-492.73	-79.23	-814.68
106	106	5.50	-698.86	-77.73	-1097.07
106	107	6.60	-698.86	-77.73	-1011.57
107	107	6.60	-698.00	-75.79	-1010.80
107	108	7.70	-698.00	-75.79	-927.42
108	108	7.70	-697.34	-73.62	-927.07
108	109	8.80	-697.34	-73.62	-846.09
109	109	8.80	-696.89	-71.35	-846.11
109	110	9.90	-696.89	-71.35	-767.63
110	110	9.90	-696.63	-69.14	-768.00
110	111	11.00	-696.63	-69.14	-691.94
111	111	11.00	-696.58	-67.10	-692.63
111	112	12.10	-696.58	-67.10	-618.81
112	112	12.10	-696.74	-65.33	-619.78
112	113	13.20	-696.74	-65.33	-547.91
113	113	13.20	-697.12	-63.95	-549.12
113	114	14.30	-697.12	-63.95	-478.78
114	114	14.30	-490.52	-63.03	-196.56
114	115	15.40	-490.52	-63.03	-127.22
115	115	15.40	-491.14	-62.65	-128.72
115	116	16.50	-491.14	-62.65	-59.81
116	116	16.50	-491.78	-62.80	-61.35
116	117	17.60	-491.78	-62.80	7.32
117	117	17.60	-285.26	-63.52	291.91
117	118	18.70	-285.26	-63.52	361.78
118	118	18.70	-285.76	-64.77	360.38
118	119	19.80	-285.76	-64.77	431.62
119	119	19.80	3.99	-66.50	836.22
119	120	20.90	3.99	-66.50	909.37
120	120	20.90	4.12	-68.58	908.55
120	121	22.00	4.12	-68.58	983.99
121	1121	22.00	-36.43	11.26	924.33
121	122	23.40	-36.43	11.26	908.57
122	122	23.40	-34.06	8.34	908.76
122	123	24.80	-34.06	8.34	897.09

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-320.59	5.74	495.03
123	124	26.20	-320.59	5.74	487.00
124	124	26.20	-316.59	3.70	488.21
124	125	27.60	-316.59	3.70	483.02
125	125	27.60	-685.01	2.40	-22.26
125	126	29.00	-685.01	2.40	-25.63
126	126	29.00	-680.87	1.90	-24.10
126	127	30.40	-680.87	1.90	-26.76
127	127	30.40	-1008.54	2.17	-469.16
127	128	31.80	-1008.54	2.17	-472.21
128	128	31.80	-1005.84	3.12	-471.06
128	129	33.20	-1005.84	3.12	-475.43
129	129	33.20	-1004.22	4.56	-474.63
129	130	34.60	-1004.22	4.56	-481.01
130	130	34.60	-1003.63	6.31	-480.55
130	131	36.00	-1003.63	6.31	-489.39
131	131	36.00	-1004.07	8.22	-489.28
131	132	37.40	-1004.07	8.22	-500.79
132	132	37.40	-1005.56	10.12	-501.03
132	133	38.80	-1005.56	10.12	-515.19
133	133	38.80	-1008.13	11.83	-515.79
133	134	40.20	-1008.13	11.83	-532.35
134	134	40.20	-1011.86	13.18	-533.33
134	135	41.60	-1011.86	13.18	-551.78
135	135	41.60	-685.34	13.96	-109.25
135	136	43.00	-685.34	13.96	-128.80
136	136	43.00	-690.79	14.07	-130.26
136	137	44.40	-690.79	14.07	-149.96
137	137	44.40	-323.88	13.44	355.32
137	138	45.80	-323.88	13.44	336.51
138	138	45.80	-329.63	12.11	335.20
138	139	47.20	-329.63	12.11	318.24
139	139	47.20	-45.16	10.20	720.10
139	140	48.60	-45.16	10.20	705.82
140	140	48.60	-49.95	7.90	705.29
140	141	50.00	-49.95	7.90	694.23
141	1141	50.00	-54.06	-7.89	694.23
141	142	51.40	-54.06	-7.89	705.28
142	142	51.40	-57.50	-10.20	705.81
142	143	52.80	-57.50	-10.20	720.09
143	143	52.80	-350.24	-12.11	318.23
143	144	54.20	-350.24	-12.11	335.19
144	144	54.20	-352.80	-13.44	336.49
144	145	55.60	-352.80	-13.44	355.31
145	145	55.60	-728.11	-14.07	-149.97
145	146	57.00	-728.11	-14.07	-130.28
146	146	57.00	-731.16	-13.96	-128.82
146	147	58.40	-731.16	-13.96	-109.27
147	147	58.40	-1066.33	-13.17	-551.80
147	148	59.80	-1066.33	-13.17	-533.35
148	148	59.80	-1071.41	-11.83	-532.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-1071.41	-11.83	-515.82
149	149	61.20	-1077.84	-10.12	-515.21
149	150	62.60	-1077.84	-10.12	-501.05
150	150	62.60	-1085.62	-8.22	-500.81
150	151	64.00	-1085.62	-8.22	-489.30
151	151	64.00	-1094.73	-6.31	-489.41
151	152	65.40	-1094.73	-6.31	-480.57
152	152	65.40	-1105.22	-4.56	-481.03
152	153	66.80	-1105.22	-4.56	-474.65
153	153	66.80	-1117.16	-3.12	-475.45
153	154	68.20	-1117.16	-3.12	-471.08
154	154	68.20	-1130.68	-2.18	-472.22
154	155	69.60	-1130.68	-2.18	-469.18
155	155	69.60	-814.41	-1.90	-26.77
155	156	71.00	-814.41	-1.90	-24.11
156	156	71.00	-830.65	-2.41	-25.64
156	157	72.40	-830.65	-2.41	-22.27
157	157	72.40	-475.15	-3.71	483.02
157	158	73.80	-475.15	-3.71	488.21
158	158	73.80	-493.01	-5.74	487.00
158	159	75.20	-493.01	-5.74	495.03
159	159	75.20	-221.47	-8.34	897.09
159	160	76.60	-221.47	-8.34	908.77
160	160	76.60	-240.16	-11.26	908.58
160	161	78.00	-240.16	-11.26	924.35
161	1161	78.00	-212.32	68.59	984.00
161	162	79.10	-212.32	68.59	908.55
162	162	79.10	-221.75	66.50	909.37
162	163	80.20	-221.75	66.50	836.22
163	163	80.20	-521.38	64.77	431.63
163	164	81.30	-521.38	64.77	360.38
164	164	81.30	-531.35	63.52	361.78
164	165	82.40	-531.35	63.52	291.90
165	165	82.40	-748.89	62.81	7.73
165	166	83.50	-748.89	62.81	-61.36
166	166	83.50	-759.81	62.65	-59.82
166	167	84.60	-759.81	62.65	-128.73
167	167	84.60	-771.30	63.04	-127.23
167	168	85.70	-771.30	63.04	-196.57
168	168	85.70	-990.55	63.95	-478.79
168	169	86.80	-990.55	63.95	-549.13
169	169	86.80	-1003.37	65.33	-547.92
169	170	87.90	-1003.37	65.33	-619.79
170	170	87.90	-1016.96	67.10	-618.82
170	171	89.00	-1016.96	67.10	-692.63
171	171	89.00	-1031.34	69.14	-691.95
171	172	90.10	-1031.34	69.14	-768.00
172	172	90.10	-1046.52	71.36	-767.63
172	173	91.20	-1046.52	71.36	-846.13
173	173	91.20	-1062.53	73.62	-846.10
173	174	92.30	-1062.53	73.62	-927.09

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEI.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEI.FAM1.TOT + [1; 1]ej2preEI.FAM2.TOT + [1; 1]ej2preEI.FAM3.TOT + [1; 1]ej2preEI.FAM

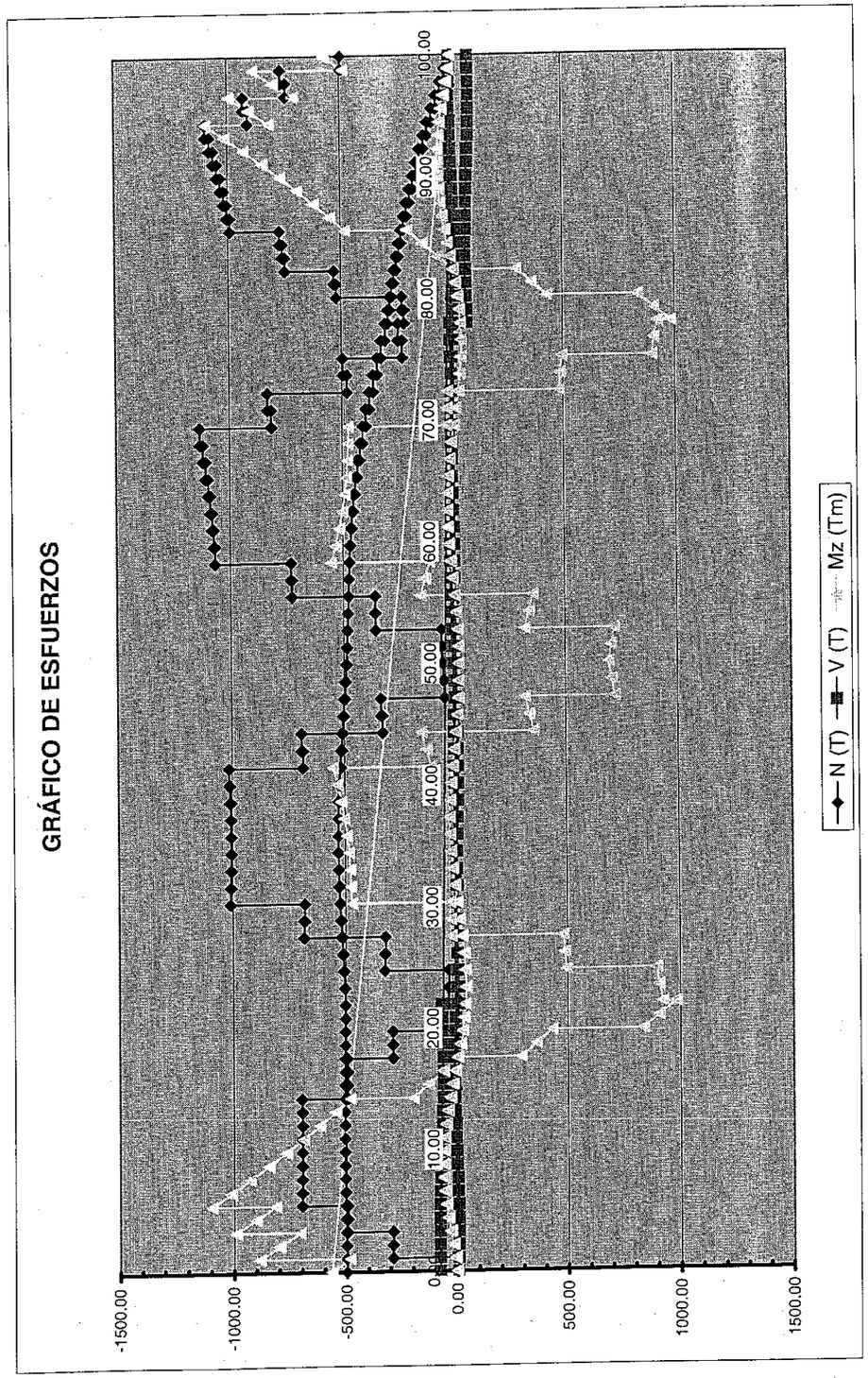
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-1079.40	75.80	-927.44
174	175	93.40	-1079.40	75.80	-1010.82
175	175	93.40	-1097.17	77.72	-1011.59
175	176	94.50	-1097.17	77.72	-1097.09
176	176	94.50	-908.71	79.22	-814.69
176	177	95.60	-908.71	79.22	-901.84
177	177	95.60	-928.25	80.11	-903.49
177	178	96.70	-928.25	80.11	-991.61
178	178	96.70	-741.47	80.22	-707.98
178	179	97.80	-741.47	80.22	-796.23
179	179	97.80	-762.60	79.38	-798.68
179	180	98.90	-762.60	79.38	-885.99
180	180	98.90	-494.46	77.41	-483.02
180	181	100.00	-494.46	77.41	-568.17

11/09/03

Programa DINTEL PACADAR S.A.
ej2preEI.TOT.To

F4.pret.esf.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-498.32	5.00	-1.55
1	2	1.10	-498.32	5.00	-7.05
2	2	1.10	-498.91	6.97	-9.89
2	3	2.20	-498.91	6.97	-17.56
3	3	2.20	-499.72	7.82	-20.01
3	4	3.30	-499.72	7.82	-28.61
4	4	3.30	-500.77	7.71	-30.70
4	5	4.40	-500.77	7.71	-39.18
5	5	4.40	-501.83	6.81	-40.84
5	6	5.50	-501.83	6.81	-48.33
6	6	5.50	-502.90	5.32	-49.59
6	7	6.60	-502.90	5.32	-55.44
7	7	6.60	-503.76	3.39	-56.22
7	8	7.70	-503.76	3.39	-59.95
8	8	7.70	-504.42	1.22	-60.30
8	9	8.80	-504.42	1.22	-61.64
9	9	8.80	-504.88	-1.05	-61.62
9	10	9.90	-504.88	-1.05	-60.46
10	10	9.90	-505.13	-3.26	-60.09
10	11	11.00	-505.13	-3.26	-56.50
11	11	11.00	-505.18	-5.31	-55.82
11	12	12.10	-505.18	-5.31	-49.98
12	12	12.10	-505.02	-7.07	-49.01
12	13	13.20	-505.02	-7.07	-41.23
13	13	13.20	-504.64	-8.46	-40.02
13	14	14.30	-504.64	-8.46	-30.71
14	14	14.30	-504.04	-9.37	-29.28
14	15	15.40	-504.04	-9.37	-18.97
15	15	15.40	-503.42	-9.76	-17.47
15	16	16.50	-503.42	-9.76	-6.73
16	16	16.50	-502.78	-9.60	-5.19
16	17	17.60	-502.78	-9.60	5.37
17	17	17.60	-502.10	-8.88	6.92
17	18	18.70	-502.10	-8.88	16.69
18	18	18.70	-501.60	-7.63	18.10
18	19	19.80	-501.60	-7.63	26.49
19	19	19.80	-501.27	-5.91	27.72
19	20	20.90	-501.27	-5.91	34.22
20	20	20.90	-501.40	-3.82	35.04
20	21	22.00	-501.40	-3.82	39.24
21	1021	22.00	-502.29	-2.32	39.68
21	22	23.40	-502.29	-2.32	42.92
22	22	23.40	-504.66	0.60	42.73
22	23	24.80	-504.66	0.60	41.88
23	23	24.80	-508.21	3.20	41.02
23	24	26.20	-508.21	3.20	36.53
24	24	26.20	-512.21	5.24	35.32
24	25	27.60	-512.21	5.24	27.99
25	25	27.60	-516.75	6.54	26.42
25	26	29.00	-516.75	6.54	17.27
26	26	29.00	-520.90	7.04	15.74

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej2preEl.TOT.Tinf

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-520.90	7.04	5.88
27	27	30.40	-524.74	6.77	4.38
27	28	31.80	-524.74	6.77	-5.10
28	28	31.80	-527.44	5.83	-6.25
28	29	33.20	-527.44	5.83	-14.41
29	29	33.20	-529.06	4.39	-15.21
29	30	34.60	-529.06	4.39	-21.36
30	30	34.60	-529.65	2.64	-21.82
30	31	36.00	-529.65	2.64	-25.51
31	31	36.00	-529.21	0.73	-25.62
31	32	37.40	-529.21	0.73	-26.65
32	32	37.40	-527.72	-1.16	-26.41
32	33	38.80	-527.72	-1.16	-24.78
33	33	38.80	-525.15	-2.87	-24.18
33	34	40.20	-525.15	-2.87	-20.16
34	34	40.20	-521.42	-4.22	-19.18
34	35	41.60	-521.42	-4.22	-13.28
35	35	41.60	-516.42	-5.00	-11.90
35	36	43.00	-516.42	-5.00	-4.90
36	36	43.00	-510.97	-5.11	-3.43
36	37	44.40	-510.97	-5.11	3.72
37	37	44.40	-504.92	-4.48	5.29
37	38	45.80	-504.92	-4.48	11.56
38	38	45.80	-499.17	-3.15	12.87
38	39	47.20	-499.17	-3.15	17.28
39	39	47.20	-493.56	-1.24	18.34
39	40	48.60	-493.56	-1.24	20.08
40	40	48.60	-488.77	1.07	20.60
40	41	50.00	-488.77	1.07	19.11
41	1041	50.00	-484.66	-1.07	19.11
41	42	51.40	-484.66	-1.07	20.60
42	42	51.40	-481.22	1.24	20.07
42	43	52.80	-481.22	1.24	18.34
43	43	52.80	-478.56	3.15	17.27
43	44	54.20	-478.56	3.15	12.87
44	44	54.20	-476.00	4.48	11.56
44	45	55.60	-476.00	4.48	5.29
45	45	55.60	-473.65	5.11	3.71
45	46	57.00	-473.65	5.11	-3.44
46	46	57.00	-470.60	5.00	-4.90
46	47	58.40	-470.60	5.00	-11.91
47	47	58.40	-466.95	4.22	-13.28
47	48	59.80	-466.95	4.22	-19.18
48	48	59.80	-461.87	2.87	-20.16
48	49	61.20	-461.87	2.87	-24.18
49	49	61.20	-455.44	1.16	-24.79
49	50	62.60	-455.44	1.16	-26.41
50	50	62.60	-447.66	-0.73	-26.65
50	51	64.00	-447.66	-0.73	-25.63
51	51	64.00	-438.55	-2.64	-25.52
51	52	65.40	-438.55	-2.64	-21.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-428.06	-4.39	-21.37
52	53	66.80	-428.06	-4.39	-15.22
53	53	66.80	-416.12	-5.83	-14.42
53	54	68.20	-416.12	-5.83	-6.26
54	54	68.20	-402.60	-6.77	-5.11
54	55	69.60	-402.60	-6.77	4.37
55	55	69.60	-387.35	-7.04	5.87
55	56	71.00	-387.35	-7.04	15.73
56	56	71.00	-371.11	-6.54	17.26
56	57	72.40	-371.11	-6.54	26.42
57	57	72.40	-353.65	-5.24	27.99
57	58	73.80	-353.65	-5.24	35.32
58	58	73.80	-335.79	-3.21	36.53
58	59	75.20	-335.79	-3.21	41.02
59	59	75.20	-317.25	-0.61	41.88
59	60	76.60	-317.25	-0.61	42.73
60	60	76.60	-298.56	2.31	42.92
60	61	78.00	-298.56	2.31	39.68
61	1061	78.00	-284.96	3.82	39.25
61	62	79.10	-284.96	3.82	35.04
62	62	79.10	-275.53	5.91	34.22
62	63	80.20	-275.53	5.91	27.72
63	63	80.20	-265.98	7.63	26.50
63	64	81.30	-265.98	7.63	18.10
64	64	81.30	-256.01	8.89	16.70
64	65	82.40	-256.01	8.89	6.93
65	65	82.40	-245.67	9.60	5.37
65	66	83.50	-245.67	9.60	-5.19
66	66	83.50	-234.75	9.76	-6.73
66	67	84.60	-234.75	9.76	-17.47
67	67	84.60	-223.26	9.37	-18.97
67	68	85.70	-223.26	9.37	-29.28
68	68	85.70	-211.21	8.46	-30.71
68	69	86.80	-211.21	8.46	-40.02
69	69	86.80	-198.39	7.08	-41.23
69	70	87.90	-198.39	7.08	-49.01
70	70	87.90	-184.80	5.31	-49.98
70	71	89.00	-184.80	5.31	-55.82
71	71	89.00	-170.42	3.26	-56.50
71	72	90.10	-170.42	3.26	-60.09
72	72	90.10	-155.24	1.05	-60.47
72	73	91.20	-155.24	1.05	-61.62
73	73	91.20	-139.23	-1.22	-61.64
73	74	92.30	-139.23	-1.22	-60.31
74	74	92.30	-122.36	-3.39	-59.95
74	75	93.40	-122.36	-3.39	-56.22
75	75	93.40	-104.59	-5.32	-55.44
75	76	94.50	-104.59	-5.32	-49.59
76	76	94.50	-85.85	-6.81	-48.33
76	77	95.60	-85.85	-6.81	-40.84
77	77	95.60	-66.31	-7.71	-39.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-66.31	-7.71	-30.71
78	78	96.70	-45.89	-7.82	-28.61
78	79	97.80	-45.89	-7.82	-20.01
79	79	97.80	-24.76	-6.97	-17.56
79	80	98.90	-24.76	-6.97	-9.89
80	80	98.90	-2.82	-5.00	-7.05
80	81	100.00	-2.82	-5.00	-1.55
101	101	0.00	1.04	-77.41	-568.17
101	102	1.10	1.04	-77.41	-483.02
102	102	1.10	-288.46	-79.38	-885.99
102	103	2.20	-288.46	-79.38	-798.67
103	103	2.20	-287.64	-80.23	-796.22
103	104	3.30	-287.64	-80.23	-707.97
104	104	3.30	-493.79	-80.12	-991.61
104	105	4.40	-493.79	-80.12	-903.48
105	105	4.40	-492.73	-79.23	-901.82
105	106	5.50	-492.73	-79.23	-814.68
106	106	5.50	-698.86	-77.73	-1097.07
106	107	6.60	-698.86	-77.73	-1011.57
107	107	6.60	-698.00	-75.79	-1010.80
107	108	7.70	-698.00	-75.79	-927.42
108	108	7.70	-697.34	-73.62	-927.07
108	109	8.80	-697.34	-73.62	-846.09
109	109	8.80	-696.89	-71.35	-846.11
109	110	9.90	-696.89	-71.35	-767.63
110	110	9.90	-696.63	-69.14	-768.00
110	111	11.00	-696.63	-69.14	-691.94
111	111	11.00	-696.58	-67.10	-692.63
111	112	12.10	-696.58	-67.10	-618.81
112	112	12.10	-696.74	-65.33	-619.78
112	113	13.20	-696.74	-65.33	-547.91
113	113	13.20	-697.12	-63.95	-549.12
113	114	14.30	-697.12	-63.95	-478.78
114	114	14.30	-490.52	-63.03	-196.56
114	115	15.40	-490.52	-63.03	-127.22
115	115	15.40	-491.14	-62.65	-128.72
115	116	16.50	-491.14	-62.65	-59.81
116	116	16.50	-491.78	-62.80	-61.35
116	117	17.60	-491.78	-62.80	7.32
117	117	17.60	-285.26	-63.52	291.91
117	118	18.70	-285.26	-63.52	361.78
118	118	18.70	-285.76	-64.77	360.38
118	119	19.80	-285.76	-64.77	431.62
119	119	19.80	3.99	-66.50	836.22
119	120	20.90	3.99	-66.50	909.37
120	120	20.90	4.12	-68.58	908.55
120	121	22.00	4.12	-68.58	983.99
121	1121	22.00	-36.43	11.26	924.33
121	122	23.40	-36.43	11.26	908.57
122	122	23.40	-34.06	8.34	908.76
122	123	24.80	-34.06	8.34	897.09

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-320.59	5.74	495.03
123	124	26.20	-320.59	5.74	487.00
124	124	26.20	-316.59	3.70	488.21
124	125	27.60	-316.59	3.70	483.02
125	125	27.60	-685.01	2.40	-22.26
125	126	29.00	-685.01	2.40	-25.63
126	126	29.00	-680.87	1.90	-24.10
126	127	30.40	-680.87	1.90	-26.76
127	127	30.40	-1008.54	2.17	-469.16
127	128	31.80	-1008.54	2.17	-472.21
128	128	31.80	-1005.84	3.12	-471.06
128	129	33.20	-1005.84	3.12	-475.43
129	129	33.20	-1004.22	4.56	-474.63
129	130	34.60	-1004.22	4.56	-481.01
130	130	34.60	-1003.63	6.31	-480.55
130	131	36.00	-1003.63	6.31	-489.39
131	131	36.00	-1004.07	8.22	-489.28
131	132	37.40	-1004.07	8.22	-500.79
132	132	37.40	-1005.56	10.12	-501.03
132	133	38.80	-1005.56	10.12	-515.19
133	133	38.80	-1008.13	11.83	-515.79
133	134	40.20	-1008.13	11.83	-532.35
134	134	40.20	-1011.86	13.18	-533.33
134	135	41.60	-1011.86	13.18	-551.78
135	135	41.60	-685.34	13.96	-109.25
135	136	43.00	-685.34	13.96	-128.80
136	136	43.00	-690.79	14.07	-130.26
136	137	44.40	-690.79	14.07	-149.96
137	137	44.40	-323.88	13.44	355.32
137	138	45.80	-323.88	13.44	336.51
138	138	45.80	-329.63	12.11	335.20
138	139	47.20	-329.63	12.11	318.24
139	139	47.20	-45.16	10.20	720.10
139	140	48.60	-45.16	10.20	705.82
140	140	48.60	-49.95	7.90	705.29
140	141	50.00	-49.95	7.90	694.23
141	1141	50.00	-54.06	-7.89	694.23
141	142	51.40	-54.06	-7.89	705.28
142	142	51.40	-57.50	-10.20	705.81
142	143	52.80	-57.50	-10.20	720.09
143	143	52.80	-350.24	-12.11	318.23
143	144	54.20	-350.24	-12.11	335.19
144	144	54.20	-352.80	-13.44	336.49
144	145	55.60	-352.80	-13.44	355.31
145	145	55.60	-728.11	-14.07	-149.97
145	146	57.00	-728.11	-14.07	-130.28
146	146	57.00	-731.16	-13.96	-128.82
146	147	58.40	-731.16	-13.96	-109.27
147	147	58.40	-1066.33	-13.17	-551.80
147	148	59.80	-1066.33	-13.17	-533.35
148	148	59.80	-1071.41	-11.83	-532.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-1071.41	-11.83	-515.82
149	149	61.20	-1077.84	-10.12	-515.21
149	150	62.60	-1077.84	-10.12	-501.05
150	150	62.60	-1085.62	-8.22	-500.81
150	151	64.00	-1085.62	-8.22	-489.30
151	151	64.00	-1094.73	-6.31	-489.41
151	152	65.40	-1094.73	-6.31	-480.57
152	152	65.40	-1105.22	-4.56	-481.03
152	153	66.80	-1105.22	-4.56	-474.65
153	153	66.80	-1117.16	-3.12	-475.45
153	154	68.20	-1117.16	-3.12	-471.08
154	154	68.20	-1130.68	-2.18	-472.22
154	155	69.60	-1130.68	-2.18	-469.18
155	155	69.60	-814.41	-1.90	-26.77
155	156	71.00	-814.41	-1.90	-24.11
156	156	71.00	-830.65	-2.41	-25.64
156	157	72.40	-830.65	-2.41	-22.27
157	157	72.40	-475.15	-3.71	483.02
157	158	73.80	-475.15	-3.71	488.21
158	158	73.80	-493.01	-5.74	487.00
158	159	75.20	-493.01	-5.74	495.03
159	159	75.20	-221.47	-8.34	897.09
159	160	76.60	-221.47	-8.34	908.77
160	160	76.60	-240.16	-11.26	908.58
160	161	78.00	-240.16	-11.26	924.35
161	1161	78.00	-212.32	68.59	984.00
161	162	79.10	-212.32	68.59	908.55
162	162	79.10	-221.75	66.50	909.37
162	163	80.20	-221.75	66.50	836.22
163	163	80.20	-521.38	64.77	431.63
163	164	81.30	-521.38	64.77	360.38
164	164	81.30	-531.35	63.52	361.78
164	165	82.40	-531.35	63.52	291.90
165	165	82.40	-748.89	62.81	7.73
165	166	83.50	-748.89	62.81	-61.36
166	166	83.50	-759.81	62.65	-59.82
166	167	84.60	-759.81	62.65	-128.73
167	167	84.60	-771.30	63.04	-127.23
167	168	85.70	-771.30	63.04	-196.57
168	168	85.70	-990.55	63.95	-478.79
168	169	86.80	-990.55	63.95	-549.13
169	169	86.80	-1003.37	65.33	-547.92
169	170	87.90	-1003.37	65.33	-619.79
170	170	87.90	-1016.96	67.10	-618.82
170	171	89.00	-1016.96	67.10	-692.63
171	171	89.00	-1031.34	69.14	-691.95
171	172	90.10	-1031.34	69.14	-768.00
172	172	90.10	-1046.52	71.36	-767.63
172	173	91.20	-1046.52	71.36	-846.13
173	173	91.20	-1062.53	73.62	-846.10
173	174	92.30	-1062.53	73.62	-927.09

CÁLCULO TENSIONAL

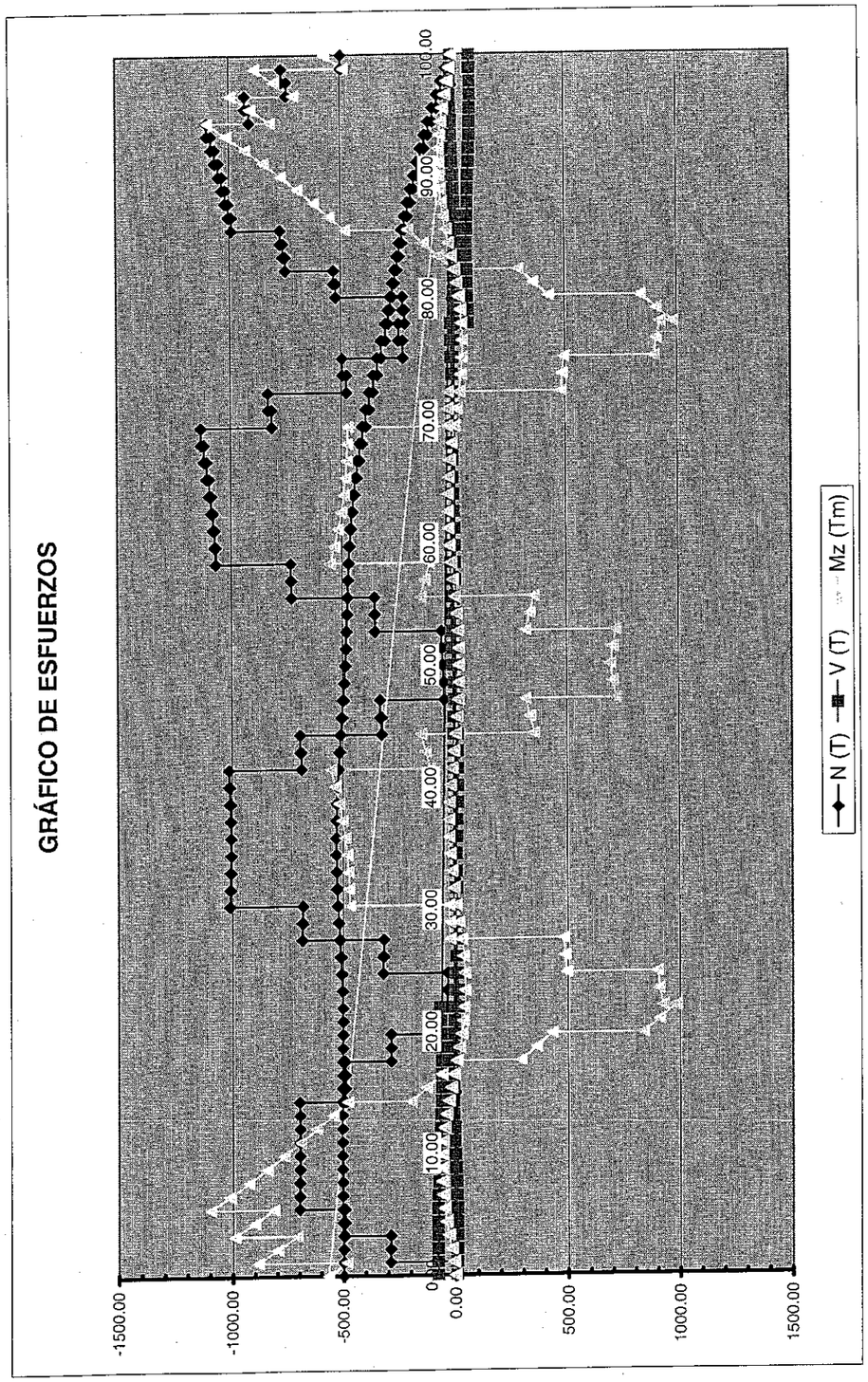
Hipótesis de cálculo:
ej2preEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEI.FAM1.TOT + [1; 1]ej2preEI.FAM2.TOT + [1; 1]ej2preEI.FAM3.TOT + [1; 1]ej2preEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-1079.40	75.80	-927.44
174	175	93.40	-1079.40	75.80	-1010.82
175	175	93.40	-1097.17	77.72	-1011.59
175	176	94.50	-1097.17	77.72	-1097.09
176	176	94.50	-908.71	79.22	-814.69
176	177	95.60	-908.71	79.22	-901.84
177	177	95.60	-928.25	80.11	-903.49
177	178	96.70	-928.25	80.11	-991.61
178	178	96.70	-741.47	80.22	-707.98
178	179	97.80	-741.47	80.22	-796.23
179	179	97.80	-762.60	79.38	-798.68
179	180	98.90	-762.60	79.38	-885.99
180	180	98.90	-494.46	77.41	-483.02
180	181	100.00	-494.46	77.41	-568.17



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-498.32	5.00	-1.55
1	2	1.10	-498.32	5.00	-7.05
2	2	1.10	-498.91	6.97	-9.89
2	3	2.20	-498.91	6.97	-17.56
3	3	2.20	-499.72	7.82	-20.01
3	4	3.30	-499.72	7.82	-28.61
4	4	3.30	-500.77	7.71	-30.70
4	5	4.40	-500.77	7.71	-39.18
5	5	4.40	-501.83	6.81	-40.84
5	6	5.50	-501.83	6.81	-48.33
6	6	5.50	-502.90	5.32	-49.59
6	7	6.60	-502.90	5.32	-55.44
7	7	6.60	-503.76	3.39	-56.22
7	8	7.70	-503.76	3.39	-59.95
8	8	7.70	-504.42	1.22	-60.30
8	9	8.80	-504.42	1.22	-61.64
9	9	8.80	-504.88	-1.05	-61.62
9	10	9.90	-504.88	-1.05	-60.46
10	10	9.90	-505.13	-3.26	-60.09
10	11	11.00	-505.13	-3.26	-56.50
11	11	11.00	-505.18	-5.31	-55.82
11	12	12.10	-505.18	-5.31	-49.98
12	12	12.10	-505.02	-7.07	-49.01
12	13	13.20	-505.02	-7.07	-41.23
13	13	13.20	-504.64	-8.46	-40.02
13	14	14.30	-504.64	-8.46	-30.71
14	14	14.30	-504.04	-9.37	-29.28
14	15	15.40	-504.04	-9.37	-18.97
15	15	15.40	-503.42	-9.76	-17.47
15	16	16.50	-503.42	-9.76	-6.73
16	16	16.50	-502.78	-9.60	-5.19
16	17	17.60	-502.78	-9.60	5.37
17	17	17.60	-502.10	-8.88	6.92
17	18	18.70	-502.10	-8.88	16.69
18	18	18.70	-501.60	-7.63	18.10
18	19	19.80	-501.60	-7.63	26.49
19	19	19.80	-501.27	-5.91	27.72
19	20	20.90	-501.27	-5.91	34.22
20	20	20.90	-501.40	-3.82	35.04
20	21	22.00	-501.40	-3.82	39.24
21	1021	22.00	-502.29	-2.32	39.68
21	22	23.40	-502.29	-2.32	42.92
22	22	23.40	-504.66	0.60	42.73
22	23	24.80	-504.66	0.60	41.88
23	23	24.80	-508.21	3.20	41.02
23	24	26.20	-508.21	3.20	36.53
24	24	26.20	-512.21	5.24	35.32
24	25	27.60	-512.21	5.24	27.99
25	25	27.60	-516.75	6.54	26.42
25	26	29.00	-516.75	6.54	17.27
26	26	29.00	-520.90	7.04	15.74

F4.pret.esf.xls Programa DINTEL PACADAR S.A. 11/09/03
ej2preEl.HIP.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-520.90	7.04	5.88
27	27	30.40	-524.74	6.77	4.38
27	28	31.80	-524.74	6.77	-5.10
28	28	31.80	-527.44	5.83	-6.25
28	29	33.20	-527.44	5.83	-14.41
29	29	33.20	-529.06	4.39	-15.21
29	30	34.60	-529.06	4.39	-21.36
30	30	34.60	-529.65	2.64	-21.82
30	31	36.00	-529.65	2.64	-25.51
31	31	36.00	-529.21	0.73	-25.62
31	32	37.40	-529.21	0.73	-26.65
32	32	37.40	-527.72	-1.16	-26.41
32	33	38.80	-527.72	-1.16	-24.78
33	33	38.80	-525.15	-2.87	-24.18
33	34	40.20	-525.15	-2.87	-20.16
34	34	40.20	-521.42	-4.22	-19.18
34	35	41.60	-521.42	-4.22	-13.28
35	35	41.60	-516.42	-5.00	-11.90
35	36	43.00	-516.42	-5.00	-4.90
36	36	43.00	-510.97	-5.11	-3.43
36	37	44.40	-510.97	-5.11	3.72
37	37	44.40	-504.92	-4.48	5.29
37	38	45.80	-504.92	-4.48	11.56
38	38	45.80	-499.17	-3.15	12.87
38	39	47.20	-499.17	-3.15	17.28
39	39	47.20	-493.56	-1.24	18.34
39	40	48.60	-493.56	-1.24	20.08
40	40	48.60	-488.77	1.07	20.60
40	41	50.00	-488.77	1.07	19.11
41	1041	50.00	-484.66	-1.07	19.11
41	42	51.40	-484.66	-1.07	20.60
42	42	51.40	-481.22	1.24	20.07
42	43	52.80	-481.22	1.24	18.34
43	43	52.80	-478.56	3.15	17.27
43	44	54.20	-478.56	3.15	12.87
44	44	54.20	-476.00	4.48	11.56
44	45	55.60	-476.00	4.48	5.29
45	45	55.60	-473.65	5.11	3.71
45	46	57.00	-473.65	5.11	-3.44
46	46	57.00	-470.60	5.00	-4.90
46	47	58.40	-470.60	5.00	-11.91
47	47	58.40	-466.95	4.22	-13.28
47	48	59.80	-466.95	4.22	-19.18
48	48	59.80	-461.87	2.87	-20.16
48	49	61.20	-461.87	2.87	-24.18
49	49	61.20	-455.44	1.16	-24.79
49	50	62.60	-455.44	1.16	-26.41
50	50	62.60	-447.66	-0.73	-26.65
50	51	64.00	-447.66	-0.73	-25.63
51	51	64.00	-438.55	-2.64	-25.52
51	52	65.40	-438.55	-2.64	-21.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-428.06	-4.39	-21.37
52	53	66.80	-428.06	-4.39	-15.22
53	53	66.80	-416.12	-5.83	-14.42
53	54	68.20	-416.12	-5.83	-6.26
54	54	68.20	-402.60	-6.77	-5.11
54	55	69.60	-402.60	-6.77	4.37
55	55	69.60	-387.35	-7.04	5.87
55	56	71.00	-387.35	-7.04	15.73
56	56	71.00	-371.11	-6.54	17.26
56	57	72.40	-371.11	-6.54	26.42
57	57	72.40	-353.65	-5.24	27.99
57	58	73.80	-353.65	-5.24	35.32
58	58	73.80	-335.79	-3.21	36.53
58	59	75.20	-335.79	-3.21	41.02
59	59	75.20	-317.25	-0.61	41.88
59	60	76.60	-317.25	-0.61	42.73
60	60	76.60	-298.56	2.31	42.92
60	61	78.00	-298.56	2.31	39.68
61	1061	78.00	-284.96	3.82	39.25
61	62	79.10	-284.96	3.82	35.04
62	62	79.10	-275.53	5.91	34.22
62	63	80.20	-275.53	5.91	27.72
63	63	80.20	-265.98	7.63	26.50
63	64	81.30	-265.98	7.63	18.10
64	64	81.30	-256.01	8.89	16.70
64	65	82.40	-256.01	8.89	6.93
65	65	82.40	-245.67	9.60	5.37
65	66	83.50	-245.67	9.60	-5.19
66	66	83.50	-234.75	9.76	-6.73
66	67	84.60	-234.75	9.76	-17.47
67	67	84.60	-223.26	9.37	-18.97
67	68	85.70	-223.26	9.37	-29.28
68	68	85.70	-211.21	8.46	-30.71
68	69	86.80	-211.21	8.46	-40.02
69	69	86.80	-198.39	7.08	-41.23
69	70	87.90	-198.39	7.08	-49.01
70	70	87.90	-184.80	5.31	-49.98
70	71	89.00	-184.80	5.31	-55.82
71	71	89.00	-170.42	3.26	-56.50
71	72	90.10	-170.42	3.26	-60.09
72	72	90.10	-155.24	1.05	-60.47
72	73	91.20	-155.24	1.05	-61.62
73	73	91.20	-139.23	-1.22	-61.64
73	74	92.30	-139.23	-1.22	-60.31
74	74	92.30	-122.36	-3.39	-59.95
74	75	93.40	-122.36	-3.39	-56.22
75	75	93.40	-104.59	-5.32	-55.44
75	76	94.50	-104.59	-5.32	-49.59
76	76	94.50	-85.85	-6.81	-48.33
76	77	95.60	-85.85	-6.81	-40.84
77	77	95.60	-66.31	-7.71	-39.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-66.31	-7.71	-30.71
78	78	96.70	-45.89	-7.82	-28.61
78	79	97.80	-45.89	-7.82	-20.01
79	79	97.80	-24.76	-6.97	-17.56
79	80	98.90	-24.76	-6.97	-9.89
80	80	98.90	-2.82	-5.00	-7.05
80	81	100.00	-2.82	-5.00	-1.55
101	101	0.00	498.32	-77.41	1.55
101	102	1.10	498.32	-77.41	86.70
102	102	1.10	498.90	-79.38	89.55
102	103	2.20	498.90	-79.38	176.87
103	103	2.20	499.72	-80.23	179.31
103	104	3.30	499.72	-80.23	267.56
104	104	3.30	500.77	-80.12	269.66
104	105	4.40	500.77	-80.12	357.79
105	105	4.40	501.83	-79.23	359.44
105	106	5.50	501.83	-79.23	446.59
106	106	5.50	502.90	-77.73	447.85
106	107	6.60	502.90	-77.73	533.35
107	107	6.60	503.76	-75.79	534.13
107	108	7.70	503.76	-75.79	617.50
108	108	7.70	504.42	-73.62	617.86
108	109	8.80	504.42	-73.62	698.84
109	109	8.80	504.88	-71.35	698.81
109	110	9.90	504.88	-71.35	777.30
110	110	9.90	505.13	-69.14	776.93
110	111	11.00	505.13	-69.14	852.98
111	111	11.00	505.18	-67.10	852.30
111	112	12.10	505.18	-67.10	926.11
112	112	12.10	505.02	-65.33	925.15
112	113	13.20	505.02	-65.33	997.01
113	113	13.20	504.64	-63.95	995.80
113	114	14.30	504.64	-63.95	1066.15
114	114	14.30	504.04	-63.03	1064.71
114	115	15.40	504.04	-63.03	1134.05
115	115	15.40	503.42	-62.65	1132.55
115	116	16.50	503.42	-62.65	1201.46
116	116	16.50	502.78	-62.80	1199.92
116	117	17.60	502.78	-62.80	1269.00
117	117	17.60	502.10	-63.52	1267.45
117	118	18.70	502.10	-63.52	1337.32
118	118	18.70	501.60	-64.77	1335.91
118	119	19.80	501.60	-64.77	1407.16
119	119	19.80	501.27	-66.50	1405.94
119	120	20.90	501.27	-66.50	1479.08
120	120	20.90	501.40	-68.58	1478.26
120	121	22.00	501.40	-68.58	1553.70
121	1121	22.00	502.29	11.26	1553.27
121	122	23.40	502.29	11.26	1537.51
122	122	23.40	504.66	8.34	1537.70
122	123	24.80	504.66	8.34	1526.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	508.21	5.74	1526.89
123	124	26.20	508.21	5.74	1518.85
124	124	26.20	512.21	3.70	1520.07
124	125	27.60	512.21	3.70	1514.88
125	125	27.60	516.75	2.40	1516.44
125	126	29.00	516.75	2.40	1513.08
126	126	29.00	520.89	1.90	1514.61
126	127	30.40	520.89	1.90	1511.95
127	127	30.40	524.74	2.17	1513.45
127	128	31.80	524.74	2.17	1510.41
128	128	31.80	527.44	3.12	1511.56
128	129	33.20	527.44	3.12	1507.19
129	129	33.20	529.06	4.56	1507.99
129	130	34.60	529.06	4.56	1501.61
130	130	34.60	529.65	6.31	1502.06
130	131	36.00	529.65	6.31	1493.23
131	131	36.00	529.21	8.22	1493.34
131	132	37.40	529.21	8.22	1481.83
132	132	37.40	527.72	10.12	1481.59
132	133	38.80	527.72	10.12	1467.43
133	133	38.80	525.15	11.83	1466.82
133	134	40.20	525.15	11.83	1450.26
134	134	40.20	521.42	13.18	1449.28
134	135	41.60	521.42	13.18	1430.83
135	135	41.60	516.42	13.96	1429.46
135	136	43.00	516.42	13.96	1409.91
136	136	43.00	510.97	14.07	1408.45
136	137	44.40	510.97	14.07	1388.75
137	137	44.40	504.92	13.44	1387.18
137	138	45.80	504.92	13.44	1368.36
138	138	45.80	499.17	12.11	1367.05
138	139	47.20	499.17	12.11	1350.10
139	139	47.20	493.56	10.20	1349.03
139	140	48.60	493.56	10.20	1334.75
140	140	48.60	488.77	7.90	1334.22
140	141	50.00	488.77	7.90	1323.17
141	1141	50.00	484.66	-7.89	1323.17
141	142	51.40	484.66	-7.89	1334.22
142	142	51.40	481.22	-10.20	1334.75
142	143	52.80	481.22	-10.20	1349.02
143	143	52.80	478.56	-12.11	1350.09
143	144	54.20	478.56	-12.11	1367.04
144	144	54.20	476.00	-13.44	1368.35
144	145	55.60	476.00	-13.44	1387.17
145	145	55.60	473.65	-14.07	1388.74
145	146	57.00	473.65	-14.07	1408.43
146	146	57.00	470.60	-13.96	1409.89
146	147	58.40	470.60	-13.96	1429.44
147	147	58.40	466.95	-13.17	1430.82
147	148	59.80	466.95	-13.17	1449.26
148	148	59.80	461.87	-11.83	1450.24

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	461.87	-11.83	1466.80
149	149	61.20	455.44	-10.12	1467.40
149	150	62.60	455.44	-10.12	1481.57
150	150	62.60	447.66	-8.22	1481.81
150	151	64.00	447.66	-8.22	1493.32
151	151	64.00	438.55	-6.31	1493.21
151	152	65.40	438.55	-6.31	1502.04
152	152	65.40	428.06	-4.56	1501.59
152	153	66.80	428.06	-4.56	1507.97
153	153	66.80	416.12	-3.12	1507.17
153	154	68.20	416.12	-3.12	1511.54
154	154	68.20	402.60	-2.18	1510.39
154	155	69.60	402.60	-2.18	1513.44
155	155	69.60	387.35	-1.90	1511.93
155	156	71.00	387.35	-1.90	1514.60
156	156	71.00	371.11	-2.41	1513.07
156	157	72.40	371.11	-2.41	1516.44
157	157	72.40	353.65	-3.71	1514.87
157	158	73.80	353.65	-3.71	1520.06
158	158	73.80	335.79	-5.74	1518.85
158	159	75.20	335.79	-5.74	1526.89
159	159	75.20	317.25	-8.34	1526.03
159	160	76.60	317.25	-8.34	1537.71
160	160	76.60	298.56	-11.26	1537.52
160	161	78.00	298.56	-11.26	1553.28
161	1161	78.00	284.96	68.59	1553.72
161	162	79.10	284.96	68.59	1478.27
162	162	79.10	275.53	66.50	1479.09
162	163	80.20	275.53	66.50	1405.94
163	163	80.20	265.98	64.77	1407.17
163	164	81.30	265.98	64.77	1335.91
164	164	81.30	256.01	63.52	1337.32
164	165	82.40	256.01	63.52	1267.44
165	165	82.40	245.67	62.81	1269.00
165	166	83.50	245.67	62.81	1199.91
166	166	83.50	234.75	62.65	1201.45
166	167	84.60	234.75	62.65	1132.54
167	167	84.60	223.26	63.04	1134.04
167	168	85.70	223.26	63.04	1064.70
168	168	85.70	211.21	63.95	1066.13
168	169	86.80	211.21	63.95	995.79
169	169	86.80	198.39	65.33	997.00
169	170	87.90	198.39	65.33	925.14
170	170	87.90	184.80	67.10	926.10
170	171	89.00	184.80	67.10	852.29
171	171	89.00	170.42	69.14	852.98
171	172	90.10	170.42	69.14	776.92
172	172	90.10	155.24	71.36	777.29
172	173	91.20	155.24	71.36	698.80
173	173	91.20	139.23	73.62	698.82
173	174	92.30	139.23	73.62	617.84

CÁLCULO TENSIONAL

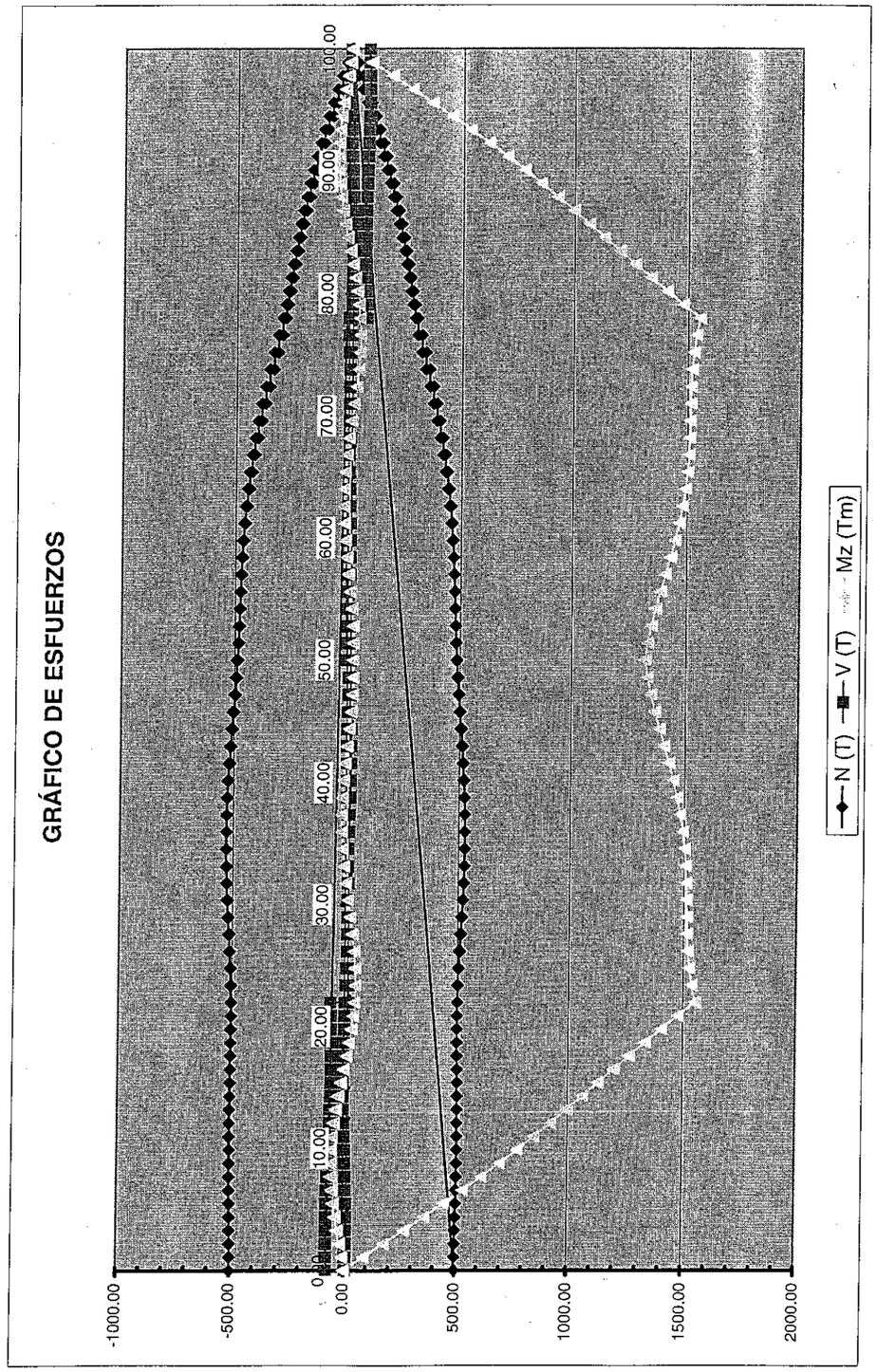
Hipótesis de cálculo:
ej2preEl.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	122.36	75.80	617.48
174	175	93.40	122.36	75.80	534.11
175	175	93.40	104.59	77.72	533.33
175	176	94.50	104.59	77.72	447.84
176	176	94.50	85.85	79.22	446.58
176	177	95.60	85.85	79.22	359.43
177	177	95.60	66.31	80.11	357.78
177	178	96.70	66.31	80.11	269.65
178	178	96.70	45.89	80.22	267.56
178	179	97.80	45.89	80.22	179.31
179	179	97.80	24.76	79.38	176.86
179	180	98.90	24.76	79.38	89.54
180	180	98.90	2.82	77.41	86.70
180	181	100.00	2.82	77.41	1.55



CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-498.32	5.00	-1.55
1	2	1.10	-498.32	5.00	-7.05
2	2	1.10	-498.91	6.97	-9.89
2	3	2.20	-498.91	6.97	-17.56
3	3	2.20	-499.72	7.82	-20.01
3	4	3.30	-499.72	7.82	-28.61
4	4	3.30	-500.77	7.71	-30.70
4	5	4.40	-500.77	7.71	-39.18
5	5	4.40	-501.83	6.81	-40.84
5	6	5.50	-501.83	6.81	-48.33
6	6	5.50	-502.90	5.32	-49.59
6	7	6.60	-502.90	5.32	-55.44
7	7	6.60	-503.76	3.39	-56.22
7	8	7.70	-503.76	3.39	-59.95
8	8	7.70	-504.42	1.22	-60.30
8	9	8.80	-504.42	1.22	-61.64
9	9	8.80	-504.88	-1.05	-61.62
9	10	9.90	-504.88	-1.05	-60.46
10	10	9.90	-505.13	-3.26	-60.09
10	11	11.00	-505.13	-3.26	-56.50
11	11	11.00	-505.18	-5.31	-55.82
11	12	12.10	-505.18	-5.31	-49.98
12	12	12.10	-505.02	-7.07	-49.01
12	13	13.20	-505.02	-7.07	-41.23
13	13	13.20	-504.64	-8.46	-40.02
13	14	14.30	-504.64	-8.46	-30.71
14	14	14.30	-504.04	-9.37	-29.28
14	15	15.40	-504.04	-9.37	-18.97
15	15	15.40	-503.42	-9.76	-17.47
15	16	16.50	-503.42	-9.76	-6.73
16	16	16.50	-502.78	-9.60	-5.19
16	17	17.60	-502.78	-9.60	5.37
17	17	17.60	-502.10	-8.88	6.92
17	18	18.70	-502.10	-8.88	16.69
18	18	18.70	-501.60	-7.63	18.10
18	19	19.80	-501.60	-7.63	26.49
19	19	19.80	-501.27	-5.91	27.72
19	20	20.90	-501.27	-5.91	34.22
20	20	20.90	-501.40	-3.82	35.04
20	21	22.00	-501.40	-3.82	39.24
21	1021	22.00	-502.29	-2.32	39.68
21	22	23.40	-502.29	-2.32	42.92
22	22	23.40	-504.66	0.60	42.73
22	23	24.80	-504.66	0.60	41.88
23	23	24.80	-508.21	3.20	41.02
23	24	26.20	-508.21	3.20	36.53
24	24	26.20	-512.21	5.24	35.32
24	25	27.60	-512.21	5.24	27.99
25	25	27.60	-516.75	6.54	26.42
25	26	29.00	-516.75	6.54	17.27
26	26	29.00	-520.90	7.04	15.74

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-520.90	7.04	5.88
27	27	30.40	-524.74	6.77	4.38
27	28	31.80	-524.74	6.77	-5.10
28	28	31.80	-527.44	5.83	-6.25
28	29	33.20	-527.44	5.83	-14.41
29	29	33.20	-529.06	4.39	-15.21
29	30	34.60	-529.06	4.39	-21.36
30	30	34.60	-529.65	2.64	-21.82
30	31	36.00	-529.65	2.64	-25.51
31	31	36.00	-529.21	0.73	-25.62
31	32	37.40	-529.21	0.73	-26.65
32	32	37.40	-527.72	-1.16	-26.41
32	33	38.80	-527.72	-1.16	-24.78
33	33	38.80	-525.15	-2.87	-24.18
33	34	40.20	-525.15	-2.87	-20.16
34	34	40.20	-521.42	-4.22	-19.18
34	35	41.60	-521.42	-4.22	-13.28
35	35	41.60	-516.42	-5.00	-11.90
35	36	43.00	-516.42	-5.00	-4.90
36	36	43.00	-510.97	-5.11	-3.43
36	37	44.40	-510.97	-5.11	3.72
37	37	44.40	-504.92	-4.48	5.29
37	38	45.80	-504.92	-4.48	11.56
38	38	45.80	-499.17	-3.15	12.87
38	39	47.20	-499.17	-3.15	17.28
39	39	47.20	-493.56	-1.24	18.34
39	40	48.60	-493.56	-1.24	20.08
40	40	48.60	-488.77	1.07	20.60
40	41	50.00	-488.77	1.07	19.11
41	1041	50.00	-484.66	-1.07	19.11
41	42	51.40	-484.66	-1.07	20.60
42	42	51.40	-481.22	1.24	20.07
42	43	52.80	-481.22	1.24	18.34
43	43	52.80	-478.56	3.15	17.27
43	44	54.20	-478.56	3.15	12.87
44	44	54.20	-476.00	4.48	11.56
44	45	55.60	-476.00	4.48	5.29
45	45	55.60	-473.65	5.11	3.71
45	46	57.00	-473.65	5.11	-3.44
46	46	57.00	-470.60	5.00	-4.90
46	47	58.40	-470.60	5.00	-11.91
47	47	58.40	-466.95	4.22	-13.28
47	48	59.80	-466.95	4.22	-19.18
48	48	59.80	-461.87	2.87	-20.16
48	49	61.20	-461.87	2.87	-24.18
49	49	61.20	-455.44	1.16	-24.79
49	50	62.60	-455.44	1.16	-26.41
50	50	62.60	-447.66	-0.73	-26.65
50	51	64.00	-447.66	-0.73	-25.63
51	51	64.00	-438.55	-2.64	-25.52
51	52	65.40	-438.55	-2.64	-21.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-428.06	-4.39	-21.37
52	53	66.80	-428.06	-4.39	-15.22
53	53	66.80	-416.12	-5.83	-14.42
53	54	68.20	-416.12	-5.83	-6.26
54	54	68.20	-402.60	-6.77	-5.11
54	55	69.60	-402.60	-6.77	4.37
55	55	69.60	-387.35	-7.04	5.87
55	56	71.00	-387.35	-7.04	15.73
56	56	71.00	-371.11	-6.54	17.26
56	57	72.40	-371.11	-6.54	26.42
57	57	72.40	-353.65	-5.24	27.99
57	58	73.80	-353.65	-5.24	35.32
58	58	73.80	-335.79	-3.21	36.53
58	59	75.20	-335.79	-3.21	41.02
59	59	75.20	-317.25	-0.61	41.88
59	60	76.60	-317.25	-0.61	42.73
60	60	76.60	-298.56	2.31	42.92
60	61	78.00	-298.56	2.31	39.68
61	1061	78.00	-284.96	3.82	39.25
61	62	79.10	-284.96	3.82	35.04
62	62	79.10	-275.53	5.91	34.22
62	63	80.20	-275.53	5.91	27.72
63	63	80.20	-265.98	7.63	26.50
63	64	81.30	-265.98	7.63	18.10
64	64	81.30	-256.01	8.89	16.70
64	65	82.40	-256.01	8.89	6.93
65	65	82.40	-245.67	9.60	5.37
65	66	83.50	-245.67	9.60	-5.19
66	66	83.50	-234.75	9.76	-6.73
66	67	84.60	-234.75	9.76	-17.47
67	67	84.60	-223.26	9.37	-18.97
67	68	85.70	-223.26	9.37	-29.28
68	68	85.70	-211.21	8.46	-30.71
68	69	86.80	-211.21	8.46	-40.02
69	69	86.80	-198.39	7.08	-41.23
69	70	87.90	-198.39	7.08	-49.01
70	70	87.90	-184.80	5.31	-49.98
70	71	89.00	-184.80	5.31	-55.82
71	71	89.00	-170.42	3.26	-56.50
71	72	90.10	-170.42	3.26	-60.09
72	72	90.10	-155.24	1.05	-60.47
72	73	91.20	-155.24	1.05	-61.62
73	73	91.20	-139.23	-1.22	-61.64
73	74	92.30	-139.23	-1.22	-60.31
74	74	92.30	-122.36	-3.39	-59.95
74	75	93.40	-122.36	-3.39	-56.22
75	75	93.40	-104.59	-5.32	-55.44
75	76	94.50	-104.59	-5.32	-49.59
76	76	94.50	-85.85	-6.81	-48.33
76	77	95.60	-85.85	-6.81	-40.84
77	77	95.60	-66.31	-7.71	-39.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	461.87	-11.83	1466.80
149	149	61.20	455.44	-10.12	1467.40
149	150	62.60	455.44	-10.12	1481.57
150	150	62.60	447.66	-8.22	1481.81
150	151	64.00	447.66	-8.22	1493.32
151	151	64.00	438.55	-6.31	1493.21
151	152	65.40	438.55	-6.31	1502.04
152	152	65.40	428.06	-4.56	1501.59
152	153	66.80	428.06	-4.56	1507.97
153	153	66.80	416.12	-3.12	1507.17
153	154	68.20	416.12	-3.12	1511.54
154	154	68.20	402.60	-2.18	1510.39
154	155	69.60	402.60	-2.18	1513.44
155	155	69.60	387.35	-1.90	1511.93
155	156	71.00	387.35	-1.90	1514.60
156	156	71.00	371.11	-2.41	1513.07
156	157	72.40	371.11	-2.41	1516.44
157	157	72.40	353.65	-3.71	1514.87
157	158	73.80	353.65	-3.71	1520.06
158	158	73.80	335.79	-5.74	1518.85
158	159	75.20	335.79	-5.74	1526.89
159	159	75.20	317.25	-8.34	1526.03
159	160	76.60	317.25	-8.34	1537.71
160	160	76.60	298.56	-11.26	1537.52
160	161	78.00	298.56	-11.26	1553.28
161	1161	78.00	284.96	68.59	1553.72
161	162	79.10	284.96	68.59	1478.27
162	162	79.10	275.53	66.50	1479.09
162	163	80.20	275.53	66.50	1405.94
163	163	80.20	265.98	64.77	1407.17
163	164	81.30	265.98	64.77	1335.91
164	164	81.30	256.01	63.52	1337.32
164	165	82.40	256.01	63.52	1267.44
165	165	82.40	245.67	62.81	1269.00
165	166	83.50	245.67	62.81	1199.91
166	166	83.50	234.75	62.65	1201.45
166	167	84.60	234.75	62.65	1132.54
167	167	84.60	223.26	63.04	1134.04
167	168	85.70	223.26	63.04	1064.70
168	168	85.70	211.21	63.95	1066.13
168	169	86.80	211.21	63.95	995.79
169	169	86.80	198.39	65.33	997.00
169	170	87.90	198.39	65.33	925.14
170	170	87.90	184.80	67.10	926.10
170	171	89.00	184.80	67.10	852.29
171	171	89.00	170.42	69.14	852.98
171	172	90.10	170.42	69.14	776.92
172	172	90.10	155.24	71.36	777.29
172	173	91.20	155.24	71.36	698.80
173	173	91.20	139.23	73.62	698.82
173	174	92.30	139.23	73.62	617.84

CÁLCULO TENSIONAL

Hipótesis de cálculo:

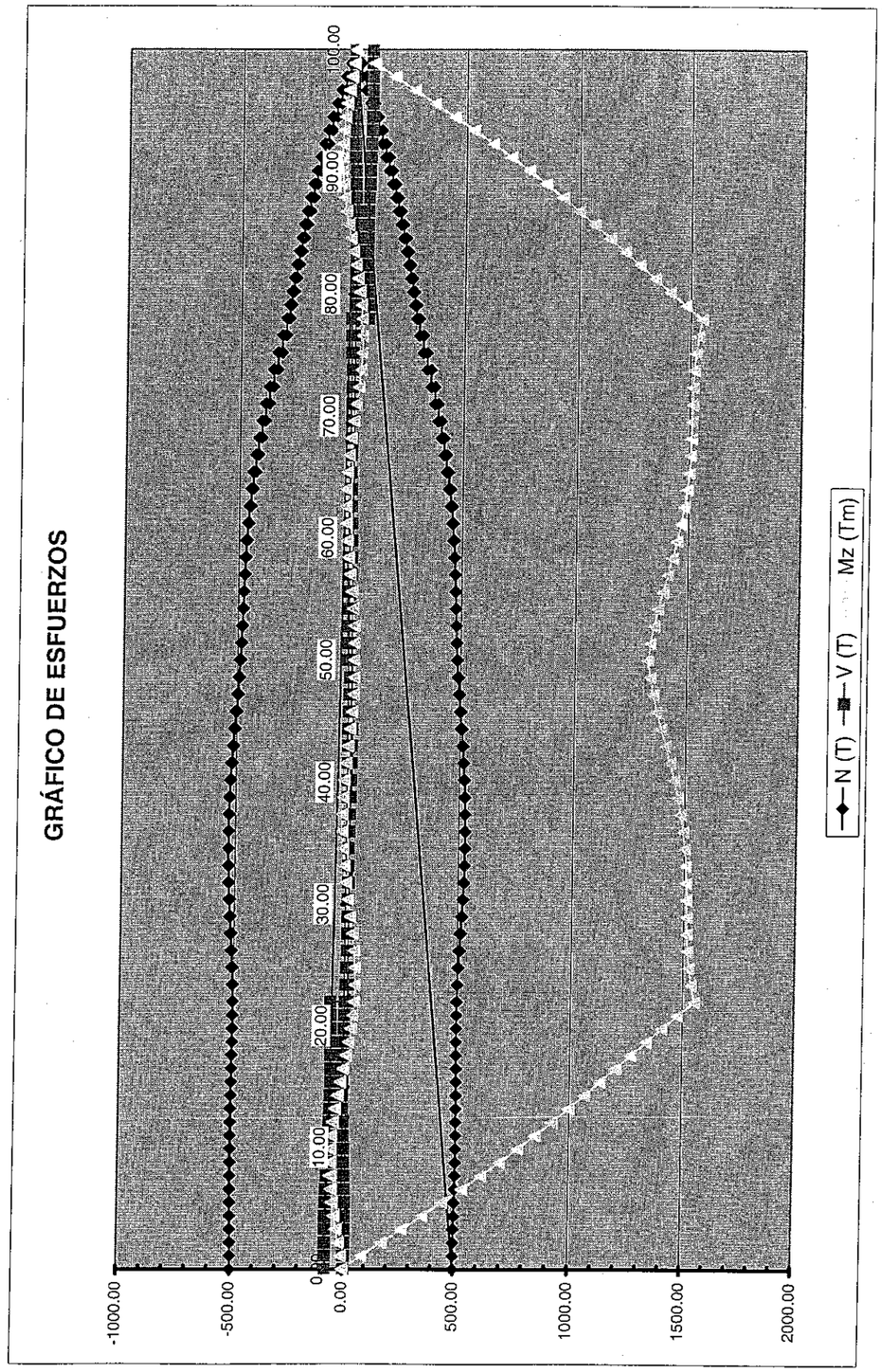
ej2preEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [-1;-1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.TOT + [-1;-1]ej2preEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	122.36	75.80	617.48
174	175	93.40	122.36	75.80	534.11
175	175	93.40	104.59	77.72	533.33
175	176	94.50	104.59	77.72	447.84
176	176	94.50	85.85	79.22	446.58
176	177	95.60	85.85	79.22	359.43
177	177	95.60	66.31	80.11	357.78
177	178	96.70	66.31	80.11	269.65
178	178	96.70	45.89	80.22	267.56
178	179	97.80	45.89	80.22	179.31
179	179	97.80	24.76	79.38	176.86
179	180	98.90	24.76	79.38	89.54
180	180	98.90	2.82	77.41	86.70
180	181	100.00	2.82	77.41	1.55



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2preEI.FAM1.ISO + [1; 1]ej2preEI.FAM2.ISO + [1; 1]ej2preEI.FAM3.ISO + [1; 1]ej2preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	0.00	0.00	0.00	0.00
2	2	0.00	0.00	0.00	0.00
2	3	0.00	0.00	0.00	0.00
3	3	0.00	0.00	0.00	0.00
3	4	0.00	0.00	0.00	0.00
4	4	0.00	0.00	0.00	0.00
4	5	0.00	0.00	0.00	0.00
5	5	0.00	0.00	0.00	0.00
5	6	0.00	0.00	0.00	0.00
6	6	0.00	0.00	0.00	0.00
6	7	0.00	0.00	0.00	0.00
7	7	0.00	0.00	0.00	0.00
7	8	0.00	0.00	0.00	0.00
8	8	0.00	0.00	0.00	0.00
8	9	0.00	0.00	0.00	0.00
9	9	0.00	0.00	0.00	0.00
9	10	0.00	0.00	0.00	0.00
10	10	0.00	0.00	0.00	0.00
10	11	0.00	0.00	0.00	0.00
11	11	0.00	0.00	0.00	0.00
11	12	0.00	0.00	0.00	0.00
12	12	0.00	0.00	0.00	0.00
12	13	0.00	0.00	0.00	0.00
13	13	0.00	0.00	0.00	0.00
13	14	0.00	0.00	0.00	0.00
14	14	0.00	0.00	0.00	0.00
14	15	0.00	0.00	0.00	0.00
15	15	0.00	0.00	0.00	0.00
15	16	0.00	0.00	0.00	0.00
16	16	0.00	0.00	0.00	0.00
16	17	0.00	0.00	0.00	0.00
17	17	0.00	0.00	0.00	0.00
17	18	0.00	0.00	0.00	0.00
18	18	0.00	0.00	0.00	0.00
18	19	0.00	0.00	0.00	0.00
19	19	0.00	0.00	0.00	0.00
19	20	0.00	0.00	0.00	0.00
20	20	0.00	0.00	0.00	0.00
20	21	0.00	0.00	0.00	0.00
21	1021	0.00	0.00	0.00	0.00
21	22	0.00	0.00	0.00	0.00
22	22	0.00	0.00	0.00	0.00
22	23	0.00	0.00	0.00	0.00
23	23	0.00	0.00	0.00	0.00
23	24	0.00	0.00	0.00	0.00
24	24	0.00	0.00	0.00	0.00
24	25	0.00	0.00	0.00	0.00
25	25	0.00	0.00	0.00	0.00
25	26	0.00	0.00	0.00	0.00
26	26	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2preEI.FAM1.ISO + [1; 1]ej2preEI.FAM2.ISO + [1; 1]ej2preEI.FAM3.ISO + [1; 1]ej2preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	0.00	0.00	0.00	0.00
27	27	0.00	0.00	0.00	0.00
27	28	0.00	0.00	0.00	0.00
28	28	0.00	0.00	0.00	0.00
28	29	0.00	0.00	0.00	0.00
29	29	0.00	0.00	0.00	0.00
29	30	0.00	0.00	0.00	0.00
30	30	0.00	0.00	0.00	0.00
30	31	0.00	0.00	0.00	0.00
31	31	0.00	0.00	0.00	0.00
31	32	0.00	0.00	0.00	0.00
32	32	0.00	0.00	0.00	0.00
32	33	0.00	0.00	0.00	0.00
33	33	0.00	0.00	0.00	0.00
33	34	0.00	0.00	0.00	0.00
34	34	0.00	0.00	0.00	0.00
34	35	0.00	0.00	0.00	0.00
35	35	0.00	0.00	0.00	0.00
35	36	0.00	0.00	0.00	0.00
36	36	0.00	0.00	0.00	0.00
36	37	0.00	0.00	0.00	0.00
37	37	0.00	0.00	0.00	0.00
37	38	0.00	0.00	0.00	0.00
38	38	0.00	0.00	0.00	0.00
38	39	0.00	0.00	0.00	0.00
39	39	0.00	0.00	0.00	0.00
39	40	0.00	0.00	0.00	0.00
40	40	0.00	0.00	0.00	0.00
40	41	0.00	0.00	0.00	0.00
41	1041	0.00	0.00	0.00	0.00
41	42	0.00	0.00	0.00	0.00
42	42	0.00	0.00	0.00	0.00
42	43	0.00	0.00	0.00	0.00
43	43	0.00	0.00	0.00	0.00
43	44	0.00	0.00	0.00	0.00
44	44	0.00	0.00	0.00	0.00
44	45	0.00	0.00	0.00	0.00
45	45	0.00	0.00	0.00	0.00
45	46	0.00	0.00	0.00	0.00
46	46	0.00	0.00	0.00	0.00
46	47	0.00	0.00	0.00	0.00
47	47	0.00	0.00	0.00	0.00
47	48	0.00	0.00	0.00	0.00
48	48	0.00	0.00	0.00	0.00
48	49	0.00	0.00	0.00	0.00
49	49	0.00	0.00	0.00	0.00
49	50	0.00	0.00	0.00	0.00
50	50	0.00	0.00	0.00	0.00
50	51	0.00	0.00	0.00	0.00
51	51	0.00	0.00	0.00	0.00
51	52	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	0.00	0.00	0.00	0.00
52	53	0.00	0.00	0.00	0.00
53	53	0.00	0.00	0.00	0.00
53	54	0.00	0.00	0.00	0.00
54	54	0.00	0.00	0.00	0.00
54	55	0.00	0.00	0.00	0.00
55	55	0.00	0.00	0.00	0.00
55	56	0.00	0.00	0.00	0.00
56	56	0.00	0.00	0.00	0.00
56	57	0.00	0.00	0.00	0.00
57	57	0.00	0.00	0.00	0.00
57	58	0.00	0.00	0.00	0.00
58	58	0.00	0.00	0.00	0.00
58	59	0.00	0.00	0.00	0.00
59	59	0.00	0.00	0.00	0.00
59	60	0.00	0.00	0.00	0.00
60	60	0.00	0.00	0.00	0.00
60	61	0.00	0.00	0.00	0.00
61	1061	0.00	0.00	0.00	0.00
61	62	0.00	0.00	0.00	0.00
62	62	0.00	0.00	0.00	0.00
62	63	0.00	0.00	0.00	0.00
63	63	0.00	0.00	0.00	0.00
63	64	0.00	0.00	0.00	0.00
64	64	0.00	0.00	0.00	0.00
64	65	0.00	0.00	0.00	0.00
65	65	0.00	0.00	0.00	0.00
65	66	0.00	0.00	0.00	0.00
66	66	0.00	0.00	0.00	0.00
66	67	0.00	0.00	0.00	0.00
67	67	0.00	0.00	0.00	0.00
67	68	0.00	0.00	0.00	0.00
68	68	0.00	0.00	0.00	0.00
68	69	0.00	0.00	0.00	0.00
69	69	0.00	0.00	0.00	0.00
69	70	0.00	0.00	0.00	0.00
70	70	0.00	0.00	0.00	0.00
70	71	0.00	0.00	0.00	0.00
71	71	0.00	0.00	0.00	0.00
71	72	0.00	0.00	0.00	0.00
72	72	0.00	0.00	0.00	0.00
72	73	0.00	0.00	0.00	0.00
73	73	0.00	0.00	0.00	0.00
73	74	0.00	0.00	0.00	0.00
74	74	0.00	0.00	0.00	0.00
74	75	0.00	0.00	0.00	0.00
75	75	0.00	0.00	0.00	0.00
75	76	0.00	0.00	0.00	0.00
76	76	0.00	0.00	0.00	0.00
76	77	0.00	0.00	0.00	0.00
77	77	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	0.00	0.00	0.00	0.00
78	78	0.00	0.00	0.00	0.00
78	79	0.00	0.00	0.00	0.00
79	79	0.00	0.00	0.00	0.00
79	80	0.00	0.00	0.00	0.00
80	80	0.00	0.00	0.00	0.00
80	81	0.00	0.00	0.00	0.00
101	101	0.00	-497.28	0.00	-569.72
101	102	1.10	-497.28	0.00	-569.72
102	102	1.10	-787.36	0.00	-975.54
102	103	2.20	-787.36	0.00	-975.54
103	103	2.20	-787.36	0.00	-975.54
103	104	3.30	-787.36	0.00	-975.54
104	104	3.30	-994.56	0.00	-1261.27
104	105	4.40	-994.56	0.00	-1261.27
105	105	4.40	-994.56	0.00	-1261.27
105	106	5.50	-994.56	0.00	-1261.27
106	106	5.50	-1201.76	0.00	-1544.93
106	107	6.60	-1201.76	0.00	-1544.93
107	107	6.60	-1201.76	0.00	-1544.93
107	108	7.70	-1201.76	0.00	-1544.93
108	108	7.70	-1201.76	0.00	-1544.93
108	109	8.80	-1201.76	0.00	-1544.93
109	109	8.80	-1201.76	0.00	-1544.93
109	110	9.90	-1201.76	0.00	-1544.93
110	110	9.90	-1201.76	0.00	-1544.93
110	111	11.00	-1201.76	0.00	-1544.93
111	111	11.00	-1201.76	0.00	-1544.93
111	112	12.10	-1201.76	0.00	-1544.93
112	112	12.10	-1201.76	0.00	-1544.93
112	113	13.20	-1201.76	0.00	-1544.93
113	113	13.20	-1201.76	0.00	-1544.93
113	114	14.30	-1201.76	0.00	-1544.93
114	114	14.30	-994.56	0.00	-1261.27
114	115	15.40	-994.56	0.00	-1261.27
115	115	15.40	-994.56	0.00	-1261.27
115	116	16.50	-994.56	0.00	-1261.27
116	116	16.50	-994.56	0.00	-1261.27
116	117	17.60	-994.56	0.00	-1261.68
117	117	17.60	-787.36	0.00	-975.54
117	118	18.70	-787.36	0.00	-975.54
118	118	18.70	-787.36	0.00	-975.54
118	119	19.80	-787.36	0.00	-975.54
119	119	19.80	-497.28	0.00	-569.72
119	120	20.90	-497.28	0.00	-569.72
120	120	20.90	-497.28	0.00	-569.72
120	121	22.00	-497.28	0.00	-569.72
121	1121	22.00	-538.72	0.00	-628.93
121	122	23.40	-538.72	0.00	-628.93
122	122	23.40	-538.72	0.00	-628.93
122	123	24.80	-538.72	0.00	-628.93

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2preEI.FAM1.ISO + [1; 1]ej2preEI.FAM2.ISO + [1; 1]ej2preEI.FAM3.ISO + [1; 1]ej2preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-828.80	0.00	-1031.86
123	124	26.20	-828.80	0.00	-1031.86
124	124	26.20	-828.80	0.00	-1031.86
124	125	27.60	-828.80	0.00	-1031.86
125	125	27.60	-1201.76	0.00	-1538.71
125	126	29.00	-1201.76	0.00	-1538.71
126	126	29.00	-1201.76	0.00	-1538.71
126	127	30.40	-1201.76	0.00	-1538.71
127	127	30.40	-1533.28	0.00	-1982.61
127	128	31.80	-1533.28	0.00	-1982.61
128	128	31.80	-1533.28	0.00	-1982.61
128	129	33.20	-1533.28	0.00	-1982.61
129	129	33.20	-1533.28	0.00	-1982.61
129	130	34.60	-1533.28	0.00	-1982.61
130	130	34.60	-1533.28	0.00	-1982.61
130	131	36.00	-1533.28	0.00	-1982.61
131	131	36.00	-1533.28	0.00	-1982.61
131	132	37.40	-1533.28	0.00	-1982.61
132	132	37.40	-1533.28	0.00	-1982.61
132	133	38.80	-1533.28	0.00	-1982.61
133	133	38.80	-1533.28	0.00	-1982.61
133	134	40.20	-1533.28	0.00	-1982.61
134	134	40.20	-1533.28	0.00	-1982.61
134	135	41.60	-1533.28	0.00	-1982.61
135	135	41.60	-1201.76	0.00	-1538.71
135	136	43.00	-1201.76	0.00	-1538.71
136	136	43.00	-1201.76	0.00	-1538.71
136	137	44.40	-1201.76	0.00	-1538.71
137	137	44.40	-828.80	0.00	-1031.86
137	138	45.80	-828.80	0.00	-1031.86
138	138	45.80	-828.80	0.00	-1031.86
138	139	47.20	-828.80	0.00	-1031.86
139	139	47.20	-538.72	0.00	-628.93
139	140	48.60	-538.72	0.00	-628.93
140	140	48.60	-538.72	0.00	-628.93
140	141	50.00	-538.72	0.00	-628.93
141	1141	50.00	-538.72	0.00	-628.93
141	142	51.40	-538.72	0.00	-628.93
142	142	51.40	-538.72	0.00	-628.93
142	143	52.80	-538.72	0.00	-628.93
143	143	52.80	-828.80	0.00	-1031.86
143	144	54.20	-828.80	0.00	-1031.86
144	144	54.20	-828.80	0.00	-1031.86
144	145	55.60	-828.80	0.00	-1031.86
145	145	55.60	-1201.76	0.00	-1538.71
145	146	57.00	-1201.76	0.00	-1538.71
146	146	57.00	-1201.76	0.00	-1538.71
146	147	58.40	-1201.76	0.00	-1538.71
147	147	58.40	-1533.28	0.00	-1982.61
147	148	59.80	-1533.28	0.00	-1982.61
148	148	59.80	-1533.28	0.00	-1982.61

F4.pret.esf.xls Programa DINTEL PACADAR S.A. 11/09/03
ej2preEI.ISO.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEI.ISO.To

Pretensado Isostático (t=0)

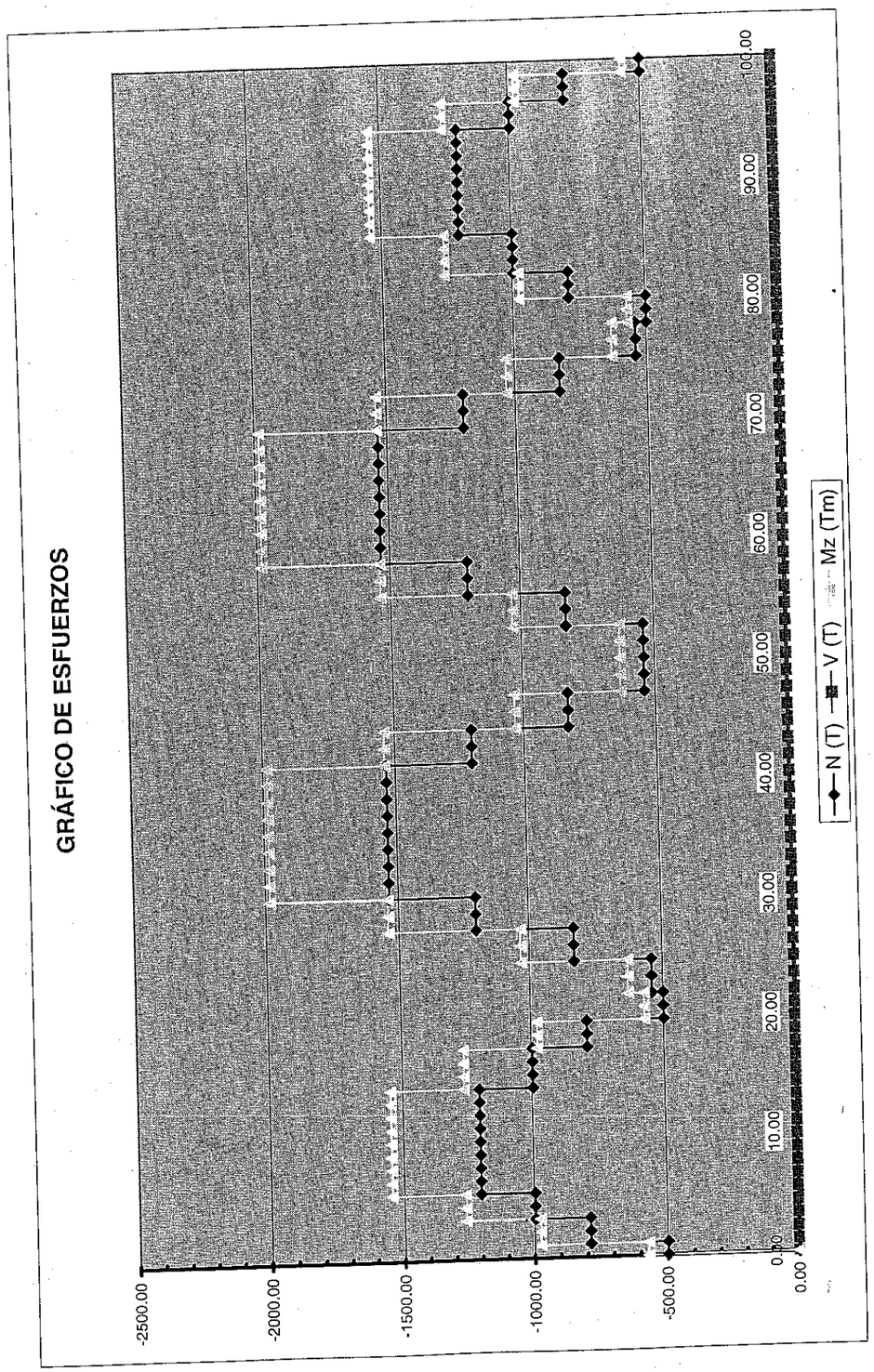
[1; 1]ej2preEI.FAM1.ISO + [1; 1]ej2preEI.FAM2.ISO + [1; 1]ej2preEI.FAM3.ISO + [1; 1]ej2preEI.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-1533.28	0.00	-1982.61
149	149	61.20	-1533.28	0.00	-1982.61
149	150	62.60	-1533.28	0.00	-1982.61
150	150	62.60	-1533.28	0.00	-1982.61
150	151	64.00	-1533.28	0.00	-1982.61
151	151	64.00	-1533.28	0.00	-1982.61
151	152	65.40	-1533.28	0.00	-1982.61
152	152	65.40	-1533.28	0.00	-1982.61
152	153	66.80	-1533.28	0.00	-1982.61
153	153	66.80	-1533.28	0.00	-1982.61
153	154	68.20	-1533.28	0.00	-1982.61
154	154	68.20	-1533.28	0.00	-1982.61
154	155	69.60	-1533.28	0.00	-1982.61
155	155	69.60	-1201.76	0.00	-1538.71
155	156	71.00	-1201.76	0.00	-1538.71
156	156	71.00	-1201.76	0.00	-1538.71
156	157	72.40	-1201.76	0.00	-1538.71
157	157	72.40	-828.80	0.00	-1031.86
157	158	73.80	-828.80	0.00	-1031.86
158	158	73.80	-828.80	0.00	-1031.86
158	159	75.20	-828.80	0.00	-1031.86
159	159	75.20	-538.72	0.00	-628.93
159	160	76.60	-538.72	0.00	-628.93
160	160	76.60	-538.72	0.00	-628.93
160	161	78.00	-538.72	0.00	-628.93
161	1161	78.00	-497.28	0.00	-569.72
161	162	79.10	-497.28	0.00	-569.72
162	162	79.10	-497.28	0.00	-569.72
162	163	80.20	-497.28	0.00	-569.72
163	163	80.20	-787.36	0.00	-975.54
163	164	81.30	-787.36	0.00	-975.54
164	164	81.30	-787.36	0.00	-975.54
164	165	82.40	-787.36	0.00	-975.54
165	165	82.40	-994.56	0.00	-1261.27
165	166	83.50	-994.56	0.00	-1261.27
166	166	83.50	-994.56	0.00	-1261.27
166	167	84.60	-994.56	0.00	-1261.27
167	167	84.60	-994.56	0.00	-1261.27
167	168	85.70	-994.56	0.00	-1261.27
168	168	85.70	-1201.76	0.00	-1544.93
168	169	86.80	-1201.76	0.00	-1544.93
169	169	86.80	-1201.76	0.00	-1544.93
169	170	87.90	-1201.76	0.00	-1544.93
170	170	87.90	-1201.76	0.00	-1544.93
170	171	89.00	-1201.76	0.00	-1544.93
171	171	89.00	-1201.76	0.00	-1544.93
171	172	90.10	-1201.76	0.00	-1544.93
172	172	90.10	-1201.76	0.00	-1544.93
172	173	91.20	-1201.76	0.00	-1544.93
173	173	91.20	-1201.76	0.00	-1544.93
173	174	92.30	-1201.76	0.00	-1544.93

Programa DINTEL PACADAR S.A.
ej2preEl.ISO.To

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ej2preEl.ISO.Tinf

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf
Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	0.00	0.00	0.00	0.00
2	2	0.00	0.00	0.00	0.00
2	3	0.00	0.00	0.00	0.00
3	3	0.00	0.00	0.00	0.00
3	4	0.00	0.00	0.00	0.00
4	4	0.00	0.00	0.00	0.00
4	5	0.00	0.00	0.00	0.00
5	5	0.00	0.00	0.00	0.00
5	6	0.00	0.00	0.00	0.00
6	6	0.00	0.00	0.00	0.00
6	7	0.00	0.00	0.00	0.00
7	7	0.00	0.00	0.00	0.00
7	8	0.00	0.00	0.00	0.00
8	8	0.00	0.00	0.00	0.00
8	9	0.00	0.00	0.00	0.00
9	9	0.00	0.00	0.00	0.00
9	10	0.00	0.00	0.00	0.00
10	10	0.00	0.00	0.00	0.00
10	11	0.00	0.00	0.00	0.00
11	11	0.00	0.00	0.00	0.00
11	12	0.00	0.00	0.00	0.00
12	12	0.00	0.00	0.00	0.00
12	13	0.00	0.00	0.00	0.00
13	13	0.00	0.00	0.00	0.00
13	14	0.00	0.00	0.00	0.00
14	14	0.00	0.00	0.00	0.00
14	15	0.00	0.00	0.00	0.00
15	15	0.00	0.00	0.00	0.00
15	16	0.00	0.00	0.00	0.00
16	16	0.00	0.00	0.00	0.00
16	17	0.00	0.00	0.00	0.00
17	17	0.00	0.00	0.00	0.00
17	18	0.00	0.00	0.00	0.00
18	18	0.00	0.00	0.00	0.00
18	19	0.00	0.00	0.00	0.00
19	19	0.00	0.00	0.00	0.00
19	20	0.00	0.00	0.00	0.00
20	20	0.00	0.00	0.00	0.00
20	21	0.00	0.00	0.00	0.00
21	1021	0.00	0.00	0.00	0.00
21	22	0.00	0.00	0.00	0.00
22	22	0.00	0.00	0.00	0.00
22	23	0.00	0.00	0.00	0.00
23	23	0.00	0.00	0.00	0.00
23	24	0.00	0.00	0.00	0.00
24	24	0.00	0.00	0.00	0.00
24	25	0.00	0.00	0.00	0.00
25	25	0.00	0.00	0.00	0.00
25	26	0.00	0.00	0.00	0.00
26	26	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	0.00	0.00	0.00	0.00
27	27	0.00	0.00	0.00	0.00
27	28	0.00	0.00	0.00	0.00
28	28	0.00	0.00	0.00	0.00
28	29	0.00	0.00	0.00	0.00
29	29	0.00	0.00	0.00	0.00
29	30	0.00	0.00	0.00	0.00
30	30	0.00	0.00	0.00	0.00
30	31	0.00	0.00	0.00	0.00
31	31	0.00	0.00	0.00	0.00
31	32	0.00	0.00	0.00	0.00
32	32	0.00	0.00	0.00	0.00
32	33	0.00	0.00	0.00	0.00
33	33	0.00	0.00	0.00	0.00
33	34	0.00	0.00	0.00	0.00
34	34	0.00	0.00	0.00	0.00
34	35	0.00	0.00	0.00	0.00
35	35	0.00	0.00	0.00	0.00
35	36	0.00	0.00	0.00	0.00
36	36	0.00	0.00	0.00	0.00
36	37	0.00	0.00	0.00	0.00
37	37	0.00	0.00	0.00	0.00
37	38	0.00	0.00	0.00	0.00
38	38	0.00	0.00	0.00	0.00
38	39	0.00	0.00	0.00	0.00
39	39	0.00	0.00	0.00	0.00
39	40	0.00	0.00	0.00	0.00
40	40	0.00	0.00	0.00	0.00
40	41	0.00	0.00	0.00	0.00
41	1041	0.00	0.00	0.00	0.00
41	42	0.00	0.00	0.00	0.00
42	42	0.00	0.00	0.00	0.00
42	43	0.00	0.00	0.00	0.00
43	43	0.00	0.00	0.00	0.00
43	44	0.00	0.00	0.00	0.00
44	44	0.00	0.00	0.00	0.00
44	45	0.00	0.00	0.00	0.00
45	45	0.00	0.00	0.00	0.00
45	46	0.00	0.00	0.00	0.00
46	46	0.00	0.00	0.00	0.00
46	47	0.00	0.00	0.00	0.00
47	47	0.00	0.00	0.00	0.00
47	48	0.00	0.00	0.00	0.00
48	48	0.00	0.00	0.00	0.00
48	49	0.00	0.00	0.00	0.00
49	49	0.00	0.00	0.00	0.00
49	50	0.00	0.00	0.00	0.00
50	50	0.00	0.00	0.00	0.00
50	51	0.00	0.00	0.00	0.00
51	51	0.00	0.00	0.00	0.00
51	52	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	0.00	0.00	0.00	0.00
52	53	0.00	0.00	0.00	0.00
53	53	0.00	0.00	0.00	0.00
53	54	0.00	0.00	0.00	0.00
54	54	0.00	0.00	0.00	0.00
54	55	0.00	0.00	0.00	0.00
55	55	0.00	0.00	0.00	0.00
55	56	0.00	0.00	0.00	0.00
56	56	0.00	0.00	0.00	0.00
56	57	0.00	0.00	0.00	0.00
57	57	0.00	0.00	0.00	0.00
57	58	0.00	0.00	0.00	0.00
58	58	0.00	0.00	0.00	0.00
58	59	0.00	0.00	0.00	0.00
59	59	0.00	0.00	0.00	0.00
59	60	0.00	0.00	0.00	0.00
60	60	0.00	0.00	0.00	0.00
60	61	0.00	0.00	0.00	0.00
61	1061	0.00	0.00	0.00	0.00
61	62	0.00	0.00	0.00	0.00
62	62	0.00	0.00	0.00	0.00
62	63	0.00	0.00	0.00	0.00
63	63	0.00	0.00	0.00	0.00
63	64	0.00	0.00	0.00	0.00
64	64	0.00	0.00	0.00	0.00
64	65	0.00	0.00	0.00	0.00
65	65	0.00	0.00	0.00	0.00
65	66	0.00	0.00	0.00	0.00
66	66	0.00	0.00	0.00	0.00
66	67	0.00	0.00	0.00	0.00
67	67	0.00	0.00	0.00	0.00
67	68	0.00	0.00	0.00	0.00
68	68	0.00	0.00	0.00	0.00
68	69	0.00	0.00	0.00	0.00
69	69	0.00	0.00	0.00	0.00
69	70	0.00	0.00	0.00	0.00
70	70	0.00	0.00	0.00	0.00
70	71	0.00	0.00	0.00	0.00
71	71	0.00	0.00	0.00	0.00
71	72	0.00	0.00	0.00	0.00
72	72	0.00	0.00	0.00	0.00
72	73	0.00	0.00	0.00	0.00
73	73	0.00	0.00	0.00	0.00
73	74	0.00	0.00	0.00	0.00
74	74	0.00	0.00	0.00	0.00
74	75	0.00	0.00	0.00	0.00
75	75	0.00	0.00	0.00	0.00
75	76	0.00	0.00	0.00	0.00
76	76	0.00	0.00	0.00	0.00
76	77	0.00	0.00	0.00	0.00
77	77	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	0.00	0.00	0.00	0.00
78	78	0.00	0.00	0.00	0.00
78	79	0.00	0.00	0.00	0.00
79	79	0.00	0.00	0.00	0.00
79	80	0.00	0.00	0.00	0.00
80	80	0.00	0.00	0.00	0.00
80	81	0.00	0.00	0.00	0.00
101	101	0.00	-497.28	0.00	-569.72
101	102	1.10	-497.28	0.00	-569.72
102	102	1.10	-787.36	0.00	-975.54
102	103	2.20	-787.36	0.00	-975.54
103	103	2.20	-787.36	0.00	-975.54
103	104	3.30	-787.36	0.00	-975.54
104	104	3.30	-994.56	0.00	-1261.27
104	105	4.40	-994.56	0.00	-1261.27
105	105	4.40	-994.56	0.00	-1261.27
105	106	5.50	-994.56	0.00	-1261.27
106	106	5.50	-1201.76	0.00	-1544.93
106	107	6.60	-1201.76	0.00	-1544.93
107	107	6.60	-1201.76	0.00	-1544.93
107	108	7.70	-1201.76	0.00	-1544.93
108	108	7.70	-1201.76	0.00	-1544.93
108	109	8.80	-1201.76	0.00	-1544.93
109	109	8.80	-1201.76	0.00	-1544.93
109	110	9.90	-1201.76	0.00	-1544.93
110	110	9.90	-1201.76	0.00	-1544.93
110	111	11.00	-1201.76	0.00	-1544.93
111	111	11.00	-1201.76	0.00	-1544.93
111	112	12.10	-1201.76	0.00	-1544.93
112	112	12.10	-1201.76	0.00	-1544.93
112	113	13.20	-1201.76	0.00	-1544.93
113	113	13.20	-1201.76	0.00	-1544.93
113	114	14.30	-1201.76	0.00	-1544.93
114	114	14.30	-994.56	0.00	-1261.27
114	115	15.40	-994.56	0.00	-1261.27
115	115	15.40	-994.56	0.00	-1261.27
115	116	16.50	-994.56	0.00	-1261.27
116	116	16.50	-994.56	0.00	-1261.27
116	117	17.60	-994.56	0.00	-1261.68
117	117	17.60	-787.36	0.00	-975.54
117	118	18.70	-787.36	0.00	-975.54
118	118	18.70	-787.36	0.00	-975.54
118	119	19.80	-787.36	0.00	-975.54
119	119	19.80	-497.28	0.00	-569.72
119	120	20.90	-497.28	0.00	-569.72
120	120	20.90	-497.28	0.00	-569.72
120	121	22.00	-497.28	0.00	-569.72
121	1121	22.00	-538.72	0.00	-628.93
121	122	23.40	-538.72	0.00	-628.93
122	122	23.40	-538.72	0.00	-628.93
122	123	24.80	-538.72	0.00	-628.93

F4.pret.esf.xls Programa DINTEL PACADAR S.A. 11/09/03
ej2preEl.ISO.Tinf

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-828.80	0.00	-1031.86
123	124	26.20	-828.80	0.00	-1031.86
124	124	26.20	-828.80	0.00	-1031.86
124	125	27.60	-828.80	0.00	-1031.86
125	125	27.60	-1201.76	0.00	-1538.71
125	126	29.00	-1201.76	0.00	-1538.71
126	126	29.00	-1201.76	0.00	-1538.71
126	127	30.40	-1201.76	0.00	-1538.71
127	127	30.40	-1533.28	0.00	-1982.61
127	128	31.80	-1533.28	0.00	-1982.61
128	128	31.80	-1533.28	0.00	-1982.61
128	129	33.20	-1533.28	0.00	-1982.61
129	129	33.20	-1533.28	0.00	-1982.61
129	130	34.60	-1533.28	0.00	-1982.61
130	130	34.60	-1533.28	0.00	-1982.61
130	131	36.00	-1533.28	0.00	-1982.61
131	131	36.00	-1533.28	0.00	-1982.61
131	132	37.40	-1533.28	0.00	-1982.61
132	132	37.40	-1533.28	0.00	-1982.61
132	133	38.80	-1533.28	0.00	-1982.61
133	133	38.80	-1533.28	0.00	-1982.61
133	134	40.20	-1533.28	0.00	-1982.61
134	134	40.20	-1533.28	0.00	-1982.61
134	135	41.60	-1533.28	0.00	-1982.61
135	135	41.60	-1201.76	0.00	-1538.71
135	136	43.00	-1201.76	0.00	-1538.71
136	136	43.00	-1201.76	0.00	-1538.71
136	137	44.40	-1201.76	0.00	-1538.71
137	137	44.40	-828.80	0.00	-1031.86
137	138	45.80	-828.80	0.00	-1031.86
138	138	45.80	-828.80	0.00	-1031.86
138	139	47.20	-828.80	0.00	-1031.86
139	139	47.20	-538.72	0.00	-628.93
139	140	48.60	-538.72	0.00	-628.93
140	140	48.60	-538.72	0.00	-628.93
140	141	50.00	-538.72	0.00	-628.93
141	1141	50.00	-538.72	0.00	-628.93
141	142	51.40	-538.72	0.00	-628.93
142	142	51.40	-538.72	0.00	-628.93
142	143	52.80	-538.72	0.00	-628.93
143	143	52.80	-828.80	0.00	-1031.86
143	144	54.20	-828.80	0.00	-1031.86
144	144	54.20	-828.80	0.00	-1031.86
144	145	55.60	-828.80	0.00	-1031.86
145	145	55.60	-1201.76	0.00	-1538.71
145	146	57.00	-1201.76	0.00	-1538.71
146	146	57.00	-1201.76	0.00	-1538.71
146	147	58.40	-1201.76	0.00	-1538.71
147	147	58.40	-1533.28	0.00	-1982.61
147	148	59.80	-1533.28	0.00	-1982.61
148	148	59.80	-1533.28	0.00	-1982.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf
Pretensado Isostático (t=INF)

[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-1533.28	0.00	-1982.61
149	149	61.20	-1533.28	0.00	-1982.61
149	150	62.60	-1533.28	0.00	-1982.61
150	150	62.60	-1533.28	0.00	-1982.61
150	151	64.00	-1533.28	0.00	-1982.61
151	151	64.00	-1533.28	0.00	-1982.61
151	152	65.40	-1533.28	0.00	-1982.61
152	152	65.40	-1533.28	0.00	-1982.61
152	153	66.80	-1533.28	0.00	-1982.61
153	153	66.80	-1533.28	0.00	-1982.61
153	154	68.20	-1533.28	0.00	-1982.61
154	154	68.20	-1533.28	0.00	-1982.61
154	155	69.60	-1533.28	0.00	-1982.61
155	155	69.60	-1201.76	0.00	-1538.71
155	156	71.00	-1201.76	0.00	-1538.71
156	156	71.00	-1201.76	0.00	-1538.71
156	157	72.40	-1201.76	0.00	-1538.71
157	157	72.40	-828.80	0.00	-1031.86
156	157	72.40	-1201.76	0.00	-1538.71
157	157	72.40	-828.80	0.00	-1031.86
157	158	73.80	-828.80	0.00	-1031.86
158	158	73.80	-828.80	0.00	-1031.86
158	159	75.20	-828.80	0.00	-1031.86
159	159	75.20	-538.72	0.00	-628.93
159	160	76.60	-538.72	0.00	-628.93
160	160	76.60	-538.72	0.00	-628.93
160	161	78.00	-538.72	0.00	-628.93
161	1161	78.00	-497.28	0.00	-569.72
161	162	79.10	-497.28	0.00	-569.72
162	162	79.10	-497.28	0.00	-569.72
162	163	80.20	-497.28	0.00	-569.72
163	163	80.20	-787.36	0.00	-975.54
163	164	81.30	-787.36	0.00	-975.54
164	164	81.30	-787.36	0.00	-975.54
164	165	82.40	-787.36	0.00	-975.54
165	165	82.40	-994.56	0.00	-1261.27
165	166	83.50	-994.56	0.00	-1261.27
166	166	83.50	-994.56	0.00	-1261.27
166	167	84.60	-994.56	0.00	-1261.27
167	167	84.60	-994.56	0.00	-1261.27
167	168	85.70	-994.56	0.00	-1261.27
168	168	85.70	-1201.76	0.00	-1544.93
168	169	86.80	-1201.76	0.00	-1544.93
169	169	86.80	-1201.76	0.00	-1544.93
169	170	87.90	-1201.76	0.00	-1544.93
170	170	87.90	-1201.76	0.00	-1544.93
170	171	89.00	-1201.76	0.00	-1544.93
171	171	89.00	-1201.76	0.00	-1544.93
171	172	90.10	-1201.76	0.00	-1544.93
172	172	90.10	-1201.76	0.00	-1544.93
172	173	91.20	-1201.76	0.00	-1544.93
173	173	91.20	-1201.76	0.00	-1544.93
173	174	92.30	-1201.76	0.00	-1544.93

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2preEl.ISO.Tinf
Pretensado Isostático (t=INF)

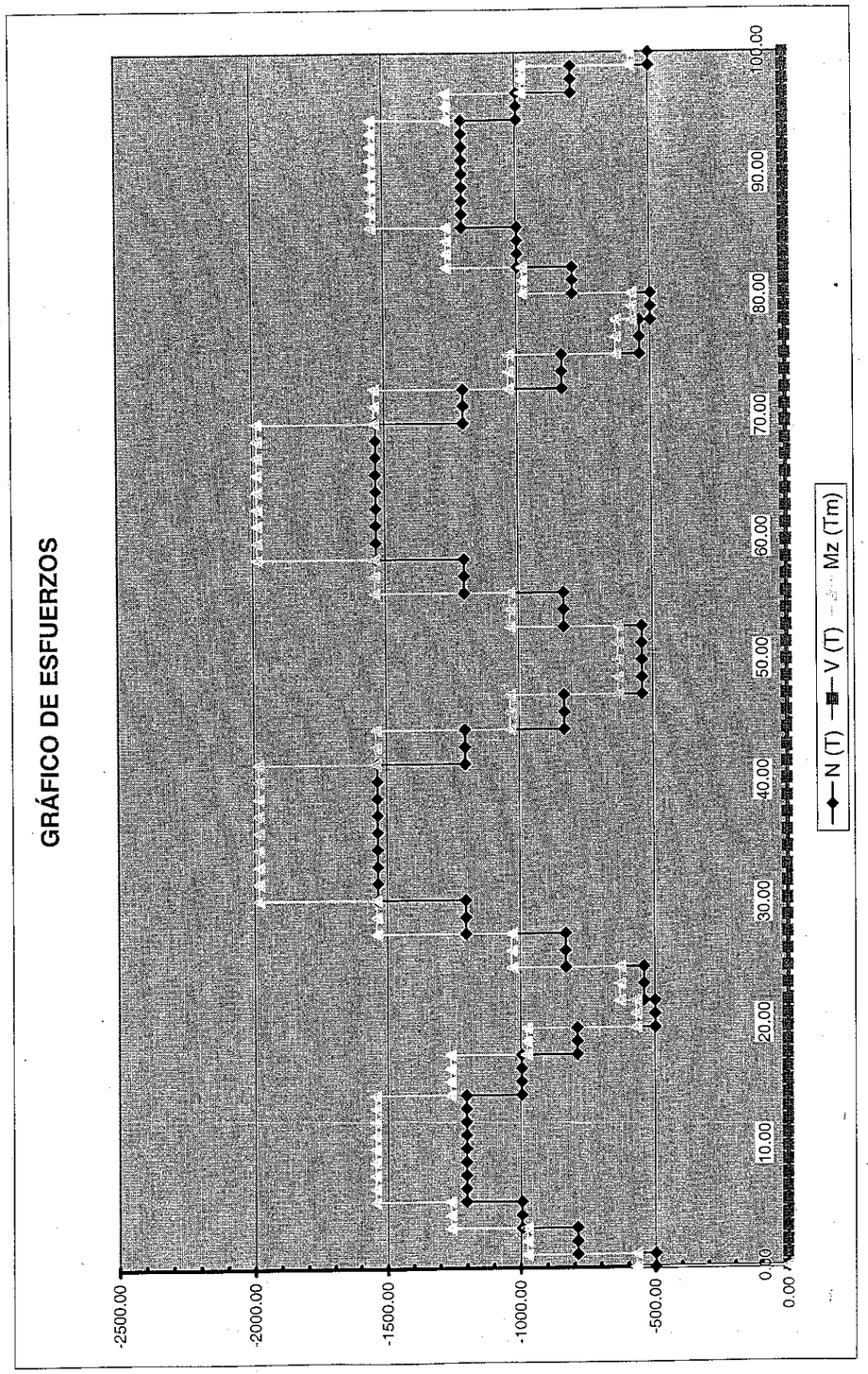
[1; 1]ej2preEl.FAM1.ISO + [1; 1]ej2preEl.FAM2.ISO + [1; 1]ej2preEl.FAM3.ISO + [1; 1]ej2preEl.FAM4

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	-1201.76	0.00	-1544.93
174	175	93.40	-1201.76	0.00	-1544.93
175	175	93.40	-1201.76	0.00	-1544.93
175	176	94.50	-1201.76	0.00	-1544.93
176	176	94.50	-994.56	0.00	-1261.27
176	177	95.60	-994.56	0.00	-1261.27
177	177	95.60	-994.56	0.00	-1261.27
177	178	96.70	-994.56	0.00	-1261.27
178	178	96.70	-787.36	0.00	-975.54
178	179	97.80	-787.36	0.00	-975.54
179	179	97.80	-787.36	0.00	-975.54
179	180	98.90	-787.36	0.00	-975.54
180	180	98.90	-497.28	0.00	-569.72
180	181	100.00	-497.28	0.00	-569.72

Programa DINTEL PACADAR S.A.
ej2preEl.ISO.Tinf

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ej2posEl.TOT.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1; 1]ej2posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-225.60	-1.58	-0.24
1	2	1.10	-225.60	-1.58	1.50
2	2	1.10	-226.45	-0.95	1.01
2	3	2.20	-226.45	-0.95	2.05
3	3	2.20	-227.77	-0.51	1.59
3	4	3.30	-227.77	-0.51	2.15
4	4	3.30	-229.54	-0.25	1.71
4	5	4.40	-229.54	-0.25	1.99
5	5	4.40	-231.75	-0.17	1.60
5	6	5.50	-231.75	-0.17	1.78
6	6	5.50	-234.40	-0.22	1.44
6	7	6.60	-234.40	-0.22	1.68
7	7	6.60	-237.48	-0.40	1.40
7	8	7.70	-237.48	-0.40	1.85
8	8	7.70	-241.01	-0.68	1.63
8	9	8.80	-241.01	-0.68	2.38
9	9	8.80	-244.98	-1.02	2.24
9	10	9.90	-244.98	-1.02	3.36
10	10	9.90	-249.41	-1.39	3.32
10	11	11.00	-249.41	-1.39	4.84
11	11	11.00	-254.31	-1.75	4.90
11	12	12.10	-254.31	-1.75	6.83
12	12	12.10	-259.71	-2.06	7.00
12	13	13.20	-259.71	-2.06	9.27
13	13	13.20	-265.64	-2.27	9.56
13	14	14.30	-265.64	-2.27	12.06
14	14	14.30	-272.13	-2.32	12.50
14	15	15.40	-272.13	-2.32	15.05
15	15	15.40	-279.22	-2.14	15.64
15	16	16.50	-279.22	-2.14	18.00
16	16	16.50	-286.01	-1.71	18.57
16	17	17.60	-286.01	-1.71	20.45
17	17	17.60	-292.54	-1.03	21.00
17	18	18.70	-292.54	-1.03	22.14
18	18	18.70	-297.91	-0.15	22.49
18	19	19.80	-297.91	-0.15	22.65
19	19	19.80	-302.13	0.86	22.81
19	20	20.90	-302.13	0.86	21.86
20	20	20.90	-305.24	1.93	21.83
20	21	22.00	-305.24	1.93	19.71
21	1021	22.00	-308.15	2.97	19.48
21	22	23.40	-308.15	2.97	15.33
22	22	23.40	-309.35	4.17	14.80
22	23	24.80	-309.35	4.17	8.96
23	23	24.80	-307.66	5.09	8.13
23	24	26.20	-307.66	5.09	1.00
24	24	26.20	-303.03	5.58	-0.13
24	25	27.60	-303.03	5.58	-7.94
25	25	27.60	-297.80	5.55	-9.09
25	26	29.00	-297.80	5.55	-16.85
26	26	29.00	-291.80	4.98	-18.02

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1; 1]ej2posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-291.80	4.98	-25.00
27	27	30.40	-287.37	3.96	-25.88
27	28	31.80	-287.37	3.96	-31.43
28	28	31.80	-284.35	2.60	-32.06
28	29	33.20	-284.35	2.60	-35.70
29	29	33.20	-282.66	1.03	-36.10
29	30	34.60	-282.66	1.03	-37.54
30	30	34.60	-282.21	-0.65	-37.70
30	31	36.00	-282.21	-0.65	-36.80
31	31	36.00	-283.01	-2.34	-36.74
31	32	37.40	-283.01	-2.34	-33.47
32	32	37.40	-285.03	-3.93	-33.19
32	33	38.80	-285.03	-3.93	-27.69
33	33	38.80	-288.33	-5.34	-27.19
33	34	40.20	-288.33	-5.34	-19.71
34	34	40.20	-292.98	-6.46	-18.99
34	35	41.60	-292.98	-6.46	-9.95
35	35	41.60	-299.08	-7.18	-9.00
35	36	43.00	-299.08	-7.18	1.05
36	36	43.00	-306.79	-7.37	2.26
36	37	44.40	-306.79	-7.37	12.57
37	37	44.40	-313.81	-6.98	13.71
37	38	45.80	-313.81	-6.98	23.49
38	38	45.80	-320.31	-6.05	24.58
38	39	47.20	-320.31	-6.05	33.04
39	39	47.20	-323.97	-4.67	33.76
39	40	48.60	-323.97	-4.67	40.30
40	40	48.60	-324.86	-3.03	40.66
40	41	50.00	-324.86	-3.03	44.90
41	1041	50.00	-323.00	3.03	44.90
41	42	51.40	-323.00	3.03	40.66
42	42	51.40	-318.38	4.67	40.30
42	43	52.80	-318.38	4.67	33.76
43	43	52.80	-310.98	6.05	33.04
43	44	54.20	-310.98	6.05	24.57
44	44	54.20	-300.72	6.98	23.48
44	45	55.60	-300.72	6.98	13.71
45	45	55.60	-289.90	7.37	12.57
45	46	57.00	-289.90	7.37	2.25
46	46	57.00	-278.33	7.18	1.05
46	47	58.40	-278.33	7.18	-9.00
47	47	58.40	-268.33	6.46	-9.95
47	48	59.80	-268.33	6.46	-19.00
48	48	59.80	-259.69	5.34	-19.72
48	49	61.20	-259.69	5.34	-27.20
49	49	61.20	-252.31	3.93	-27.69
49	50	62.60	-252.31	3.93	-33.20
50	50	62.60	-246.10	2.34	-33.47
50	51	64.00	-246.10	2.34	-36.75
51	51	64.00	-240.98	0.65	-36.80
51	52	65.40	-240.98	0.65	-37.71

F4.pret.esf.xls

Programa DINTEL PACADAR S.A.
ej2posEl.TOT.To

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1; 1]ej2posEl.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-32.88	0.25	1.72
78	78	96.70	-22.35	0.51	2.15
78	79	97.80	-22.35	0.51	1.59
79	79	97.80	-11.83	0.95	2.06
79	80	98.90	-11.83	0.95	1.01
80	80	98.90	-1.32	1.58	1.50
80	81	100.00	-1.32	1.58	-0.24
101	101	0.00	225.60	21.91	0.24
101	102	1.10	225.60	21.91	-23.86
102	102	1.10	226.45	21.27	-23.37
102	103	2.20	226.45	21.27	-46.77
103	103	2.20	227.77	20.84	-46.31
103	104	3.30	227.77	20.84	-69.23
104	104	3.30	229.54	20.58	-68.80
104	105	4.40	229.54	20.58	-91.43
105	105	4.40	231.75	20.49	-91.04
105	106	5.50	231.75	20.49	-113.58
106	106	5.50	234.40	20.55	-113.24
106	107	6.60	234.40	20.55	-135.84
107	107	6.60	237.48	20.73	-135.56
107	108	7.70	237.48	20.73	-158.37
108	108	7.70	241.01	21.01	-158.15
108	109	8.80	241.01	21.01	-181.26
109	109	8.80	244.98	21.35	-181.13
109	110	9.90	244.98	21.35	-204.61
110	110	9.90	249.41	21.72	-204.56
110	111	11.00	249.41	21.72	-228.45
111	111	11.00	254.31	22.08	-228.51
111	112	12.10	254.31	22.08	-252.79
112	112	12.10	259.71	22.39	-252.97
112	113	13.20	259.71	22.39	-277.59
113	113	13.20	265.64	22.60	-277.89
113	114	14.30	265.64	22.60	-302.75
114	114	14.30	272.13	22.64	-303.18
114	115	15.40	272.13	22.64	-328.09
115	115	15.40	-591.02	22.47	89.90
115	116	16.50	-591.02	22.47	65.18
116	116	16.50	-584.23	22.04	64.61
116	117	17.60	-584.23	22.04	40.37
117	117	17.60	-1447.94	21.36	458.40
117	118	18.70	-1447.94	21.36	434.90
118	118	18.70	-1442.58	20.48	434.55
118	119	19.80	-1442.58	20.48	412.03
119	119	19.80	-1438.35	19.46	411.87
119	120	20.90	-1438.35	19.46	390.46
120	120	20.90	-1435.25	18.40	390.49
120	121	22.00	-1435.25	18.40	370.25
121	1121	22.00	-1432.33	-8.74	370.48
121	122	23.40	-1432.33	-8.74	382.72
122	122	23.40	-1431.14	-9.95	383.25
122	123	24.80	-1431.14	-9.95	397.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.TOT.To

Pretensado Total (t=0)

[1; 1]ej2posEI.FAM1.TOT + [1; 1]ej2posEI.FAM2.TOT + [1; 1)ej2posEI.FAM3.TOT + [1; 1]ej2posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-1432.82	-10.87	398.00
123	124	26.20	-1432.82	-10.87	413.21
124	124	26.20	-567.21	-11.35	-4.24
124	125	27.60	-567.21	-11.35	11.65
125	125	27.60	-572.44	-11.32	12.80
125	126	29.00	-572.44	-11.32	28.64
126	126	29.00	291.80	-10.76	-388.77
126	127	30.40	291.80	-10.76	-373.71
127	127	30.40	287.37	-9.73	-372.83
127	128	31.80	287.37	-9.73	-359.21
128	128	31.80	284.35	-8.37	-358.57
128	129	33.20	284.35	-8.37	-346.85
129	129	33.20	282.66	-6.80	-346.46
129	130	34.60	282.66	-6.80	-336.95
130	130	34.60	282.21	-5.11	-336.78
130	131	36.00	282.21	-5.11	-329.62
131	131	36.00	283.01	-3.43	-329.67
131	132	37.40	283.01	-3.43	-324.88
132	132	37.40	285.03	-1.83	-325.15
132	133	38.80	285.03	-1.83	-322.59
133	133	38.80	288.33	-0.42	-323.09
133	134	40.20	288.33	-0.42	-322.51
134	134	40.20	292.98	0.70	-323.23
134	135	41.60	292.98	0.70	-324.21
135	135	41.60	299.08	1.42	-325.16
135	136	43.00	299.08	1.42	-327.15
136	136	43.00	-563.45	1.61	90.23
136	137	44.40	-563.45	1.61	87.97
137	137	44.40	-556.43	1.23	86.83
137	138	45.80	-556.43	1.23	85.12
138	138	45.80	-1420.17	0.29	502.61
138	139	47.20	-1420.17	0.29	502.20
139	139	47.20	-1416.51	-1.09	501.48
139	140	48.60	-1416.51	-1.09	503.00
140	140	48.60	-1415.62	-2.73	502.64
140	141	50.00	-1415.62	-2.73	506.46
141	1141	50.00	-1417.48	2.73	506.46
141	142	51.40	-1417.48	2.73	502.64
142	142	51.40	-1422.10	1.09	503.00
142	143	52.80	-1422.10	1.09	501.48
143	143	52.80	-1429.50	-0.29	502.20
143	144	54.20	-1429.50	-0.29	502.60
144	144	54.20	-569.52	-1.23	85.11
144	145	55.60	-569.52	-1.23	86.82
145	145	55.60	-580.34	-1.61	87.96
145	146	57.00	-580.34	-1.61	90.22
146	146	57.00	278.33	-1.42	-327.16
146	147	58.40	278.33	-1.42	-325.18
147	147	58.40	268.33	-0.70	-324.23
147	148	59.80	268.33	-0.70	-323.24
148	148	59.80	259.69	0.42	-322.52

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.TOT.To

Pretensado Total (t=0)

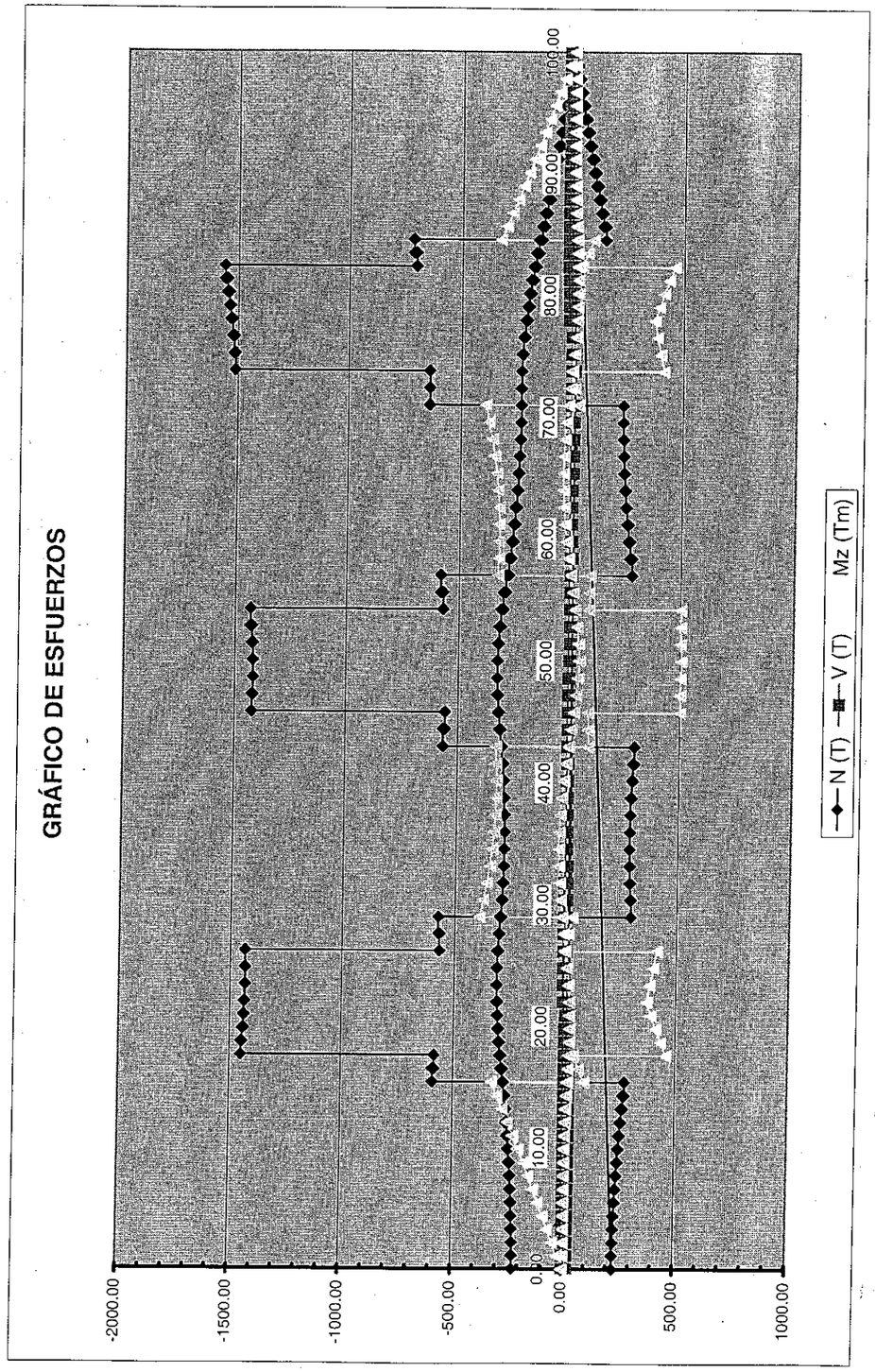
[1; 1]ej2posEI.FAM1.TOT + [1; 1]ej2posEI.FAM2.TOT + [1; 1)ej2posEI.FAM3.TOT + [1; 1]ej2posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	259.69	0.42	-323.11
149	149	61.20	252.31	1.83	-322.61
149	150	62.60	252.31	1.83	-325.17
150	150	62.60	246.10	3.43	-324.89
150	151	64.00	246.10	3.43	-329.69
151	151	64.00	240.98	5.11	-329.64
151	152	65.40	240.98	5.11	-336.80
152	152	65.40	236.94	6.80	-336.96
152	153	66.80	236.94	6.80	-346.48
153	153	66.80	233.96	8.37	-346.87
153	154	68.20	233.96	8.37	-358.59
154	154	68.20	232.09	9.73	-359.22
154	155	69.60	232.09	9.73	-372.84
155	155	69.60	231.35	10.75	-373.73
155	156	71.00	231.35	10.75	-388.78
156	156	71.00	-638.37	11.31	28.63
156	157	72.40	-638.37	11.31	12.79
157	157	72.40	-638.98	11.35	11.65
157	158	73.80	-638.98	11.35	-4.24
158	158	73.80	-1510.86	10.86	413.21
158	159	75.20	-1510.86	10.86	398.00
159	159	75.20	-1515.96	9.94	397.18
159	160	76.60	-1515.96	9.94	383.26
160	160	76.60	-1524.55	8.74	382.73
160	161	78.00	-1524.55	8.74	370.49
161	1161	78.00	-1533.21	-18.40	370.27
161	162	79.10	-1533.21	-18.40	390.50
162	162	79.10	-1540.53	-19.46	390.48
162	163	80.20	-1540.53	-19.46	411.89
163	163	80.20	-1549.23	-20.48	412.04
163	164	81.30	-1549.23	-20.48	434.57
164	164	81.30	-1559.33	-21.36	434.91
164	165	82.40	-1559.33	-21.36	458.41
165	165	82.40	-700.60	-22.04	40.38
165	166	83.50	-700.60	-22.04	64.62
166	166	83.50	-712.63	-22.47	65.19
166	167	84.60	-712.63	-22.47	89.90
167	167	84.60	145.04	-22.64	-328.09
167	168	85.70	145.04	-22.64	-303.18
168	168	85.70	132.83	-22.60	-302.74
168	169	86.80	132.83	-22.60	-277.88
169	169	86.80	120.92	-22.39	-277.59
169	170	87.90	120.92	-22.39	-252.96
170	170	87.90	109.29	-22.08	-252.79
170	171	89.00	109.29	-22.08	-228.50
171	171	89.00	97.90	-21.72	-228.45
171	172	90.10	97.90	-21.72	-204.56
172	172	90.10	86.72	-21.35	-204.60
172	173	91.20	86.72	-21.35	-181.12
173	173	91.20	75.71	-21.01	-181.26
173	174	92.30	75.71	-21.01	-158.15

Programa DINTEL PACADAR S.A.
ej2posEI.TOT.To

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ej2posEI.TOT.Tinf

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [1; 1]ej2posEI.FAM2.TOT + [1; 1]ej2posEI.FAM3.TOT + [1; 1]ej2posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-291.80	4.98	-25.00
27	27	30.40	-287.37	3.96	-25.88
27	28	31.80	-287.37	3.96	-31.43
28	28	31.80	-284.35	2.60	-32.06
28	29	33.20	-284.35	2.60	-35.70
29	29	33.20	-282.66	1.03	-36.10
29	30	34.60	-282.66	1.03	-37.54
30	30	34.60	-282.21	-0.65	-37.70
30	31	36.00	-282.21	-0.65	-36.80
31	31	36.00	-283.01	-2.34	-36.74
31	32	37.40	-283.01	-2.34	-33.47
32	32	37.40	-285.03	-3.93	-33.19
32	33	38.80	-285.03	-3.93	-27.69
33	33	38.80	-288.33	-5.34	-27.19
33	34	40.20	-288.33	-5.34	-19.71
34	34	40.20	-292.98	-6.46	-18.99
34	35	41.60	-292.98	-6.46	-9.95
35	35	41.60	-299.08	-7.18	-9.00
35	36	43.00	-299.08	-7.18	1.05
36	36	43.00	-306.79	-7.37	2.26
36	37	44.40	-306.79	-7.37	12.57
37	37	44.40	-313.81	-6.98	13.71
37	38	45.80	-313.81	-6.98	23.49
38	38	45.80	-320.31	-6.05	24.58
38	39	47.20	-320.31	-6.05	33.04
39	39	47.20	-323.97	-4.67	33.76
39	40	48.60	-323.97	-4.67	40.30
40	40	48.60	-324.86	-3.03	40.66
40	41	50.00	-324.86	-3.03	44.90
41	1041	50.00	-323.00	3.03	44.90
41	42	51.40	-323.00	3.03	40.66
42	42	51.40	-318.38	4.67	40.30
42	43	52.80	-318.38	4.67	33.76
43	43	52.80	-310.98	6.05	33.04
43	44	54.20	-310.98	6.05	24.57
44	44	54.20	-300.72	6.98	23.48
44	45	55.60	-300.72	6.98	13.71
45	45	55.60	-289.90	7.37	12.57
45	46	57.00	-289.90	7.37	2.25
46	46	57.00	-278.33	7.18	1.05
46	47	58.40	-278.33	7.18	-9.00
47	47	58.40	-268.33	6.46	-9.95
47	48	59.80	-268.33	6.46	-19.00
48	48	59.80	-259.69	5.34	-19.72
48	49	61.20	-259.69	5.34	-27.20
49	49	61.20	-252.31	3.93	-27.69
49	50	62.60	-252.31	3.93	-33.20
50	50	62.60	-246.10	2.34	-33.47
50	51	64.00	-246.10	2.34	-36.75
51	51	64.00	-240.98	0.65	-36.80
51	52	65.40	-240.98	0.65	-37.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1; 1]ej2posEl.F/
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-236.94	-1.03	-37.54
52	53	66.80	-236.94	-1.03	-36.10
53	53	66.80	-233.96	-2.60	-35.71
53	54	68.20	-233.96	-2.60	-32.07
54	54	68.20	-232.09	-3.96	-31.43
54	55	69.60	-232.09	-3.96	-25.89
55	55	69.60	-231.35	-4.99	-25.00
55	56	71.00	-231.35	-4.99	-18.02
56	56	71.00	-231.87	-5.55	-16.85
56	57	72.40	-231.87	-5.55	-9.09
57	57	72.40	-231.26	-5.58	-7.95
57	58	73.80	-231.26	-5.58	-0.13
58	58	73.80	-229.62	-5.09	1.00
58	59	75.20	-229.62	-5.09	8.13
59	59	75.20	-224.52	-4.17	8.96
59	60	76.60	-224.52	-4.17	14.80
60	60	76.60	-215.93	-2.97	15.33
60	61	78.00	-215.93	-2.97	19.49
61	1061	78.00	-207.27	-1.93	19.71
61	62	79.10	-207.27	-1.93	21.84
62	62	79.10	-199.95	-0.86	21.86
62	63	80.20	-199.95	-0.86	22.81
63	63	80.20	-191.25	0.15	22.66
63	64	81.30	-191.25	0.15	22.49
64	64	81.30	-181.15	1.03	22.14
64	65	82.40	-181.15	1.03	21.01
65	65	82.40	-169.64	1.71	20.45
65	66	83.50	-169.64	1.71	18.57
66	66	83.50	-157.61	2.14	18.00
66	67	84.60	-157.61	2.14	15.65
67	67	84.60	-145.04	2.32	15.05
67	68	85.70	-145.04	2.32	12.50
68	68	85.70	-132.83	2.27	12.06
68	69	86.80	-132.83	2.27	9.57
69	69	86.80	-120.92	2.06	9.27
69	70	87.90	-120.92	2.06	7.00
70	70	87.90	-109.29	1.75	6.83
70	71	89.00	-109.29	1.75	4.91
71	71	89.00	-97.90	1.39	4.85
71	72	90.10	-97.90	1.39	3.32
72	72	90.10	-86.72	1.02	3.36
72	73	91.20	-86.72	1.02	2.24
73	73	91.20	-75.71	0.68	2.38
73	74	92.30	-75.71	0.68	1.63
74	74	92.30	-64.85	0.40	1.85
74	75	93.40	-64.85	0.40	1.40
75	75	93.40	-54.11	0.22	1.69
75	76	94.50	-54.11	0.22	1.44
76	76	94.50	-43.46	0.17	1.78
76	77	95.60	-43.46	0.17	1.60
77	77	95.60	-32.88	0.25	2.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1; 1]ej2posEl.F/
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-32.88	0.25	1.72
78	78	96.70	-22.35	0.51	2.15
78	79	97.80	-22.35	0.51	1.59
79	79	97.80	-11.83	0.95	2.06
79	80	98.90	-11.83	0.95	1.01
80	80	98.90	-1.32	1.58	1.50
80	81	100.00	-1.32	1.58	-0.24
101	101	0.00	225.60	21.91	0.24
101	102	1.10	225.60	21.91	-23.86
102	102	1.10	226.45	21.27	-23.37
102	103	2.20	226.45	21.27	-46.77
103	103	2.20	227.77	20.84	-46.31
103	104	3.30	227.77	20.84	-69.23
104	104	3.30	229.54	20.58	-68.80
104	105	4.40	229.54	20.58	-91.43
105	105	4.40	231.75	20.49	-91.04
105	106	5.50	231.75	20.49	-113.58
106	106	5.50	234.40	20.55	-113.24
106	107	6.60	234.40	20.55	-135.84
107	107	6.60	237.48	20.73	-135.56
107	108	7.70	237.48	20.73	-158.37
108	108	7.70	241.01	21.01	-158.15
108	109	8.80	241.01	21.01	-181.26
109	109	8.80	244.98	21.35	-181.13
109	110	9.90	244.98	21.35	-204.61
110	110	9.90	249.41	21.72	-204.56
110	111	11.00	249.41	21.72	-228.45
111	111	11.00	254.31	22.08	-228.51
111	112	12.10	254.31	22.08	-252.79
112	112	12.10	259.71	22.39	-252.97
112	113	13.20	259.71	22.39	-277.59
113	113	13.20	265.64	22.60	-277.89
113	114	14.30	265.64	22.60	-302.75
114	114	14.30	272.13	22.64	-303.18
114	115	15.40	272.13	22.64	-328.09
115	115	15.40	-591.02	22.47	89.90
115	116	16.50	-591.02	22.47	65.18
116	116	16.50	-584.23	22.04	64.61
116	117	17.60	-584.23	22.04	40.37
117	117	17.60	-1447.94	21.36	458.40
117	118	18.70	-1447.94	21.36	434.90
118	118	18.70	-1442.58	20.48	434.55
118	119	19.80	-1442.58	20.48	412.03
119	119	19.80	-1438.35	19.46	411.87
119	120	20.90	-1438.35	19.46	390.46
120	120	20.90	-1435.25	18.40	390.49
120	121	22.00	-1435.25	18.40	370.25
121	1121	22.00	-1432.33	-8.74	370.48
121	122	23.40	-1432.33	-8.74	382.72
122	122	23.40	-1431.14	-9.95	383.25
122	123	24.80	-1431.14	-9.95	397.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [1; 1]ej2posEI.FAM2.TOT + [1; 1]ej2posEI.FAM3.TOT + [1; 1]ej2posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-1432.82	-10.87	398.00
123	124	26.20	-1432.82	-10.87	413.21
124	124	26.20	-567.21	-11.35	-4.24
124	125	27.60	-567.21	-11.35	11.65
125	125	27.60	-572.44	-11.32	12.80
125	126	29.00	-572.44	-11.32	28.64
126	126	29.00	291.80	-10.76	-388.77
126	127	30.40	291.80	-10.76	-373.71
127	127	30.40	287.37	-9.73	-372.83
127	128	31.80	287.37	-9.73	-359.21
128	128	31.80	284.35	-8.37	-358.57
128	129	33.20	284.35	-8.37	-346.85
129	129	33.20	282.66	-6.80	-346.46
129	130	34.60	282.66	-6.80	-336.95
130	130	34.60	282.21	-5.11	-336.78
130	131	36.00	282.21	-5.11	-329.62
131	131	36.00	283.01	-3.43	-329.67
131	132	37.40	283.01	-3.43	-324.88
132	132	37.40	285.03	-1.83	-325.15
132	133	38.80	285.03	-1.83	-322.59
133	133	38.80	288.33	-0.42	-323.09
133	134	40.20	288.33	-0.42	-322.51
134	134	40.20	292.98	0.70	-323.23
134	135	41.60	292.98	0.70	-324.21
135	135	41.60	299.08	1.42	-325.16
135	136	43.00	299.08	1.42	-327.15
136	136	43.00	-563.45	1.61	90.23
136	137	44.40	-563.45	1.61	87.97
137	137	44.40	-556.43	1.23	86.83
137	138	45.80	-556.43	1.23	85.12
138	138	45.80	-1420.17	0.29	502.61
138	139	47.20	-1420.17	0.29	502.20
139	139	47.20	-1416.51	-1.09	501.48
139	140	48.60	-1416.51	-1.09	503.00
140	140	48.60	-1415.62	-2.73	502.64
140	141	50.00	-1415.62	-2.73	506.46
141	1141	50.00	-1417.48	2.73	506.46
141	142	51.40	-1417.48	2.73	502.64
142	142	51.40	-1422.10	1.09	503.00
142	143	52.80	-1422.10	1.09	501.48
143	143	52.80	-1429.50	-0.29	502.20
143	144	54.20	-1429.50	-0.29	502.60
144	144	54.20	-569.52	-1.23	85.11
144	145	55.60	-569.52	-1.23	86.82
145	145	55.60	-580.34	-1.61	87.96
145	146	57.00	-580.34	-1.61	90.22
146	146	57.00	278.33	-1.42	-327.16
146	147	58.40	278.33	-1.42	-325.18
147	147	58.40	268.33	-0.70	-324.23
147	148	59.80	268.33	-0.70	-323.24
148	148	59.80	259.69	0.42	-322.52

CÁLCULO TENSIONAL

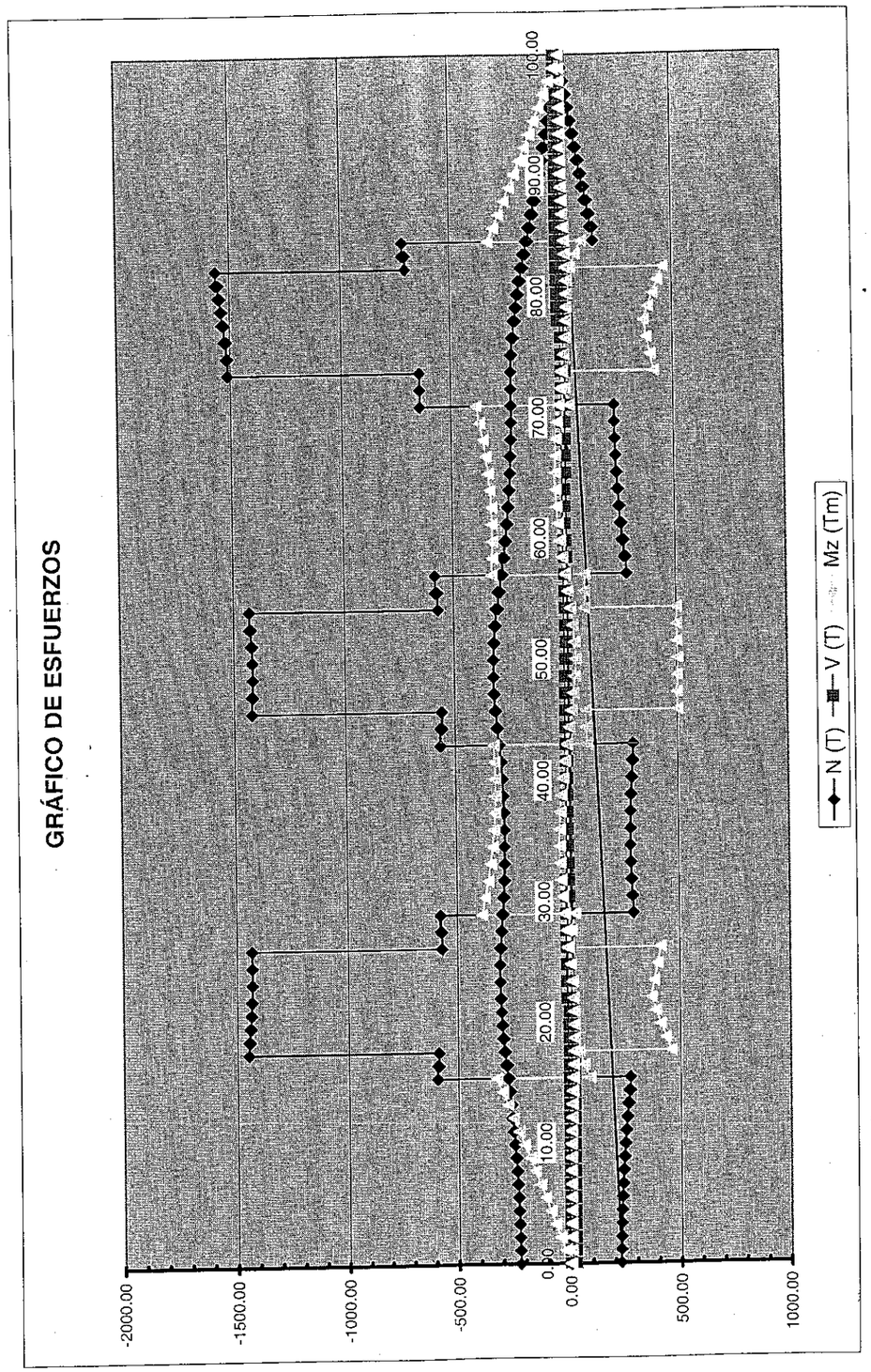
Hipótesis de cálculo:
ej2posEI.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [1; 1]ej2posEI.FAM2.TOT + [1; 1]ej2posEI.FAM3.TOT + [1; 1]ej2posEI.F/

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	64.85	-20.73	-158.37
174	175	93.40	64.85	-20.73	-135.56
175	175	93.40	54.11	-20.55	-135.84
175	176	94.50	54.11	-20.55	-113.24
176	176	94.50	43.46	-20.49	-113.58
176	177	95.60	43.46	-20.49	-91.04
177	177	95.60	32.88	-20.58	-91.43
177	178	96.70	32.88	-20.58	-68.79
178	178	96.70	22.35	-20.84	-69.23
178	179	97.80	22.35	-20.84	-46.31
179	179	97.80	11.83	-21.27	-46.77
179	180	98.90	11.83	-21.27	-23.37
180	180	98.90	1.32	-21.91	-23.86
180	181	100.00	1.32	-21.91	0.24



Programa DINTEL PACADAR S.A.
ej2posEI.HIP.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-291.80	4.98	-25.00
27	27	30.40	-287.37	3.96	-25.88
27	28	31.80	-287.37	3.96	-31.43
28	28	31.80	-284.35	2.60	-32.06
28	29	33.20	-284.35	2.60	-35.70
29	29	33.20	-282.66	1.03	-36.10
29	30	34.60	-282.66	1.03	-37.54
30	30	34.60	-282.21	-0.65	-37.70
30	31	36.00	-282.21	-0.65	-36.80
31	31	36.00	-283.01	-2.34	-36.74
31	32	37.40	-283.01	-2.34	-33.47
32	32	37.40	-285.03	-3.93	-33.19
32	33	38.80	-285.03	-3.93	-27.69
33	33	38.80	-288.33	-5.34	-27.19
33	34	40.20	-288.33	-5.34	-19.71
34	34	40.20	-292.98	-6.46	-18.99
34	35	41.60	-292.98	-6.46	-9.95
35	35	41.60	-299.08	-7.18	-9.00
35	36	43.00	-299.08	-7.18	1.05
36	36	43.00	-306.79	-7.37	2.26
36	37	44.40	-306.79	-7.37	12.57
37	37	44.40	-313.81	-6.98	13.71
37	38	45.80	-313.81	-6.98	23.49
38	38	45.80	-320.31	-6.05	24.58
38	39	47.20	-320.31	-6.05	33.04
39	39	47.20	-323.97	-4.67	33.76
39	40	48.60	-323.97	-4.67	40.30
40	40	48.60	-324.86	-3.03	40.66
40	41	50.00	-324.86	-3.03	44.90
41	1041	50.00	-323.00	3.03	44.90
41	42	51.40	-323.00	3.03	40.66
42	42	51.40	-318.38	4.67	40.30
42	43	52.80	-318.38	4.67	33.76
43	43	52.80	-310.98	6.05	33.04
43	44	54.20	-310.98	6.05	24.57
44	44	54.20	-300.72	6.98	23.48
44	45	55.60	-300.72	6.98	13.71
45	45	55.60	-289.90	7.37	12.57
45	46	57.00	-289.90	7.37	2.25
46	46	57.00	-278.33	7.18	1.05
46	47	58.40	-278.33	7.18	-9.00
47	47	58.40	-268.33	6.46	-9.95
47	48	59.80	-268.33	6.46	-19.00
48	48	59.80	-259.69	5.34	-19.72
48	49	61.20	-259.69	5.34	-27.20
49	49	61.20	-252.31	3.93	-27.69
49	50	62.60	-252.31	3.93	-33.20
50	50	62.60	-246.10	2.34	-33.47
50	51	64.00	-246.10	2.34	-36.75
51	51	64.00	-240.98	0.65	-36.80
51	52	65.40	-240.98	0.65	-37.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-236.94	-1.03	-37.54
52	53	66.80	-236.94	-1.03	-36.10
53	53	66.80	-233.96	-2.60	-35.71
53	54	68.20	-233.96	-2.60	-32.07
54	54	68.20	-232.09	-3.96	-31.43
54	55	69.60	-232.09	-3.96	-25.89
55	55	69.60	-231.35	-4.99	-25.00
55	56	71.00	-231.35	-4.99	-18.02
56	56	71.00	-231.87	-5.55	-16.85
56	57	72.40	-231.87	-5.55	-9.09
57	57	72.40	-231.26	-5.58	-7.95
57	58	73.80	-231.26	-5.58	-0.13
58	58	73.80	-229.62	-5.09	1.00
58	59	75.20	-229.62	-5.09	8.13
59	59	75.20	-224.52	-4.17	8.96
59	60	76.60	-224.52	-4.17	14.80
60	60	76.60	-215.93	-2.97	15.33
60	61	78.00	-215.93	-2.97	19.49
61	1061	78.00	-207.27	-1.93	19.71
61	62	79.10	-207.27	-1.93	21.84
62	62	79.10	-199.95	-0.86	21.86
62	63	80.20	-199.95	-0.86	22.81
63	63	80.20	-191.25	0.15	22.66
63	64	81.30	-191.25	0.15	22.49
64	64	81.30	-181.15	1.03	22.14
64	65	82.40	-181.15	1.03	21.01
65	65	82.40	-169.64	1.71	20.45
65	66	83.50	-169.64	1.71	18.57
66	66	83.50	-157.61	2.14	18.00
66	67	84.60	-157.61	2.14	15.65
67	67	84.60	-145.04	2.32	15.05
67	68	85.70	-145.04	2.32	12.50
68	68	85.70	-132.83	2.27	12.06
68	69	86.80	-132.83	2.27	9.57
69	69	86.80	-120.92	2.06	9.27
69	70	87.90	-120.92	2.06	7.00
70	70	87.90	-109.29	1.75	6.83
70	71	89.00	-109.29	1.75	4.91
71	71	89.00	-97.90	1.39	4.85
71	72	90.10	-97.90	1.39	3.32
72	72	90.10	-86.72	1.02	3.36
72	73	91.20	-86.72	1.02	2.24
73	73	91.20	-75.71	0.68	2.38
73	74	92.30	-75.71	0.68	1.63
74	74	92.30	-64.85	0.40	1.85
74	75	93.40	-64.85	0.40	1.40
75	75	93.40	-54.11	0.22	1.69
75	76	94.50	-54.11	0.22	1.44
76	76	94.50	-43.46	0.17	1.78
76	77	95.60	-43.46	0.17	1.60
77	77	95.60	-32.88	0.25	2.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-32.88	0.25	1.72
78	78	96.70	-22.35	0.51	2.15
78	79	97.80	-22.35	0.51	1.59
79	79	97.80	-11.83	0.95	2.06
79	80	98.90	-11.83	0.95	1.01
80	80	98.90	-1.32	1.58	1.50
80	81	100.00	-1.32	1.58	-0.24
101	101	0.00	225.60	21.91	0.24
101	102	1.10	225.60	21.91	-23.86
102	102	1.10	226.45	21.27	-23.37
102	103	2.20	226.45	21.27	-46.77
103	103	2.20	227.77	20.84	-46.31
103	104	3.30	227.77	20.84	-69.23
104	104	3.30	229.54	20.58	-68.80
104	105	4.40	229.54	20.58	-91.43
105	105	4.40	231.75	20.49	-91.04
105	106	5.50	231.75	20.49	-113.58
106	106	5.50	234.40	20.55	-113.24
106	107	6.60	234.40	20.55	-135.84
107	107	6.60	237.48	20.73	-135.56
107	108	7.70	237.48	20.73	-158.37
108	108	7.70	241.01	21.01	-158.15
108	109	8.80	241.01	21.01	-181.26
109	109	8.80	244.98	21.35	-181.13
109	110	9.90	244.98	21.35	-204.61
110	110	9.90	249.41	21.72	-204.56
110	111	11.00	249.41	21.72	-228.45
111	111	11.00	254.31	22.08	-228.51
111	112	12.10	254.31	22.08	-252.79
112	112	12.10	259.71	22.39	-252.97
112	113	13.20	259.71	22.39	-277.59
113	113	13.20	265.64	22.60	-277.89
113	114	14.30	265.64	22.60	-302.75
114	114	14.30	272.13	22.64	-303.18
114	115	15.40	272.13	22.64	-328.09
115	115	15.40	279.22	22.47	-328.69
115	116	16.50	279.22	22.47	-353.41
116	116	16.50	286.01	22.04	-353.97
116	117	17.60	286.01	22.04	-378.22
117	117	17.60	292.54	21.36	-378.77
117	118	18.70	292.54	21.36	-402.27
118	118	18.70	297.91	20.48	-402.62
118	119	19.80	297.91	20.48	-425.14
119	119	19.80	302.13	19.46	-425.30
119	120	20.90	302.13	19.46	-446.71
120	120	20.90	305.24	18.40	-446.68
120	121	22.00	305.24	18.40	-466.92
121	1121	22.00	308.15	-8.74	-466.69
121	122	23.40	308.15	-8.74	-454.45
122	122	23.40	309.35	-9.95	-453.92
122	123	24.80	309.35	-9.95	-440.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	307.66	-10.87	-439.17
123	124	26.20	307.66	-10.87	-423.96
124	124	26.20	303.03	-11.35	-422.82
124	125	27.60	303.03	-11.35	-406.93
125	125	27.60	297.80	-11.32	-405.79
125	126	29.00	297.80	-11.32	-389.94
126	126	29.00	291.80	-10.76	-388.77
126	127	30.40	291.80	-10.76	-373.71
127	127	30.40	287.37	-9.73	-372.83
127	128	31.80	287.37	-9.73	-359.21
128	128	31.80	284.35	-8.37	-358.57
128	129	33.20	284.35	-8.37	-346.85
129	129	33.20	282.66	-6.80	-346.46
129	130	34.60	282.66	-6.80	-336.95
130	130	34.60	282.21	-5.11	-336.78
130	131	36.00	282.21	-5.11	-329.62
131	131	36.00	283.01	-3.43	-329.67
131	132	37.40	283.01	-3.43	-324.88
132	132	37.40	285.03	-1.83	-325.15
132	133	38.80	285.03	-1.83	-322.59
133	133	38.80	288.33	-0.42	-323.09
133	134	40.20	288.33	-0.42	-322.51
134	134	40.20	292.98	0.70	-323.23
134	135	41.60	292.98	0.70	-324.21
135	135	41.60	299.08	1.42	-325.16
135	136	43.00	299.08	1.42	-327.15
136	136	43.00	306.79	1.61	-328.35
136	137	44.40	306.79	1.61	-330.61
137	137	44.40	313.82	1.23	-331.75
137	138	45.80	313.82	1.23	-333.47
138	138	45.80	320.31	0.29	-334.56
138	139	47.20	320.31	0.29	-334.97
139	139	47.20	323.97	-1.09	-335.69
139	140	48.60	323.97	-1.09	-334.17
140	140	48.60	324.86	-2.73	-334.53
140	141	50.00	324.86	-2.73	-330.71
141	1141	50.00	323.00	2.73	-330.71
141	142	51.40	323.00	2.73	-334.53
142	142	51.40	318.38	1.09	-334.17
142	143	52.80	318.38	1.09	-335.70
143	143	52.80	310.98	-0.29	-334.98
143	144	54.20	310.98	-0.29	-334.57
144	144	54.20	300.72	-1.23	-333.48
144	145	55.60	300.72	-1.23	-331.76
145	145	55.60	289.90	-1.61	-330.62
145	146	57.00	289.90	-1.61	-328.37
146	146	57.00	278.33	-1.42	-327.16
146	147	58.40	278.33	-1.42	-325.18
147	147	58.40	268.33	-0.70	-324.23
147	148	59.80	268.33	-0.70	-323.24
148	148	59.80	259.69	0.42	-322.52

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	259.69	0.42	-323.11
149	149	61.20	252.31	1.83	-322.61
149	150	62.60	252.31	1.83	-325.17
150	150	62.60	246.10	3.43	-324.89
150	151	64.00	246.10	3.43	-329.69
151	151	64.00	240.98	5.11	-329.64
151	152	65.40	240.98	5.11	-336.80
152	152	65.40	236.94	6.80	-336.96
152	153	66.80	236.94	6.80	-346.48
153	153	66.80	233.96	8.37	-346.87
153	154	68.20	233.96	8.37	-358.59
154	154	68.20	232.09	9.73	-359.22
154	155	69.60	232.09	9.73	-372.84
155	155	69.60	231.35	10.75	-373.73
155	156	71.00	231.35	10.75	-388.78
156	156	71.00	231.87	11.31	-389.95
156	157	72.40	231.87	11.31	-405.79
157	157	72.40	231.26	11.35	-406.94
157	158	73.80	231.26	11.35	-422.82
158	158	73.80	229.62	10.86	-423.96
158	159	75.20	229.62	10.86	-439.17
159	159	75.20	224.52	9.94	-439.99
159	160	76.60	224.52	9.94	-453.91
160	160	76.60	215.93	8.74	-454.44
160	161	78.00	215.93	8.74	-466.68
161	1161	78.00	207.27	-18.40	-466.90
161	162	79.10	207.27	-18.40	-446.67
162	162	79.10	199.96	-19.46	-446.69
162	163	80.20	199.96	-19.46	-425.28
163	163	80.20	191.25	-20.48	-425.13
163	164	81.30	191.25	-20.48	-402.60
164	164	81.30	181.15	-21.36	-402.26
164	165	82.40	181.15	-21.36	-378.76
165	165	82.40	169.64	-22.04	-378.21
165	166	83.50	169.64	-22.04	-353.97
166	166	83.50	157.61	-22.47	-353.40
166	167	84.60	157.61	-22.47	-328.68
167	167	84.60	145.04	-22.64	-328.09
167	168	85.70	145.04	-22.64	-303.18
168	168	85.70	132.83	-22.60	-302.74
168	169	86.80	132.83	-22.60	-277.88
169	169	86.80	120.92	-22.39	-277.59
169	170	87.90	120.92	-22.39	-252.96
170	170	87.90	109.29	-22.08	-252.79
170	171	89.00	109.29	-22.08	-228.50
171	171	89.00	97.90	-21.72	-228.45
171	172	90.10	97.90	-21.72	-204.56
172	172	90.10	86.72	-21.35	-204.60
172	173	91.20	86.72	-21.35	-181.12
173	173	91.20	75.71	-21.01	-181.26
173	174	92.30	75.71	-21.01	-158.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.HIP.To

Pretensado Hiperestático (t=0)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

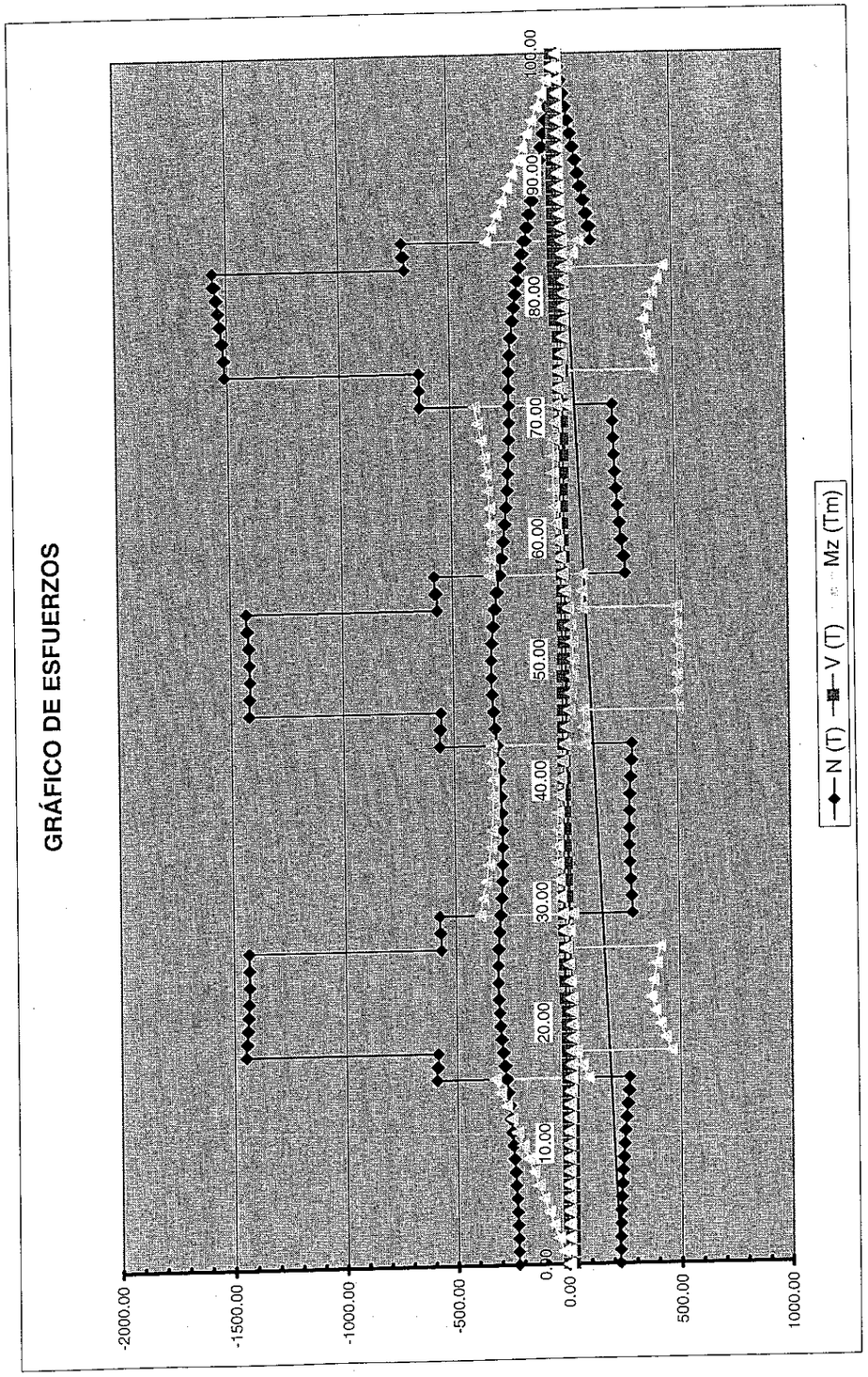
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	64.85	-20.73	-158.37
174	175	93.40	64.85	-20.73	-135.56
175	175	93.40	54.11	-20.55	-135.84
175	176	94.50	54.11	-20.55	-113.24
176	176	94.50	43.46	-20.49	-113.58
176	177	95.60	43.46	-20.49	-91.04
177	177	95.60	32.88	-20.58	-91.43
177	178	96.70	32.88	-20.58	-68.79
178	178	96.70	22.35	-20.84	-69.23
178	179	97.80	22.35	-20.84	-46.31
179	179	97.80	11.83	-21.27	-46.77
179	180	98.90	11.83	-21.27	-23.37
180	180	98.90	1.32	-21.91	-23.86
180	181	100.00	1.32	-21.91	0.24

11/09/03

Programa DINTEL PACADAR S.A.
ej2posEI.TOT.Tinf

GRÁFICO DE ESFUERZOS



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CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.Tinf
Pretensado Hiperestático (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	-225.60	-1.58	-0.24
1	2	1.10	-225.60	-1.58	1.50
2	2	1.10	-226.45	-0.95	1.01
2	3	2.20	-226.45	-0.95	2.05
3	3	2.20	-227.77	-0.51	1.59
3	4	3.30	-227.77	-0.51	2.15
4	4	3.30	-229.54	-0.25	1.71
4	5	4.40	-229.54	-0.25	1.99
5	5	4.40	-231.75	-0.17	1.60
5	6	5.50	-231.75	-0.17	1.78
6	6	5.50	-234.40	-0.22	1.44
6	7	6.60	-234.40	-0.22	1.68
7	7	6.60	-237.48	-0.40	1.40
7	8	7.70	-237.48	-0.40	1.85
8	8	7.70	-241.01	-0.68	1.63
8	9	8.80	-241.01	-0.68	2.38
9	9	8.80	-244.98	-1.02	2.24
9	10	9.90	-244.98	-1.02	3.36
10	10	9.90	-249.41	-1.39	3.32
10	11	11.00	-249.41	-1.39	4.84
11	11	11.00	-254.31	-1.75	4.90
11	12	12.10	-254.31	-1.75	6.83
12	12	12.10	-259.71	-2.06	7.00
12	13	13.20	-259.71	-2.06	9.27
13	13	13.20	-265.64	-2.27	9.56
13	14	14.30	-265.64	-2.27	12.06
14	14	14.30	-272.13	-2.32	12.50
14	15	15.40	-272.13	-2.32	15.05
15	15	15.40	-279.22	-2.14	15.64
15	16	16.50	-279.22	-2.14	18.00
16	16	16.50	-286.01	-1.71	18.57
16	17	17.60	-286.01	-1.71	20.45
17	17	17.60	-292.54	-1.03	21.00
17	18	18.70	-292.54	-1.03	22.14
18	18	18.70	-297.91	-0.15	22.49
18	19	19.80	-297.91	-0.15	22.65
19	19	19.80	-302.13	0.86	22.81
19	20	20.90	-302.13	0.86	21.86
20	20	20.90	-305.24	1.93	21.83
20	21	22.00	-305.24	1.93	19.71
21	1021	22.00	-308.15	2.97	19.48
21	22	23.40	-308.15	2.97	15.33
22	22	23.40	-309.35	4.17	14.80
22	23	24.80	-309.35	4.17	8.96
23	23	24.80	-307.66	5.09	8.13
23	24	26.20	-307.66	5.09	1.00
24	24	26.20	-303.03	5.58	-0.13
24	25	27.60	-303.03	5.58	-7.94
25	25	27.60	-297.80	5.55	-9.09
25	26	29.00	-297.80	5.55	-16.85
26	26	29.00	-291.80	4.98	-18.02

F4.pret.esf.xls
Programa DINTEL PACADAR S.A.
ej2posEI.HIP.Tinf
11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.HIP.Tinf
Pretensado Hiperestático (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	-291.80	4.98	-25.00
27	27	30.40	-287.37	3.96	-25.88
27	28	31.80	-287.37	3.96	-31.43
28	28	31.80	-284.35	2.60	-32.06
28	29	33.20	-284.35	2.60	-35.70
29	29	33.20	-282.66	1.03	-36.10
29	30	34.60	-282.66	1.03	-37.54
30	30	34.60	-282.21	-0.65	-37.70
30	31	36.00	-282.21	-0.65	-36.80
31	31	36.00	-283.01	-2.34	-36.74
31	32	37.40	-283.01	-2.34	-33.47
32	32	37.40	-285.03	-3.93	-33.19
32	33	38.80	-285.03	-3.93	-27.69
33	33	38.80	-288.33	-5.34	-27.19
33	34	40.20	-288.33	-5.34	-19.71
34	34	40.20	-292.98	-6.46	-18.99
34	35	41.60	-292.98	-6.46	-9.95
35	35	41.60	-299.08	-7.18	-9.00
35	36	43.00	-299.08	-7.18	1.05
36	36	43.00	-306.79	-7.37	2.26
36	37	44.40	-306.79	-7.37	12.57
37	37	44.40	-313.81	-6.98	13.71
37	38	45.80	-313.81	-6.98	23.49
38	38	45.80	-320.31	-6.05	24.58
38	39	47.20	-320.31	-6.05	33.04
39	39	47.20	-323.97	-4.67	33.76
39	40	48.60	-323.97	-4.67	40.30
40	40	48.60	-324.86	-3.03	40.66
40	41	50.00	-324.86	-3.03	44.90
41	1041	50.00	-323.00	3.03	44.90
41	42	51.40	-323.00	3.03	40.66
42	42	51.40	-318.38	4.67	40.30
42	43	52.80	-318.38	4.67	33.76
43	43	52.80	-310.98	6.05	33.04
43	44	54.20	-310.98	6.05	24.57
44	44	54.20	-300.72	6.98	23.48
44	45	55.60	-300.72	6.98	13.71
45	45	55.60	-289.90	7.37	12.57
45	46	57.00	-289.90	7.37	2.25
46	46	57.00	-278.33	7.18	1.05
46	47	58.40	-278.33	7.18	-9.00
47	47	58.40	-268.33	6.46	-9.95
47	48	59.80	-268.33	6.46	-19.00
48	48	59.80	-259.69	5.34	-19.72
48	49	61.20	-259.69	5.34	-27.20
49	49	61.20	-252.31	3.93	-27.69
49	50	62.60	-252.31	3.93	-33.20
50	50	62.60	-246.10	2.34	-33.47
50	51	64.00	-246.10	2.34	-36.75
51	51	64.00	-240.98	0.65	-36.80
51	52	65.40	-240.98	0.65	-37.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	-236.94	-1.03	-37.54
52	53	66.80	-236.94	-1.03	-36.10
53	53	66.80	-233.96	-2.60	-35.71
53	54	68.20	-233.96	-2.60	-32.07
54	54	68.20	-232.09	-3.96	-31.43
54	55	69.60	-232.09	-3.96	-25.89
55	55	69.60	-231.35	-4.99	-25.00
55	56	71.00	-231.35	-4.99	-18.02
56	56	71.00	-231.87	-5.55	-16.85
56	57	72.40	-231.87	-5.55	-9.09
57	57	72.40	-231.26	-5.58	-7.95
57	58	73.80	-231.26	-5.58	-0.13
58	58	73.80	-229.62	-5.09	1.00
58	59	75.20	-229.62	-5.09	8.13
59	59	75.20	-224.52	-4.17	8.96
59	60	76.60	-224.52	-4.17	14.80
60	60	76.60	-215.93	-2.97	15.33
60	61	78.00	-215.93	-2.97	19.49
61	1061	78.00	-207.27	-1.93	19.71
61	62	79.10	-207.27	-1.93	21.84
62	62	79.10	-199.95	-0.86	21.86
62	63	80.20	-199.95	-0.86	22.81
63	63	80.20	-191.25	0.15	22.66
63	64	81.30	-191.25	0.15	22.49
64	64	81.30	-181.15	1.03	22.14
64	65	82.40	-181.15	1.03	21.01
65	65	82.40	-169.64	1.71	20.45
65	66	83.50	-169.64	1.71	18.57
66	66	83.50	-157.61	2.14	18.00
66	67	84.60	-157.61	2.14	15.65
67	67	84.60	-145.04	2.32	15.05
67	68	85.70	-145.04	2.32	12.50
68	68	85.70	-132.83	2.27	12.06
68	69	86.80	-132.83	2.27	9.57
69	69	86.80	-120.92	2.06	9.27
69	70	87.90	-120.92	2.06	7.00
70	70	87.90	-109.29	1.75	6.83
70	71	89.00	-109.29	1.75	4.91
71	71	89.00	-97.90	1.39	4.85
71	72	90.10	-97.90	1.39	3.32
72	72	90.10	-86.72	1.02	3.36
72	73	91.20	-86.72	1.02	2.24
73	73	91.20	-75.71	0.68	2.38
73	74	92.30	-75.71	0.68	1.63
74	74	92.30	-64.85	0.40	1.85
74	75	93.40	-64.85	0.40	1.40
75	75	93.40	-54.11	0.22	1.69
75	76	94.50	-54.11	0.22	1.44
76	76	94.50	-43.46	0.17	1.78
76	77	95.60	-43.46	0.17	1.60
77	77	95.60	-32.88	0.25	2.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2posEI.FAM1.TOT + [-1;-1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.TOT + [-1;-1]ej2posEI.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	-32.88	0.25	1.72
78	78	96.70	-22.35	0.51	2.15
78	79	97.80	-22.35	0.51	1.59
79	79	97.80	-11.83	0.95	2.06
79	80	98.90	-11.83	0.95	1.01
80	80	98.90	-1.32	1.58	1.50
80	81	100.00	-1.32	1.58	-0.24
101	101	0.00	225.60	21.91	0.24
101	102	1.10	225.60	21.91	-23.86
102	102	1.10	226.45	21.27	-23.37
102	103	2.20	226.45	21.27	-46.77
103	103	2.20	227.77	20.84	-46.31
103	104	3.30	227.77	20.84	-69.23
104	104	3.30	229.54	20.58	-68.80
104	105	4.40	229.54	20.58	-91.43
105	105	4.40	231.75	20.49	-91.04
105	106	5.50	231.75	20.49	-113.58
106	106	5.50	234.40	20.55	-113.24
106	107	6.60	234.40	20.55	-135.84
107	107	6.60	237.48	20.73	-135.56
107	108	7.70	237.48	20.73	-158.37
108	108	7.70	241.01	21.01	-158.15
108	109	8.80	241.01	21.01	-181.26
109	109	8.80	244.98	21.35	-181.13
109	110	9.90	244.98	21.35	-204.61
110	110	9.90	249.41	21.72	-204.56
110	111	11.00	249.41	21.72	-228.45
111	111	11.00	254.31	22.08	-228.51
111	112	12.10	254.31	22.08	-252.79
112	112	12.10	259.71	22.39	-252.97
112	113	13.20	259.71	22.39	-277.59
113	113	13.20	265.64	22.60	-277.89
113	114	14.30	265.64	22.60	-302.75
114	114	14.30	272.13	22.64	-303.18
114	115	15.40	272.13	22.64	-328.09
115	115	15.40	279.22	22.47	-328.69
115	116	16.50	279.22	22.47	-353.41
116	116	16.50	286.01	22.04	-353.97
116	117	17.60	286.01	22.04	-378.22
117	117	17.60	292.54	21.36	-378.77
117	118	18.70	292.54	21.36	-402.27
118	118	18.70	297.91	20.48	-402.62
118	119	19.80	297.91	20.48	-425.14
119	119	19.80	302.13	19.46	-425.30
119	120	20.90	302.13	19.46	-446.71
120	120	20.90	305.24	18.40	-446.68
120	121	22.00	305.24	18.40	-466.92
121	1121	22.00	308.15	-8.74	-466.69
121	122	23.40	308.15	-8.74	-454.45
122	122	23.40	309.35	-9.95	-453.92
122	123	24.80	309.35	-9.95	-440.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

[1; 1]ej2posEl.FAM1.TOT + [-1;-1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.TOT + [-1;-1]ej2posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	307.66	-10.87	-439.17
123	124	26.20	307.66	-10.87	-423.96
124	124	26.20	303.03	-11.35	-422.82
124	125	27.60	303.03	-11.35	-406.93
125	125	27.60	297.80	-11.32	-405.79
125	126	29.00	297.80	-11.32	-389.94
126	126	29.00	291.80	-10.76	-388.77
126	127	30.40	291.80	-10.76	-373.71
127	127	30.40	287.37	-9.73	-372.83
127	128	31.80	287.37	-9.73	-359.21
128	128	31.80	284.35	-8.37	-358.57
128	129	33.20	284.35	-8.37	-346.85
129	129	33.20	282.66	-6.80	-346.46
129	130	34.60	282.66	-6.80	-336.95
130	130	34.60	282.21	-5.11	-336.78
130	131	36.00	282.21	-5.11	-329.62
131	131	36.00	283.01	-3.43	-329.67
131	132	37.40	283.01	-3.43	-324.88
132	132	37.40	285.03	-1.83	-325.15
132	133	38.80	285.03	-1.83	-322.59
133	133	38.80	288.33	-0.42	-323.09
133	134	40.20	288.33	-0.42	-322.51
134	134	40.20	292.98	0.70	-323.23
134	135	41.60	292.98	0.70	-324.21
135	135	41.60	299.08	1.42	-325.16
135	136	43.00	299.08	1.42	-327.15
136	136	43.00	306.79	1.61	-328.35
136	137	44.40	306.79	1.61	-330.61
137	137	44.40	313.82	1.23	-331.75
137	138	45.80	313.82	1.23	-333.47
138	138	45.80	320.31	0.29	-334.56
138	139	47.20	320.31	0.29	-334.97
139	139	47.20	323.97	-1.09	-335.69
139	140	48.60	323.97	-1.09	-334.17
140	140	48.60	324.86	-2.73	-334.53
140	141	50.00	324.86	-2.73	-330.71
141	1141	50.00	323.00	2.73	-330.71
141	142	51.40	323.00	2.73	-334.53
142	142	51.40	318.38	1.09	-334.17
142	143	52.80	318.38	1.09	-335.70
143	143	52.80	310.98	-0.29	-334.98
143	144	54.20	310.98	-0.29	-334.57
144	144	54.20	300.72	-1.23	-333.48
144	145	55.60	300.72	-1.23	-331.76
145	145	55.60	289.90	-1.61	-330.62
145	146	57.00	289.90	-1.61	-328.37
146	146	57.00	278.33	-1.42	-327.16
146	147	58.40	278.33	-1.42	-325.18
147	147	58.40	268.33	-0.70	-324.23
147	148	59.80	268.33	-0.70	-323.24
148	148	59.80	259.69	0.42	-322.52

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEl.HIP.Tinf

Pretensado Hiperestático (t=INF)

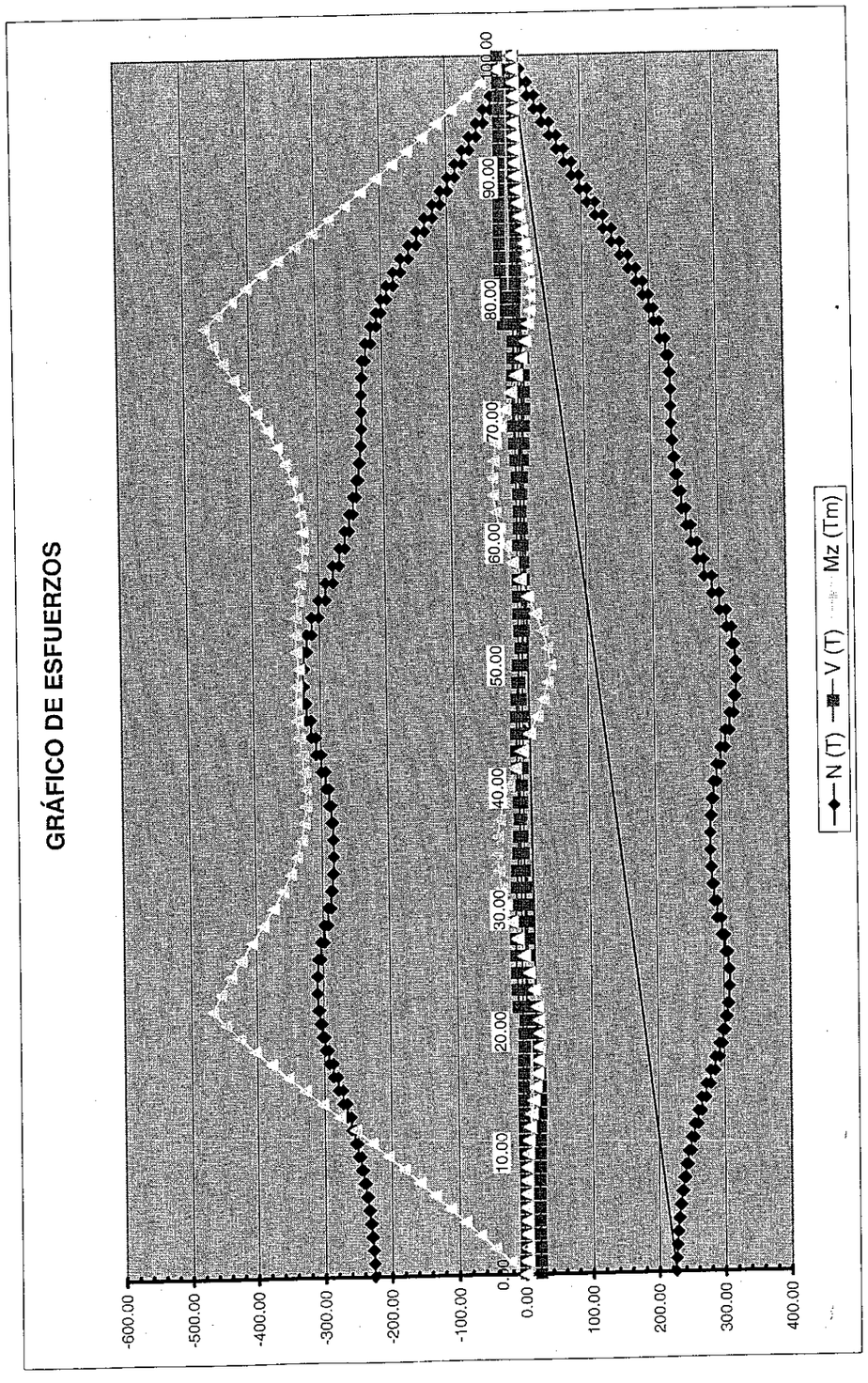
[1; 1]ej2posEl.FAM1.TOT + [-1;-1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.TOT + [-1;-1]ej2posEl.FA

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	259.69	0.42	-323.11
149	149	61.20	252.31	1.83	-322.61
149	150	62.60	252.31	1.83	-325.17
150	150	62.60	246.10	3.43	-324.89
150	151	64.00	246.10	3.43	-329.69
151	151	64.00	240.98	5.11	-329.64
151	152	65.40	240.98	5.11	-336.80
152	152	65.40	236.94	6.80	-336.96
152	153	66.80	236.94	6.80	-346.48
153	153	66.80	233.96	8.37	-346.87
153	154	68.20	233.96	8.37	-358.59
154	154	68.20	232.09	9.73	-359.22
154	155	69.60	232.09	9.73	-372.84
155	155	69.60	231.35	10.75	-373.73
155	156	71.00	231.35	10.75	-388.78
156	156	71.00	231.87	11.31	-389.95
156	157	72.40	231.87	11.31	-405.79
157	157	72.40	231.26	11.35	-406.94
157	158	73.80	231.26	11.35	-422.82
158	158	73.80	229.62	10.86	-423.96
158	159	75.20	229.62	10.86	-439.17
159	159	75.20	224.52	9.94	-439.99
159	160	76.60	224.52	9.94	-453.91
160	160	76.60	215.93	8.74	-454.44
160	161	78.00	215.93	8.74	-466.68
161	1161	78.00	207.27	-18.40	-466.90
161	162	79.10	207.27	-18.40	-446.67
162	162	79.10	199.96	-19.46	-446.69
162	163	80.20	199.96	-19.46	-425.28
163	163	80.20	191.25	-20.48	-425.13
163	164	81.30	191.25	-20.48	-402.60
164	164	81.30	181.15	-21.36	-402.26
164	165	82.40	181.15	-21.36	-378.76
165	165	82.40	169.64	-22.04	-378.21
165	166	83.50	169.64	-22.04	-353.97
166	166	83.50	157.61	-22.47	-353.40
166	167	84.60	157.61	-22.47	-328.68
167	167	84.60	145.04	-22.64	-328.09
167	168	85.70	145.04	-22.64	-303.18
168	168	85.70	132.83	-22.60	-302.74
168	169	86.80	132.83	-22.60	-277.88
169	169	86.80	120.92	-22.39	-277.59
169	170	87.90	120.92	-22.39	-252.96
170	170	87.90	109.29	-22.08	-252.79
170	171	89.00	109.29	-22.08	-228.50
171	171	89.00	97.90	-21.72	-228.45
171	172	90.10	97.90	-21.72	-204.56
172	172	90.10	86.72	-21.35	-204.60
172	173	91.20	86.72	-21.35	-181.12
173	173	91.20	75.71	-21.01	-181.26
173	174	92.30	75.71	-21.01	-158.15

Programa DINTEL PACADAR S.A.
ej2posEI.HIP.Tinf

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ej2posEI.ISO.To

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	0.00	0.00	0.00	0.00
2	2	0.00	0.00	0.00	0.00
2	3	0.00	0.00	0.00	0.00
3	3	0.00	0.00	0.00	0.00
3	4	0.00	0.00	0.00	0.00
4	4	0.00	0.00	0.00	0.00
4	5	0.00	0.00	0.00	0.00
5	5	0.00	0.00	0.00	0.00
5	6	0.00	0.00	0.00	0.00
6	6	0.00	0.00	0.00	0.00
6	7	0.00	0.00	0.00	0.00
7	7	0.00	0.00	0.00	0.00
7	8	0.00	0.00	0.00	0.00
8	8	0.00	0.00	0.00	0.00
8	9	0.00	0.00	0.00	0.00
9	9	0.00	0.00	0.00	0.00
9	10	0.00	0.00	0.00	0.00
10	10	0.00	0.00	0.00	0.00
10	11	0.00	0.00	0.00	0.00
11	11	0.00	0.00	0.00	0.00
11	12	0.00	0.00	0.00	0.00
12	12	0.00	0.00	0.00	0.00
12	13	0.00	0.00	0.00	0.00
13	13	0.00	0.00	0.00	0.00
13	14	0.00	0.00	0.00	0.00
14	14	0.00	0.00	0.00	0.00
14	15	0.00	0.00	0.00	0.00
15	15	0.00	0.00	0.00	0.00
15	16	0.00	0.00	0.00	0.00
16	16	0.00	0.00	0.00	0.00
16	17	0.00	0.00	0.00	0.00
17	17	0.00	0.00	0.00	0.00
17	18	0.00	0.00	0.00	0.00
18	18	0.00	0.00	0.00	0.00
18	19	0.00	0.00	0.00	0.00
19	19	0.00	0.00	0.00	0.00
19	20	0.00	0.00	0.00	0.00
20	20	0.00	0.00	0.00	0.00
20	21	0.00	0.00	0.00	0.00
21	1021	0.00	0.00	0.00	0.00
21	22	0.00	0.00	0.00	0.00
22	22	0.00	0.00	0.00	0.00
22	23	0.00	0.00	0.00	0.00
23	23	0.00	0.00	0.00	0.00
23	24	0.00	0.00	0.00	0.00
24	24	0.00	0.00	0.00	0.00
24	25	0.00	0.00	0.00	0.00
25	25	0.00	0.00	0.00	0.00
25	26	0.00	0.00	0.00	0.00
26	26	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	0.00	0.00	0.00	0.00
27	27	0.00	0.00	0.00	0.00
27	28	0.00	0.00	0.00	0.00
28	28	0.00	0.00	0.00	0.00
28	29	0.00	0.00	0.00	0.00
29	29	0.00	0.00	0.00	0.00
29	30	0.00	0.00	0.00	0.00
30	30	0.00	0.00	0.00	0.00
30	31	0.00	0.00	0.00	0.00
31	31	0.00	0.00	0.00	0.00
31	32	0.00	0.00	0.00	0.00
32	32	0.00	0.00	0.00	0.00
32	33	0.00	0.00	0.00	0.00
33	33	0.00	0.00	0.00	0.00
33	34	0.00	0.00	0.00	0.00
34	34	0.00	0.00	0.00	0.00
34	35	0.00	0.00	0.00	0.00
35	35	0.00	0.00	0.00	0.00
35	36	0.00	0.00	0.00	0.00
36	36	0.00	0.00	0.00	0.00
36	37	0.00	0.00	0.00	0.00
37	37	0.00	0.00	0.00	0.00
37	38	0.00	0.00	0.00	0.00
38	38	0.00	0.00	0.00	0.00
38	39	0.00	0.00	0.00	0.00
39	39	0.00	0.00	0.00	0.00
39	40	0.00	0.00	0.00	0.00
40	40	0.00	0.00	0.00	0.00
40	41	0.00	0.00	0.00	0.00
41	1041	0.00	0.00	0.00	0.00
41	42	0.00	0.00	0.00	0.00
42	42	0.00	0.00	0.00	0.00
42	43	0.00	0.00	0.00	0.00
43	43	0.00	0.00	0.00	0.00
43	44	0.00	0.00	0.00	0.00
44	44	0.00	0.00	0.00	0.00
44	45	0.00	0.00	0.00	0.00
45	45	0.00	0.00	0.00	0.00
45	46	0.00	0.00	0.00	0.00
46	46	0.00	0.00	0.00	0.00
46	47	0.00	0.00	0.00	0.00
47	47	0.00	0.00	0.00	0.00
47	48	0.00	0.00	0.00	0.00
48	48	0.00	0.00	0.00	0.00
48	49	0.00	0.00	0.00	0.00
49	49	0.00	0.00	0.00	0.00
49	50	0.00	0.00	0.00	0.00
50	50	0.00	0.00	0.00	0.00
50	51	0.00	0.00	0.00	0.00
51	51	0.00	0.00	0.00	0.00
51	52	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1)ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	0.00	0.00	0.00	0.00
52	53	0.00	0.00	0.00	0.00
53	53	0.00	0.00	0.00	0.00
53	54	0.00	0.00	0.00	0.00
54	54	0.00	0.00	0.00	0.00
54	55	0.00	0.00	0.00	0.00
55	55	0.00	0.00	0.00	0.00
55	56	0.00	0.00	0.00	0.00
56	56	0.00	0.00	0.00	0.00
56	57	0.00	0.00	0.00	0.00
57	57	0.00	0.00	0.00	0.00
57	58	0.00	0.00	0.00	0.00
58	58	0.00	0.00	0.00	0.00
58	59	0.00	0.00	0.00	0.00
59	59	0.00	0.00	0.00	0.00
59	60	0.00	0.00	0.00	0.00
60	60	0.00	0.00	0.00	0.00
60	61	0.00	0.00	0.00	0.00
61	1061	0.00	0.00	0.00	0.00
61	62	0.00	0.00	0.00	0.00
62	62	0.00	0.00	0.00	0.00
62	63	0.00	0.00	0.00	0.00
63	63	0.00	0.00	0.00	0.00
63	64	0.00	0.00	0.00	0.00
64	64	0.00	0.00	0.00	0.00
64	65	0.00	0.00	0.00	0.00
65	65	0.00	0.00	0.00	0.00
65	66	0.00	0.00	0.00	0.00
66	66	0.00	0.00	0.00	0.00
66	67	0.00	0.00	0.00	0.00
67	67	0.00	0.00	0.00	0.00
67	68	0.00	0.00	0.00	0.00
68	68	0.00	0.00	0.00	0.00
68	69	0.00	0.00	0.00	0.00
69	69	0.00	0.00	0.00	0.00
69	70	0.00	0.00	0.00	0.00
70	70	0.00	0.00	0.00	0.00
70	71	0.00	0.00	0.00	0.00
71	71	0.00	0.00	0.00	0.00
71	72	0.00	0.00	0.00	0.00
72	72	0.00	0.00	0.00	0.00
72	73	0.00	0.00	0.00	0.00
73	73	0.00	0.00	0.00	0.00
73	74	0.00	0.00	0.00	0.00
74	74	0.00	0.00	0.00	0.00
74	75	0.00	0.00	0.00	0.00
75	75	0.00	0.00	0.00	0.00
75	76	0.00	0.00	0.00	0.00
76	76	0.00	0.00	0.00	0.00
76	77	0.00	0.00	0.00	0.00
77	77	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	0.00	0.00	0.00	0.00
78	78	0.00	0.00	0.00	0.00
78	79	0.00	0.00	0.00	0.00
79	79	0.00	0.00	0.00	0.00
79	80	0.00	0.00	0.00	0.00
80	80	0.00	0.00	0.00	0.00
80	81	0.00	0.00	0.00	0.00
101	101	0.00	0.00	0.00	0.00
101	102	1.10	0.00	0.00	0.00
102	102	1.10	0.00	0.00	0.00
102	103	2.20	0.00	0.00	0.00
103	103	2.20	0.00	0.00	0.00
103	104	3.30	0.00	0.00	0.00
104	104	3.30	0.00	0.00	0.00
104	105	4.40	0.00	0.00	0.00
105	105	4.40	0.00	0.00	0.00
105	106	5.50	0.00	0.00	0.00
106	106	5.50	0.00	0.00	0.00
106	107	6.60	0.00	0.00	0.00
107	107	6.60	0.00	0.00	0.00
107	108	7.70	0.00	0.00	0.00
108	108	7.70	0.00	0.00	0.00
108	109	8.80	0.00	0.00	0.00
109	109	8.80	0.00	0.00	0.00
109	110	9.90	0.00	0.00	0.00
110	110	9.90	0.00	0.00	0.00
110	111	11.00	0.00	0.00	0.00
111	111	11.00	0.00	0.00	0.00
111	112	12.10	0.00	0.00	0.00
112	112	12.10	0.00	0.00	0.00
112	113	13.20	0.00	0.00	0.00
113	113	13.20	0.00	0.00	0.00
113	114	14.30	0.00	0.00	0.00
114	114	14.30	0.00	0.00	0.00
114	115	15.40	0.00	0.00	0.00
115	115	15.40	-870.24	0.00	418.59
115	116	16.50	-870.24	0.00	418.59
116	116	16.50	-870.24	0.00	418.59
116	117	17.60	-870.24	0.00	418.59
117	117	17.60	-1740.48	0.00	837.17
117	118	18.70	-1740.48	0.00	837.17
118	118	18.70	-1740.48	0.00	837.17
118	119	19.80	-1740.48	0.00	837.17
119	119	19.80	-1740.48	0.00	837.17
119	120	20.90	-1740.48	0.00	837.17
120	120	20.90	-1740.48	0.00	837.17
120	121	22.00	-1740.48	0.00	837.17
121	1121	22.00	-1740.48	0.00	837.17
121	122	23.40	-1740.48	0.00	837.17
122	122	23.40	-1740.48	0.00	837.17
122	123	24.80	-1740.48	0.00	837.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ej2posEI.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-1740.48	0.00	837.17
123	124	26.20	-1740.48	0.00	837.17
124	124	26.20	-870.24	0.00	418.59
124	125	27.60	-870.24	0.00	418.59
125	125	27.60	-870.24	0.00	418.59
125	126	29.00	-870.24	0.00	418.59
126	126	29.00	0.00	0.00	0.00
126	127	30.40	0.00	0.00	0.00
127	127	30.40	0.00	0.00	0.00
127	128	31.80	0.00	0.00	0.00
128	128	31.80	0.00	0.00	0.00
128	129	33.20	0.00	0.00	0.00
129	129	33.20	0.00	0.00	0.00
129	130	34.60	0.00	0.00	0.00
130	130	34.60	0.00	0.00	0.00
130	131	36.00	0.00	0.00	0.00
131	131	36.00	0.00	0.00	0.00
131	132	37.40	0.00	0.00	0.00
132	132	37.40	0.00	0.00	0.00
132	133	38.80	0.00	0.00	0.00
133	133	38.80	0.00	0.00	0.00
133	134	40.20	0.00	0.00	0.00
134	134	40.20	0.00	0.00	0.00
134	135	41.60	0.00	0.00	0.00
135	135	41.60	0.00	0.00	0.00
135	136	43.00	0.00	0.00	0.00
136	136	43.00	-870.24	0.00	418.59
136	137	44.40	-870.24	0.00	418.59
137	137	44.40	-870.24	0.00	418.59
137	138	45.80	-870.24	0.00	418.59
138	138	45.80	-1740.48	0.00	837.17
138	139	47.20	-1740.48	0.00	837.17
139	139	47.20	-1740.48	0.00	837.17
139	140	48.60	-1740.48	0.00	837.17
140	140	48.60	-1740.48	0.00	837.17
140	141	50.00	-1740.48	0.00	837.17
141	1141	50.00	-1740.48	0.00	837.17
141	142	51.40	-1740.48	0.00	837.17
142	142	51.40	-1740.48	0.00	837.17
142	143	52.80	-1740.48	0.00	837.17
143	143	52.80	-1740.48	0.00	837.17
143	144	54.20	-1740.48	0.00	837.17
144	144	54.20	-870.24	0.00	418.59
144	145	55.60	-870.24	0.00	418.59
145	145	55.60	-870.24	0.00	418.59
145	146	57.00	-870.24	0.00	418.59
146	146	57.00	0.00	0.00	0.00
146	147	58.40	0.00	0.00	0.00
147	147	58.40	0.00	0.00	0.00
147	148	59.80	0.00	0.00	0.00
148	148	59.80	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.ISO.To

Pretensado Isostático (t=0)

[1; 1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.ISO + [1; 1]ej2posEl.FAM3.ISO + [1; 1]ej2posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	0.00	0.00
149	149	61.20	0.00	0.00	0.00
149	150	62.60	0.00	0.00	0.00
150	150	62.60	0.00	0.00	0.00
150	151	64.00	0.00	0.00	0.00
151	151	64.00	0.00	0.00	0.00
151	152	65.40	0.00	0.00	0.00
152	152	65.40	0.00	0.00	0.00
152	153	66.80	0.00	0.00	0.00
153	153	66.80	0.00	0.00	0.00
153	154	68.20	0.00	0.00	0.00
154	154	68.20	0.00	0.00	0.00
154	155	69.60	0.00	0.00	0.00
155	155	69.60	0.00	0.00	0.00
155	156	71.00	0.00	0.00	0.00
156	156	71.00	-870.24	0.00	418.59
156	157	72.40	-870.24	0.00	418.59
157	157	72.40	-870.24	0.00	418.59
157	158	73.80	-870.24	0.00	418.59
158	158	73.80	-1740.48	0.00	837.17
158	159	75.20	-1740.48	0.00	837.17
159	159	75.20	-1740.48	0.00	837.17
159	160	76.60	-1740.48	0.00	837.17
160	160	76.60	-1740.48	0.00	837.17
160	161	78.00	-1740.48	0.00	837.17
161	1161	78.00	-1740.48	0.00	837.17
161	162	79.10	-1740.48	0.00	837.17
162	162	79.10	-1740.48	0.00	837.17
162	163	80.20	-1740.48	0.00	837.17
163	163	80.20	-1740.48	0.00	837.17
163	164	81.30	-1740.48	0.00	837.17
164	164	81.30	-1740.48	0.00	837.17
164	165	82.40	-1740.48	0.00	837.17
165	165	82.40	-870.24	0.00	418.59
165	166	83.50	-870.24	0.00	418.59
166	166	83.50	-870.24	0.00	418.59
166	167	84.60	-870.24	0.00	418.59
167	167	84.60	0.00	0.00	0.00
167	168	85.70	0.00	0.00	0.00
168	168	85.70	0.00	0.00	0.00
168	169	86.80	0.00	0.00	0.00
169	169	86.80	0.00	0.00	0.00
169	170	87.90	0.00	0.00	0.00
170	170	87.90	0.00	0.00	0.00
170	171	89.00	0.00	0.00	0.00
171	171	89.00	0.00	0.00	0.00
171	172	90.10	0.00	0.00	0.00
172	172	90.10	0.00	0.00	0.00
172	173	91.20	0.00	0.00	0.00
173	173	91.20	0.00	0.00	0.00
173	174	92.30	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.ISO.To

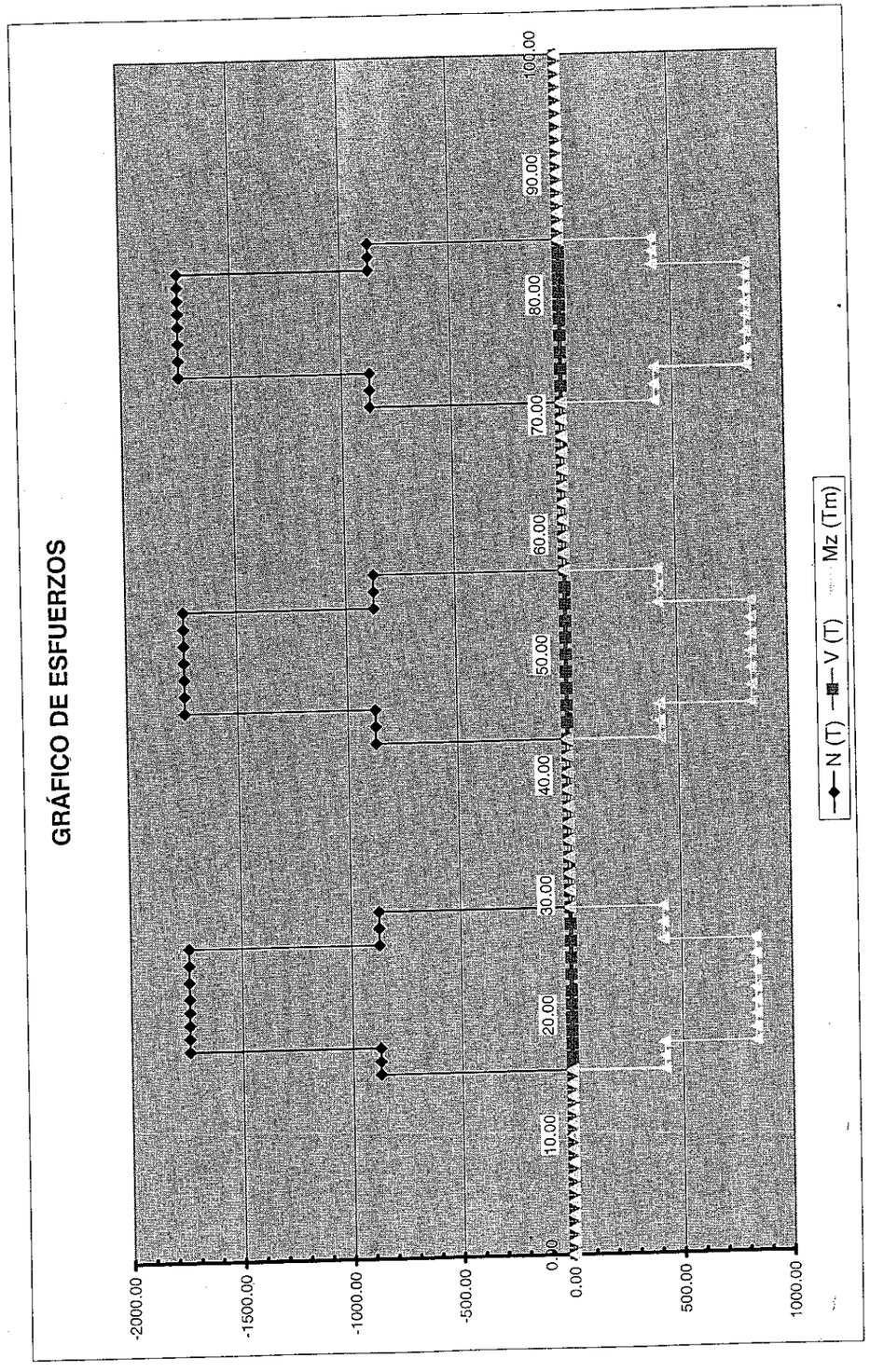
Pretensado Isostático (t=0)

[1; 1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.ISO + [1; 1]ej2posEl.FAM3.ISO + [1; 1]ej2posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	0.00	0.00
174	175	93.40	0.00	0.00	0.00
175	175	93.40	0.00	0.00	0.00
175	176	94.50	0.00	0.00	0.00
176	176	94.50	0.00	0.00	0.00
176	177	95.60	0.00	0.00	0.00
177	177	95.60	0.00	0.00	0.00
177	178	96.70	0.00	0.00	0.00
178	178	96.70	0.00	0.00	0.00
178	179	97.80	0.00	0.00	0.00
179	179	97.80	0.00	0.00	0.00
179	180	98.90	0.00	0.00	0.00
180	180	98.90	0.00	0.00	0.00
180	181	100.00	0.00	0.00	0.00

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.ISO + [1; 1]ej2posEl.FAM3.ISO + [1; 1]ej2posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	0.00	0.00
1	2	0.00	0.00	0.00	0.00
2	2	0.00	0.00	0.00	0.00
2	3	0.00	0.00	0.00	0.00
3	3	0.00	0.00	0.00	0.00
3	4	0.00	0.00	0.00	0.00
4	4	0.00	0.00	0.00	0.00
4	5	0.00	0.00	0.00	0.00
5	5	0.00	0.00	0.00	0.00
5	6	0.00	0.00	0.00	0.00
6	6	0.00	0.00	0.00	0.00
6	7	0.00	0.00	0.00	0.00
7	7	0.00	0.00	0.00	0.00
7	8	0.00	0.00	0.00	0.00
8	8	0.00	0.00	0.00	0.00
8	9	0.00	0.00	0.00	0.00
9	9	0.00	0.00	0.00	0.00
9	10	0.00	0.00	0.00	0.00
10	10	0.00	0.00	0.00	0.00
10	11	0.00	0.00	0.00	0.00
11	11	0.00	0.00	0.00	0.00
11	12	0.00	0.00	0.00	0.00
12	12	0.00	0.00	0.00	0.00
12	13	0.00	0.00	0.00	0.00
13	13	0.00	0.00	0.00	0.00
13	14	0.00	0.00	0.00	0.00
14	14	0.00	0.00	0.00	0.00
14	15	0.00	0.00	0.00	0.00
15	15	0.00	0.00	0.00	0.00
15	16	0.00	0.00	0.00	0.00
16	16	0.00	0.00	0.00	0.00
16	17	0.00	0.00	0.00	0.00
17	17	0.00	0.00	0.00	0.00
17	18	0.00	0.00	0.00	0.00
18	18	0.00	0.00	0.00	0.00
18	19	0.00	0.00	0.00	0.00
19	19	0.00	0.00	0.00	0.00
19	20	0.00	0.00	0.00	0.00
20	20	0.00	0.00	0.00	0.00
20	21	0.00	0.00	0.00	0.00
21	1021	0.00	0.00	0.00	0.00
21	22	0.00	0.00	0.00	0.00
22	22	0.00	0.00	0.00	0.00
22	23	0.00	0.00	0.00	0.00
23	23	0.00	0.00	0.00	0.00
23	24	0.00	0.00	0.00	0.00
24	24	0.00	0.00	0.00	0.00
24	25	0.00	0.00	0.00	0.00
25	25	0.00	0.00	0.00	0.00
25	26	0.00	0.00	0.00	0.00
26	26	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	0.00	0.00	0.00	0.00
27	27	0.00	0.00	0.00	0.00
27	28	0.00	0.00	0.00	0.00
28	28	0.00	0.00	0.00	0.00
28	29	0.00	0.00	0.00	0.00
29	29	0.00	0.00	0.00	0.00
29	30	0.00	0.00	0.00	0.00
30	30	0.00	0.00	0.00	0.00
30	31	0.00	0.00	0.00	0.00
31	31	0.00	0.00	0.00	0.00
31	32	0.00	0.00	0.00	0.00
32	32	0.00	0.00	0.00	0.00
32	33	0.00	0.00	0.00	0.00
33	33	0.00	0.00	0.00	0.00
33	34	0.00	0.00	0.00	0.00
34	34	0.00	0.00	0.00	0.00
34	35	0.00	0.00	0.00	0.00
35	35	0.00	0.00	0.00	0.00
35	36	0.00	0.00	0.00	0.00
36	36	0.00	0.00	0.00	0.00
36	37	0.00	0.00	0.00	0.00
37	37	0.00	0.00	0.00	0.00
37	38	0.00	0.00	0.00	0.00
38	38	0.00	0.00	0.00	0.00
38	39	0.00	0.00	0.00	0.00
39	39	0.00	0.00	0.00	0.00
39	40	0.00	0.00	0.00	0.00
40	40	0.00	0.00	0.00	0.00
40	41	0.00	0.00	0.00	0.00
41	1041	0.00	0.00	0.00	0.00
41	42	0.00	0.00	0.00	0.00
42	42	0.00	0.00	0.00	0.00
42	43	0.00	0.00	0.00	0.00
43	43	0.00	0.00	0.00	0.00
43	44	0.00	0.00	0.00	0.00
44	44	0.00	0.00	0.00	0.00
44	45	0.00	0.00	0.00	0.00
45	45	0.00	0.00	0.00	0.00
45	46	0.00	0.00	0.00	0.00
46	46	0.00	0.00	0.00	0.00
46	47	0.00	0.00	0.00	0.00
47	47	0.00	0.00	0.00	0.00
47	48	0.00	0.00	0.00	0.00
48	48	0.00	0.00	0.00	0.00
48	49	0.00	0.00	0.00	0.00
49	49	0.00	0.00	0.00	0.00
49	50	0.00	0.00	0.00	0.00
50	50	0.00	0.00	0.00	0.00
50	51	0.00	0.00	0.00	0.00
51	51	0.00	0.00	0.00	0.00
51	52	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	0.00	0.00	0.00	0.00
52	53	0.00	0.00	0.00	0.00
53	53	0.00	0.00	0.00	0.00
53	54	0.00	0.00	0.00	0.00
54	54	0.00	0.00	0.00	0.00
54	55	0.00	0.00	0.00	0.00
55	55	0.00	0.00	0.00	0.00
55	56	0.00	0.00	0.00	0.00
56	56	0.00	0.00	0.00	0.00
56	57	0.00	0.00	0.00	0.00
57	57	0.00	0.00	0.00	0.00
57	58	0.00	0.00	0.00	0.00
58	58	0.00	0.00	0.00	0.00
58	59	0.00	0.00	0.00	0.00
59	59	0.00	0.00	0.00	0.00
59	60	0.00	0.00	0.00	0.00
60	60	0.00	0.00	0.00	0.00
60	61	0.00	0.00	0.00	0.00
61	1061	0.00	0.00	0.00	0.00
61	62	0.00	0.00	0.00	0.00
62	62	0.00	0.00	0.00	0.00
62	63	0.00	0.00	0.00	0.00
63	63	0.00	0.00	0.00	0.00
63	64	0.00	0.00	0.00	0.00
64	64	0.00	0.00	0.00	0.00
64	65	0.00	0.00	0.00	0.00
65	65	0.00	0.00	0.00	0.00
65	66	0.00	0.00	0.00	0.00
66	66	0.00	0.00	0.00	0.00
66	67	0.00	0.00	0.00	0.00
67	67	0.00	0.00	0.00	0.00
67	68	0.00	0.00	0.00	0.00
68	68	0.00	0.00	0.00	0.00
68	69	0.00	0.00	0.00	0.00
69	69	0.00	0.00	0.00	0.00
69	70	0.00	0.00	0.00	0.00
70	70	0.00	0.00	0.00	0.00
70	71	0.00	0.00	0.00	0.00
71	71	0.00	0.00	0.00	0.00
71	72	0.00	0.00	0.00	0.00
72	72	0.00	0.00	0.00	0.00
72	73	0.00	0.00	0.00	0.00
73	73	0.00	0.00	0.00	0.00
73	74	0.00	0.00	0.00	0.00
74	74	0.00	0.00	0.00	0.00
74	75	0.00	0.00	0.00	0.00
75	75	0.00	0.00	0.00	0.00
75	76	0.00	0.00	0.00	0.00
76	76	0.00	0.00	0.00	0.00
76	77	0.00	0.00	0.00	0.00
77	77	0.00	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAN

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	0.00	0.00	0.00	0.00
78	78	0.00	0.00	0.00	0.00
78	79	0.00	0.00	0.00	0.00
79	79	0.00	0.00	0.00	0.00
79	80	0.00	0.00	0.00	0.00
80	80	0.00	0.00	0.00	0.00
80	81	0.00	0.00	0.00	0.00
101	101	0.00	0.00	0.00	0.00
101	102	1.10	0.00	0.00	0.00
102	102	1.10	0.00	0.00	0.00
102	103	2.20	0.00	0.00	0.00
103	103	2.20	0.00	0.00	0.00
103	104	3.30	0.00	0.00	0.00
104	104	3.30	0.00	0.00	0.00
104	105	4.40	0.00	0.00	0.00
105	105	4.40	0.00	0.00	0.00
105	106	5.50	0.00	0.00	0.00
106	106	5.50	0.00	0.00	0.00
106	107	6.60	0.00	0.00	0.00
107	107	6.60	0.00	0.00	0.00
107	108	7.70	0.00	0.00	0.00
108	108	7.70	0.00	0.00	0.00
108	109	8.80	0.00	0.00	0.00
109	109	8.80	0.00	0.00	0.00
109	110	9.90	0.00	0.00	0.00
110	110	9.90	0.00	0.00	0.00
110	111	11.00	0.00	0.00	0.00
111	111	11.00	0.00	0.00	0.00
111	112	12.10	0.00	0.00	0.00
112	112	12.10	0.00	0.00	0.00
112	113	13.20	0.00	0.00	0.00
113	113	13.20	0.00	0.00	0.00
113	114	14.30	0.00	0.00	0.00
114	114	14.30	0.00	0.00	0.00
114	115	15.40	0.00	0.00	0.00
115	115	15.40	-870.24	0.00	418.59
115	116	16.50	-870.24	0.00	418.59
116	116	16.50	-870.24	0.00	418.59
116	117	17.60	-870.24	0.00	418.59
117	117	17.60	-1740.48	0.00	837.17
117	118	18.70	-1740.48	0.00	837.17
118	118	18.70	-1740.48	0.00	837.17
118	119	19.80	-1740.48	0.00	837.17
119	119	19.80	-1740.48	0.00	837.17
119	120	20.90	-1740.48	0.00	837.17
120	120	20.90	-1740.48	0.00	837.17
120	121	22.00	-1740.48	0.00	837.17
121	1121	22.00	-1740.48	0.00	837.17
121	122	23.40	-1740.48	0.00	837.17
122	122	23.40	-1740.48	0.00	837.17
122	123	24.80	-1740.48	0.00	837.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ej2posEI.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEI.FAM1.ISO + [1; 1]ej2posEI.FAM2.ISO + [1; 1]ej2posEI.FAM3.ISO + [1; 1]ej2posEI.FAN

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	-1740.48	0.00	837.17
123	124	26.20	-1740.48	0.00	837.17
124	124	26.20	-870.24	0.00	418.59
124	125	27.60	-870.24	0.00	418.59
125	125	27.60	-870.24	0.00	418.59
125	126	29.00	-870.24	0.00	418.59
126	126	29.00	0.00	0.00	0.00
126	127	30.40	0.00	0.00	0.00
127	127	30.40	0.00	0.00	0.00
127	128	31.80	0.00	0.00	0.00
128	128	31.80	0.00	0.00	0.00
128	129	33.20	0.00	0.00	0.00
129	129	33.20	0.00	0.00	0.00
129	130	34.60	0.00	0.00	0.00
130	130	34.60	0.00	0.00	0.00
130	131	36.00	0.00	0.00	0.00
131	131	36.00	0.00	0.00	0.00
131	132	37.40	0.00	0.00	0.00
132	132	37.40	0.00	0.00	0.00
132	133	38.80	0.00	0.00	0.00
133	133	38.80	0.00	0.00	0.00
133	134	40.20	0.00	0.00	0.00
134	134	40.20	0.00	0.00	0.00
134	135	41.60	0.00	0.00	0.00
135	135	41.60	0.00	0.00	0.00
135	136	43.00	0.00	0.00	0.00
136	136	43.00	-870.24	0.00	418.59
136	137	44.40	-870.24	0.00	418.59
137	137	44.40	-870.24	0.00	418.59
137	138	45.80	-870.24	0.00	418.59
138	138	45.80	-1740.48	0.00	837.17
138	139	47.20	-1740.48	0.00	837.17
139	139	47.20	-1740.48	0.00	837.17
139	140	48.60	-1740.48	0.00	837.17
140	140	48.60	-1740.48	0.00	837.17
140	141	50.00	-1740.48	0.00	837.17
141	1141	50.00	-1740.48	0.00	837.17
141	142	51.40	-1740.48	0.00	837.17
142	142	51.40	-1740.48	0.00	837.17
142	143	52.80	-1740.48	0.00	837.17
143	143	52.80	-1740.48	0.00	837.17
143	144	54.20	-1740.48	0.00	837.17
144	144	54.20	-870.24	0.00	418.59
144	145	55.60	-870.24	0.00	418.59
145	145	55.60	-870.24	0.00	418.59
145	146	57.00	-870.24	0.00	418.59
146	146	57.00	0.00	0.00	0.00
146	147	58.40	0.00	0.00	0.00
147	147	58.40	0.00	0.00	0.00
147	148	59.80	0.00	0.00	0.00
148	148	59.80	0.00	0.00	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

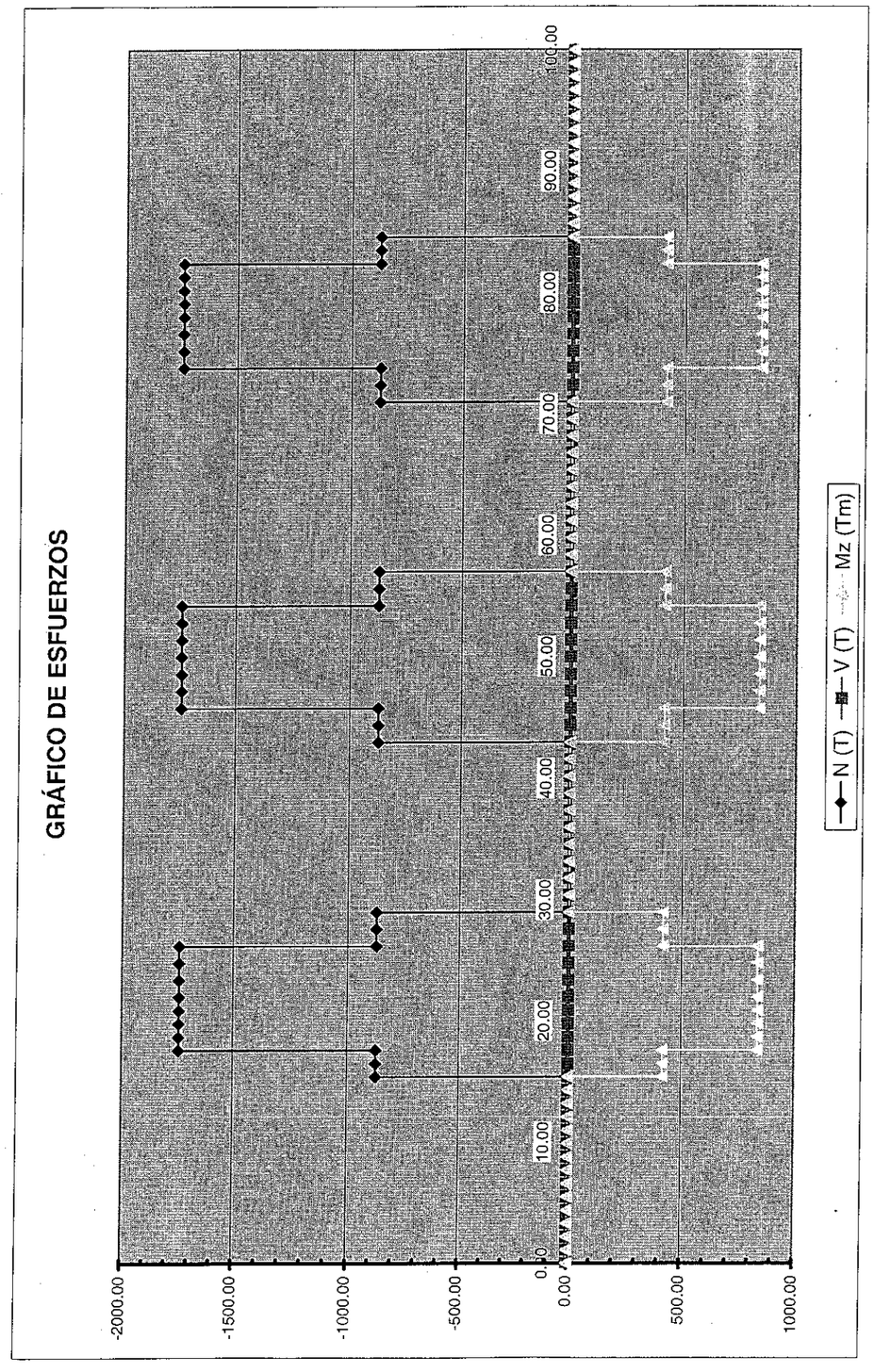
ej2posEl.ISO.Tinf

Pretensado Isostático (t=INF)

[1; 1]ej2posEl.FAM1.ISO + [1; 1]ej2posEl.FAM2.ISO + [1; 1]ej2posEl.FAM3.ISO + [1; 1]ej2posEl.FAM

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	0.00	0.00
149	149	61.20	0.00	0.00	0.00
149	150	62.60	0.00	0.00	0.00
150	150	62.60	0.00	0.00	0.00
150	151	64.00	0.00	0.00	0.00
151	151	64.00	0.00	0.00	0.00
151	152	65.40	0.00	0.00	0.00
152	152	65.40	0.00	0.00	0.00
152	153	66.80	0.00	0.00	0.00
153	153	66.80	0.00	0.00	0.00
153	154	68.20	0.00	0.00	0.00
154	154	68.20	0.00	0.00	0.00
154	155	69.60	0.00	0.00	0.00
155	155	69.60	0.00	0.00	0.00
155	156	71.00	0.00	0.00	0.00
156	156	71.00	-870.24	0.00	418.59
156	157	72.40	-870.24	0.00	418.59
157	157	72.40	-870.24	0.00	418.59
157	158	73.80	-870.24	0.00	418.59
158	158	73.80	-1740.48	0.00	837.17
158	159	75.20	-1740.48	0.00	837.17
159	159	75.20	-1740.48	0.00	837.17
159	160	76.60	-1740.48	0.00	837.17
160	160	76.60	-1740.48	0.00	837.17
160	161	78.00	-1740.48	0.00	837.17
161	1161	78.00	-1740.48	0.00	837.17
161	162	79.10	-1740.48	0.00	837.17
162	162	79.10	-1740.48	0.00	837.17
162	163	80.20	-1740.48	0.00	837.17
163	163	80.20	-1740.48	0.00	837.17
163	164	81.30	-1740.48	0.00	837.17
164	164	81.30	-1740.48	0.00	837.17
164	165	82.40	-1740.48	0.00	837.17
165	165	82.40	-870.24	0.00	418.59
165	166	83.50	-870.24	0.00	418.59
166	166	83.50	-870.24	0.00	418.59
166	167	84.60	-870.24	0.00	418.59
167	167	84.60	0.00	0.00	0.00
167	168	85.70	0.00	0.00	0.00
168	168	85.70	0.00	0.00	0.00
168	169	86.80	0.00	0.00	0.00
169	169	86.80	0.00	0.00	0.00
169	170	87.90	0.00	0.00	0.00
170	170	87.90	0.00	0.00	0.00
170	171	89.00	0.00	0.00	0.00
171	171	89.00	0.00	0.00	0.00
171	172	90.10	0.00	0.00	0.00
172	172	90.10	0.00	0.00	0.00
172	173	91.20	0.00	0.00	0.00
173	173	91.20	0.00	0.00	0.00
173	174	92.30	0.00	0.00	0.00



TENSIONES EN ESTADOS COMBINADOS

TIEMPO 0

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ+

Construcción sin gradiente en fase constructiva 1

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-35.67	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
1	2	1.10	-472.42	-30.38	-142.56	0	-604.79	1.8	-46.79	1.8	0.00	2.12	0.00
2	2	1.10	-747.99	-30.38	-316.72	0	-1102.35	1.8	137.39	1.8	0.00	2.12	0.00
2	3	2.20	-747.99	-27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
3	3	2.20	-747.99	-27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
3	4	3.30	-747.99	-23.65	-257.28	0	-1007.80	1.8	-0.73	1.8	0.00	2.12	0.00
4	4	3.30	-944.83	-23.65	-377.75	0	-1356.94	1.8	121.68	1.8	0.00	2.12	0.00
4	5	4.40	-944.83	-20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
5	5	4.40	-944.83	-20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
5	6	5.50	-944.83	-16.92	-333.12	0	-1285.95	1.8	17.98	1.8	0.00	2.12	0.00
6	6	5.50	-1141.67	-16.92	-451.61	0	-1631.95	1.8	135.80	1.8	0.00	2.12	0.00
6	7	6.60	-1141.67	-13.55	-434.85	0	-1605.29	1.8	96.86	1.8	0.00	2.12	0.00
7	7	6.60	-1141.67	-13.55	-434.85	0	-1594.00	1.8	81.57	1.8	0.00	2.12	0.00
7	8	7.70	-1141.67	-10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
8	8	7.70	-1141.67	-10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
8	9	8.80	-1141.67	-6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
9	9	8.80	-1141.67	-6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
9	10	9.90	-1141.67	-3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
10	10	9.90	-1141.67	-3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
10	11	11.00	-1141.67	-0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
11	11	11.00	-1141.67	-0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
11	12	12.10	-1141.67	3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
12	12	12.10	-1141.67	3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
12	13	13.20	-1141.67	6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
13	13	13.20	-1141.67	6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
13	14	14.30	-1141.67	10.01	-421.20	0	-1573.20	1.8	49.78	1.8	0.00	2.12	0.00
14	14	14.30	-944.83	10.01	-302.71	0	-1237.58	1.8	-52.68	1.8	0.00	2.12	0.00
14	15	15.40	-944.83	13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
15	15	15.40	-944.83	13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
15	16	16.50	-944.83	16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
16	16	16.50	-944.83	16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
16	17	17.60	-944.83	20.11	-352.79	0	-1317.24	1.8	63.68	1.8	0.00	2.12	0.00
17	17	17.60	-747.99	20.11	-231.93	0	-967.48	1.8	-59.64	1.8	0.00	2.12	0.00
17	18	18.70	-747.99	23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
18	18	18.70	-747.99	23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
18	19	19.80	-747.99	26.84	-283.57	0	-1049.62	1.8	60.36	1.8	0.00	2.12	0.00
19	19	19.80	-472.42	26.84	-109.41	0	-552.06	1.8	-123.82	1.8	0.00	2.12	0.00
19	20	20.90	-472.42	30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
20	20	20.90	-472.42	30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
20	21	22.00	-472.42	39.07	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
21	1021	22.00	-511.78	-49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
21	22	23.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
22	22	23.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
22	23	24.80	-511.78	-34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
23	23	24.80	-787.36	-34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
23	24	26.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
24	24	26.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
24	25	27.60	-787.36	-25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
25	25	27.60	-1141.67	-25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
25	26	29.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
26	26	29.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
26	27	30.40	-1141.67	-17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
27	27	30.40	-1456.62	-17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
27	28	31.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
28	28	31.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
28	29	33.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
29	29	33.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
29	30	34.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
30	30	34.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
30	31	36.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
31	31	36.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
31	32	37.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
32	32	37.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
32	33	38.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
33	33	38.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
33	34	40.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
34	34	40.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
34	35	41.60	-1456.62	17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
35	35	41.60	-1141.67	17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
35	36	43.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
36	36	43.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
36	37	44.40	-1141.67	25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
37	37	44.40	-787.36	25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
37	38	45.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
38	38	45.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ+

Construcción sin gradiente en fase constructiva 1

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-787.36	34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
39	39	47.20	-511.78	34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
39	40	48.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
40	40	48.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
40	41	50.00	-511.78	49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
41	1041	50.00	-511.78	-49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
41	42	51.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
42	42	51.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
42	43	52.80	-511.78	-34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
43	43	52.80	-787.36	-34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
43	44	54.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
44	44	54.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
44	45	55.60	-787.36	-25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
45	45	55.60	-1141.67	-25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
45	46	57.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
46	46	57.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
46	47	58.40	-1141.67	-17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
47	47	58.40	-1456.62	-17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
47	48	59.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
48	48	59.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
48	49	61.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
49	49	61.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
49	50	62.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
50	50	62.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
50	51	64.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
51	51	64.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
51	52	65.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
52	52	65.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
52	53	66.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
53	53	66.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
53	54	68.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
54	54	68.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
54	55	69.60	-1456.62	17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
55	55	69.60	-1141.67	17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
55	56	71.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
56	56	71.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
56	57	72.40	-1141.67	25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
57	57	72.40	-787.36	25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
57	58	73.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
58	58	73.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
58	59	75.20	-787.36	34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
59	59	75.20	-511.78	34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
59	60	76.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
60	60	76.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
60	61	78.00	-511.78	49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
61	1061	78.00	-472.42	-39.07	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
61	62	79.10	-472.42	-30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
62	62	79.10	-472.42	-30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
62	63	80.20	-472.42	-26.84	-109.41	0	-552.06	1.8	-123.82	1.8	0.00	2.12	0.00
63	63	80.20	-747.99	-26.84	-283.57	0	-1049.62	1.8	60.36	1.8	0.00	2.12	0.00
63	64	81.30	-747.99	-23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
64	64	81.30	-747.99	-23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
64	65	82.40	-747.99	-20.11	-231.93	0	-967.48	1.8	-59.64	1.8	0.00	2.12	0.00
65	65	82.40	-944.83	-20.11	-352.40	0	-1316.62	1.8	62.78	1.8	0.00	2.12	0.00
65	66	83.50	-944.83	-16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
66	66	83.50	-944.83	-16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
66	67	84.60	-944.83	-13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
67	67	84.60	-944.83	-13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
67	68	85.70	-944.83	-10.01	-302.71	0	-1237.58	1.8	-52.68	1.8	0.00	2.12	0.00
68	68	85.70	-1141.67	-10.01	-421.20	0	-1573.20	1.8	49.78	1.8	0.00	2.12	0.00
68	69	86.80	-1141.67	-6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
69	69	86.80	-1141.67	-6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
69	70	87.90	-1141.67	-3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
70	70	87.90	-1141.67	-3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
70	71	89.00	-1141.67	0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
71	71	89.00	-1141.67	0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
71	72	90.10	-1141.67	3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
72	72	90.10	-1141.67	3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
72	73	91.20	-1141.67	6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
73	73	91.20	-1141.67	6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
73	74	92.30	-1141.67	10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
74	74	92.30	-1141.67	10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
74	75	93.40	-1141.67	13.55	-434.85	0	-1594.00	1.8	81.57	1.8	0.00	2.12	0.00
75	75	93.40	-1141.67	13.55	-434.85	0	-1605.29	1.8	96.86	1.8	0.00	2.12	0.00
75	76	94.50	-1141.67	16.92	-451.61	0	-1631.95	1.8	135.80	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ+

Construcción sin gradiente en fase constructiva 1

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	16.92	-333.12	0	-1285.95	1.8	17.98	1.8	0.00	2.12	0.00
76	77	95.60	-944.83	20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
77	77	95.60	-944.83	20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
77	78	96.70	-944.83	23.65	-377.75	0	-1356.94	1.8	121.68	1.8	0.00	2.12	0.00
78	78	96.70	-747.99	23.65	-257.28	0	-1007.80	1.8	-0.73	1.8	0.00	2.12	0.00
78	79	97.80	-747.99	27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
79	79	97.80	-747.99	27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
79	80	98.90	-747.99	30.38	-316.72	0	-1102.35	1.8	137.39	1.8	0.00	2.12	0.00
80	80	98.90	-472.42	30.38	-142.56	0	-604.79	1.8	-46.79	1.8	0.00	2.12	0.00
80	81	100.00	-472.42	35.67	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	101	0.00	-472.42	-35.67	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	102	1.10	-472.42	-30.38	-142.56	0	-604.79	1.8	-46.79	1.8	0.00	2.12	0.00
102	102	1.10	-747.99	-30.38	-316.72	0	-1102.35	1.8	137.39	1.8	0.00	2.12	0.00
102	103	2.20	-747.99	-27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
103	103	2.20	-747.99	-27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
103	104	3.30	-747.99	-23.65	-257.28	0	-1007.80	1.8	-0.73	1.8	0.00	2.12	0.00
104	104	3.30	-944.83	-23.65	-377.75	0	-1356.94	1.8	121.68	1.8	0.00	2.12	0.00
104	105	4.40	-944.83	-20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
105	105	4.40	-944.83	-20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
105	106	5.50	-944.83	-16.92	-333.12	0	-1285.95	1.8	17.98	1.8	0.00	2.12	0.00
106	106	5.50	-1141.67	-16.92	-451.61	0	-1631.95	1.8	135.80	1.8	0.00	2.12	0.00
106	107	6.60	-1141.67	-13.55	-434.85	0	-1605.29	1.8	96.86	1.8	0.00	2.12	0.00
107	107	6.60	-1141.67	-13.55	-434.85	0	-1594.00	1.8	81.57	1.8	0.00	2.12	0.00
107	108	7.70	-1141.67	-10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
108	108	7.70	-1141.67	-10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
108	109	8.80	-1141.67	-6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
109	109	8.80	-1141.67	-6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
109	110	9.90	-1141.67	-3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
110	110	9.90	-1141.67	-3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
110	111	11.00	-1141.67	-0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
111	111	11.00	-1141.67	-0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
111	112	12.10	-1141.67	3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
112	112	12.10	-1141.67	3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
112	113	13.20	-1141.67	6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
113	113	13.20	-1141.67	6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
113	114	14.30	-1141.67	10.01	-421.20	0	-1573.20	1.8	49.78	1.8	0.00	2.12	0.00
114	114	14.30	-944.83	10.01	-302.71	0	-1237.58	1.8	-52.68	1.8	0.00	2.12	0.00
114	115	15.40	-944.83	13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
115	115	15.40	-944.83	13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
115	116	16.50	-944.83	16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
116	116	16.50	-944.83	16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
116	117	17.60	-944.83	20.11	-352.79	0	-1317.24	1.8	63.68	1.8	0.00	2.12	0.00
117	117	17.60	-747.99	20.11	-231.93	0	-967.48	1.8	-59.64	1.8	0.00	2.12	0.00
117	118	18.70	-747.99	23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
118	118	18.70	-747.99	23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
118	119	19.80	-747.99	26.84	-283.57	0	-1049.62	1.8	60.36	1.8	0.00	2.12	0.00
119	119	19.80	-472.42	26.84	-109.41	0	-552.06	1.8	-123.82	1.8	0.00	2.12	0.00
119	120	20.90	-472.42	30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
120	120	20.90	-472.42	30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
120	121	22.00	-472.42	39.07	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
121	1121	22.00	-511.78	-49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
121	122	23.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
122	122	23.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
122	123	24.80	-511.78	-34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
123	123	24.80	-787.36	-34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
123	124	26.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
124	124	26.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
124	125	27.60	-787.36	-25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
125	125	27.60	-1141.67	-25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
125	126	29.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
126	126	29.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
126	127	30.40	-1141.67	-17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
127	127	30.40	-1456.62	-17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
127	128	31.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
128	128	31.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
128	129	33.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
129	129	33.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
129	130	34.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
130	130	34.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
130	131	36.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
131	131	36.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
131	132	37.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
132	132	37.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
132	133	38.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
133	133	38.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ+
Construcción sin gradiente en fase constructiva 1
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra	InfCajón	Fibra	SupCajón	Fibra	InfLosa	Fibra	SupLosa
						y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)
133	134	40.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
134	134	40.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
134	135	41.60	-1456.62	17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
135	135	41.60	-1141.67	17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
135	136	43.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
136	136	43.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
136	137	44.40	-1141.67	25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
137	137	44.40	-787.36	25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
137	138	45.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
138	138	45.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
138	139	47.20	-787.36	34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
139	139	47.20	-511.78	34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
139	140	48.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
140	140	48.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
140	141	50.00	-511.78	49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
141	1141	50.00	-511.78	-49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
141	142	51.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
142	142	51.40	-511.78	-38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
142	143	52.80	-511.78	-34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
143	143	52.80	-787.36	-34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
143	144	54.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
144	144	54.20	-787.36	-29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
144	145	55.60	-787.36	-25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
145	145	55.60	-1141.67	-25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
145	146	57.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
146	146	57.00	-1141.67	-21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
146	147	58.40	-1141.67	-17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
147	147	58.40	-1456.62	-17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
147	148	59.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
148	148	59.80	-1456.62	-12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
148	149	61.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
149	149	61.20	-1456.62	-8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
149	150	62.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
150	150	62.60	-1456.62	-4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
150	151	64.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
151	151	64.00	-1456.62	0.00	-461.48	0	-1891.51	1.8	-113.33	1.8	0.00	2.12	0.00
151	152	65.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
152	152	65.40	-1456.62	4.28	-464.48	0	-1896.08	1.8	-106.34	1.8	0.00	2.12	0.00
152	153	66.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
153	153	66.80	-1456.62	8.57	-473.47	0	-1909.78	1.8	-85.40	1.8	0.00	2.12	0.00
153	154	68.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
154	154	68.20	-1456.62	12.85	-488.47	0	-1932.63	1.8	-50.46	1.8	0.00	2.12	0.00
154	155	69.60	-1456.62	17.14	-509.46	0	-1964.62	1.8	-1.57	1.8	0.00	2.12	0.00
155	155	69.60	-1141.67	17.14	-329.31	0	-1437.41	1.8	-148.38	1.8	0.00	2.12	0.00
155	156	71.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
156	156	71.00	-1141.67	21.42	-356.30	0	-1480.34	1.8	-85.67	1.8	0.00	2.12	0.00
156	157	72.40	-1141.67	25.70	-389.28	0	-1532.80	1.8	-9.03	1.8	0.00	2.12	0.00
157	157	72.40	-787.36	25.70	-179.53	0	-915.64	1.8	-212.89	1.8	0.00	2.12	0.00
157	158	73.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
158	158	73.80	-787.36	29.99	-218.52	0	-977.65	1.8	-122.29	1.8	0.00	2.12	0.00
158	159	75.20	-787.36	34.27	-263.50	0	-1049.20	1.8	-17.77	1.8	0.00	2.12	0.00
159	159	75.20	-511.78	34.27	-92.09	0	-556.03	1.8	-195.55	1.8	0.00	2.12	0.00
159	160	76.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
160	160	76.60	-511.78	38.56	-143.07	0	-637.12	1.8	-77.09	1.8	0.00	2.12	0.00
160	161	78.00	-511.78	49.84	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
161	1161	78.00	-472.42	-39.07	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
161	162	79.10	-472.42	-30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
162	162	79.10	-472.42	-30.20	-140.79	0	-601.98	1.8	-50.90	1.8	0.00	2.12	0.00
162	163	80.20	-472.42	-26.84	-109.41	0	-552.06	1.8	-123.82	1.8	0.00	2.12	0.00
163	163	80.20	-747.99	-26.84	-283.57	0	-1049.62	1.8	60.36	1.8	0.00	2.12	0.00
163	164	81.30	-747.99	-23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
164	164	81.30	-747.99	-23.47	-255.90	0	-1005.60	1.8	-3.94	1.8	0.00	2.12	0.00
164	165	82.40	-747.99	-20.11	-231.93	0	-967.48	1.8	-59.64	1.8	0.00	2.12	0.00
165	165	82.40	-944.83	-20.11	-352.40	0	-1316.62	1.8	62.78	1.8	0.00	2.12	0.00
165	166	83.50	-944.83	-16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
166	166	83.50	-944.83	-16.74	-332.14	0	-1284.39	1.8	15.70	1.8	0.00	2.12	0.00
166	167	84.60	-944.83	-13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
167	167	84.60	-944.83	-13.37	-315.57	0	-1258.03	1.8	-22.80	1.8	0.00	2.12	0.00
167	168	85.70	-944.83	-10.01	-302.71	0	-1237.58	1.8	-52.68	1.8	0.00	2.12	0.00
168	168	85.70	-1141.67	-10.01	-421.20	0	-1573.20	1.8	49.78	1.8	0.00	2.12	0.00
168	169	86.80	-1141.67	-6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
169	169	86.80	-1141.67	-6.64	-412.05	0	-1559.26	1.8	28.46	1.8	0.00	2.12	0.00
169	170	87.90	-1141.67	-3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
170	170	87.90	-1141.67	-3.28	-406.59	0	-1550.94	1.8	15.74	1.8	0.00	2.12	0.00
170	171	89.00	-1141.67	0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ+

11/09/03

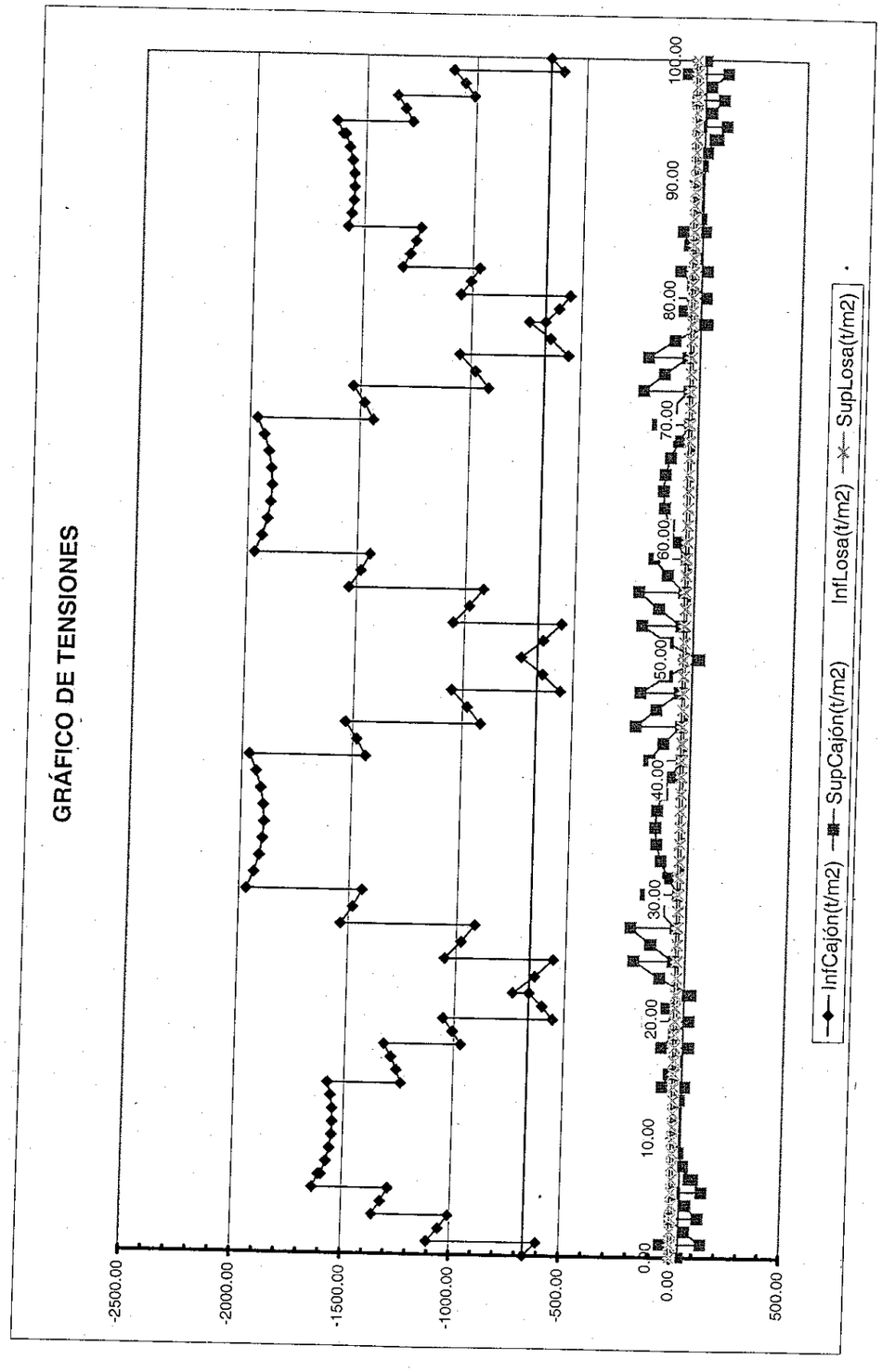
CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ+
Construcción sin gradiente en fase constructiva 1
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra	InfCajón	Fibra	SupCajón	Fibra	InfLosa	Fibra	SupLosa
						y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)
171	171	89.00	-1141.67	0.09	-404.84	0	-1548.27	1.8	11.67	1.8	0.00	2.12	0.00
171	172	90.10	-1141.67	3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
172	172	90.10	-1141.67	3.46	-406.79	0	-1551.24	1.8	16.21	1.8	0.00	2.12	0.00
172	173	91.20	-1141.67	6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
173	173	91.20	-1141.67	6.82	-412.44	0	-1559.85	1.8	29.37	1.8	0.00	2.12	0.00
173	174	92.30	-1141.67	10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
174	174	92.30	-1141.67	10.19	-421.79	0	-1574.10	1.8	51.15	1.8	0.00	2.12	0.00
174	175	93.40	-1141.67	13.55	-434.85	0	-1594.00	1.8	81.57	1.8	0.00	2.12	0.00
175	175	93.40	-1141.67	13.55	-434.85	0	-1605.29	1.8	96.86	1.8	0.00	2.12	0.00
175	176	94.50	-1141.67	16.92	-451.61	0	-1631.95	1.8	135.80	1.8	0.00	2.12	0.00
176	176	94.50	-944.83	16.92	-333.12	0	-1285.95	1.8	17.98	1.8	0.00	2.12	0.00
176	177	95.60	-944.83	20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
177	177	95.60	-944.83	20.29	-353.58	0	-1318.49	1.8	65.52	1.8	0.00	2.12	0.00
177	178	96.70	-944.83	23.65	-377.75	0	-1356.94	1.8	121.68	1.8	0.00	2.12	0.00
178	178	96.70	-747.99	23.65	-257.28	0	-1007.80	1.8	-0.73	1.8	0.00	2.12	0.00
178	179	97.80	-747.99	27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
179	179	97.80	-747.99	27.02	-285.15	0	-1052.13	1.8	64.03	1.8	0.00	2.12	0.00
179	180	98.90	-747.99	30.38	-316.72	0	-1102.35	1.8	137.39	1.8	0.00	2.12	0.00
180	180	98.90	-472.42	30.38	-142.56	0	-604.79	1.8	-46.79	1.8	0.00	2.12	0.00
180	181	100.00	-472.42	35.67	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ+

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ-

Construcción sin gradiente en fase constructiva 1

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-35.67	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
1	2	1.10	-522.14	-30.38	-161.39	0	-674.54	1.8	-42.83	1.8	0.00	2.12	0.00
2	2	1.10	-826.73	-30.38	-353.88	0	-1224.47	1.8	160.74	1.8	0.00	2.12	0.00
2	3	2.20	-826.73	-27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
3	3	2.20	-826.73	-27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
3	4	3.30	-826.73	-23.65	-294.44	0	-1129.92	1.8	22.62	1.8	0.00	2.12	0.00
4	4	3.30	-1044.29	-23.65	-427.59	0	-1515.81	1.8	157.92	1.8	0.00	2.12	0.00
4	5	4.40	-1044.29	-20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
5	5	4.40	-1044.29	-20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
5	6	5.50	-1044.29	-16.92	-382.96	0	-1444.82	1.8	54.21	1.8	0.00	2.12	0.00
6	6	5.50	-1261.85	-16.92	-513.93	0	-1827.24	1.8	184.44	1.8	0.00	2.12	0.00
6	7	6.60	-1261.85	-13.55	-497.17	0	-1800.58	1.8	145.49	1.8	0.00	2.12	0.00
7	7	6.60	-1261.85	-13.55	-497.17	0	-1786.99	1.8	128.69	1.8	0.00	2.12	0.00
7	8	7.70	-1261.85	-10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
8	8	7.70	-1261.85	-10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
8	9	8.80	-1261.85	-6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
9	9	8.80	-1261.85	-6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
9	10	9.90	-1261.85	-3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
10	10	9.90	-1261.85	-3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
10	11	11.00	-1261.85	-0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
11	11	11.00	-1261.85	-0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
11	12	12.10	-1261.85	3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
12	12	12.10	-1261.85	3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
12	13	13.20	-1261.85	6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
13	13	13.20	-1261.85	6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
13	14	14.30	-1261.85	10.01	-483.52	0	-1766.20	1.8	96.90	1.8	0.00	2.12	0.00
14	14	14.30	-1044.29	10.01	-352.55	0	-1396.45	1.8	-16.45	1.8	0.00	2.12	0.00
14	15	15.40	-1044.29	13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
15	15	15.40	-1044.29	13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
15	16	16.50	-1044.29	16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
16	16	16.50	-1044.29	16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
16	17	17.60	-1044.29	20.11	-402.67	0	-1476.17	1.8	100.01	1.8	0.00	2.12	0.00
17	17	17.60	-826.73	20.11	-269.09	0	-1089.60	1.8	-36.29	1.8	0.00	2.12	0.00
17	18	18.70	-826.73	23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
18	18	18.70	-826.73	23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
18	19	19.80	-826.73	26.84	-320.73	0	-1171.74	1.8	83.71	1.8	0.00	2.12	0.00
19	19	19.80	-522.14	26.84	-128.24	0	-621.81	1.8	-119.86	1.8	0.00	2.12	0.00
19	20	20.90	-522.14	30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
20	20	20.90	-522.14	30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
20	21	22.00	-522.14	39.07	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
21	1021	22.00	-565.66	-49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
21	22	23.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
22	22	23.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
22	23	24.80	-565.66	-34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
23	23	24.80	-870.24	-34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
23	24	26.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
24	24	26.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
24	25	27.60	-870.24	-25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
25	25	27.60	-1261.85	-25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
25	26	29.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
26	26	29.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
26	27	30.40	-1261.85	-17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
27	27	30.40	-1609.94	-17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
27	28	31.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
28	28	31.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
28	29	33.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
29	29	33.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
29	30	34.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
30	30	34.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
30	31	36.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
31	31	36.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
31	32	37.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
32	32	37.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
32	33	38.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
33	33	38.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
33	34	40.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
34	34	40.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
34	35	41.60	-1609.94	17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
35	35	41.60	-1261.85	17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
35	36	43.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
36	36	43.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
36	37	44.40	-1261.85	25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
37	37	44.40	-870.24	25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
37	38	45.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
38	38	45.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ-
Construcción sin gradiente en fase constructiva 1
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-870.24	34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
39	39	47.20	-565.66	34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
39	40	48.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
40	40	48.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
40	41	50.00	-565.66	49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
41	1041	50.00	-565.66	-49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
41	42	51.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
42	42	51.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
42	43	52.80	-565.66	-34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
43	43	52.80	-870.24	-34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
43	44	54.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
44	44	54.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
44	45	55.60	-870.24	-25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
45	45	55.60	-1261.85	-25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
45	46	57.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
46	46	57.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
46	47	58.40	-1261.85	-17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
47	47	58.40	-1609.94	-17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
47	48	59.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
48	48	59.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
48	49	61.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
49	49	61.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
49	50	62.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
50	50	62.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
50	51	64.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
51	51	64.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
51	52	65.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
52	52	65.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
52	53	66.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
53	53	66.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
53	54	68.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
54	54	68.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
54	55	69.60	-1609.94	17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
55	55	69.60	-1261.85	17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
55	56	71.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
56	56	71.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
56	57	72.40	-1261.85	25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
57	57	72.40	-870.24	25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
57	58	73.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
58	58	73.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
58	59	75.20	-870.24	34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
59	59	75.20	-565.66	34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
59	60	76.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
60	60	76.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
60	61	78.00	-565.66	49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
61	1061	78.00	-522.14	-39.07	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
61	62	79.10	-522.14	-30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
62	62	79.10	-522.14	-30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
62	63	80.20	-522.14	-26.84	-128.24	0	-621.81	1.8	-119.86	1.8	0.00	2.12	0.00
63	63	80.20	-826.73	-26.84	-320.73	0	-1171.74	1.8	83.71	1.8	0.00	2.12	0.00
63	64	81.30	-826.73	-23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
64	64	81.30	-826.73	-23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
64	65	82.40	-826.73	-20.11	-269.09	0	-1089.60	1.8	-36.29	1.8	0.00	2.12	0.00
65	65	82.40	-1044.29	-20.11	-402.24	0	-1475.49	1.8	99.01	1.8	0.00	2.12	0.00
65	66	83.50	-1044.29	-16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
66	66	83.50	-1044.29	-16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
66	67	84.60	-1044.29	-13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
67	67	84.60	-1044.29	-13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
67	68	85.70	-1044.29	-10.01	-352.55	0	-1396.45	1.8	-16.45	1.8	0.00	2.12	0.00
68	68	85.70	-1261.85	-10.01	-483.52	0	-1766.20	1.8	96.90	1.8	0.00	2.12	0.00
68	69	86.80	-1261.85	-6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
69	69	86.80	-1261.85	-6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
69	70	87.90	-1261.85	-3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
70	70	87.90	-1261.85	-3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
70	71	89.00	-1261.85	0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
71	71	89.00	-1261.85	0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
71	72	90.10	-1261.85	3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
72	72	90.10	-1261.85	3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
72	73	91.20	-1261.85	6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
73	73	91.20	-1261.85	6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
73	74	92.30	-1261.85	10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
74	74	92.30	-1261.85	10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
74	75	93.40	-1261.85	13.55	-497.17	0	-1786.99	1.8	128.69	1.8	0.00	2.12	0.00
75	75	93.40	-1261.85	13.55	-497.17	0	-1800.58	1.8	145.49	1.8	0.00	2.12	0.00
75	76	94.50	-1261.85	16.92	-513.93	0	-1827.24	1.8	184.44	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ-
Construcción sin gradiente en fase constructiva 1
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	16.92	-382.96	0	-1444.82	1.8	54.21	1.8	0.00	2.12	0.00
76	77	95.60	-1044.29	20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
77	77	95.60	-1044.29	20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
77	78	96.70	-1044.29	23.65	-427.59	0	-1515.81	1.8	157.92	1.8	0.00	2.12	0.00
78	78	96.70	-826.73	23.65	-294.44	0	-1129.92	1.8	22.62	1.8	0.00	2.12	0.00
78	79	97.80	-826.73	27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
79	79	97.80	-826.73	27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
79	80	98.90	-826.73	30.38	-353.88	0	-1224.47	1.8	160.74	1.8	0.00	2.12	0.00
80	80	98.90	-522.14	30.38	-161.39	0	-674.54	1.8	-42.83	1.8	0.00	2.12	0.00
80	81	100.00	-522.14	35.67	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	101	0.00	-522.14	-35.67	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	102	1.10	-522.14	-30.38	-161.39	0	-674.54	1.8	-42.83	1.8	0.00	2.12	0.00
102	102	1.10	-826.73	-30.38	-353.88	0	-1224.47	1.8	160.74	1.8	0.00	2.12	0.00
102	103	2.20	-826.73	-27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
103	103	2.20	-826.73	-27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
103	104	3.30	-826.73	-23.65	-294.44	0	-1129.92	1.8	22.62	1.8	0.00	2.12	0.00
104	104	3.30	-1044.29	-23.65	-427.59	0	-1515.81	1.8	157.92	1.8	0.00	2.12	0.00
104	105	4.40	-1044.29	-20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
105	105	4.40	-1044.29	-20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
105	106	5.50	-1044.29	-16.92	-382.96	0	-1444.82	1.8	54.21	1.8	0.00	2.12	0.00
106	106	5.50	-1261.85	-16.92	-513.93	0	-1827.24	1.8	184.44	1.8	0.00	2.12	0.00
106	107	6.60	-1261.85	-13.55	-497.17	0	-1800.58	1.8	145.49	1.8	0.00	2.12	0.00
107	107	6.60	-1261.85	-13.55	-497.17	0	-1786.99	1.8	128.69	1.8	0.00	2.12	0.00
107	108	7.70	-1261.85	-10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
108	108	7.70	-1261.85	-10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
108	109	8.80	-1261.85	-6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
109	109	8.80	-1261.85	-6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
109	110	9.90	-1261.85	-3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
110	110	9.90	-1261.85	-3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
110	111	11.00	-1261.85	-0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
111	111	11.00	-1261.85	-0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
111	112	12.10	-1261.85	3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
112	112	12.10	-1261.85	3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
112	113	13.20	-1261.85	6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
113	113	13.20	-1261.85	6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
113	114	14.30	-1261.85	10.01	-483.52	0	-1766.20	1.8	96.90	1.8	0.00	2.12	0.00
114	114	14.30	-1044.29	10.01	-352.55	0	-1396.45	1.8	-16.45	1.8	0.00	2.12	0.00
114	115	15.40	-1044.29	13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
115	115	15.40	-1044.29	13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
115	116	16.50	-1044.29	16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
116	116	16.50	-1044.29	16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
116	117	17.60	-1044.29	20.11	-402.67	0	-1476.17	1.8	100.01	1.8	0.00	2.12	0.00
117	117	17.60	-826.73	20.11	-269.09	0	-1089.60	1.8	-36.29	1.8	0.00	2.12	0.00
117	118	18.70	-826.73	23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
118	118	18.70	-826.73	23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
118	119	19.80	-826.73	26.84	-320.73	0	-1171.74	1.8	83.71	1.8	0.00	2.12	0.00
119	119	19.80	-522.14	26.84	-128.24	0	-621.81	1.8	-119.86	1.8	0.00	2.12	0.00
119	120	20.90	-522.14	30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
120	120	20.90	-522.14	30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
120	121	22.00	-522.14	39.07	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
121	1121	22.00	-565.66	-49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
121	122	23.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
122	122	23.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
122	123	24.80	-565.66	-34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
123	123	24.80	-870.24	-34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
123	124	26.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
124	124	26.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
124	125	27.60	-870.24	-25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
125	125	27.60	-1261.85	-25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
125	126	29.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
126	126	29.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
126	127	30.40	-1261.85	-17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
127	127	30.40	-1609.94	-17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
127	128	31.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
128	128	31.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
128	129	33.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
129	129	33.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
129	130	34.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
130	130	34.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
130	131	36.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
131	131	36.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
131	132	37.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
132	132	37.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
132	133	38.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
133	133	38.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ-

Construcción sin gradiente en fase constructiva 1

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
134	134	40.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
134	135	41.60	-1609.94	17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
135	135	41.60	-1261.85	17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
135	136	43.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
136	136	43.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
136	137	44.40	-1261.85	25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
137	137	44.40	-870.24	25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
137	138	45.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
138	138	45.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
138	139	47.20	-870.24	34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
139	139	47.20	-565.66	34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
139	140	48.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
140	140	48.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
140	141	50.00	-565.66	49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
141	1141	50.00	-565.66	-49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
141	142	51.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
142	142	51.40	-565.66	-38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
142	143	52.80	-565.66	-34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
143	143	52.80	-870.24	-34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
143	144	54.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
144	144	54.20	-870.24	-29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
144	145	55.60	-870.24	-25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
145	145	55.60	-1261.85	-25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
145	146	57.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
146	146	57.00	-1261.85	-21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
146	147	58.40	-1261.85	-17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
147	147	58.40	-1609.94	-17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
147	148	59.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
148	148	59.80	-1609.94	-12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
148	149	61.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
149	149	61.20	-1609.94	-8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
149	150	62.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
150	150	62.60	-1609.94	-4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
150	151	64.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
151	151	64.00	-1609.94	0.00	-542.14	0	-2139.50	1.8	-50.53	1.8	0.00	2.12	0.00
151	152	65.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
152	152	65.40	-1609.94	4.28	-545.14	0	-2144.07	1.8	-43.54	1.8	0.00	2.12	0.00
152	153	66.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
153	153	66.80	-1609.94	8.57	-554.13	0	-2157.77	1.8	-22.60	1.8	0.00	2.12	0.00
153	154	68.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
154	154	68.20	-1609.94	12.85	-569.13	0	-2180.63	1.8	12.34	1.8	0.00	2.12	0.00
154	155	69.60	-1609.94	17.14	-590.12	0	-2212.61	1.8	61.24	1.8	0.00	2.12	0.00
155	155	69.60	-1261.85	17.14	-391.01	0	-1631.72	1.8	-101.19	1.8	0.00	2.12	0.00
155	156	71.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
156	156	71.00	-1261.85	21.42	-418.00	0	-1674.65	1.8	-38.47	1.8	0.00	2.12	0.00
156	157	72.40	-1261.85	25.70	-450.98	0	-1727.11	1.8	38.16	1.8	0.00	2.12	0.00
157	157	72.40	-870.24	25.70	-219.15	0	-1044.98	1.8	-187.16	1.8	0.00	2.12	0.00
157	158	73.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
158	158	73.80	-870.24	29.99	-258.14	0	-1106.99	1.8	-96.56	1.8	0.00	2.12	0.00
158	159	75.20	-870.24	34.27	-303.12	0	-1178.54	1.8	7.96	1.8	0.00	2.12	0.00
159	159	75.20	-565.66	34.27	-113.67	0	-633.46	1.8	-188.53	1.8	0.00	2.12	0.00
159	160	76.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
160	160	76.60	-565.66	38.56	-164.65	0	-714.55	1.8	-70.07	1.8	0.00	2.12	0.00
160	161	78.00	-565.66	49.84	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
161	1161	78.00	-522.14	-39.07	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
161	162	79.10	-522.14	-30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
162	162	79.10	-522.14	-30.20	-159.62	0	-671.72	1.8	-46.94	1.8	0.00	2.12	0.00
162	163	80.20	-522.14	-26.84	-128.24	0	-621.81	1.8	-119.86	1.8	0.00	2.12	0.00
163	163	80.20	-826.73	-26.84	-320.73	0	-1171.74	1.8	83.71	1.8	0.00	2.12	0.00
163	164	81.30	-826.73	-23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
164	164	81.30	-826.73	-23.47	-293.06	0	-1127.72	1.8	19.41	1.8	0.00	2.12	0.00
164	165	82.40	-826.73	-20.11	-269.09	0	-1089.60	1.8	-36.29	1.8	0.00	2.12	0.00
165	165	82.40	-1044.29	-20.11	-402.24	0	-1475.49	1.8	99.01	1.8	0.00	2.12	0.00
165	166	83.50	-1044.29	-16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
166	166	83.50	-1044.29	-16.74	-381.98	0	-1443.26	1.8	51.94	1.8	0.00	2.12	0.00
166	167	84.60	-1044.29	-13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
167	167	84.60	-1044.29	-13.37	-365.41	0	-1416.90	1.8	13.43	1.8	0.00	2.12	0.00
167	168	85.70	-1044.29	-10.01	-352.55	0	-1396.45	1.8	-16.45	1.8	0.00	2.12	0.00
168	168	85.70	-1261.85	-10.01	-483.52	0	-1766.20	1.8	96.90	1.8	0.00	2.12	0.00
168	169	86.80	-1261.85	-6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
169	169	86.80	-1261.85	-6.64	-474.37	0	-1752.25	1.8	75.58	1.8	0.00	2.12	0.00
169	170	87.90	-1261.85	-3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
170	170	87.90	-1261.85	-3.28	-468.91	0	-1743.93	1.8	62.86	1.8	0.00	2.12	0.00
170	171	89.00	-1261.85	0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F1.T0.MZ-

Construcción sin gradiente en fase constructiva 1

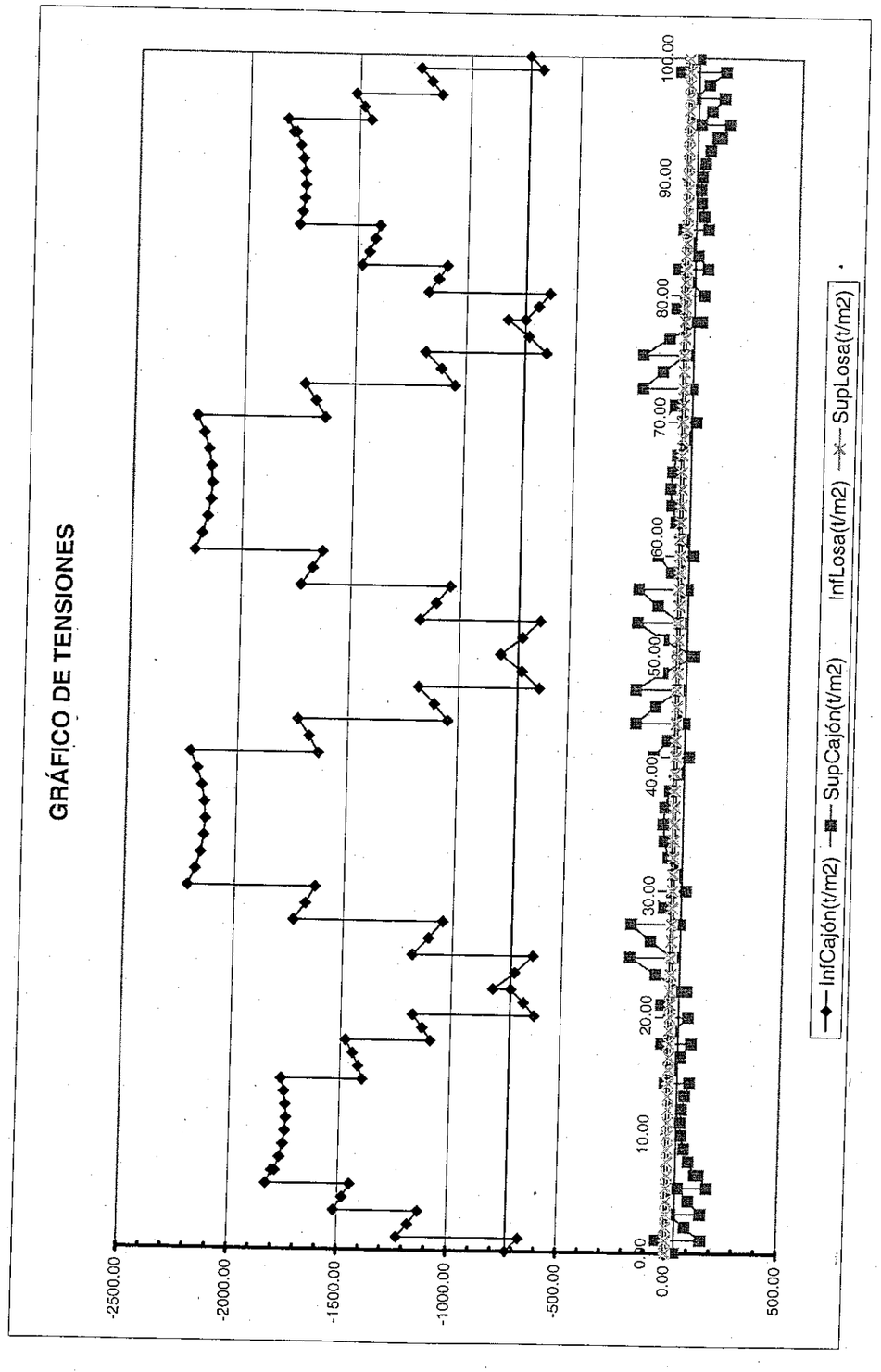
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	0.09	-467.16	0	-1741.27	1.8	58.79	1.8	0.00	2.12	0.00
171	172	90.10	-1261.85	3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
172	172	90.10	-1261.85	3.46	-469.11	0	-1744.24	1.8	63.33	1.8	0.00	2.12	0.00
172	173	91.20	-1261.85	6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
173	173	91.20	-1261.85	6.82	-474.76	0	-1752.85	1.8	76.49	1.8	0.00	2.12	0.00
173	174	92.30	-1261.85	10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
174	174	92.30	-1261.85	10.19	-484.11	0	-1767.09	1.8	98.27	1.8	0.00	2.12	0.00
174	175	93.40	-1261.85	13.55	-497.17	0	-1786.99	1.8	128.69	1.8	0.00	2.12	0.00
175	175	93.40	-1261.85	13.55	-497.17	0	-1800.58	1.8	145.49	1.8	0.00	2.12	0.00
175	176	94.50	-1261.85	16.92	-513.93	0	-1827.24	1.8	184.44	1.8	0.00	2.12	0.00
176	176	94.50	-1044.29	16.92	-382.96	0	-1444.82	1.8	54.21	1.8	0.00	2.12	0.00
176	177	95.60	-1044.29	20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
177	177	95.60	-1044.29	20.29	-403.42	0	-1477.36	1.8	101.76	1.8	0.00	2.12	0.00
177	178	96.70	-1044.29	23.65	-427.59	0	-1515.81	1.8	157.92	1.8	0.00	2.12	0.00
178	178	96.70	-826.73	23.65	-294.44	0	-1129.92	1.8	22.62	1.8	0.00	2.12	0.00
178	179	97.80	-826.73	27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
179	179	97.80	-826.73	27.02	-322.31	0	-1174.25	1.8	87.38	1.8	0.00	2.12	0.00
179	180	98.90	-826.73	30.38	-353.88	0	-1224.47	1.8	160.74	1.8	0.00	2.12	0.00
180	180	98.90	-522.14	30.38	-161.39	0	-674.54	1.8	-42.83	1.8	0.00	2.12	0.00
180	181	100.00	-522.14	35.67	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F1.T0.MZ-

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ+

Construcción sin gradiente en fase constructiva 2

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-46.89	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
1	2	1.10	-472.42	-40.48	-130.84	0	-586.15	1.8	-74.02	1.8	0.00	2.12	0.00
2	2	1.10	-747.99	-40.48	-305.00	0	-1083.70	1.8	110.15	1.8	0.00	2.12	0.00
2	3	2.20	-747.99	-36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
3	3	2.20	-747.99	-36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
3	4	3.30	-747.99	-31.50	-225.81	0	-957.74	1.8	-73.86	1.8	0.00	2.12	0.00
4	4	3.30	-944.83	-31.50	-346.28	0	-1306.88	1.8	48.56	1.8	0.00	2.12	0.00
4	5	4.40	-944.83	-27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
5	5	4.40	-944.83	-27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
5	6	5.50	-944.83	-22.53	-286.84	0	-1212.34	1.8	-89.56	1.8	0.00	2.12	0.00
6	6	5.50	-1141.67	-22.53	-405.33	0	-1558.33	1.8	28.26	1.8	0.00	2.12	0.00
6	7	6.60	-1141.67	-18.04	-383.01	0	-1522.83	1.8	-23.60	1.8	0.00	2.12	0.00
7	7	6.60	-1141.67	-18.04	-383.01	0	-1515.01	1.8	-39.19	1.8	0.00	2.12	0.00
7	8	7.70	-1141.67	-13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
8	8	7.70	-1141.67	-13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
8	9	8.80	-1141.67	-9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
9	9	8.80	-1141.67	-9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
9	10	9.90	-1141.67	-4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
10	10	9.90	-1141.67	-4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
10	11	11.00	-1141.67	-0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
11	11	11.00	-1141.67	-0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
11	12	12.10	-1141.67	4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
12	12	12.10	-1141.67	4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
12	13	13.20	-1141.67	8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
13	13	13.20	-1141.67	8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
13	14	14.30	-1141.67	13.38	-365.04	0	-1487.62	1.8	-81.05	1.8	0.00	2.12	0.00
14	14	14.30	-944.83	13.38	-246.55	0	-1148.25	1.8	-183.18	1.8	0.00	2.12	0.00
14	15	15.40	-944.83	17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
15	15	15.40	-944.83	17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
15	16	16.50	-944.83	22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
16	16	16.50	-944.83	22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
16	17	17.60	-944.83	26.84	-313.30	0	-1254.42	1.8	-28.08	1.8	0.00	2.12	0.00
17	17	17.60	-747.99	26.84	-192.44	0	-904.66	1.8	-151.40	1.8	0.00	2.12	0.00
17	18	18.70	-747.99	31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
18	18	18.70	-747.99	31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
18	19	19.80	-747.99	35.82	-261.35	0	-1014.27	1.8	8.73	1.8	0.00	2.12	0.00
19	19	19.80	-472.42	35.82	-87.18	0	-516.72	1.8	-175.45	1.8	0.00	2.12	0.00
19	20	20.90	-472.42	40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
20	20	20.90	-472.42	40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
20	21	22.00	-472.42	50.29	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
21	1021	22.00	-511.78	-64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
21	22	23.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
22	22	23.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
22	23	24.80	-511.78	-45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
23	23	24.80	-787.36	-45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
23	24	26.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
24	24	26.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
24	25	27.60	-787.36	-34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
25	25	27.60	-1141.67	-34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
25	26	29.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
26	26	29.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
26	27	30.40	-1141.67	-22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
27	27	30.40	-1456.62	-22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
27	28	31.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
28	28	31.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
28	29	33.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
29	29	33.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
29	30	34.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
30	30	34.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
30	31	36.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
31	31	36.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
31	32	37.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
32	32	37.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
32	33	38.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
33	33	38.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
33	34	40.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
34	34	40.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
34	35	41.60	-1456.62	22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
35	35	41.60	-1141.67	22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
35	36	43.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
36	36	43.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
36	37	44.40	-1141.67	34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
37	37	44.40	-787.36	34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
37	38	45.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
38	38	45.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ+
Construcción sin gradiente en fase constructiva 2
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-787.36	45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
39	39	47.20	-511.78	45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
39	40	48.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
40	40	48.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
40	41	50.00	-511.78	64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
41	1041	50.00	-511.78	-64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
41	42	51.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
42	42	51.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
42	43	52.80	-511.78	-45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
43	43	52.80	-787.36	-45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
43	44	54.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
44	44	54.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
44	45	55.60	-787.36	-34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
45	45	55.60	-1141.67	-34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
45	46	57.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
46	46	57.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
46	47	58.40	-1141.67	-22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
47	47	58.40	-1456.62	-22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
47	48	59.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
48	48	59.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
48	49	61.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
49	49	61.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
49	50	62.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
50	50	62.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
50	51	64.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
51	51	64.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
51	52	65.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
52	52	65.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
52	53	66.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
53	53	66.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
53	54	68.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
54	54	68.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
54	55	69.60	-1456.62	22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
55	55	69.60	-1141.67	22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
55	56	71.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
56	56	71.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
56	57	72.40	-1141.67	34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
57	57	72.40	-787.36	34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
57	58	73.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
58	58	73.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
58	59	75.20	-787.36	45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
59	59	75.20	-511.78	45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
59	60	76.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
60	60	76.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
60	61	78.00	-511.78	64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
61	1061	78.00	-472.42	-50.29	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
61	62	79.10	-472.42	-40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
62	62	79.10	-472.42	-40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
62	63	80.20	-472.42	-35.82	-87.18	0	-516.72	1.8	-175.45	1.8	0.00	2.12	0.00
63	63	80.20	-747.99	-35.82	-261.35	0	-1014.27	1.8	8.73	1.8	0.00	2.12	0.00
63	64	81.30	-747.99	-31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
64	64	81.30	-747.99	-31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
64	65	82.40	-747.99	-26.84	-192.44	0	-904.66	1.8	-151.40	1.8	0.00	2.12	0.00
65	65	82.40	-944.83	-26.84	-312.91	0	-1253.80	1.8	-28.98	1.8	0.00	2.12	0.00
65	66	83.50	-944.83	-22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
66	66	83.50	-944.83	-22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
66	67	84.60	-944.83	-17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
67	67	84.60	-944.83	-17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
67	68	85.70	-944.83	-13.38	-246.55	0	-1148.25	1.8	-183.18	1.8	0.00	2.12	0.00
68	68	85.70	-1141.67	-13.38	-365.04	0	-1487.62	1.8	-81.05	1.8	0.00	2.12	0.00
68	69	86.80	-1141.67	-8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
69	69	86.80	-1141.67	-8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
69	70	87.90	-1141.67	-4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
70	70	87.90	-1141.67	-4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
70	71	89.00	-1141.67	0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
71	71	89.00	-1141.67	0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
71	72	90.10	-1141.67	4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
72	72	90.10	-1141.67	4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
72	73	91.20	-1141.67	9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
73	73	91.20	-1141.67	9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
73	74	92.30	-1141.67	13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
74	74	92.30	-1141.67	13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
74	75	93.40	-1141.67	18.04	-383.01	0	-1515.01	1.8	-39.19	1.8	0.00	2.12	0.00
75	75	93.40	-1141.67	18.04	-383.01	0	-1522.83	1.8	-23.60	1.8	0.00	2.12	0.00
75	76	94.50	-1141.67	22.53	-405.33	0	-1558.33	1.8	28.26	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F2.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ+
Construcción sin gradiente en fase constructiva 2
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	22.53	-286.84	0	-1212.34	1.8	-89.56	1.8	0.00	2.12	0.00
76	77	95.60	-944.83	27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
77	77	95.60	-944.83	27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
77	78	96.70	-944.83	31.50	-346.28	0	-1306.88	1.8	48.56	1.8	0.00	2.12	0.00
78	78	96.70	-747.99	31.50	-225.81	0	-957.74	1.8	-73.86	1.8	0.00	2.12	0.00
78	79	97.80	-747.99	36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
79	79	97.80	-747.99	36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
79	80	98.90	-747.99	40.48	-305.00	0	-1083.70	1.8	110.15	1.8	0.00	2.12	0.00
80	80	98.90	-472.42	40.48	-130.84	0	-586.15	1.8	-74.02	1.8	0.00	2.12	0.00
80	81	100.00	-472.42	46.89	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	101	0.00	-472.42	-46.89	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	102	1.10	-472.42	-40.48	-130.84	0	-586.15	1.8	-74.02	1.8	0.00	2.12	0.00
102	102	1.10	-747.99	-40.48	-305.00	0	-1083.70	1.8	110.15	1.8	0.00	2.12	0.00
102	103	2.20	-747.99	-36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
103	103	2.20	-747.99	-36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
103	104	3.30	-747.99	-31.50	-225.81	0	-957.74	1.8	-73.86	1.8	0.00	2.12	0.00
104	104	3.30	-944.83	-31.50	-346.28	0	-1306.88	1.8	48.56	1.8	0.00	2.12	0.00
104	105	4.40	-944.83	-27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
105	105	4.40	-944.83	-27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
105	106	5.50	-944.83	-22.53	-286.84	0	-1212.34	1.8	-89.56	1.8	0.00	2.12	0.00
106	106	5.50	-1141.67	-22.53	-405.33	0	-1558.33	1.8	28.26	1.8	0.00	2.12	0.00
106	107	6.60	-1141.67	-18.04	-383.01	0	-1522.83	1.8	-23.60	1.8	0.00	2.12	0.00
107	107	6.60	-1141.67	-18.04	-383.01	0	-1515.01	1.8	-39.19	1.8	0.00	2.12	0.00
107	108	7.70	-1141.67	-13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
108	108	7.70	-1141.67	-13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
108	109	8.80	-1141.67	-9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
109	109	8.80	-1141.67	-9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
109	110	9.90	-1141.67	-4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
110	110	9.90	-1141.67	-4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
110	111	11.00	-1141.67	-0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
111	111	11.00	-1141.67	-0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
111	112	12.10	-1141.67	4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
112	112	12.10	-1141.67	4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
112	113	13.20	-1141.67	8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
113	113	13.20	-1141.67	8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
113	114	14.30	-1141.67	13.38	-365.04	0	-1487.62	1.8	-81.05	1.8	0.00	2.12	0.00
114	114	14.30	-944.83	13.38	-246.55	0	-1148.25	1.8	-183.18	1.8	0.00	2.12	0.00
114	115	15.40	-944.83	17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
115	115	15.40	-944.83	17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
115	116	16.50	-944.83	22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
116	116	16.50	-944.83	22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
116	117	17.60	-944.83	26.84	-313.30	0	-1254.42	1.8	-28.08	1.8	0.00	2.12	0.00
117	117	17.60	-747.99	26.84	-192.44	0	-904.66	1.8	-151.40	1.8	0.00	2.12	0.00
117	118	18.70	-747.99	31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
118	118	18.70	-747.99	31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
118	119	19.80	-747.99	35.82	-261.35	0	-1014.27	1.8	8.73	1.8	0.00	2.12	0.00
119	119	19.80	-472.42	35.82	-87.18	0	-516.72	1.8	-175.45	1.8	0.00	2.12	0.00
119	120	20.90	-472.42	40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
120	120	20.90	-472.42	40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
120	121	22.00	-472.42	50.29	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
121	1121	22.00	-511.78	-64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
121	122	23.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
122	122	23.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
122	123	24.80	-511.78	-45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
123	123	24.80	-787.36	-45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
123	124	26.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
124	124	26.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
124	125	27.60	-787.36	-34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
125	125	27.60	-1141.67	-34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
125	126	29.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
126	126	29.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
126	127	30.40	-1141.67	-22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
127	127	30.40	-1456.62	-22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
127	128	31.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
128	128	31.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
128	129	33.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
129	129	33.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
129	130	34.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
130	130	34.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
130	131	36.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
131	131	36.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
131	132	37.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
132	132	37.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
132	133	38.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
133	133	38.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ+

Construcción sin gradiente en fase constructiva 2

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
134	134	40.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
134	135	41.60	-1456.62	22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
135	135	41.60	-1141.67	22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
135	136	43.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
136	136	43.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
136	137	44.40	-1141.67	34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
137	137	44.40	-787.36	34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
137	138	45.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
138	138	45.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
138	139	47.20	-787.36	45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
139	139	47.20	-511.78	45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
139	140	48.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
140	140	48.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
140	141	50.00	-511.78	64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
141	1141	50.00	-511.78	-64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
141	142	51.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
142	142	51.40	-511.78	-51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
142	143	52.80	-511.78	-45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
143	143	52.80	-787.36	-45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
143	144	54.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
144	144	54.20	-787.36	-39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
144	145	55.60	-787.36	-34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
145	145	55.60	-1141.67	-34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
145	146	57.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
146	146	57.00	-1141.67	-28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
146	147	58.40	-1141.67	-22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
147	147	58.40	-1456.62	-22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
147	148	59.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
148	148	59.80	-1456.62	-17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
148	149	61.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
149	149	61.20	-1456.62	-11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
149	150	62.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
150	150	62.60	-1456.62	-5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
150	151	64.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
151	151	64.00	-1456.62	0.00	-361.52	0	-1739.19	1.8	-346.18	1.8	0.00	2.12	0.00
151	152	65.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
152	152	65.40	-1456.62	5.71	-365.52	0	-1745.29	1.8	-336.86	1.8	0.00	2.12	0.00
152	153	66.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
153	153	66.80	-1456.62	11.43	-377.51	0	-1763.56	1.8	-308.93	1.8	0.00	2.12	0.00
153	154	68.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
154	154	68.20	-1456.62	17.13	-397.51	0	-1794.03	1.8	-262.35	1.8	0.00	2.12	0.00
154	155	69.60	-1456.62	22.85	-425.49	0	-1836.67	1.8	-197.17	1.8	0.00	2.12	0.00
155	155	69.60	-1141.67	22.85	-245.34	0	-1303.85	1.8	-343.50	1.8	0.00	2.12	0.00
155	156	71.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
156	156	71.00	-1141.67	28.56	-281.33	0	-1361.09	1.8	-259.87	1.8	0.00	2.12	0.00
156	157	72.40	-1141.67	34.27	-325.31	0	-1431.05	1.8	-157.68	1.8	0.00	2.12	0.00
157	157	72.40	-787.36	34.27	-115.56	0	-813.88	1.8	-361.54	1.8	0.00	2.12	0.00
157	158	73.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
158	158	73.80	-787.36	39.99	-167.54	0	-896.56	1.8	-240.76	1.8	0.00	2.12	0.00
158	159	75.20	-787.36	45.69	-227.51	0	-991.95	1.8	-101.40	1.8	0.00	2.12	0.00
159	159	75.20	-511.78	45.69	-56.10	0	-498.78	1.8	-279.18	1.8	0.00	2.12	0.00
159	160	76.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
160	160	76.60	-511.78	51.41	-124.08	0	-606.91	1.8	-121.21	1.8	0.00	2.12	0.00
160	161	78.00	-511.78	64.12	-204.95	0	-735.55	1.8	66.70	1.8	0.00	2.12	0.00
161	1161	78.00	-472.42	-50.29	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
161	162	79.10	-472.42	-40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
162	162	79.10	-472.42	-40.30	-129.07	0	-583.34	1.8	-78.13	1.8	0.00	2.12	0.00
162	163	80.20	-472.42	-35.82	-87.18	0	-516.72	1.8	-175.45	1.8	0.00	2.12	0.00
163	163	80.20	-747.99	-35.82	-261.35	0	-1014.27	1.8	8.73	1.8	0.00	2.12	0.00
163	164	81.30	-747.99	-31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
164	164	81.30	-747.99	-31.32	-224.43	0	-955.55	1.8	-77.06	1.8	0.00	2.12	0.00
164	165	82.40	-747.99	-26.84	-192.44	0	-904.66	1.8	-151.40	1.8	0.00	2.12	0.00
165	165	82.40	-944.83	-26.84	-312.91	0	-1253.80	1.8	-28.98	1.8	0.00	2.12	0.00
165	166	83.50	-944.83	-22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
166	166	83.50	-944.83	-22.35	-285.86	0	-1210.78	1.8	-91.84	1.8	0.00	2.12	0.00
166	167	84.60	-944.83	-17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
167	167	84.60	-944.83	-17.86	-263.73	0	-1175.58	1.8	-143.26	1.8	0.00	2.12	0.00
167	168	85.70	-944.83	-13.38	-246.55	0	-1148.25	1.8	-183.18	1.8	0.00	2.12	0.00
168	168	85.70	-1141.67	-13.38	-365.04	0	-1487.62	1.8	-81.05	1.8	0.00	2.12	0.00
168	169	86.80	-1141.67	-8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
169	169	86.80	-1141.67	-8.88	-352.81	0	-1468.99	1.8	-109.53	1.8	0.00	2.12	0.00
169	170	87.90	-1141.67	-4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
170	170	87.90	-1141.67	-4.40	-345.50	0	-1457.85	1.8	-126.56	1.8	0.00	2.12	0.00
170	171	89.00	-1141.67	0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F2.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ+

Construcción sin gradiente en fase constructiva 2

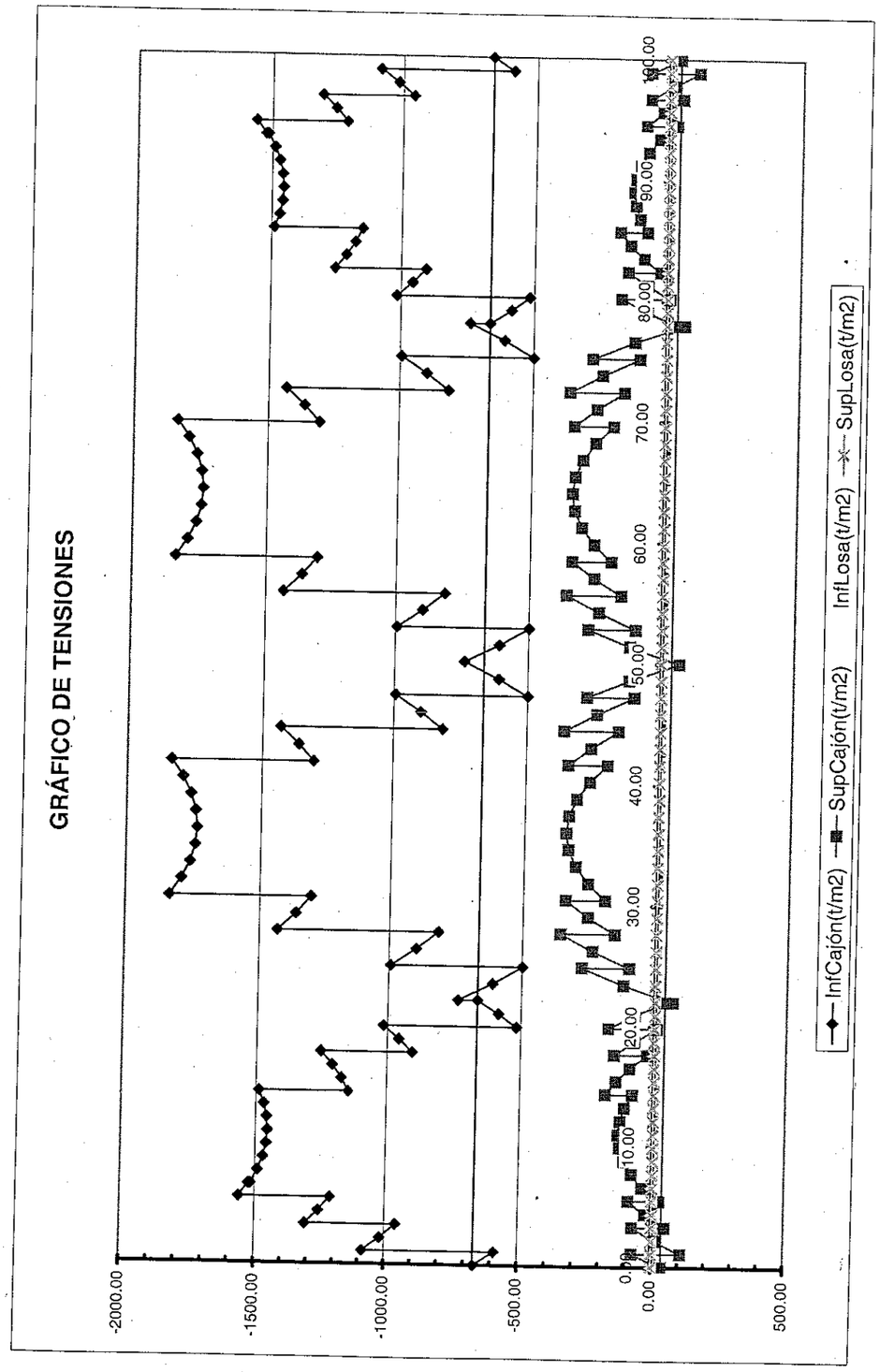
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	0.09	-343.13	0	-1454.24	1.8	-132.08	1.8	0.00	2.12	0.00
171	172	90.10	-1141.67	4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
172	172	90.10	-1141.67	4.58	-345.70	0	-1458.15	1.8	-126.10	1.8	0.00	2.12	0.00
172	173	91.20	-1141.67	9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
173	173	91.20	-1141.67	9.06	-353.20	0	-1469.58	1.8	-108.63	1.8	0.00	2.12	0.00
173	174	92.30	-1141.67	13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
174	174	92.30	-1141.67	13.56	-365.63	0	-1488.52	1.8	-79.67	1.8	0.00	2.12	0.00
174	175	93.40	-1141.67	18.04	-383.01	0	-1515.01	1.8	-39.19	1.8	0.00	2.12	0.00
175	175	93.40	-1141.67	18.04	-383.01	0	-1522.83	1.8	-23.60	1.8	0.00	2.12	0.00
175	176	94.50	-1141.67	22.53	-405.33	0	-1558.33	1.8	28.26	1.8	0.00	2.12	0.00
176	176	94.50	-944.83	22.53	-286.84	0	-1212.34	1.8	-89.56	1.8	0.00	2.12	0.00
176	177	95.60	-944.83	27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
177	177	95.60	-944.83	27.02	-314.09	0	-1255.68	1.8	-26.24	1.8	0.00	2.12	0.00
177	178	96.70	-944.83	31.50	-346.28	0	-1306.88	1.8	48.56	1.8	0.00	2.12	0.00
178	178	96.70	-747.99	31.50	-225.81	0	-957.74	1.8	-73.86	1.8	0.00	2.12	0.00
178	179	97.80	-747.99	36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
179	179	97.80	-747.99	36.00	-262.93	0	-1016.79	1.8	12.40	1.8	0.00	2.12	0.00
179	180	98.90	-747.99	40.48	-305.00	0	-1083.70	1.8	110.15	1.8	0.00	2.12	0.00
180	180	98.90	-472.42	40.48	-130.84	0	-586.15	1.8	-74.02	1.8	0.00	2.12	0.00
180	181	100.00	-472.42	46.89	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F2.T0.MZ+

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ-
Construcción sin gradiente en fase constructiva 2
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-46.89	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
1	2	1.10	-522.14	-40.48	-149.67	0	-655.90	1.8	-70.06	1.8	0.00	2.12	0.00
2	2	1.10	-826.73	-40.48	-342.16	0	-1205.82	1.8	133.50	1.8	0.00	2.12	0.00
2	3	2.20	-826.73	-36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
3	3	2.20	-826.73	-36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
3	4	3.30	-826.73	-31.50	-262.97	0	-1079.86	1.8	-50.51	1.8	0.00	2.12	0.00
4	4	3.30	-1044.29	-31.50	-396.12	0	-1465.75	1.8	84.79	1.8	0.00	2.12	0.00
4	5	4.40	-1044.29	-27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
5	5	4.40	-1044.29	-27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
5	6	5.50	-1044.29	-22.53	-336.68	0	-1371.21	1.8	-53.33	1.8	0.00	2.12	0.00
6	6	5.50	-1261.85	-22.53	-467.65	0	-1753.62	1.8	76.90	1.8	0.00	2.12	0.00
6	7	6.60	-1261.85	-18.04	-445.33	0	-1718.12	1.8	25.03	1.8	0.00	2.12	0.00
7	7	6.60	-1261.85	-18.04	-445.33	0	-1708.00	1.8	7.94	1.8	0.00	2.12	0.00
7	8	7.70	-1261.85	-13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
8	8	7.70	-1261.85	-13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
8	9	8.80	-1261.85	-9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
9	9	8.80	-1261.85	-9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
9	10	9.90	-1261.85	-4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
10	10	9.90	-1261.85	-4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
10	11	11.00	-1261.85	-0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
11	11	11.00	-1261.85	-0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
11	12	12.10	-1261.85	4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
12	12	12.10	-1261.85	4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
12	13	13.20	-1261.85	8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
13	13	13.20	-1261.85	8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
13	14	14.30	-1261.85	13.38	-427.36	0	-1680.62	1.8	-33.92	1.8	0.00	2.12	0.00
14	14	14.30	-1044.29	13.38	-296.39	0	-1307.12	1.8	-146.95	1.8	0.00	2.12	0.00
14	15	15.40	-1044.29	17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
15	15	15.40	-1044.29	17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
15	16	16.50	-1044.29	22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
16	16	16.50	-1044.29	22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
16	17	17.60	-1044.29	26.84	-363.18	0	-1413.36	1.8	8.25	1.8	0.00	2.12	0.00
17	17	17.60	-826.73	26.84	-229.60	0	-1026.78	1.8	-128.05	1.8	0.00	2.12	0.00
17	18	18.70	-826.73	31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
18	18	18.70	-826.73	31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
18	19	19.80	-826.73	35.82	-298.51	0	-1136.39	1.8	32.07	1.8	0.00	2.12	0.00
19	19	19.80	-522.14	35.82	-106.02	0	-586.47	1.8	-171.49	1.8	0.00	2.12	0.00
19	20	20.90	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
20	20	20.90	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
20	21	22.00	-522.14	50.29	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
21	1021	22.00	-565.66	-64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
21	22	23.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
22	22	23.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
22	23	24.80	-565.66	-45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
23	23	24.80	-870.24	-45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
23	24	26.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
24	24	26.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
24	25	27.60	-870.24	-34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
25	25	27.60	-1261.85	-34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
25	26	29.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
26	26	29.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
26	27	30.40	-1261.85	-22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
27	27	30.40	-1609.94	-22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
27	28	31.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
28	28	31.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
28	29	33.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
29	29	33.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
29	30	34.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
30	30	34.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
30	31	36.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
31	31	36.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
31	32	37.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
32	32	37.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
32	33	38.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
33	33	38.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
33	34	40.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
34	34	40.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
34	35	41.60	-1609.94	22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
35	35	41.60	-1261.85	22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
35	36	43.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
36	36	43.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
36	37	44.40	-1261.85	34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
37	37	44.40	-870.24	34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
37	38	45.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
38	38	45.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ-

Construcción sin gradiente en fase constructiva 2

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-870.24	45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
39	39	47.20	-565.66	45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
39	40	48.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
40	40	48.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
40	41	50.00	-565.66	64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
41	1041	50.00	-565.66	-64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
41	42	51.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
42	42	51.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
42	43	52.80	-565.66	-45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
43	43	52.80	-870.24	-45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
43	44	54.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
44	44	54.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
44	45	55.60	-870.24	-34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
45	45	55.60	-1261.85	-34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
45	46	57.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
46	46	57.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
46	47	58.40	-1261.85	-22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
47	47	58.40	-1609.94	-22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
47	48	59.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
48	48	59.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
48	49	61.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
49	49	61.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
49	50	62.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
50	50	62.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
50	51	64.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
51	51	64.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
51	52	65.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
52	52	65.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
52	53	66.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
53	53	66.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
53	54	68.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
54	54	68.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
54	55	69.60	-1609.94	22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
55	55	69.60	-1261.85	22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
55	56	71.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
56	56	71.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
56	57	72.40	-1261.85	34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
57	57	72.40	-870.24	34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
57	58	73.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
58	58	73.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
58	59	75.20	-870.24	45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
59	59	75.20	-565.66	45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
59	60	76.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
60	60	76.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
60	61	78.00	-565.66	64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
61	1061	78.00	-522.14	-50.29	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
61	62	79.10	-522.14	-40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
62	62	79.10	-522.14	-40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
62	63	80.20	-522.14	-35.82	-106.02	0	-586.47	1.8	-171.49	1.8	0.00	2.12	0.00
63	63	80.20	-826.73	-35.82	-298.51	0	-1136.39	1.8	32.07	1.8	0.00	2.12	0.00
63	64	81.30	-826.73	-31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
64	64	81.30	-826.73	-31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
64	65	82.40	-826.73	-26.84	-229.60	0	-1026.78	1.8	-128.05	1.8	0.00	2.12	0.00
65	65	82.40	-1044.29	-26.84	-362.75	0	-1412.67	1.8	7.25	1.8	0.00	2.12	0.00
65	66	83.50	-1044.29	-22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
66	66	83.50	-1044.29	-22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
66	67	84.60	-1044.29	-17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
67	67	84.60	-1044.29	-17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
67	68	85.70	-1044.29	-13.38	-296.39	0	-1307.12	1.8	-146.95	1.8	0.00	2.12	0.00
68	68	85.70	-1261.85	-13.38	-427.36	0	-1680.62	1.8	-33.92	1.8	0.00	2.12	0.00
68	69	86.80	-1261.85	-8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
69	69	86.80	-1261.85	-8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
69	70	87.90	-1261.85	-4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
70	70	87.90	-1261.85	-4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
70	71	89.00	-1261.85	0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
71	71	89.00	-1261.85	0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
71	72	90.10	-1261.85	4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
72	72	90.10	-1261.85	4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
72	73	91.20	-1261.85	9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
73	73	91.20	-1261.85	9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
73	74	92.30	-1261.85	13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
74	74	92.30	-1261.85	13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
74	75	93.40	-1261.85	18.04	-445.33	0	-1708.00	1.8	7.94	1.8	0.00	2.12	0.00
75	75	93.40	-1261.85	18.04	-445.33	0	-1718.12	1.8	25.03	1.8	0.00	2.12	0.00
75	76	94.50	-1261.85	22.53	-467.65	0	-1753.62	1.8	76.90	1.8	0.00	2.12	0.00

Combi_to.xls Programa DINTEL PACADAR S.A. 11/09/03
CONST1.F2.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.MZ-

Construcción sin gradiente en fase constructiva 2

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	22.53	-336.68	0	-1371.21	1.8	-53.33	1.8	0.00	2.12	0.00
76	77	95.60	-1044.29	27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
77	77	95.60	-1044.29	27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
77	78	96.70	-1044.29	31.50	-396.12	0	-1465.75	1.8	84.79	1.8	0.00	2.12	0.00
78	78	96.70	-826.73	31.50	-262.97	0	-1079.86	1.8	-50.51	1.8	0.00	2.12	0.00
78	79	97.80	-826.73	36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
79	79	97.80	-826.73	36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
79	80	98.90	-826.73	40.48	-342.16	0	-1205.82	1.8	133.50	1.8	0.00	2.12	0.00
80	80	98.90	-522.14	40.48	-149.67	0	-655.90	1.8	-70.06	1.8	0.00	2.12	0.00
80	81	100.00	-522.14	46.89	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	101	0.00	-522.14	-46.89	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	102	1.10	-522.14	-40.48	-149.67	0	-655.90	1.8	-70.06	1.8	0.00	2.12	0.00
102	102	1.10	-826.73	-40.48	-342.16	0	-1205.82	1.8	133.50	1.8	0.00	2.12	0.00
102	103	2.20	-826.73	-36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
103	103	2.20	-826.73	-36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
103	104	3.30	-826.73	-31.50	-262.97	0	-1079.86	1.8	-50.51	1.8	0.00	2.12	0.00
104	104	3.30	-1044.29	-31.50	-396.12	0	-1465.75	1.8	84.79	1.8	0.00	2.12	0.00
104	105	4.40	-1044.29	-27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
105	105	4.40	-1044.29	-27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
105	106	5.50	-1044.29	-22.53	-336.68	0	-1371.21	1.8	-53.33	1.8	0.00	2.12	0.00
106	106	5.50	-1261.85	-22.53	-467.65	0	-1753.62	1.8	76.90	1.8	0.00	2.12	0.00
106	107	6.60	-1261.85	-18.04	-445.33	0	-1718.12	1.8	25.03	1.8	0.00	2.12	0.00
107	107	6.60	-1261.85	-18.04	-445.33	0	-1708.00	1.8	7.94	1.8	0.00	2.12	0.00
107	108	7.70	-1261.85	-13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
108	108	7.70	-1261.85	-13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
108	109	8.80	-1261.85	-9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
109	109	8.80	-1261.85	-9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
109	110	9.90	-1261.85	-4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
110	110	9.90	-1261.85	-4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
110	111	11.00	-1261.85	-0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
111	111	11.00	-1261.85	-0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
111	112	12.10	-1261.85	4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
112	112	12.10	-1261.85	4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
112	113	13.20	-1261.85	8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
113	113	13.20	-1261.85	8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
113	114	14.30	-1261.85	13.38	-427.36	0	-1680.62	1.8	-33.92	1.8	0.00	2.12	0.00
114	114	14.30	-1044.29	13.38	-296.39	0	-1307.12	1.8	-146.95	1.8	0.00	2.12	0.00
114	115	15.40	-1044.29	17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
115	115	15.40	-1044.29	17.86	-313.57	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
115	116	16.50	-1044.29	22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
116	116	16.50	-1044.29	22.35	-335.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
116	117	17.60	-1044.29	26.84	-363.18	0	-1413.36	1.8	8.25	1.8	0.00	2.12	0.00
117	117	17.60	-826.73	26.84	-229.60	0	-1026.78	1.8	-128.05	1.8	0.00	2.12	0.00
117	118	18.70	-826.73	31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
118	118	18.70	-826.73	31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
118	119	19.80	-826.73	35.82	-298.51	0	-1136.39	1.8	32.07	1.8	0.00	2.12	0.00
119	119	19.80	-522.14	35.82	-106.02	0	-586.47	1.8	-171.49	1.8	0.00	2.12	0.00
119	120	20.90	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
120	120	20.90	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
120	121	22.00	-522.14	50.29	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
121	1121	22.00	-565.66	-64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
121	122	23.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
122	122	23.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
122	123	24.80	-565.66	-45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
123	123	24.80	-870.24	-45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
123	124	26.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
124	124	26.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
124	125	27.60	-870.24	-34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
125	125	27.60	-1261.85	-34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
125	126	29.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
126	126	29.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
126	127	30.40	-1261.85	-22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
127	127	30.40	-1609.94	-22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
127	128	31.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
128	128	31.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
128	129	33.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
129	129	33.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
129	130	34.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
130	130	34.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
130	131	36.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
131	131	36.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
131	132	37.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
132	132	37.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
132	133	38.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
133	133	38.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

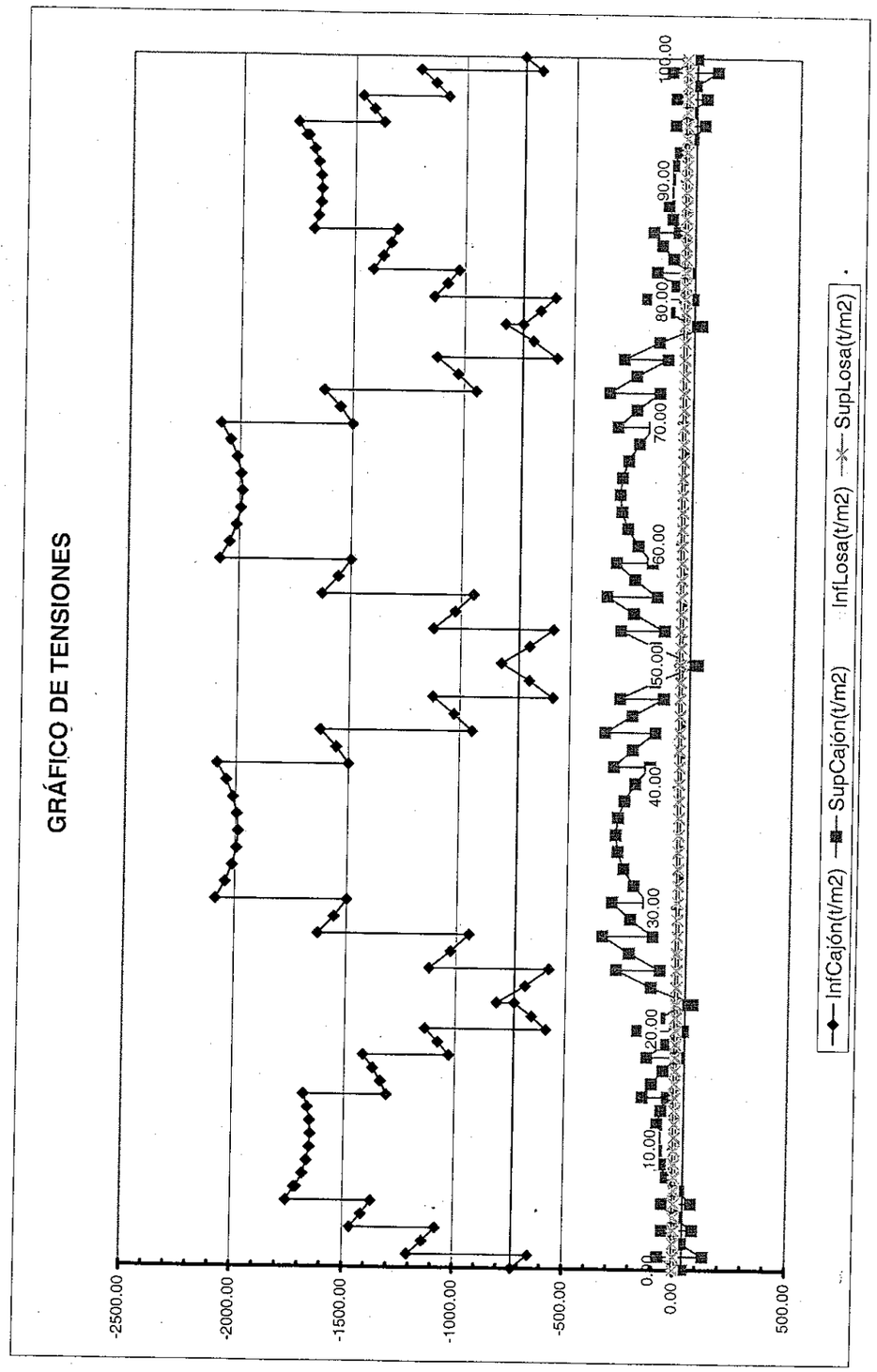
Hipótesis de cálculo:
CONST1.F2.T0.MZ-
Construcción sin gradiente en fase constructiva 2
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
134	134	40.20	-1609.94	17.13	-476.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
134	135	41.60	-1609.94	22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
135	135	41.60	-1261.85	22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
135	136	43.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
136	136	43.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
136	137	44.40	-1261.85	34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
137	137	44.40	-870.24	34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
137	138	45.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
138	138	45.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
138	139	47.20	-870.24	45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
139	139	47.20	-565.66	45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
139	140	48.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
140	140	48.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
140	141	50.00	-565.66	64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
141	1141	50.00	-565.66	-64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
141	142	51.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
142	142	51.40	-565.66	-51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
142	143	52.80	-565.66	-45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
143	143	52.80	-870.24	-45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
143	144	54.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
144	144	54.20	-870.24	-39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
144	145	55.60	-870.24	-34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
145	145	55.60	-1261.85	-34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
145	146	57.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
146	146	57.00	-1261.85	-28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
146	147	58.40	-1261.85	-22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
147	147	58.40	-1609.94	-22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
147	148	59.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
148	148	59.80	-1609.94	-17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
148	149	61.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
149	149	61.20	-1609.94	-11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
149	150	62.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
150	150	62.60	-1609.94	-5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
150	151	64.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
151	151	64.00	-1609.94	0.00	-442.18	0	-1987.18	1.8	-283.38	1.8	0.00	2.12	0.00
151	152	65.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
152	152	65.40	-1609.94	5.71	-446.18	0	-1993.28	1.8	-274.06	1.8	0.00	2.12	0.00
152	153	66.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
153	153	66.80	-1609.94	11.43	-458.17	0	-2011.55	1.8	-246.13	1.8	0.00	2.12	0.00
153	154	68.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
154	154	68.20	-1609.94	17.13	-478.17	0	-2042.02	1.8	-199.54	1.8	0.00	2.12	0.00
154	155	69.60	-1609.94	22.85	-506.15	0	-2084.66	1.8	-134.36	1.8	0.00	2.12	0.00
155	155	69.60	-1261.85	22.85	-307.04	0	-1498.15	1.8	-296.31	1.8	0.00	2.12	0.00
155	156	71.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
156	156	71.00	-1261.85	28.56	-343.03	0	-1555.40	1.8	-212.68	1.8	0.00	2.12	0.00
156	157	72.40	-1261.85	34.27	-387.01	0	-1625.35	1.8	-110.48	1.8	0.00	2.12	0.00
157	157	72.40	-870.24	34.27	-155.18	0	-943.22	1.8	-335.81	1.8	0.00	2.12	0.00
157	158	73.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
158	158	73.80	-870.24	39.99	-207.16	0	-1025.90	1.8	-215.02	1.8	0.00	2.12	0.00
158	159	75.20	-870.24	45.69	-267.13	0	-1121.29	1.8	-75.67	1.8	0.00	2.12	0.00
159	159	75.20	-565.66	45.69	-77.68	0	-576.21	1.8	-272.16	1.8	0.00	2.12	0.00
159	160	76.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
160	160	76.60	-565.66	51.41	-145.66	0	-684.34	1.8	-114.19	1.8	0.00	2.12	0.00
160	161	78.00	-565.66	64.12	-226.53	0	-812.97	1.8	73.72	1.8	0.00	2.12	0.00
161	1161	78.00	-522.14	-50.29	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
161	162	79.10	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
162	162	79.10	-522.14	40.30	-147.90	0	-653.08	1.8	-74.17	1.8	0.00	2.12	0.00
162	163	80.20	-522.14	-35.52	-106.02	0	-586.47	1.8	-171.49	1.8	0.00	2.12	0.00
163	163	80.20	-826.73	-35.52	-298.51	0	-1136.39	1.8	32.07	1.8	0.00	2.12	0.00
163	164	81.30	-826.73	-31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
164	164	81.30	-826.73	-31.32	-261.59	0	-1077.67	1.8	-53.72	1.8	0.00	2.12	0.00
164	165	82.40	-826.73	-26.84	-229.60	0	-1026.78	1.8	-128.05	1.8	0.00	2.12	0.00
165	165	82.40	-1044.29	-26.84	362.75	0	-1412.67	1.8	7.25	1.8	0.00	2.12	0.00
165	166	83.50	-1044.29	-22.35	35.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
166	166	83.50	-1044.29	-22.35	-37.70	0	-1369.65	1.8	-55.60	1.8	0.00	2.12	0.00
166	167	84.60	-1044.29	-17.66	-38.52	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
167	167	84.60	-1044.29	-17.66	-296.35	0	-1334.45	1.8	-107.03	1.8	0.00	2.12	0.00
167	168	85.70	-1044.29	-13.98	-427.36	0	-1307.12	1.8	-146.95	1.8	0.00	2.12	0.00
168	168	85.70	-1261.85	-13.98	-415.13	0	-1680.62	1.8	-33.92	1.8	0.00	2.12	0.00
168	169	86.80	-1261.85	-8.88	-415.13	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
169	169	86.80	-1261.85	-8.88	-407.82	0	-1661.98	1.8	-62.41	1.8	0.00	2.12	0.00
169	170	87.90	-1261.85	-4.40	-407.82	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
170	170	87.90	-1261.85	-4.40	-406.45	0	-1650.85	1.8	-79.44	1.8	0.00	2.12	0.00
170	171	89.00	-1261.85	0.09	-406.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00

Combi_to.xls Programa DINTEL PACADAR S.A. 11/09/03
CONST1.F2.T0.MZ-

CÁLCULO TENSIONAL
Hipótesis de cálculo:
CONST1.F2.T0.MZ-
Construcción sin gradiente en fase constructiva 2
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	0.09	-405.45	0	-1647.23	1.8	-84.96	1.8	0.00	2.12	0.00
171	172	90.10	-1261.85	4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
172	172	90.10	-1261.85	4.58	-408.02	0	-1651.15	1.8	-78.97	1.8	0.00	2.12	0.00
172	173	91.20	-1261.85	9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
173	173	91.20	-1261.85	9.06	-415.52	0	-1662.58	1.8	-61.50	1.8	0.00	2.12	0.00
173	174	92.30	-1261.85	13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
174	174	92.30	-1261.85	13.56	-427.95	0	-1681.52	1.8	-32.55	1.8	0.00	2.12	0.00
174	175	93.40	-1261.85	18.04	-445.33	0	-1708.00	1.8	7.94	1.8	0.00	2.12	0.00
175	175	93.40	-1261.85	18.04	-445.33	0	-1718.12	1.8	25.03	1.8	0.00	2.12	0.00
175	176	94.50	-1261.85	22.53	-467.65	0	-1752.62	1.8	76.90	1.8	0.00	2.12	0.00
176	176	94.50	-1044.29	22.53	-336.68	0	-1371.21	1.8	-53.33	1.8	0.00	2.12	0.00
176	177	95.60	-1044.29	27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
177	177	95.60	-1044.29	27.02	-363.93	0	-1414.55	1.8	9.99	1.8	0.00	2.12	0.00
177	178	96.70	-1044.29	31.50	-396.12	0	-1465.75	1.8	84.79	1.8	0.00	2.12	0.00
178	178	96.70	-826.73	31.50	-262.97	0	-1079.86	1.8	-50.51	1.8	0.00	2.12	0.00
178	179	97.80	-826.73	36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
179	179	97.80	-826.73	36.00	-300.09	0	-1138.91	1.8	35.75	1.8	0.00	2.12	0.00
179	180	98.90	-826.73	40.48	-342.16	0	-1205.82	1.8	133.50	1.8	0.00	2.12	0.00
180	180	98.90	-522.14	40.48	-149.67	0	-655.90	1.8	-70.06	1.8	0.00	2.12	0.00
180	181	100.00	-522.14	46.89	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ+

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-47.66	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
1	2	1.10	-472.42	-41.25	-129.99	0	-584.80	1.8	-76.00	1.8	0.00	2.12	0.00
2	2	1.10	-747.99	-41.25	-304.15	0	-1082.35	1.8	108.18	1.8	0.00	2.12	0.00
2	3	2.20	-747.99	-36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
3	3	2.20	-747.99	-36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
3	4	3.30	-747.99	-32.27	-223.27	0	-953.70	1.8	-79.76	1.8	0.00	2.12	0.00
4	4	3.30	-944.83	-32.27	-343.74	0	-1302.84	1.8	42.66	1.8	0.00	2.12	0.00
4	5	4.40	-944.83	-27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
5	5	4.40	-944.83	-27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
5	6	5.50	-944.83	-23.30	-282.61	0	-1205.61	1.8	-99.39	1.8	0.00	2.12	0.00
6	6	5.50	-1141.67	-23.30	-401.10	0	-1551.60	1.8	18.43	1.8	0.00	2.12	0.00
6	7	6.60	-1141.67	-18.81	-377.93	0	-1514.75	1.8	-35.41	1.8	0.00	2.12	0.00
7	7	6.60	-1141.67	-18.81	-377.93	0	-1507.26	1.8	-51.02	1.8	0.00	2.12	0.00
7	8	7.70	-1141.67	-14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
8	8	7.70	-1141.67	-14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
8	9	8.80	-1141.67	-9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
9	9	8.80	-1141.67	-9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
9	10	9.90	-1141.67	-5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
10	10	9.90	-1141.67	-5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
10	11	11.00	-1141.67	-0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
11	11	11.00	-1141.67	-0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
11	12	12.10	-1141.67	3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
12	12	12.10	-1141.67	3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
12	13	13.20	-1141.67	8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
13	13	13.20	-1141.67	8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
13	14	14.30	-1141.67	12.61	-354.04	0	-1470.86	1.8	-106.67	1.8	0.00	2.12	0.00
14	14	14.30	-944.83	12.61	-235.55	0	-1130.75	1.8	-208.74	1.8	0.00	2.12	0.00
14	15	15.40	-944.83	17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
15	15	15.40	-944.83	17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
15	16	16.50	-944.83	26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
16	16	16.50	-944.83	26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
16	17	17.60	-944.83	36.08	-310.77	0	-1250.40	1.8	-33.96	1.8	0.00	2.12	0.00
17	17	17.60	-747.99	36.08	-189.91	0	-900.64	1.8	-157.28	1.8	0.00	2.12	0.00
17	18	18.70	-747.99	45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
18	18	18.70	-747.99	45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
18	19	19.80	-747.99	55.07	-290.16	0	-1060.10	1.8	75.67	1.8	0.00	2.12	0.00
19	19	19.80	-472.42	55.07	-116.00	0	-562.55	1.8	-108.51	1.8	0.00	2.12	0.00
19	20	20.90	-472.42	64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
20	20	20.90	-472.42	64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
20	21	22.00	-472.42	79.55	-261.07	0	-793.30	1.8	228.59	1.8	0.00	2.12	0.00
21	1021	22.00	-511.78	-95.38	-287.13	0	-866.27	1.8	257.66	1.8	0.00	2.12	0.00
21	22	23.40	-511.78	-76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
22	22	23.40	-511.78	-76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
22	23	24.80	-511.78	-64.21	-68.57	0	-518.62	1.8	-250.20	1.8	0.00	2.12	0.00
23	23	24.80	-787.36	-64.21	-239.98	0	-1011.79	1.8	-72.43	1.8	0.00	2.12	0.00
23	24	26.20	-787.36	-52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
24	24	26.20	-787.36	-52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
24	25	27.60	-787.36	-40.05	-94.00	0	-779.59	1.8	-411.64	1.8	0.00	2.12	0.00
25	25	27.60	-1141.67	-40.05	-303.75	0	-1396.76	1.8	-207.78	1.8	0.00	2.12	0.00
25	26	29.00	-1141.67	-27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
26	26	29.00	-1141.67	-27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
26	27	30.40	-1141.67	-22.26	-220.96	0	-1265.07	1.8	-400.15	1.8	0.00	2.12	0.00
27	27	30.40	-1456.62	-22.26	-401.11	0	-1799.52	1.8	-253.96	1.8	0.00	2.12	0.00
27	28	31.80	-1456.62	-16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
28	28	31.80	-1456.62	-16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
28	29	33.20	-1456.62	-10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
29	29	33.20	-1456.62	-10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
29	30	34.60	-1456.62	-5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
30	30	34.60	-1456.62	-5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
30	31	36.00	-1456.62	0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
31	31	36.00	-1456.62	0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
31	32	37.40	-1456.62	6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
32	32	37.40	-1456.62	6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
32	33	38.80	-1456.62	12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
33	33	38.80	-1456.62	12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
33	34	40.20	-1456.62	17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
34	34	40.20	-1456.62	17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
34	35	41.60	-1456.62	23.44	-407.68	0	-1809.53	1.8	-238.65	1.8	0.00	2.12	0.00
35	35	41.60	-1141.67	23.44	-227.53	0	-1275.52	1.8	-384.89	1.8	0.00	2.12	0.00
35	36	43.00	-1141.67	29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
36	36	43.00	-1141.67	29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
36	37	44.40	-1141.67	41.23	-313.60	0	-1412.42	1.8	-184.89	1.8	0.00	2.12	0.00
37	37	44.40	-787.36	41.23	-103.85	0	-795.26	1.8	-388.75	1.8	0.00	2.12	0.00
37	38	45.80	-787.36	53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
38	38	45.80	-787.36	53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ+

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-787.36	65.39	-253.11	0	-1032.68	1.8	-41.92	1.8	0.00	2.12	0.00
39	39	47.20	-511.78	65.39	-81.70	0	-539.50	1.8	-219.69	1.8	0.00	2.12	0.00
39	40	48.60	-511.78	77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
40	40	48.60	-511.78	77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
40	41	50.00	-511.78	96.56	-303.54	0	-892.37	1.8	295.79	1.8	0.00	2.12	0.00
41	1041	50.00	-511.78	-96.56	-303.54	0	-892.37	1.8	295.79	1.8	0.00	2.12	0.00
41	42	51.40	-511.78	-77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
42	42	51.40	-511.78	-77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
42	43	52.80	-511.78	-65.39	-81.70	0	-539.50	1.8	-219.69	1.8	0.00	2.12	0.00
43	43	52.80	-787.36	-65.39	-253.11	0	-1032.68	1.8	-41.92	1.8	0.00	2.12	0.00
43	44	54.20	-787.36	-53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
44	44	54.20	-787.36	-53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
44	45	55.60	-787.36	-41.23	-103.85	0	-795.26	1.8	-388.75	1.8	0.00	2.12	0.00
45	45	55.60	-1141.67	-41.23	-313.60	0	-1412.42	1.8	-184.89	1.8	0.00	2.12	0.00
45	46	57.00	-1141.67	-29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
46	46	57.00	-1141.67	-29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
46	47	58.40	-1141.67	-23.44	-227.53	0	-1275.52	1.8	-384.89	1.8	0.00	2.12	0.00
47	47	58.40	-1456.62	-23.44	-407.68	0	-1809.53	1.8	-238.65	1.8	0.00	2.12	0.00
47	48	59.80	-1456.62	-17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
48	48	59.80	-1456.62	-17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
48	49	61.20	-1456.62	-12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
49	49	61.20	-1456.62	-12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
49	50	62.60	-1456.62	-6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
50	50	62.60	-1456.62	-6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
50	51	64.00	-1456.62	-0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
51	51	64.00	-1456.62	-0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
51	52	65.40	-1456.62	5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
52	52	65.40	-1456.62	5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
52	53	66.80	-1456.62	10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
53	53	66.80	-1456.62	10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
53	54	68.20	-1456.62	16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
54	54	68.20	-1456.62	16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
54	55	69.60	-1456.62	22.26	-401.11	0	-1799.52	1.8	-253.96	1.8	0.00	2.12	0.00
55	55	69.60	-1141.67	22.26	-220.96	0	-1265.07	1.8	-400.15	1.8	0.00	2.12	0.00
55	56	71.00	-1141.67	27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
56	56	71.00	-1141.67	27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
56	57	72.40	-1141.67	40.05	-303.75	0	-1396.76	1.8	-207.78	1.8	0.00	2.12	0.00
57	57	72.40	-787.36	40.05	-94.00	0	-779.59	1.8	-411.64	1.8	0.00	2.12	0.00
57	58	73.80	-787.36	52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
58	58	73.80	-787.36	52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
58	59	75.20	-787.36	64.21	-239.98	0	-1011.79	1.8	-72.43	1.8	0.00	2.12	0.00
59	59	75.20	-511.78	64.21	-68.57	0	-518.62	1.8	-250.20	1.8	0.00	2.12	0.00
59	60	76.60	-511.78	76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
60	60	76.60	-511.78	76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
60	61	78.00	-511.78	95.38	-287.13	0	-866.27	1.8	257.66	1.8	0.00	2.12	0.00
61	1061	78.00	-472.42	-79.55	-261.07	0	-793.30	1.8	228.59	1.8	0.00	2.12	0.00
61	62	79.10	-472.42	-64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
62	62	79.10	-472.42	-64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
62	63	80.20	-472.42	-55.07	-116.00	0	-562.55	1.8	-108.51	1.8	0.00	2.12	0.00
63	63	80.20	-747.99	-55.07	-290.16	0	-1060.10	1.8	75.67	1.8	0.00	2.12	0.00
63	64	81.30	-747.99	-45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
64	64	81.30	-747.99	-45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
64	65	82.40	-747.99	-36.08	-189.91	0	-900.64	1.8	-157.28	1.8	0.00	2.12	0.00
65	65	82.40	-944.83	-36.08	-310.38	0	-1249.78	1.8	-34.86	1.8	0.00	2.12	0.00
65	66	83.50	-944.83	-26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
66	66	83.50	-944.83	-26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
66	67	84.60	-944.83	-17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
67	67	84.60	-944.83	-17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
67	68	85.70	-944.83	-12.61	-235.55	0	-1130.75	1.8	-208.74	1.8	0.00	2.12	0.00
68	68	85.70	-1141.67	-12.61	-354.04	0	-1470.86	1.8	-106.67	1.8	0.00	2.12	0.00
68	69	86.80	-1141.67	-8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
69	69	86.80	-1141.67	-8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
69	70	87.90	-1141.67	-3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
70	70	87.90	-1141.67	-3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
70	71	89.00	-1141.67	0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
71	71	89.00	-1141.67	0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
71	72	90.10	-1141.67	5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
72	72	90.10	-1141.67	5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
72	73	91.20	-1141.67	9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
73	73	91.20	-1141.67	9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
73	74	92.30	-1141.67	14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
74	74	92.30	-1141.67	14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
74	75	93.40	-1141.67	18.81	-377.93	0	-1507.26	1.8	-51.02	1.8	0.00	2.12	0.00
75	75	93.40	-1141.67	18.81	-377.93	0	-1514.75	1.8	-35.41	1.8	0.00	2.12	0.00
75	76	94.50	-1141.67	23.30	-401.10	0	-1551.60	1.8	18.43	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F3.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ+

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	23.30	-282.61	0	-1205.61	1.8	-99.39	1.8	0.00	2.12	0.00
76	77	95.60	-944.83	27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
77	77	95.60	-944.83	27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
77	78	96.70	-944.83	32.27	-343.74	0	-1302.84	1.8	42.66	1.8	0.00	2.12	0.00
78	78	96.70	-747.99	32.27	-223.27	0	-953.70	1.8	-79.76	1.8	0.00	2.12	0.00
78	79	97.80	-747.99	36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
79	79	97.80	-747.99	36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
79	80	98.90	-747.99	41.25	-304.15	0	-1082.35	1.8	108.18	1.8	0.00	2.12	0.00
80	80	98.90	-472.42	41.25	-129.99	0	-584.80	1.8	-76.00	1.8	0.00	2.12	0.00
80	81	100.00	-472.42	47.66	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	101	0.00	-472.42	-47.66	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	102	1.10	-472.42	-41.25	-129.99	0	-584.80	1.8	-76.00	1.8	0.00	2.12	0.00
102	102	1.10	-747.99	-41.25	-304.15	0	-1082.35	1.8	108.18	1.8	0.00	2.12	0.00
102	103	2.20	-747.99	-36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
103	103	2.20	-747.99	-36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
103	104	3.30	-747.99	-32.27	-223.27	0	-953.70	1.8	-79.76	1.8	0.00	2.12	0.00
104	104	3.30	-944.83	-32.27	-343.74	0	-1302.84	1.8	42.66	1.8	0.00	2.12	0.00
104	105	4.40	-944.83	-27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
105	105	4.40	-944.83	-27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
105	106	5.50	-944.83	-23.30	-282.61	0	-1205.61	1.8	-99.39	1.8	0.00	2.12	0.00
106	106	5.50	-1141.67	-23.30	-401.10	0	-1551.60	1.8	18.43	1.8	0.00	2.12	0.00
106	107	6.60	-1141.67	-18.81	-377.93	0	-1514.75	1.8	-35.41	1.8	0.00	2.12	0.00
107	107	6.60	-1141.67	-18.81	-377.93	0	-1507.26	1.8	-51.02	1.8	0.00	2.12	0.00
107	108	7.70	-1141.67	-14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
108	108	7.70	-1141.67	-14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
108	109	8.80	-1141.67	-9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
109	109	8.80	-1141.67	-9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
109	110	9.90	-1141.67	-5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
110	110	9.90	-1141.67	-5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
110	111	11.00	-1141.67	-0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
111	111	11.00	-1141.67	-0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
111	112	12.10	-1141.67	3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
112	112	12.10	-1141.67	3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
112	113	13.20	-1141.67	8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
113	113	13.20	-1141.67	8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
113	114	14.30	-1141.67	12.61	-354.04	0	-1470.86	1.8	-106.67	1.8	0.00	2.12	0.00
114	114	14.30	-944.83	12.61	-235.55	0	-1130.75	1.8	-208.74	1.8	0.00	2.12	0.00
114	115	15.40	-944.83	17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
115	115	15.40	-944.83	17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
115	116	16.50	-944.83	26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
116	116	16.50	-944.83	26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
116	117	17.60	-944.83	36.08	-310.77	0	-1250.40	1.8	-33.96	1.8	0.00	2.12	0.00
117	117	17.60	-747.99	36.08	-189.91	0	-900.64	1.8	-157.28	1.8	0.00	2.12	0.00
117	118	18.70	-747.99	45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
118	118	18.70	-747.99	45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
118	119	19.80	-747.99	55.07	-290.16	0	-1060.10	1.8	75.67	1.8	0.00	2.12	0.00
119	119	19.80	-472.42	55.07	-116.00	0	-562.55	1.8	-108.51	1.8	0.00	2.12	0.00
119	120	20.90	-472.42	64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
120	120	20.90	-472.42	64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
120	121	22.00	-472.42	79.55	-261.07	0	-793.30	1.8	228.59	1.8	0.00	2.12	0.00
121	1121	22.00	-511.78	-95.38	-287.13	0	-866.27	1.8	257.66	1.8	0.00	2.12	0.00
121	122	23.40	-511.78	-76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
122	122	23.40	-511.78	-76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
122	123	24.80	-511.78	-64.21	-68.57	0	-518.62	1.8	-250.20	1.8	0.00	2.12	0.00
123	123	24.80	-787.36	-64.21	-239.98	0	-1011.79	1.8	-72.43	1.8	0.00	2.12	0.00
123	124	26.20	-787.36	-52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
124	124	26.20	-787.36	-52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
124	125	27.60	-787.36	-40.05	-94.00	0	-779.59	1.8	-411.64	1.8	0.00	2.12	0.00
125	125	27.60	-1141.67	-40.05	-303.75	0	-1396.76	1.8	-207.78	1.8	0.00	2.12	0.00
125	126	29.00	-1141.67	-27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
126	126	29.00	-1141.67	-27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
126	127	30.40	-1141.67	-22.26	-220.96	0	-1265.07	1.8	-400.15	1.8	0.00	2.12	0.00
127	127	30.40	-1456.62	-22.26	-401.11	0	-1799.52	1.8	-253.96	1.8	0.00	2.12	0.00
127	128	31.80	-1456.62	-16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
128	128	31.80	-1456.62	-16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
128	129	33.20	-1456.62	-10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
129	129	33.20	-1456.62	-10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
129	130	34.60	-1456.62	-5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
130	130	34.60	-1456.62	-5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
130	131	36.00	-1456.62	0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
131	131	36.00	-1456.62	0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
131	132	37.40	-1456.62	6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
132	132	37.40	-1456.62	6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
132	133	38.80	-1456.62	12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
133	133	38.80	-1456.62	12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ+

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1456.62	17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
134	134	40.20	-1456.62	17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
134	135	41.60	-1456.62	23.44	-407.68	0	-1809.53	1.8	-238.65	1.8	0.00	2.12	0.00
135	135	41.60	-1141.67	23.44	-227.53	0	-1275.52	1.8	-384.89	1.8	0.00	2.12	0.00
135	136	43.00	-1141.67	29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
136	136	43.00	-1141.67	29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
136	137	44.40	-1141.67	41.23	-313.60	0	-1412.42	1.8	-184.89	1.8	0.00	2.12	0.00
137	137	44.40	-787.36	41.23	-103.85	0	-795.26	1.8	-388.75	1.8	0.00	2.12	0.00
137	138	45.80	-787.36	53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
138	138	45.80	-787.36	53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
138	139	47.20	-787.36	65.39	-253.11	0	-1032.68	1.8	-41.92	1.8	0.00	2.12	0.00
139	139	47.20	-511.78	65.39	-81.70	0	-539.50	1.8	-219.69	1.8	0.00	2.12	0.00
139	140	48.60	-511.78	77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
140	140	48.60	-511.78	77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
140	141	50.00	-511.78	96.56	-303.54	0	-892.37	1.8	295.79	1.8	0.00	2.12	0.00
141	1141	50.00	-511.78	-96.56	-303.54	0	-892.37	1.8	295.79	1.8	0.00	2.12	0.00
141	142	51.40	-511.78	-77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
142	142	51.40	-511.78	-77.48	-181.72	0	-698.60	1.8	12.72	1.8	0.00	2.12	0.00
142	143	52.80	-511.78	-65.39	-81.70	0	-539.50	1.8	-219.69	1.8	0.00	2.12	0.00
143	143	52.80	-787.36	-65.39	-253.11	0	-1032.68	1.8	-41.92	1.8	0.00	2.12	0.00
143	144	54.20	-787.36	-53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
144	144	54.20	-787.36	-53.32	-170.03	0	-900.53	1.8	-234.97	1.8	0.00	2.12	0.00
144	145	55.60	-787.36	-41.23	-103.85	0	-795.26	1.8	-388.75	1.8	0.00	2.12	0.00
145	145	55.60	-1141.67	-41.23	-313.60	0	-1412.42	1.8	-184.89	1.8	0.00	2.12	0.00
145	146	57.00	-1141.67	-29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
146	146	57.00	-1141.67	-29.15	-264.34	0	-1334.07	1.8	-299.35	1.8	0.00	2.12	0.00
146	147	58.40	-1141.67	-23.44	-227.53	0	-1275.52	1.8	-384.89	1.8	0.00	2.12	0.00
147	147	58.40	-1456.62	-23.44	-407.68	0	-1809.53	1.8	-238.65	1.8	0.00	2.12	0.00
147	148	59.80	-1456.62	-17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
148	148	59.80	-1456.62	-17.72	-378.88	0	-1765.65	1.8	-305.74	1.8	0.00	2.12	0.00
148	149	61.20	-1456.62	-12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
149	149	61.20	-1456.62	-12.02	-358.06	0	-1733.92	1.8	-354.24	1.8	0.00	2.12	0.00
149	150	62.60	-1456.62	-6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
150	150	62.60	-1456.62	-6.30	-345.25	0	-1714.40	1.8	-384.08	1.8	0.00	2.12	0.00
150	151	64.00	-1456.62	-0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
151	151	64.00	-1456.62	-0.59	-340.43	0	-1707.06	1.8	-395.31	1.8	0.00	2.12	0.00
151	152	65.40	-1456.62	5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
152	152	65.40	-1456.62	5.12	-343.61	0	-1711.90	1.8	-387.90	1.8	0.00	2.12	0.00
152	153	66.80	-1456.62	10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
153	153	66.80	-1456.62	10.84	-354.78	0	-1728.92	1.8	-361.88	1.8	0.00	2.12	0.00
153	154	68.20	-1456.62	16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
154	154	68.20	-1456.62	16.54	-373.96	0	-1758.15	1.8	-317.20	1.8	0.00	2.12	0.00
154	155	69.60	-1456.62	22.26	-401.11	0	-1799.52	1.8	-253.96	1.8	0.00	2.12	0.00
155	155	69.60	-1141.67	22.26	-220.96	0	-1265.07	1.8	-400.15	1.8	0.00	2.12	0.00
155	156	71.00	-1141.67	27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
156	156	71.00	-1141.67	27.97	-256.13	0	-1321.01	1.8	-318.43	1.8	0.00	2.12	0.00
156	157	72.40	-1141.67	40.05	-303.75	0	-1396.76	1.8	-207.78	1.8	0.00	2.12	0.00
157	157	72.40	-787.36	40.05	-94.00	0	-779.59	1.8	-411.64	1.8	0.00	2.12	0.00
157	158	73.80	-787.36	52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
158	158	73.80	-787.36	52.14	-158.54	0	-882.25	1.8	-261.67	1.8	0.00	2.12	0.00
158	159	75.20	-787.36	64.21	-239.98	0	-1011.79	1.8	-72.43	1.8	0.00	2.12	0.00
159	159	75.20	-511.78	64.21	-68.57	0	-518.62	1.8	-250.20	1.8	0.00	2.12	0.00
159	160	76.60	-511.78	76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
160	160	76.60	-511.78	76.30	-166.95	0	-675.10	1.8	-21.60	1.8	0.00	2.12	0.00
160	161	78.00	-511.78	95.38	-287.13	0	-866.27	1.8	257.66	1.8	0.00	2.12	0.00
161	1161	78.00	-472.42	-79.55	-261.07	0	-793.30	1.8	228.59	1.8	0.00	2.12	0.00
161	162	79.10	-472.42	-64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
162	162	79.10	-472.42	-64.56	-181.81	0	-667.23	1.8	44.42	1.8	0.00	2.12	0.00
162	163	80.20	-472.42	-55.07	-116.00	0	-562.55	1.8	-108.51	1.8	0.00	2.12	0.00
163	163	80.20	-747.99	-55.07	-290.16	0	-1060.10	1.8	75.67	1.8	0.00	2.12	0.00
163	164	81.30	-747.99	-45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
164	164	81.30	-747.99	-45.57	-234.82	0	-972.07	1.8	-52.92	1.8	0.00	2.12	0.00
164	165	82.40	-747.99	-36.08	-189.91	0	-900.64	1.8	-157.28	1.8	0.00	2.12	0.00
165	165	82.40	-944.83	-36.08	-310.38	0	-1249.78	1.8	-34.86	1.8	0.00	2.12	0.00
165	166	83.50	-944.83	-26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
166	166	83.50	-944.83	-26.59	-275.92	0	-1194.97	1.8	-114.94	1.8	0.00	2.12	0.00
166	167	84.60	-944.83	-17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
167	167	84.60	-944.83	-17.09	-251.88	0	-1156.73	1.8	-170.80	1.8	0.00	2.12	0.00
167	168	85.70	-944.83	-12.61	-235.55	0	-1130.75	1.8	-208.74	1.8	0.00	2.12	0.00
168	168	85.70	-1141.67	-12.61	-354.04	0	-1470.86	1.8	-106.67	1.8	0.00	2.12	0.00
168	169	86.80	-1141.67	-8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
169	169	86.80	-1141.67	-8.11	-342.66	0	-1453.52	1.8	-133.18	1.8	0.00	2.12	0.00
169	170	87.90	-1141.67	-3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
170	170	87.90	-1141.67	-3.63	-336.19	0	-1443.66	1.8	-148.25	1.8	0.00	2.12	0.00
170	171	89.00	-1141.67	0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00

Combi_to.xls Programa DINTEL PACADAR S.A. 11/09/03
CONST1.F3.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ+

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	0.86	-334.67	0	-1441.35	1.8	-151.79	1.8	0.00	2.12	0.00
171	172	90.10	-1141.67	5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
172	172	90.10	-1141.67	5.35	-338.08	0	-1446.54	1.8	-143.85	1.8	0.00	2.12	0.00
172	173	91.20	-1141.67	9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
173	173	91.20	-1141.67	9.83	-346.43	0	-1459.27	1.8	-124.40	1.8	0.00	2.12	0.00
173	174	92.30	-1141.67	14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
174	174	92.30	-1141.67	14.33	-359.71	0	-1479.50	1.8	-93.46	1.8	0.00	2.12	0.00
174	175	93.40	-1141.67	18.81	-377.93	0	-1507.26	1.8	-51.02	1.8	0.00	2.12	0.00
175	175	93.40	-1141.67	18.81	-377.93	0	-1514.75	1.8	-35.41	1.8	0.00	2.12	0.00
175	176	94.50	-1141.67	23.30	-401.10	0	-1551.60	1.8	18.43	1.8	0.00	2.12	0.00
176	176	94.50	-944.83	23.30	-282.61	0	-1205.61	1.8	-99.39	1.8	0.00	2.12	0.00
176	177	95.60	-944.83	27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
177	177	95.60	-944.83	27.79	-310.71	0	-1250.30	1.8	-34.10	1.8	0.00	2.12	0.00
177	178	96.70	-944.83	32.27	-343.74	0	-1302.84	1.8	42.66	1.8	0.00	2.12	0.00
178	178	96.70	-747.99	32.27	-223.27	0	-953.70	1.8	-79.76	1.8	0.00	2.12	0.00
178	179	97.80	-747.99	36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
179	179	97.80	-747.99	36.77	-261.24	0	-1014.10	1.8	8.47	1.8	0.00	2.12	0.00
179	180	98.90	-747.99	41.25	-304.15	0	-1082.35	1.8	108.18	1.8	0.00	2.12	0.00
180	180	98.90	-472.42	41.25	-129.99	0	-584.80	1.8	-76.00	1.8	0.00	2.12	0.00
180	181	100.00	-472.42	47.66	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ-
Construcción sin gradiente en fase constructiva 3
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-47.66	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
1	2	1.10	-522.14	-41.25	-148.82	0	-654.54	1.8	-72.04	1.8	0.00	2.12	0.00
2	2	1.10	-826.73	-41.25	-341.31	0	-1204.47	1.8	131.53	1.8	0.00	2.12	0.00
2	3	2.20	-826.73	-36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
3	3	2.20	-826.73	-36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
3	4	3.30	-826.73	-32.27	-260.43	0	-1075.82	1.8	-56.41	1.8	0.00	2.12	0.00
4	4	3.30	-1044.29	-32.27	-393.58	0	-1451.71	1.8	78.89	1.8	0.00	2.12	0.00
4	5	4.40	-1044.29	-27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
5	5	4.40	-1044.29	-27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
5	6	5.50	-1044.29	-23.30	-332.45	0	-1364.48	1.8	-63.16	1.8	0.00	2.12	0.00
6	6	5.50	-1261.85	-23.30	-463.42	0	-1746.89	1.8	67.07	1.8	0.00	2.12	0.00
6	7	6.60	-1261.85	-18.81	-440.25	0	-1710.04	1.8	13.23	1.8	0.00	2.12	0.00
7	7	6.60	-1261.85	-18.81	-440.25	0	-1700.26	1.8	-3.90	1.8	0.00	2.12	0.00
7	8	7.70	-1261.85	-14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
8	8	7.70	-1261.85	-14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
8	9	8.80	-1261.85	-9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
9	9	8.80	-1261.85	-9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
9	10	9.90	-1261.85	-5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
10	10	9.90	-1261.85	-5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
10	11	11.00	-1261.85	-0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
11	11	11.00	-1261.85	-0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
11	12	12.10	-1261.85	3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
12	12	12.10	-1261.85	3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
12	13	13.20	-1261.85	8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
13	13	13.20	-1261.85	8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
13	14	14.30	-1261.85	12.61	-416.36	0	-1663.86	1.8	-59.55	1.8	0.00	2.12	0.00
14	14	14.30	-1044.29	12.61	-285.39	0	-1289.62	1.8	-172.51	1.8	0.00	2.12	0.00
14	15	15.40	-1044.29	17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
15	15	15.40	-1044.29	17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
15	16	16.50	-1044.29	26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
16	16	16.50	-1044.29	26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
16	17	17.60	-1044.29	36.08	-360.65	0	-1409.33	1.8	2.37	1.8	0.00	2.12	0.00
17	17	17.60	-826.73	36.08	-227.07	0	-1022.76	1.8	-133.93	1.8	0.00	2.12	0.00
17	18	18.70	-826.73	45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
18	18	18.70	-826.73	45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
18	19	19.80	-826.73	55.07	-327.32	0	-1182.22	1.8	99.02	1.8	0.00	2.12	0.00
19	19	19.80	-522.14	55.07	-134.83	0	-632.29	1.8	-104.54	1.8	0.00	2.12	0.00
19	20	20.90	-522.14	64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
20	20	20.90	-522.14	64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
20	21	22.00	-522.14	79.55	-279.90	0	-863.04	1.8	232.55	1.8	0.00	2.12	0.00
21	1021	22.00	-565.66	-95.38	-308.71	0	-943.69	1.8	264.68	1.8	0.00	2.12	0.00
21	22	23.40	-565.66	-76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
22	22	23.40	-565.66	-76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
22	23	24.80	-565.66	-64.21	-90.15	0	-596.04	1.8	-243.18	1.8	0.00	2.12	0.00
23	23	24.80	-870.24	-64.21	-279.60	0	-1141.13	1.8	-46.69	1.8	0.00	2.12	0.00
23	24	26.20	-870.24	-52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
24	24	26.20	-870.24	-52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
24	25	27.60	-870.24	-40.05	-133.62	0	-908.93	1.8	-385.90	1.8	0.00	2.12	0.00
25	25	27.60	-1261.85	-40.05	-365.45	0	-1591.06	1.8	-160.58	1.8	0.00	2.12	0.00
25	26	29.00	-1261.85	-27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
26	26	29.00	-1261.85	-27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
26	27	30.40	-1261.85	-22.26	-282.66	0	-1459.37	1.8	-352.96	1.8	0.00	2.12	0.00
27	27	30.40	-1609.94	-22.26	-481.77	0	-2047.51	1.8	-191.16	1.8	0.00	2.12	0.00
27	28	31.80	-1609.94	-16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
28	28	31.80	-1609.94	-16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
28	29	33.20	-1609.94	-10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
29	29	33.20	-1609.94	-10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
29	30	34.60	-1609.94	-5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
30	30	34.60	-1609.94	-5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
30	31	36.00	-1609.94	0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
31	31	36.00	-1609.94	0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
31	32	37.40	-1609.94	6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
32	32	37.40	-1609.94	6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
32	33	38.80	-1609.94	12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
33	33	38.80	-1609.94	12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
33	34	40.20	-1609.94	17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
34	34	40.20	-1609.94	17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
34	35	41.60	-1609.94	23.44	-488.34	0	-2057.52	1.8	-175.85	1.8	0.00	2.12	0.00
35	35	41.60	-1261.85	23.44	-289.23	0	-1469.82	1.8	-337.69	1.8	0.00	2.12	0.00
35	36	43.00	-1261.85	29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
36	36	43.00	-1261.85	29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
36	37	44.40	-1261.85	41.23	-375.30	0	-1606.73	1.8	-137.69	1.8	0.00	2.12	0.00
37	37	44.40	-870.24	41.23	-143.47	0	-924.60	1.8	-363.02	1.8	0.00	2.12	0.00
37	38	45.80	-870.24	53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
38	38	45.80	-870.24	53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00

Combi_to.xls Programa DINTEL PACADAR S.A. 11/09/03
CONST1.F3.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ-
Construcción sin gradiente en fase constructiva 3
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-870.24	65.39	-292.73	0	-1162.01	1.8	-16.18	1.8	0.00	2.12	0.00
39	39	47.20	-565.66	65.39	-103.28	0	-616.93	1.8	-212.67	1.8	0.00	2.12	0.00
39	40	48.60	-565.66	77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
40	40	48.60	-565.66	77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
40	41	50.00	-565.66	96.56	-325.12	0	-969.79	1.8	302.81	1.8	0.00	2.12	0.00
41	1041	50.00	-565.66	-96.56	-325.12	0	-969.79	1.8	302.81	1.8	0.00	2.12	0.00
41	42	51.40	-565.66	-77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
42	42	51.40	-565.66	-77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
42	43	52.80	-565.66	-65.39	-103.28	0	-616.93	1.8	-212.67	1.8	0.00	2.12	0.00
43	43	52.80	-870.24	-65.39	-292.73	0	-1162.01	1.8	-16.18	1.8	0.00	2.12	0.00
43	44	54.20	-870.24	-53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
44	44	54.20	-870.24	-53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
44	45	55.60	-870.24	-41.23	-143.47	0	-924.60	1.8	-363.02	1.8	0.00	2.12	0.00
45	45	55.60	-1261.85	-41.23	-375.30	0	-1606.73	1.8	-137.69	1.8	0.00	2.12	0.00
45	46	57.00	-1261.85	-29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
46	46	57.00	-1261.85	-29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
46	47	58.40	-1261.85	-23.44	-289.23	0	-1469.82	1.8	-337.69	1.8	0.00	2.12	0.00
47	47	58.40	-1609.94	-23.44	-488.34	0	-2057.52	1.8	-175.85	1.8	0.00	2.12	0.00
47	48	59.80	-1609.94	-17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
48	48	59.80	-1609.94	-17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
48	49	61.20	-1609.94	-12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
49	49	61.20	-1609.94	-12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
49	50	62.60	-1609.94	-6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
50	50	62.60	-1609.94	-6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
50	51	64.00	-1609.94	-0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
51	51	64.00	-1609.94	-0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
51	52	65.40	-1609.94	5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
52	52	65.40	-1609.94	5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
52	53	66.80	-1609.94	10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
53	53	66.80	-1609.94	10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
53	54	68.20	-1609.94	16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
54	54	68.20	-1609.94	16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
54	55	69.60	-1609.94	22.26	-481.77	0	-2047.51	1.8	-191.16	1.8	0.00	2.12	0.00
55	55	69.60	-1261.85	22.26	-282.66	0	-1459.37	1.8	-352.96	1.8	0.00	2.12	0.00
55	56	71.00	-1261.85	27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
56	56	71.00	-1261.85	27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
56	57	72.40	-1261.85	40.05	-365.45	0	-1591.06	1.8	-160.58	1.8	0.00	2.12	0.00
57	57	72.40	-870.24	40.05	-133.62	0	-908.93	1.8	-385.90	1.8	0.00	2.12	0.00
57	58	73.80	-870.24	52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
58	58	73.80	-870.24	52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
58	59	75.20	-870.24	64.21	-279.60	0	-1141.13	1.8	-46.69	1.8	0.00	2.12	0.00
59	59	75.20	-565.66	64.21	-90.15	0	-596.04	1.8	-243.18	1.8	0.00	2.12	0.00
59	60	76.60	-565.66	76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
60	60	76.60	-565.66	76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
60	61	78.00	-565.66	95.38	-308.71	0	-943.69	1.8	264.68	1.8	0.00	2.12	0.00
61	1061	78.00	-522.14	-79.55	-279.90	0	-863.04	1.8	232.55	1.8	0.00	2.12	0.00
61	62	79.10	-522.14	-64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
62	62	79.10	-522.14	-64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
62	63	80.20	-522.14	-55.07	-134.83	0	-632.29	1.8	-104.54	1.8	0.00	2.12	0.00
63	63	80.20	-826.73	-55.07	-327.32	0	-1182.22	1.8	99.02	1.8	0.00	2.12	0.00
63	64	81.30	-826.73	-45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
64	64	81.30	-826.73	-45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
64	65	82.40	-826.73	-36.08	-227.07	0	-1022.76	1.8	-133.93	1.8	0.00	2.12	0.00
65	65	82.40	-1044.29	-36.08	-360.22	0	-1408.65	1.8	1.37	1.8	0.00	2.12	0.00
65	66	83.50	-1044.29	-26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
66	66	83.50	-1044.29	-26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
66	67	84.60	-1044.29	-17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
67	67	84.60	-1044.29	-17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
67	68	85.70	-1044.29	-12.61	-285.39	0	-1289.62	1.8	-172.51	1.8	0.00	2.12	0.00
68	68	85.70	-1261.85	-12.61	-416.36	0	-1663.86	1.8	-59.55	1.8	0.00	2.12	0.00
68	69	86.80	-1261.85	-8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
69	69	86.80	-1261.85	-8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
69	70	87.90	-1261.85	-3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
70	70	87.90	-1261.85	-3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
70	71	89.00	-1261.85	0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
71	71	89.00	-1261.85	0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
71	72	90.10	-1261.85	5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
72	72	90.10	-1261.85	5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
72	73	91.20	-1261.85	9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
73	73	91.20	-1261.85	9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
73	74	92.30	-1261.85	14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
74	74	92.30	-1261.85	14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
74	75	93.40	-1261.85	18.81	-440.25	0	-1700.26	1.8	-3.90	1.8	0.00	2.12	0.00
75	75	93.40	-1261.85	18.81	-440.25	0	-1710.04	1.8	13.23	1.8	0.00	2.12	0.00
75	76	94.50	-1261.85	23.30	-463.42	0	-1746.89	1.8	67.07	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ-

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	23.30	-332.45	0	-1364.48	1.8	-63.16	1.8	0.00	2.12	0.00
76	77	95.60	-1044.29	27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
77	77	95.60	-1044.29	27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
77	78	96.70	-1044.29	32.27	-393.58	0	-1461.71	1.8	78.89	1.8	0.00	2.12	0.00
78	78	96.70	-826.73	32.27	-260.43	0	-1075.82	1.8	-56.41	1.8	0.00	2.12	0.00
78	79	97.80	-826.73	36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
79	79	97.80	-826.73	36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
79	80	98.90	-826.73	41.25	-341.31	0	-1204.47	1.8	131.53	1.8	0.00	2.12	0.00
80	80	98.90	-522.14	41.25	-148.82	0	-654.54	1.8	-72.04	1.8	0.00	2.12	0.00
80	81	100.00	-522.14	47.66	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	101	0.00	-522.14	-47.66	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	102	1.10	-522.14	-41.25	-148.82	0	-654.54	1.8	-72.04	1.8	0.00	2.12	0.00
102	102	1.10	-826.73	-41.25	-341.31	0	-1204.47	1.8	131.53	1.8	0.00	2.12	0.00
102	103	2.20	-826.73	-36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
103	103	2.20	-826.73	-36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
103	104	3.30	-826.73	-32.27	-260.43	0	-1075.82	1.8	-56.41	1.8	0.00	2.12	0.00
104	104	3.30	-1044.29	-32.27	-393.58	0	-1461.71	1.8	78.89	1.8	0.00	2.12	0.00
104	105	4.40	-1044.29	-27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
105	105	4.40	-1044.29	-27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
105	106	5.50	-1044.29	-23.30	-332.45	0	-1364.48	1.8	-63.16	1.8	0.00	2.12	0.00
106	106	5.50	-1261.85	-23.30	-463.42	0	-1746.89	1.8	67.07	1.8	0.00	2.12	0.00
106	107	6.60	-1261.85	-18.81	-440.25	0	-1710.04	1.8	13.23	1.8	0.00	2.12	0.00
107	107	6.60	-1261.85	-18.81	-440.25	0	-1700.26	1.8	-3.90	1.8	0.00	2.12	0.00
107	108	7.70	-1261.85	-14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
108	108	7.70	-1261.85	-14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
108	109	8.80	-1261.85	-9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
109	109	8.80	-1261.85	-9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
109	110	9.90	-1261.85	-5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
110	110	9.90	-1261.85	-5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
110	111	11.00	-1261.85	-0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
111	111	11.00	-1261.85	-0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
111	112	12.10	-1261.85	3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
112	112	12.10	-1261.85	3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
112	113	13.20	-1261.85	8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
113	113	13.20	-1261.85	8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
113	114	14.30	-1261.85	12.61	-416.36	0	-1663.86	1.8	-59.55	1.8	0.00	2.12	0.00
114	114	14.30	-1044.29	12.61	-285.39	0	-1289.62	1.8	-172.51	1.8	0.00	2.12	0.00
114	115	15.40	-1044.29	17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
115	115	15.40	-1044.29	17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
115	116	16.50	-1044.29	26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
116	116	16.50	-1044.29	26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
116	117	17.60	-1044.29	36.08	-360.65	0	-1409.33	1.8	2.37	1.8	0.00	2.12	0.00
117	117	17.60	-826.73	36.08	-227.07	0	-1022.76	1.8	-133.93	1.8	0.00	2.12	0.00
117	118	18.70	-826.73	45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
118	118	18.70	-826.73	45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
118	119	19.80	-826.73	55.07	-327.32	0	-1182.22	1.8	99.02	1.8	0.00	2.12	0.00
119	119	19.80	-522.14	55.07	-134.83	0	-632.29	1.8	-104.54	1.8	0.00	2.12	0.00
119	120	20.90	-522.14	64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
120	120	20.90	-522.14	64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
120	121	22.00	-522.14	79.55	-279.90	0	-863.04	1.8	232.55	1.8	0.00	2.12	0.00
121	1121	22.00	-565.66	-95.38	-308.71	0	-943.69	1.8	264.68	1.8	0.00	2.12	0.00
121	122	23.40	-565.66	-76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
122	122	23.40	-565.66	-76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
122	123	24.80	-565.66	-64.21	-90.15	0	-596.04	1.8	-243.18	1.8	0.00	2.12	0.00
123	123	24.80	-870.24	-64.21	-279.60	0	-1141.13	1.8	-46.69	1.8	0.00	2.12	0.00
123	124	26.20	-870.24	-52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
124	124	26.20	-870.24	-52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
124	125	27.60	-870.24	-40.05	-133.62	0	-908.93	1.8	-385.90	1.8	0.00	2.12	0.00
125	125	27.60	-1261.85	-40.05	-365.45	0	-1591.06	1.8	-160.58	1.8	0.00	2.12	0.00
125	126	29.00	-1261.85	-27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
126	126	29.00	-1261.85	-27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
126	127	30.40	-1261.85	-22.26	-282.66	0	-1459.37	1.8	-352.96	1.8	0.00	2.12	0.00
127	127	30.40	-1609.94	-22.26	-481.77	0	-2047.51	1.8	-191.16	1.8	0.00	2.12	0.00
127	128	31.80	-1609.94	-16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
128	128	31.80	-1609.94	-16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
128	129	33.20	-1609.94	-10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
129	129	33.20	-1609.94	-10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
129	130	34.60	-1609.94	-5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
130	130	34.60	-1609.94	-5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
130	131	36.00	-1609.94	0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
131	131	36.00	-1609.94	0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
131	132	37.40	-1609.94	6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
132	132	37.40	-1609.94	6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
132	133	38.80	-1609.94	12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
133	133	38.80	-1609.94	12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00

Combi_to.xls Programa DINTEL PACADAR S.A. CONST1.F3.T0.MZ- 11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ-

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1609.94	17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
134	134	40.20	-1609.94	17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
134	135	41.60	-1609.94	23.44	-488.34	0	-2057.52	1.8	-175.85	1.8	0.00	2.12	0.00
135	135	41.60	-1261.85	23.44	-289.23	0	-1469.82	1.8	-337.69	1.8	0.00	2.12	0.00
135	136	43.00	-1261.85	29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
136	136	43.00	-1261.85	29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
136	137	44.40	-1261.85	41.23	-375.30	0	-1606.73	1.8	-137.69	1.8	0.00	2.12	0.00
137	137	44.40	-870.24	41.23	-143.47	0	-924.60	1.8	-363.02	1.8	0.00	2.12	0.00
137	138	45.80	-870.24	53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
138	138	45.80	-870.24	53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
138	139	47.20	-870.24	65.39	-292.73	0	-1162.01	1.8	-16.18	1.8	0.00	2.12	0.00
139	139	47.20	-565.66	65.39	-103.28	0	-616.93	1.8	-212.67	1.8	0.00	2.12	0.00
139	140	48.60	-565.66	77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
140	140	48.60	-565.66	77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
140	141	50.00	-565.66	96.56	-325.12	0	-969.79	1.8	302.81	1.8	0.00	2.12	0.00
141	1141	50.00	-565.66	-96.56	-325.12	0	-969.79	1.8	302.81	1.8	0.00	2.12	0.00
141	142	51.40	-565.66	-77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
142	142	51.40	-565.66	-77.48	-203.30	0	-776.02	1.8	19.74	1.8	0.00	2.12	0.00
142	143	52.80	-565.66	-65.39	-103.28	0	-616.93	1.8	-212.67	1.8	0.00	2.12	0.00
143	143	52.80	-870.24	-65.39	-292.73	0	-1162.01	1.8	-16.18	1.8	0.00	2.12	0.00
143	144	54.20	-870.24	-53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
144	144	54.20	-870.24	-53.32	-209.65	0	-1029.86	1.8	-209.23	1.8	0.00	2.12	0.00
144	145	55.60	-870.24	-41.23	-143.47	0	-924.60	1.8	-363.02	1.8	0.00	2.12	0.00
145	145	55.60	-1261.85	-41.23	-375.30	0	-1606.73	1.8	-137.69	1.8	0.00	2.12	0.00
145	146	57.00	-1261.85	-29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
146	146	57.00	-1261.85	-29.15	-326.04	0	-1528.37	1.8	-252.16	1.8	0.00	2.12	0.00
146	147	58.40	-1261.85	-23.44	-289.23	0	-1469.82	1.8	-337.69	1.8	0.00	2.12	0.00
147	147	58.40	-1609.94	-23.44	-488.34	0	-2057.52	1.8	-175.85	1.8	0.00	2.12	0.00
147	148	59.80	-1609.94	-17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
148	148	59.80	-1609.94	-17.72	-459.54	0	-2013.64	1.8	-242.94	1.8	0.00	2.12	0.00
148	149	61.20	-1609.94	-12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
149	149	61.20	-1609.94	-12.02	-438.72	0	-1981.91	1.8	-291.44	1.8	0.00	2.12	0.00
149	150	62.60	-1609.94	-6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
150	150	62.60	-1609.94	-6.30	-425.91	0	-1962.39	1.8	-321.28	1.8	0.00	2.12	0.00
150	151	64.00	-1609.94	-0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
151	151	64.00	-1609.94	-0.59	-421.09	0	-1955.05	1.8	-332.51	1.8	0.00	2.12	0.00
151	152	65.40	-1609.94	5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
152	152	65.40	-1609.94	5.12	-424.27	0	-1959.89	1.8	-325.10	1.8	0.00	2.12	0.00
152	153	66.80	-1609.94	10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
153	153	66.80	-1609.94	10.84	-435.44	0	-1976.91	1.8	-299.08	1.8	0.00	2.12	0.00
153	154	68.20	-1609.94	16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
154	154	68.20	-1609.94	16.54	-454.62	0	-2006.14	1.8	-254.40	1.8	0.00	2.12	0.00
154	155	69.60	-1609.94	22.26	-481.77	0	-2047.51	1.8	-191.16	1.8	0.00	2.12	0.00
155	155	69.60	-1261.85	22.26	-282.66	0	-1459.37	1.8	-352.96	1.8	0.00	2.12	0.00
155	156	71.00	-1261.85	27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
156	156	71.00	-1261.85	27.97	-317.83	0	-1515.31	1.8	-271.24	1.8	0.00	2.12	0.00
156	157	72.40	-1261.85	40.05	-365.45	0	-1591.06	1.8	-160.58	1.8	0.00	2.12	0.00
157	157	72.40	-870.24	40.05	-133.62	0	-908.93	1.8	-385.90	1.8	0.00	2.12	0.00
157	158	73.80	-870.24	52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
158	158	73.80	-870.24	52.14	-198.16	0	-1011.59	1.8	-235.93	1.8	0.00	2.12	0.00
158	159	75.20	-870.24	64.21	-279.60	0	-1141.13	1.8	-46.69	1.8	0.00	2.12	0.00
159	159	75.20	-565.66	64.21	-90.15	0	-596.04	1.8	-243.18	1.8	0.00	2.12	0.00
159	160	76.60	-565.66	76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
160	160	76.60	-565.66	76.30	-188.53	0	-752.53	1.8	-14.58	1.8	0.00	2.12	0.00
160	161	78.00	-565.66	95.38	-308.71	0	-943.69	1.8	264.68	1.8	0.00	2.12	0.00
161	1161	78.00	-522.14	-79.55	-279.90	0	-863.04	1.8	232.55	1.8	0.00	2.12	0.00
161	162	79.10	-522.14	-64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
162	162	79.10	-522.14	-64.56	-200.64	0	-736.97	1.8	48.38	1.8	0.00	2.12	0.00
162	163	80.20	-522.14	-55.07	-134.83	0	-632.29	1.8	-104.54	1.8	0.00	2.12	0.00
163	163	80.20	-826.73	-55.07	-327.32	0	-1182.22	1.8	99.02	1.8	0.00	2.12	0.00
163	164	81.30	-826.73	-45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
164	164	81.30	-826.73	-45.57	-271.98	0	-1094.19	1.8	-29.57	1.8	0.00	2.12	0.00
164	165	82.40	-826.73	-36.08	-227.07	0	-1022.76	1.8	-133.93	1.8	0.00	2.12	0.00
165	165	82.40	-1044.29	-36.08	-360.22	0	-1408.65	1.8	1.37	1.8	0.00	2.12	0.00
165	166	83.50	-1044.29	-26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
166	166	83.50	-1044.29	-26.59	-325.76	0	-1353.84	1.8	-78.70	1.8	0.00	2.12	0.00
166	167	84.60	-1044.29	-17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
167	167	84.60	-1044.29	-17.09	-301.72	0	-1315.60	1.8	-134.56	1.8	0.00	2.12	0.00
167	168	85.70	-1044.29	-12.61	-285.39	0	-1289.62	1.8	-172.51	1.8	0.00	2.12	0.00
168	168	85.70	-1261.85	-12.61	-416.36	0	-1663.86	1.8	-59.55	1.8	0.00	2.12	0.00
168	169	86.80	-1261.85	-8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
169	169	86.80	-1261.85	-8.11	-404.98	0	-1646.52	1.8	-86.06	1.8	0.00	2.12	0.00
169	170	87.90	-1261.85	-3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
170	170	87.90	-1261.85	-3.63	-398.51	0	-1636.66	1.8	-101.13	1.8	0.00	2.12	0.00
170	171	89.00	-1261.85	0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.MZ-

Construcción sin gradiente en fase constructiva 3

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	0.86	-396.99	0	-1634.34	1.8	-104.67	1.8	0.00	2.12	0.00
171	172	90.10	-1261.85	5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
172	172	90.10	-1261.85	5.35	-400.40	0	-1639.54	1.8	-96.72	1.8	0.00	2.12	0.00
172	173	91.20	-1261.85	9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
173	173	91.20	-1261.85	9.83	-408.75	0	-1652.26	1.8	-77.27	1.8	0.00	2.12	0.00
173	174	92.30	-1261.85	14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
174	174	92.30	-1261.85	14.33	-422.03	0	-1672.50	1.8	-46.34	1.8	0.00	2.12	0.00
174	175	93.40	-1261.85	18.81	-440.25	0	-1700.26	1.8	-3.90	1.8	0.00	2.12	0.00
175	175	93.40	-1261.85	18.81	-440.25	0	-1710.04	1.8	13.23	1.8	0.00	2.12	0.00
175	176	94.50	-1261.85	23.30	-463.42	0	-1746.89	1.8	67.07	1.8	0.00	2.12	0.00
176	176	94.50	-1044.29	23.30	-332.45	0	-1364.48	1.8	-63.16	1.8	0.00	2.12	0.00
176	177	95.60	-1044.29	27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
177	177	95.60	-1044.29	27.79	-360.55	0	-1409.17	1.8	2.14	1.8	0.00	2.12	0.00
177	178	96.70	-1044.29	32.27	-393.58	0	-1461.71	1.8	78.89	1.8	0.00	2.12	0.00
178	178	96.70	-826.73	32.27	-260.43	0	-1075.82	1.8	-56.41	1.8	0.00	2.12	0.00
178	179	97.80	-826.73	36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
179	179	97.80	-826.73	36.77	-298.40	0	-1136.22	1.8	31.82	1.8	0.00	2.12	0.00
179	180	98.90	-826.73	41.25	-341.31	0	-1204.47	1.8	131.53	1.8	0.00	2.12	0.00
180	180	98.90	-522.14	41.25	-148.82	0	-654.54	1.8	-72.04	1.8	0.00	2.12	0.00
180	181	100.00	-522.14	47.66	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00

11/09/03

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CONST1.F3.T0.MZ-

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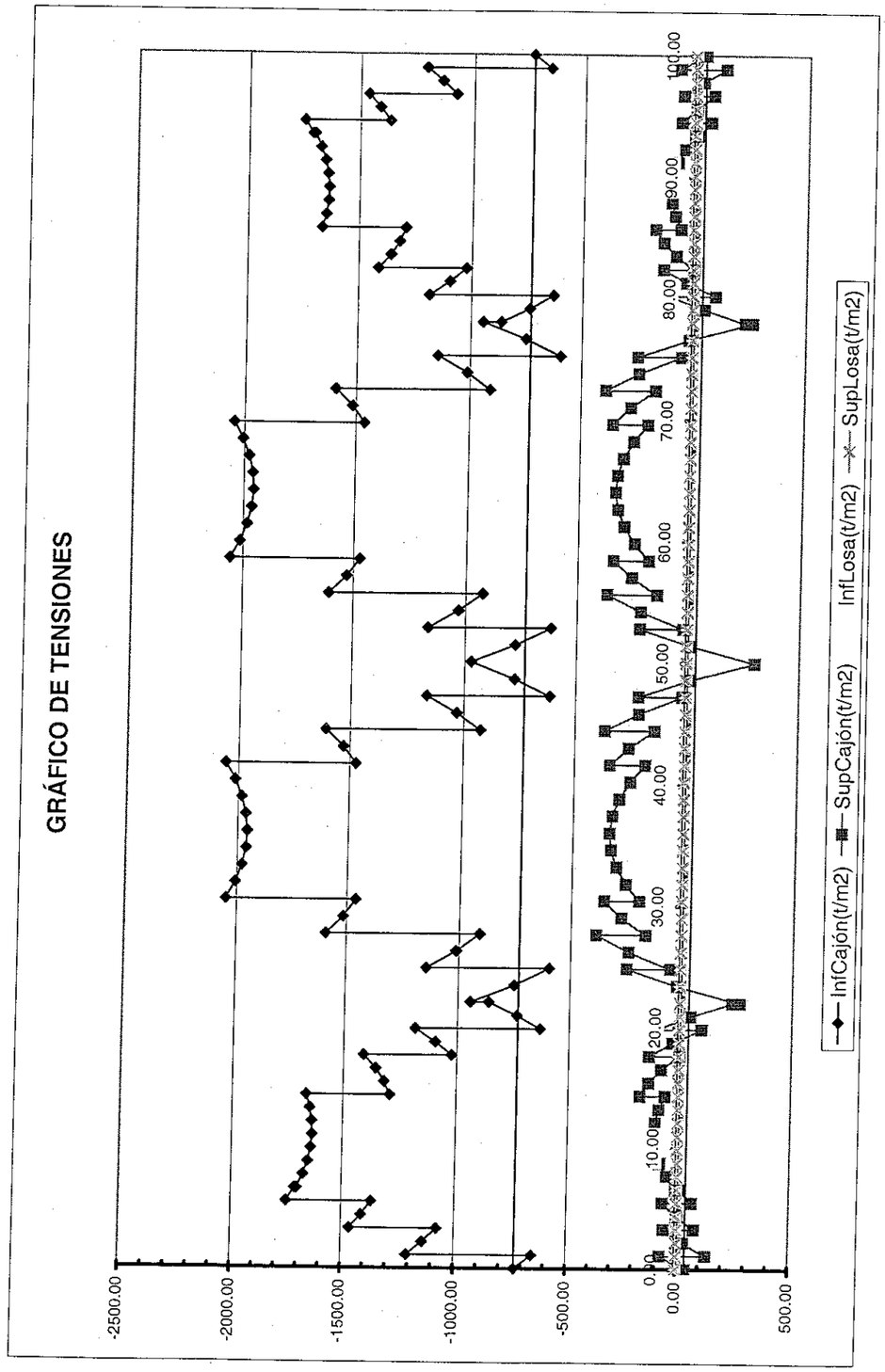


CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ+

Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-38.21	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
1	2	1.10	-476.85	-31.89	-140.28	0	-604.73	1.8	-55.61	1.8	0.00	2.12	0.00
2	2	1.10	-752.42	-31.89	-314.45	0	-1102.28	1.8	128.57	1.8	0.00	2.12	0.00
2	3	2.20	-752.42	-27.41	-281.83	0	-1050.39	1.8	52.77	1.8	0.00	2.12	0.00
3	3	2.20	-752.42	-27.41	-281.83	0	-1050.39	1.8	52.77	1.8	0.00	2.12	0.00
3	4	3.30	-752.42	-22.91	-254.16	0	-1006.38	1.8	-11.53	1.8	0.00	2.12	0.00
4	4	3.30	-949.26	-22.91	-374.63	0	-1355.52	1.8	110.88	1.8	0.00	2.12	0.00
4	5	4.40	-949.26	-18.43	-351.91	0	-1319.38	1.8	58.09	1.8	0.00	2.12	0.00
5	5	4.40	-949.26	-18.43	-351.91	0	-1319.38	1.8	58.09	1.8	0.00	2.12	0.00
5	6	5.50	-949.26	-13.94	-334.10	0	-1291.06	1.8	16.72	1.8	0.00	2.12	0.00
6	6	5.50	-1146.10	-13.94	-452.60	0	-1637.06	1.8	134.55	1.8	0.00	2.12	0.00
6	7	6.60	-1146.10	-9.45	-439.72	0	-1616.57	1.8	104.62	1.8	0.00	2.12	0.00
7	7	6.60	-1146.10	-9.45	-439.72	0	-1605.03	1.8	89.29	1.8	0.00	2.12	0.00
7	8	7.70	-1146.10	-4.97	-431.80	0	-1592.96	1.8	70.84	1.8	0.00	2.12	0.00
8	8	7.70	-1146.10	-4.97	-431.80	0	-1592.96	1.8	70.84	1.8	0.00	2.12	0.00
8	9	8.80	-1146.10	-0.47	-428.82	0	-1588.42	1.8	63.90	1.8	0.00	2.12	0.00
9	9	8.80	-1146.10	-0.47	-428.82	0	-1588.42	1.8	63.90	1.8	0.00	2.12	0.00
9	10	9.90	-1146.10	4.01	-430.77	0	-1591.39	1.8	68.44	1.8	0.00	2.12	0.00
10	10	9.90	-1146.10	4.01	-430.77	0	-1591.39	1.8	68.44	1.8	0.00	2.12	0.00
10	11	11.00	-1146.10	8.50	-437.64	0	-1601.87	1.8	84.46	1.8	0.00	2.12	0.00
11	11	11.00	-1146.10	8.50	-437.64	0	-1601.87	1.8	84.46	1.8	0.00	2.12	0.00
11	12	12.10	-1146.10	12.99	-449.46	0	-1619.88	1.8	112.00	1.8	0.00	2.12	0.00
12	12	12.10	-1146.10	12.99	-449.46	0	-1619.88	1.8	112.00	1.8	0.00	2.12	0.00
12	13	13.20	-1146.10	17.47	-466.24	0	-1645.45	1.8	151.08	1.8	0.00	2.12	0.00
13	13	13.20	-1146.10	17.47	-466.24	0	-1645.45	1.8	151.08	1.8	0.00	2.12	0.00
13	14	14.30	-1146.10	21.97	-487.91	0	-1678.46	1.8	201.56	1.8	0.00	2.12	0.00
14	14	14.30	-943.11	22.83	-369.42	0	-1333.34	1.8	104.50	1.8	0.00	2.12	0.00
14	15	15.40	-939.43	24.85	-397.49	0	-1374.20	1.8	172.82	1.8	0.00	2.12	0.00
15	15	15.40	-1858.58	26.54	42.03	0	-1185.04	1.8	-507.41	1.8	-292.36	2.12	-339.96
15	16	16.50	-1858.58	36.04	7.59	0	-1232.23	1.8	-449.60	1.8	-290.66	2.12	-336.58
16	16	16.50	-1858.58	36.04	7.58	0	-1202.07	1.8	-479.03	1.8	-316.23	2.12	-371.35
16	17	17.60	-1858.58	45.53	-37.66	0	-1267.56	1.8	-395.03	1.8	-313.60	2.12	-366.70
17	17	17.60	-2575.51	45.53	522.70	0	-773.93	1.8	-927.91	1.8	-669.31	2.12	-807.86
17	18	18.70	-2575.51	55.02	467.40	0	-855.43	1.8	-820.52	1.8	-666.68	2.12	-803.21
18	18	18.70	-2575.50	55.02	467.40	0	-855.42	1.8	-820.52	1.8	-666.68	2.12	-803.21
18	19	19.80	-2575.50	64.52	401.64	0	-953.53	1.8	-688.89	1.8	-664.04	2.12	-798.55
19	19	19.80	-2299.92	64.52	575.81	0	-455.97	1.8	-873.07	1.8	-664.04	2.12	-798.55
19	20	20.90	-2299.92	74.01	499.60	0	-570.71	1.8	-717.12	1.8	-661.41	2.12	-793.90
20	20	20.90	-2299.92	74.01	499.60	0	-570.71	1.8	-717.12	1.8	-661.41	2.12	-793.90
20	21	22.00	-2299.92	89.00	409.94	0	-706.85	1.8	-529.91	1.8	-658.78	2.12	-789.24
21	1021	22.00	-2339.29	-99.87	383.87	0	-779.82	1.8	-500.84	1.8	-658.78	2.12	-789.24
21	22	23.40	-2339.29	-80.79	510.34	0	-582.57	1.8	-781.93	1.8	-660.37	2.12	-792.06
22	22	23.40	-2339.29	-80.79	510.34	0	-582.57	1.8	-781.93	1.8	-660.37	2.12	-792.06
22	23	24.80	-2339.29	-68.70	615.01	0	-420.00	1.8	-1012.37	1.8	-661.96	2.12	-794.87
23	23	24.80	-2614.86	-68.69	443.60	0	-913.17	1.8	-834.60	1.8	-661.96	2.12	-794.87
23	24	26.20	-2614.86	-56.62	531.32	0	-777.55	1.8	-1025.67	1.8	-663.55	2.12	-797.68
24	24	26.20	-1701.11	-56.62	91.81	0	-921.43	1.8	-616.11	1.8	-307.84	2.12	-356.52
24	25	27.60	-1701.11	-44.53	162.64	0	-812.69	1.8	-767.91	1.8	-309.43	2.12	-359.33
25	25	27.60	-2055.42	-44.54	-47.11	0	-1429.85	1.8	-564.05	1.8	-309.43	2.12	-359.33
25	26	29.00	-2055.42	-32.46	6.80	0	-1348.02	1.8	-676.53	1.8	-311.02	2.12	-362.15
26	26	29.00	-1139.52	-31.90	-432.72	0	-1588.33	1.8	94.67	1.8	0.00	2.12	0.00
26	27	30.40	-1142.78	-28.07	-391.16	0	-1525.31	1.8	-4.59	1.8	0.00	2.12	0.00
27	27	30.40	-1460.38	-26.83	-571.31	0	-2061.92	1.8	139.43	1.8	0.00	2.12	0.00
27	28	31.80	-1460.38	-21.11	-537.77	0	-2010.82	1.8	61.30	1.8	0.00	2.12	0.00
28	28	31.80	-1460.38	-21.11	-537.77	0	-2010.82	1.8	61.30	1.8	0.00	2.12	0.00
28	29	33.20	-1460.38	-15.41	-512.19	0	-1971.84	1.8	1.71	1.8	0.00	2.12	0.00
29	29	33.20	-1460.38	-15.41	-512.19	0	-1971.84	1.8	1.71	1.8	0.00	2.12	0.00
29	30	34.60	-1460.38	-9.69	-494.62	0	-1945.08	1.8	-39.19	1.8	0.00	2.12	0.00
30	30	34.60	-1460.38	-9.69	-494.62	0	-1945.08	1.8	-39.19	1.8	0.00	2.12	0.00
30	31	36.00	-1460.38	-3.98	-485.05	0	-1930.50	1.8	-61.49	1.8	0.00	2.12	0.00
31	31	36.00	-1460.38	-3.98	-485.05	0	-1930.50	1.8	-61.49	1.8	0.00	2.12	0.00
31	32	37.40	-1460.38	1.73	-483.47	0	-1928.09	1.8	-65.17	1.8	0.00	2.12	0.00
32	32	37.40	-1460.38	1.73	-483.47	0	-1928.09	1.8	-65.17	1.8	0.00	2.12	0.00
32	33	38.80	-1460.38	7.45	-489.89	0	-1937.87	1.8	-50.21	1.8	0.00	2.12	0.00
33	33	38.80	-1460.38	7.45	-489.89	0	-1937.87	1.8	-50.21	1.8	0.00	2.12	0.00
33	34	40.20	-1460.38	13.15	-504.32	0	-1959.85	1.8	-16.60	1.8	0.00	2.12	0.00
34	34	40.20	-1460.38	13.15	-504.32	0	-1959.85	1.8	-16.60	1.8	0.00	2.12	0.00
34	35	41.60	-1460.38	18.87	-526.73	0	-1994.00	1.8	35.60	1.8	0.00	2.12	0.00
35	35	41.60	-1147.16	21.23	-346.58	0	-1461.40	1.8	-112.05	1.8	0.00	2.12	0.00
35	36	43.00	-1143.83	25.21	-378.12	0	-1509.21	1.8	-36.07	1.8	0.00	2.12	0.00
36	36	43.00	-2055.42	24.66	61.40	0	-1300.30	1.8	-675.76	1.8	-326.92	2.12	-390.25
36	37	44.40	-2055.42	36.74	18.43	0	-1372.56	1.8	-563.13	1.8	-328.51	2.12	-393.07
37	37	44.40	-1701.11	36.75	228.17	0	-755.41	1.8	-766.99	1.8	-328.51	2.12	-393.06
37	38	45.80	-1701.11	48.84	168.27	0	-854.59	1.8	-615.04	1.8	-330.10	2.12	-395.88
38	38	45.80	-2614.86	48.84	607.78	0	-710.71	1.8	-1024.60	1.8	-685.81	2.12	-837.04

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ+

Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	60.91	530.97	0	-836.79	1.8	-833.37	1.8	-687.40	2.12	-839.85
39	39	47.20	-2339.29	60.91	702.39	0	-343.61	1.8	-1011.15	1.8	-687.40	2.12	-839.85
39	40	48.60	-2345.74	72.50	609.25	0	-498.03	1.8	-782.73	1.8	-690.87	2.12	-844.66
40	40	48.60	-2345.92	72.49	609.30	0	-498.04	1.8	-782.80	1.8	-690.93	2.12	-844.73
40	41	50.00	-2345.92	91.57	494.47	0	-685.04	1.8	-501.76	1.8	-692.70	2.12	-847.86
41	1041	50.00	-2345.70	-91.65	494.48	0	-684.97	1.8	-501.70	1.8	-692.64	2.12	-847.80
41	42	51.40	-2345.70	-72.57	609.44	0	-497.84	1.8	-782.77	1.8	-690.91	2.12	-844.73
42	42	51.40	-2345.10	-72.58	609.39	0	-497.71	1.8	-782.57	1.8	-690.73	2.12	-844.55
42	43	52.80	-2345.10	-60.49	702.55	0	-345.25	1.8	-1012.99	1.8	-689.00	2.12	-841.48
43	43	52.80	-2619.68	-60.54	531.02	0	-838.23	1.8	-834.87	1.8	-688.70	2.12	-841.16
43	44	54.20	-2614.86	-48.84	607.77	0	-710.72	1.8	-1024.59	1.8	-685.81	2.12	-837.04
44	44	54.20	-1701.11	-48.84	168.27	0	-854.60	1.8	-615.03	1.8	-330.10	2.12	-395.87
44	45	55.60	-1701.11	-36.75	228.18	0	-755.40	1.8	-766.99	1.8	-328.51	2.12	-393.07
45	45	55.60	-2055.42	-36.74	18.42	0	-1372.57	1.8	-563.12	1.8	-328.51	2.12	-393.06
45	46	57.00	-2055.42	-24.66	61.41	0	-1300.29	1.8	-675.76	1.8	-326.92	2.12	-390.26
46	46	57.00	-1143.83	-25.22	-378.11	0	-1509.19	1.8	-36.09	1.8	0.00	2.12	0.00
46	47	58.40	-1145.37	-20.33	-347.48	0	-1461.31	1.8	-108.50	1.8	0.00	2.12	0.00
47	47	58.40	-1458.36	-18.92	-527.63	0	-1993.72	1.8	39.33	1.8	0.00	2.12	0.00
47	48	59.80	-1458.36	-13.20	-505.14	0	-1959.46	1.8	-13.06	1.8	0.00	2.12	0.00
48	48	59.80	-1458.36	-13.20	-505.14	0	-1959.46	1.8	-13.06	1.8	0.00	2.12	0.00
48	49	61.20	-1458.36	-7.50	-490.64	0	-1937.36	1.8	-46.83	1.8	0.00	2.12	0.00
49	49	61.20	-1458.36	-7.50	-490.64	0	-1937.36	1.8	-46.83	1.8	0.00	2.12	0.00
49	50	62.60	-1458.36	-1.78	-484.13	0	-1927.45	1.8	-62.00	1.8	0.00	2.12	0.00
50	50	62.60	-1458.36	-1.78	-484.13	0	-1927.45	1.8	-62.00	1.8	0.00	2.12	0.00
50	51	64.00	-1456.62	3.90	-485.62	0	-1928.29	1.8	-57.10	1.8	0.00	2.12	0.00
51	51	64.00	-1456.62	3.90	-485.62	0	-1928.29	1.8	-57.10	1.8	0.00	2.12	0.00
51	52	65.40	-1456.62	9.61	-495.08	0	-1942.70	1.8	-35.07	1.8	0.00	2.12	0.00
52	52	65.40	-1456.62	9.61	-495.08	0	-1942.70	1.8	-35.07	1.8	0.00	2.12	0.00
52	53	66.80	-1456.62	15.33	-512.53	0	-1969.29	1.8	5.58	1.8	0.00	2.12	0.00
53	53	66.80	-1456.62	15.33	-512.53	0	-1969.29	1.8	5.58	1.8	0.00	2.12	0.00
53	54	68.20	-1456.62	21.03	-537.99	0	-2008.09	1.8	64.89	1.8	0.00	2.12	0.00
54	54	68.20	-1456.62	21.03	-537.99	0	-2008.09	1.8	64.89	1.8	0.00	2.12	0.00
54	55	69.60	-1456.62	26.75	-571.42	0	-2059.03	1.8	142.76	1.8	0.00	2.12	0.00
55	55	69.60	-1139.52	26.19	-391.27	0	-1522.82	1.8	-1.68	1.8	0.00	2.12	0.00
55	56	71.00	-1139.52	31.90	-432.73	0	-1588.34	1.8	94.70	1.8	0.00	2.12	0.00
56	56	71.00	-2055.42	32.46	6.79	0	-1348.03	1.8	-676.53	1.8	-311.02	2.12	-362.14
56	57	72.40	-2055.42	44.54	-47.10	0	-1429.84	1.8	-564.05	1.8	-309.43	2.12	-359.34
57	57	72.40	-1701.11	44.54	162.65	0	-812.68	1.8	-767.91	1.8	-309.43	2.12	-359.34
57	58	73.80	-1701.11	56.63	91.82	0	-921.42	1.8	-616.11	1.8	-307.84	2.12	-356.52
58	58	73.80	-2614.86	56.62	531.33	0	-777.54	1.8	-1025.67	1.8	-663.56	2.12	-797.69
58	59	75.20	-2614.86	68.69	443.59	0	-913.18	1.8	-834.59	1.8	-661.96	2.12	-794.87
59	59	75.20	-2339.29	68.69	615.01	0	-420.00	1.8	-1012.37	1.8	-661.96	2.12	-794.87
59	60	76.60	-2343.12	80.32	510.86	0	-583.25	1.8	-783.26	1.8	-661.53	2.12	-793.31
60	60	76.60	-2343.06	80.30	510.94	0	-583.16	1.8	-783.27	1.8	-661.53	2.12	-793.34
60	61	78.00	-2343.06	99.38	385.16	0	-779.73	1.8	-502.38	1.8	-660.12	2.12	-790.83
61	1061	78.00	-2303.37	-88.85	411.27	0	-706.63	1.8	-531.36	1.8	-660.04	2.12	-790.76
61	62	79.10	-2303.37	-73.86	500.75	0	-570.66	1.8	-718.52	1.8	-662.63	2.12	-795.34
62	62	79.10	-2302.99	-73.85	500.75	0	-570.55	1.8	-718.40	1.8	-662.53	2.12	-795.24
62	63	80.20	-2302.99	-64.36	576.79	0	-455.97	1.8	-874.30	1.8	-665.11	2.12	-799.81
63	63	80.20	-2578.03	-64.36	402.61	0	-953.37	1.8	-689.95	1.8	-664.97	2.12	-799.66
63	64	81.30	-2578.03	-54.86	468.17	0	-855.45	1.8	-821.53	1.8	-667.55	2.12	-804.24
64	64	81.30	-2577.33	-54.87	468.11	0	-855.30	1.8	-821.29	1.8	-667.35	2.12	-804.02
64	65	82.40	-2577.33	-45.38	523.26	0	-773.96	1.8	-928.63	1.8	-669.94	2.12	-808.60
65	65	82.40	-1859.54	-45.43	-36.81	0	-1266.79	1.8	-396.36	1.8	-313.97	2.12	-367.16
65	66	83.50	-1859.54	-35.94	7.94	0	-1202.02	1.8	-479.43	1.8	-316.58	2.12	-371.77
66	66	83.50	-1858.58	-36.04	7.84	0	-1232.02	1.8	-449.65	1.8	-290.70	2.12	-336.66
66	67	84.60	-1858.58	-26.54	42.26	0	-1184.83	1.8	-507.46	1.8	-292.40	2.12	-340.04
67	67	84.60	-939.44	-24.83	-397.26	0	-1373.85	1.8	172.25	1.8	0.00	2.12	0.00
67	68	85.70	-939.44	-20.35	-370.54	0	-1332.05	1.8	110.12	1.8	0.00	2.12	0.00
68	68	85.70	-1141.67	-22.06	-489.03	0	-1676.56	1.8	207.79	1.8	0.00	2.12	0.00
68	69	86.80	-1141.67	-17.56	-467.27	0	-1643.39	1.8	157.09	1.8	0.00	2.12	0.00
69	69	86.80	-1141.67	-17.56	-467.27	0	-1643.39	1.8	157.09	1.8	0.00	2.12	0.00
69	70	87.90	-1141.67	-13.08	-450.42	0	-1617.72	1.8	117.84	1.8	0.00	2.12	0.00
70	70	87.90	-1141.67	-13.08	-450.42	0	-1617.72	1.8	117.84	1.8	0.00	2.12	0.00
70	71	89.00	-1141.67	-8.59	-438.52	0	-1599.58	1.8	90.11	1.8	0.00	2.12	0.00
71	71	89.00	-1141.67	-8.59	-438.52	0	-1599.58	1.8	90.11	1.8	0.00	2.12	0.00
71	72	90.10	-1141.67	-4.10	-431.54	0	-1588.95	1.8	73.86	1.8	0.00	2.12	0.00
72	72	90.10	-1141.67	-4.10	-431.54	0	-1588.95	1.8	73.86	1.8	0.00	2.12	0.00
72	73	91.20	-1141.67	0.38	-429.51	0	-1585.85	1.8	69.12	1.8	0.00	2.12	0.00
73	73	91.20	-1141.67	0.38	-429.51	0	-1585.85	1.8	69.12	1.8	0.00	2.12	0.00
73	74	92.30	-1141.67	4.88	-432.40	0	-1590.26	1.8	75.86	1.8	0.00	2.12	0.00
74	74	92.30	-1141.67	4.88	-432.40	0	-1590.26	1.8	75.86	1.8	0.00	2.12	0.00
74	75	93.40	-1141.67	9.36	-440.24	0	-1602.20	1.8	94.11	1.8	0.00	2.12	0.00
75	75	93.40	-1141.67	9.36	-440.24	0	-1613.85	1.8	109.37	1.8	0.00	2.12	0.00
75	76	94.50	-1141.67	13.85	-453.02	0	-1634.19	1.8	139.07	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ+
Construcción sin gradiente en fase constructiva 4
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	13.85	-334.53	0	-1288.19	1.8	21.25	1.8	0.00	2.12	0.00
76	77	95.60	-944.83	18.34	-352.24	0	-1316.37	1.8	62.41	1.8	0.00	2.12	0.00
77	77	95.60	-944.83	18.34	-352.24	0	-1316.37	1.8	62.41	1.8	0.00	2.12	0.00
77	78	96.70	-944.83	22.82	-374.89	0	-1352.40	1.8	115.05	1.8	0.00	2.12	0.00
78	78	96.70	-747.99	22.82	-254.43	0	-1003.26	1.8	-7.36	1.8	0.00	2.12	0.00
78	79	97.80	-747.99	27.32	-282.01	0	-1047.14	1.8	56.74	1.8	0.00	2.12	0.00
79	79	97.80	-747.99	27.32	-282.01	0	-1047.14	1.8	56.74	1.8	0.00	2.12	0.00
79	80	98.90	-747.99	31.80	-314.53	0	-1098.87	1.8	132.31	1.8	0.00	2.12	0.00
80	80	98.90	-472.42	31.80	-140.37	0	-601.32	1.8	-51.86	1.8	0.00	2.12	0.00
80	81	100.00	-472.42	38.20	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	101	0.00	-472.42	-38.21	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	102	1.10	-476.85	-31.89	-140.28	0	-604.73	1.8	-55.61	1.8	0.00	2.12	0.00
102	102	1.10	-752.42	-31.89	-314.45	0	-1102.28	1.8	128.57	1.8	0.00	2.12	0.00
102	103	2.20	-752.42	-27.41	-281.83	0	-1050.39	1.8	52.77	1.8	0.00	2.12	0.00
103	103	2.20	-752.42	-27.41	-281.83	0	-1050.39	1.8	52.77	1.8	0.00	2.12	0.00
103	104	3.30	-752.42	-22.91	-254.16	0	-1006.38	1.8	-11.53	1.8	0.00	2.12	0.00
104	104	3.30	-949.26	-22.91	-374.63	0	-1355.52	1.8	110.88	1.8	0.00	2.12	0.00
104	105	4.40	-949.26	-18.43	-351.90	0	-1319.36	1.8	58.07	1.8	0.00	2.12	0.00
105	105	4.40	-949.26	-18.43	-351.90	0	-1319.36	1.8	58.07	1.8	0.00	2.12	0.00
105	106	5.50	-949.26	-13.94	-334.10	0	-1291.05	1.8	16.70	1.8	0.00	2.12	0.00
106	106	5.50	-1146.10	-13.94	-452.59	0	-1637.05	1.8	134.53	1.8	0.00	2.12	0.00
106	107	6.60	-1146.10	-9.45	-439.72	0	-1616.57	1.8	104.62	1.8	0.00	2.12	0.00
107	107	6.60	-1146.10	-9.45	-439.72	0	-1605.03	1.8	89.29	1.8	0.00	2.12	0.00
107	108	7.70	-1146.10	-4.97	-431.80	0	-1592.96	1.8	70.84	1.8	0.00	2.12	0.00
108	108	7.70	-1146.10	-4.97	-431.80	0	-1592.96	1.8	70.84	1.8	0.00	2.12	0.00
108	109	8.80	-1146.10	-0.47	-428.82	0	-1588.42	1.8	63.90	1.8	0.00	2.12	0.00
109	109	8.80	-1146.10	-0.47	-428.82	0	-1588.42	1.8	63.90	1.8	0.00	2.12	0.00
109	110	9.90	-1146.10	4.01	-430.77	0	-1591.39	1.8	68.44	1.8	0.00	2.12	0.00
110	110	9.90	-1146.10	4.01	-430.77	0	-1591.39	1.8	68.44	1.8	0.00	2.12	0.00
110	111	11.00	-1146.10	8.50	-437.64	0	-1601.87	1.8	84.46	1.8	0.00	2.12	0.00
111	111	11.00	-1146.10	8.50	-437.64	0	-1601.87	1.8	84.46	1.8	0.00	2.12	0.00
111	112	12.10	-1146.10	12.99	-449.46	0	-1619.88	1.8	112.00	1.8	0.00	2.12	0.00
112	112	12.10	-1146.10	12.99	-449.46	0	-1619.88	1.8	112.00	1.8	0.00	2.12	0.00
112	113	13.20	-1146.10	17.47	-466.23	0	-1645.43	1.8	151.06	1.8	0.00	2.12	0.00
113	113	13.20	-1146.10	17.47	-466.23	0	-1645.43	1.8	151.06	1.8	0.00	2.12	0.00
113	114	14.30	-1146.10	21.97	-487.91	0	-1678.47	1.8	201.56	1.8	0.00	2.12	0.00
114	114	14.30	-943.11	22.83	-369.42	0	-1333.34	1.8	104.50	1.8	0.00	2.12	0.00
114	115	15.40	-939.43	24.85	-397.49	0	-1374.20	1.8	172.82	1.8	0.00	2.12	0.00
115	115	15.40	-1858.58	26.54	42.03	0	-1185.04	1.8	-507.41	1.8	-292.36	2.12	-339.96
115	116	16.50	-1858.58	36.04	7.58	0	-1232.24	1.8	-449.60	1.8	-290.66	2.12	-336.58
116	116	16.50	-1858.58	36.04	7.58	0	-1202.07	1.8	-479.03	1.8	-316.23	2.12	-371.35
116	117	17.60	-1858.58	45.53	-37.67	0	-1267.57	1.8	-395.02	1.8	-313.60	2.12	-366.69
117	117	17.60	-2575.50	45.53	522.71	0	-773.92	1.8	-927.91	1.8	-669.31	2.12	-807.87
117	118	18.70	-2575.50	55.02	467.40	0	-855.42	1.8	-820.52	1.8	-666.68	2.12	-803.21
118	118	18.70	-2575.50	55.02	467.40	0	-855.42	1.8	-820.52	1.8	-666.68	2.12	-803.21
118	119	19.80	-2575.50	64.52	401.65	0	-953.52	1.8	-688.89	1.8	-664.05	2.12	-798.56
119	119	19.80	-2299.92	64.52	575.82	0	-455.96	1.8	-873.07	1.8	-664.05	2.12	-798.56
119	120	20.90	-2299.92	74.01	499.60	0	-570.71	1.8	-717.12	1.8	-661.41	2.12	-793.90
120	120	20.90	-2299.92	74.01	499.60	0	-570.71	1.8	-717.12	1.8	-661.41	2.12	-793.90
120	121	22.00	-2299.92	89.00	409.94	0	-706.85	1.8	-529.91	1.8	-658.78	2.12	-789.24
121	1121	22.00	-2339.29	-99.87	383.87	0	-779.82	1.8	-500.84	1.8	-658.78	2.12	-789.24
121	122	23.40	-2339.29	-80.79	510.34	0	-582.57	1.8	-781.93	1.8	-660.37	2.12	-792.06
122	122	23.40	-2339.29	-80.79	510.34	0	-582.57	1.8	-781.93	1.8	-660.37	2.12	-792.06
122	123	24.80	-2339.29	-68.70	615.00	0	-420.01	1.8	-1012.37	1.8	-661.96	2.12	-794.87
123	123	24.80	-2614.86	-68.69	443.60	0	-913.17	1.8	-834.60	1.8	-661.96	2.12	-794.87
123	124	26.20	-2614.86	-56.62	531.32	0	-777.55	1.8	-1025.67	1.8	-663.55	2.12	-797.68
124	124	26.20	-1701.11	-56.62	91.81	0	-921.43	1.8	-616.11	1.8	-307.84	2.12	-356.52
124	125	27.60	-1701.11	-44.53	162.63	0	-812.70	1.8	-767.91	1.8	-309.43	2.12	-359.33
125	125	27.60	-2055.42	-44.54	-47.12	0	-1429.86	1.8	-564.04	1.8	-309.43	2.12	-359.33
125	126	29.00	-2055.42	-32.46	6.79	0	-1348.03	1.8	-676.53	1.8	-311.02	2.12	-362.14
126	126	29.00	-1139.52	-31.90	-432.73	0	-1588.34	1.8	94.70	1.8	0.00	2.12	0.00
126	127	30.40	-1142.78	-28.07	-391.16	0	-1525.31	1.8	-4.59	1.8	0.00	2.12	0.00
127	127	30.40	-1460.38	-26.83	-571.31	0	-2061.92	1.8	139.43	1.8	0.00	2.12	0.00
127	128	31.80	-1460.38	-21.11	-537.77	0	-2010.82	1.8	61.30	1.8	0.00	2.12	0.00
128	128	31.80	-1460.38	-21.11	-537.77	0	-2010.82	1.8	61.30	1.8	0.00	2.12	0.00
128	129	33.20	-1460.38	-15.41	-512.19	0	-1971.84	1.8	1.71	1.8	0.00	2.12	0.00
129	129	33.20	-1460.38	-15.41	-512.19	0	-1971.84	1.8	1.71	1.8	0.00	2.12	0.00
129	130	34.60	-1460.38	-9.69	-494.62	0	-1945.08	1.8	-39.19	1.8	0.00	2.12	0.00
130	130	34.60	-1460.38	-9.69	-494.62	0	-1945.08	1.8	-39.19	1.8	0.00	2.12	0.00
130	131	36.00	-1460.38	-3.98	-485.04	0	-1930.48	1.8	-61.51	1.8	0.00	2.12	0.00
131	131	36.00	-1460.38	-3.98	-485.04	0	-1930.48	1.8	-61.51	1.8	0.00	2.12	0.00
131	132	37.40	-1460.38	1.73	-483.48	0	-1928.10	1.8	-65.15	1.8	0.00	2.12	0.00
132	132	37.40	-1460.38	1.73	-483.48	0	-1928.10	1.8	-65.15	1.8	0.00	2.12	0.00
132	133	38.80	-1460.38	7.45	-489.90	0	-1937.88	1.8	-50.19	1.8	0.00	2.12	0.00
133	133	38.80	-1460.38	7.45	-489.90	0	-1937.88	1.8	-50.19	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ+

11/09/03

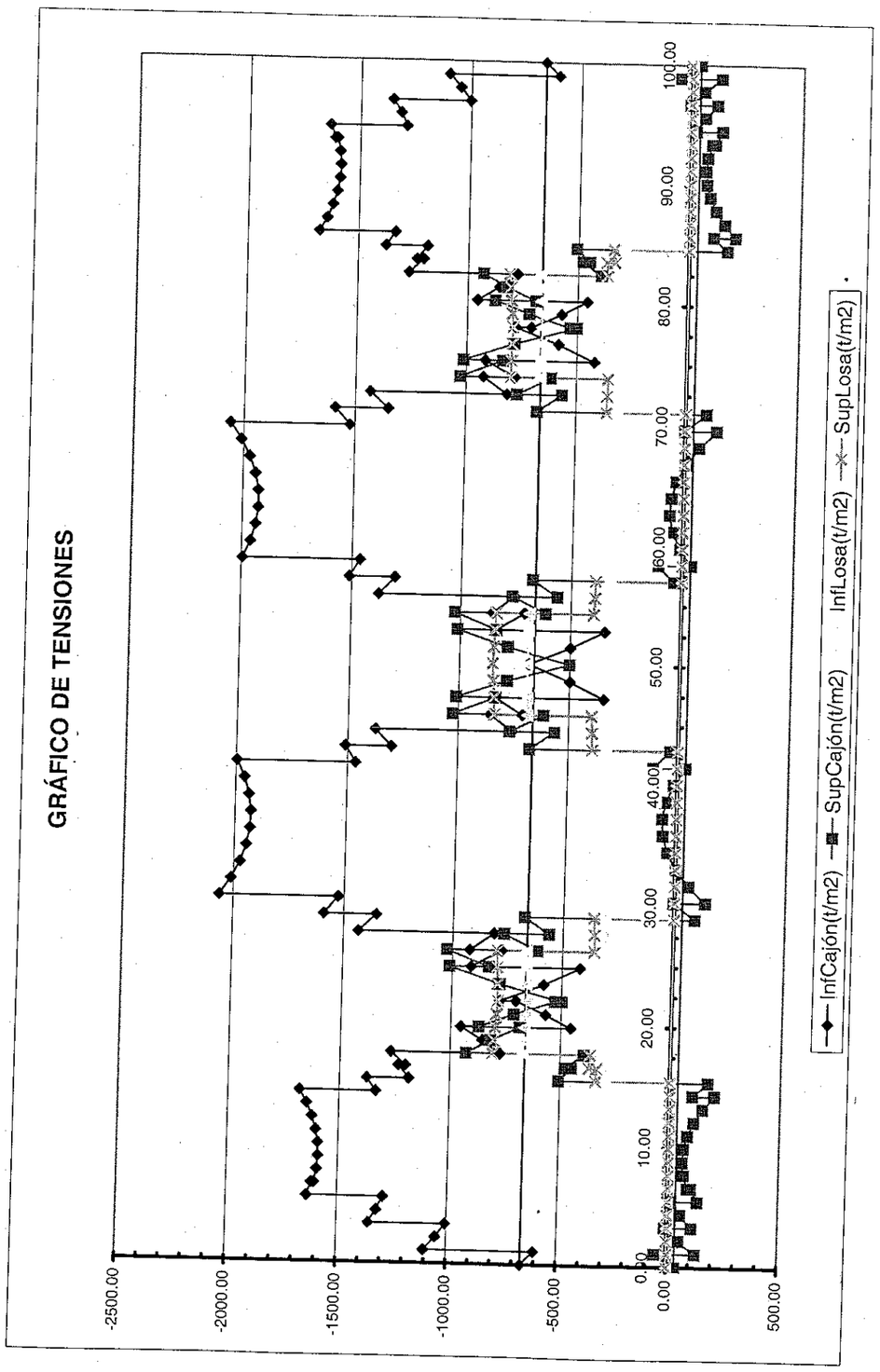
CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ+
Construcción sin gradiente en fase constructiva 4
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	-8.59	-438.51	0	-1599.57	1.8	90.09	1.8	0.00	2.12	0.00
171	172	90.10	-1141.67	-4.10	-431.54	0	-1588.95	1.8	73.86	1.8	0.00	2.12	0.00
172	172	90.10	-1141.67	-4.10	-431.54	0	-1588.95	1.8	73.86	1.8	0.00	2.12	0.00
172	173	91.20	-1141.67	0.38	-429.51	0	-1585.85	1.8	69.12	1.8	0.00	2.12	0.00
173	173	91.20	-1141.67	0.38	-429.51	0	-1585.85	1.8	69.12	1.8	0.00	2.12	0.00
173	174	92.30	-1141.67	4.88	-432.40	0	-1590.26	1.8	75.86	1.8	0.00	2.12	0.00
174	174	92.30	-1141.67	4.88	-432.40	0	-1590.26	1.8	75.86	1.8	0.00	2.12	0.00
174	175	93.40	-1141.67	9.36	-440.24	0	-1602.20	1.8	94.11	1.8	0.00	2.12	0.00
175	175	93.40	-1141.67	9.36	-440.24	0	-1613.85	1.8	109.37	1.8	0.00	2.12	0.00
175	176	94.50	-1141.67	13.85	-453.02	0	-1634.19	1.8	139.07	1.8	0.00	2.12	0.00
176	176	94.50	-944.83	13.85	-334.53	0	-1288.19	1.8	21.25	1.8	0.00	2.12	0.00
176	177	95.60	-944.83	18.34	-352.24	0	-1316.37	1.8	62.41	1.8	0.00	2.12	0.00
177	177	95.60	-944.83	18.34	-352.24	0	-1316.37	1.8	62.41	1.8	0.00	2.12	0.00
177	178	96.70	-944.83	22.82	-374.89	0	-1352.40	1.8	115.05	1.8	0.00	2.12	0.00
178	178	96.70	-747.99	22.82	-254.43	0	-1003.26	1.8	-7.36	1.8	0.00	2.12	0.00
178	179	97.80	-747.99	27.32	-282.01	0	-1047.14	1.8	56.74	1.8	0.00	2.12	0.00
179	179	97.80	-747.99	27.32	-282.01	0	-1047.14	1.8	56.74	1.8	0.00	2.12	0.00
179	180	98.90	-747.99	31.80	-314.53	0	-1098.87	1.8	132.31	1.8	0.00	2.12	0.00
180	180	98.90	-472.42	31.80	-140.37	0	-601.32	1.8	-51.86	1.8	0.00	2.12	0.00
180	181	100.00	-472.42	38.20	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ+

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ-

Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-38.21	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
1	2	1.10	-517.71	-30.71	-160.42	0	-669.45	1.8	-41.53	1.8	0.00	2.12	0.00
2	2	1.10	-822.30	-30.71	-352.91	0	-1219.38	1.8	162.03	1.8	0.00	2.12	0.00
2	3	2.20	-822.30	-26.23	-321.59	0	-1169.56	1.8	89.25	1.8	0.00	2.12	0.00
3	3	2.20	-822.30	-26.23	-321.59	0	-1169.56	1.8	89.25	1.8	0.00	2.12	0.00
3	4	3.30	-822.30	-21.73	-295.22	0	-1127.62	1.8	27.98	1.8	0.00	2.12	0.00
4	4	3.30	-1039.86	-21.73	-428.37	0	-1513.51	1.8	163.28	1.8	0.00	2.12	0.00
4	5	4.40	-1039.86	-17.25	-406.96	0	-1479.44	1.8	113.51	1.8	0.00	2.12	0.00
5	5	4.40	-1039.86	-17.25	-406.96	0	-1479.44	1.8	113.51	1.8	0.00	2.12	0.00
5	6	5.50	-1039.86	-12.76	-390.46	0	-1453.19	1.8	75.17	1.8	0.00	2.12	0.00
6	6	5.50	-1257.42	-12.76	-521.42	0	-1835.61	1.8	205.40	1.8	0.00	2.12	0.00
6	7	6.60	-1257.42	-8.27	-509.84	0	-1817.19	1.8	178.49	1.8	0.00	2.12	0.00
7	7	6.60	-1257.42	-8.27	-509.84	0	-1802.69	1.8	161.83	1.8	0.00	2.12	0.00
7	8	7.70	-1257.42	-3.79	-503.22	0	-1792.61	1.8	146.41	1.8	0.00	2.12	0.00
8	8	7.70	-1257.42	-3.79	-503.22	0	-1792.61	1.8	146.41	1.8	0.00	2.12	0.00
8	9	8.80	-1257.42	0.71	-501.54	0	-1790.05	1.8	142.50	1.8	0.00	2.12	0.00
9	9	8.80	-1257.42	0.71	-501.54	0	-1790.05	1.8	142.50	1.8	0.00	2.12	0.00
9	10	9.90	-1257.42	5.19	-504.79	0	-1795.00	1.8	150.07	1.8	0.00	2.12	0.00
10	10	9.90	-1257.42	5.19	-504.79	0	-1795.00	1.8	150.07	1.8	0.00	2.12	0.00
10	11	11.00	-1257.42	9.68	-512.98	0	-1807.47	1.8	169.13	1.8	0.00	2.12	0.00
11	11	11.00	-1257.42	9.68	-512.98	0	-1807.47	1.8	169.13	1.8	0.00	2.12	0.00
11	12	12.10	-1257.42	14.17	-526.10	0	-1827.46	1.8	199.69	1.8	0.00	2.12	0.00
12	12	12.10	-1257.42	14.17	-526.10	0	-1827.46	1.8	199.69	1.8	0.00	2.12	0.00
12	13	13.20	-1257.42	18.65	-544.18	0	-1855.01	1.8	241.81	1.8	0.00	2.12	0.00
13	13	13.20	-1257.42	18.65	-544.18	0	-1855.01	1.8	241.81	1.8	0.00	2.12	0.00
13	14	14.30	-1257.42	23.15	-567.15	0	-1890.01	1.8	295.32	1.8	0.00	2.12	0.00
14	14	14.30	-1034.63	18.73	-436.18	0	-1511.51	1.8	186.63	1.8	0.00	2.12	0.00
14	15	15.40	-1038.31	25.67	-462.67	0	-1555.96	1.8	245.22	1.8	0.00	2.12	0.00
15	15	15.40	-1871.02	27.54	-65.01	0	-1366.36	1.8	-433.64	1.8	-259.76	2.12	-298.10
15	16	16.50	-1871.02	37.04	-100.53	0	-1414.50	1.8	-375.63	1.8	-257.89	2.12	-294.37
16	16	16.50	-1871.02	37.04	-100.54	0	-1390.54	1.8	-399.01	1.8	-278.19	2.12	-321.98
16	17	17.60	-1871.02	46.53	-146.92	0	-1457.16	1.8	-314.59	1.8	-275.29	2.12	-316.84
17	17	17.60	-2480.19	46.53	384.30	0	-940.41	1.8	-821.44	1.8	-597.12	2.12	-715.99
17	18	18.70	-2480.19	56.02	327.90	0	-1022.97	1.8	-713.74	1.8	-594.22	2.12	-710.85
18	18	18.70	-2480.18	56.02	327.90	0	-1022.96	1.8	-713.74	1.8	-594.21	2.12	-710.85
18	19	19.80	-2480.18	65.52	261.06	0	-1122.13	1.8	-581.79	1.8	-591.30	2.12	-705.70
19	19	19.80	-2175.60	65.52	453.55	0	-572.20	1.8	-785.35	1.8	-591.30	2.12	-705.70
19	20	20.90	-2175.60	75.01	376.26	0	-688.00	1.8	-629.08	1.8	-588.39	2.12	-700.56
20	20	20.90	-2175.60	75.01	376.26	0	-688.00	1.8	-629.08	1.8	-588.39	2.12	-700.56
20	21	22.00	-2175.60	90.00	285.50	0	-825.20	1.8	-441.56	1.8	-585.48	2.12	-695.41
21	1021	22.00	-2219.11	-100.35	256.69	0	-905.84	1.8	-409.43	1.8	-585.48	2.12	-695.41
21	22	23.40	-2219.11	-81.27	383.82	0	-707.96	1.8	-690.71	1.8	-587.24	2.12	-698.52
22	22	23.40	-2219.11	-81.27	383.82	0	-707.96	1.8	-690.71	1.8	-587.24	2.12	-698.52
22	23	24.80	-2219.11	-69.18	489.15	0	-544.74	1.8	-921.34	1.8	-589.00	2.12	-701.63
23	23	24.80	-2523.70	-69.17	299.70	0	-1089.83	1.8	-724.86	1.8	-589.00	2.12	-701.63
23	24	26.20	-2523.70	-57.10	388.08	0	-953.57	1.8	-916.12	1.8	-590.76	2.12	-704.74
24	24	26.20	-1696.97	-57.10	-9.57	0	-1083.75	1.8	-545.56	1.8	-268.92	2.12	-305.59
24	25	27.60	-1696.97	-45.01	61.92	0	-974.36	1.8	-697.56	1.8	-270.68	2.12	-308.70
25	25	27.60	-2088.58	-45.02	-169.91	0	-1656.49	1.8	-472.24	1.8	-270.68	2.12	-308.70
25	26	29.00	-2088.58	-32.94	-115.34	0	-1574.02	1.8	-584.92	1.8	-272.44	2.12	-311.81
26	26	29.00	-1259.46	-32.32	-513.00	0	-1810.77	1.8	185.35	1.8	0.00	2.12	0.00
26	27	30.40	-1256.21	-24.73	-471.02	0	-1741.79	1.8	90.42	1.8	0.00	2.12	0.00
27	27	30.40	-1606.18	-27.15	-670.13	0	-2331.46	1.8	250.69	1.8	0.00	2.12	0.00
27	28	31.80	-1606.18	-21.43	-636.15	0	-2279.69	1.8	171.54	1.8	0.00	2.12	0.00
28	28	31.80	-1606.18	-21.43	-636.15	0	-2279.69	1.8	171.54	1.8	0.00	2.12	0.00
28	29	33.20	-1606.18	-15.73	-610.14	0	-2240.04	1.8	110.93	1.8	0.00	2.12	0.00
29	29	33.20	-1606.18	-15.73	-610.14	0	-2240.04	1.8	110.93	1.8	0.00	2.12	0.00
29	30	34.60	-1606.18	-10.01	-592.14	0	-2212.61	1.8	69.00	1.8	0.00	2.12	0.00
30	30	34.60	-1606.18	-10.01	-592.14	0	-2212.61	1.8	69.00	1.8	0.00	2.12	0.00
30	31	36.00	-1606.18	-4.30	-582.13	0	-2197.36	1.8	45.69	1.8	0.00	2.12	0.00
31	31	36.00	-1606.18	-4.30	-582.13	0	-2197.36	1.8	45.69	1.8	0.00	2.12	0.00
31	32	37.40	-1606.18	1.41	-580.11	0	-2194.29	1.8	40.98	1.8	0.00	2.12	0.00
32	32	37.40	-1606.18	1.41	-580.11	0	-2194.29	1.8	40.98	1.8	0.00	2.12	0.00
32	33	38.80	-1606.18	7.13	-586.09	0	-2203.40	1.8	54.91	1.8	0.00	2.12	0.00
33	33	38.80	-1606.18	7.13	-586.09	0	-2203.40	1.8	54.91	1.8	0.00	2.12	0.00
33	34	40.20	-1606.18	12.83	-600.08	0	-2224.72	1.8	87.51	1.8	0.00	2.12	0.00
34	34	40.20	-1606.18	12.83	-600.08	0	-2224.72	1.8	87.51	1.8	0.00	2.12	0.00
34	35	41.60	-1606.18	18.55	-622.05	0	-2258.20	1.8	138.68	1.8	0.00	2.12	0.00
35	35	41.60	-1260.90	17.35	-422.94	0	-1672.79	1.8	-25.45	1.8	0.00	2.12	0.00
35	36	43.00	-1264.23	24.79	-451.80	0	-1721.94	1.8	38.84	1.8	0.00	2.12	0.00
36	36	43.00	-2088.58	24.18	-54.14	0	-1519.90	1.8	-586.07	1.8	-290.01	2.12	-342.88
36	37	44.40	-2088.58	36.26	-96.44	0	-1591.52	1.8	-473.63	1.8	-291.77	2.12	-345.99
37	37	44.40	-1696.97	36.27	135.37	0	-909.40	1.8	-698.95	1.8	-291.77	2.12	-345.98
37	38	45.80	-1696.97	48.36	76.15	0	-1007.94	1.8	-547.19	1.8	-293.53	2.12	-349.09
38	38	45.80	-2523.70	48.36	473.80	0	-877.76	1.8	-917.75	1.8	-615.36	2.12	-748.24

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ-
Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	60.43	397.65	0	-1003.21	1.8	-726.71	1.8	-617.12	2.12	-751.35
39	39	47.20	-2219.11	60.43	587.11	0	-458.11	1.8	-923.21	1.8	-617.12	2.12	-751.35
39	40	48.60	-2212.66	73.02	493.43	0	-609.08	1.8	-690.65	1.8	-617.00	2.12	-752.46
40	40	48.60	-2212.49	73.03	493.36	0	-609.10	1.8	-690.58	1.8	-616.93	2.12	-752.38
40	41	50.00	-2212.49	92.11	377.77	0	-796.84	1.8	-409.32	1.8	-618.51	2.12	-755.17
41	1041	50.00	-2212.70	-92.03	377.76	0	-796.91	1.8	-409.38	1.8	-618.56	2.12	-755.22
41	42	51.40	-2212.70	-72.95	493.24	0	-609.27	1.8	-690.61	1.8	-616.96	2.12	-752.39
42	42	51.40	-2213.30	-72.94	493.29	0	-609.41	1.8	-690.81	1.8	-617.13	2.12	-752.57
42	43	52.80	-2213.30	-60.85	586.96	0	-456.47	1.8	-921.37	1.8	-615.52	2.12	-749.73
43	43	52.80	-2518.88	-60.80	397.60	0	-1001.77	1.8	-725.22	1.8	-615.82	2.12	-750.04
43	44	54.20	-2523.70	-48.36	473.79	0	-877.77	1.8	-917.74	1.8	-615.36	2.12	-748.24
44	44	54.20	-1696.97	-48.36	76.13	0	-1007.95	1.8	-547.19	1.8	-293.52	2.12	-349.09
44	45	55.60	-1696.97	-36.27	135.38	0	-909.39	1.8	-698.95	1.8	-291.77	2.12	-345.99
45	45	55.60	-2088.58	-36.26	-96.46	0	-1591.53	1.8	-473.63	1.8	-291.77	2.12	-345.98
45	46	57.00	-2088.58	-24.18	-54.13	0	-1519.89	1.8	-586.07	1.8	-290.01	2.12	-342.88
46	46	57.00	-1264.23	-24.80	-451.79	0	-1721.93	1.8	38.82	1.8	0.00	2.12	0.00
46	47	58.40	-1262.69	-18.27	-422.04	0	-1672.88	1.8	-29.00	1.8	0.00	2.12	0.00
47	47	58.40	-1608.20	-18.50	-621.15	0	-2258.47	1.8	134.96	1.8	0.00	2.12	0.00
47	48	59.80	-1608.20	-12.78	-599.26	0	-2225.11	1.8	83.96	1.8	0.00	2.12	0.00
48	48	59.80	-1608.20	-12.78	-599.26	0	-2225.11	1.8	83.96	1.8	0.00	2.12	0.00
48	49	61.20	-1608.20	-7.08	-585.36	0	-2203.93	1.8	51.58	1.8	0.00	2.12	0.00
49	49	61.20	-1608.20	-7.08	-585.36	0	-2203.93	1.8	51.58	1.8	0.00	2.12	0.00
49	50	62.60	-1608.20	-1.36	-579.45	0	-2194.93	1.8	37.81	1.8	0.00	2.12	0.00
50	50	62.60	-1608.20	-1.36	-579.45	0	-2194.93	1.8	37.81	1.8	0.00	2.12	0.00
50	51	64.00	-1609.94	4.38	-581.56	0	-2199.57	1.8	41.30	1.8	0.00	2.12	0.00
51	51	64.00	-1609.94	4.38	-581.56	0	-2199.57	1.8	41.30	1.8	0.00	2.12	0.00
51	52	65.40	-1609.94	10.09	-591.68	0	-2214.99	1.8	64.88	1.8	0.00	2.12	0.00
52	52	65.40	-1609.94	10.09	-591.68	0	-2214.99	1.8	64.88	1.8	0.00	2.12	0.00
52	53	66.80	-1609.94	15.81	-609.79	0	-2242.59	1.8	107.06	1.8	0.00	2.12	0.00
53	53	66.80	-1609.94	15.81	-609.79	0	-2242.59	1.8	107.06	1.8	0.00	2.12	0.00
53	54	68.20	-1609.94	21.51	-635.91	0	-2282.39	1.8	167.91	1.8	0.00	2.12	0.00
54	54	68.20	-1609.94	21.51	-635.91	0	-2282.39	1.8	167.91	1.8	0.00	2.12	0.00
54	55	69.60	-1609.94	27.23	-670.00	0	-2334.33	1.8	247.32	1.8	0.00	2.12	0.00
55	55	69.60	-1259.46	26.61	-470.89	0	-1744.25	1.8	87.46	1.8	0.00	2.12	0.00
55	56	71.00	-1259.46	32.32	-513.01	0	-1810.78	1.8	185.38	1.8	0.00	2.12	0.00
56	56	71.00	-2088.58	32.94	-115.35	0	-1574.03	1.8	-584.91	1.8	-272.44	2.12	-311.81
56	57	72.40	-2088.58	45.02	-169.90	0	-1656.48	1.8	-472.24	1.8	-270.68	2.12	-308.70
57	57	72.40	-1696.97	45.02	61.93	0	-974.35	1.8	-697.56	1.8	-270.68	2.12	-308.70
57	58	73.80	-1696.97	57.11	-9.56	0	-1083.74	1.8	-545.57	1.8	-268.92	2.12	-305.59
58	58	73.80	-2523.70	57.10	388.09	0	-953.56	1.8	-916.12	1.8	-590.76	2.12	-704.75
58	59	75.20	-2523.70	69.17	299.69	0	-1089.84	1.8	-724.85	1.8	-589.00	2.12	-701.63
59	59	75.20	-2219.11	69.17	489.15	0	-544.74	1.8	-921.34	1.8	-589.00	2.12	-701.63
59	60	76.60	-2215.29	81.73	383.30	0	-707.27	1.8	-689.39	1.8	-586.09	2.12	-697.27
60	60	76.60	-2215.34	81.76	383.22	0	-707.37	1.8	-689.38	1.8	-586.08	2.12	-697.25
60	61	78.00	-2215.34	100.84	255.40	0	-905.93	1.8	-407.89	1.8	-584.15	2.12	-693.83
61	1061	78.00	-2172.15	-90.15	284.18	0	-825.41	1.8	-440.11	1.8	-584.22	2.12	-693.90
61	62	79.10	-2172.15	-75.16	375.09	0	-688.06	1.8	-627.68	1.8	-587.17	2.12	-699.11
62	62	79.10	-2172.53	-75.17	375.09	0	-688.18	1.8	-627.80	1.8	-587.28	2.12	-699.21
62	63	80.20	-2172.53	-65.68	452.57	0	-572.20	1.8	-784.12	1.8	-590.23	2.12	-704.44
63	63	80.20	-2477.65	-65.68	260.11	0	-1122.26	1.8	-580.73	1.8	-590.38	2.12	-704.60
63	64	81.30	-2477.65	-56.18	327.13	0	-1022.94	1.8	-712.73	1.8	-593.34	2.12	-709.82
64	64	81.30	-2478.35	-56.17	327.17	0	-1023.10	1.8	-712.96	1.8	-593.54	2.12	-710.03
64	65	82.40	-2478.35	-46.68	383.74	0	-940.38	1.8	-820.71	1.8	-596.49	2.12	-715.25
65	65	82.40	-1870.06	-46.63	-146.97	0	-1456.64	1.8	-315.15	1.8	-274.91	2.12	-316.37
65	66	83.50	-1870.06	-37.14	-100.90	0	-1390.59	1.8	-398.61	1.8	-277.85	2.12	-321.57
66	66	83.50	-1871.02	-37.06	-100.80	0	-1414.73	1.8	-375.58	1.8	-257.84	2.12	-294.28
66	67	84.60	-1871.02	-27.56	-65.24	0	-1366.57	1.8	-433.60	1.8	-259.72	2.12	-298.02
67	67	84.60	-1038.30	-25.67	-462.90	0	-1556.32	1.8	245.78	1.8	0.00	2.12	0.00
67	68	85.70	-1038.30	-21.19	-435.06	0	-1512.80	1.8	181.01	1.8	0.00	2.12	0.00
68	68	85.70	-1261.85	-23.08	-566.03	0	-1891.92	1.8	289.09	1.8	0.00	2.12	0.00
68	69	86.80	-1261.85	-18.58	-543.13	0	-1857.03	1.8	235.76	1.8	0.00	2.12	0.00
69	69	86.80	-1261.85	-18.58	-543.13	0	-1857.03	1.8	235.76	1.8	0.00	2.12	0.00
69	70	87.90	-1261.85	-14.10	-525.16	0	-1829.64	1.8	193.89	1.8	0.00	2.12	0.00
70	70	87.90	-1261.85	-14.10	-525.16	0	-1829.64	1.8	193.89	1.8	0.00	2.12	0.00
70	71	89.00	-1261.85	-9.61	-512.12	0	-1809.78	1.8	163.53	1.8	0.00	2.12	0.00
71	71	89.00	-1261.85	-9.61	-512.12	0	-1809.78	1.8	163.53	1.8	0.00	2.12	0.00
71	72	90.10	-1261.85	-5.12	-504.02	0	-1797.43	1.8	144.65	1.8	0.00	2.12	0.00
72	72	90.10	-1261.85	-5.12	-504.02	0	-1797.43	1.8	144.65	1.8	0.00	2.12	0.00
72	73	91.20	-1261.85	-0.64	-500.85	0	-1792.61	1.8	137.28	1.8	0.00	2.12	0.00
73	73	91.20	-1261.85	-0.64	-500.85	0	-1792.61	1.8	137.28	1.8	0.00	2.12	0.00
73	74	92.30	-1261.85	3.86	-502.62	0	-1795.30	1.8	141.39	1.8	0.00	2.12	0.00
74	74	92.30	-1261.85	3.86	-502.62	0	-1795.30	1.8	141.39	1.8	0.00	2.12	0.00
74	75	93.40	-1261.85	8.34	-509.33	0	-1805.52	1.8	157.01	1.8	0.00	2.12	0.00
75	75	93.40	-1261.85	8.34	-509.33	0	-1819.91	1.8	173.74	1.8	0.00	2.12	0.00
75	76	94.50	-1261.85	12.83	-520.98	0	-1838.45	1.8	200.83	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ-
Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	12.83	-390.01	0	-1456.04	1.8	70.60	1.8	0.00	2.12	0.00
76	77	95.60	-1044.29	17.32	-406.60	0	-1482.42	1.8	109.14	1.8	0.00	2.12	0.00
77	77	95.60	-1044.29	17.32	-406.60	0	-1482.42	1.8	109.14	1.8	0.00	2.12	0.00
77	78	96.70	-1044.29	21.80	-428.13	0	-1516.66	1.8	159.16	1.8	0.00	2.12	0.00
78	78	96.70	-826.73	21.80	-294.98	0	-1130.77	1.8	23.86	1.8	0.00	2.12	0.00
78	79	97.80	-826.73	26.30	-321.43	0	-1172.85	1.8	85.33	1.8	0.00	2.12	0.00
79	79	97.80	-826.73	26.30	-321.43	0	-1172.85	1.8	85.33	1.8	0.00	2.12	0.00
79	80	98.90	-826.73	30.78	-352.83	0	-1222.79	1.8	158.28	1.8	0.00	2.12	0.00
80	80	98.90	-522.14	30.78	-160.33	0	-672.86	1.8	-45.28	1.8	0.00	2.12	0.00
80	81	100.00	-522.14	38.20	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	101	0.00	-522.14	-38.21	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	102	1.10	-517.71	-30.71	-160.42	0	-669.45	1.8	-41.53	1.8	0.00	2.12	0.00
102	102	1.10	-822.30	-30.71	-352.91	0	-1219.38	1.8	162.03	1.8	0.00	2.12	0.00
102	103	2.20	-822.30	-26.23	-321.59	0	-1169.56	1.8	89.25	1.8	0.00	2.12	0.00
103	103	2.20	-822.30	-26.23	-321.59	0	-1169.56	1.8	89.25	1.8	0.00	2.12	0.00
103	104	3.30	-822.30	-21.73	-295.22	0	-1127.62	1.8	27.98	1.8	0.00	2.12	0.00
104	104	3.30	-1039.86	-21.73	-428.37	0	-1513.51	1.8	163.28	1.8	0.00	2.12	0.00
104	105	4.40	-1039.86	-17.25	-406.94	0	-1479.42	1.8	113.49	1.8	0.00	2.12	0.00
105	105	4.40	-1039.86	-17.25	-406.94	0	-1479.42	1.8	113.49	1.8	0.00	2.12	0.00
105	106	5.50	-1039.86	-12.76	-390.45	0	-1453.18	1.8	75.15	1.8	0.00	2.12	0.00
106	106	5.50	-1257.42	-12.76	-521.41	0	-1835.59	1.8	205.37	1.8	0.00	2.12	0.00
106	107	6.60	-1257.42	-8.27	-509.84	0	-1817.19	1.8	178.49	1.8	0.00	2.12	0.00
107	107	6.60	-1257.42	-8.27	-509.84	0	-1802.69	1.8	161.83	1.8	0.00	2.12	0.00
107	108	7.70	-1257.42	-3.79	-503.22	0	-1792.61	1.8	146.41	1.8	0.00	2.12	0.00
108	108	7.70	-1257.42	-3.79	-503.22	0	-1792.61	1.8	146.41	1.8	0.00	2.12	0.00
108	109	8.80	-1257.42	0.71	-501.54	0	-1790.05	1.8	142.50	1.8	0.00	2.12	0.00
109	109	8.80	-1257.42	0.71	-501.54	0	-1790.05	1.8	142.50	1.8	0.00	2.12	0.00
109	110	9.90	-1257.42	5.19	-504.79	0	-1795.00	1.8	150.07	1.8	0.00	2.12	0.00
110	110	9.90	-1257.42	5.19	-504.79	0	-1795.00	1.8	150.07	1.8	0.00	2.12	0.00
110	111	11.00	-1257.42	9.68	-512.98	0	-1807.47	1.8	169.13	1.8	0.00	2.12	0.00
111	111	11.00	-1257.42	9.68	-512.98	0	-1807.47	1.8	169.13	1.8	0.00	2.12	0.00
111	112	12.10	-1257.42	14.17	-526.10	0	-1827.46	1.8	199.69	1.8	0.00	2.12	0.00
112	112	12.10	-1257.42	14.17	-526.10	0	-1827.46	1.8	199.69	1.8	0.00	2.12	0.00
112	113	13.20	-1257.42	18.65	-544.17	0	-1854.99	1.8	241.79	1.8	0.00	2.12	0.00
113	113	13.20	-1257.42	18.65	-544.17	0	-1854.99	1.8	241.79	1.8	0.00	2.12	0.00
113	114	14.30	-1257.42	23.15	-567.15	0	-1890.01	1.8	295.32	1.8	0.00	2.12	0.00
114	114	14.30	-1034.63	18.73	-436.18	0	-1511.51	1.8	186.63	1.8	0.00	2.12	0.00
114	115	15.40	-1038.31	25.67	-462.67	0	-1555.96	1.8	245.22	1.8	0.00	2.12	0.00
115	115	15.40	-1871.02	27.54	-65.01	0	-1366.36	1.8	-433.64	1.8	-259.76	2.12	-298.10
115	116	16.50	-1871.02	37.04	-100.54	0	-1414.51	1.8	-375.62	1.8	-257.88	2.12	-294.36
116	116	16.50	-1871.02	37.04	-100.54	0	-1390.54	1.8	-399.01	1.8	-278.19	2.12	-321.98
116	117	17.60	-1871.02	46.53	-146.93	0	-1457.17	1.8	-314.58	1.8	-275.28	2.12	-316.84
117	117	17.60	-2480.18	46.53	384.31	0	-940.40	1.8	-821.44	1.8	-597.12	2.12	-715.99
117	118	18.70	-2480.18	56.02	327.90	0	-1022.96	1.8	-713.74	1.8	-594.21	2.12	-710.85
118	118	18.70	-2480.18	56.02	327.90	0	-1022.96	1.8	-713.74	1.8	-594.21	2.12	-710.85
118	119	19.80	-2480.18	65.52	261.07	0	-1122.12	1.8	-581.79	1.8	-591.30	2.12	-705.70
119	119	19.80	-2175.60	65.52	453.56	0	-572.19	1.8	-785.36	1.8	-591.30	2.12	-705.70
119	120	20.90	-2175.60	75.01	376.26	0	-688.00	1.8	-629.08	1.8	-588.39	2.12	-700.56
120	120	20.90	-2175.60	75.01	376.26	0	-688.00	1.8	-629.08	1.8	-588.39	2.12	-700.56
120	121	22.00	-2175.60	90.00	285.50	0	-825.20	1.8	-441.56	1.8	-585.48	2.12	-695.41
121	1121	22.00	-2219.11	-100.35	256.69	0	-905.84	1.8	-409.43	1.8	-585.48	2.12	-695.41
121	122	23.40	-2219.11	-81.27	383.82	0	-707.96	1.8	-690.71	1.8	-587.24	2.12	-698.52
122	122	23.40	-2219.11	-81.27	383.82	0	-707.96	1.8	-690.71	1.8	-587.24	2.12	-698.52
122	123	24.80	-2219.11	-69.18	489.14	0	-544.75	1.8	-921.34	1.8	-589.00	2.12	-701.63
123	123	24.80	-2523.70	-69.17	299.70	0	-1089.83	1.8	-724.86	1.8	-589.00	2.12	-701.63
123	124	26.20	-2523.70	-57.10	388.08	0	-953.57	1.8	-916.12	1.8	-590.76	2.12	-704.74
124	124	26.20	-1696.97	-57.10	-9.57	0	-1083.75	1.8	-545.56	1.8	-268.92	2.12	-305.59
124	125	27.60	-1696.97	-45.01	61.91	0	-974.37	1.8	-697.56	1.8	-270.68	2.12	-308.69
125	125	27.60	-2088.58	-45.02	-169.92	0	-1656.50	1.8	-472.24	1.8	-270.68	2.12	-308.69
125	126	29.00	-2088.58	-32.94	-115.35	0	-1574.03	1.8	-584.91	1.8	-272.44	2.12	-311.81
126	126	29.00	-1259.46	-32.32	-513.01	0	-1810.78	1.8	185.38	1.8	0.00	2.12	0.00
126	127	30.40	-1256.21	-24.73	-471.02	0	-1741.79	1.8	90.42	1.8	0.00	2.12	0.00
127	127	30.40	-1606.18	-27.15	-670.13	0	-2331.46	1.8	250.69	1.8	0.00	2.12	0.00
127	128	31.80	-1606.18	-21.43	-636.15	0	-2279.69	1.8	171.54	1.8	0.00	2.12	0.00
128	128	31.80	-1606.18	-21.43	-636.15	0	-2279.69	1.8	171.54	1.8	0.00	2.12	0.00
128	129	33.20	-1606.18	-15.73	-610.14	0	-2240.04	1.8	110.93	1.8	0.00	2.12	0.00
129	129	33.20	-1606.18	-15.73	-610.14	0	-2240.04	1.8	110.93	1.8	0.00	2.12	0.00
129	130	34.60	-1606.18	-10.01	-592.14	0	-2212.61	1.8	69.00	1.8	0.00	2.12	0.00
130	130	34.60	-1606.18	-10.01	-592.14	0	-2212.61	1.8	69.00	1.8	0.00	2.12	0.00
130	131	36.00	-1606.18	-4.30	-582.12	0	-2197.35	1.8	45.66	1.8	0.00	2.12	0.00
131	131	36.00	-1606.18	-4.30	-582.12	0	-2197.35	1.8	45.66	1.8	0.00	2.12	0.00
131	132	37.40	-1606.18	1.41	-580.12	0	-2194.30	1.8	41.01	1.8	0.00	2.12	0.00
132	132	37.40	-1606.18	1.41	-580.12	0	-2194.30	1.8	41.01	1.8	0.00	2.12	0.00
132	133	38.80	-1606.18	7.13	-586.10	0	-2203.41	1.8	54.94	1.8	0.00	2.12	0.00
133	133	38.80	-1606.18	7.13	-586.10	0	-2203.41	1.8	54.94	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ-
Construcción sin gradiente en fase constructiva 4

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	12.83	-600.08	0	-2224.72	1.8	87.51	1.8	0.00	2.12	0.00
134	134	40.20	-1606.18	12.83	-600.08	0	-2224.72	1.8	87.51	1.8	0.00	2.12	0.00
134	135	41.60	-1606.18	18.55	-622.05	0	-2258.20	1.8	138.68	1.8	0.00	2.12	0.00
135	135	41.60	-1260.90	17.35	-422.94	0	-1672.79	1.8	-25.45	1.8	0.00	2.12	0.00
135	136	43.00	-1264.23	24.79	-451.80	0	-1721.94	1.8	38.84	1.8	0.00	2.12	0.00
136	136	43.00	-2088.58	24.18	-54.14	0	-1519.90	1.8	-586.07	1.8	-290.01	2.12	-342.88
136	137	44.40	-2088.58	36.26	-96.44	0	-1591.52	1.8	-473.63	1.8	-291.77	2.12	-345.99
137	137	44.40	-1696.97	36.26	135.37	0	-909.40	1.8	-698.95	1.8	-291.77	2.12	-345.98
137	138	45.80	-1696.97	48.35	76.14	0	-1007.94	1.8	-547.19	1.8	-293.53	2.12	-349.09
138	138	45.80	-2523.70	48.36	473.80	0	-877.76	1.8	-917.75	1.8	-615.36	2.12	-748.24
138	139	47.20	-2523.70	60.43	397.66	0	-1003.20	1.8	-726.72	1.8	-617.12	2.12	-751.35
139	139	47.20	-2219.11	60.43	587.11	0	-458.11	1.8	-923.21	1.8	-617.12	2.12	-751.35
139	140	48.60	-2212.66	73.02	493.44	0	-609.07	1.8	-690.65	1.8	-617.00	2.12	-752.47
140	140	48.60	-2212.49	73.03	493.37	0	-609.09	1.8	-690.58	1.8	-616.93	2.12	-752.39
140	141	50.00	-2212.49	92.11	377.79	0	-796.82	1.8	-409.33	1.8	-618.51	2.12	-755.18
141	1141	50.00	-2212.71	-92.03	377.78	0	-796.89	1.8	-409.39	1.8	-618.57	2.12	-755.24
141	142	51.40	-2212.71	-72.95	493.24	0	-609.28	1.8	-690.61	1.8	-616.96	2.12	-752.39
142	142	51.40	-2213.30	-72.93	493.30	0	-609.41	1.8	-690.81	1.8	-617.13	2.12	-752.57
142	143	52.80	-2213.30	-60.84	586.97	0	-456.46	1.8	-921.37	1.8	-615.53	2.12	-749.73
143	143	52.80	-2518.88	-60.80	397.62	0	-1001.75	1.8	-725.22	1.8	-615.82	2.12	-750.05
143	144	54.20	-2523.70	-48.36	473.80	0	-877.76	1.8	-917.75	1.8	-615.36	2.12	-748.24
144	144	54.20	-1696.97	-48.36	76.14	0	-1007.94	1.8	-547.19	1.8	-293.53	2.12	-349.09
144	145	55.60	-1696.97	-36.27	135.38	0	-909.39	1.8	-698.95	1.8	-291.77	2.12	-345.99
145	145	55.60	-2088.58	-36.26	-96.44	0	-1591.52	1.8	-473.63	1.8	-291.77	2.12	-345.99
145	146	57.00	-2088.58	-24.18	-54.14	0	-1519.90	1.8	-586.07	1.8	-290.01	2.12	-342.88
146	146	57.00	-1264.23	-24.80	-451.80	0	-1721.94	1.8	38.84	1.8	0.00	2.12	0.00
146	147	58.40	-1262.69	-18.27	-422.03	0	-1672.87	1.8	-29.02	1.8	0.00	2.12	0.00
147	147	58.40	-1608.20	-18.50	-621.14	0	-2258.46	1.8	134.93	1.8	0.00	2.12	0.00
147	148	59.80	-1608.20	-12.78	-599.26	0	-2225.11	1.8	83.96	1.8	0.00	2.12	0.00
148	148	59.80	-1608.20	-12.78	-599.26	0	-2225.11	1.8	83.96	1.8	0.00	2.12	0.00
148	149	61.20	-1608.20	-7.08	-585.36	0	-2203.93	1.8	51.58	1.8	0.00	2.12	0.00
149	149	61.20	-1608.20	-7.08	-585.36	0	-2203.93	1.8	51.58	1.8	0.00	2.12	0.00
149	150	62.60	-1608.20	-1.36	-579.45	0	-2194.93	1.8	37.81	1.8	0.00	2.12	0.00
150	150	62.60	-1608.20	-1.36	-579.45	0	-2194.93	1.8	37.81	1.8	0.00	2.12	0.00
150	151	64.00	-1609.94	4.38	-581.56	0	-2199.57	1.8	41.30	1.8	0.00	2.12	0.00
151	151	64.00	-1609.94	4.38	-581.56	0	-2199.57	1.8	41.30	1.8	0.00	2.12	0.00
151	152	65.40	-1609.94	10.09	-591.68	0	-2214.99	1.8	64.88	1.8	0.00	2.12	0.00
152	152	65.40	-1609.94	10.09	-591.68	0	-2214.99	1.8	64.88	1.8	0.00	2.12	0.00
152	153	66.80	-1609.94	15.81	-609.79	0	-2242.59	1.8	107.06	1.8	0.00	2.12	0.00
153	153	66.80	-1609.94	15.81	-609.79	0	-2242.59	1.8	107.06	1.8	0.00	2.12	0.00
153	154	68.20	-1609.94	21.51	-635.92	0	-2282.40	1.8	167.93	1.8	0.00	2.12	0.00
154	154	68.20	-1609.94	21.51	-635.92	0	-2282.40	1.8	167.93	1.8	0.00	2.12	0.00
154	155	69.60	-1609.94	27.23	-670.01	0	-2334.35	1.8	247.35	1.8	0.00	2.12	0.00
155	155	69.60	-1259.46	26.61	-470.90	0	-1744.27	1.8	87.49	1.8	0.00	2.12	0.00
155	156	71.00	-1259.46	32.32	-513.02	0	-1810.80	1.8	185.40	1.8	0.00	2.12	0.00
156	156	71.00	-2088.58	32.94	-115.36	0	-1574.04	1.8	-584.91	1.8	-272.44	2.12	-311.80
156	157	72.40	-2088.58	45.02	-169.91	0	-1656.49	1.8	-472.24	1.8	-270.68	2.12	-308.70
157	157	72.40	-1696.97	45.02	61.92	0	-974.36	1.8	-697.56	1.8	-270.68	2.12	-308.70
157	158	73.80	-1696.97	57.11	-9.57	0	-1083.75	1.8	-545.56	1.8	-268.92	2.12	-305.59
158	158	73.80	-2523.70	57.10	388.08	0	-953.57	1.8	-916.12	1.8	-590.76	2.12	-704.74
158	159	75.20	-2523.70	69.17	299.69	0	-1089.84	1.8	-724.85	1.8	-589.00	2.12	-701.63
159	159	75.20	-2219.11	69.17	489.14	0	-544.75	1.8	-921.34	1.8	-589.00	2.12	-701.63
159	160	76.60	-2215.29	81.73	383.30	0	-707.27	1.8	-689.39	1.8	-586.09	2.12	-697.27
160	160	76.60	-2215.34	81.76	383.22	0	-707.37	1.8	-689.38	1.8	-586.08	2.12	-697.25
160	161	78.00	-2215.34	100.84	255.41	0	-905.92	1.8	-407.89	1.8	-584.15	2.12	-693.83
161	1161	78.00	-2172.15	-90.15	284.18	0	-825.41	1.8	-440.11	1.8	-584.22	2.12	-693.90
161	162	79.10	-2172.15	-75.16	375.10	0	-688.05	1.8	-627.68	1.8	-587.18	2.12	-699.12
162	162	79.10	-2172.53	-75.17	375.10	0	-688.17	1.8	-627.80	1.8	-587.28	2.12	-699.22
162	163	80.20	-2172.53	-65.68	452.58	0	-572.19	1.8	-784.12	1.8	-590.23	2.12	-704.44
163	163	80.20	-2477.65	-65.68	260.11	0	-1122.26	1.8	-580.73	1.8	-590.38	2.12	-704.60
163	164	81.30	-2477.65	-56.18	327.13	0	-1022.94	1.8	-712.73	1.8	-593.34	2.12	-709.82
164	164	81.30	-2478.35	-56.17	327.17	0	-1023.10	1.8	-712.96	1.8	-593.54	2.12	-710.03
164	165	82.40	-2478.35	-46.68	383.75	0	-940.37	1.8	-820.72	1.8	-596.49	2.12	-715.25
165	165	82.40	-1870.06	-46.63	-146.96	0	-1456.63	1.8	-315.15	1.8	-274.91	2.12	-316.38
165	166	83.50	-1870.06	-37.14	-100.89	0	-1390.58	1.8	-398.61	1.8	-277.85	2.12	-321.57
166	166	83.50	-1871.02	-37.06	-100.80	0	-1414.73	1.8	-375.58	1.8	-257.84	2.12	-294.28
166	167	84.60	-1871.02	-27.56	-65.24	0	-1366.57	1.8	-433.60	1.8	-259.72	2.12	-298.02
167	167	84.60	-1038.30	-25.67	-462.90	0	-1556.32	1.8	245.78	1.8	0.00	2.12	0.00
167	168	85.70	-1038.30	-21.19	-435.06	0	-1512.80	1.8	181.01	1.8	0.00	2.12	0.00
168	168	85.70	-1261.85	-23.08	-566.03	0	-1891.92	1.8	289.09	1.8	0.00	2.12	0.00
168	169	86.80	-1261.85	-18.58	-543.13	0	-1857.03	1.8	235.76	1.8	0.00	2.12	0.00
169	169	86.80	-1261.85	-18.58	-543.13	0	-1857.03	1.8	235.76	1.8	0.00	2.12	0.00
169	170	87.90	-1261.85	-14.10	-525.15	0	-1829.63	1.8	193.87	1.8	0.00	2.12	0.00
170	170	87.90	-1261.85	-14.10	-525.15	0	-1829.63	1.8	193.87	1.8	0.00	2.12	0.00
170	171	89.00	-1261.85	-9.61	-512.11	0	-1809.77	1.8	163.51	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.MZ-
Construcción sin gradiente en fase constructiva 4

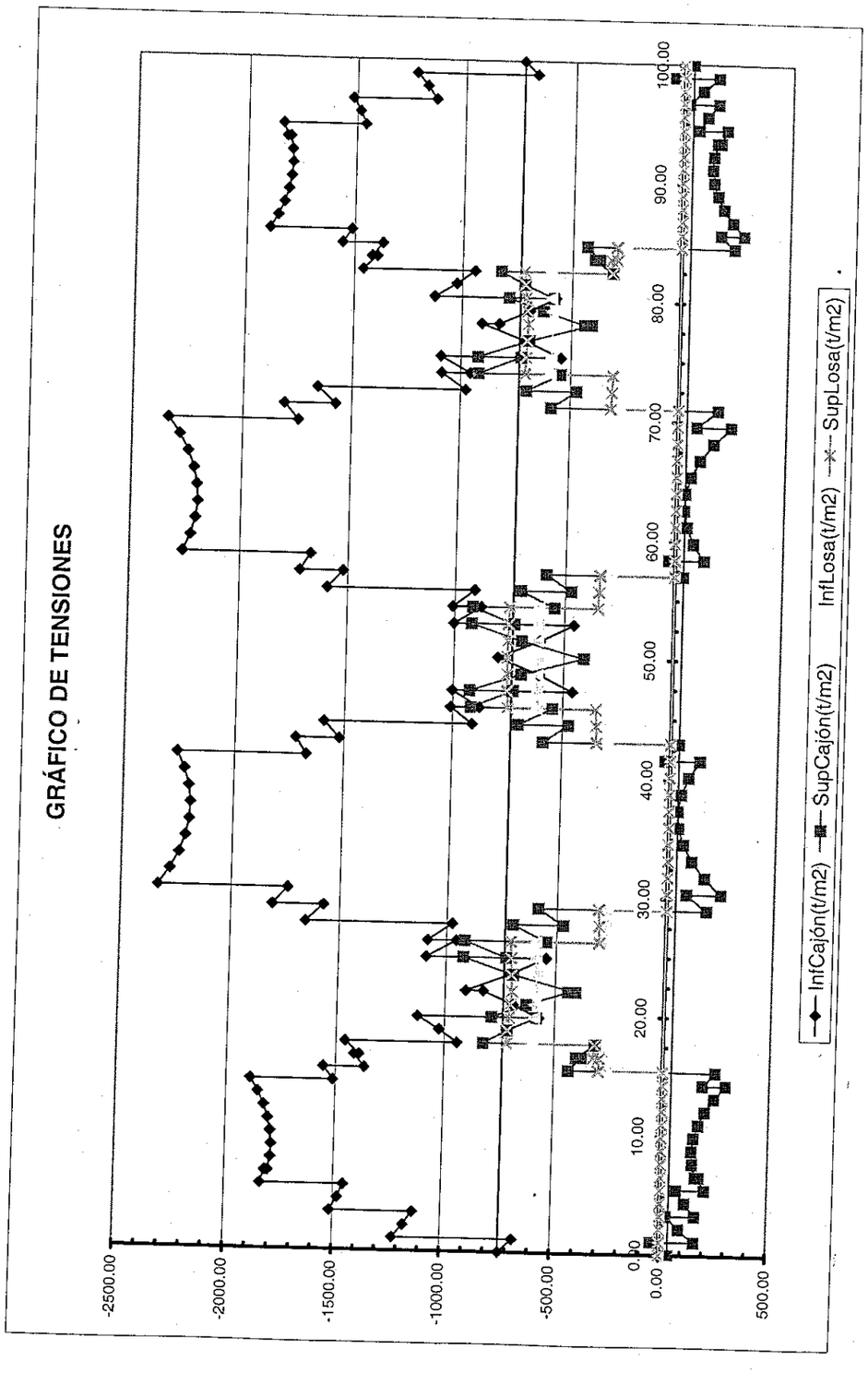
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	-9.61	-512.11	0	-1809.77	1.8	163.51	1.8	0.00	2.12	0.00
171	172	90.10	-1261.85	-5.12	-504.02	0	-1797.43	1.8	144.65	1.8	0.00	2.12	0.00
172	172	90.10	-1261.85	-5.12	-504.02	0	-1797.43	1.8	144.65	1.8	0.00	2.12	0.00
172	173	91.20	-1261.85	-0.64	-500.85	0	-1792.61	1.8	137.28	1.8	0.00	2.12	0.00
173	173	91.20	-1261.85	-0.64	-500.85	0	-1792.61	1.8	137.28	1.8	0.00	2.12	0.00
173	174	92.30	-1261.85	3.86	-502.62	0	-1795.30	1.8	141.39	1.8	0.00	2.12	0.00
174	174	92.30	-1261.85	3.86	-502.62	0	-1795.30	1.8	141.39	1.8	0.00	2.12	0.00
174	175	93.40	-1261.85	8.34	-509.33	0	-1805.52	1.8	157.01	1.8	0.00	2.12	0.00
175	175	93.40	-1261.85	8.34	-509.33	0	-1819.91	1.8	173.74	1.8	0.00	2.12	0.00
175	176	94.50	-1261.85	12.83	-520.98	0	-1838.45	1.8	200.83	1.8	0.00	2.12	0.00
176	176	94.50	-1044.29	12.83	-390.01	0	-1456.04	1.8	70.60	1.8	0.00	2.12	0.00
176	177	95.60	-1044.29	17.32	-406.60	0	-1482.42	1.8	109.14	1.8	0.00	2.12	0.00
177	177	95.60	-1044.29	17.32	-406.60	0	-1482.42	1.8	109.14	1.8	0.00	2.12	0.00
177	178	96.70	-1044.29	21.80	-428.13	0	-1516.66	1.8	159.16	1.8	0.00	2.12	0.00
178	178	96.70	-826.73	21.80	-294.98	0	-1130.77	1.8	23.86	1.8	0.00	2.12	0.00
178	179	97.80	-826.73	26.30	-321.43	0	-1172.85	1.8	85.33	1.8	0.00	2.12	0.00
179	179	97.80	-826.73	26.30	-321.43	0	-1172.85	1.8	85.33	1.8	0.00	2.12	0.00
179	180	98.90	-826.73	30.78	-352.83	0	-1222.79	1.8	158.28	1.8	0.00	2.12	0.00
180	180	98.90	-522.14	30.78	-160.33	0	-672.86	1.8	-45.28	1.8	0.00	2.12	0.00
180	181	100.00	-522.14	38.20	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F4.T0.MZ-

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ+

Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-70.85	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
1	2	1.10	-476.85	-59.52	-107.13	0	-552.00	1.8	-132.64	1.8	0.00	2.12	0.00
2	2	1.10	-752.42	-59.52	-281.30	0	-1049.55	1.8	51.54	1.8	0.00	2.12	0.00
2	3	2.20	-752.42	-50.04	-221.04	0	-953.70	1.8	-88.49	1.8	0.00	2.12	0.00
3	3	2.20	-752.42	-50.04	-221.04	0	-953.70	1.8	-88.49	1.8	0.00	2.12	0.00
3	4	3.30	-752.42	-40.53	-171.23	0	-874.47	1.8	-204.23	1.8	0.00	2.12	0.00
4	4	3.30	-949.26	-40.53	-291.70	0	-1223.61	1.8	-81.82	1.8	0.00	2.12	0.00
4	5	4.40	-949.26	-31.05	-252.35	0	-1161.02	1.8	-173.26	1.8	0.00	2.12	0.00
5	5	4.40	-949.26	-31.05	-252.35	0	-1161.02	1.8	-173.26	1.8	0.00	2.12	0.00
5	6	5.50	-949.26	-21.55	-223.42	0	-1115.01	1.8	-240.46	1.8	0.00	2.12	0.00
6	6	5.50	-1146.10	-21.55	-341.92	0	-1461.01	1.8	-122.64	1.8	0.00	2.12	0.00
6	7	6.60	-1146.10	-12.06	-323.42	0	-1431.58	1.8	-165.63	1.8	0.00	2.12	0.00
7	7	6.60	-1146.10	-12.06	-323.42	0	-1427.81	1.8	-181.62	1.8	0.00	2.12	0.00
7	8	7.70	-1146.10	-2.57	-315.38	0	-1415.56	1.8	-200.35	1.8	0.00	2.12	0.00
8	8	7.70	-1146.10	-2.57	-315.38	0	-1415.56	1.8	-200.35	1.8	0.00	2.12	0.00
8	9	8.80	-1146.10	6.93	-317.79	0	-1419.23	1.8	-194.74	1.8	0.00	2.12	0.00
9	9	8.80	-1146.10	6.93	-317.79	0	-1419.23	1.8	-194.74	1.8	0.00	2.12	0.00
9	10	9.90	-1146.10	16.42	-330.64	0	-1438.81	1.8	-164.81	1.8	0.00	2.12	0.00
10	10	9.90	-1146.10	16.42	-330.64	0	-1438.81	1.8	-164.81	1.8	0.00	2.12	0.00
10	11	11.00	-1146.10	25.91	-353.91	0	-1474.28	1.8	-110.58	1.8	0.00	2.12	0.00
11	11	11.00	-1146.10	25.91	-353.91	0	-1474.28	1.8	-110.58	1.8	0.00	2.12	0.00
11	12	12.10	-1146.10	35.41	-387.64	0	-1525.68	1.8	-32.01	1.8	0.00	2.12	0.00
12	12	12.10	-1146.10	35.41	-387.64	0	-1525.68	1.8	-32.01	1.8	0.00	2.12	0.00
12	13	13.20	-1146.10	44.89	-431.83	0	-1593.01	1.8	70.93	1.8	0.00	2.12	0.00
13	13	13.20	-1146.10	44.89	-431.83	0	-1593.01	1.8	70.93	1.8	0.00	2.12	0.00
13	14	14.30	-1146.10	54.40	-486.42	0	-1676.19	1.8	198.09	1.8	0.00	2.12	0.00
14	14	14.30	-924.56	49.43	-367.93	0	-1315.93	1.8	116.16	1.8	0.00	2.12	0.00
14	15	15.40	-917.39	56.45	-435.03	0	-1413.42	1.8	278.24	1.8	0.00	2.12	0.00
15	15	15.40	-1858.58	65.07	4.49	0	-1217.38	1.8	-500.37	1.8	-286.24	2.12	-327.76
15	16	16.50	-1858.58	74.57	-72.33	0	-1301.07	1.8	-434.61	1.8	-277.64	2.12	-310.62
16	16	16.50	-1858.58	74.57	-72.34	0	-1279.42	1.8	-455.74	1.8	-296.00	2.12	-335.58
16	17	17.60	-1858.58	84.06	-159.96	0	-1385.93	1.8	-359.39	1.8	-282.64	2.12	-311.97
17	17	17.60	-2575.51	84.06	400.40	0	-892.30	1.8	-892.27	1.8	-638.36	2.12	-753.13
17	18	18.70	-2575.51	93.55	302.71	0	-1014.82	1.8	-772.53	1.8	-625.00	2.12	-729.51
18	18	18.70	-2575.50	93.55	302.71	0	-1014.81	1.8	-772.53	1.8	-625.00	2.12	-729.51
18	19	19.80	-2575.50	103.05	194.57	0	-1153.93	1.8	-628.55	1.8	-611.64	2.12	-705.88
19	19	19.80	-2299.92	103.05	368.74	0	-656.38	1.8	-812.73	1.8	-611.64	2.12	-705.88
19	20	20.90	-2299.92	112.54	250.14	0	-812.14	1.8	-644.42	1.8	-598.28	2.12	-682.26
20	20	20.90	-2299.92	112.54	250.14	0	-812.14	1.8	-644.42	1.8	-598.28	2.12	-682.26
20	21	22.00	-2299.92	127.53	118.10	0	-989.30	1.8	-444.87	1.8	-584.92	2.12	-658.64
21	1021	22.00	-2339.29	-134.33	92.03	0	-1062.27	1.8	-415.80	1.8	-584.92	2.12	-658.64
21	22	23.40	-2339.29	-115.25	266.74	0	-818.33	1.8	-710.95	1.8	-598.72	2.12	-683.04
22	22	23.40	-2339.29	-115.25	266.74	0	-818.33	1.8	-710.95	1.8	-598.72	2.12	-683.04
22	23	24.80	-2339.29	-103.16	419.65	0	-609.07	1.8	-955.44	1.8	-612.52	2.12	-707.45
23	23	24.80	-2614.86	-103.15	248.24	0	-1102.24	1.8	-777.67	1.8	-612.52	2.12	-707.45
23	24	26.20	-2614.86	-91.08	384.20	0	-919.94	1.8	-982.79	1.8	-626.32	2.12	-731.84
24	24	26.20	-1701.11	-91.08	-55.31	0	-1063.82	1.8	-573.24	1.8	-270.60	2.12	-290.68
24	25	27.60	-1701.11	-78.99	63.76	0	-908.39	1.8	-739.10	1.8	-284.41	2.12	-315.08
25	25	27.60	-2055.42	-79.00	-145.99	0	-1525.55	1.8	-535.23	1.8	-284.41	2.12	-315.08
25	26	29.00	-2055.42	-66.92	-43.84	0	-1397.03	1.8	-661.78	1.8	-298.21	2.12	-339.48
26	26	29.00	-1122.96	-62.12	-483.36	0	-1651.98	1.8	226.15	1.8	0.00	2.12	0.00
26	27	30.40	-1129.71	-51.92	-398.64	0	-1526.04	1.8	23.49	1.8	0.00	2.12	0.00
27	27	30.40	-1460.38	-54.02	-578.79	0	-2073.32	1.8	156.86	1.8	0.00	2.12	0.00
27	28	31.80	-1460.38	-41.93	-511.64	0	-1971.00	1.8	0.44	1.8	0.00	2.12	0.00
28	28	31.80	-1460.38	-41.93	-511.64	0	-1971.00	1.8	0.44	1.8	0.00	2.12	0.00
28	29	33.20	-1460.38	-29.86	-461.37	0	-1894.40	1.8	-116.67	1.8	0.00	2.12	0.00
29	29	33.20	-1460.38	-29.86	-461.37	0	-1894.40	1.8	-116.67	1.8	0.00	2.12	0.00
29	30	34.60	-1460.38	-17.77	-428.02	0	-1843.60	1.8	-194.33	1.8	0.00	2.12	0.00
30	30	34.60	-1460.38	-17.77	-428.02	0	-1843.60	1.8	-194.33	1.8	0.00	2.12	0.00
30	31	36.00	-1460.38	-5.69	-411.59	0	-1818.56	1.8	-232.61	1.8	0.00	2.12	0.00
31	31	36.00	-1460.38	-5.69	-411.59	0	-1818.56	1.8	-232.61	1.8	0.00	2.12	0.00
31	32	37.40	-1460.38	6.39	-412.07	0	-1819.29	1.8	-231.49	1.8	0.00	2.12	0.00
32	32	37.40	-1460.38	6.39	-412.07	0	-1819.29	1.8	-231.49	1.8	0.00	2.12	0.00
32	33	38.80	-1460.38	18.48	-429.47	0	-1845.80	1.8	-190.96	1.8	0.00	2.12	0.00
33	33	38.80	-1460.38	18.48	-429.47	0	-1845.80	1.8	-190.96	1.8	0.00	2.12	0.00
33	34	40.20	-1460.38	30.55	-463.79	0	-1898.10	1.8	-111.02	1.8	0.00	2.12	0.00
34	34	40.20	-1460.38	30.55	-463.79	0	-1898.10	1.8	-111.02	1.8	0.00	2.12	0.00
34	35	41.60	-1460.38	42.64	-515.02	0	-1976.16	1.8	8.32	1.8	0.00	2.12	0.00
35	35	41.60	-1135.74	42.07	-334.87	0	-1434.24	1.8	-130.01	1.8	0.00	2.12	0.00
35	36	43.00	-1128.92	52.42	-404.77	0	-1537.65	1.8	38.18	1.8	0.00	2.12	0.00
36	36	43.00	-2055.42	55.69	34.75	0	-1326.09	1.8	-667.99	1.8	-320.17	2.12	-378.33
36	37	44.40	-2055.42	67.77	-51.67	0	-1440.40	1.8	-542.70	1.8	-310.77	2.12	-361.70
37	37	44.40	-1701.11	67.78	158.08	0	-823.24	1.8	-746.56	1.8	-310.77	2.12	-361.70
37	38	45.80	-1701.11	79.87	54.74	0	-964.47	1.8	-581.95	1.8	-301.37	2.12	-345.07
38	38	45.80	-2614.86	79.87	494.25	0	-820.58	1.8	-991.51	1.8	-657.08	2.12	-786.24

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ+
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	91.94	374.00	0	-988.71	1.8	-787.63	1.8	-647.67	2.12	-769.60
39	39	47.20	-2339.29	91.94	545.42	0	-495.53	1.8	-965.41	1.8	-647.67	2.12	-769.61
39	40	48.60	-2345.74	103.53	408.84	0	-691.99	1.8	-724.33	1.8	-640.15	2.12	-754.97
40	40	48.60	-2345.92	103.52	408.89	0	-692.00	1.8	-724.40	1.8	-640.21	2.12	-755.04
40	41	50.00	-2345.92	122.60	250.62	0	-921.04	1.8	-430.70	1.8	-630.98	2.12	-738.73
41	1041	50.00	-2345.70	-122.68	250.63	0	-920.97	1.8	-430.64	1.8	-630.93	2.12	-738.67
41	42	51.40	-2345.70	-103.60	409.03	0	-691.80	1.8	-724.37	1.8	-640.18	2.12	-755.04
42	42	51.40	-2345.10	-103.61	408.98	0	-691.67	1.8	-724.17	1.8	-640.01	2.12	-754.86
42	43	52.80	-2345.10	-91.52	545.58	0	-497.17	1.8	-967.24	1.8	-649.27	2.12	-771.23
43	43	52.80	-2619.68	-91.57	374.05	0	-990.15	1.8	-789.13	1.8	-648.97	2.12	-770.91
43	44	54.20	-2614.86	-79.87	494.24	0	-820.59	1.8	-991.51	1.8	-657.08	2.12	-786.23
44	44	54.20	-1701.11	-79.87	54.74	0	-964.47	1.8	-581.95	1.8	-301.36	2.12	-345.06
44	45	55.60	-1701.11	-67.78	158.09	0	-823.23	1.8	-746.56	1.8	-310.77	2.12	-361.70
45	45	55.60	-2055.42	-67.77	-51.67	0	-1440.41	1.8	-542.70	1.8	-310.77	2.12	-361.70
45	46	57.00	-2055.42	-55.69	34.76	0	-1326.08	1.8	-668.00	1.8	-320.18	2.12	-378.33
46	46	57.00	-1128.92	-52.43	-404.76	0	-1537.64	1.8	38.16	1.8	0.00	2.12	0.00
46	47	58.40	-1133.95	-41.17	-335.77	0	-1434.15	1.8	-126.46	1.8	0.00	2.12	0.00
47	47	58.40	-1458.36	-42.69	-515.92	0	-1975.88	1.8	12.05	1.8	0.00	2.12	0.00
47	48	59.80	-1458.36	-30.60	-464.61	0	-1897.70	1.8	-107.47	1.8	0.00	2.12	0.00
48	48	59.80	-1458.36	-30.60	-464.61	0	-1897.70	1.8	-107.47	1.8	0.00	2.12	0.00
48	49	61.20	-1458.36	-18.53	-430.22	0	-1845.30	1.8	-187.58	1.8	0.00	2.12	0.00
49	49	61.20	-1458.36	-18.53	-430.22	0	-1845.30	1.8	-187.58	1.8	0.00	2.12	0.00
49	50	62.60	-1458.36	-6.44	-412.73	0	-1818.65	1.8	-228.32	1.8	0.00	2.12	0.00
50	50	62.60	-1458.36	-6.44	-412.73	0	-1818.65	1.8	-228.32	1.8	0.00	2.12	0.00
50	51	64.00	-1456.62	5.61	-412.16	0	-1816.35	1.8	-228.22	1.8	0.00	2.12	0.00
51	51	64.00	-1456.62	5.61	-412.16	0	-1816.35	1.8	-228.22	1.8	0.00	2.12	0.00
51	52	65.40	-1456.62	17.69	-428.48	0	-1841.22	1.8	-190.21	1.8	0.00	2.12	0.00
52	52	65.40	-1456.62	17.69	-428.48	0	-1841.22	1.8	-190.21	1.8	0.00	2.12	0.00
52	53	66.80	-1456.62	29.78	-461.71	0	-1891.85	1.8	-112.80	1.8	0.00	2.12	0.00
53	53	66.80	-1456.62	29.78	-461.71	0	-1891.85	1.8	-112.80	1.8	0.00	2.12	0.00
53	54	68.20	-1456.62	41.85	-511.86	0	-1968.27	1.8	4.02	1.8	0.00	2.12	0.00
54	54	68.20	-1456.62	41.85	-511.86	0	-1968.27	1.8	4.02	1.8	0.00	2.12	0.00
54	55	69.60	-1456.62	53.94	-578.90	0	-2070.42	1.8	160.18	1.8	0.00	2.12	0.00
55	55	69.60	-1126.45	50.04	-398.75	0	-1523.55	1.8	26.41	1.8	0.00	2.12	0.00
55	56	71.00	-1122.96	62.12	-483.37	0	-1651.99	1.8	226.17	1.8	0.00	2.12	0.00
56	56	71.00	-2055.42	66.92	-43.85	0	-1397.04	1.8	-661.77	1.8	-298.20	2.12	-339.48
56	57	72.40	-2055.42	79.00	-145.98	0	-1525.54	1.8	-535.24	1.8	-284.41	2.12	-315.08
57	57	72.40	-1701.11	79.00	63.77	0	-908.38	1.8	-739.10	1.8	-284.41	2.12	-315.08
57	58	73.80	-1701.11	91.09	-55.30	0	-1063.81	1.8	-573.24	1.8	-270.61	2.12	-290.68
58	58	73.80	-2614.86	91.08	384.21	0	-919.93	1.8	-982.80	1.8	-626.32	2.12	-731.85
58	59	75.20	-2614.86	103.15	248.23	0	-1102.25	1.8	-777.66	1.8	-612.52	2.12	-707.44
59	59	75.20	-2339.29	103.15	419.65	0	-609.07	1.8	-955.44	1.8	-612.52	2.12	-707.44
59	60	76.60	-2343.12	114.78	267.26	0	-819.01	1.8	-712.28	1.8	-599.87	2.12	-684.30
60	60	76.60	-2343.06	114.76	267.34	0	-818.92	1.8	-712.28	1.8	-599.88	2.12	-684.32
60	61	78.00	-2343.06	133.84	93.32	0	-1062.18	1.8	-417.34	1.8	-586.25	2.12	-660.23
61	1061	78.00	-2303.37	-127.38	119.43	0	-989.08	1.8	-446.32	1.8	-586.18	2.12	-660.15
61	62	79.10	-2303.37	-112.39	251.29	0	-812.10	1.8	-645.82	1.8	-599.49	2.12	-683.70
62	62	79.10	-2302.99	-112.38	251.29	0	-811.98	1.8	-645.71	1.8	-599.39	2.12	-683.60
62	63	80.20	-2302.99	-102.89	369.72	0	-656.37	1.8	-813.96	1.8	-612.71	2.12	-707.14
63	63	80.20	-2578.03	-102.89	195.54	0	-1153.78	1.8	-629.61	1.8	-612.56	2.12	-706.99
63	64	81.30	-2578.03	-93.39	303.48	0	-1014.84	1.8	-773.53	1.8	-625.87	2.12	-730.53
64	64	81.30	-2577.33	-93.40	303.42	0	-1014.69	1.8	-773.30	1.8	-625.67	2.12	-730.32
64	65	82.40	-2577.33	-83.91	400.96	0	-892.32	1.8	-892.99	1.8	-638.99	2.12	-753.87
65	65	82.40	-1859.54	-83.96	-159.11	0	-1385.16	1.8	-360.72	1.8	-283.02	2.12	-312.43
65	66	83.50	-1859.54	-74.47	-71.98	0	-1279.37	1.8	-456.14	1.8	-296.35	2.12	-336.00
66	66	83.50	-1858.58	-74.57	-72.08	0	-1300.86	1.8	-434.65	1.8	-277.68	2.12	-310.70
66	67	84.60	-1858.58	-65.07	4.72	0	-1217.17	1.8	-500.41	1.8	-286.28	2.12	-327.84
67	67	84.60	-917.40	-56.43	-434.80	0	-1413.07	1.8	277.68	1.8	0.00	2.12	0.00
67	68	85.70	-920.89	-46.95	-369.05	0	-1314.64	1.8	121.78	1.8	0.00	2.12	0.00
68	68	85.70	-1141.67	-54.49	-487.54	0	-1674.29	1.8	204.32	1.8	0.00	2.12	0.00
68	69	86.80	-1141.67	-44.98	-432.86	0	-1590.96	1.8	76.93	1.8	0.00	2.12	0.00
69	69	86.80	-1141.67	-44.98	-432.86	0	-1590.96	1.8	76.93	1.8	0.00	2.12	0.00
69	70	87.90	-1141.67	-35.50	-388.60	0	-1523.52	1.8	-26.16	1.8	0.00	2.12	0.00
70	70	87.90	-1141.67	-35.50	-388.60	0	-1523.52	1.8	-26.16	1.8	0.00	2.12	0.00
70	71	89.00	-1141.67	-26.00	-354.79	0	-1472.00	1.8	-104.93	1.8	0.00	2.12	0.00
71	71	89.00	-1141.67	-26.00	-354.79	0	-1472.00	1.8	-104.93	1.8	0.00	2.12	0.00
71	72	90.10	-1141.67	-16.51	-331.41	0	-1436.38	1.8	-159.38	1.8	0.00	2.12	0.00
72	72	90.10	-1141.67	-16.51	-331.41	0	-1436.38	1.8	-159.38	1.8	0.00	2.12	0.00
72	73	91.20	-1141.67	-7.02	-318.48	0	-1416.67	1.8	-189.52	1.8	0.00	2.12	0.00
73	73	91.20	-1141.67	-7.02	-318.48	0	-1416.67	1.8	-189.52	1.8	0.00	2.12	0.00
73	74	92.30	-1141.67	2.48	-315.98	0	-1412.87	1.8	-195.33	1.8	0.00	2.12	0.00
74	74	92.30	-1141.67	2.48	-315.98	0	-1412.87	1.8	-195.33	1.8	0.00	2.12	0.00
74	75	93.40	-1141.67	11.97	-323.93	0	-1424.99	1.8	-176.80	1.8	0.00	2.12	0.00
75	75	93.40	-1141.67	11.97	-323.93	0	-1428.86	1.8	-160.88	1.8	0.00	2.12	0.00
75	76	94.50	-1141.67	21.46	-342.34	0	-1458.13	1.8	-118.11	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F5.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ+
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	21.46	-223.85	0	-1112.14	1.8	-235.94	1.8	0.00	2.12	0.00
76	77	95.60	-944.83	30.96	-252.68	0	-1158.00	1.8	-168.93	1.8	0.00	2.12	0.00
77	77	95.60	-944.83	30.96	-252.68	0	-1158.00	1.8	-168.93	1.8	0.00	2.12	0.00
77	78	96.70	-944.83	40.44	-291.96	0	-1220.49	1.8	-77.65	1.8	0.00	2.12	0.00
78	78	96.70	-747.99	40.44	-171.50	0	-871.35	1.8	-200.07	1.8	0.00	2.12	0.00
78	79	97.80	-747.99	49.95	-221.22	0	-950.44	1.8	-84.52	1.8	0.00	2.12	0.00
79	79	97.80	-747.99	49.95	-221.22	0	-950.44	1.8	-84.52	1.8	0.00	2.12	0.00
79	80	98.90	-747.99	59.43	-281.38	0	-1046.14	1.8	55.28	1.8	0.00	2.12	0.00
80	80	98.90	-472.42	59.43	-107.22	0	-548.59	1.8	-128.89	1.8	0.00	2.12	0.00
80	81	100.00	-472.42	70.84	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	101	0.00	-472.42	-70.85	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00
101	102	1.10	-476.85	-59.52	-107.13	0	-552.00	1.8	-132.64	1.8	0.00	2.12	0.00
102	102	1.10	-752.42	-59.52	-281.30	0	-1049.55	1.8	51.54	1.8	0.00	2.12	0.00
102	103	2.20	-752.42	-50.04	-221.04	0	-953.70	1.8	-88.49	1.8	0.00	2.12	0.00
103	103	2.20	-752.42	-50.04	-221.04	0	-953.70	1.8	-88.49	1.8	0.00	2.12	0.00
103	104	3.30	-752.42	-40.53	-171.23	0	-874.47	1.8	-204.23	1.8	0.00	2.12	0.00
104	104	3.30	-949.26	-40.53	-291.70	0	-1223.61	1.8	-81.82	1.8	0.00	2.12	0.00
104	105	4.40	-949.26	-31.05	-252.34	0	-1161.00	1.8	-173.28	1.8	0.00	2.12	0.00
105	105	4.40	-949.26	-31.05	-252.34	0	-1161.00	1.8	-173.28	1.8	0.00	2.12	0.00
105	106	5.50	-949.26	-21.55	-223.42	0	-1115.00	1.8	-240.48	1.8	0.00	2.12	0.00
106	106	5.50	-1146.10	-21.55	-341.91	0	-1460.99	1.8	-122.66	1.8	0.00	2.12	0.00
106	107	6.60	-1146.10	-12.06	-323.42	0	-1431.58	1.8	-165.63	1.8	0.00	2.12	0.00
107	107	6.60	-1146.10	-12.06	-323.42	0	-1427.81	1.8	-181.62	1.8	0.00	2.12	0.00
107	108	7.70	-1146.10	-2.57	-315.38	0	-1415.56	1.8	-200.35	1.8	0.00	2.12	0.00
108	108	7.70	-1146.10	-2.57	-315.38	0	-1415.56	1.8	-200.35	1.8	0.00	2.12	0.00
108	109	8.80	-1146.10	6.93	-317.79	0	-1419.23	1.8	-194.74	1.8	0.00	2.12	0.00
109	109	8.80	-1146.10	6.93	-317.79	0	-1419.23	1.8	-194.74	1.8	0.00	2.12	0.00
109	110	9.90	-1146.10	16.42	-330.64	0	-1438.81	1.8	-164.81	1.8	0.00	2.12	0.00
110	110	9.90	-1146.10	16.42	-330.64	0	-1438.81	1.8	-164.81	1.8	0.00	2.12	0.00
110	111	11.00	-1146.10	25.91	-353.91	0	-1474.28	1.8	-110.58	1.8	0.00	2.12	0.00
111	111	11.00	-1146.10	25.91	-353.91	0	-1474.28	1.8	-110.58	1.8	0.00	2.12	0.00
111	112	12.10	-1146.10	35.41	-387.64	0	-1525.68	1.8	-32.01	1.8	0.00	2.12	0.00
112	112	12.10	-1146.10	35.41	-387.64	0	-1525.68	1.8	-32.01	1.8	0.00	2.12	0.00
112	113	13.20	-1146.10	44.89	-431.82	0	-1593.00	1.8	70.90	1.8	0.00	2.12	0.00
113	113	13.20	-1146.10	44.89	-431.82	0	-1593.00	1.8	70.90	1.8	0.00	2.12	0.00
113	114	14.30	-1146.10	54.40	-486.42	0	-1676.20	1.8	198.09	1.8	0.00	2.12	0.00
114	114	14.30	-924.56	49.43	-367.93	0	-1315.94	1.8	116.17	1.8	0.00	2.12	0.00
114	115	15.40	-917.39	56.45	-435.03	0	-1413.42	1.8	278.24	1.8	0.00	2.12	0.00
115	115	15.40	-1858.58	65.07	4.49	0	-1217.38	1.8	-500.37	1.8	-286.24	2.12	-327.76
115	116	16.50	-1858.58	74.57	-72.34	0	-1301.08	1.8	-434.61	1.8	-277.64	2.12	-310.62
116	116	16.50	-1858.58	74.57	-72.34	0	-1279.42	1.8	-455.74	1.8	-296.00	2.12	-335.58
116	117	17.60	-1858.58	84.06	-159.98	0	-1385.95	1.8	-359.38	1.8	-282.64	2.12	-311.96
117	117	17.60	-2575.50	84.06	400.40	0	-892.29	1.8	-892.26	1.8	-638.36	2.12	-753.13
117	118	18.70	-2575.50	93.55	302.71	0	-1014.81	1.8	-772.53	1.8	-625.00	2.12	-729.51
118	118	18.70	-2575.50	93.55	302.71	0	-1014.81	1.8	-772.53	1.8	-625.00	2.12	-729.51
118	119	19.80	-2575.50	103.05	194.58	0	-1153.92	1.8	-628.55	1.8	-611.64	2.12	-705.89
119	119	19.80	-2299.92	103.05	368.75	0	-656.37	1.8	-812.73	1.8	-611.64	2.12	-705.89
119	120	20.90	-2299.92	112.54	250.14	0	-812.14	1.8	-644.42	1.8	-598.28	2.12	-682.26
120	120	20.90	-2299.92	112.54	250.14	0	-812.14	1.8	-644.42	1.8	-598.28	2.12	-682.26
120	121	22.00	-2299.92	127.53	118.10	0	-989.30	1.8	-444.87	1.8	-584.92	2.12	-658.64
121	1121	22.00	-2339.29	-134.33	92.03	0	-1062.27	1.8	-415.80	1.8	-584.92	2.12	-658.64
121	122	23.40	-2339.29	-115.25	266.74	0	-818.33	1.8	-710.95	1.8	-598.72	2.12	-683.04
122	122	23.40	-2339.29	-115.25	266.74	0	-818.33	1.8	-710.95	1.8	-598.72	2.12	-683.04
122	123	24.80	-2339.29	-103.16	419.64	0	-609.08	1.8	-955.44	1.8	-612.52	2.12	-707.44
123	123	24.80	-2614.86	-103.15	248.24	0	-1102.24	1.8	-777.67	1.8	-612.52	2.12	-707.45
123	124	26.20	-2614.86	-91.08	384.20	0	-919.94	1.8	-982.79	1.8	-626.32	2.12	-731.84
124	124	26.20	-1701.11	-91.08	-55.31	0	-1063.82	1.8	-573.24	1.8	-270.60	2.12	-290.68
124	125	27.60	-1701.11	-78.99	63.75	0	-908.39	1.8	-739.09	1.8	-284.40	2.12	-315.08
125	125	27.60	-2055.42	-79.00	-146.00	0	-1525.56	1.8	-535.23	1.8	-284.40	2.12	-315.08
125	126	29.00	-2055.42	-66.92	-43.85	0	-1397.04	1.8	-661.77	1.8	-298.20	2.12	-339.48
126	126	29.00	-1122.96	-62.12	-483.37	0	-1651.99	1.8	226.17	1.8	0.00	2.12	0.00
126	127	30.40	-1129.71	-51.92	-398.64	0	-1526.04	1.8	23.49	1.8	0.00	2.12	0.00
127	127	30.40	-1460.38	-54.02	-578.79	0	-2073.32	1.8	156.86	1.8	0.00	2.12	0.00
127	128	31.80	-1460.38	-41.93	-511.64	0	-1971.00	1.8	0.44	1.8	0.00	2.12	0.00
128	128	31.80	-1460.38	-41.93	-511.64	0	-1971.00	1.8	0.44	1.8	0.00	2.12	0.00
128	129	33.20	-1460.38	-29.86	-461.36	0	-1894.38	1.8	-116.69	1.8	0.00	2.12	0.00
129	129	33.20	-1460.38	-29.86	-461.36	0	-1894.38	1.8	-116.69	1.8	0.00	2.12	0.00
129	130	34.60	-1460.38	-17.77	-428.02	0	-1843.60	1.8	-194.33	1.8	0.00	2.12	0.00
130	130	34.60	-1460.38	-17.77	-428.02	0	-1843.60	1.8	-194.33	1.8	0.00	2.12	0.00
130	131	36.00	-1460.38	-5.69	-411.58	0	-1818.54	1.8	-232.63	1.8	0.00	2.12	0.00
131	131	36.00	-1460.38	-5.69	-411.58	0	-1818.54	1.8	-232.63	1.8	0.00	2.12	0.00
131	132	37.40	-1460.38	6.39	-412.08	0	-1819.30	1.8	-231.47	1.8	0.00	2.12	0.00
132	132	37.40	-1460.38	6.39	-412.08	0	-1819.30	1.8	-231.47	1.8	0.00	2.12	0.00
132	133	38.80	-1460.38	18.48	-429.48	0	-1845.82	1.8	-190.94	1.8	0.00	2.12	0.00
133	133	38.80	-1460.38	18.48	-429.48	0	-1845.82	1.8	-190.94	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ+
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	30.55	-463.79	0	-1898.10	1.8	-111.02	1.8	0.00	2.12	0.00
134	134	40.20	-1460.38	30.55	-463.79	0	-1898.10	1.8	-111.02	1.8	0.00	2.12	0.00
134	135	41.60	-1460.38	42.64	-515.02	0	-1976.16	1.8	8.32	1.8	0.00	2.12	0.00
135	135	41.60	-1135.74	42.07	-334.87	0	-1434.24	1.8	-130.01	1.8	0.00	2.12	0.00
135	136	43.00	-1128.92	52.42	-404.77	0	-1537.65	1.8	38.18	1.8	0.00	2.12	0.00
136	136	43.00	-2055.42	55.69	34.75	0	-1326.09	1.8	-667.99	1.8	-320.17	2.12	-378.33
136	137	44.40	-2055.42	67.77	-51.67	0	-1440.40	1.8	-542.70	1.8	-310.77	2.12	-361.70
137	137	44.40	-1701.11	67.77	158.08	0	-823.24	1.8	-746.56	1.8	-310.77	2.12	-361.70
137	138	45.80	-1701.11	79.86	54.74	0	-964.47	1.8	-581.95	1.8	-301.37	2.12	-345.07
138	138	45.80	-2614.86	79.87	494.25	0	-820.58	1.8	-991.51	1.8	-657.08	2.12	-786.24
138	139	47.20	-2614.86	91.94	374.01	0	-988.70	1.8	-787.63	1.8	-647.67	2.12	-769.61
139	139	47.20	-2339.29	91.94	545.42	0	-495.53	1.8	-965.41	1.8	-647.67	2.12	-769.61
139	140	48.60	-2345.74	103.53	408.84	0	-691.99	1.8	-724.33	1.8	-640.15	2.12	-754.97
140	140	48.60	-2345.92	103.52	408.89	0	-692.00	1.8	-724.40	1.8	-640.21	2.12	-755.04
140	141	50.00	-2345.92	122.60	250.63	0	-921.03	1.8	-430.71	1.8	-630.98	2.12	-738.73
141	1141	50.00	-2345.71	-122.68	250.64	0	-920.97	1.8	-430.65	1.8	-630.93	2.12	-738.68
141	142	51.40	-2345.71	-103.60	409.02	0	-691.82	1.8	-724.37	1.8	-640.18	2.12	-755.04
142	142	51.40	-2345.10	-103.60	408.96	0	-691.68	1.8	-724.17	1.8	-640.01	2.12	-754.86
142	143	52.80	-2345.10	-91.51	545.58	0	-497.16	1.8	-967.25	1.8	-649.27	2.12	-771.23
143	143	52.80	-2619.68	-91.57	374.07	0	-990.13	1.8	-789.13	1.8	-648.98	2.12	-770.92
143	144	54.20	-2614.86	-79.87	494.25	0	-820.58	1.8	-991.51	1.8	-657.08	2.12	-786.24
144	144	54.20	-1701.11	-79.87	54.74	0	-964.47	1.8	-581.95	1.8	-301.37	2.12	-345.07
144	145	55.60	-1701.11	-67.78	158.09	0	-823.23	1.8	-746.56	1.8	-310.77	2.12	-361.70
145	145	55.60	-2055.42	-67.77	-51.67	0	-1440.40	1.8	-542.70	1.8	-310.77	2.12	-361.70
145	146	57.00	-2055.42	-55.69	34.75	0	-1326.09	1.8	-667.99	1.8	-320.17	2.12	-378.33
146	146	57.00	-1128.92	-52.43	-404.77	0	-1537.65	1.8	38.18	1.8	0.00	2.12	0.00
146	147	58.40	-1133.95	-41.17	-335.76	0	-1434.13	1.8	-126.48	1.8	0.00	2.12	0.00
147	147	58.40	-1458.36	-42.69	-515.91	0	-1975.87	1.8	12.03	1.8	0.00	2.12	0.00
147	148	59.80	-1458.36	-30.60	-464.61	0	-1897.70	1.8	-107.47	1.8	0.00	2.12	0.00
148	148	59.80	-1458.36	-30.60	-464.61	0	-1897.70	1.8	-107.47	1.8	0.00	2.12	0.00
148	149	61.20	-1458.36	-18.53	-430.22	0	-1845.30	1.8	-187.58	1.8	0.00	2.12	0.00
149	149	61.20	-1458.36	-18.53	-430.22	0	-1845.30	1.8	-187.58	1.8	0.00	2.12	0.00
149	150	62.60	-1458.36	-6.44	-412.73	0	-1818.65	1.8	-228.32	1.8	0.00	2.12	0.00
150	150	62.60	-1458.36	-6.44	-412.73	0	-1818.65	1.8	-228.32	1.8	0.00	2.12	0.00
150	151	64.00	-1456.62	5.61	-412.16	0	-1816.35	1.8	-228.22	1.8	0.00	2.12	0.00
151	151	64.00	-1456.62	5.61	-412.16	0	-1816.35	1.8	-228.22	1.8	0.00	2.12	0.00
151	152	65.40	-1456.62	17.69	-428.48	0	-1841.22	1.8	-190.21	1.8	0.00	2.12	0.00
152	152	65.40	-1456.62	17.69	-428.48	0	-1841.22	1.8	-190.21	1.8	0.00	2.12	0.00
152	153	66.80	-1456.62	29.78	-461.70	0	-1891.84	1.8	-112.82	1.8	0.00	2.12	0.00
153	153	66.80	-1456.62	29.78	-461.70	0	-1891.84	1.8	-112.82	1.8	0.00	2.12	0.00
153	154	68.20	-1456.62	41.85	-511.87	0	-1968.29	1.8	4.04	1.8	0.00	2.12	0.00
154	154	68.20	-1456.62	41.85	-511.87	0	-1968.29	1.8	4.04	1.8	0.00	2.12	0.00
154	155	69.60	-1456.62	53.94	-578.91	0	-2070.44	1.8	160.20	1.8	0.00	2.12	0.00
155	155	69.60	-1126.45	50.04	-398.76	0	-1523.57	1.8	26.43	1.8	0.00	2.12	0.00
155	156	71.00	-1122.96	62.12	-483.38	0	-1652.01	1.8	226.19	1.8	0.00	2.12	0.00
156	156	71.00	-2055.42	66.92	-43.86	0	-1397.05	1.8	-661.77	1.8	-298.20	2.12	-339.47
156	157	72.40	-2055.42	79.00	-145.99	0	-1525.55	1.8	-535.23	1.8	-284.41	2.12	-315.08
157	157	72.40	-1701.11	79.00	63.76	0	-908.39	1.8	-739.10	1.8	-284.41	2.12	-315.08
157	158	73.80	-1701.11	91.09	-55.31	0	-1063.82	1.8	-573.24	1.8	-270.60	2.12	-290.68
158	158	73.80	-2614.86	91.08	384.20	0	-919.94	1.8	-982.79	1.8	-626.32	2.12	-731.84
158	159	75.20	-2614.86	103.15	248.23	0	-1102.25	1.8	-777.66	1.8	-612.52	2.12	-707.44
159	159	75.20	-2339.29	103.15	419.64	0	-609.08	1.8	-955.44	1.8	-612.52	2.12	-707.44
159	160	76.60	-2343.12	114.78	267.26	0	-819.01	1.8	-712.28	1.8	-599.87	2.12	-684.30
160	160	76.60	-2343.06	114.76	267.34	0	-818.92	1.8	-712.28	1.8	-599.88	2.12	-684.32
160	161	78.00	-2343.06	133.84	93.33	0	-1062.17	1.8	-417.34	1.8	-586.26	2.12	-660.23
161	1161	78.00	-2303.37	-127.38	119.43	0	-989.08	1.8	-446.32	1.8	-586.18	2.12	-660.15
161	162	79.10	-2303.37	-112.39	251.30	0	-812.09	1.8	-645.82	1.8	-599.49	2.12	-683.70
162	162	79.10	-2302.99	-112.38	251.30	0	-811.97	1.8	-645.71	1.8	-599.39	2.12	-683.60
162	163	80.20	-2302.99	-102.89	369.73	0	-656.36	1.8	-813.96	1.8	-612.71	2.12	-707.15
163	163	80.20	-2578.03	-102.89	195.54	0	-1153.78	1.8	-629.61	1.8	-612.56	2.12	-706.99
163	164	81.30	-2578.03	-93.39	303.48	0	-1014.84	1.8	-773.53	1.8	-625.87	2.12	-730.53
164	164	81.30	-2577.33	-93.40	303.42	0	-1014.69	1.8	-773.30	1.8	-625.67	2.12	-730.32
164	165	82.40	-2577.33	-83.91	400.96	0	-892.32	1.8	-892.99	1.8	-638.99	2.12	-753.87
165	165	82.40	-1859.54	-83.96	-159.11	0	-1385.16	1.8	-360.72	1.8	-283.02	2.12	-312.43
165	166	83.50	-1859.54	-74.47	-71.97	0	-1279.36	1.8	-456.15	1.8	-296.35	2.12	-336.00
166	166	83.50	-1858.58	-74.57	-72.08	0	-1300.86	1.8	-434.65	1.8	-277.68	2.12	-310.70
166	167	84.60	-1858.58	-65.07	4.72	0	-1217.17	1.8	-500.41	1.8	-286.28	2.12	-327.84
167	167	84.60	-917.40	-56.43	-434.80	0	-1413.07	1.8	277.68	1.8	0.00	2.12	0.00
167	168	85.70	-920.89	-46.95	-369.05	0	-1314.64	1.8	121.78	1.8	0.00	2.12	0.00
168	168	85.70	-1141.67	-54.49	-487.54	0	-1674.29	1.8	204.32	1.8	0.00	2.12	0.00
168	169	86.80	-1141.67	-44.98	-432.86	0	-1590.96	1.8	76.93	1.8	0.00	2.12	0.00
169	169	86.80	-1141.67	-44.98	-432.86	0	-1590.96	1.8	76.93	1.8	0.00	2.12	0.00
169	170	87.90	-1141.67	-35.50	-388.59	0	-1523.51	1.8	-26.18	1.8	0.00	2.12	0.00
170	170	87.90	-1141.67	-35.50	-388.59	0	-1523.51	1.8	-26.18	1.8	0.00	2.12	0.00
170	171	89.00	-1141.67	-26.00	-354.78	0	-1471.98	1.8	-104.96	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F5.T0.MZ+

11/09/03

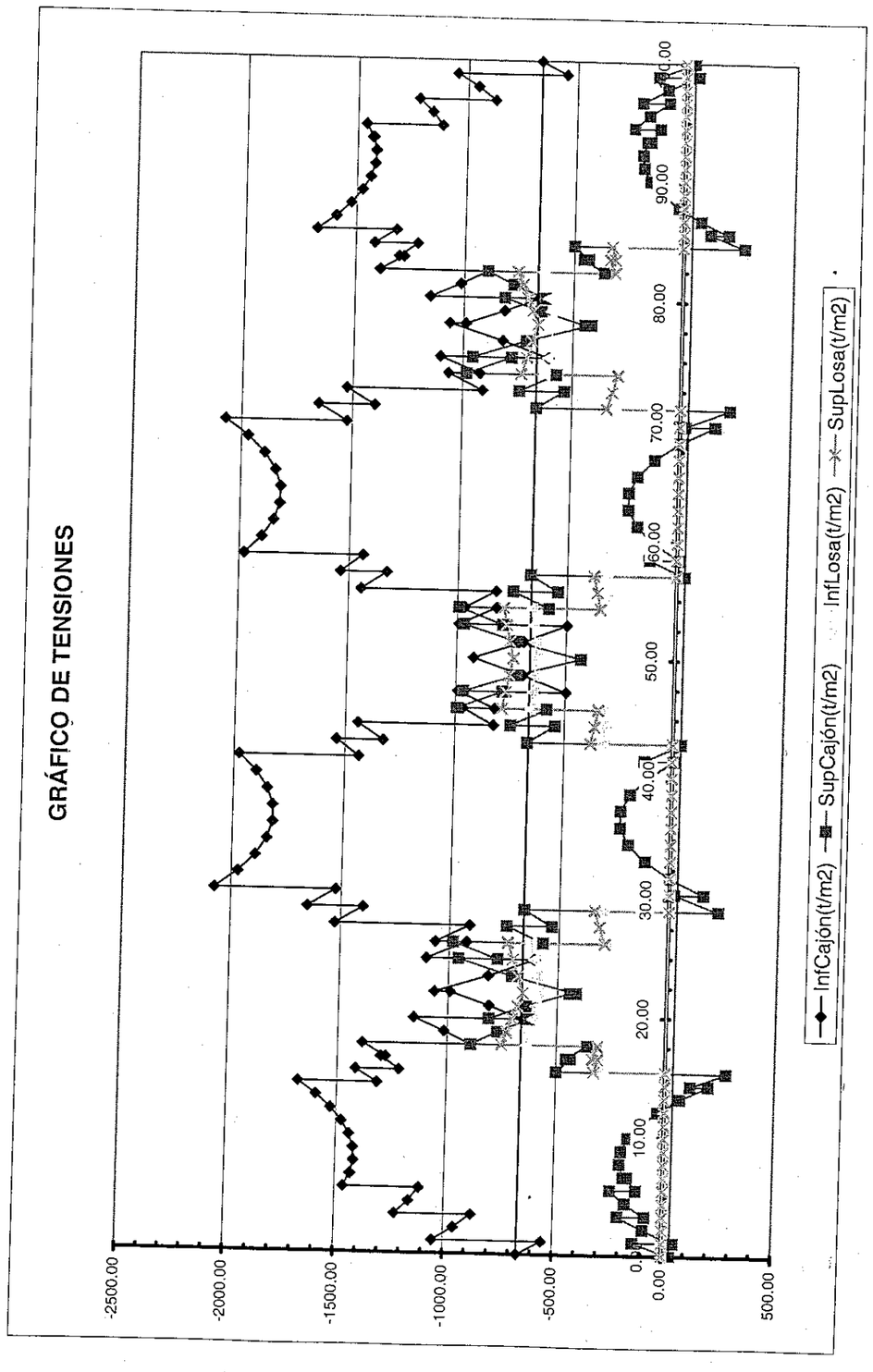
CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ+
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	-26.00	-354.78	0	-1471.98	1.8	-104.96	1.8	0.00	2.12	0.00
171	172	90.10	-1141.67	-16.51	-331.41	0	-1436.38	1.8	-159.38	1.8	0.00	2.12	0.00
172	172	90.10	-1141.67	-16.51	-331.41	0	-1436.38	1.8	-159.38	1.8	0.00	2.12	0.00
172	173	91.20	-1141.67	-7.02	-318.48	0	-1416.67	1.8	-189.52	1.8	0.00	2.12	0.00
173	173	91.20	-1141.67	-7.02	-318.48	0	-1416.67	1.8	-189.52	1.8	0.00	2.12	0.00
173	174	92.30	-1141.67	2.48	-315.98	0	-1412.87	1.8	-195.33	1.8	0.00	2.12	0.00
174	174	92.30	-1141.67	2.48	-315.98	0	-1412.87	1.8	-195.33	1.8	0.00	2.12	0.00
174	175	93.40	-1141.67	11.97	-323.94	0	-1424.99	1.8	-176.80	1.8	0.00	2.12	0.00
175	175	93.40	-1141.67	11.97	-323.94	0	-1428.86	1.8	-160.88	1.8	0.00	2.12	0.00
175	176	94.50	-1141.67	21.46	-342.34	0	-1458.13	1.8	-118.11	1.8	0.00	2.12	0.00
176	176	94.50	-944.83	21.46	-223.85	0	-1112.14	1.8	-235.94	1.8	0.00	2.12	0.00
176	177	95.60	-944.83	30.96	-252.68	0	-1158.00	1.8	-168.93	1.8	0.00	2.12	0.00
177	177	95.60	-944.83	30.96	-252.68	0	-1158.00	1.8	-168.93	1.8	0.00	2.12	0.00
177	178	96.70	-944.83	40.44	-291.96	0	-1220.49	1.8	-77.65	1.8	0.00	2.12	0.00
178	178	96.70	-747.99	40.44	-171.50	0	-871.35	1.8	-200.07	1.8	0.00	2.12	0.00
178	179	97.80	-747.99	49.95	-221.22	0	-950.44	1.8	-84.52	1.8	0.00	2.12	0.00
179	179	97.80	-747.99	49.95	-221.22	0	-950.44	1.8	-84.52	1.8	0.00	2.12	0.00
179	180	98.90	-747.99	59.43	-281.38	0	-1046.14	1.8	55.28	1.8	0.00	2.12	0.00
180	180	98.90	-472.42	59.43	-107.22	0	-548.59	1.8	-128.89	1.8	0.00	2.12	0.00
180	181	100.00	-472.42	70.84	-178.89	0	-662.58	1.8	37.63	1.8	0.00	2.12	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ-

Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-70.85	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
1	2	1.10	-517.71	-58.34	-127.27	0	-616.72	1.8	-118.56	1.8	0.00	2.12	0.00
2	2	1.10	-822.30	-58.34	-319.76	0	-1166.65	1.8	85.00	1.8	0.00	2.12	0.00
2	3	2.20	-822.30	-48.86	-260.80	0	-1072.87	1.8	-52.00	1.8	0.00	2.12	0.00
3	3	2.20	-822.30	-48.86	-260.80	0	-1072.87	1.8	-52.00	1.8	0.00	2.12	0.00
3	4	3.30	-822.30	-39.35	-212.29	0	-995.71	1.8	-164.72	1.8	0.00	2.12	0.00
4	4	3.30	-1039.86	-39.35	-345.44	0	-1381.60	1.8	-29.42	1.8	0.00	2.12	0.00
4	5	4.40	-1039.86	-29.87	-307.40	0	-1321.08	1.8	-117.84	1.8	0.00	2.12	0.00
5	5	4.40	-1039.86	-29.87	-307.40	0	-1321.08	1.8	-117.84	1.8	0.00	2.12	0.00
5	6	5.50	-1039.86	-20.37	-279.78	0	-1277.14	1.8	-182.01	1.8	0.00	2.12	0.00
6	6	5.50	-1257.42	-20.37	-410.74	0	-1659.56	1.8	-51.79	1.8	0.00	2.12	0.00
6	7	6.60	-1257.42	-10.88	-393.54	0	-1632.20	1.8	-91.75	1.8	0.00	2.12	0.00
7	7	6.60	-1257.42	-10.88	-393.54	0	-1625.48	1.8	-109.08	1.8	0.00	2.12	0.00
7	8	7.70	-1257.42	-1.39	-386.80	0	-1615.21	1.8	-124.78	1.8	0.00	2.12	0.00
8	8	7.70	-1257.42	-1.39	-386.80	0	-1615.21	1.8	-124.78	1.8	0.00	2.12	0.00
8	9	8.80	-1257.42	8.11	-390.51	0	-1620.86	1.8	-116.14	1.8	0.00	2.12	0.00
9	9	8.80	-1257.42	8.11	-390.51	0	-1620.86	1.8	-116.14	1.8	0.00	2.12	0.00
9	10	9.90	-1257.42	17.60	-404.66	0	-1642.43	1.8	-83.17	1.8	0.00	2.12	0.00
10	10	9.90	-1257.42	17.60	-404.66	0	-1642.43	1.8	-83.17	1.8	0.00	2.12	0.00
10	11	11.00	-1257.42	27.09	-429.25	0	-1679.88	1.8	-25.91	1.8	0.00	2.12	0.00
11	11	11.00	-1257.42	27.09	-429.25	0	-1679.88	1.8	-25.91	1.8	0.00	2.12	0.00
11	12	12.10	-1257.42	36.59	-464.28	0	-1733.26	1.8	55.69	1.8	0.00	2.12	0.00
12	12	12.10	-1257.42	36.59	-464.28	0	-1733.26	1.8	55.69	1.8	0.00	2.12	0.00
12	13	13.20	-1257.42	46.07	-509.77	0	-1802.58	1.8	161.66	1.8	0.00	2.12	0.00
13	13	13.20	-1257.42	46.07	-509.77	0	-1802.58	1.8	161.66	1.8	0.00	2.12	0.00
13	14	14.30	-1257.42	55.58	-565.66	0	-1887.74	1.8	291.85	1.8	0.00	2.12	0.00
14	14	14.30	-1016.08	45.33	-434.69	0	-1494.10	1.8	198.29	1.8	0.00	2.12	0.00
14	15	15.40	-1016.27	57.27	-500.21	0	-1595.19	1.8	350.65	1.8	0.00	2.12	0.00
15	15	15.40	-1871.02	66.07	-102.55	0	-1398.70	1.8	-426.60	1.8	-253.64	2.12	-285.90
15	16	16.50	-1871.02	75.57	-180.45	0	-1483.34	1.8	-360.63	1.8	-244.87	2.12	-268.40
16	16	16.50	-1871.02	75.57	-180.46	0	-1467.89	1.8	-375.72	1.8	-257.97	2.12	-286.22
16	17	17.60	-1871.02	85.06	-269.22	0	-1575.52	1.8	-278.95	1.8	-244.33	2.12	-262.11
17	17	17.60	-2480.19	85.06	262.00	0	-1058.78	1.8	-785.80	1.8	-566.17	2.12	-661.26
17	18	18.70	-2480.19	94.55	163.21	0	-1182.36	1.8	-665.75	1.8	-552.53	2.12	-637.15
18	18	18.70	-2480.18	94.55	163.21	0	-1182.35	1.8	-665.74	1.8	-552.53	2.12	-637.15
18	19	19.80	-2480.18	104.05	53.99	0	-1322.53	1.8	-521.45	1.8	-538.89	2.12	-613.03
19	19	19.80	-2175.60	104.05	246.48	0	-772.61	1.8	-725.01	1.8	-538.89	2.12	-613.03
19	20	20.90	-2175.60	113.54	126.80	0	-929.43	1.8	-556.39	1.8	-525.26	2.12	-588.92
20	20	20.90	-2175.60	113.54	126.80	0	-929.43	1.8	-556.39	1.8	-525.26	2.12	-588.92
20	21	22.00	-2175.60	128.53	-6.34	0	-1107.65	1.8	-356.51	1.8	-511.62	2.12	-564.81
21	1021	22.00	-2219.11	-134.81	-35.15	0	-1188.29	1.8	-324.38	1.8	-511.62	2.12	-564.81
21	22	23.40	-2219.11	-115.73	140.22	0	-943.72	1.8	-619.73	1.8	-525.59	2.12	-589.51
22	22	23.40	-2219.11	-115.73	140.22	0	-943.72	1.8	-619.73	1.8	-525.59	2.12	-589.51
22	23	24.80	-2219.11	-103.64	293.79	0	-733.82	1.8	-864.41	1.8	-539.56	2.12	-614.21
23	23	24.80	-2523.70	-103.63	104.34	0	-1278.90	1.8	-667.93	1.8	-539.56	2.12	-614.21
23	24	26.20	-2523.70	-91.56	240.96	0	-1095.95	1.8	-873.25	1.8	-553.52	2.12	-638.90
24	24	26.20	-1696.97	-91.56	-156.69	0	-1226.13	1.8	-502.69	1.8	-231.69	2.12	-239.75
24	25	27.60	-1696.97	-79.47	-36.96	0	-1070.06	1.8	-668.75	1.8	-245.66	2.12	-264.45
25	25	27.60	-2088.58	-79.48	-268.79	0	-1752.19	1.8	-443.42	1.8	-245.66	2.12	-264.45
25	26	29.00	-2088.58	-67.40	-165.98	0	-1623.03	1.8	-570.16	1.8	-259.62	2.12	-289.15
26	26	29.00	-1242.90	-62.54	-563.64	0	-1874.42	1.8	316.83	1.8	0.00	2.12	0.00
26	27	30.40	-1243.14	-48.58	-478.50	0	-1742.53	1.8	118.51	1.8	0.00	2.12	0.00
27	27	30.40	-1606.18	-54.34	-677.61	0	-2342.86	1.8	268.12	1.8	0.00	2.12	0.00
27	28	31.80	-1606.18	-42.25	-610.02	0	-2239.87	1.8	110.67	1.8	0.00	2.12	0.00
28	28	31.80	-1606.18	-42.25	-610.02	0	-2239.87	1.8	110.67	1.8	0.00	2.12	0.00
28	29	33.20	-1606.18	-30.18	-559.32	0	-2162.60	1.8	-7.45	1.8	0.00	2.12	0.00
29	29	33.20	-1606.18	-30.18	-559.32	0	-2162.60	1.8	-7.45	1.8	0.00	2.12	0.00
29	30	34.60	-1606.18	-18.09	-525.54	0	-2111.13	1.8	-86.14	1.8	0.00	2.12	0.00
30	30	34.60	-1606.18	-18.09	-525.54	0	-2111.13	1.8	-86.14	1.8	0.00	2.12	0.00
30	31	36.00	-1606.18	-6.01	-508.67	0	-2085.43	1.8	-125.43	1.8	0.00	2.12	0.00
31	31	36.00	-1606.18	-6.01	-508.67	0	-2085.43	1.8	-125.43	1.8	0.00	2.12	0.00
31	32	37.40	-1606.18	6.07	-508.71	0	-2085.49	1.8	-125.34	1.8	0.00	2.12	0.00
32	32	37.40	-1606.18	6.07	-508.71	0	-2085.49	1.8	-125.34	1.8	0.00	2.12	0.00
32	33	38.80	-1606.18	18.16	-525.67	0	-2111.33	1.8	-85.83	1.8	0.00	2.12	0.00
33	33	38.80	-1606.18	18.16	-525.67	0	-2111.33	1.8	-85.83	1.8	0.00	2.12	0.00
33	34	40.20	-1606.18	30.23	-559.55	0	-2162.96	1.8	-6.91	1.8	0.00	2.12	0.00
34	34	40.20	-1606.18	30.23	-559.55	0	-2162.96	1.8	-6.91	1.8	0.00	2.12	0.00
34	35	41.60	-1606.18	42.32	-610.34	0	-2240.35	1.8	111.41	1.8	0.00	2.12	0.00
35	35	41.60	-1249.48	38.19	-411.23	0	-1645.63	1.8	-43.41	1.8	0.00	2.12	0.00
35	36	43.00	-1249.32	52.00	-478.45	0	-1750.39	1.8	113.09	1.8	0.00	2.12	0.00
36	36	43.00	-2088.58	55.21	-80.79	0	-1545.69	1.8	-578.30	1.8	-283.26	2.12	-330.95
36	37	44.40	-2088.58	67.29	-166.54	0	-1659.36	1.8	-453.20	1.8	-274.03	2.12	-314.62
37	37	44.40	-1696.97	67.30	65.28	0	-977.24	1.8	-678.52	1.8	-274.03	2.12	-314.61
37	38	45.80	-1696.97	79.39	-37.39	0	-1117.82	1.8	-514.11	1.8	-264.79	2.12	-298.28
38	38	45.80	-2523.70	79.39	360.27	0	-987.64	1.8	-884.66	1.8	-586.63	2.12	-697.44

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ-
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	91.46	240.68	0	-1155.13	1.8	-680.97	1.8	-577.39	2.12	-681.10
39	39	47.20	-2219.11	91.46	430.14	0	-610.03	1.8	-877.46	1.8	-577.39	2.12	-681.10
39	40	48.60	-2212.66	104.05	293.02	0	-803.04	1.8	-632.25	1.8	-566.27	2.12	-662.77
40	40	48.60	-2212.49	104.06	292.95	0	-803.06	1.8	-632.18	1.8	-566.21	2.12	-662.69
40	41	50.00	-2212.49	123.14	133.92	0	-1032.84	1.8	-338.26	1.8	-556.79	2.12	-646.04
41	1041	50.00	-2212.70	-123.06	133.91	0	-1032.91	1.8	-338.32	1.8	-556.85	2.12	-646.10
41	42	51.40	-2212.70	-103.98	292.83	0	-803.23	1.8	-632.21	1.8	-566.24	2.12	-662.70
42	42	51.40	-2213.30	-103.97	292.88	0	-803.37	1.8	-632.41	1.8	-566.41	2.12	-662.88
42	43	52.80	-2213.30	-91.88	429.99	0	-608.39	1.8	-875.63	1.8	-575.80	2.12	-679.48
43	43	52.80	-2518.88	-91.83	240.63	0	-1153.69	1.8	-679.48	1.8	-576.09	2.12	-679.79
43	44	54.20	-2523.70	-79.39	360.26	0	-987.65	1.8	-884.66	1.8	-586.62	2.12	-697.43
44	44	54.20	-1696.97	-79.39	-37.40	0	-1117.83	1.8	-514.11	1.8	-264.79	2.12	-298.28
44	45	55.60	-1696.97	-67.30	65.29	0	-977.23	1.8	-678.53	1.8	-274.03	2.12	-314.62
45	45	55.60	-2088.58	-67.29	-166.55	0	-1659.37	1.8	-453.20	1.8	-274.03	2.12	-314.61
45	46	57.00	-2088.58	-55.21	-80.78	0	-1545.68	1.8	-578.31	1.8	-283.27	2.12	-330.95
46	46	57.00	-1249.32	-52.01	-478.44	0	-1750.37	1.8	113.06	1.8	0.00	2.12	0.00
46	47	58.40	-1251.27	-39.11	-410.33	0	-1645.72	1.8	-46.96	1.8	0.00	2.12	0.00
47	47	58.40	-1608.20	-42.27	-609.44	0	-2240.63	1.8	107.68	1.8	0.00	2.12	0.00
47	48	59.80	-1608.20	-30.18	-558.73	0	-2163.36	1.8	-10.45	1.8	0.00	2.12	0.00
48	48	59.80	-1608.20	-30.18	-558.73	0	-2163.36	1.8	-10.45	1.8	0.00	2.12	0.00
48	49	61.20	-1608.20	-18.11	-524.94	0	-2111.87	1.8	-89.16	1.8	0.00	2.12	0.00
49	49	61.20	-1608.20	-18.11	-524.94	0	-2111.87	1.8	-89.16	1.8	0.00	2.12	0.00
49	50	62.60	-1608.20	-6.02	-508.05	0	-2086.13	1.8	-128.51	1.8	0.00	2.12	0.00
50	50	62.60	-1608.20	-6.02	-508.05	0	-2086.13	1.8	-128.51	1.8	0.00	2.12	0.00
50	51	64.00	-1609.94	6.09	-508.10	0	-2087.63	1.8	-129.82	1.8	0.00	2.12	0.00
51	51	64.00	-1609.94	6.09	-508.10	0	-2087.63	1.8	-129.82	1.8	0.00	2.12	0.00
51	52	65.40	-1609.94	18.17	-525.08	0	-2113.51	1.8	-90.26	1.8	0.00	2.12	0.00
52	52	65.40	-1609.94	18.17	-525.08	0	-2113.51	1.8	-90.26	1.8	0.00	2.12	0.00
52	53	66.80	-1609.94	30.26	-558.97	0	-2165.15	1.8	-11.32	1.8	0.00	2.12	0.00
53	53	66.80	-1609.94	30.26	-558.97	0	-2165.15	1.8	-11.32	1.8	0.00	2.12	0.00
53	54	68.20	-1609.94	42.33	-609.78	0	-2242.57	1.8	107.04	1.8	0.00	2.12	0.00
54	54	68.20	-1609.94	42.33	-609.78	0	-2242.57	1.8	107.04	1.8	0.00	2.12	0.00
54	55	69.60	-1609.94	54.42	-677.48	0	-2345.73	1.8	264.75	1.8	0.00	2.12	0.00
55	55	69.60	-1246.39	50.46	-478.37	0	-1744.99	1.8	115.55	1.8	0.00	2.12	0.00
55	56	71.00	-1242.90	62.54	-563.65	0	-1874.44	1.8	316.85	1.8	0.00	2.12	0.00
56	56	71.00	-2088.58	67.40	-165.99	0	-1623.04	1.8	-570.16	1.8	-259.62	2.12	-289.14
56	57	72.40	-2088.58	79.48	-268.78	0	-1752.18	1.8	-443.43	1.8	-245.66	2.12	-264.45
57	57	72.40	-1696.97	79.48	-36.95	0	-1070.05	1.8	-668.75	1.8	-245.66	2.12	-264.45
57	58	73.80	-1696.97	91.57	-156.68	0	-1226.12	1.8	-502.70	1.8	-231.69	2.12	-239.75
58	58	73.80	-2523.70	91.56	240.97	0	-1095.94	1.8	-873.25	1.8	-553.53	2.12	-638.91
58	59	75.20	-2523.70	103.63	104.33	0	-1278.91	1.8	-667.92	1.8	-539.55	2.12	-614.20
59	59	75.20	-2219.11	103.63	293.79	0	-733.82	1.8	-864.41	1.8	-539.56	2.12	-614.21
59	60	76.60	-2215.29	116.19	139.70	0	-943.03	1.8	-618.40	1.8	-524.43	2.12	-588.25
60	60	76.60	-2215.34	116.22	139.62	0	-943.13	1.8	-618.39	1.8	-524.43	2.12	-588.23
60	61	78.00	-2215.34	135.30	-36.44	0	-1188.38	1.8	-322.85	1.8	-510.28	2.12	-563.22
61	1061	78.00	-2172.15	-128.68	-7.66	0	-1107.86	1.8	-355.07	1.8	-510.36	2.12	-563.29
61	62	79.10	-2172.15	-113.69	125.63	0	-929.49	1.8	-554.99	1.8	-524.04	2.12	-587.47
62	62	79.10	-2172.53	-113.70	125.63	0	-929.61	1.8	-555.10	1.8	-524.14	2.12	-587.57
62	63	80.20	-2172.53	-104.21	245.50	0	-772.61	1.8	-723.78	1.8	-537.82	2.12	-611.77
63	63	80.20	-2477.65	-104.21	53.04	0	-1322.67	1.8	-520.39	1.8	-537.97	2.12	-611.93
63	64	81.30	-2477.65	-94.71	162.44	0	-1182.33	1.8	-664.74	1.8	-551.66	2.12	-636.12
64	64	81.30	-2478.35	-94.70	162.48	0	-1182.50	1.8	-664.97	1.8	-551.86	2.12	-636.33
64	65	82.40	-2478.35	-85.21	261.44	0	-1058.75	1.8	-785.07	1.8	-565.54	2.12	-660.52
65	65	82.40	-1870.06	-85.16	-269.27	0	-1575.00	1.8	-279.51	1.8	-243.96	2.12	-261.64
65	66	83.50	-1870.06	-75.67	-180.82	0	-1467.94	1.8	-375.32	1.8	-257.62	2.12	-285.80
66	66	83.50	-1871.02	-75.59	-180.72	0	-1483.57	1.8	-360.58	1.8	-244.82	2.12	-268.31
66	67	84.60	-1871.02	-66.09	-102.78	0	-1398.91	1.8	-426.56	1.8	-253.60	2.12	-285.82
67	67	84.60	-1016.26	-57.27	-500.44	0	-1595.54	1.8	351.21	1.8	0.00	2.12	0.00
67	68	85.70	-1019.75	-47.79	-433.57	0	-1495.40	1.8	192.68	1.8	0.00	2.12	0.00
68	68	85.70	-1261.85	-55.51	-564.54	0	-1889.65	1.8	285.62	1.8	0.00	2.12	0.00
68	69	86.80	-1261.85	-46.00	-508.72	0	-1804.60	1.8	155.61	1.8	0.00	2.12	0.00
69	69	86.80	-1261.85	-46.00	-508.72	0	-1804.60	1.8	155.61	1.8	0.00	2.12	0.00
69	70	87.90	-1261.85	-36.52	-463.34	0	-1735.44	1.8	49.89	1.8	0.00	2.12	0.00
70	70	87.90	-1261.85	-36.52	-463.34	0	-1735.44	1.8	49.89	1.8	0.00	2.12	0.00
70	71	89.00	-1261.85	-27.02	-428.39	0	-1682.20	1.8	-31.51	1.8	0.00	2.12	0.00
71	71	89.00	-1261.85	-27.02	-428.39	0	-1682.20	1.8	-31.51	1.8	0.00	2.12	0.00
71	72	90.10	-1261.85	-17.53	-403.89	0	-1644.86	1.8	-88.59	1.8	0.00	2.12	0.00
72	72	90.10	-1261.85	-17.53	-403.89	0	-1644.86	1.8	-88.59	1.8	0.00	2.12	0.00
72	73	91.20	-1261.85	-8.04	-389.82	0	-1623.43	1.8	-121.36	1.8	0.00	2.12	0.00
73	73	91.20	-1261.85	-8.04	-389.82	0	-1623.43	1.8	-121.36	1.8	0.00	2.12	0.00
73	74	92.30	-1261.85	1.46	-386.20	0	-1617.90	1.8	-129.80	1.8	0.00	2.12	0.00
74	74	92.30	-1261.85	1.46	-386.20	0	-1617.90	1.8	-129.80	1.8	0.00	2.12	0.00
74	75	93.40	-1261.85	10.95	-393.03	0	-1628.30	1.8	-113.90	1.8	0.00	2.12	0.00
75	75	93.40	-1261.85	10.95	-393.03	0	-1634.92	1.8	-96.50	1.8	0.00	2.12	0.00
75	76	94.50	-1261.85	20.44	-410.30	0	-1662.40	1.8	-56.36	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F5.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ-
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	20.44	-279.33	0	-1279.99	1.8	-186.59	1.8	0.00	2.12	0.00
76	77	95.60	-1044.29	29.94	-307.04	0	-1324.06	1.8	-122.21	1.8	0.00	2.12	0.00
77	77	95.60	-1044.29	29.94	-307.04	0	-1324.06	1.8	-122.21	1.8	0.00	2.12	0.00
77	78	96.70	-1044.29	39.42	-345.20	0	-1384.75	1.8	-33.54	1.8	0.00	2.12	0.00
78	78	96.70	-826.73	39.42	-212.05	0	-998.86	1.8	-168.85	1.8	0.00	2.12	0.00
78	79	97.80	-826.73	48.93	-260.64	0	-1076.15	1.8	-55.93	1.8	0.00	2.12	0.00
79	79	97.80	-826.73	48.93	-260.64	0	-1076.15	1.8	-55.93	1.8	0.00	2.12	0.00
79	80	98.90	-826.73	58.41	-319.68	0	-1170.06	1.8	81.25	1.8	0.00	2.12	0.00
80	80	98.90	-522.14	58.41	-127.18	0	-620.13	1.8	-122.31	1.8	0.00	2.12	0.00
80	81	100.00	-522.14	70.84	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	101	0.00	-522.14	-70.85	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00
101	102	1.10	-517.71	-58.34	-127.27	0	-616.72	1.8	-118.56	1.8	0.00	2.12	0.00
102	102	1.10	-822.30	-58.34	-319.76	0	-1166.65	1.8	85.00	1.8	0.00	2.12	0.00
102	103	2.20	-822.30	-48.86	-260.80	0	-1072.87	1.8	-52.00	1.8	0.00	2.12	0.00
103	103	2.20	-822.30	-48.86	-260.80	0	-1072.87	1.8	-52.00	1.8	0.00	2.12	0.00
103	104	3.30	-822.30	-39.35	-212.29	0	-995.71	1.8	-164.72	1.8	0.00	2.12	0.00
104	104	3.30	-1039.86	-39.35	-345.44	0	-1381.60	1.8	-29.42	1.8	0.00	2.12	0.00
104	105	4.40	-1039.86	-29.87	-307.38	0	-1321.06	1.8	-117.86	1.8	0.00	2.12	0.00
105	105	4.40	-1039.86	-29.87	-307.38	0	-1321.06	1.8	-117.86	1.8	0.00	2.12	0.00
105	106	5.50	-1039.86	-20.37	-279.77	0	-1277.13	1.8	-182.04	1.8	0.00	2.12	0.00
106	106	5.50	-1257.42	-20.37	-410.73	0	-1659.54	1.8	-51.81	1.8	0.00	2.12	0.00
106	107	6.60	-1257.42	-10.88	-393.54	0	-1632.20	1.8	-91.75	1.8	0.00	2.12	0.00
107	107	6.60	-1257.42	-10.88	-393.54	0	-1625.48	1.8	-109.08	1.8	0.00	2.12	0.00
107	108	7.70	-1257.42	-1.39	-386.80	0	-1615.21	1.8	-124.78	1.8	0.00	2.12	0.00
108	108	7.70	-1257.42	-1.39	-386.80	0	-1615.21	1.8	-124.78	1.8	0.00	2.12	0.00
108	109	8.80	-1257.42	8.11	-390.51	0	-1620.86	1.8	-116.14	1.8	0.00	2.12	0.00
109	109	8.80	-1257.42	8.11	-390.51	0	-1620.86	1.8	-116.14	1.8	0.00	2.12	0.00
109	110	9.90	-1257.42	17.60	-404.66	0	-1642.43	1.8	-83.17	1.8	0.00	2.12	0.00
110	110	9.90	-1257.42	17.60	-404.66	0	-1642.43	1.8	-83.17	1.8	0.00	2.12	0.00
110	111	11.00	-1257.42	27.09	-429.25	0	-1679.88	1.8	-25.91	1.8	0.00	2.12	0.00
111	111	11.00	-1257.42	27.09	-429.25	0	-1679.88	1.8	-25.91	1.8	0.00	2.12	0.00
111	112	12.10	-1257.42	36.59	-464.28	0	-1733.26	1.8	55.69	1.8	0.00	2.12	0.00
112	112	12.10	-1257.42	36.59	-464.28	0	-1733.26	1.8	55.69	1.8	0.00	2.12	0.00
112	113	13.20	-1257.42	46.07	-509.76	0	-1802.56	1.8	161.63	1.8	0.00	2.12	0.00
113	113	13.20	-1257.42	46.07	-509.76	0	-1802.56	1.8	161.63	1.8	0.00	2.12	0.00
113	114	14.30	-1257.42	55.58	-565.66	0	-1887.74	1.8	291.85	1.8	0.00	2.12	0.00
114	114	14.30	-1016.08	45.33	-434.69	0	-1494.10	1.8	198.29	1.8	0.00	2.12	0.00
114	115	15.40	-1016.27	57.27	-500.21	0	-1595.19	1.8	350.65	1.8	0.00	2.12	0.00
115	115	15.40	-1871.02	66.07	-102.55	0	-1398.70	1.8	-426.60	1.8	-253.64	2.12	-285.90
115	116	16.50	-1871.02	75.57	-180.46	0	-1483.35	1.8	-360.63	1.8	-244.86	2.12	-268.40
116	116	16.50	-1871.02	75.57	-180.46	0	-1467.89	1.8	-375.72	1.8	-257.97	2.12	-286.22
116	117	17.60	-1871.02	85.06	-269.24	0	-1575.54	1.8	-278.94	1.8	-244.33	2.12	-262.10
117	117	17.60	-2480.18	85.06	262.00	0	-1058.78	1.8	-785.80	1.8	-566.17	2.12	-661.26
117	118	18.70	-2480.18	94.55	163.21	0	-1182.35	1.8	-665.74	1.8	-552.53	2.12	-637.15
118	118	18.70	-2480.18	94.55	163.21	0	-1182.35	1.8	-665.74	1.8	-552.53	2.12	-637.15
118	119	19.80	-2480.18	104.05	54.00	0	-1322.52	1.8	-521.45	1.8	-538.89	2.12	-613.03
119	119	19.80	-2175.60	104.05	246.49	0	-772.60	1.8	-725.01	1.8	-538.89	2.12	-613.03
119	120	20.90	-2175.60	113.54	126.80	0	-929.43	1.8	-556.39	1.8	-525.26	2.12	-588.92
120	120	20.90	-2175.60	113.54	126.80	0	-929.43	1.8	-556.39	1.8	-525.26	2.12	-588.92
120	121	22.00	-2175.60	128.53	-6.34	0	-1107.65	1.8	-356.51	1.8	-511.62	2.12	-564.81
121	1121	22.00	-2219.11	-134.81	-35.15	0	-1188.29	1.8	-324.38	1.8	-511.62	2.12	-564.81
121	122	23.40	-2219.11	-115.73	140.22	0	-943.72	1.8	-619.73	1.8	-525.59	2.12	-589.51
122	122	23.40	-2219.11	-115.73	140.22	0	-943.72	1.8	-619.73	1.8	-525.59	2.12	-589.51
122	123	24.80	-2219.11	-103.64	293.78	0	-733.83	1.8	-864.41	1.8	-539.55	2.12	-614.20
123	123	24.80	-2523.70	-103.63	104.34	0	-1278.90	1.8	-667.93	1.8	-539.56	2.12	-614.21
123	124	26.20	-2523.70	-91.56	240.96	0	-1095.95	1.8	-873.25	1.8	-553.52	2.12	-638.90
124	124	26.20	-1696.97	-91.56	-156.69	0	-1226.13	1.8	-502.69	1.8	-231.69	2.12	-239.75
124	125	27.60	-1696.97	-79.47	-36.97	0	-1070.07	1.8	-668.74	1.8	-245.65	2.12	-264.44
125	125	27.60	-2088.58	-79.48	-268.80	0	-1752.20	1.8	-443.42	1.8	-245.65	2.12	-264.44
125	126	29.00	-2088.58	-67.40	-165.99	0	-1623.04	1.8	-570.16	1.8	-259.62	2.12	-289.14
126	126	29.00	-1242.90	-62.54	-563.65	0	-1874.44	1.8	316.85	1.8	0.00	2.12	0.00
126	127	30.40	-1243.14	-48.58	-478.50	0	-1742.53	1.8	118.51	1.8	0.00	2.12	0.00
127	127	30.40	-1606.18	-54.34	-677.61	0	-2342.86	1.8	268.12	1.8	0.00	2.12	0.00
127	128	31.80	-1606.18	-42.25	-610.02	0	-2239.87	1.8	110.67	1.8	0.00	2.12	0.00
128	128	31.80	-1606.18	-42.25	-610.02	0	-2239.87	1.8	110.67	1.8	0.00	2.12	0.00
128	129	33.20	-1606.18	-30.18	-559.31	0	-2162.59	1.8	-7.47	1.8	0.00	2.12	0.00
129	129	33.20	-1606.18	-30.18	-559.31	0	-2162.59	1.8	-7.47	1.8	0.00	2.12	0.00
129	130	34.60	-1606.18	-18.09	-525.54	0	-2111.13	1.8	-86.14	1.8	0.00	2.12	0.00
130	130	34.60	-1606.18	-18.09	-525.54	0	-2111.13	1.8	-86.14	1.8	0.00	2.12	0.00
130	131	36.00	-1606.18	-6.01	-508.66	0	-2085.41	1.8	-125.46	1.8	0.00	2.12	0.00
131	131	36.00	-1606.18	-6.01	-508.66	0	-2085.41	1.8	-125.46	1.8	0.00	2.12	0.00
131	132	37.40	-1606.18	6.07	-508.72	0	-2085.51	1.8	-125.31	1.8	0.00	2.12	0.00
132	132	37.40	-1606.18	6.07	-508.72	0	-2085.51	1.8	-125.31	1.8	0.00	2.12	0.00
132	133	38.80	-1606.18	18.16	-525.68	0	-2111.35	1.8	-85.81	1.8	0.00	2.12	0.00
133	133	38.80	-1606.18	18.16	-525.68	0	-2111.35	1.8	-85.81	1.8	0.00	2.12	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ-
Construcción sin gradiente en fase constructiva 5

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	30.23	-559.55	0	-2162.96	1.8	-6.91	1.8	0.00	2.12	0.00
134	134	40.20	-1606.18	30.23	-559.55	0	-2162.96	1.8	-6.91	1.8	0.00	2.12	0.00
134	135	41.60	-1606.18	42.32	-610.34	0	-2240.35	1.8	111.41	1.8	0.00	2.12	0.00
135	135	41.60	-1249.48	38.19	-411.23	0	-1645.63	1.8	-43.41	1.8	0.00	2.12	0.00
135	136	43.00	-1249.32	52.00	-478.45	0	-1750.39	1.8	113.09	1.8	0.00	2.12	0.00
136	136	43.00	-2088.58	55.21	-80.79	0	-1545.69	1.8	-578.30	1.8	-283.26	2.12	-330.95
136	137	44.40	-2088.58	67.29	-166.54	0	-1659.36	1.8	-453.20	1.8	-274.03	2.12	-314.62
137	137	44.40	-1696.97	67.29	65.28	0	-977.24	1.8	-678.52	1.8	-274.03	2.12	-314.61
137	138	45.80	-1696.97	79.38	-37.39	0	-1117.82	1.8	-514.11	1.8	-264.79	2.12	-298.28
138	138	45.80	-2523.70	79.39	360.27	0	-987.64	1.8	-884.66	1.8	-586.63	2.12	-697.44
138	139	47.20	-2523.70	91.46	240.69	0	-1155.12	1.8	-680.98	1.8	-577.39	2.12	-681.10
139	139	47.20	-2219.11	91.46	430.14	0	-610.03	1.8	-877.46	1.8	-577.39	2.12	-681.10
139	140	48.60	-2212.66	104.05	293.02	0	-803.04	1.8	-632.25	1.8	-566.27	2.12	-662.77
140	140	48.60	-2212.49	104.06	292.95	0	-803.06	1.8	-632.18	1.8	-566.21	2.12	-662.69
140	141	50.00	-2212.49	123.14	133.93	0	-1032.83	1.8	-338.26	1.8	-556.79	2.12	-646.05
141	1141	50.00	-2212.71	-123.06	133.92	0	-1032.91	1.8	-338.33	1.8	-556.85	2.12	-646.10
141	142	51.40	-2212.71	-103.98	292.82	0	-803.25	1.8	-632.21	1.8	-566.24	2.12	-662.70
142	142	51.40	-2213.30	-103.96	292.88	0	-803.38	1.8	-632.40	1.8	-566.41	2.12	-662.88
142	143	52.80	-2213.30	-91.87	430.00	0	-608.38	1.8	-875.63	1.8	-575.80	2.12	-679.48
143	143	52.80	-2518.88	-91.83	240.65	0	-1153.67	1.8	-679.48	1.8	-576.09	2.12	-679.80
143	144	54.20	-2523.70	-79.39	360.27	0	-987.64	1.8	-884.66	1.8	-586.63	2.12	-697.44
144	144	54.20	-1696.97	-79.39	-37.39	0	-1117.82	1.8	-514.11	1.8	-264.79	2.12	-298.28
144	145	55.60	-1696.97	-67.30	65.29	0	-977.23	1.8	-678.53	1.8	-274.03	2.12	-314.62
145	145	55.60	-2088.58	-67.29	-166.54	0	-1659.36	1.8	-453.20	1.8	-274.03	2.12	-314.62
145	146	57.00	-2088.58	-55.21	-80.79	0	-1545.69	1.8	-578.30	1.8	-283.26	2.12	-330.95
146	146	57.00	-1249.32	-52.01	-478.45	0	-1750.39	1.8	113.09	1.8	0.00	2.12	0.00
146	147	58.40	-1251.27	-39.11	-410.32	0	-1645.71	1.8	-46.98	1.8	0.00	2.12	0.00
147	147	58.40	-1608.20	-42.27	-609.43	0	-2240.61	1.8	107.65	1.8	0.00	2.12	0.00
147	148	59.80	-1608.20	-30.18	-558.73	0	-2163.36	1.8	-10.45	1.8	0.00	2.12	0.00
148	148	59.80	-1608.20	-30.18	-558.73	0	-2163.36	1.8	-10.45	1.8	0.00	2.12	0.00
148	149	61.20	-1608.20	-18.11	-524.94	0	-2111.87	1.8	-89.16	1.8	0.00	2.12	0.00
149	149	61.20	-1608.20	-18.11	-524.94	0	-2111.87	1.8	-89.16	1.8	0.00	2.12	0.00
149	150	62.60	-1608.20	-6.02	-508.05	0	-2086.13	1.8	-128.51	1.8	0.00	2.12	0.00
150	150	62.60	-1608.20	-6.02	-508.05	0	-2086.13	1.8	-128.51	1.8	0.00	2.12	0.00
150	151	64.00	-1609.94	6.09	-508.10	0	-2087.63	1.8	-129.82	1.8	0.00	2.12	0.00
151	151	64.00	-1609.94	6.09	-508.10	0	-2087.63	1.8	-129.82	1.8	0.00	2.12	0.00
151	152	65.40	-1609.94	18.17	-525.08	0	-2113.51	1.8	-90.26	1.8	0.00	2.12	0.00
152	152	65.40	-1609.94	18.17	-525.08	0	-2113.51	1.8	-90.26	1.8	0.00	2.12	0.00
152	153	66.80	-1609.94	30.26	-558.96	0	-2165.13	1.8	-11.34	1.8	0.00	2.12	0.00
153	153	66.80	-1609.94	30.26	-558.96	0	-2165.13	1.8	-11.34	1.8	0.00	2.12	0.00
153	154	68.20	-1609.94	42.33	-609.79	0	-2242.59	1.8	107.07	1.8	0.00	2.12	0.00
154	154	68.20	-1609.94	42.33	-609.79	0	-2242.59	1.8	107.07	1.8	0.00	2.12	0.00
154	155	69.60	-1609.94	54.42	-677.49	0	-2345.75	1.8	264.77	1.8	0.00	2.12	0.00
155	155	69.60	-1246.39	50.46	-478.38	0	-1745.00	1.8	115.57	1.8	0.00	2.12	0.00
155	156	71.00	-1242.90	62.54	-563.66	0	-1874.45	1.8	316.87	1.8	0.00	2.12	0.00
156	156	71.00	-2088.58	67.40	-166.00	0	-1623.05	1.8	-570.15	1.8	-259.62	2.12	-289.14
156	157	72.40	-2088.58	79.48	-268.79	0	-1752.19	1.8	-443.42	1.8	-245.66	2.12	-264.45
157	157	72.40	-1696.97	79.48	-36.96	0	-1070.06	1.8	-668.75	1.8	-245.66	2.12	-264.45
157	158	73.80	-1696.97	91.57	-156.69	0	-1226.13	1.8	-502.69	1.8	-231.69	2.12	-239.75
158	158	73.80	-2523.70	91.56	240.96	0	-1095.95	1.8	-873.25	1.8	-553.52	2.12	-638.90
158	159	75.20	-2523.70	103.63	104.33	0	-1278.91	1.8	-667.92	1.8	-539.55	2.12	-614.20
159	159	75.20	-2219.11	103.63	293.78	0	-733.83	1.8	-864.41	1.8	-539.55	2.12	-614.20
159	160	76.60	-2215.29	116.19	139.70	0	-943.03	1.8	-618.40	1.8	-524.43	2.12	-588.25
160	160	76.60	-2215.34	116.22	139.62	0	-943.13	1.8	-618.39	1.8	-524.43	2.12	-588.23
160	161	78.00	-2215.34	135.30	-36.43	0	-1188.37	1.8	-322.85	1.8	-510.29	2.12	-563.22
161	1161	78.00	-2172.15	-128.68	-7.67	0	-1107.86	1.8	-355.07	1.8	-510.36	2.12	-563.29
161	162	79.10	-2172.15	-113.69	125.64	0	-929.48	1.8	-554.99	1.8	-524.04	2.12	-587.48
162	162	79.10	-2172.53	-113.70	125.64	0	-929.60	1.8	-555.11	1.8	-524.14	2.12	-587.58
162	163	80.20	-2172.53	-104.21	245.51	0	-772.60	1.8	-723.78	1.8	-537.82	2.12	-611.77
163	163	80.20	-2477.65	-104.21	53.04	0	-1322.67	1.8	-520.39	1.8	-537.97	2.12	-611.93
163	164	81.30	-2477.65	-94.71	162.44	0	-1182.33	1.8	-664.74	1.8	-551.66	2.12	-636.12
164	164	81.30	-2478.35	-94.70	162.48	0	-1182.50	1.8	-664.97	1.8	-551.86	2.12	-636.33
164	165	82.40	-2478.35	-85.21	261.44	0	-1058.75	1.8	-785.07	1.8	-565.54	2.12	-660.52
165	165	82.40	-1870.06	-85.16	-269.27	0	-1575.00	1.8	-279.51	1.8	-243.96	2.12	-261.64
165	166	83.50	-1870.06	-75.67	-180.81	0	-1467.93	1.8	-375.32	1.8	-257.62	2.12	-285.81
166	166	83.50	-1871.02	-75.59	-180.72	0	-1483.57	1.8	-360.58	1.8	-244.82	2.12	-268.31
166	167	84.60	-1871.02	-66.09	-102.78	0	-1398.91	1.8	-426.56	1.8	-253.60	2.12	-285.82
167	167	84.60	-1016.26	-57.27	-500.44	0	-1595.54	1.8	351.21	1.8	0.00	2.12	0.00
167	168	85.70	-1019.75	-47.79	-433.57	0	-1495.40	1.8	192.68	1.8	0.00	2.12	0.00
168	168	85.70	-1261.85	-55.51	-564.54	0	-1889.65	1.8	285.62	1.8	0.00	2.12	0.00
168	169	86.80	-1261.85	-46.00	-508.72	0	-1804.60	1.8	155.61	1.8	0.00	2.12	0.00
169	169	86.80	-1261.85	-46.00	-508.72	0	-1804.60	1.8	155.61	1.8	0.00	2.12	0.00
169	170	87.90	-1261.85	-36.52	-463.33	0	-1735.43	1.8	49.86	1.8	0.00	2.12	0.00
170	170	87.90	-1261.85	-36.52	-463.33	0	-1735.43	1.8	49.86	1.8	0.00	2.12	0.00
170	171	89.00	-1261.85	-27.02	-428.38	0	-1682.18	1.8	-31.54	1.8	0.00	2.12	0.00

Combi_to.xls

Programa DINTEL PACADAR S.A.
CONST1.F5.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F5.T0.MZ-
Construcción sin gradiente en fase constructiva 5

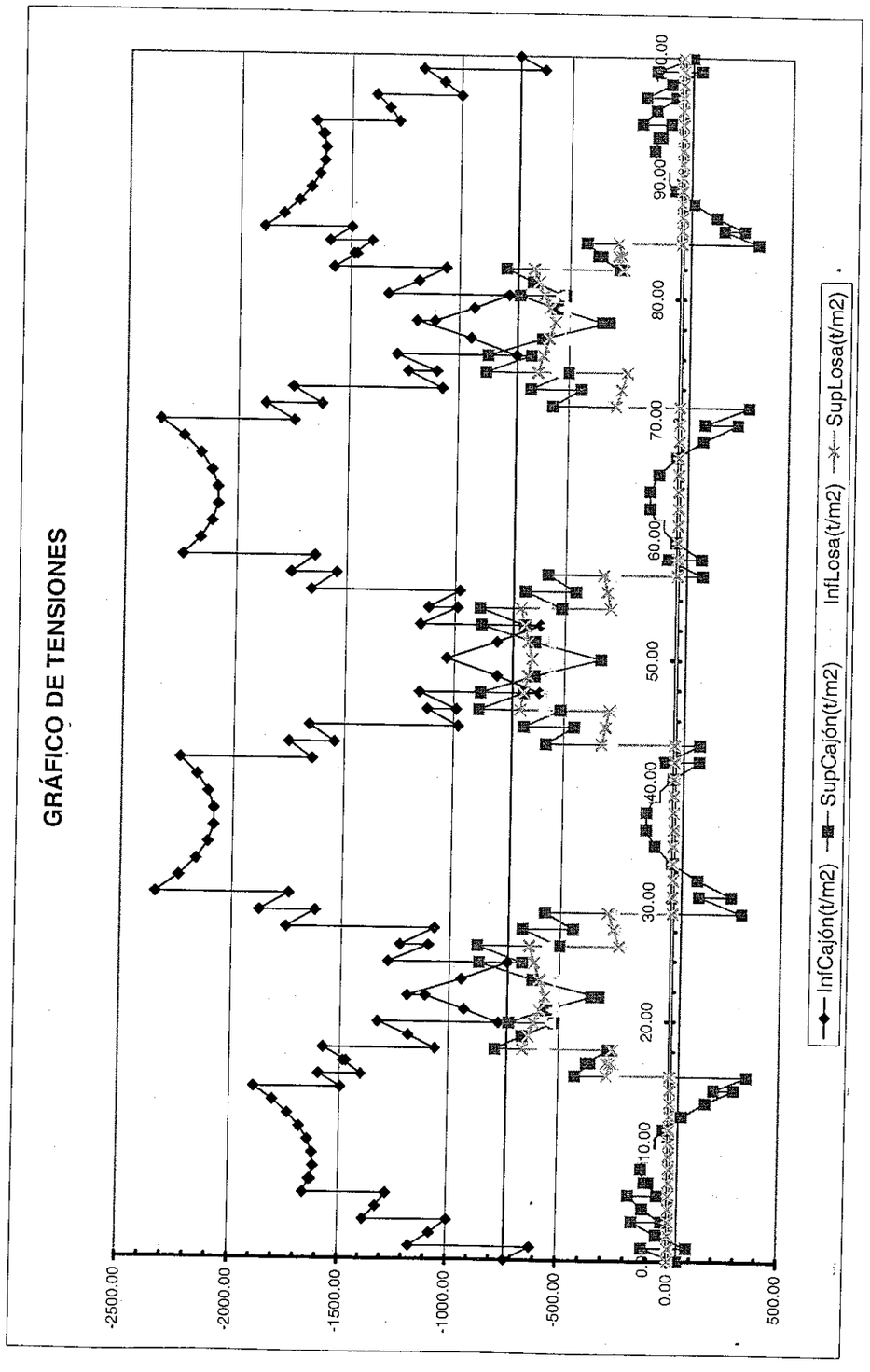
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	-27.02	-428.38	0	-1682.18	1.8	-31.54	1.8	0.00	2.12	0.00
171	172	90.10	-1261.85	-17.53	-403.89	0	-1644.86	1.8	-88.59	1.8	0.00	2.12	0.00
172	172	90.10	-1261.85	-17.53	-403.89	0	-1644.86	1.8	-88.59	1.8	0.00	2.12	0.00
172	173	91.20	-1261.85	-8.04	-389.82	0	-1623.43	1.8	-121.36	1.8	0.00	2.12	0.00
173	173	91.20	-1261.85	-8.04	-389.82	0	-1623.43	1.8	-121.36	1.8	0.00	2.12	0.00
173	174	92.30	-1261.85	1.46	-386.20	0	-1617.90	1.8	-129.80	1.8	0.00	2.12	0.00
174	174	92.30	-1261.85	1.46	-386.20	0	-1617.90	1.8	-129.80	1.8	0.00	2.12	0.00
174	175	93.40	-1261.85	10.95	-393.03	0	-1628.30	1.8	-113.90	1.8	0.00	2.12	0.00
175	175	93.40	-1261.85	10.95	-393.03	0	-1634.92	1.8	-96.50	1.8	0.00	2.12	0.00
175	176	94.50	-1261.85	20.44	-410.30	0	-1662.40	1.8	-56.36	1.8	0.00	2.12	0.00
176	176	94.50	-1044.29	20.44	-279.33	0	-1279.99	1.8	-186.59	1.8	0.00	2.12	0.00
176	177	95.60	-1044.29	29.94	-307.04	0	-1324.06	1.8	-122.21	1.8	0.00	2.12	0.00
177	177	95.60	-1044.29	29.94	-307.04	0	-1324.06	1.8	-122.21	1.8	0.00	2.12	0.00
177	178	96.70	-1044.29	39.42	-345.20	0	-1384.75	1.8	-33.54	1.8	0.00	2.12	0.00
178	178	96.70	-826.73	39.42	-212.05	0	-998.86	1.8	-168.85	1.8	0.00	2.12	0.00
178	179	97.80	-826.73	48.93	-260.64	0	-1076.15	1.8	-55.93	1.8	0.00	2.12	0.00
179	179	97.80	-826.73	48.93	-260.64	0	-1076.15	1.8	-55.93	1.8	0.00	2.12	0.00
179	180	98.90	-826.73	58.41	-319.68	0	-1170.06	1.8	81.25	1.8	0.00	2.12	0.00
180	180	98.90	-522.14	58.41	-127.18	0	-620.13	1.8	-122.31	1.8	0.00	2.12	0.00
180	181	100.00	-522.14	70.84	-197.72	0	-732.33	1.8	41.59	1.8	0.00	2.12	0.00

Programa DINTEL PACADAR S.A.
CONST1.F5.T0.MZ-

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-127.46	-178.92	0	-662.61	1.8	37.64	1.8	0.01	2.12	0.01
1	2	1.10	-476.85	-136.15	-16.51	0	-473.77	1.8	-150.18	1.8	-15.24	2.12	-30.02
2	2	1.10	-752.42	-135.76	-190.80	0	-971.44	1.8	34.02	1.8	-15.21	2.12	-29.98
2	3	2.20	-752.42	-114.62	-53.09	0	-808.74	1.8	-121.00	1.8	-28.24	2.12	-55.64
3	3	2.20	-752.42	-114.29	-53.22	0	-808.85	1.8	-120.98	1.8	-28.21	2.12	-55.60
3	4	3.30	-752.42	-93.12	60.84	0	-674.16	1.8	-249.16	1.8	-39.02	2.12	-76.88
4	4	3.30	-949.26	-92.84	-59.74	0	-1023.39	1.8	-126.72	1.8	-39.00	2.12	-76.84
4	5	4.40	-949.26	-71.69	30.73	0	-916.68	1.8	-228.05	1.8	-47.59	2.12	-93.78
5	5	4.40	-949.26	-71.45	30.64	0	-916.76	1.8	-228.04	1.8	-47.58	2.12	-93.75
5	6	5.50	-949.26	-50.30	97.60	0	-837.93	1.8	-302.60	1.8	-53.97	2.12	-106.35
6	6	5.50	-1146.10	-50.09	-20.97	0	-1183.99	1.8	-184.76	1.8	-53.96	2.12	-106.32
6	7	6.60	-1146.10	-28.94	22.51	0	-1133.00	1.8	-232.59	1.8	-58.16	2.12	-114.60
7	7	6.60	-1146.10	-28.77	22.46	0	-1144.90	1.8	-249.13	1.8	-58.63	2.12	-112.74
7	8	7.70	-1146.10	-7.62	42.47	0	-1122.85	1.8	-270.19	1.8	-60.66	2.12	-116.64
8	8	7.70	-1146.10	-7.45	42.43	0	-1122.88	1.8	-270.19	1.8	-60.65	2.12	-116.63
8	9	8.80	-1146.10	13.71	38.98	0	-1127.41	1.8	-264.37	1.8	-60.48	2.12	-116.29
9	9	8.80	-1146.10	13.85	38.98	0	-1127.41	1.8	-264.37	1.8	-60.48	2.12	-116.29
9	10	9.90	-1146.10	35.00	12.10	0	-1158.46	1.8	-231.70	1.8	-58.10	2.12	-111.71
10	10	9.90	-1146.10	35.16	12.11	0	-1158.45	1.8	-231.70	1.8	-58.10	2.12	-111.72
10	11	11.00	-1146.10	56.30	-38.19	0	-1216.03	1.8	-172.20	1.8	-53.52	2.12	-102.91
11	11	11.00	-1146.10	56.46	-38.16	0	-1216.00	1.8	-172.21	1.8	-53.53	2.12	-102.92
11	12	12.10	-1146.10	77.62	-111.91	0	-1300.13	1.8	-85.83	1.8	-46.74	2.12	-89.87
12	12	12.10	-1146.10	77.80	-111.86	0	-1300.09	1.8	-85.84	1.8	-46.75	2.12	-89.89
12	13	13.20	-1146.10	98.94	-209.09	0	-1410.82	1.8	27.45	1.8	-37.76	2.12	-72.60
13	13	13.20	-1146.10	99.15	-209.03	0	-1410.76	1.8	27.44	1.8	-37.77	2.12	-72.62
13	14	14.30	-1146.10	120.33	-329.72	0	-1548.02	1.8	167.50	1.8	-26.56	2.12	-51.08
14	14	14.30	-924.56	115.58	-211.15	0	-1180.61	1.8	85.81	1.8	-26.36	2.12	-51.94
14	15	15.40	-917.39	134.26	-357.42	0	-1346.43	1.8	263.22	1.8	-13.05	2.12	-25.71
15	15	15.40	-1858.58	143.15	82.19	0	-1150.44	1.8	-514.94	1.8	-298.90	2.12	-353.01
15	16	16.50	-1858.58	132.17	-81.82	0	-1309.25	1.8	-432.83	1.8	-276.10	2.12	-307.54
16	16	16.50	-1858.58	132.33	-81.78	0	-1288.56	1.8	-452.99	1.8	-293.61	2.12	-331.36
16	17	17.60	-1858.58	149.32	-237.05	0	-1460.54	1.8	-336.92	1.8	-263.13	2.12	-277.46
17	17	17.60	-2575.51	149.51	323.35	0	-966.86	1.8	-869.82	1.8	-618.86	2.12	-718.65
17	18	18.70	-2575.51	166.50	149.55	0	-1163.04	1.8	-727.90	1.8	-586.24	2.12	-660.97
18	18	18.70	-2575.50	166.69	149.59	0	-1163.00	1.8	-727.91	1.8	-586.24	2.12	-660.99
18	19	19.80	-2575.50	183.69	-43.12	0	-1383.98	1.8	-559.28	1.8	-551.48	2.12	-599.51
19	19	19.80	-2299.92	183.91	131.07	0	-886.40	1.8	-743.47	1.8	-551.48	2.12	-599.52
19	20	20.90	-2299.92	200.90	-80.59	0	-1132.24	1.8	-548.05	1.8	-514.57	2.12	-534.25
20	20	20.90	-2299.92	201.13	-80.57	0	-1132.22	1.8	-548.05	1.8	-514.57	2.12	-534.26
20	21	22.00	-2299.92	223.62	-314.19	0	-1407.68	1.8	-318.89	1.8	-475.51	2.12	-465.18
21	1021	22.00	-2339.29	-230.48	-340.26	0	-1480.65	1.8	-289.82	1.8	-475.50	2.12	-465.17
21	22	23.40	-2339.29	-201.86	-37.62	0	-1112.90	1.8	-622.25	1.8	-521.68	2.12	-546.83
22	22	23.40	-2339.29	-201.58	-37.66	0	-1112.94	1.8	-622.24	1.8	-521.67	2.12	-546.81
22	23	24.80	-2339.29	-179.93	229.40	0	-793.20	1.8	-900.00	1.8	-564.37	2.12	-622.30
23	23	24.80	-2614.86	-179.66	57.94	0	-1286.42	1.8	-722.21	1.8	-564.35	2.12	-622.28
23	24	26.20	-2614.86	-158.04	294.32	0	-1006.93	1.8	-956.60	1.8	-603.57	2.12	-691.62
24	24	26.20	-1701.11	-157.81	-145.26	0	-1150.88	1.8	-547.02	1.8	-247.84	2.12	-250.42
24	25	27.60	-1701.11	-136.17	60.54	0	-911.50	1.8	-738.16	1.8	-283.59	2.12	-313.64
25	25	27.60	-2055.42	-135.98	-149.28	0	-1528.73	1.8	-534.28	1.8	-283.57	2.12	-313.61
25	26	29.00	-2055.42	-140.83	64.90	0	-1291.79	1.8	-693.46	1.8	-325.73	2.12	-388.15
26	26	29.00	-1122.96	-135.73	-374.75	0	-1558.23	1.8	205.12	1.8	-18.26	2.12	-35.98
26	27	30.40	-1129.71	-110.68	-197.36	0	-1352.31	1.8	-15.47	1.8	-33.84	2.12	-66.68
27	27	30.40	-1460.38	-112.55	-377.63	0	-1908.78	1.8	117.60	1.8	-34.10	2.12	-65.57
27	28	31.80	-1460.38	-85.62	-238.93	0	-1747.93	1.8	-52.79	1.8	-46.23	2.12	-88.89
28	28	31.80	-1460.38	-85.43	-239.02	0	-1748.01	1.8	-52.77	1.8	-46.21	2.12	-88.86
28	29	33.20	-1460.38	-58.51	-138.25	0	-1630.10	1.8	-179.73	1.8	-54.77	2.12	-105.32
29	29	33.20	-1460.38	-58.36	-138.31	0	-1630.15	1.8	-179.72	1.8	-54.76	2.12	-105.30
29	30	34.60	-1460.38	-31.43	-75.46	0	-1555.21	1.8	-263.14	1.8	-59.76	2.12	-114.92
30	30	34.60	-1460.38	-31.29	-75.50	0	-1555.24	1.8	-263.14	1.8	-59.76	2.12	-114.90
30	31	36.00	-1460.38	-4.37	-50.53	0	-1523.22	1.8	-303.08	1.8	-61.21	2.12	-117.69
31	31	36.00	-1460.38	-4.24	-50.52	0	-1523.21	1.8	-303.08	1.8	-61.21	2.12	-117.69
31	32	37.40	-1460.38	22.68	-63.42	0	-1534.10	1.8	-299.54	1.8	-59.10	2.12	-113.64
32	32	37.40	-1460.38	22.81	-63.38	0	-1534.07	1.8	-299.55	1.8	-59.11	2.12	-113.65
32	33	38.80	-1460.38	49.74	-114.16	0	-1587.88	1.8	-252.50	1.8	-53.45	2.12	-102.78
33	33	38.80	-1460.38	49.91	-114.09	0	-1587.83	1.8	-252.51	1.8	-53.46	2.12	-102.80
33	34	40.20	-1460.38	76.82	-202.81	0	-1684.62	1.8	-161.95	1.8	-44.24	2.12	-85.07
34	34	40.20	-1460.38	77.02	-202.72	0	-1684.55	1.8	-161.97	1.8	-44.25	2.12	-85.09
34	35	41.60	-1460.38	103.95	-329.38	0	-1824.31	1.8	-27.91	1.8	-31.47	2.12	-60.51
35	35	41.60	-1135.74	103.64	-149.13	0	-1273.92	1.8	-165.96	1.8	-31.23	2.12	-61.53
35	36	43.00	-1128.92	128.82	-315.60	0	-1460.68	1.8	20.92	1.8	-14.99	2.12	-29.54
36	36	43.00	-2055.42	132.40	124.06	0	-1239.65	1.8	-694.02	1.8	-342.78	2.12	-418.29
36	37	44.40	-2055.42	126.56	-70.05	0	-1458.20	1.8	-537.34	1.8	-306.12	2.12	-353.47
37	37	44.40	-1701.11	126.78	139.77	0	-840.96	1.8	-741.23	1.8	-306.13	2.12	-353.50
37	38	45.80	-1701.11	148.41	-52.84	0	-1068.59	1.8	-550.60	1.8	-274.14	2.12	-296.92
38	38	45.80	-2614.86	148.65	386.74	0	-924.64	1.8	-960.18	1.8	-629.87	2.12	-738.12

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	170.27	163.50	0	-1192.44	1.8	-726.29	1.8	-594.39	2.12	-675.40
39	39	47.20	-2339.29	170.54	334.97	0	-699.20	1.8	-904.08	1.8	-594.41	2.12	-675.43
39	40	48.60	-2345.74	191.68	81.67	0	-1008.63	1.8	-628.99	1.8	-557.34	2.12	-608.56
40	40	48.60	-2345.92	191.96	81.76	0	-1008.60	1.8	-629.07	1.8	-557.41	2.12	-608.64
40	41	50.00	-2345.92	220.59	-207.02	0	-1363.96	1.8	-297.34	1.8	-515.15	2.12	-533.92
41	1041	50.00	-2345.70	-220.68	-207.02	0	-1363.89	1.8	-297.28	1.8	-515.10	2.12	-533.87
41	42	51.40	-2345.70	-192.04	81.90	0	-1008.41	1.8	-629.04	1.8	-557.39	2.12	-608.64
42	42	51.40	-2345.10	-191.76	81.81	0	-1008.30	1.8	-628.83	1.8	-557.21	2.12	-608.45
42	43	52.80	-2345.10	-170.12	335.13	0	-700.85	1.8	-905.92	1.8	-596.01	2.12	-677.05
43	43	52.80	-2619.68	-169.91	163.54	0	-1193.88	1.8	-727.78	1.8	-595.69	2.12	-676.70
43	44	54.20	-2614.86	-148.65	386.73	0	-924.65	1.8	-960.18	1.8	-629.87	2.12	-738.12
44	44	54.20	-1701.11	-148.41	-52.85	0	-1068.60	1.8	-550.60	1.8	-274.13	2.12	-296.92
44	45	55.60	-1701.11	-126.78	139.78	0	-840.95	1.8	-741.23	1.8	-306.14	2.12	-353.51
45	45	55.60	-2055.42	-126.56	-70.05	0	-1458.20	1.8	-537.34	1.8	-306.12	2.12	-353.47
45	46	57.00	-2055.42	-132.40	124.07	0	-1239.64	1.8	-694.02	1.8	-342.78	2.12	-418.30
46	46	57.00	-1128.92	-128.83	-315.58	0	-1460.66	1.8	20.89	1.8	-14.99	2.12	-29.54
46	47	58.40	-1133.95	-102.74	-150.01	0	-1273.81	1.8	-162.42	1.8	-31.23	2.12	-61.54
47	47	58.40	-1458.36	-104.00	-330.27	0	-1824.03	1.8	-24.18	1.8	-31.47	2.12	-60.51
47	48	59.80	-1458.36	-77.08	-203.52	0	-1684.13	1.8	-158.43	1.8	-44.26	2.12	-85.10
48	48	59.80	-1458.36	-76.88	-203.61	0	-1684.21	1.8	-158.41	1.8	-44.24	2.12	-85.07
48	49	61.20	-1458.36	-49.97	-114.84	0	-1587.32	1.8	-249.13	1.8	-53.46	2.12	-102.80
49	49	61.20	-1458.36	-49.80	-114.90	0	-1587.38	1.8	-249.12	1.8	-53.45	2.12	-102.78
49	50	62.60	-1458.36	-22.87	-64.03	0	-1533.42	1.8	-296.38	1.8	-59.11	2.12	-113.66
50	50	62.60	-1458.36	-22.73	-64.07	0	-1533.45	1.8	-296.37	1.8	-59.10	2.12	-113.65
50	51	64.00	-1456.62	4.18	-51.08	0	-1521.00	1.8	-298.70	1.8	-61.21	2.12	-117.69
51	51	64.00	-1456.62	4.29	-51.08	0	-1521.00	1.8	-298.70	1.8	-61.21	2.12	-117.69
51	52	65.40	-1456.62	31.21	-75.94	0	-1552.85	1.8	-259.01	1.8	-59.76	2.12	-114.91
52	52	65.40	-1456.62	31.35	-75.91	0	-1552.83	1.8	-259.02	1.8	-59.76	2.12	-114.92
52	53	66.80	-1456.62	58.28	-138.64	0	-1627.59	1.8	-175.86	1.8	-54.76	2.12	-105.30
53	53	66.80	-1456.62	58.44	-138.58	0	-1627.54	1.8	-175.87	1.8	-54.77	2.12	-105.32
53	54	68.20	-1456.62	85.35	-239.23	0	-1745.27	1.8	-49.19	1.8	-46.21	2.12	-88.86
54	54	68.20	-1456.62	85.54	-239.14	0	-1745.19	1.8	-49.21	1.8	-46.23	2.12	-88.89
54	55	69.60	-1456.62	112.47	-377.73	0	-1905.87	1.8	120.92	1.8	-34.10	2.12	-65.57
55	55	69.60	-1126.45	108.82	-197.46	0	-1349.81	1.8	-12.55	1.8	-33.84	2.12	-66.68
55	56	71.00	-1122.96	135.74	-374.74	0	-1558.24	1.8	205.14	1.8	-18.26	2.12	-35.99
56	56	71.00	-2055.42	140.83	64.90	0	-1291.79	1.8	-693.47	1.8	-325.73	2.12	-388.15
56	57	72.40	-2055.42	135.98	-149.27	0	-1528.72	1.8	-534.28	1.8	-283.58	2.12	-313.61
57	57	72.40	-1701.11	136.18	60.55	0	-911.49	1.8	-738.16	1.8	-283.59	2.12	-313.64
57	58	73.80	-1701.11	157.83	-145.26	0	-1150.88	1.8	-547.02	1.8	-247.84	2.12	-250.42
58	58	73.80	-2614.86	158.04	294.32	0	-1006.93	1.8	-956.60	1.8	-603.57	2.12	-691.62
58	59	75.20	-2614.86	179.66	57.92	0	-1286.44	1.8	-722.21	1.8	-564.35	2.12	-622.27
59	59	75.20	-2339.29	179.92	229.40	0	-793.20	1.8	-900.00	1.8	-564.37	2.12	-622.30
59	60	76.60	-2343.12	201.10	-37.15	0	-1113.63	1.8	-623.57	1.8	-522.83	2.12	-548.07
60	60	76.60	-2343.06	201.36	-37.03	0	-1113.49	1.8	-623.59	1.8	-522.84	2.12	-548.11
60	61	78.00	-2343.06	229.99	-338.98	0	-1480.58	1.8	-291.36	1.8	-476.84	2.12	-466.76
61	1061	78.00	-2303.37	-223.47	-312.87	0	-1407.47	1.8	-320.34	1.8	-476.76	2.12	-466.69
61	62	79.10	-2303.37	-200.98	-79.43	0	-1132.17	1.8	-549.45	1.8	-515.79	2.12	-535.69
62	62	79.10	-2302.99	-200.75	-79.45	0	-1132.08	1.8	-549.32	1.8	-515.68	2.12	-535.58
62	63	80.20	-2302.99	-183.76	132.06	0	-886.39	1.8	-744.70	1.8	-552.55	2.12	-600.78
63	63	80.20	-2578.03	-183.54	-42.16	0	-1383.83	1.8	-560.35	1.8	-552.40	2.12	-600.62
63	64	81.30	-2578.03	-166.54	150.37	0	-1163.03	1.8	-728.92	1.8	-587.12	2.12	-662.01
64	64	81.30	-2577.33	-166.35	150.26	0	-1162.92	1.8	-728.67	1.8	-586.90	2.12	-661.78
64	65	82.40	-2577.33	-149.36	323.91	0	-966.89	1.8	-870.54	1.8	-619.49	2.12	-719.39
65	65	82.40	-1859.54	-149.22	-236.21	0	-1459.77	1.8	-338.26	1.8	-263.51	2.12	-277.93
65	66	83.50	-1859.54	-132.23	-81.42	0	-1288.51	1.8	-453.39	1.8	-293.96	2.12	-331.77
66	66	83.50	-1858.58	-132.17	-81.57	0	-1309.04	1.8	-432.87	1.8	-276.14	2.12	-307.62
66	67	84.60	-1858.58	-143.15	82.43	0	-1150.24	1.8	-514.99	1.8	-298.94	2.12	-353.09
67	67	84.60	-917.40	-134.24	-357.18	0	-1346.08	1.8	262.66	1.8	-13.05	2.12	-25.71
67	68	85.70	-920.89	-113.09	-212.26	0	-1179.31	1.8	91.43	1.8	-26.36	2.12	-51.94
68	68	85.70	-1141.67	-120.42	-330.84	0	-1546.11	1.8	173.73	1.8	-26.56	2.12	-51.08
68	69	86.80	-1141.67	-99.24	-210.05	0	-1408.71	1.8	33.44	1.8	-37.77	2.12	-72.62
69	69	86.80	-1141.67	-99.03	-210.12	0	-1408.76	1.8	33.46	1.8	-37.76	2.12	-72.60
69	70	87.90	-1141.67	-77.89	-112.82	0	-1297.94	1.8	-79.99	1.8	-46.75	2.12	-89.89
70	70	87.90	-1141.67	-77.71	-112.87	0	-1297.98	1.8	-79.98	1.8	-46.74	2.12	-89.87
70	71	89.00	-1141.67	-56.55	-39.03	0	-1213.72	1.8	-166.56	1.8	-53.53	2.12	-102.92
71	71	89.00	-1141.67	-56.39	-39.05	0	-1213.74	1.8	-166.56	1.8	-53.52	2.12	-102.91
71	72	90.10	-1141.67	-35.24	11.35	0	-1156.01	1.8	-226.28	1.8	-58.10	2.12	-111.72
72	72	90.10	-1141.67	-35.09	11.33	0	-1156.02	1.8	-226.28	1.8	-58.10	2.12	-111.72
72	73	91.20	-1141.67	-13.94	38.29	0	-1124.84	1.8	-259.15	1.8	-60.48	2.12	-116.29
73	73	91.20	-1141.67	-13.80	38.30	0	-1124.83	1.8	-259.15	1.8	-60.48	2.12	-116.29
73	74	92.30	-1141.67	7.36	41.84	0	-1120.18	1.8	-265.17	1.8	-60.66	2.12	-116.63
74	74	92.30	-1141.67	7.53	41.87	0	-1120.15	1.8	-265.17	1.8	-60.66	2.12	-116.64
74	75	93.40	-1141.67	28.68	21.95	0	-1142.06	1.8	-244.31	1.8	-58.63	2.12	-112.74
75	75	93.40	-1141.67	28.85	22.00	0	-1130.27	1.8	-227.84	1.8	-58.16	2.12	-114.60
75	76	94.50	-1141.67	50.00	-21.40	0	-1181.12	1.8	-180.24	1.8	-53.96	2.12	-106.32

Combi_to.xls

Programa DINTEL PACADAR S.A.
PERM1.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	50.21	97.17	0	-835.05	1.8	-298.08	1.8	-53.97	2.12	-106.35
76	77	95.60	-944.83	71.37	30.31	0	-913.74	1.8	-223.71	1.8	-47.58	2.12	-93.75
77	77	95.60	-944.83	71.60	30.41	0	-913.65	1.8	-223.73	1.8	-47.59	2.12	-93.78
77	78	96.70	-944.83	92.75	-60.00	0	-1020.28	1.8	-122.55	1.8	-39.00	2.12	-76.84
78	78	96.70	-747.99	93.04	60.58	0	-671.03	1.8	-244.99	1.8	-39.02	2.12	-76.88
78	79	97.80	-747.99	114.20	-53.40	0	-805.59	1.8	-117.01	1.8	-28.21	2.12	-55.60
79	79	97.80	-747.99	114.53	-53.27	0	-805.48	1.8	-117.03	1.8	-28.24	2.12	-55.64
79	80	98.90	-747.99	135.67	-190.89	0	-968.03	1.8	37.76	1.8	-15.21	2.12	-29.98
80	80	98.90	-472.42	136.06	-16.59	0	-470.37	1.8	-146.44	1.8	-15.24	2.12	-30.02
80	81	100.00	-472.42	127.45	-178.92	0	-662.61	1.8	37.64	1.8	0.01	2.12	0.01
101	101	0.00	-472.42	-146.68	-178.82	0	-662.52	1.8	37.62	1.8	-0.01	2.12	-0.02
101	102	1.10	-476.85	-124.89	-29.42	0	-484.92	1.8	-147.68	1.8	-13.07	2.12	-25.75
102	102	1.10	-752.42	-125.28	-203.44	0	-982.35	1.8	36.46	1.8	-13.09	2.12	-25.79
102	103	2.20	-752.42	-105.34	-76.61	0	-829.04	1.8	-116.45	1.8	-24.28	2.12	-47.85
103	103	2.20	-752.42	-105.66	-76.48	0	-828.92	1.8	-116.47	1.8	-24.30	2.12	-47.89
103	104	3.30	-752.42	-85.70	28.75	0	-701.86	1.8	-242.95	1.8	-33.62	2.12	-66.25
104	104	3.30	-949.26	-85.96	-91.60	0	-1050.90	1.8	-120.55	1.8	-33.64	2.12	-66.29
104	105	4.40	-949.26	-66.03	-8.01	0	-950.11	1.8	-220.58	1.8	-41.08	2.12	-80.94
105	105	4.40	-949.26	-66.27	-7.92	0	-950.03	1.8	-220.59	1.8	-41.09	2.12	-80.97
105	106	5.50	-949.26	-46.32	53.99	0	-875.56	1.8	-294.18	1.8	-46.64	2.12	-91.90
106	106	5.50	-1146.10	-46.51	-64.42	0	-1221.49	1.8	-176.37	1.8	-46.65	2.12	-91.93
106	107	6.60	-1146.10	-26.57	-24.21	0	-1173.33	1.8	-223.54	1.8	-50.30	2.12	-99.12
107	107	6.60	-1146.10	-26.74	-24.16	0	-1183.03	1.8	-240.03	1.8	-50.73	2.12	-97.54
107	108	7.70	-1146.10	-6.80	-5.72	0	-1162.27	1.8	-260.79	1.8	-52.49	2.12	-100.93
108	108	7.70	-1146.10	-6.96	-5.69	0	-1162.25	1.8	-260.79	1.8	-52.50	2.12	-100.94
108	109	8.80	-1146.10	12.99	-9.02	0	-1166.67	1.8	-255.00	1.8	-52.34	2.12	-100.64
109	109	8.80	-1146.10	12.85	-9.01	0	-1166.66	1.8	-255.00	1.8	-52.34	2.12	-100.65
109	110	9.90	-1146.10	32.79	-34.13	0	-1196.28	1.8	-222.68	1.8	-50.26	2.12	-96.64
110	110	9.90	-1146.10	32.65	-34.14	0	-1196.29	1.8	-222.67	1.8	-50.26	2.12	-96.64
110	111	11.00	-1146.10	52.59	-81.01	0	-1251.05	1.8	-163.84	1.8	-46.26	2.12	-88.95
111	111	11.00	-1146.10	52.43	-81.05	0	-1251.08	1.8	-163.84	1.8	-46.25	2.12	-88.94
111	112	12.10	-1146.10	72.39	-149.71	0	-1331.06	1.8	-78.45	1.8	-40.33	2.12	-77.55
112	112	12.10	-1146.10	72.21	-149.77	0	-1331.10	1.8	-78.44	1.8	-40.32	2.12	-77.54
112	113	13.20	-1146.10	92.14	-240.18	0	-1436.24	1.8	33.50	1.8	-32.49	2.12	-62.47
113	113	13.20	-1146.10	91.95	-240.24	0	-1436.29	1.8	33.51	1.8	-32.48	2.12	-62.45
113	114	14.30	-1146.10	111.91	-352.36	0	-1566.53	1.8	171.92	1.8	-22.73	2.12	-43.70
114	114	14.30	-924.56	106.73	-233.94	0	-1200.29	1.8	90.23	1.8	-22.53	2.12	-44.39
114	115	15.40	-917.39	124.20	-369.82	0	-1357.14	1.8	265.62	1.8	-10.96	2.12	-21.60
115	115	15.40	-1858.58	132.56	69.60	0	-1161.28	1.8	-512.58	1.8	-296.85	2.12	-348.92
115	116	16.50	-1858.58	125.82	-81.96	0	-1309.38	1.8	-432.80	1.8	-276.07	2.12	-307.49
116	116	16.50	-1858.58	125.65	-82.01	0	-1288.78	1.8	-452.93	1.8	-293.55	2.12	-331.25
116	117	17.60	-1858.58	142.00	-229.62	0	-1453.34	1.8	-339.09	1.8	-265.01	2.12	-280.79
117	117	17.60	-2575.50	141.82	330.71	0	-959.74	1.8	-871.96	1.8	-620.72	2.12	-721.94
117	118	18.70	-2575.50	158.16	165.72	0	-1147.39	1.8	-732.61	1.8	-590.33	2.12	-668.20
118	118	18.70	-2575.50	157.96	165.68	0	-1147.43	1.8	-732.60	1.8	-590.32	2.12	-668.18
118	119	19.80	-2575.50	174.31	-17.06	0	-1358.76	1.8	-566.88	1.8	-558.07	2.12	-611.17
119	119	19.80	-2299.92	174.10	157.06	0	-861.24	1.8	-751.04	1.8	-558.06	2.12	-611.15
119	120	20.90	-2299.92	190.44	-43.46	0	-1096.30	1.8	-558.87	1.8	-523.97	2.12	-550.87
120	120	20.90	-2299.92	190.21	-43.47	0	-1096.31	1.8	-558.86	1.8	-523.96	2.12	-550.86
120	121	22.00	-2299.92	212.06	-264.73	0	-1359.81	1.8	-333.31	1.8	-488.02	2.12	-487.31
121	1121	22.00	-2339.29	-219.16	-290.80	0	-1432.78	1.8	-304.24	1.8	-488.02	2.12	-487.31
121	122	23.40	-2339.29	-191.36	-3.44	0	-1079.82	1.8	-632.21	1.8	-530.34	2.12	-562.13
122	122	23.40	-2339.29	-191.63	-3.41	0	-1079.79	1.8	-632.22	1.8	-530.34	2.12	-562.14
122	123	24.80	-2339.29	-170.83	250.32	0	-772.95	1.8	-906.10	1.8	-569.66	2.12	-631.67
123	123	24.80	-2614.86	-171.08	78.99	0	-1266.05	1.8	-728.34	1.8	-569.68	2.12	-631.70
123	124	26.20	-2614.86	-150.29	303.93	0	-997.63	1.8	-959.40	1.8	-606.00	2.12	-695.92
124	124	26.20	-1701.11	-150.52	-135.52	0	-1141.45	1.8	-549.86	1.8	-250.30	2.12	-254.78
124	125	27.60	-1701.11	-129.69	60.64	0	-911.41	1.8	-738.19	1.8	-283.61	2.12	-313.68
125	125	27.60	-2055.42	-129.90	-149.04	0	-1528.51	1.8	-534.34	1.8	-283.63	2.12	-313.71
125	126	29.00	-2055.42	-131.07	50.61	0	-1305.62	1.8	-689.30	1.8	-322.11	2.12	-381.75
126	126	29.00	-1122.96	-126.57	-388.77	0	-1570.34	1.8	207.86	1.8	-15.90	2.12	-31.34
126	127	30.40	-1129.71	-103.05	-223.14	0	-1374.56	1.8	-10.48	1.8	-29.50	2.12	-58.14
127	127	30.40	-1460.38	-105.40	-403.17	0	-1929.68	1.8	122.58	1.8	-29.77	2.12	-57.24
127	128	31.80	-1460.38	-80.00	-273.42	0	-1776.14	1.8	-46.06	1.8	-40.38	2.12	-77.65
128	128	31.80	-1460.38	-80.19	-273.33	0	-1776.07	1.8	-46.08	1.8	-40.40	2.12	-77.68
128	129	33.20	-1460.38	-54.82	-178.80	0	-1663.26	1.8	-171.84	1.8	-47.90	2.12	-92.10
129	129	33.20	-1460.38	-54.97	-178.73	0	-1663.20	1.8	-171.85	1.8	-47.91	2.12	-92.12
129	130	34.60	-1460.38	-29.57	-119.57	0	-1591.29	1.8	-254.53	1.8	-52.29	2.12	-100.54
130	130	34.60	-1460.38	-29.72	-119.53	0	-1591.26	1.8	-254.54	1.8	-52.29	2.12	-100.55
130	131	36.00	-1460.38	-4.32	-95.71	0	-1560.16	1.8	-294.28	1.8	-53.55	2.12	-102.96
131	131	36.00	-1460.38	-4.45	-95.71	0	-1560.16	1.8	-294.28	1.8	-53.55	2.12	-102.96
131	132	37.40	-1460.38	20.94	-107.26	0	-1569.96	1.8	-290.96	1.8	-51.67	2.12	-99.36
132	132	37.40	-1460.38	20.80	-107.30	0	-1570.00	1.8	-290.95	1.8	-51.67	2.12	-99.34
132	133	38.80	-1460.38	46.20	-154.19	0	-1620.64	1.8	-244.67	1.8	-46.67	2.12	-89.73
133	133	38.80	-1460.38	46.03	-154.26	0	-1620.69	1.8	-244.65	1.8	-46.65	2.12	-89.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	71.42	-236.46	0	-1712.14	1.8	-155.39	1.8	-38.54	2.12	-74.10
134	134	40.20	-1460.38	71.22	-236.55	0	-1712.22	1.8	-155.37	1.8	-38.52	2.12	-74.07
134	135	41.60	-1460.38	96.61	-354.04	0	-1844.48	1.8	-23.10	1.8	-27.29	2.12	-52.47
135	135	41.60	-1135.74	95.80	-174.01	0	-1295.39	1.8	-161.15	1.8	-27.04	2.12	-53.29
135	136	43.00	-1128.92	119.45	-328.44	0	-1471.76	1.8	23.40	1.8	-12.83	2.12	-25.29
136	136	43.00	-2055.42	122.41	110.94	0	-1252.35	1.8	-690.20	1.8	-339.46	2.12	-412.42
136	137	44.40	-2055.42	120.35	-68.99	0	-1457.16	1.8	-537.65	1.8	-306.39	2.12	-353.95
137	137	44.40	-1701.11	120.15	140.68	0	-840.08	1.8	-741.49	1.8	-306.37	2.12	-353.91
137	138	45.80	-1701.11	140.96	-42.10	0	-1058.19	1.8	-553.73	1.8	-276.85	2.12	-301.73
138	138	45.80	-2614.86	140.73	397.35	0	-914.37	1.8	-963.27	1.8	-632.55	2.12	-742.87
138	139	47.20	-2614.86	161.53	185.78	0	-1170.87	1.8	-732.78	1.8	-600.03	2.12	-685.37
139	139	47.20	-2339.29	161.26	357.13	0	-677.76	1.8	-910.54	1.8	-600.02	2.12	-685.34
139	140	48.60	-2345.74	181.57	117.39	0	-974.07	1.8	-639.40	1.8	-566.38	2.12	-624.54
140	140	48.60	-2345.92	181.27	117.41	0	-974.10	1.8	-639.46	1.8	-566.43	2.12	-624.60
140	141	50.00	-2345.92	209.08	-155.81	0	-1314.40	1.8	-312.26	1.8	-528.11	2.12	-556.84
141	1141	50.00	-2345.71	-209.17	-155.81	0	-1314.33	1.8	-312.20	1.8	-528.06	2.12	-556.79
141	142	51.40	-2345.71	-181.35	117.54	0	-973.92	1.8	-639.43	1.8	-566.41	2.12	-624.60
142	142	51.40	-2345.10	-181.65	117.52	0	-973.74	1.8	-639.24	1.8	-566.24	2.12	-624.43
142	143	52.80	-2345.10	-160.84	357.29	0	-679.39	1.8	-912.38	1.8	-601.61	2.12	-686.97
143	143	52.80	-2619.68	-161.17	185.83	0	-1172.31	1.8	-734.28	1.8	-601.33	2.12	-686.68
143	144	54.20	-2614.86	-140.73	397.34	0	-914.38	1.8	-963.27	1.8	-632.55	2.12	-742.86
144	144	54.20	-1701.11	-140.97	-42.10	0	-1058.20	1.8	-553.73	1.8	-276.85	2.12	-301.73
144	145	55.60	-1701.11	-120.16	140.68	0	-840.07	1.8	-741.49	1.8	-306.37	2.12	-353.91
145	145	55.60	-2055.42	-120.35	-68.99	0	-1457.17	1.8	-537.65	1.8	-306.39	2.12	-353.95
145	146	57.00	-2055.42	-122.41	110.95	0	-1252.33	1.8	-690.20	1.8	-339.46	2.12	-412.43
146	146	57.00	-1128.92	-119.46	-328.42	0	-1471.75	1.8	23.40	1.8	-12.84	2.12	-25.29
146	147	58.40	-1133.95	-94.90	-174.88	0	-1295.27	1.8	-157.62	1.8	-27.05	2.12	-53.30
147	147	58.40	-1458.36	-96.67	-354.91	0	-1844.18	1.8	-19.40	1.8	-27.29	2.12	-52.48
147	148	59.80	-1458.36	-71.28	-237.36	0	-1711.82	1.8	-151.82	1.8	-38.52	2.12	-74.07
148	148	59.80	-1458.36	-71.47	-237.27	0	-1711.75	1.8	-151.84	1.8	-38.54	2.12	-74.10
148	149	61.20	-1458.36	-46.09	-154.98	0	-1620.16	1.8	-241.30	1.8	-46.66	2.12	-89.71
149	149	61.20	-1458.36	-46.26	-154.92	0	-1620.11	1.8	-241.31	1.8	-46.67	2.12	-89.73
149	150	62.60	-1458.36	-20.86	-107.93	0	-1569.33	1.8	-287.81	1.8	-51.67	2.12	-99.35
150	150	62.60	-1458.36	-21.00	-107.89	0	-1569.30	1.8	-287.81	1.8	-51.67	2.12	-99.36
150	151	64.00	-1456.62	4.37	-96.27	0	-1557.96	1.8	-289.88	1.8	-53.55	2.12	-102.96
151	151	64.00	-1456.62	4.24	-96.27	0	-1557.96	1.8	-289.88	1.8	-53.55	2.12	-102.96
151	152	65.40	-1456.62	29.64	-119.98	0	-1588.88	1.8	-250.42	1.8	-52.29	2.12	-100.55
152	152	65.40	-1456.62	29.49	-120.01	0	-1588.90	1.8	-250.41	1.8	-52.29	2.12	-100.54
152	153	66.80	-1456.62	54.88	-179.06	0	-1660.65	1.8	-167.99	1.8	-47.91	2.12	-92.12
153	153	66.80	-1456.62	54.74	-179.13	0	-1660.70	1.8	-167.98	1.8	-47.90	2.12	-92.10
153	154	68.20	-1456.62	80.11	-273.54	0	-1773.34	1.8	-42.47	1.8	-40.40	2.12	-77.68
154	154	68.20	-1456.62	79.92	-273.64	0	-1773.42	1.8	-42.46	1.8	-40.38	2.12	-77.65
154	155	69.60	-1456.62	105.32	-403.28	0	-1926.78	1.8	125.93	1.8	-29.77	2.12	-57.24
155	155	69.60	-1126.45	101.17	-223.25	0	-1372.08	1.8	-7.54	1.8	-29.51	2.12	-58.14
155	156	71.00	-1122.96	126.57	-388.77	0	-1570.35	1.8	207.88	1.8	-15.91	2.12	-31.34
156	156	71.00	-2055.42	131.07	50.62	0	-1305.61	1.8	-689.30	1.8	-322.11	2.12	-381.76
156	157	72.40	-2055.42	129.91	-149.02	0	-1528.49	1.8	-534.35	1.8	-283.64	2.12	-313.72
157	157	72.40	-1701.11	129.70	60.66	0	-911.39	1.8	-738.19	1.8	-283.62	2.12	-313.69
157	158	73.80	-1701.11	150.53	-135.52	0	-1141.45	1.8	-549.86	1.8	-250.30	2.12	-254.78
158	158	73.80	-2614.86	150.29	303.92	0	-997.63	1.8	-959.40	1.8	-606.00	2.12	-695.92
158	159	75.20	-2614.86	171.08	78.98	0	-1266.06	1.8	-728.34	1.8	-569.68	2.12	-631.69
159	159	75.20	-2339.29	170.82	250.33	0	-772.94	1.8	-906.10	1.8	-569.66	2.12	-631.67
159	160	76.60	-2343.12	191.17	-2.90	0	-1080.47	1.8	-633.55	1.8	-531.50	2.12	-563.40
160	160	76.60	-2343.06	190.86	-2.85	0	-1080.42	1.8	-633.55	1.8	-531.49	2.12	-563.40
160	161	78.00	-2343.06	218.67	-289.50	0	-1432.69	1.8	-305.78	1.8	-489.36	2.12	-488.90
161	1161	78.00	-2303.37	-211.91	-263.41	0	-1359.60	1.8	-334.76	1.8	-489.28	2.12	-488.83
161	162	79.10	-2303.37	-190.07	-42.32	0	-1096.26	1.8	-560.26	1.8	-525.18	2.12	-552.30
162	162	79.10	-2302.99	-190.28	-42.31	0	-1096.13	1.8	-560.15	1.8	-525.08	2.12	-552.20
162	163	80.20	-2302.99	-173.94	158.04	0	-861.24	1.8	-752.28	1.8	-559.13	2.12	-612.41
163	163	80.20	-2578.03	-174.15	-16.11	0	-1358.62	1.8	-567.94	1.8	-558.99	2.12	-612.27
163	164	81.30	-2578.03	-157.80	166.45	0	-1147.47	1.8	-733.60	1.8	-591.19	2.12	-669.21
164	164	81.30	-2577.33	-158.01	166.43	0	-1147.27	1.8	-733.38	1.8	-591.00	2.12	-669.01
164	165	82.40	-2577.33	-141.67	331.27	0	-959.77	1.8	-872.68	1.8	-621.35	2.12	-722.68
165	165	82.40	-1859.54	-141.90	-228.75	0	-1452.56	1.8	-340.43	1.8	-265.39	2.12	-281.26
165	166	83.50	-1859.54	-125.55	-81.66	0	-1288.74	1.8	-453.32	1.8	-293.90	2.12	-331.67
166	166	83.50	-1858.58	-125.81	-81.72	0	-1309.16	1.8	-432.85	1.8	-276.11	2.12	-307.57
166	167	84.60	-1858.58	-132.55	69.84	0	-1161.08	1.8	-512.63	1.8	-296.89	2.12	-349.00
167	167	84.60	-917.40	-124.18	-369.59	0	-1356.78	1.8	265.06	1.8	-10.96	2.12	-21.60
167	168	85.70	-920.89	-104.25	-235.07	0	-1199.00	1.8	95.84	1.8	-22.52	2.12	-44.38
168	168	85.70	-1141.67	-112.00	-353.49	0	-1564.63	1.8	178.15	1.8	-22.72	2.12	-43.70
168	169	86.80	-1141.67	-92.04	-241.28	0	-1434.25	1.8	39.54	1.8	-32.48	2.12	-62.45
169	169	86.80	-1141.67	-92.23	-241.21	0	-1434.20	1.8	39.53	1.8	-32.49	2.12	-62.47
169	170	87.90	-1141.67	-72.30	-150.71	0	-1328.93	1.8	-72.61	1.8	-40.32	2.12	-77.54
170	170	87.90	-1141.67	-72.47	-150.66	0	-1328.89	1.8	-72.62	1.8	-40.33	2.12	-77.55
170	171	89.00	-1141.67	-52.52	-81.91	0	-1248.78	1.8	-158.21	1.8	-46.25	2.12	-88.94

Combi_to.xls

Programa DINTEL PACADAR S.A.
PERM1.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente

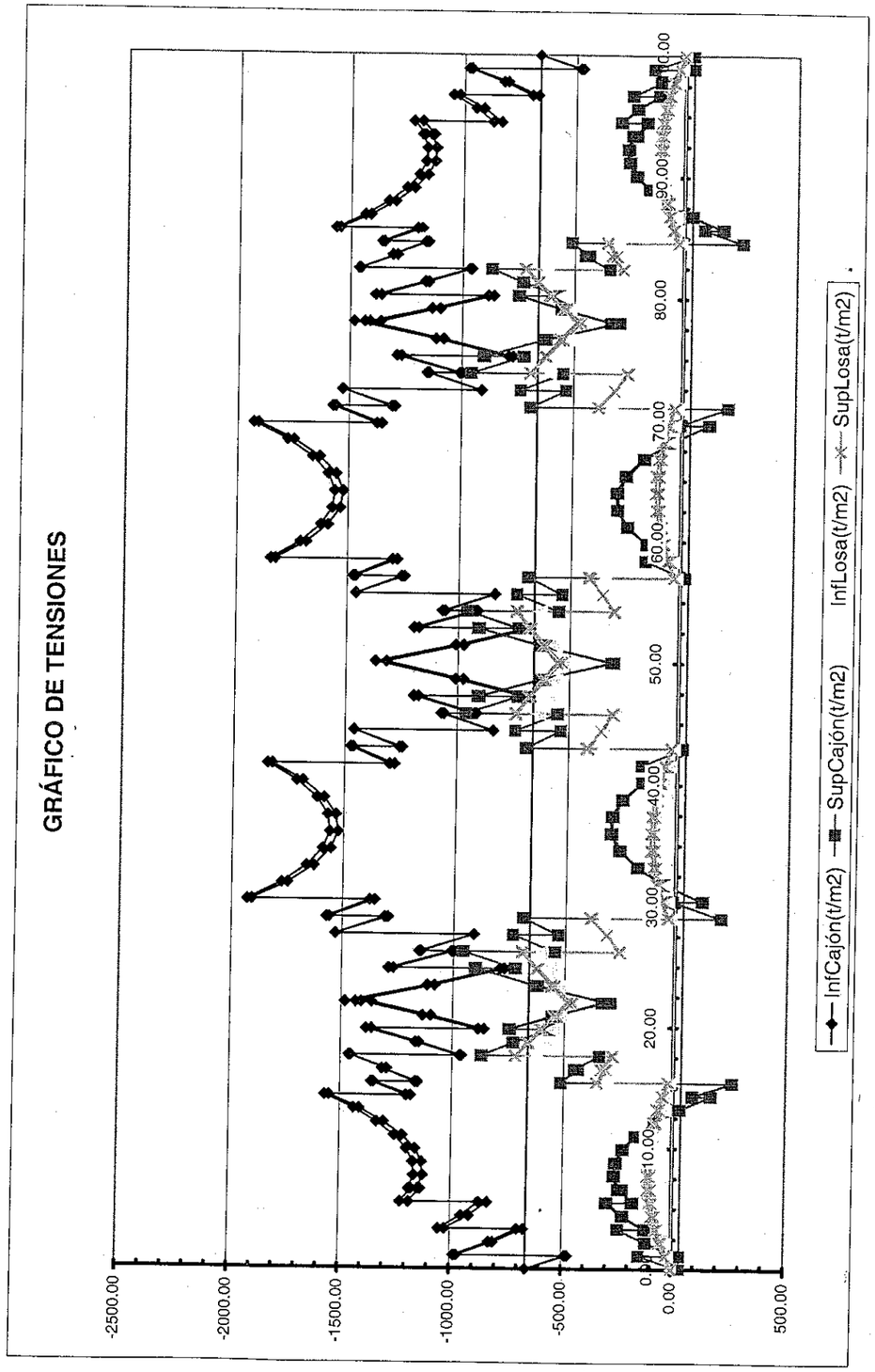
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	-52.68	-81.87	0	-1248.75	1.8	-158.22	1.8	-46.26	2.12	-88.95
171	172	90.10	-1141.67	-32.74	-34.92	0	-1193.86	1.8	-217.25	1.8	-50.26	2.12	-96.64
172	172	90.10	-1141.67	-32.88	-34.91	0	-1193.85	1.8	-217.25	1.8	-50.26	2.12	-96.64
172	173	91.20	-1141.67	-12.94	-9.71	0	-1164.10	1.8	-249.78	1.8	-52.34	2.12	-100.64
173	173	91.20	-1141.67	-13.09	-9.71	0	-1164.10	1.8	-249.78	1.8	-52.34	2.12	-100.64
173	174	92.30	-1141.67	6.87	-6.28	0	-1159.54	1.8	-255.77	1.8	-52.50	2.12	-100.94
174	174	92.30	-1141.67	6.71	-6.32	0	-1159.57	1.8	-255.77	1.8	-52.49	2.12	-100.93
174	175	93.40	-1141.67	26.65	-24.68	0	-1180.20	1.8	-235.21	1.8	-50.73	2.12	-97.54
175	175	93.40	-1141.67	26.48	-24.73	0	-1170.60	1.8	-218.80	1.8	-50.30	2.12	-99.12
175	176	94.50	-1141.67	46.42	-64.86	0	-1218.63	1.8	-171.82	1.8	-46.65	2.12	-91.93
176	176	94.50	-944.83	46.23	53.57	0	-872.69	1.8	-289.64	1.8	-46.64	2.12	-91.90
176	177	95.60	-944.83	66.18	-8.25	0	-947.03	1.8	-216.25	1.8	-41.09	2.12	-80.98
177	177	95.60	-944.83	65.95	-8.35	0	-947.12	1.8	-216.23	1.8	-41.08	2.12	-80.94
177	178	96.70	-944.83	85.89	-91.87	0	-1047.78	1.8	-116.38	1.8	-33.64	2.12	-66.29
178	178	96.70	-747.99	85.61	28.49	0	-698.74	1.8	-238.78	1.8	-33.62	2.12	-66.25
178	179	97.80	-747.99	105.57	-76.66	0	-825.67	1.8	-112.50	1.8	-24.30	2.12	-47.89
179	179	97.80	-747.99	105.25	-76.79	0	-825.78	1.8	-112.48	1.8	-24.28	2.12	-47.85
179	180	98.90	-747.99	125.19	-203.52	0	-978.94	1.8	40.21	1.8	-13.09	2.12	-25.79
180	180	98.90	-472.42	124.80	-29.49	0	-481.50	1.8	-143.94	1.8	-13.07	2.12	-25.75
180	181	100.00	-472.42	146.67	-178.82	0	-662.52	1.8	37.62	1.8	-0.01	2.12	-0.02

Programa DINTEL PACADAR S.A.
PERM1.T0.MZ+

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-159.13	-197.78	0	-732.38	1.8	41.60	1.8	0.01	2.12	0.02
1	2	1.10	-517.71	-107.45	-69.15	0	-566.56	1.8	-129.81	1.8	-9.77	2.12	-19.25
2	2	1.10	-822.30	-107.24	-261.72	0	-1116.55	1.8	73.76	1.8	-9.76	2.12	-19.23
2	3	2.20	-822.30	-90.26	-153.09	0	-979.90	1.8	-72.85	1.8	-18.11	2.12	-35.68
3	3	2.20	-822.30	-90.09	-153.16	0	-979.96	1.8	-72.84	1.8	-18.10	2.12	-35.66
3	4	3.30	-822.30	-73.08	-63.44	0	-867.22	1.8	-193.54	1.8	-25.03	2.12	-49.31
4	4	3.30	-1039.86	-72.92	-196.64	0	-1253.16	1.8	-58.23	1.8	-25.02	2.12	-49.30
4	5	4.40	-1039.86	-55.93	-125.79	0	-1164.33	1.8	-152.99	1.8	-30.53	2.12	-60.16
5	5	4.40	-1039.86	-55.81	-125.84	0	-1164.37	1.8	-152.98	1.8	-30.52	2.12	-60.15
5	6	5.50	-1039.86	-38.80	-73.82	0	-1099.37	1.8	-221.88	1.8	-34.63	2.12	-68.23
6	6	5.50	-1257.42	-38.69	-204.83	0	-1481.82	1.8	-91.65	1.8	-34.62	2.12	-68.22
6	7	6.60	-1257.42	-21.70	-171.59	0	-1440.62	1.8	-134.72	1.8	-37.32	2.12	-73.53
7	7	6.60	-1257.42	-21.61	-171.62	0	-1443.95	1.8	-152.39	1.8	-37.62	2.12	-72.34
7	8	7.70	-1257.42	-4.62	-157.19	0	-1427.39	1.8	-169.59	1.8	-38.92	2.12	-74.84
8	8	7.70	-1257.42	-4.53	-157.21	0	-1427.41	1.8	-169.59	1.8	-38.92	2.12	-74.83
8	9	8.80	-1257.42	12.47	-161.60	0	-1433.62	1.8	-160.81	1.8	-38.80	2.12	-74.61
9	9	8.80	-1257.42	12.55	-161.60	0	-1433.62	1.8	-160.81	1.8	-38.80	2.12	-74.61
9	10	9.90	-1257.42	29.54	-184.76	0	-1462.55	1.8	-126.09	1.8	-37.28	2.12	-71.68
10	10	9.90	-1257.42	29.62	-184.75	0	-1462.54	1.8	-126.09	1.8	-37.28	2.12	-71.68
10	11	11.00	-1257.42	46.62	-226.69	0	-1514.19	1.8	-65.45	1.8	-34.34	2.12	-66.02
11	11	11.00	-1257.42	46.70	-226.66	0	-1514.17	1.8	-65.45	1.8	-34.34	2.12	-66.03
11	12	12.10	-1257.42	63.70	-287.39	0	-1588.57	1.8	21.17	1.8	-29.98	2.12	-57.66
12	12	12.10	-1257.42	63.80	-287.36	0	-1588.55	1.8	21.16	1.8	-29.99	2.12	-57.66
12	13	13.20	-1257.42	80.78	-366.91	0	-1685.72	1.8	133.78	1.8	-24.22	2.12	-46.56
13	13	13.20	-1257.42	80.89	-366.87	0	-1685.69	1.8	133.77	1.8	-24.22	2.12	-46.58
13	14	14.30	-1257.42	97.91	-465.20	0	-1805.57	1.8	272.24	1.8	-17.03	2.12	-32.74
14	14	14.30	-1016.08	87.78	-334.19	0	-1407.36	1.8	178.84	1.8	-16.90	2.12	-33.29
14	15	15.40	-1016.27	107.22	-450.52	0	-1552.30	1.8	341.03	1.8	-8.35	2.12	-16.46
15	15	15.40	-1871.02	116.17	-52.81	0	-1355.86	1.8	-435.93	1.8	-261.74	2.12	-302.06
15	16	16.50	-1871.02	165.31	-195.04	0	-1495.91	1.8	-357.90	1.8	-242.49	2.12	-263.66
16	16	16.50	-1871.02	165.61	-194.96	0	-1481.92	1.8	-371.49	1.8	-254.30	2.12	-279.73
16	17	17.60	-1871.02	186.76	-389.17	0	-1691.61	1.8	-243.99	1.8	-213.98	2.12	-208.43
17	17	17.60	-2480.19	187.09	142.15	0	-1174.78	1.8	-750.88	1.8	-535.83	2.12	-607.62
17	18	18.70	-2480.19	208.24	-75.29	0	-1413.19	1.8	-596.24	1.8	-492.17	2.12	-530.41
18	18	18.70	-2480.18	208.61	-75.21	0	-1413.11	1.8	-596.26	1.8	-492.19	2.12	-530.44
18	19	19.80	-2480.18	229.77	-316.32	0	-1680.92	1.8	-413.54	1.8	-445.17	2.12	-447.31
19	19	19.80	-2175.60	230.17	-123.77	0	-1130.94	1.8	-617.12	1.8	-445.18	2.12	-447.33
19	20	20.90	-2175.60	251.32	-388.61	0	-1428.25	1.8	-406.20	1.8	-394.81	2.12	-358.26
20	20	20.90	-2175.60	251.75	-388.57	0	-1428.21	1.8	-406.21	1.8	-394.82	2.12	-358.28
20	21	22.00	-2175.60	278.40	-680.15	0	-1759.77	1.8	-160.16	1.8	-341.08	2.12	-263.26
21	1021	22.00	-2219.11	-284.72	-708.98	0	-1840.43	1.8	-128.03	1.8	-341.08	2.12	-263.25
21	22	23.40	-2219.11	-250.80	-334.10	0	-1402.77	1.8	-481.51	1.8	-405.54	2.12	-377.24
22	22	23.40	-2219.11	-250.28	-334.18	0	-1402.84	1.8	-481.49	1.8	-405.52	2.12	-377.20
22	23	24.80	-2219.11	-223.35	-2.62	0	-1020.69	1.8	-778.04	1.8	-464.54	2.12	-481.55
23	23	24.80	-2523.70	-222.84	-192.18	0	-1565.87	1.8	-581.52	1.8	-464.51	2.12	-481.51
23	24	26.20	-2523.70	-195.94	100.96	0	-1231.45	1.8	-832.45	1.8	-518.09	2.12	-576.25
24	24	26.20	-1696.97	-195.51	-296.82	0	-1361.75	1.8	-461.86	1.8	-196.22	2.12	-177.04
24	25	27.60	-1696.97	-168.57	-41.94	0	-1074.88	1.8	-667.29	1.8	-244.39	2.12	-262.22
25	25	27.60	-2088.58	-168.22	-273.90	0	-1757.14	1.8	-441.93	1.8	-244.36	2.12	-262.16
25	26	29.00	-2088.58	-114.83	-96.18	0	-1555.48	1.8	-590.50	1.8	-277.29	2.12	-320.39
26	26	29.00	-1242.90	-109.81	-493.91	0	-1814.24	1.8	303.33	1.8	-11.72	2.12	-23.10
26	27	30.40	-1243.14	-86.30	-349.28	0	-1630.99	1.8	93.50	1.8	-21.73	2.12	-42.81
27	27	30.40	-1606.18	-91.93	-548.45	0	-2237.21	1.8	242.91	1.8	-21.89	2.12	-42.10
27	28	31.80	-1606.18	-70.30	-434.91	0	-2096.64	1.8	76.50	1.8	-29.68	2.12	-57.08
28	28	31.80	-1606.18	-70.19	-434.96	0	-2096.68	1.8	76.50	1.8	-29.68	2.12	-57.06
28	29	33.20	-1606.18	-48.57	-351.82	0	-1992.87	1.8	-47.95	1.8	-35.17	2.12	-67.63
29	29	33.20	-1606.18	-48.48	-351.85	0	-1992.90	1.8	-47.94	1.8	-35.17	2.12	-67.62
29	30	34.60	-1606.18	-26.85	-299.12	0	-1925.93	1.8	-130.33	1.8	-38.38	2.12	-73.80
30	30	34.60	-1606.18	-26.77	-299.14	0	-1925.95	1.8	-130.32	1.8	-38.38	2.12	-73.79
30	31	36.00	-1606.18	-5.15	-276.79	0	-1895.76	1.8	-170.69	1.8	-39.31	2.12	-75.58
31	31	36.00	-1606.18	-5.08	-276.79	0	-1895.75	1.8	-170.69	1.8	-39.31	2.12	-75.58
31	32	37.40	-1606.18	16.56	-284.82	0	-1902.35	1.8	-169.04	1.8	-37.95	2.12	-72.98
32	32	37.40	-1606.18	16.63	-284.80	0	-1902.34	1.8	-169.04	1.8	-37.96	2.12	-72.98
32	33	38.80	-1606.18	38.26	-323.20	0	-1945.72	1.8	-125.35	1.8	-34.32	2.12	-65.99
33	33	38.80	-1606.18	38.35	-323.17	0	-1945.69	1.8	-125.35	1.8	-34.33	2.12	-66.00
33	34	40.20	-1606.18	59.98	-392.01	0	-2025.92	1.8	-39.61	1.8	-28.40	2.12	-54.61
34	34	40.20	-1606.18	60.08	-391.96	0	-2025.88	1.8	-39.62	1.8	-28.41	2.12	-54.63
34	35	41.60	-1606.18	81.71	-491.20	0	-2142.90	1.8	88.15	1.8	-20.20	2.12	-38.83
35	35	41.60	-1249.48	77.72	-292.03	0	-1542.75	1.8	-66.48	1.8	-20.04	2.12	-39.49
35	36	43.00	-1249.32	101.08	-421.28	0	-1701.04	1.8	102.02	1.8	-9.61	2.12	-18.94
36	36	43.00	-2088.58	104.46	-23.54	0	-1490.28	1.8	-594.99	1.8	-297.75	2.12	-356.57
36	37	44.40	-2088.58	158.86	-195.03	0	-1686.93	1.8	-444.90	1.8	-266.82	2.12	-301.87
37	37	44.40	-1696.97	159.24	36.94	0	-1004.67	1.8	-670.26	1.8	-266.85	2.12	-301.93
37	38	45.80	-1696.97	186.17	-204.82	0	-1279.87	1.8	-465.32	1.8	-222.41	2.12	-223.35
38	38	45.80	-2523.70	186.61	192.96	0	-1149.57	1.8	-835.91	1.8	-544.28	2.12	-622.56

ULO TENSIONAL

s de culo:

T0.M

anentes sin gradiente

+ [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

.7; 1.3]CME

Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)	Losa (t/m2)
39	47.20	-2523.70	213.53	-87.14	0	-1472.39	1.8	-585.44	1.8	-494.42	2.12	-534.39	-68.23
39	47.20	-2219.11	214.02	102.43	0	-927.20	1.8	-781.97	1.8	-494.45	2.12	-534.44	-60.15
40	48.60	-2212.66	241.45	-216.65	0	-1296.32	1.8	-483.73	1.8	-437.28	2.12	-434.68	-60.16
40	48.60	-2212.49	242.00	-216.66	0	-1296.27	1.8	-483.67	1.8	-437.23	2.12	-434.63	-49.30
41	50.00	-2212.49	275.93	-579.22	0	-1723.03	1.8	-130.45	1.8	-376.30	2.12	-326.90	-49.32
1041	50.00	-2212.70	-275.84	-579.22	0	-1723.10	1.8	-130.51	1.8	-376.36	2.12	-326.95	-35.66
42	51.40	-2212.70	-241.92	-216.78	0	-1296.44	1.8	-483.70	1.8	-437.26	2.12	-434.64	-35.68
42	51.40	-2213.30	-241.36	-216.79	0	-1296.64	1.8	-483.88	1.8	-437.41	2.12	-434.79	-19.23
43	52.80	-2213.30	-214.44	102.27	0	-925.55	1.8	-780.13	1.8	-492.85	2.12	-532.82	-19.25
43	52.80	-2518.88	-213.89	-87.19	0	-1470.95	1.8	-583.95	1.8	-493.12	2.12	-533.08	0.02
44	54.20	-2523.70	-186.61	192.95	0	-1149.58	1.8	-835.91	1.8	-544.28	2.12	-622.56	-0.01
44	54.20	-1696.97	-186.17	-204.83	0	-1279.88	1.8	-465.31	1.8	-222.41	2.12	-223.35	-16.95
45	55.60	-1696.97	-159.24	36.96	0	-1004.65	1.8	-670.27	1.8	-266.86	2.12	-301.94	-16.97
45	55.60	-2088.58	-158.86	-195.03	0	-1686.93	1.8	-444.90	1.8	-266.82	2.12	-301.87	-31.49
46	57.00	-2088.58	-104.46	-23.53	0	-1490.27	1.8	-594.99	1.8	-297.76	2.12	-356.57	-31.51
46	57.00	-1249.32	-101.09	-421.26	0	-1701.02	1.8	101.99	1.8	-9.61	2.12	-18.94	-43.59
47	58.40	-1251.27	-78.64	-291.13	0	-1542.84	1.8	-70.03	1.8	-20.04	2.12	-39.49	-43.61
47	58.40	-1608.20	-81.66	-490.31	0	-2143.18	1.8	84.43	1.8	-20.20	2.12	-38.83	-53.25
48	59.80	-1608.20	-60.02	-391.13	0	-2026.26	1.8	-43.16	1.8	-28.41	2.12	-54.63	-53.26
48	59.80	-1608.20	-59.92	-391.17	0	-2026.30	1.8	-43.15	1.8	-28.40	2.12	-54.62	-60.45
49	61.20	-1608.20	-38.29	-322.44	0	-1946.23	1.8	-128.69	1.8	-34.33	2.12	-66.00	-60.46
49	61.20	-1608.20	-38.20	-322.48	0	-1946.26	1.8	-128.68	1.8	-34.32	2.12	-65.99	-65.20
50	62.60	-1608.20	-16.57	-284.13	0	-1902.97	1.8	-172.21	1.8	-37.96	2.12	-72.99	-64.15
50	62.60	-1608.20	-16.49	-284.15	0	-1902.99	1.8	-172.21	1.8	-37.95	2.12	-72.98	-66.38
51	64.00	-1609.94	5.16	-276.22	0	-1897.96	1.8	-175.08	1.8	-39.31	2.12	-75.58	-66.39
51	64.00	-1609.94	5.23	-276.22	0	-1897.96	1.8	-175.08	1.8	-39.31	2.12	-75.58	-66.19
52	65.40	-1609.94	26.85	-298.68	0	-1928.32	1.8	-134.45	1.8	-38.38	2.12	-73.79	-66.19
52	65.40	-1609.94	26.93	-298.67	0	-1928.31	1.8	-134.45	1.8	-38.38	2.12	-73.80	-63.56
53	66.80	-1609.94	48.56	-351.50	0	-1995.44	1.8	-51.81	1.8	-35.17	2.12	-67.62	-63.56
53	66.80	-1609.94	48.66	-351.47	0	-1995.41	1.8	-51.82	1.8	-35.17	2.12	-67.64	-58.51
54	68.20	-1609.94	70.27	-434.71	0	-2099.37	1.8	72.87	1.8	-29.68	2.12	-57.06	-58.50
54	68.20	-1609.94	70.38	-434.66	0	-2099.33	1.8	72.86	1.8	-29.68	2.12	-57.08	-51.02
55	69.60	-1609.94	92.01	-548.31	0	-2240.07	1.8	239.54	1.8	-21.90	2.12	-42.10	-51.01
55	69.60	-1246.39	86.18	-349.14	0	-1633.44	1.8	90.53	1.8	-21.73	2.12	-42.81	-41.11
56	71.00	-1242.90	109.82	-493.92	0	-1814.25	1.8	303.35	1.8	-11.72	2.12	-23.10	-41.10
56	71.00	-2088.58	114.83	-96.18	0	-1555.48	1.8	-590.50	1.8	-277.29	2.12	-320.38	-28.77
57	72.40	-2088.58	168.22	-273.89	0	-1757.13	1.8	-441.94	1.8	-244.36	2.12	-262.17	-29.23
57	72.40	-1696.97	168.60	-41.93	0	-1074.87	1.8	-667.30	1.8	-244.40	2.12	-262.22	-14.25
58	73.80	-1696.97	195.53	-296.82	0	-1361.75	1.8	-461.86	1.8	-196.22	2.12	-177.04	-299.86
58	73.80	-2523.70	195.94	100.96	0	-1231.45	1.8	-832.45	1.8	-518.09	2.12	-576.25	-263.57
59	75.20	-2523.70	222.84	-192.20	0	-1565.90	1.8	-581.51	1.8	-464.50	2.12	-481.50	-279.53
59	75.20	-2219.11	223.34	-2.62	0	-1020.69	1.8	-778.04	1.8	-464.54	2.12	-481.55	-214.62
60	76.60	-2215.29	250.74	-334.69	0	-1402.16	1.8	-480.16	1.8	-404.37	2.12	-375.95	-613.73
60	76.60	-2215.34	251.30	-334.71	0	-1402.20	1.8	-480.17	1.8	-404.38	2.12	-375.95	-543.85
61	78.00	-2215.34	285.21	-710.28	0	-1840.53	1.8	-126.48	1.8	-339.74	2.12	-261.66	-543.81
1061	78.00	-2172.15	-278.55	-681.49	0	-1760.00	1.8	-158.71	1.8	-339.82	2.12	-261.74	-468.96
62	79.10	-2172.15	-251.90	-389.75	0	-1428.29	1.8	-404.80	1.8	-393.60	2.12	-356.83	-468.93
62	79.10	-2172.53	-251.49	-389.79	0	-1428.44	1.8	-404.91	1.8	-393.69	2.12	-356.91	-389.13
63	80.20	-2172.53	-230.34	-124.76	0	-1130.95	1.8	-615.88	1.8	-444.11	2.12	-446.07	-389.11
63	80.20	-2477.65	-229.94	-317.28	0	-1681.07	1.8	-412.48	1.8	-444.25	2.12	-446.20	-304.37
64	81.30	-2477.65	-208.78	-75.99	0	-1413.08	1.8	-595.26	1.8	-491.31	2.12	-529.42	-304.37
64	81.30	-2478.35	-208.39	-76.02	0	-1413.32	1.8	-595.46	1.8	-491.49	2.12	-529.59	-405.65
65	82.40	-2478.35	-187.24	141.59	0	-1174.75	1.8	-750.15	1.8	-535.20	2.12	-606.88	-405.68
65	82.40	-1870.06	-186.86	-389.21	0	-1691.09	1.8	-244.56	1.8	-213.60	2.12	-207.96	-498.95
66	83.50	-1870.06	-165.71	-195.32	0	-1481.97	1.8	-371.09	1.8	-253.95	2.12	-279.31	-499.00
66	83.50	-1871.02	-165.33	-195.31	0	-1496.14	1.8	-357.85	1.8	-242.45	2.12	-263.57	-584.24
67	84.60	-1871.02	-116.19	-53.05	0	-1356.06	1.8	-435.88	1.8	-261.71	2.12	-301.98	-185.14
67	84.60	-1016.26	-107.22	-450.76	0	-1552.65	1.8	341.59	1.8	-8.35	2.12	-16.46	-262.30
68	85.70	-1019.75	-90.23	-333.06	0	-1408.64	1.8	173.22	1.8	-16.90	2.12	-33.30	-262.36
68	85.70	-1261.85	-97.84	-464.08	0	-1807.47	1.8	266.02	1.8	-17.03	2.12	-32.74	-316.94
69	86.80	-1261.85	-80.82	-365.83	0	-1687.72	1.8	127.72	1.8	-24.22	2.12	-46.58	-20.60
69	86.80	-1261.85	-80.71	-365.86	0	-1687.74	1.8	127.72	1.8	-24.22	2.12	-46.56	-38.21
70	87.90	-1261.85	-63.73	-286.42	0	-1590.73	1.8	15.36	1.8	-29.99	2.12	-57.66	-37.62
70	87.90	-1261.85	-63.63	-286.45	0	-1590.76	1.8	15.36	1.8	-29.98	2.12	-57.65	-51.02
71	89.00	-1261.85	-46.63	-225.81	0	-1516.49	1.8	-71.05	1.8	-34.34	2.12	-66.03	-51.04
71	89.00	-1261.85	-46.55	-225.83	0	-1516.50	1.8	-71.05	1.8	-34.34	2.12	-66.03	-60.52
72	90.10	-1261.85	-29.56	-183.97	0	-1464.97	1.8	-131.52	1.8	-37.28	2.12	-71.68	-60.53
72	90.10	-1261.85	-29.47	-183.97	0	-1464.97	1.8	-131.52	1.8	-37.28	2.12	-71.68	-66.06
73	91.20	-1261.85	-12.48	-160.91	0	-1436.18	1.8	-166.04	1.8	-38.80	2.12	-74.61	-66.06
73	91.20	-1261.85	-12.40	-160.90	0	-1436.17	1.8	-166.04	1.8	-38.81	2.12	-74.62	-67.65
74	92.30	-1261.85	4.60	-156.60	0	-1430.10	1.8	-174.61	1.8	-38.92	2.12	-74.84	-67.65
74	92.30	-1261.85	4.69	-156.59	0	-1430.09	1.8	-174.61	1.8	-38.92	2.12	-74.84	-65.29
75	93.40	-1261.85	21.68	-171.09	0	-1446.77	1.8	-157.22	1.8	-37.62	2.12	-72.34	-65.28
75	93.40	-1261.85	21.77	-171.06	0	-1443.34	1.8	-139.47	1.8	-37.32	2.12	-73.53	-58.97
76	94.50	-1261.85	38.76	-204.38	0	-1484.67	1.8	-96.22	1.8	-34.62	2.12	-68.22	-58.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	57.06	-410.12	0	-2040.73	1.8	-36.07	1.8	-25.33	2.12	-48.71
134	134	40.20	-1606.18	56.96	-410.17	0	-2040.77	1.8	-36.06	1.8	-25.32	2.12	-48.69
134	135	41.60	-1606.18	77.77	-504.48	0	-2153.76	1.8	90.75	1.8	-17.94	2.12	-34.50
135	135	41.60	-1249.48	73.50	-305.43	0	-1554.31	1.8	-63.89	1.8	-17.79	2.12	-35.05
135	136	43.00	-1249.32	96.03	-428.18	0	-1707.01	1.8	103.36	1.8	-8.45	2.12	-16.65
136	136	43.00	-2088.58	99.07	-30.60	0	-1497.12	1.8	-592.93	1.8	-295.97	2.12	-353.41
136	137	44.40	-2088.58	147.33	-193.05	0	-1685.02	1.8	-445.48	1.8	-267.32	2.12	-302.75
137	137	44.40	-1696.97	146.95	38.62	0	-1003.04	1.8	-670.75	1.8	-267.28	2.12	-302.68
137	138	45.80	-1696.97	172.34	-184.88	0	-1260.57	1.8	-471.13	1.8	-227.46	2.12	-232.28
138	138	45.80	-2523.70	171.91	212.65	0	-1130.50	1.8	-841.65	1.8	-549.27	2.12	-631.38
138	139	47.20	-2523.70	197.29	-45.78	0	-1432.36	1.8	-597.50	1.8	-504.89	2.12	-552.90
139	139	47.20	-2219.11	196.80	143.57	0	-887.38	1.8	-793.95	1.8	-504.86	2.12	-552.85
139	140	48.60	-2212.66	222.69	-150.33	0	-1232.12	1.8	-503.05	1.8	-454.06	2.12	-464.36
140	140	48.60	-2212.49	222.15	-150.45	0	-1232.19	1.8	-502.97	1.8	-453.99	2.12	-464.26
140	141	50.00	-2212.49	254.56	-484.13	0	-1631.00	1.8	-158.16	1.8	-400.37	2.12	-369.45
141	1141	50.00	-2212.71	-254.47	-484.13	0	-1631.07	1.8	-158.23	1.8	-400.43	2.12	-369.51
141	142	51.40	-2212.71	-222.07	-150.58	0	-1232.38	1.8	-503.00	1.8	-454.01	2.12	-464.27
142	142	51.40	-2213.30	-222.59	-150.46	0	-1232.45	1.8	-503.21	1.8	-454.20	2.12	-464.48
142	143	52.80	-2213.30	-197.20	143.43	0	-885.72	1.8	-792.12	1.8	-503.27	2.12	-551.24
143	143	52.80	-2518.88	-197.67	-45.81	0	-1430.91	1.8	-596.01	1.8	-503.59	2.12	-551.60
143	144	54.20	-2523.70	-171.91	212.64	0	-1130.51	1.8	-841.64	1.8	-549.26	2.12	-631.37
144	144	54.20	-1696.97	-172.35	-184.88	0	-1260.57	1.8	-471.13	1.8	-227.46	2.12	-232.28
144	145	55.60	-1696.97	-146.96	38.64	0	-1003.03	1.8	-670.76	1.8	-267.28	2.12	-302.69
145	145	55.60	-2088.58	-147.33	-193.05	0	-1685.02	1.8	-445.48	1.8	-267.32	2.12	-302.75
145	146	57.00	-2088.58	-99.07	-30.59	0	-1497.11	1.8	-592.93	1.8	-295.97	2.12	-353.41
146	146	57.00	-1249.32	-96.04	-428.18	0	-1707.00	1.8	103.36	1.8	-8.45	2.12	-16.65
146	147	58.40	-1251.27	-74.42	-304.52	0	-1554.39	1.8	-67.46	1.8	-17.79	2.12	-35.05
147	147	58.40	-1608.20	-77.71	-503.57	0	-2154.02	1.8	86.99	1.8	-17.95	2.12	-34.51
147	148	59.80	-1608.20	-56.90	-409.36	0	-2041.17	1.8	-39.60	1.8	-25.32	2.12	-48.69
148	148	59.80	-1608.20	-57.01	-409.31	0	-2041.13	1.8	-39.61	1.8	-25.33	2.12	-48.70
148	149	61.20	-1608.20	-36.21	-344.06	0	-1963.91	1.8	-124.47	1.8	-30.66	2.12	-58.96
149	149	61.20	-1608.20	-36.30	-344.02	0	-1963.88	1.8	-124.47	1.8	-30.67	2.12	-58.97
149	150	62.60	-1608.20	-15.48	-307.77	0	-1922.31	1.8	-167.60	1.8	-33.95	2.12	-65.28
150	150	62.60	-1608.20	-15.56	-307.75	0	-1922.29	1.8	-167.60	1.8	-33.95	2.12	-65.29
150	151	64.00	-1609.94	5.27	-300.55	0	-1917.86	1.8	-170.33	1.8	-35.18	2.12	-67.65
151	151	64.00	-1609.94	5.20	-300.55	0	-1917.86	1.8	-170.33	1.8	-35.18	2.12	-67.65
151	152	65.40	-1609.94	26.00	-322.40	0	-1947.72	1.8	-129.82	1.8	-34.36	2.12	-66.06
152	152	65.40	-1609.94	25.93	-322.41	0	-1947.73	1.8	-129.82	1.8	-34.36	2.12	-66.06
152	153	66.80	-1609.94	46.74	-373.26	0	-2013.23	1.8	-47.58	1.8	-31.48	2.12	-60.53
153	153	66.80	-1609.94	46.66	-373.30	0	-2013.26	1.8	-47.58	1.8	-31.47	2.12	-60.52
153	154	68.20	-1609.94	67.45	-453.20	0	-2114.50	1.8	76.50	1.8	-26.55	2.12	-51.04
154	154	68.20	-1609.94	67.34	-453.25	0	-2114.54	1.8	76.51	1.8	-26.54	2.12	-51.03
154	155	69.60	-1609.94	88.16	-562.08	0	-2251.34	1.8	242.24	1.8	-19.56	2.12	-37.62
155	155	69.60	-1246.39	84.07	-363.03	0	-1645.44	1.8	93.24	1.8	-19.39	2.12	-38.21
155	156	71.00	-1242.90	104.88	-501.47	0	-1820.77	1.8	304.84	1.8	-10.46	2.12	-20.60
156	156	71.00	-2088.58	109.57	-103.88	0	-1562.93	1.8	-588.26	1.8	-275.34	2.12	-316.94
156	157	72.40	-2088.58	156.93	-273.44	0	-1756.68	1.8	-442.07	1.8	-244.48	2.12	-262.37
157	157	72.40	-1696.97	156.56	-41.74	0	-1074.68	1.8	-667.35	1.8	-244.45	2.12	-262.31
157	158	73.80	-1696.97	181.97	-278.72	0	-1344.24	1.8	-467.13	1.8	-200.80	2.12	-185.14
158	158	73.80	-2523.70	181.53	118.80	0	-1214.18	1.8	-837.65	1.8	-522.60	2.12	-584.23
158	159	75.20	-2523.70	206.91	-153.10	0	-1528.05	1.8	-592.91	1.8	-474.40	2.12	-499.00
159	159	75.20	-2219.11	206.42	36.25	0	-983.07	1.8	-789.36	1.8	-474.37	2.12	-498.95
159	160	76.60	-2215.29	232.30	-271.06	0	-1340.58	1.8	-498.70	1.8	-420.47	2.12	-404.42
160	160	76.60	-2215.34	231.80	-271.23	0	-1340.76	1.8	-498.67	1.8	-420.44	2.12	-404.36
160	161	78.00	-2215.34	264.19	-618.40	0	-1751.60	1.8	-153.26	1.8	-362.99	2.12	-302.78
161	1161	78.00	-2172.15	-257.07	-589.63	0	-1671.10	1.8	-185.48	1.8	-363.07	2.12	-302.85
161	162	79.10	-2172.15	-231.63	-320.84	0	-1361.60	1.8	-424.88	1.8	-411.04	2.12	-387.67
162	162	79.10	-2172.53	-232.06	-320.81	0	-1361.69	1.8	-425.01	1.8	-411.15	2.12	-387.78
162	163	80.20	-2172.53	-212.12	-76.50	0	-1084.25	1.8	-629.94	1.8	-456.32	2.12	-467.66
163	163	80.20	-2477.65	-212.51	-268.91	0	-1634.25	1.8	-426.57	1.8	-456.49	2.12	-467.85
163	164	81.30	-2477.65	-192.56	-46.13	0	-1384.18	1.8	-603.96	1.8	-498.87	2.12	-542.78
164	164	81.30	-2478.35	-192.91	-45.99	0	-1384.26	1.8	-604.21	1.8	-499.09	2.12	-543.03
164	165	82.40	-2478.35	-172.97	155.25	0	-1161.52	1.8	-754.13	1.8	-538.66	2.12	-612.99
165	165	82.40	-1870.06	-173.26	-375.37	0	-1677.69	1.8	-248.59	1.8	-217.10	2.12	-214.16
165	166	83.50	-1870.06	-153.31	-195.76	0	-1482.40	1.8	-370.96	1.8	-253.84	2.12	-279.11
166	166	83.50	-1871.02	-153.53	-195.58	0	-1496.37	1.8	-357.80	1.8	-242.40	2.12	-263.49
166	167	84.60	-1871.02	-110.49	-59.82	0	-1361.90	1.8	-434.61	1.8	-260.60	2.12	-299.78
167	167	84.60	-1016.26	-101.80	-457.43	0	-1558.42	1.8	342.88	1.8	-7.23	2.12	-14.25
167	168	85.70	-1019.75	-85.47	-345.35	0	-1419.25	1.8	175.60	1.8	-14.83	2.12	-29.23
168	168	85.70	-1261.85	-93.31	-476.27	0	-1817.45	1.8	268.40	1.8	-14.96	2.12	-28.77
168	169	86.80	-1261.85	-76.95	-382.64	0	-1701.47	1.8	131.00	1.8	-21.37	2.12	-41.10
169	169	86.80	-1261.85	-77.05	-382.61	0	-1701.44	1.8	130.99	1.8	-21.38	2.12	-41.11
169	170	87.90	-1261.85	-60.72	-306.83	0	-1607.41	1.8	19.32	1.8	-26.53	2.12	-51.01
170	170	87.90	-1261.85	-60.81	-306.80	0	-1607.39	1.8	19.31	1.8	-26.53	2.12	-51.02
170	171	89.00	-1261.85	-44.46	-248.89	0	-1535.36	1.8	-66.57	1.8	-30.43	2.12	-58.50

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	64.06	217.10	0	-731.54	1.8	-321.29	1.8	-74.13	2.12	-146.08
76	77	95.60	-944.83	88.51	132.00	0	-825.97	1.8	-243.40	1.8	-64.67	2.12	-127.44
77	77	95.60	-944.83	88.66	132.06	0	-825.92	1.8	-243.41	1.8	-64.68	2.12	-127.46
77	78	96.70	-944.83	113.90	21.42	0	-949.99	1.8	-138.31	1.8	-52.69	2.12	-103.82
78	78	96.70	-747.99	114.08	141.95	0	-600.80	1.8	-260.74	1.8	-52.70	2.12	-103.84
78	79	97.80	-747.99	138.11	4.30	0	-755.79	1.8	-128.17	1.8	-37.91	2.12	-74.71
79	79	97.80	-747.99	138.29	4.37	0	-755.73	1.8	-128.19	1.8	-37.93	2.12	-74.73
79	80	98.90	-747.99	162.31	-160.31	0	-941.64	1.8	31.85	1.8	-20.36	2.12	-40.11
80	80	98.90	-472.42	162.53	13.92	0	-444.03	1.8	-152.34	1.8	-20.37	2.12	-40.13
80	81	100.00	-472.42	133.81	-178.73	0	-662.45	1.8	37.60	1.8	-0.03	2.12	-0.05
101	101	0.00	-472.42	-151.76	-178.67	0	-662.40	1.8	37.59	1.8	-0.04	2.12	-0.07
101	102	1.10	-476.85	-157.92	8.50	0	-452.19	1.8	-155.02	1.8	-19.44	2.12	-38.31
102	102	1.10	-752.42	-158.00	-165.63	0	-949.71	1.8	29.15	1.8	-19.45	2.12	-38.32
102	103	2.20	-752.42	-134.58	-5.55	0	-767.70	1.8	-130.20	1.8	-36.23	2.12	-71.39
103	103	2.20	-752.42	-134.64	-5.52	0	-767.68	1.8	-130.21	1.8	-36.23	2.12	-71.40
103	104	3.30	-752.42	-111.23	128.38	0	-615.87	1.8	-262.23	1.8	-50.37	2.12	-99.25
104	104	3.30	-949.26	-111.26	7.93	0	-964.99	1.8	-139.82	1.8	-50.37	2.12	-99.26
104	105	4.40	-949.26	-87.85	115.75	0	-843.29	1.8	-244.53	1.8	-61.88	2.12	-121.94
105	105	4.40	-949.26	-87.89	115.75	0	-843.29	1.8	-244.53	1.8	-61.88	2.12	-121.94
105	106	5.50	-949.26	-62.52	199.05	0	-750.35	1.8	-322.26	1.8	-71.03	2.12	-139.96
106	106	5.50	-1146.10	-62.57	80.57	0	-1096.34	1.8	-204.44	1.8	-71.03	2.12	-139.96
106	107	6.60	-1146.10	-39.15	137.82	0	-1033.47	1.8	-254.91	1.8	-77.54	2.12	-152.80
107	107	6.60	-1146.10	-39.20	137.82	0	-1050.53	1.8	-271.64	1.8	-78.19	2.12	-150.34
107	108	7.70	-1146.10	-15.80	168.96	0	-1019.39	1.8	-294.88	1.8	-82.10	2.12	-157.87
108	108	7.70	-1146.10	-15.85	168.96	0	-1019.39	1.8	-294.88	1.8	-82.10	2.12	-157.87
108	109	8.80	-1146.10	7.56	173.99	0	-1016.97	1.8	-290.72	1.8	-83.36	2.12	-160.29
109	109	8.80	-1146.10	7.50	174.00	0	-1016.97	1.8	-290.72	1.8	-83.36	2.12	-160.29
109	110	9.90	-1146.10	30.91	154.21	0	-1042.22	1.8	-259.44	1.8	-82.19	2.12	-158.03
110	110	9.90	-1146.10	30.84	154.19	0	-1042.23	1.8	-259.43	1.8	-82.18	2.12	-158.03
110	111	11.00	-1146.10	54.27	108.60	0	-1095.96	1.8	-200.85	1.8	-78.40	2.12	-150.76
111	111	11.00	-1146.10	54.19	108.57	0	-1095.98	1.8	-200.85	1.8	-78.40	2.12	-150.75
111	112	12.10	-1146.10	77.62	36.97	0	-1178.36	1.8	-114.88	1.8	-71.98	2.12	-138.40
112	112	12.10	-1146.10	77.52	36.95	0	-1178.38	1.8	-114.88	1.8	-71.97	2.12	-138.39
112	113	13.20	-1146.10	100.89	-60.62	0	-1289.36	1.8	-1.55	1.8	-62.92	2.12	-120.99
113	113	13.20	-1146.10	100.77	-60.65	0	-1289.39	1.8	-1.54	1.8	-62.92	2.12	-120.98
113	114	14.30	-1146.10	124.20	-183.25	0	-1428.21	1.8	138.92	1.8	-51.39	2.12	-98.82
114	114	14.30	-924.56	119.12	-64.78	0	-1054.27	1.8	57.48	1.8	-50.97	2.12	-100.43
114	115	15.40	-917.39	140.02	-215.07	0	-1223.56	1.8	235.66	1.8	-36.98	2.12	-72.87
115	115	15.40	-1858.58	148.48	224.43	0	-1027.92	1.8	-541.62	1.8	-322.07	2.12	-399.22
115	116	16.50	-1858.58	145.07	54.39	0	-1191.92	1.8	-458.38	1.8	-298.29	2.12	-351.79
116	116	16.50	-1858.58	145.05	54.41	0	-1156.75	1.8	-492.68	1.8	-328.08	2.12	-392.31
116	117	17.60	-1858.58	161.42	-115.24	0	-1342.65	1.8	-372.42	1.8	-293.96	2.12	-331.98
117	117	17.60	-2575.50	161.38	445.13	0	-849.00	1.8	-905.30	1.8	-649.68	2.12	-773.15
117	118	18.70	-2575.50	170.52	260.77	0	-1055.40	1.8	-760.31	1.8	-614.38	2.12	-710.74
118	118	18.70	-2575.50	170.44	260.69	0	-1055.48	1.8	-760.28	1.8	-614.36	2.12	-710.70
118	119	19.80	-2575.50	180.91	67.16	0	-1277.25	1.8	-591.42	1.8	-579.39	2.12	-648.86
119	119	19.80	-2299.92	180.71	241.24	0	-779.78	1.8	-775.57	1.8	-579.37	2.12	-648.82
119	120	20.90	-2299.92	191.50	36.44	0	-1018.97	1.8	-582.15	1.8	-544.19	2.12	-586.62
120	120	20.90	-2299.92	191.21	36.43	0	-1018.98	1.8	-582.15	1.8	-544.19	2.12	-586.62
120	121	22.00	-2299.92	211.10	-185.56	0	-1283.20	1.8	-356.38	1.8	-508.06	2.12	-522.74
121	1121	22.00	-2339.29	-217.01	-211.63	0	-1356.16	1.8	-327.31	1.8	-508.06	2.12	-522.74
121	122	23.40	-2339.29	-191.75	75.25	0	-1003.66	1.8	-655.15	1.8	-550.25	2.12	-597.35
122	122	23.40	-2339.29	-192.09	75.29	0	-1003.62	1.8	-655.16	1.8	-550.26	2.12	-597.36
122	123	24.80	-2339.29	-175.52	333.16	0	-692.78	1.8	-930.24	1.8	-590.63	2.12	-668.74
123	123	24.80	-2614.86	-175.90	161.77	0	-1185.93	1.8	-752.47	1.8	-590.63	2.12	-668.75
123	124	26.20	-2614.86	-167.90	400.58	0	-904.09	1.8	-987.57	1.8	-630.46	2.12	-739.17
124	124	26.20	-1701.11	-168.00	-38.80	0	-1047.85	1.8	-578.04	1.8	-274.78	2.12	-298.06
124	125	27.60	-1701.11	-150.58	183.61	0	-792.40	1.8	-774.02	1.8	-314.74	2.12	-368.71
125	125	27.60	-2055.42	-150.61	-26.04	0	-1409.47	1.8	-570.19	1.8	-314.76	2.12	-368.76
125	126	29.00	-2055.42	-154.06	202.70	0	-1158.43	1.8	-733.62	1.8	-360.60	2.12	-449.81
126	126	29.00	-1122.96	-149.46	-236.76	0	-1439.14	1.8	178.43	1.8	-41.46	2.12	-81.70
126	127	30.40	-1129.71	-121.97	-42.87	0	-1218.97	1.8	-45.37	1.8	-59.81	2.12	-117.86
127	127	30.40	-1460.38	-124.26	-222.98	0	-1782.28	1.8	87.41	1.8	-60.31	2.12	-115.97
127	128	31.80	-1460.38	-94.21	-71.37	0	-1610.87	1.8	-85.49	1.8	-74.63	2.12	-143.50
128	128	31.80	-1460.38	-94.37	-71.34	0	-1610.85	1.8	-85.50	1.8	-74.64	2.12	-143.51
128	129	33.20	-1460.38	-63.20	38.87	0	-1485.21	1.8	-214.32	1.8	-84.79	2.12	-163.05
129	129	33.20	-1460.38	-63.35	38.90	0	-1485.19	1.8	-214.33	1.8	-84.80	2.12	-163.06
129	130	34.60	-1460.38	-35.10	108.01	0	-1405.13	1.8	-298.95	1.8	-90.87	2.12	-174.72
130	130	34.60	-1460.38	-35.24	108.03	0	-1405.12	1.8	-298.96	1.8	-90.87	2.12	-174.73
130	131	36.00	-1460.38	-5.31	134.93	0	-1371.51	1.8	-339.29	1.8	-92.64	2.12	-178.13
131	131	36.00	-1460.38	-5.44	134.92	0	-1371.52	1.8	-339.29	1.8	-92.64	2.12	-178.13
131	132	37.40	-1460.38	25.89	121.12	0	-1383.16	1.8	-335.53	1.8	-90.38	2.12	-173.80
132	132	37.40	-1460.38	25.75	121.10	0	-1383.18	1.8	-335.53	1.8	-90.38	2.12	-173.79
132	133	38.80	-1460.38	53.99	65.04	0	-1441.31	1.8	-287.45	1.8	-83.83	2.12	-161.19
133	133	38.80	-1460.38	53.84	65.02	0	-1441.33	1.8	-287.45	1.8	-83.82	2.12	-161.18

Combi_to.xls

Programa DINTEL PACADAR S.A.
CUASIPERM1.T0.MZ+

11/09/03

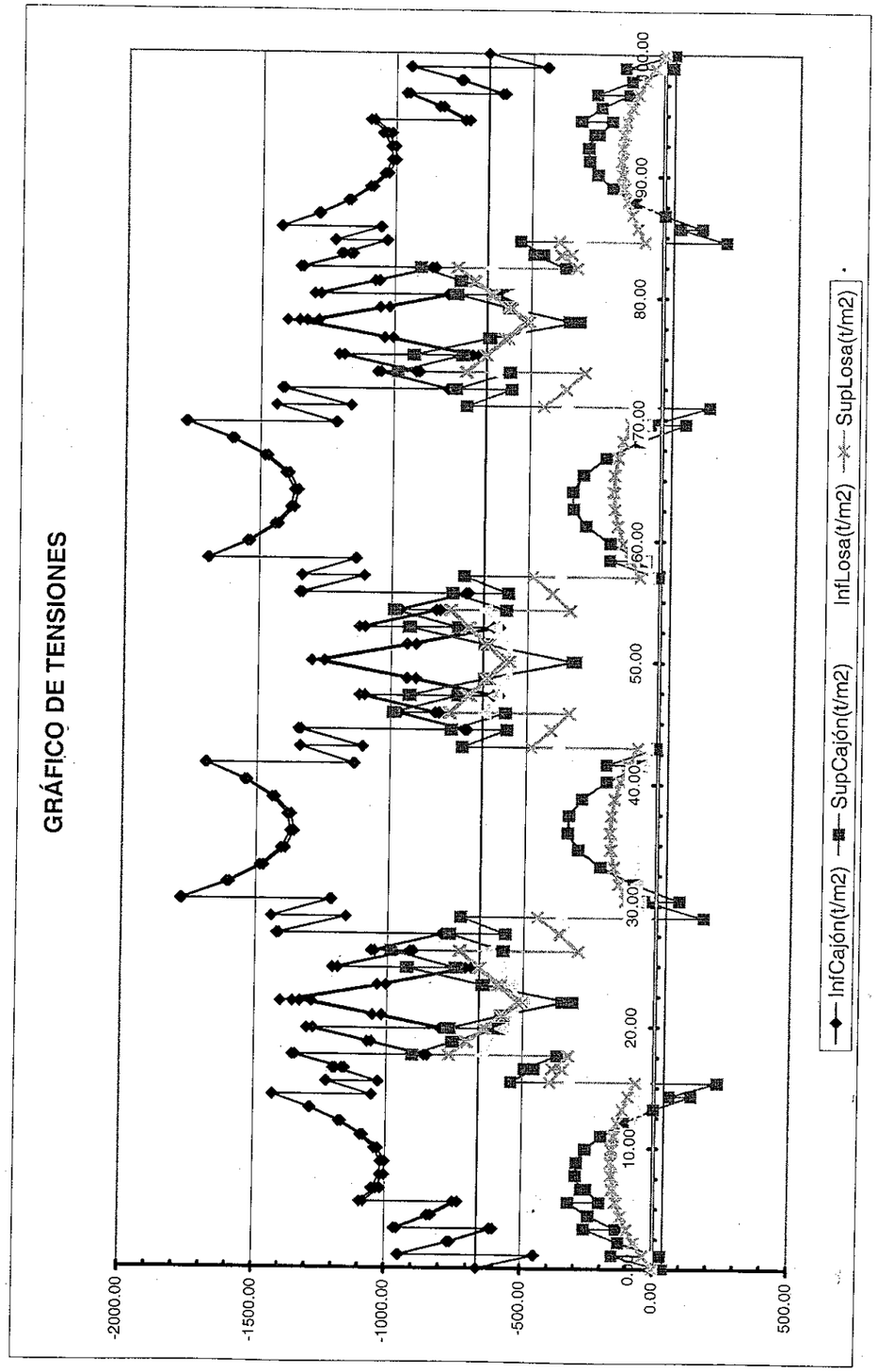
CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	85.02	-32.02	0	-1544.92	1.8	-195.29	1.8	-73.19	2.12	-140.73
134	134	40.20	-1460.38	84.86	-32.06	0	-1544.95	1.8	-195.28	1.8	-73.18	2.12	-140.72
134	135	41.60	-1460.38	114.88	-170.59	0	-1694.42	1.8	-58.90	1.8	-58.39	2.12	-112.27
135	135	41.60	-1135.74	114.14	9.51	0	-1136.99	1.8	-196.67	1.8	-57.90	2.12	-114.09
135	136	43.00	-1128.92	141.79	-172.37	0	-1337.05	1.8	-6.81	1.8	-39.07	2.12	-76.99
136	136	43.00	-2055.42	144.83	267.09	0	-1101.22	1.8	-735.70	1.8	-378.98	2.12	-482.31
136	137	44.40	-2055.42	142.75	57.08	0	-1335.16	1.8	-574.39	1.8	-338.29	2.12	-410.36
137	137	44.40	-1701.11	142.71	266.73	0	-718.08	1.8	-778.23	1.8	-338.27	2.12	-410.32
137	138	45.80	-1701.11	160.78	54.57	0	-964.64	1.8	-581.90	1.8	-301.32	2.12	-344.99
138	138	45.80	-2614.86	160.74	493.93	0	-820.89	1.8	-991.42	1.8	-657.00	2.12	-786.09
138	139	47.20	-2614.86	170.20	263.59	0	-1095.57	1.8	-755.45	1.8	-619.73	2.12	-720.19
139	139	47.20	-2339.29	170.03	434.92	0	-602.47	1.8	-933.21	1.8	-619.71	2.12	-720.15
139	140	48.60	-2345.74	184.51	187.03	0	-906.66	1.8	-659.69	1.8	-584.01	2.12	-655.71
140	140	48.60	-2345.92	184.14	187.06	0	-906.69	1.8	-659.75	1.8	-584.06	2.12	-655.77
140	141	50.00	-2345.92	209.17	-89.23	0	-1249.96	1.8	-331.67	1.8	-544.97	2.12	-586.64
141	1141	50.00	-2345.71	-209.25	-89.22	0	-1249.89	1.8	-331.61	1.8	-544.91	2.12	-586.58
141	142	51.40	-2345.71	-184.22	187.19	0	-906.51	1.8	-659.73	1.8	-584.04	2.12	-655.77
142	142	51.40	-2345.10	-184.59	187.16	0	-906.34	1.8	-659.53	1.8	-583.87	2.12	-655.59
142	143	52.80	-2345.10	-169.61	435.08	0	-604.11	1.8	-935.04	1.8	-621.30	2.12	-721.78
143	143	52.80	-2619.68	-169.84	263.64	0	-1097.00	1.8	-756.95	1.8	-621.03	2.12	-721.50
143	144	54.20	-2614.86	-160.74	493.92	0	-820.90	1.8	-991.42	1.8	-657.00	2.12	-786.09
144	144	54.20	-1701.11	-160.79	54.57	0	-964.64	1.8	-581.90	1.8	-301.32	2.12	-344.99
144	145	55.60	-1701.11	-142.72	266.75	0	-718.07	1.8	-778.23	1.8	-338.27	2.12	-410.33
145	145	55.60	-2055.42	-142.76	57.08	0	-1335.16	1.8	-574.39	1.8	-338.29	2.12	-410.36
145	146	57.00	-2055.42	-144.83	267.11	0	-1101.20	1.8	-735.71	1.8	-378.98	2.12	-482.32
146	146	57.00	-1128.92	-141.80	-172.34	0	-1337.03	1.8	-6.81	1.8	-39.08	2.12	-77.00
146	147	58.40	-1133.95	-113.23	8.65	0	-1136.86	1.8	-193.15	1.8	-57.90	2.12	-114.10
147	147	58.40	-1458.36	-114.94	-171.46	0	-1694.12	1.8	-55.20	1.8	-58.39	2.12	-112.27
147	148	59.80	-1458.36	-84.92	-32.86	0	-1544.54	1.8	-191.74	1.8	-73.19	2.12	-140.73
148	148	59.80	-1458.36	-85.08	-32.82	0	-1544.51	1.8	-191.74	1.8	-73.19	2.12	-140.74
148	149	61.20	-1458.36	-53.90	64.30	0	-1440.79	1.8	-284.10	1.8	-83.83	2.12	-161.19
149	149	61.20	-1458.36	-54.05	64.32	0	-1440.77	1.8	-284.10	1.8	-83.83	2.12	-161.19
149	150	62.60	-1458.36	-25.81	120.48	0	-1382.50	1.8	-332.39	1.8	-90.39	2.12	-173.80
150	150	62.60	-1458.36	-25.95	120.50	0	-1382.48	1.8	-332.39	1.8	-90.39	2.12	-173.80
150	151	64.00	-1456.62	5.36	134.37	0	-1369.31	1.8	-334.89	1.8	-92.64	2.12	-178.14
151	151	64.00	-1456.62	5.23	134.37	0	-1369.30	1.8	-334.89	1.8	-92.64	2.12	-178.14
151	152	65.40	-1456.62	35.16	107.59	0	-1402.73	1.8	-294.83	1.8	-90.87	2.12	-174.73
152	152	65.40	-1456.62	35.02	107.58	0	-1402.74	1.8	-294.83	1.8	-90.87	2.12	-174.73
152	153	66.80	-1456.62	63.25	38.58	0	-1482.63	1.8	-210.46	1.8	-84.80	2.12	-163.06
153	153	66.80	-1456.62	63.12	38.56	0	-1482.64	1.8	-210.46	1.8	-84.80	2.12	-163.06
153	154	68.20	-1456.62	94.29	-71.55	0	-1608.11	1.8	-81.90	1.8	-74.64	2.12	-143.52
154	154	68.20	-1456.62	94.13	-71.58	0	-1608.14	1.8	-81.89	1.8	-74.63	2.12	-143.51
154	155	69.60	-1456.62	124.18	-223.08	0	-1779.38	1.8	90.76	1.8	-60.32	2.12	-115.98
155	155	69.60	-1126.45	120.10	-42.97	0	-1216.47	1.8	-42.44	1.8	-59.82	2.12	-117.87
155	156	71.00	-1122.96	149.46	-236.75	0	-1439.14	1.8	178.45	1.8	-41.46	2.12	-81.70
156	156	71.00	-2055.42	154.07	202.71	0	-1158.41	1.8	-733.62	1.8	-360.61	2.12	-449.82
156	157	72.40	-2055.42	150.62	-26.02	0	-1409.45	1.8	-570.19	1.8	-314.77	2.12	-368.77
157	157	72.40	-1701.11	150.59	183.63	0	-792.38	1.8	-774.03	1.8	-314.74	2.12	-368.72
157	158	73.80	-1701.11	168.01	-38.81	0	-1047.85	1.8	-578.04	1.8	-274.78	2.12	-298.06
158	158	73.80	-2614.86	167.90	400.57	0	-904.09	1.8	-987.56	1.8	-630.46	2.12	-739.17
158	159	75.20	-2614.86	175.90	161.76	0	-1185.94	1.8	-752.47	1.8	-590.63	2.12	-668.74
159	159	75.20	-2339.29	175.51	333.17	0	-692.77	1.8	-930.24	1.8	-590.63	2.12	-668.74
159	160	76.60	-2343.12	191.62	75.80	0	-1004.31	1.8	-656.49	1.8	-551.42	2.12	-598.61
160	160	76.60	-2343.06	191.25	75.85	0	-1004.25	1.8	-656.48	1.8	-551.41	2.12	-598.62
160	161	78.00	-2343.06	216.52	-210.34	0	-1356.07	1.8	-328.85	1.8	-509.40	2.12	-524.33
161	1161	78.00	-2303.37	-210.95	-184.25	0	-1282.99	1.8	-357.82	1.8	-509.32	2.12	-524.25
161	162	79.10	-2303.37	-191.07	37.58	0	-1018.93	1.8	-583.54	1.8	-545.40	2.12	-588.06
162	162	79.10	-2302.99	-191.34	37.59	0	-1018.81	1.8	-583.43	1.8	-545.30	2.12	-587.96
162	163	80.20	-2302.99	-180.56	242.21	0	-779.78	1.8	-776.80	1.8	-580.43	2.12	-650.08
163	163	80.20	-2578.03	-180.75	68.10	0	-1277.12	1.8	-592.48	1.8	-580.30	2.12	-649.96
163	164	81.30	-2578.03	-170.27	261.46	0	-1055.51	1.8	-761.29	1.8	-615.24	2.12	-711.73
164	164	81.30	-2577.33	-170.38	261.49	0	-1055.27	1.8	-761.08	1.8	-615.05	2.12	-711.55
164	165	82.40	-2577.33	-161.23	445.69	0	-849.03	1.8	-906.03	1.8	-650.31	2.12	-773.89
165	165	82.40	-1859.54	-161.32	-114.37	0	-1341.86	1.8	-373.76	1.8	-294.34	2.12	-332.45
165	166	83.50	-1859.54	-144.95	54.77	0	-1156.70	1.8	-493.08	1.8	-328.43	2.12	-392.73
166	166	83.50	-1858.58	-145.06	54.65	0	-1191.69	1.8	-458.43	1.8	-298.33	2.12	-351.87
166	167	84.60	-1858.58	-148.48	224.67	0	-1027.71	1.8	-541.67	1.8	-322.11	2.12	-399.30
167	167	84.60	-917.40	-140.00	-214.82	0	-1223.20	1.8	235.10	1.8	-36.98	2.12	-72.87
167	168	85.70	-920.89	-116.63	-65.90	0	-1052.98	1.8	63.10	1.8	-50.97	2.12	-100.43
168	168	85.70	-1141.67	-124.29	-184.37	0	-1426.30	1.8	145.14	1.8	-51.39	2.12	-98.82
168	169	86.80	-1141.67	-100.86	-61.67	0	-1287.34	1.8	4.48	1.8	-62.92	2.12	-120.99
169	169	86.80	-1141.67	-100.98	-61.65	0	-1287.32	1.8	4.48	1.8	-62.92	2.12	-120.99
169	170	87.90	-1141.67	-77.61	36.00	0	-1176.20	1.8	-109.05	1.8	-71.97	2.12	-138.40
170	170	87.90	-1141.67	-77.69	36.03	0	-1176.18	1.8	-109.06	1.8	-71.98	2.12	-138.40
170	171	89.00	-1141.67	-54.28	107.72	0	-1093.67	1.8	-195.22	1.8	-78.40	2.12	-150.75



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ-

C. Cuasipermanentes Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-180.20	-197.93	0	-732.51	1.8	41.63	1.8	0.04	2.12	0.07
1	2	1.10	-517.71	-103.22	-73.67	0	-570.46	1.8	-128.94	1.8	-9.01	2.12	-17.76
2	2	1.10	-822.30	-103.12	-266.23	0	-1120.44	1.8	74.64	1.8	-9.00	2.12	-17.74
2	3	2.20	-822.30	-85.90	-162.26	0	-987.81	1.8	-71.08	1.8	-16.57	2.12	-32.64
3	3	2.20	-822.30	-85.82	-162.32	0	-987.87	1.8	-71.07	1.8	-16.56	2.12	-32.62
3	4	3.30	-822.30	-68.57	-77.42	0	-879.29	1.8	-190.83	1.8	-22.67	2.12	-44.68
4	4	3.30	-1039.86	-68.52	-210.62	0	-1265.23	1.8	-55.52	1.8	-22.67	2.12	-44.66
4	5	4.40	-1039.86	-51.29	-144.75	0	-1180.69	1.8	-149.32	1.8	-27.34	2.12	-53.88
5	5	4.40	-1039.86	-51.26	-144.79	0	-1180.73	1.8	-149.31	1.8	-27.34	2.12	-53.87
5	6	5.50	-1039.86	-34.02	-97.90	0	-1120.16	1.8	-217.22	1.8	-30.58	2.12	-60.25
6	6	5.50	-1257.42	-34.00	-228.91	0	-1502.61	1.8	-86.99	1.8	-30.57	2.12	-60.24
6	7	6.60	-1257.42	-16.77	-200.96	0	-1465.97	1.8	-129.03	1.8	-32.38	2.12	-63.80
7	7	6.60	-1257.42	-16.78	-200.99	0	-1467.98	1.8	-146.66	1.8	-32.64	2.12	-62.76
7	8	7.70	-1257.42	0.45	-192.01	0	-1455.87	1.8	-162.80	1.8	-33.02	2.12	-63.49
8	8	7.70	-1257.42	0.44	-192.03	0	-1455.89	1.8	-162.79	1.8	-33.02	2.12	-63.48
8	9	8.80	-1257.42	17.74	-202.02	0	-1466.68	1.8	-152.92	1.8	-31.95	2.12	-61.44
9	9	8.80	-1257.42	17.69	-202.02	0	-1466.68	1.8	-152.92	1.8	-31.95	2.12	-61.44
9	10	9.90	-1257.42	34.95	-230.97	0	-1500.35	1.8	-117.07	1.8	-29.44	2.12	-56.61
10	10	9.90	-1257.42	34.91	-230.97	0	-1500.35	1.8	-117.07	1.8	-29.44	2.12	-56.61
10	11	11.00	-1257.42	52.14	-278.85	0	-1556.86	1.8	-55.26	1.8	-25.49	2.12	-49.02
11	11	11.00	-1257.42	52.09	-278.84	0	-1556.85	1.8	-55.27	1.8	-25.50	2.12	-49.02
11	12	12.10	-1257.42	69.34	-345.63	0	-1636.21	1.8	32.53	1.8	-20.11	2.12	-38.67
12	12	12.10	-1257.42	69.30	-345.62	0	-1636.20	1.8	32.53	1.8	-20.11	2.12	-38.68
12	13	13.20	-1257.42	86.54	-431.37	0	-1738.45	1.8	146.36	1.8	-13.29	2.12	-25.55
13	13	13.20	-1257.42	86.51	-431.35	0	-1738.43	1.8	146.35	1.8	-13.29	2.12	-25.56
13	14	14.30	-1257.42	103.77	-535.99	0	-1863.47	1.8	286.06	1.8	-5.03	2.12	-9.67
14	14	14.30	-1016.08	93.49	-404.99	0	-1468.47	1.8	192.54	1.8	-4.99	2.12	-9.84
14	15	15.40	-1016.27	113.18	-527.75	0	-1618.96	1.8	355.98	1.8	4.63	2.12	9.12
15	15	15.40	-1871.02	121.97	-130.05	0	-1422.39	1.8	-421.44	1.8	-249.16	2.12	-276.97
15	16	16.50	-1871.02	171.43	-278.86	0	-1568.11	1.8	-342.18	1.8	-228.83	2.12	-236.43
16	16	16.50	-1871.02	171.58	-278.77	0	-1563.04	1.8	-347.07	1.8	-233.08	2.12	-242.22
16	17	17.60	-1871.02	194.67	-480.05	0	-1779.56	1.8	-217.51	1.8	-190.97	2.12	-167.76
17	17	17.60	-2480.19	194.79	51.29	0	-1262.70	1.8	-724.40	1.8	-512.84	2.12	-566.96
17	18	18.70	-2480.19	221.23	-177.41	0	-1512.02	1.8	-566.49	1.8	-466.32	2.12	-484.71
18	18	18.70	-2480.18	221.38	-177.25	0	-1511.86	1.8	-566.53	1.8	-466.36	2.12	-484.78
18	19	19.80	-2480.18	249.04	-435.65	0	-1796.41	1.8	-378.76	1.8	-414.97	2.12	-393.90
19	19	19.80	-2175.60	249.24	-242.98	0	-1246.32	1.8	-582.38	1.8	-415.01	2.12	-393.98
19	20	20.90	-2175.60	279.86	-535.34	0	-1570.26	1.8	-363.44	1.8	-357.67	2.12	-292.60
20	20	20.90	-2175.60	280.13	-535.30	0	-1570.22	1.8	-363.45	1.8	-357.68	2.12	-292.61
20	21	22.00	-2175.60	313.63	-861.62	0	-1935.40	1.8	-107.28	1.8	-295.15	2.12	-182.05
21	1021	22.00	-2219.11	-323.86	-890.41	0	-2016.03	1.8	-75.15	1.8	-295.16	2.12	-182.06
21	22	23.40	-2219.11	-283.96	-466.15	0	-1530.57	1.8	-443.03	1.8	-372.12	2.12	-318.14
22	22	23.40	-2219.11	-283.63	-466.17	0	-1530.59	1.8	-443.02	1.8	-372.11	2.12	-318.13
22	23	24.80	-2219.11	-247.87	-94.16	0	-1109.28	1.8	-751.36	1.8	-441.37	2.12	-440.59
23	23	24.80	-2523.70	-247.16	-283.69	0	-1654.44	1.8	-554.85	1.8	-441.35	2.12	-440.55
23	24	26.20	-2523.70	-208.64	33.09	0	-1297.13	1.8	-812.67	1.8	-500.91	2.12	-545.87
24	24	26.20	-1696.97	-208.29	-364.81	0	-1427.55	1.8	-442.05	1.8	-179.01	2.12	-146.61
24	25	27.60	-1696.97	-174.14	-97.26	0	-1128.42	1.8	-651.18	1.8	-230.39	2.12	-237.46
25	25	27.60	-2088.58	-174.00	-329.33	0	-1810.78	1.8	-425.78	1.8	-230.33	2.12	-237.36
25	26	29.00	-2088.58	-115.03	-147.26	0	-1604.91	1.8	-575.62	1.8	-264.36	2.12	-297.53
26	26	29.00	-1242.90	-110.22	-545.00	0	-1858.33	1.8	313.22	1.8	-3.13	2.12	-6.18
26	27	30.40	-1243.14	-86.06	-400.33	0	-1675.05	1.8	103.38	1.8	-13.14	2.12	-25.90
27	27	30.40	-1606.18	-91.87	-599.50	0	-2278.97	1.8	252.87	1.8	-13.24	2.12	-25.46
27	28	31.80	-1605.18	-69.92	-486.26	0	-2138.64	1.8	86.52	1.8	-20.98	2.12	-40.34
28	28	31.80	-1606.18	-69.99	-486.31	0	-2138.68	1.8	86.53	1.8	-20.97	2.12	-40.32
28	29	33.20	-1606.18	-48.06	-403.66	0	-2035.28	1.8	-37.83	1.8	-26.38	2.12	-50.73
29	29	33.20	-1606.18	-48.14	-403.69	0	-2035.31	1.8	-37.82	1.8	-26.38	2.12	-50.72
29	30	34.60	-1606.18	-25.88	-351.94	0	-1969.14	1.8	-120.02	1.8	-29.43	2.12	-56.58
30	30	34.60	-1606.18	-25.96	-351.98	0	-1969.17	1.8	-120.01	1.8	-29.42	2.12	-56.57
30	31	36.00	-1606.18	-3.11	-331.78	0	-1940.74	1.8	-159.96	1.8	-29.98	2.12	-57.66
31	31	36.00	-1606.18	-3.19	-331.78	0	-1940.74	1.8	-159.96	1.8	-29.98	2.12	-57.66
31	32	37.40	-1606.18	18.78	-342.68	0	-1949.68	1.8	-157.74	1.8	-28.14	2.12	-54.12
32	32	37.40	-1606.18	18.68	-342.67	0	-1949.67	1.8	-157.75	1.8	-28.15	2.12	-54.12
32	33	38.80	-1606.18	40.62	-384.17	0	-1995.59	1.8	-113.45	1.8	-23.99	2.12	-46.12
33	33	38.80	-1606.18	40.54	-384.14	0	-1995.57	1.8	-113.45	1.8	-23.99	2.12	-46.13
33	34	40.20	-1606.18	62.48	-456.26	0	-2078.48	1.8	-27.06	1.8	-17.51	2.12	-33.67
34	34	40.20	-1606.18	62.40	-456.22	0	-2078.44	1.8	-27.07	1.8	-17.52	2.12	-33.68
34	35	41.60	-1606.18	84.36	-558.94	0	-2198.31	1.8	101.37	1.8	-8.71	2.12	-16.75
35	35	41.60	-1249.48	80.18	-359.78	0	-1601.22	1.8	-53.37	1.8	-8.65	2.12	-17.05
35	36	43.00	-1249.32	104.13	-492.78	0	-1762.76	1.8	115.86	1.8	2.41	2.12	4.75
36	36	43.00	-2088.58	107.29	-95.04	0	-1559.49	1.8	-574.15	1.8	-279.66	2.12	-324.57
36	37	44.40	-2088.58	165.45	-273.10	0	-1762.50	1.8	-422.15	1.8	-247.06	2.12	-266.93
37	37	44.40	-1696.97	165.60	-41.06	0	-1080.16	1.8	-647.53	1.8	-247.11	2.12	-267.02
37	38	45.80	-1696.97	199.02	-295.51	0	-1367.64	1.8	-438.89	1.8	-199.46	2.12	-182.77
38	38	45.80	-2523.70	199.23	102.42	0	-1237.19	1.8	-809.52	1.8	-521.37	2.12	-582.04

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ-

C. Cuasipermanentes Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	234.13	-199.98	0	-1581.60	1.8	-552.56	1.8	-465.86	2.12	-483.89
39	39	47.20	-2219.11	234.30	-10.34	0	-1036.34	1.8	-749.10	1.8	-465.91	2.12	-483.98
39	40	48.60	-2212.66	273.95	-366.90	0	-1441.72	1.8	-439.94	1.8	-399.25	2.12	-367.44
40	40	48.60	-2212.49	274.30	-366.92	0	-1441.70	1.8	-439.88	1.8	-399.20	2.12	-367.38
40	41	50.00	-2212.49	314.87	-778.50	0	-1915.89	1.8	-72.38	1.8	-325.86	2.12	-237.71
41	1041	50.00	-2212.70	-314.79	-778.50	0	-1915.96	1.8	-72.44	1.8	-325.92	2.12	-237.77
41	42	51.40	-2212.70	-274.22	-367.04	0	-1441.87	1.8	-439.92	1.8	-399.23	2.12	-367.39
42	42	51.40	-2213.30	-273.87	-367.03	0	-1442.05	1.8	-440.10	1.8	-399.39	2.12	-367.55
42	43	52.80	-2213.30	-234.72	-10.49	0	-1034.69	1.8	-747.27	1.8	-464.31	2.12	-482.35
43	43	52.80	-2518.88	-234.50	-200.02	0	-1580.16	1.8	-551.07	1.8	-464.56	2.12	-482.59
43	44	54.20	-2523.70	-199.23	102.41	0	-1237.20	1.8	-809.52	1.8	-521.37	2.12	-582.04
44	44	54.20	-1696.97	-199.02	-295.52	0	-1367.64	1.8	-438.89	1.8	-199.46	2.12	-182.76
44	45	55.60	-1696.97	-165.59	-41.04	0	-1080.14	1.8	-647.54	1.8	-247.12	2.12	-267.03
45	45	55.60	-2088.58	-165.45	-273.10	0	-1762.50	1.8	-422.15	1.8	-247.06	2.12	-266.93
45	46	57.00	-2088.58	-107.29	-95.02	0	-1559.47	1.8	-574.15	1.8	-279.66	2.12	-324.58
46	46	57.00	-1249.32	-104.14	-492.76	0	-1762.74	1.8	115.84	1.8	2.41	2.12	4.75
46	47	58.40	-1251.27	-81.11	-358.87	0	-1601.31	1.8	-56.92	1.8	-8.65	2.12	-17.05
47	47	58.40	-1608.20	-84.31	-558.04	0	-2198.58	1.8	97.65	1.8	-8.71	2.12	-16.75
47	48	59.80	-1608.20	-62.35	-455.39	0	-2078.82	1.8	-30.62	1.8	-17.52	2.12	-33.69
48	48	59.80	-1608.20	-62.42	-455.43	0	-2078.86	1.8	-30.61	1.8	-17.51	2.12	-33.67
48	49	61.20	-1608.20	-40.48	-383.41	0	-1996.10	1.8	-116.79	1.8	-23.99	2.12	-46.13
49	49	61.20	-1608.20	-40.57	-383.44	0	-1996.12	1.8	-116.78	1.8	-23.99	2.12	-46.12
49	50	62.60	-1608.20	-18.63	-342.00	0	-1950.30	1.8	-160.92	1.8	-28.15	2.12	-54.12
50	50	62.60	-1608.20	-18.72	-342.02	0	-1950.32	1.8	-160.92	1.8	-28.14	2.12	-54.12
50	51	64.00	-1609.94	3.27	-331.21	0	-1942.94	1.8	-164.34	1.8	-29.98	2.12	-57.66
51	51	64.00	-1609.94	3.19	-331.21	0	-1942.94	1.8	-164.34	1.8	-29.98	2.12	-57.66
51	52	65.40	-1609.94	26.04	-351.52	0	-1971.54	1.8	-124.14	1.8	-29.42	2.12	-56.57
52	52	65.40	-1609.94	25.96	-351.49	0	-1971.52	1.8	-124.14	1.8	-29.43	2.12	-56.58
52	53	66.80	-1609.94	48.22	-403.35	0	-2037.85	1.8	-41.69	1.8	-26.38	2.12	-50.73
53	53	66.80	-1609.94	48.15	-403.31	0	-2037.82	1.8	-41.70	1.8	-26.39	2.12	-50.74
53	54	68.20	-1609.94	70.07	-486.06	0	-2141.37	1.8	82.90	1.8	-20.97	2.12	-40.33
54	54	68.20	-1609.94	70.00	-486.02	0	-2141.34	1.8	82.89	1.8	-20.98	2.12	-40.34
54	55	69.60	-1609.94	91.95	-599.37	0	-2281.83	1.8	249.50	1.8	-13.24	2.12	-25.46
55	55	69.60	-1246.39	87.95	-400.20	0	-1677.51	1.8	100.42	1.8	-13.14	2.12	-25.90
55	56	71.00	-1242.90	110.23	-545.00	0	-1858.34	1.8	313.24	1.8	-3.14	2.12	-6.18
56	56	71.00	-2088.58	115.03	-147.26	0	-1604.91	1.8	-575.62	1.8	-264.36	2.12	-297.52
56	57	72.40	-2088.58	174.00	-329.32	0	-1810.77	1.8	-425.79	1.8	-230.34	2.12	-237.36
57	57	72.40	-1696.97	174.16	-97.25	0	-1128.41	1.8	-651.18	1.8	-230.40	2.12	-237.47
57	58	73.80	-1696.97	208.31	-364.81	0	-1427.55	1.8	-442.05	1.8	-179.01	2.12	-146.61
58	58	73.80	-2523.70	208.64	33.09	0	-1297.13	1.8	-812.67	1.8	-500.91	2.12	-545.87
58	59	75.20	-2523.70	247.16	-283.72	0	-1654.46	1.8	-554.84	1.8	-441.34	2.12	-440.54
59	59	75.20	-2219.11	247.86	-94.16	0	-1109.28	1.8	-751.36	1.8	-441.37	2.12	-440.59
59	60	76.60	-2215.29	284.09	-466.69	0	-1529.91	1.8	-441.69	1.8	-370.96	2.12	-316.88
60	60	76.60	-2215.34	284.45	-466.76	0	-1530.00	1.8	-441.69	1.8	-370.96	2.12	-316.86
60	61	78.00	-2215.34	324.36	-891.72	0	-2016.13	1.8	-73.61	1.8	-293.82	2.12	-180.46
61	1061	78.00	-2172.15	-313.78	-862.96	0	-1935.63	1.8	-105.83	1.8	-293.89	2.12	-180.52
61	62	79.10	-2172.15	-280.28	-536.49	0	-1570.31	1.8	-362.04	1.8	-356.46	2.12	-291.16
62	62	79.10	-2172.53	-280.03	-536.53	0	-1570.46	1.8	-362.15	1.8	-356.55	2.12	-291.24
62	63	80.20	-2172.53	-249.41	-243.97	0	-1246.33	1.8	-581.14	1.8	-413.94	2.12	-392.72
63	63	80.20	-2477.65	-249.21	-436.62	0	-1796.57	1.8	-377.70	1.8	-414.04	2.12	-392.79
63	64	81.30	-2477.65	-221.56	-178.03	0	-1511.83	1.8	-565.52	1.8	-465.49	2.12	-483.75
64	64	81.30	-2478.35	-221.38	-178.14	0	-1512.16	1.8	-565.71	1.8	-465.64	2.12	-483.89
64	65	82.40	-2478.35	-194.94	50.74	0	-1262.68	1.8	-723.67	1.8	-512.21	2.12	-566.22
65	65	82.40	-1870.06	-194.77	-480.10	0	-1779.05	1.8	-218.08	1.8	-190.60	2.12	-167.29
65	66	83.50	-1870.06	-171.68	-279.13	0	-1563.09	1.8	-346.67	1.8	-232.74	2.12	-241.80
66	66	83.50	-1871.02	-171.45	-279.12	0	-1568.34	1.8	-342.13	1.8	-228.79	2.12	-236.35
66	67	84.60	-1871.02	-122.00	-130.29	0	-1422.60	1.8	-421.40	1.8	-249.12	2.12	-276.89
67	67	84.60	-1016.26	-113.19	-527.99	0	-1619.32	1.8	356.54	1.8	4.63	2.12	9.13
67	68	85.70	-1019.75	-95.94	-403.87	0	-1469.76	1.8	186.93	1.8	-4.99	2.12	-9.84
68	68	85.70	-1261.85	-103.70	-534.87	0	-1865.38	1.8	279.83	1.8	-5.03	2.12	-9.67
68	69	86.80	-1261.85	-86.44	-430.30	0	-1740.46	1.8	140.30	1.8	-13.29	2.12	-25.56
69	69	86.80	-1261.85	-86.47	-430.33	0	-1740.47	1.8	140.31	1.8	-13.29	2.12	-25.55
69	70	87.90	-1261.85	-69.23	-344.69	0	-1638.39	1.8	26.73	1.8	-20.11	2.12	-38.67
70	70	87.90	-1261.85	-69.27	-344.70	0	-1638.40	1.8	26.73	1.8	-20.11	2.12	-38.67
70	71	89.00	-1261.85	-52.02	-277.99	0	-1559.17	1.8	-60.87	1.8	-25.49	2.12	-49.02
71	71	89.00	-1261.85	-52.07	-278.00	0	-1559.18	1.8	-60.87	1.8	-25.49	2.12	-49.02
71	72	90.10	-1261.85	-34.84	-230.20	0	-1502.78	1.8	-122.49	1.8	-29.44	2.12	-56.61
72	72	90.10	-1261.85	-34.88	-230.20	0	-1502.78	1.8	-122.49	1.8	-29.44	2.12	-56.61
72	73	91.20	-1261.85	-17.62	-201.34	0	-1469.25	1.8	-158.14	1.8	-31.95	2.12	-61.44
73	73	91.20	-1261.85	-17.67	-201.32	0	-1469.24	1.8	-158.15	1.8	-31.95	2.12	-61.44
73	74	92.30	-1261.85	-0.37	-191.43	0	-1458.59	1.8	-167.81	1.8	-33.02	2.12	-63.49
74	74	92.30	-1261.85	-0.38	-191.41	0	-1458.57	1.8	-167.82	1.8	-33.02	2.12	-63.49
74	75	93.40	-1261.85	16.85	-200.47	0	-1470.80	1.8	-151.48	1.8	-32.64	2.12	-62.76
75	75	93.40	-1261.85	16.84	-200.44	0	-1468.70	1.8	-133.78	1.8	-32.38	2.12	-63.80
75	76	94.50	-1261.85	34.07	-228.47	0	-1505.46	1.8	-91.56	1.8	-30.57	2.12	-60.24

Combi_to.xls

Programa DINTEL PACADAR S.A.
CUASIPERM1.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ-

C. Cuasipermanentes Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	34.09	-97.46	0	-1123.00	1.8	-221.79	1.8	-30.58	2.12	-60.25
76	77	95.60	-1044.29	51.33	-144.44	0	-1183.71	1.8	-153.68	1.8	-27.34	2.12	-53.87
77	77	95.60	-1044.29	51.36	-144.39	0	-1183.67	1.8	-153.69	1.8	-27.35	2.12	-53.88
77	78	96.70	-1044.29	68.59	-210.38	0	-1268.38	1.8	-59.64	1.8	-22.67	2.12	-44.66
78	78	96.70	-826.73	68.64	-77.17	0	-882.44	1.8	-194.95	1.8	-22.68	2.12	-44.68
78	79	97.80	-826.73	85.89	-162.16	0	-991.15	1.8	-74.99	1.8	-16.56	2.12	-32.62
79	79	97.80	-826.73	85.96	-162.10	0	-991.10	1.8	-75.00	1.8	-16.57	2.12	-32.64
79	80	98.90	-826.73	103.18	-266.14	0	-1123.85	1.8	70.89	1.8	-9.00	2.12	-17.74
80	80	98.90	-522.14	103.29	-73.58	0	-573.87	1.8	-132.69	1.8	-9.01	2.12	-17.76
80	81	100.00	-522.14	180.19	-197.93	0	-732.51	1.8	41.63	1.8	0.04	2.12	0.07
101	101	0.00	-522.14	-150.67	-197.87	0	-732.46	1.8	41.62	1.8	0.03	2.12	0.05
101	102	1.10	-517.71	-97.72	-79.97	0	-575.90	1.8	-127.72	1.8	-7.95	2.12	-15.67
102	102	1.10	-822.30	-97.96	-272.36	0	-1125.74	1.8	75.82	1.8	-7.97	2.12	-15.70
102	103	2.20	-822.30	-81.32	-173.77	0	-997.74	1.8	-68.85	1.8	-14.63	2.12	-28.83
103	103	2.20	-822.30	-81.51	-173.67	0	-997.66	1.8	-68.87	1.8	-14.65	2.12	-28.87
103	104	3.30	-822.30	-64.87	-93.18	0	-892.89	1.8	-187.78	1.8	-20.03	2.12	-39.46
104	104	3.30	-1039.86	-65.00	-226.24	0	-1278.71	1.8	-52.50	1.8	-20.04	2.12	-39.49
104	105	4.40	-1039.86	-48.38	-163.89	0	-1197.20	1.8	-145.64	1.8	-24.13	2.12	-47.54
105	105	4.40	-1039.86	-48.50	-163.82	0	-1197.14	1.8	-145.65	1.8	-24.14	2.12	-47.56
105	106	5.50	-1039.86	-31.86	-119.64	0	-1138.91	1.8	-213.04	1.8	-26.92	2.12	-53.05
106	106	5.50	-1257.42	-31.93	-250.54	0	-1521.28	1.8	-82.82	1.8	-26.93	2.12	-53.07
106	107	6.60	-1257.42	-15.29	-224.56	0	-1486.35	1.8	-124.46	1.8	-28.41	2.12	-55.98
107	107	6.60	-1257.42	-15.34	-224.51	0	-1487.22	1.8	-142.07	1.8	-28.65	2.12	-55.10
107	108	7.70	-1257.42	1.29	-216.79	0	-1476.14	1.8	-157.96	1.8	-28.82	2.12	-55.42
108	108	7.70	-1257.42	1.25	-216.75	0	-1476.11	1.8	-157.97	1.8	-28.83	2.12	-55.43
108	109	8.80	-1257.42	17.89	-227.29	0	-1487.35	1.8	-147.99	1.8	-27.67	2.12	-53.20
109	109	8.80	-1257.42	17.86	-227.26	0	-1487.33	1.8	-148.00	1.8	-27.67	2.12	-53.21
109	110	9.90	-1257.42	34.49	-256.08	0	-1520.89	1.8	-112.17	1.8	-25.19	2.12	-48.43
110	110	9.90	-1257.42	34.48	-256.08	0	-1520.89	1.8	-112.17	1.8	-25.19	2.12	-48.43
110	111	11.00	-1257.42	51.11	-303.14	0	-1576.73	1.8	-50.52	1.8	-21.38	2.12	-41.10
111	111	11.00	-1257.42	51.11	-303.15	0	-1576.74	1.8	-50.52	1.8	-21.37	2.12	-41.10
111	112	12.10	-1257.42	67.75	-368.54	0	-1654.95	1.8	37.00	1.8	-16.23	2.12	-31.20
112	112	12.10	-1257.42	67.74	-368.56	0	-1654.97	1.8	37.01	1.8	-16.22	2.12	-31.20
112	113	13.20	-1257.42	84.36	-452.23	0	-1755.51	1.8	150.41	1.8	-9.75	2.12	-18.75
113	113	13.20	-1257.42	84.34	-452.27	0	-1755.54	1.8	150.41	1.8	-9.74	2.12	-18.74
113	114	14.30	-1257.42	101.00	-554.20	0	-1878.37	1.8	289.61	1.8	-1.94	2.12	-3.73
114	114	14.30	-1016.08	90.74	-423.28	0	-1484.25	1.8	196.08	1.8	-1.92	2.12	-3.78
114	115	15.40	-1016.27	109.88	-542.69	0	-1631.85	1.8	358.87	1.8	7.14	2.12	14.07
115	115	15.40	-1871.02	118.65	-145.09	0	-1435.35	1.8	-418.62	1.8	-246.71	2.12	-272.08
115	116	16.50	-1871.02	162.08	-290.05	0	-1577.75	1.8	-340.08	1.8	-227.01	2.12	-232.79
116	116	16.50	-1871.02	161.92	-290.15	0	-1574.04	1.8	-343.76	1.8	-230.21	2.12	-237.13
116	117	17.60	-1871.02	183.77	-480.21	0	-1779.72	1.8	-217.46	1.8	-190.93	2.12	-167.69
117	117	17.60	-2480.18	183.54	50.95	0	-1263.03	1.8	-724.30	1.8	-512.75	2.12	-566.81
117	118	18.70	-2480.18	210.98	-166.33	0	-1501.29	1.8	-569.71	1.8	-469.13	2.12	-489.67
118	118	18.70	-2480.18	210.78	-166.32	0	-1501.28	1.8	-569.71	1.8	-469.13	2.12	-489.67
118	119	19.80	-2480.18	239.90	-413.87	0	-1775.33	1.8	-385.11	1.8	-420.48	2.12	-403.65
119	119	19.80	-2175.60	239.77	-221.37	0	-1225.40	1.8	-588.68	1.8	-420.48	2.12	-403.65
119	120	20.90	-2175.60	272.38	-504.91	0	-1540.80	1.8	-372.31	1.8	-365.38	2.12	-306.22
120	120	20.90	-2175.60	272.30	-504.91	0	-1540.81	1.8	-372.30	1.8	-365.37	2.12	-306.21
120	121	22.00	-2175.60	304.02	-821.04	0	-1896.13	1.8	-119.10	1.8	-305.42	2.12	-200.21
121	1121	22.00	-2219.11	-314.18	-849.85	0	-1976.77	1.8	-86.98	1.8	-305.42	2.12	-200.21
121	122	23.40	-2219.11	-274.48	-438.70	0	-1504.00	1.8	-451.03	1.8	-379.07	2.12	-330.43
122	122	23.40	-2219.11	-274.55	-438.67	0	-1503.98	1.8	-451.03	1.8	-379.07	2.12	-330.44
122	123	24.80	-2219.11	-239.31	-79.20	0	-1094.80	1.8	-755.72	1.8	-445.16	2.12	-447.29
123	123	24.80	-2523.70	-239.30	-268.55	0	-1639.79	1.8	-559.26	1.8	-445.18	2.12	-447.33
123	124	26.20	-2523.70	-199.50	36.09	0	-1294.23	1.8	-813.55	1.8	-501.67	2.12	-547.22
124	124	26.20	-1696.97	-199.73	-361.58	0	-1424.42	1.8	-442.99	1.8	-179.83	2.12	-148.06
124	125	27.60	-1696.97	-165.86	-106.13	0	-1137.00	1.8	-648.59	1.8	-228.15	2.12	-233.50
125	125	27.60	-2088.58	-166.14	-337.94	0	-1819.12	1.8	-423.27	1.8	-228.15	2.12	-233.50
125	126	29.00	-2088.58	-111.69	-160.04	0	-1617.28	1.8	-571.89	1.8	-261.13	2.12	-291.81
126	126	29.00	-1242.90	-106.85	-557.61	0	-1869.23	1.8	315.68	1.8	-1.02	2.12	-2.00
126	127	30.40	-1243.14	-83.59	-417.00	0	-1689.44	1.8	106.61	1.8	-10.34	2.12	-20.37
127	127	30.40	-1606.18	-89.33	-616.05	0	-2292.51	1.8	256.10	1.8	-10.44	2.12	-20.07
127	128	31.80	-1606.18	-68.12	-505.87	0	-2154.67	1.8	90.34	1.8	-17.66	2.12	-33.95
128	128	31.80	-1606.18	-68.08	-505.81	0	-2154.63	1.8	90.33	1.8	-17.66	2.12	-33.97
128	129	33.20	-1606.18	-46.92	-425.29	0	-2052.97	1.8	-33.63	1.8	-22.72	2.12	-43.68
129	129	33.20	-1606.18	-46.87	-425.25	0	-2052.94	1.8	-33.64	1.8	-22.72	2.12	-43.69
129	130	34.60	-1606.18	-25.40	-374.69	0	-1987.74	1.8	-115.58	1.8	-25.57	2.12	-49.17
130	130	34.60	-1606.18	-25.34	-374.68	0	-1987.73	1.8	-115.58	1.8	-25.57	2.12	-49.17
130	131	36.00	-1606.18	-3.06	-354.93	0	-1959.67	1.8	-155.46	1.8	-26.06	2.12	-50.11
131	131	36.00	-1606.18	-3.00	-354.93	0	-1959.66	1.8	-155.46	1.8	-26.06	2.12	-50.11
131	132	37.40	-1606.18	18.19	-365.57	0	-1968.41	1.8	-153.25	1.8	-24.27	2.12	-46.66
132	132	37.40	-1606.18	18.24	-365.58	0	-1968.42	1.8	-153.25	1.8	-24.26	2.12	-46.65
132	133	38.80	-1606.18	39.43	-405.95	0	-2013.41	1.8	-109.17	1.8	-20.30	2.12	-39.03
133	133	38.80	-1606.18	39.48	-405.98	0	-2013.44	1.8	-109.17	1.8	-20.29	2.12	-39.01

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ-

C. Cuasipermanentes Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	60.65	-476.06	0	-2094.67	1.8	-23.20	1.8	-14.15	2.12	-27.21
134	134	40.20	-1606.18	60.69	-476.11	0	-2094.71	1.8	-23.19	1.8	-14.14	2.12	-27.20
134	135	41.60	-1606.18	81.90	-575.92	0	-2212.20	1.8	104.69	1.8	-5.84	2.12	-11.22
135	135	41.60	-1249.48	77.78	-376.87	0	-1615.97	1.8	-50.06	1.8	-5.78	2.12	-11.38
135	136	43.00	-1249.32	100.88	-505.96	0	-1774.13	1.8	118.41	1.8	4.63	2.12	9.11
136	136	43.00	-2088.58	104.09	-108.37	0	-1572.39	1.8	-570.26	1.8	-276.28	2.12	-318.60
136	137	44.40	-2088.58	157.18	-281.44	0	-1770.56	1.8	-419.72	1.8	-244.95	2.12	-263.20
137	137	44.40	-1696.97	156.94	-49.67	0	-1088.49	1.8	-645.03	1.8	-244.93	2.12	-263.17
137	138	45.80	-1696.97	190.09	-291.77	0	-1364.02	1.8	-439.98	1.8	-200.41	2.12	-184.44
138	138	45.80	-2523.70	189.80	105.92	0	-1233.80	1.8	-810.55	1.8	-522.25	2.12	-583.61
138	139	47.20	-2523.70	225.22	-183.70	0	-1565.84	1.8	-557.31	1.8	-469.98	2.12	-491.18
139	139	47.20	-2219.11	224.98	5.72	0	-1020.79	1.8	-753.79	1.8	-469.97	2.12	-491.17
139	140	48.60	-2212.66	264.86	-338.60	0	-1414.34	1.8	-448.19	1.8	-406.41	2.12	-380.11
140	140	48.60	-2212.49	264.78	-338.69	0	-1414.37	1.8	-448.11	1.8	-406.35	2.12	-380.02
140	141	50.00	-2212.49	305.20	-737.16	0	-1875.89	1.8	-84.42	1.8	-336.33	2.12	-256.21
141	1141	50.00	-2212.71	305.12	-737.17	0	-1875.96	1.8	-84.49	1.8	-336.38	2.12	-256.27
141	142	51.40	-2212.71	-264.70	-338.81	0	-1414.55	1.8	-448.15	1.8	-406.37	2.12	-380.03
142	142	51.40	-2213.30	-264.77	-338.73	0	-1414.66	1.8	-448.35	1.8	-406.55	2.12	-380.22
142	143	52.80	-2213.30	-225.39	5.59	0	-1019.13	1.8	-751.96	1.8	-468.38	2.12	-489.55
143	143	52.80	-2518.88	-225.59	-183.72	0	-1564.38	1.8	-555.82	1.8	-468.69	2.12	-489.88
143	144	54.20	-2523.70	-189.80	105.92	0	-1233.81	1.8	-810.54	1.8	-522.25	2.12	-583.61
144	144	54.20	-1696.97	-190.10	-291.76	0	-1364.01	1.8	-439.98	1.8	-200.41	2.12	-184.44
144	145	55.60	-1696.97	-156.95	-49.65	0	-1088.47	1.8	-645.03	1.8	-244.94	2.12	-263.18
145	145	55.60	-2088.58	-157.18	-281.43	0	-1770.55	1.8	-419.72	1.8	-244.95	2.12	-263.20
145	146	57.00	-2088.58	-104.09	-108.36	0	-1572.38	1.8	-570.27	1.8	-276.28	2.12	-318.61
146	146	57.00	-1249.32	-100.89	-505.95	0	-1774.13	1.8	118.41	1.8	4.62	2.12	9.11
146	147	58.40	-1251.27	-78.71	-375.95	0	-1616.04	1.8	-53.64	1.8	-5.78	2.12	-11.39
147	147	58.40	-1608.20	-81.84	-575.00	0	-2212.45	1.8	100.93	1.8	-5.84	2.12	-11.22
147	148	59.80	-1608.20	-60.63	-475.30	0	-2095.11	1.8	-26.73	1.8	-14.14	2.12	-27.20
148	148	59.80	-1608.20	-60.59	-475.24	0	-2095.06	1.8	-26.75	1.8	-14.15	2.12	-27.21
148	149	61.20	-1608.20	-39.42	-405.24	0	-2013.95	1.8	-112.53	1.8	-20.29	2.12	-39.02
149	149	61.20	-1608.20	-39.37	-405.21	0	-2013.93	1.8	-112.53	1.8	-20.30	2.12	-39.03
149	150	62.60	-1608.20	-18.19	-364.91	0	-1969.05	1.8	-156.45	1.8	-24.26	2.12	-46.66
150	150	62.60	-1608.20	-18.13	-364.89	0	-1969.03	1.8	-156.45	1.8	-24.27	2.12	-46.66
150	151	64.00	-1609.94	3.08	-354.37	0	-1961.88	1.8	-159.82	1.8	-26.06	2.12	-50.11
151	151	64.00	-1609.94	3.14	-354.37	0	-1961.88	1.8	-159.82	1.8	-26.06	2.12	-50.11
151	152	65.40	-1609.94	25.42	-374.23	0	-1990.12	1.8	-119.71	1.8	-25.57	2.12	-49.17
152	152	65.40	-1609.94	25.48	-374.23	0	-1990.12	1.8	-119.70	1.8	-25.57	2.12	-49.17
152	153	66.80	-1609.94	46.94	-424.91	0	-2055.48	1.8	-37.50	1.8	-22.72	2.12	-43.69
153	153	66.80	-1609.94	47.00	-424.95	0	-2055.51	1.8	-37.50	1.8	-22.72	2.12	-43.68
153	154	68.20	-1609.94	68.16	-505.59	0	-2157.35	1.8	86.73	1.8	-17.66	2.12	-33.97
154	154	68.20	-1609.94	68.20	-505.64	0	-2157.39	1.8	86.74	1.8	-17.66	2.12	-33.95
154	155	69.60	-1609.94	89.41	-615.93	0	-2295.39	1.8	252.76	1.8	-10.44	2.12	-20.07
155	155	69.60	-1246.39	85.46	-416.88	0	-1691.92	1.8	103.67	1.8	-10.34	2.12	-20.37
155	156	71.00	-1242.90	106.85	-557.62	0	-1869.24	1.8	315.70	1.8	-1.02	2.12	-2.00
156	156	71.00	-2088.58	111.69	-160.04	0	-1617.28	1.8	-571.89	1.8	-261.13	2.12	-291.81
156	157	72.40	-2088.58	166.15	-337.93	0	-1819.10	1.8	-423.28	1.8	-228.16	2.12	-233.51
157	157	72.40	-1696.97	165.87	-106.11	0	-1136.98	1.8	-648.60	1.8	-228.15	2.12	-233.50
157	158	73.80	-1696.97	199.74	-361.58	0	-1424.43	1.8	-442.99	1.8	-179.83	2.12	-148.06
158	158	73.80	-2523.70	199.50	36.08	0	-1294.24	1.8	-813.54	1.8	-501.67	2.12	-547.21
158	159	75.20	-2523.70	239.31	-268.56	0	-1639.80	1.8	-559.26	1.8	-445.18	2.12	-447.32
159	159	75.20	-2219.11	239.30	-79.19	0	-1094.79	1.8	-755.73	1.8	-445.16	2.12	-447.29
159	160	76.60	-2215.29	275.02	-439.19	0	-1503.30	1.8	-449.71	1.8	-377.92	2.12	-329.18
160	160	76.60	-2215.34	274.97	-439.32	0	-1503.44	1.8	-449.68	1.8	-377.90	2.12	-329.14
160	161	78.00	-2215.34	314.67	-851.15	0	-1976.87	1.8	-85.43	1.8	-304.09	2.12	-198.62
161	1161	78.00	-2172.15	-304.17	-822.38	0	-1896.36	1.8	-117.65	1.8	-304.16	2.12	-198.68
161	162	79.10	-2172.15	-272.46	-506.09	0	-1540.88	1.8	-370.90	1.8	-364.15	2.12	-304.76
162	162	79.10	-2172.53	-272.54	-506.09	0	-1541.00	1.8	-371.02	1.8	-364.25	2.12	-304.86
162	163	80.20	-2172.53	-239.94	-222.37	0	-1225.43	1.8	-587.44	1.8	-419.41	2.12	-402.38
163	163	80.20	-2477.65	-240.06	-414.84	0	-1775.49	1.8	-384.05	1.8	-419.56	2.12	-402.54
163	164	81.30	-2477.65	-210.94	-167.11	0	-1501.27	1.8	-568.70	1.8	-468.25	2.12	-488.64
164	164	81.30	-2478.35	-211.13	-167.06	0	-1501.43	1.8	-568.93	1.8	-468.45	2.12	-488.85
164	165	82.40	-2478.35	-183.69	50.39	0	-1263.01	1.8	-723.57	1.8	-512.12	2.12	-566.07
165	165	82.40	-1870.06	-183.87	-480.24	0	-1779.19	1.8	-218.03	1.8	-190.56	2.12	-167.22
165	166	83.50	-1870.06	-162.02	-290.51	0	-1574.10	1.8	-343.36	1.8	-229.86	2.12	-236.71
166	166	83.50	-1871.02	-162.11	-290.32	0	-1577.98	1.8	-340.03	1.8	-226.97	2.12	-232.71
166	167	84.60	-1871.02	-118.68	-145.33	0	-1435.55	1.8	-418.58	1.8	-246.67	2.12	-272.00
167	167	84.60	-1016.26	-109.88	-542.93	0	-1632.21	1.8	359.43	1.8	7.14	2.12	14.08
167	168	85.70	-1019.75	-93.20	-422.17	0	-1485.56	1.8	190.47	1.8	-1.92	2.12	-3.78
168	168	85.70	-1261.85	-100.93	-553.09	0	-1880.29	1.8	283.39	1.8	-1.94	2.12	-3.73
168	169	86.80	-1261.85	-84.28	-451.24	0	-1757.58	1.8	144.39	1.8	-9.74	2.12	-18.74
169	169	86.80	-1261.85	-84.29	-451.20	0	-1757.55	1.8	144.38	1.8	-9.75	2.12	-18.75
169	170	87.90	-1261.85	-67.67	-367.62	0	-1657.14	1.8	31.18	1.8	-16.22	2.12	-31.20
170	170	87.90	-1261.85	-67.68	-367.60	0	-1657.12	1.8	31.18	1.8	-16.23	2.12	-31.20
170	171	89.00	-1261.85	-51.04	-302.30	0	-1579.04	1.8	-56.15	1.8	-21.37	2.12	-41.10

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.T0.MZ-

C. Cuasipermanentes Mz-

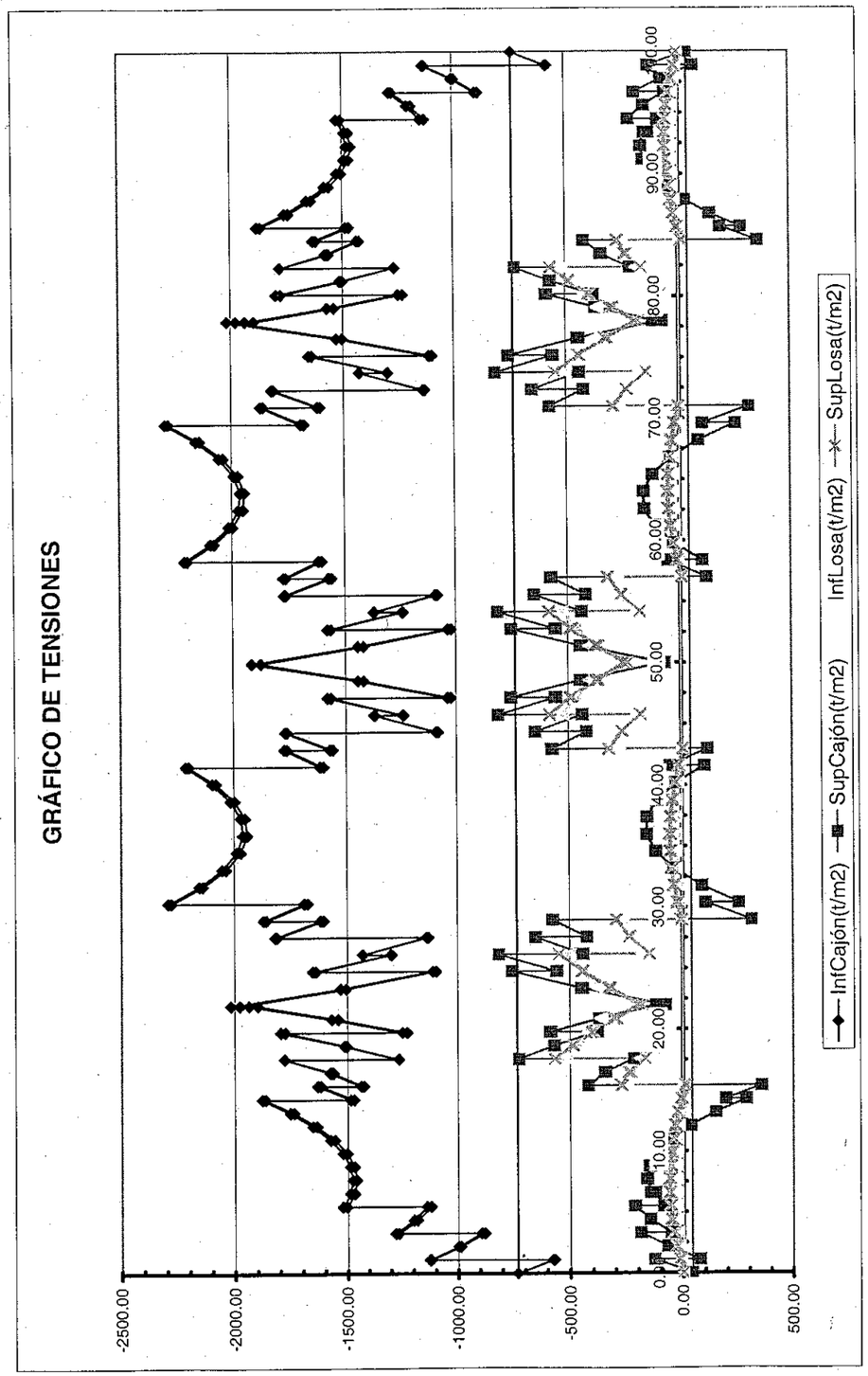
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	-51.05	-302.28	0	-1579.03	1.8	-56.15	1.8	-21.38	2.12	-41.10
171	172	90.10	-1261.85	-34.41	-255.31	0	-1523.32	1.8	-117.59	1.8	-25.19	2.12	-48.43
172	172	90.10	-1261.85	-34.42	-255.31	0	-1523.33	1.8	-117.59	1.8	-25.19	2.12	-48.43
172	173	91.20	-1261.85	-17.79	-226.59	0	-1489.90	1.8	-153.22	1.8	-27.67	2.12	-53.21
173	173	91.20	-1261.85	-17.83	-226.60	0	-1489.92	1.8	-153.21	1.8	-27.67	2.12	-53.20
173	174	92.30	-1261.85	-1.18	-216.15	0	-1478.81	1.8	-162.99	1.8	-28.83	2.12	-55.43
174	174	92.30	-1261.85	-1.22	-216.18	0	-1478.84	1.8	-162.98	1.8	-28.82	2.12	-55.42
174	175	93.40	-1261.85	15.41	-224.00	0	-1490.04	1.8	-146.89	1.8	-28.65	2.12	-55.09
175	175	93.40	-1261.85	15.36	-224.04	0	-1489.07	1.8	-129.21	1.8	-28.41	2.12	-55.98
175	176	94.50	-1261.85	32.00	-250.11	0	-1524.14	1.8	-87.37	1.8	-26.93	2.12	-53.07
176	176	94.50	-1044.29	31.92	-119.20	0	-1141.77	1.8	-217.58	1.8	-26.92	2.12	-53.05
176	177	95.60	-1044.29	48.56	-163.47	0	-1200.13	1.8	-150.00	1.8	-24.14	2.12	-47.56
177	177	95.60	-1044.29	48.45	-163.55	0	-1200.20	1.8	-149.98	1.8	-24.12	2.12	-47.54
177	178	96.70	-1044.29	65.08	-226.00	0	-1281.86	1.8	-56.62	1.8	-20.04	2.12	-39.49
178	178	96.70	-826.73	64.93	-92.93	0	-896.04	1.8	-191.90	1.8	-20.03	2.12	-39.46
178	179	97.80	-826.73	81.58	-173.51	0	-1000.95	1.8	-72.79	1.8	-14.65	2.12	-28.87
179	179	97.80	-826.73	81.39	-173.61	0	-1001.03	1.8	-72.77	1.8	-14.63	2.12	-28.83
179	180	98.90	-826.73	98.03	-272.28	0	-1129.14	1.8	72.08	1.8	-7.97	2.12	-15.70
180	180	98.90	-522.14	97.79	-79.88	0	-579.30	1.8	-131.47	1.8	-7.95	2.12	-15.67
180	181	100.00	-522.14	150.66	-197.87	0	-732.46	1.8	41.62	1.8	0.03	2.12	0.05

Programa DINTEL PACADAR S.A.
CUASIPERM1.T0.MZ-

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ+

C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-144.14	-178.17	0	-661.96	1.8	37.49	1.8	-0.12	2.12	-0.24
1	2	1.10	-476.85	-233.28	95.91	0	-376.74	1.8	-171.95	1.8	-34.14	2.12	-67.27
2	2	1.10	-752.42	-233.59	-78.11	0	-874.17	1.8	12.21	1.8	-34.16	2.12	-67.31
2	3	2.20	-752.42	-200.92	158.23	0	-626.33	1.8	-161.91	1.8	-63.76	2.12	-125.65
3	3	2.20	-752.42	-201.18	158.35	0	-626.24	1.8	-161.93	1.8	-63.78	2.12	-125.68
3	4	3.30	-752.42	-168.55	357.45	0	-418.15	1.8	-306.57	1.8	-88.88	2.12	-175.14
4	4	3.30	-949.26	-168.72	237.12	0	-767.16	1.8	-184.18	1.8	-88.91	2.12	-175.19
4	5	4.40	-949.26	-131.18	398.81	0	-598.98	1.8	-299.30	1.8	-109.47	2.12	-215.72
5	5	4.40	-949.26	-131.27	398.93	0	-598.88	1.8	-299.33	1.8	-109.49	2.12	-215.76
5	6	5.50	-949.26	-96.97	529.16	0	-465.43	1.8	-386.14	1.8	-126.53	2.12	-249.32
6	6	5.50	-1146.10	-97.06	410.74	0	-811.36	1.8	-268.33	1.8	-126.54	2.12	-249.35
6	7	6.60	-1146.10	-64.34	503.90	0	-717.49	1.8	-325.77	1.8	-139.09	2.12	-274.08
7	7	6.60	-1146.10	-64.42	503.98	0	-751.02	1.8	-343.11	1.8	-140.25	2.12	-269.69
7	8	7.70	-1146.10	-31.76	559.98	0	-699.54	1.8	-371.20	1.8	-148.38	2.12	-285.32
8	8	7.70	-1146.10	-31.75	560.04	0	-699.49	1.8	-371.21	1.8	-148.39	2.12	-285.34
8	9	8.80	-1146.10	0.66	577.96	0	-686.53	1.8	-369.56	1.8	-151.84	2.12	-291.97
9	9	8.80	-1146.10	0.71	578.01	0	-686.49	1.8	-369.57	1.8	-151.85	2.12	-291.98
9	10	9.90	-1146.10	33.28	564.20	0	-706.86	1.8	-339.45	1.8	-151.69	2.12	-291.67
10	10	9.90	-1146.10	33.36	564.21	0	-706.85	1.8	-339.46	1.8	-151.69	2.12	-291.67
10	11	11.00	-1146.10	66.11	513.57	0	-764.70	1.8	-279.89	1.8	-147.05	2.12	-282.75
11	11	11.00	-1146.10	66.17	513.59	0	-764.69	1.8	-279.89	1.8	-147.05	2.12	-282.76
11	12	12.10	-1146.10	98.86	425.89	0	-860.23	1.8	-190.79	1.8	-137.90	2.12	-265.17
12	12	12.10	-1146.10	98.97	425.87	0	-860.24	1.8	-190.78	1.8	-137.90	2.12	-265.16
12	13	13.20	-1146.10	131.39	300.58	0	-993.92	1.8	-72.02	1.8	-124.15	2.12	-238.73
13	13	13.20	-1146.10	131.48	300.55	0	-993.94	1.8	-72.01	1.8	-124.15	2.12	-238.72
13	14	14.30	-1146.10	164.23	141.94	0	-1162.21	1.8	75.45	1.8	-106.51	2.12	-204.81
14	14	14.30	-924.56	159.34	260.36	0	-773.63	1.8	-5.46	1.8	-105.63	2.12	-208.14
14	15	15.40	-917.39	189.52	63.37	0	-983.23	1.8	181.76	1.8	-83.79	2.12	-165.11
15	15	15.40	-1858.58	198.21	502.83	0	-788.10	1.8	-593.85	1.8	-367.43	2.12	-489.67
15	16	16.50	-1858.58	198.46	275.12	0	-1001.78	1.8	-499.78	1.8	-334.25	2.12	-423.50
16	16	16.50	-1858.58	198.33	274.93	0	-943.33	1.8	-556.94	1.8	-383.89	2.12	-490.99
16	17	17.60	-1858.58	213.96	44.75	0	-1187.80	1.8	-419.04	1.8	-334.46	2.12	-403.58
17	17	17.60	-2575.51	213.97	604.84	0	-694.44	1.8	-951.84	1.8	-690.10	2.12	-844.62
17	18	18.70	-2575.51	211.56	363.58	0	-955.90	1.8	-790.27	1.8	-640.41	2.12	-756.75
18	18	18.70	-2575.50	211.57	363.12	0	-956.34	1.8	-790.13	1.8	-640.29	2.12	-756.54
18	19	19.80	-2575.50	213.53	128.05	0	-1218.32	1.8	-609.16	1.8	-594.80	2.12	-676.11
19	19	19.80	-2299.92	213.48	301.63	0	-721.33	1.8	-793.17	1.8	-594.65	2.12	-675.85
19	20	20.90	-2299.92	215.48	65.44	0	-990.90	1.8	-590.60	1.8	-551.53	2.12	-599.60
20	20	20.90	-2299.92	215.09	65.47	0	-990.88	1.8	-590.61	1.8	-551.53	2.12	-599.61
20	21	22.00	-2299.92	224.45	-176.74	0	-1274.65	1.8	-358.95	1.8	-510.29	2.12	-526.69
21	1021	22.00	-2339.29	-219.56	-202.82	0	-1347.63	1.8	-329.88	1.8	-510.29	2.12	-526.69
21	22	23.40	-2339.29	-198.79	94.42	0	-985.11	1.8	-660.73	1.8	-555.10	2.12	-605.92
22	22	23.40	-2339.29	-199.21	94.35	0	-985.17	1.8	-660.71	1.8	-555.09	2.12	-605.89
22	23	24.80	-2339.29	-193.81	370.83	0	-656.32	1.8	-941.22	1.8	-600.16	2.12	-685.60
23	23	24.80	-2614.86	-194.30	199.43	0	-1149.49	1.8	-763.44	1.8	-600.16	2.12	-685.60
23	24	26.20	-2614.86	-215.33	482.24	0	-825.05	1.8	-1011.37	1.8	-651.13	2.12	-775.72
24	24	26.20	-1701.11	-216.06	43.46	0	-968.23	1.8	-602.02	1.8	-295.60	2.12	-334.88
24	25	27.60	-1701.11	-206.58	336.30	0	-644.62	1.8	-818.51	1.8	-353.38	2.12	-437.05
25	25	27.60	-2055.42	-206.62	127.22	0	-1261.13	1.8	-614.85	1.8	-353.55	2.12	-437.35
25	26	29.00	-2055.42	-217.86	440.58	0	-928.21	1.8	-802.94	1.8	-420.81	2.12	-556.27
26	26	29.00	-1122.96	-212.88	1.27	0	-1233.68	1.8	132.34	1.8	-81.48	2.12	-160.55
26	27	30.40	-1129.71	-175.27	274.67	0	-944.88	1.8	-106.84	1.8	-113.20	2.12	-223.06
27	27	30.40	-1460.38	-177.24	94.68	0	-1522.44	1.8	25.42	1.8	-114.16	2.12	-219.51
27	28	31.80	-1460.38	-134.87	308.80	0	-1299.90	1.8	-159.69	1.8	-139.07	2.12	-267.42
28	28	31.80	-1460.38	-134.69	308.92	0	-1299.81	1.8	-159.71	1.8	-139.09	2.12	-267.46
28	29	33.20	-1460.38	-88.54	464.77	0	-1136.85	1.8	-297.42	1.8	-156.99	2.12	-301.87
29	29	33.20	-1460.38	-88.32	464.88	0	-1136.75	1.8	-297.45	1.8	-157.01	2.12	-301.91
29	30	34.60	-1460.38	-51.95	563.81	0	-1032.30	1.8	-387.91	1.8	-168.13	2.12	-323.28
30	30	34.60	-1460.38	-51.71	563.85	0	-1032.27	1.8	-387.92	1.8	-168.14	2.12	-323.30
30	31	36.00	-1460.38	-9.85	602.10	0	-989.38	1.8	-430.45	1.8	-171.83	2.12	-330.41
31	31	36.00	-1460.38	-9.65	602.11	0	-989.37	1.8	-430.45	1.8	-171.84	2.12	-330.42
31	32	37.40	-1460.38	36.89	584.69	0	-1003.96	1.8	-426.03	1.8	-168.96	2.12	-324.89
32	32	37.40	-1460.38	37.10	584.67	0	-1003.98	1.8	-426.03	1.8	-168.96	2.12	-324.88
32	33	38.80	-1460.38	73.47	506.49	0	-1080.21	1.8	-373.63	1.8	-158.66	2.12	-305.08
33	33	38.80	-1460.38	73.70	506.40	0	-1080.28	1.8	-373.62	1.8	-158.64	2.12	-305.04
33	34	40.20	-1460.38	119.88	371.40	0	-1214.93	1.8	-274.02	1.8	-141.57	2.12	-272.23
34	34	40.20	-1460.38	120.07	371.28	0	-1215.03	1.8	-274.00	1.8	-141.55	2.12	-272.19
34	35	41.60	-1460.38	162.44	177.84	0	-1409.41	1.8	-126.91	1.8	-117.45	2.12	-225.84
35	35	41.60	-1135.74	162.02	357.81	0	-836.36	1.8	-264.09	1.8	-116.46	2.12	-229.48
35	36	43.00	-1128.92	200.07	103.81	0	-1098.67	1.8	-60.27	1.8	-85.50	2.12	-168.49
36	36	43.00	-2055.42	203.51	543.14	0	-834.06	1.8	-816.14	1.8	-448.85	2.12	-605.84
36	37	44.40	-2055.42	198.55	252.37	0	-1146.15	1.8	-631.30	1.8	-387.72	2.12	-497.76
37	37	44.40	-1701.11	198.60	461.52	0	-529.56	1.8	-834.99	1.8	-387.57	2.12	-497.50
37	38	45.80	-1701.11	210.96	175.55	0	-847.55	1.8	-617.16	1.8	-331.94	2.12	-399.13
38	38	45.80	-2614.86	210.66	614.23	0	-704.47	1.8	-1026.48	1.8	-687.44	2.12	-839.93

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.T0.MZ+

5. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	196.48	332.01	0	-1029.35	1.8	-775.39	1.8	-637.04	2.12	-750.81
39	39	47.20	-2339.29	196.69	503.00	0	-536.58	1.8	-953.05	1.8	-636.94	2.12	-750.62
39	40	48.60	-2345.74	195.44	227.61	0	-867.39	1.8	-671.52	1.8	-594.28	2.12	-673.87
40	40	48.60	-2345.92	195.01	227.71	0	-867.35	1.8	-671.60	1.8	-594.35	2.12	-673.96
40	41	50.00	-2345.92	214.93	-64.40	0	-1225.93	1.8	-338.90	1.8	-551.25	2.12	-597.75
41	1041	50.00	-2345.70	-215.02	-64.40	0	-1225.86	1.8	-338.84	1.8	-551.19	2.12	-597.69
41	42	51.40	-2345.70	-195.10	227.84	0	-867.16	1.8	-671.57	1.8	-594.33	2.12	-673.96
42	42	51.40	-2345.10	-195.52	227.75	0	-867.06	1.8	-671.36	1.8	-594.14	2.12	-673.76
42	43	52.80	-2345.10	-196.28	503.14	0	-538.23	1.8	-954.88	1.8	-638.53	2.12	-752.24
43	43	52.80	-2619.68	-196.12	332.04	0	-1030.80	1.8	-776.89	1.8	-638.34	2.12	-752.11
43	44	54.20	-2614.86	-210.66	614.23	0	-704.47	1.8	-1026.48	1.8	-687.44	2.12	-839.93
44	44	54.20	-1701.11	-210.96	175.55	0	-847.55	1.8	-617.16	1.8	-331.94	2.12	-399.13
44	45	55.60	-1701.11	-198.61	461.55	0	-529.53	1.8	-835.00	1.8	-387.58	2.12	-497.51
45	45	55.60	-2055.42	-198.55	252.38	0	-1146.14	1.8	-631.30	1.8	-387.72	2.12	-497.77
45	46	57.00	-2055.42	-203.51	543.16	0	-834.04	1.8	-816.15	1.8	-448.85	2.12	-605.85
46	46	57.00	-1128.92	-200.08	103.84	0	-1098.64	1.8	-60.30	1.8	-85.51	2.12	-168.49
46	47	58.40	-1133.95	-161.11	356.94	0	-836.24	1.8	-260.55	1.8	-116.46	2.12	-229.48
47	47	58.40	-1458.36	-162.50	176.97	0	-1409.12	1.8	-123.18	1.8	-117.45	2.12	-225.84
47	48	59.80	-1458.36	-120.13	370.51	0	-1214.60	1.8	-270.46	1.8	-141.56	2.12	-272.20
48	48	59.80	-1458.36	-119.94	370.62	0	-1214.50	1.8	-270.49	1.8	-141.58	2.12	-272.24
48	49	61.20	-1458.36	-73.75	505.66	0	-1079.77	1.8	-370.24	1.8	-158.64	2.12	-305.05
49	49	61.20	-1458.36	-73.53	505.74	0	-1079.71	1.8	-370.25	1.8	-158.66	2.12	-305.07
49	50	62.60	-1458.36	-37.16	584.03	0	-1003.33	1.8	-422.86	1.8	-168.96	2.12	-324.89
50	50	62.60	-1458.36	-36.93	584.08	0	-1003.29	1.8	-422.87	1.8	-168.97	2.12	-324.91
50	51	64.00	-1456.62	9.57	601.56	0	-987.16	1.8	-426.07	1.8	-171.84	2.12	-330.42
51	51	64.00	-1456.62	9.77	601.56	0	-987.16	1.8	-426.07	1.8	-171.84	2.12	-330.42
51	52	65.40	-1456.62	51.62	563.42	0	-1029.87	1.8	-383.80	1.8	-168.14	2.12	-323.31
52	52	65.40	-1456.62	51.86	563.36	0	-1029.92	1.8	-383.79	1.8	-168.13	2.12	-323.29
52	53	66.80	-1456.62	88.24	464.58	0	-1134.17	1.8	-293.59	1.8	-157.02	2.12	-301.92
53	53	66.80	-1456.62	88.46	464.47	0	-1134.27	1.8	-293.57	1.8	-157.00	2.12	-301.88
53	54	68.20	-1456.62	134.61	308.74	0	-1297.04	1.8	-156.14	1.8	-139.10	2.12	-267.47
54	54	68.20	-1456.62	134.79	308.63	0	-1297.14	1.8	-156.12	1.8	-139.08	2.12	-267.43
54	55	69.60	-1456.62	177.16	94.59	0	-1519.53	1.8	28.74	1.8	-114.16	2.12	-219.52
55	55	69.60	-1126.45	173.40	274.60	0	-942.36	1.8	-103.93	1.8	-113.20	2.12	-223.07
55	56	71.00	-1122.96	212.90	1.29	0	-1233.67	1.8	132.35	1.8	-81.48	2.12	-160.56
56	56	71.00	-2055.42	217.85	440.59	0	-928.19	1.8	-802.94	1.8	-420.81	2.12	-556.28
56	57	72.40	-2055.42	206.62	127.24	0	-1261.11	1.8	-614.85	1.8	-353.56	2.12	-437.36
57	57	72.40	-1701.11	206.60	336.32	0	-644.60	1.8	-818.52	1.8	-353.39	2.12	-437.05
57	58	73.80	-1701.11	216.07	43.45	0	-968.24	1.8	-602.01	1.8	-295.60	2.12	-334.87
58	58	73.80	-2614.86	215.32	482.23	0	-825.06	1.8	-1011.36	1.8	-651.13	2.12	-775.72
58	59	75.20	-2614.86	194.31	199.42	0	-1149.50	1.8	-763.44	1.8	-600.16	2.12	-685.59
59	59	75.20	-2339.29	193.80	370.82	0	-656.33	1.8	-941.21	1.8	-600.16	2.12	-685.59
59	60	76.60	-2343.12	198.73	94.86	0	-985.86	1.8	-662.04	1.8	-556.24	2.12	-607.14
60	60	76.60	-2343.06	198.30	95.00	0	-985.71	1.8	-662.06	1.8	-556.26	2.12	-607.19
60	61	78.00	-2343.06	219.07	-201.53	0	-1347.55	1.8	-331.41	1.8	-511.63	2.12	-528.27
61	1061	78.00	-2303.37	-224.30	-175.43	0	-1274.45	1.8	-360.39	1.8	-511.55	2.12	-528.20
61	62	79.10	-2303.37	-214.94	66.61	0	-990.84	1.8	-592.00	1.8	-552.75	2.12	-601.05
62	62	79.10	-2302.99	-215.32	66.58	0	-990.74	1.8	-591.88	1.8	-552.64	2.12	-600.93
62	63	80.20	-2302.99	-213.33	302.62	0	-721.32	1.8	-794.41	1.8	-595.72	2.12	-677.11
63	63	80.20	-2578.03	-213.37	129.00	0	-1218.17	1.8	-610.22	1.8	-595.72	2.12	-677.22
63	64	81.30	-2578.03	-211.41	363.91	0	-956.36	1.8	-791.14	1.8	-641.17	2.12	-757.58
64	64	81.30	-2577.33	-211.41	364.29	0	-955.78	1.8	-791.04	1.8	-641.07	2.12	-757.56
64	65	82.40	-2577.33	-213.82	605.40	0	-694.46	1.8	-952.57	1.8	-690.73	2.12	-845.36
65	65	82.40	-1859.54	-213.86	45.60	0	-1187.03	1.8	-420.38	1.8	-334.83	2.12	-404.04
65	66	83.50	-1859.54	-198.23	275.30	0	-943.26	1.8	-557.35	1.8	-384.24	2.12	-491.42
66	66	83.50	-1858.58	-198.46	275.38	0	-1001.56	1.8	-499.83	1.8	-334.29	2.12	-423.58
66	67	84.60	-1858.58	-198.20	503.08	0	-787.88	1.8	-593.89	1.8	-367.47	2.12	-489.75
67	67	84.60	-917.40	-189.50	63.65	0	-982.84	1.8	181.20	1.8	-83.80	2.12	-165.13
67	68	85.70	-920.89	-156.85	259.29	0	-772.29	1.8	0.15	1.8	-105.64	2.12	-208.16
68	68	85.70	-1141.67	-164.32	140.84	0	-1160.28	1.8	81.67	1.8	-106.52	2.12	-204.82
68	69	86.80	-1141.67	-131.57	299.55	0	-991.87	1.8	-66.02	1.8	-124.15	2.12	-238.73
69	69	86.80	-1141.67	-131.49	299.60	0	-991.82	1.8	-66.03	1.8	-124.16	2.12	-238.74
69	70	87.90	-1141.67	-99.06	424.94	0	-858.07	1.8	-184.94	1.8	-137.91	2.12	-265.17
70	70	87.90	-1141.67	-98.94	424.97	0	-858.04	1.8	-184.95	1.8	-137.91	2.12	-265.18
70	71	89.00	-1141.67	-66.27	512.74	0	-762.38	1.8	-274.25	1.8	-147.06	2.12	-282.77
71	71	89.00	-1141.67	-66.20	512.75	0	-762.38	1.8	-274.25	1.8	-147.06	2.12	-282.77
71	72	90.10	-1141.67	-33.45	563.48	0	-704.38	1.8	-334.04	1.8	-151.70	2.12	-291.69
72	72	90.10	-1141.67	-33.37	563.46	0	-704.39	1.8	-334.04	1.8	-151.69	2.12	-291.68
72	73	91.20	-1141.67	-0.81	577.37	0	-683.89	1.8	-364.36	1.8	-151.86	2.12	-292.00
73	73	91.20	-1141.67	-0.75	577.33	0	-683.93	1.8	-364.35	1.8	-151.85	2.12	-291.98
73	74	92.30	-1141.67	31.66	559.48	0	-696.76	1.8	-366.19	1.8	-148.40	2.12	-285.35
74	74	92.30	-1141.67	31.66	559.42	0	-696.81	1.8	-366.18	1.8	-148.39	2.12	-285.33
74	75	93.40	-1141.67	64.32	503.51	0	-748.16	1.8	-338.29	1.8	-140.26	2.12	-269.70
75	75	93.40	-1141.67	64.25	503.41	0	-714.74	1.8	-321.03	1.8	-139.10	2.12	-274.09
75	76	94.50	-1141.67	96.97	410.35	0	-808.46	1.8	-263.81	1.8	-126.54	2.12	-249.35

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.T0.MZ+

C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	96.88	528.76	0	-462.53	1.8	-381.62	1.8	-126.53	2.12	-249.33
76	77	95.60	-944.83	131.18	398.62	0	-595.84	1.8	-295.01	1.8	-109.50	2.12	-215.77
77	77	95.60	-944.83	131.08	398.51	0	-595.94	1.8	-294.99	1.8	-109.48	2.12	-215.73
77	78	96.70	-944.83	168.63	236.85	0	-764.05	1.8	-180.01	1.8	-88.91	2.12	-175.19
78	78	96.70	-747.99	168.46	357.20	0	-415.01	1.8	-302.41	1.8	-88.89	2.12	-175.15
78	79	97.80	-747.99	201.09	158.15	0	-622.99	1.8	-157.96	1.8	-63.78	2.12	-125.68
79	79	97.80	-747.99	200.83	158.05	0	-623.08	1.8	-157.94	1.8	-63.76	2.12	-125.65
79	80	98.90	-747.99	233.50	-78.20	0	-870.76	1.8	15.95	1.8	-34.16	2.12	-67.31
80	80	98.90	-472.42	233.19	95.83	0	-373.33	1.8	-168.20	1.8	-34.14	2.12	-67.27
80	81	100.00	-472.42	144.13	-178.17	0	-661.96	1.8	37.49	1.8	-0.12	2.12	-0.24
101	101	0.00	-472.42	-158.27	-178.23	0	-662.02	1.8	37.50	1.8	-0.11	2.12	-0.22
101	102	1.10	-476.85	-248.28	112.63	0	-362.31	1.8	-175.18	1.8	-36.95	2.12	-72.81
102	102	1.10	-752.42	-247.40	-61.83	0	-860.12	1.8	9.05	1.8	-36.90	2.12	-72.71
102	103	2.20	-752.42	-213.57	188.39	0	-600.30	1.8	-167.75	1.8	-68.83	2.12	-135.64
103	103	2.20	-752.42	-212.81	188.11	0	-600.55	1.8	-167.69	1.8	-68.79	2.12	-135.54
103	104	3.30	-752.42	-179.05	398.38	0	-382.82	1.8	-314.50	1.8	-95.76	2.12	-188.70
104	104	3.30	-949.26	-178.38	277.65	0	-732.18	1.8	-192.03	1.8	-95.72	2.12	-188.62
104	105	4.40	-949.26	-144.54	448.55	0	-556.04	1.8	-308.95	1.8	-117.84	2.12	-232.19
105	105	4.40	-949.26	-144.03	448.29	0	-556.26	1.8	-308.90	1.8	-117.79	2.12	-232.11
105	106	5.50	-949.26	-102.38	586.15	0	-416.23	1.8	-397.19	1.8	-136.11	2.12	-268.20
106	106	5.50	-1146.10	-102.02	467.45	0	-762.40	1.8	-279.33	1.8	-136.07	2.12	-268.13
106	107	6.60	-1146.10	-68.15	566.19	0	-663.73	1.8	-337.83	1.8	-149.56	2.12	-294.71
107	107	6.60	-1146.10	-67.83	566.04	0	-700.26	1.8	-355.22	1.8	-150.77	2.12	-289.92
107	108	7.70	-1146.10	-34.04	625.66	0	-645.82	1.8	-384.02	1.8	-159.52	2.12	-306.73
108	108	7.70	-1146.10	-33.77	625.57	0	-645.89	1.8	-384.00	1.8	-159.50	2.12	-306.70
108	109	8.80	-1146.10	0.00	646.09	0	-630.81	1.8	-382.86	1.8	-163.39	2.12	-314.17
109	109	8.80	-1146.10	0.20	646.05	0	-630.84	1.8	-382.85	1.8	-163.38	2.12	-314.16
109	110	9.90	-1146.10	33.99	632.67	0	-650.85	1.8	-352.82	1.8	-163.29	2.12	-313.99
110	110	9.90	-1146.10	34.17	632.63	0	-650.89	1.8	-352.81	1.8	-163.28	2.12	-313.97
110	111	11.00	-1146.10	68.05	581.23	0	-709.36	1.8	-293.09	1.8	-158.52	2.12	-304.81
111	111	11.00	-1146.10	68.20	581.24	0	-709.35	1.8	-293.10	1.8	-158.52	2.12	-304.81
111	112	12.10	-1146.10	102.03	491.21	0	-806.80	1.8	-203.54	1.8	-148.98	2.12	-286.46
112	112	12.10	-1146.10	102.17	491.27	0	-806.75	1.8	-203.55	1.8	-148.99	2.12	-286.48
112	113	13.20	-1146.10	135.87	362.63	0	-943.16	1.8	-84.15	1.8	-134.67	2.12	-258.95
113	113	13.20	-1146.10	135.99	362.70	0	-943.10	1.8	-84.17	1.8	-134.68	2.12	-258.97
113	114	14.30	-1146.10	169.84	199.03	0	-1115.51	1.8	64.31	1.8	-116.19	2.12	-223.42
114	114	14.30	-924.56	165.02	317.66	0	-724.18	1.8	-16.55	1.8	-115.26	2.12	-227.12
114	115	15.40	-917.39	196.24	114.54	0	-939.06	1.8	171.86	1.8	-92.40	2.12	-182.07
115	115	15.40	-1858.58	204.99	554.22	0	-743.83	1.8	-603.49	1.8	-375.80	2.12	-506.36
115	116	16.50	-1858.58	211.57	319.18	0	-963.83	1.8	-508.05	1.8	-341.43	2.12	-437.81
116	116	16.50	-1858.58	211.98	319.39	0	-900.30	1.8	-569.90	1.8	-395.15	2.12	-510.89
116	117	17.60	-1858.58	228.41	73.98	0	-1159.51	1.8	-427.56	1.8	-341.85	2.12	-416.66
117	117	17.60	-2575.50	228.80	634.49	0	-665.74	1.8	-960.48	1.8	-697.60	2.12	-857.89
117	118	18.70	-2575.50	216.36	382.41	0	-937.67	1.8	-795.75	1.8	-645.17	2.12	-765.18
118	118	18.70	-2575.50	216.60	382.19	0	-937.89	1.8	-795.69	1.8	-645.11	2.12	-765.08
118	119	19.80	-2575.50	209.45	146.67	0	-1200.29	1.8	-614.59	1.8	-599.51	2.12	-684.44
119	119	19.80	-2299.92	209.30	320.61	0	-702.96	1.8	-798.70	1.8	-599.45	2.12	-684.34
119	120	20.90	-2299.92	203.40	93.37	0	-963.87	1.8	-598.74	1.8	-558.60	2.12	-612.10
120	120	20.90	-2299.92	202.95	93.37	0	-963.87	1.8	-598.74	1.8	-558.60	2.12	-612.10
120	121	22.00	-2299.92	216.96	-140.46	0	-1239.54	1.8	-369.52	1.8	-519.48	2.12	-542.92
121	1121	22.00	-2339.29	-212.61	-166.53	0	-1312.51	1.8	-340.45	1.8	-519.48	2.12	-542.93
121	122	23.40	-2339.29	-194.98	121.86	0	-958.55	1.8	-668.73	1.8	-562.05	2.12	-618.20
122	122	23.40	-2339.29	-195.54	121.89	0	-958.52	1.8	-668.74	1.8	-562.06	2.12	-618.22
122	123	24.80	-2339.29	-191.67	395.06	0	-632.87	1.8	-948.28	1.8	-606.30	2.12	-696.44
123	123	24.80	-2614.86	-192.45	223.53	0	-1126.16	1.8	-770.47	1.8	-606.26	2.12	-696.38
123	124	26.20	-2614.86	-222.80	506.83	0	-801.26	1.8	-1018.53	1.8	-657.35	2.12	-786.72
124	124	26.20	-1701.11	-222.52	67.63	0	-944.84	1.8	-609.06	1.8	-301.72	2.12	-345.69
124	125	27.60	-1701.11	-215.32	371.70	0	-610.36	1.8	-828.83	1.8	-362.34	2.12	-452.89
125	125	27.60	-2055.42	-214.80	162.14	0	-1227.34	1.8	-625.02	1.8	-362.39	2.12	-452.98
125	126	29.00	-2055.42	-225.12	481.03	0	-889.05	1.8	-814.73	1.8	-431.05	2.12	-574.38
126	126	29.00	-1122.96	-220.21	41.34	0	-1199.10	1.8	124.60	1.8	-88.22	2.12	-173.83
126	127	30.40	-1129.71	-180.80	322.91	0	-903.25	1.8	-116.18	1.8	-121.31	2.12	-239.04
127	127	30.40	-1460.38	-182.90	142.57	0	-1483.27	1.8	16.07	1.8	-122.28	2.12	-235.13
127	128	31.80	-1460.38	-138.94	362.63	0	-1255.88	1.8	-170.20	1.8	-148.20	2.12	-284.96
128	128	31.80	-1460.38	-138.98	362.48	0	-1256.00	1.8	-170.17	1.8	-148.17	2.12	-284.92
128	129	33.20	-1460.38	-90.41	522.63	0	-1089.51	1.8	-308.74	1.8	-166.80	2.12	-320.73
129	129	33.20	-1460.38	-90.53	522.52	0	-1089.60	1.8	-308.72	1.8	-166.78	2.12	-320.69
129	130	34.60	-1460.38	-53.75	624.40	0	-982.74	1.8	-399.74	1.8	-178.40	2.12	-343.03
130	130	34.60	-1460.38	-53.88	624.36	0	-982.77	1.8	-399.73	1.8	-178.39	2.12	-343.02
130	131	36.00	-1460.38	-10.35	663.35	0	-939.27	1.8	-442.43	1.8	-182.22	2.12	-350.37
131	131	36.00	-1460.38	-10.48	663.33	0	-939.29	1.8	-442.42	1.8	-182.21	2.12	-350.37
131	132	37.40	-1460.38	38.69	645.66	0	-954.10	1.8	-437.91	1.8	-179.30	2.12	-344.77
132	132	37.40	-1460.38	38.54	645.69	0	-954.07	1.8	-437.92	1.8	-179.31	2.12	-344.78
132	133	38.80	-1460.38	75.29	565.04	0	-1032.32	1.8	-385.04	1.8	-168.58	2.12	-324.16
133	133	38.80	-1460.38	75.19	565.16	0	-1032.23	1.8	-385.06	1.8	-168.60	2.12	-324.20

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ+

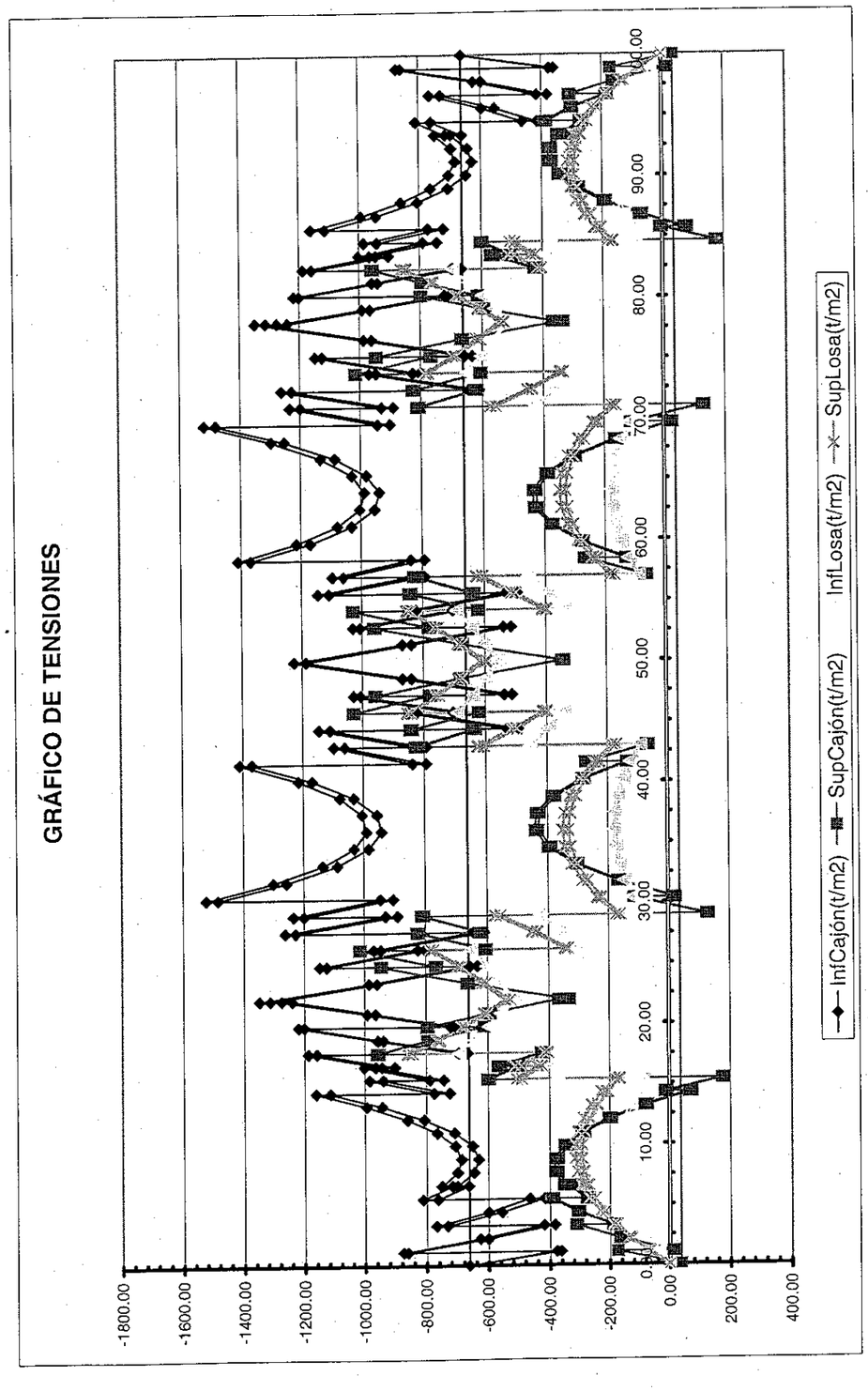
Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	123.77	426.49	0	-1169.87	1.8	-284.77	1.8	-150.91	2.12	-290.18
134	134	40.20	-1460.38	123.71	426.63	0	-1169.76	1.8	-284.80	1.8	-150.94	2.12	-290.23
134	135	41.60	-1460.38	167.61	227.84	0	-1368.52	1.8	-136.67	1.8	-125.92	2.12	-242.13
135	135	41.60	-1135.74	167.07	408.17	0	-792.89	1.8	-273.84	1.8	-124.92	2.12	-246.16
135	136	43.00	-1128.92	206.74	146.82	0	-1061.55	1.8	-68.59	1.8	-92.74	2.12	-182.73
136	136	43.00	-2055.42	210.05	586.52	0	-792.07	1.8	-828.78	1.8	-459.82	2.12	-625.26
136	137	44.40	-2055.42	207.88	289.13	0	-1110.57	1.8	-642.01	1.8	-397.02	2.12	-514.21
137	137	44.40	-1701.11	208.31	498.78	0	-493.51	1.8	-845.84	1.8	-397.00	2.12	-514.17
137	138	45.80	-1701.11	218.16	201.32	0	-822.61	1.8	-624.67	1.8	-338.46	2.12	-410.66
138	138	45.80	-2614.86	218.68	640.44	0	-679.10	1.8	-1034.12	1.8	-694.08	2.12	-851.66
138	139	47.20	-2614.86	194.15	356.66	0	-1005.50	1.8	-782.58	1.8	-643.28	2.12	-761.84
139	139	47.20	-2339.29	194.28	527.93	0	-512.45	1.8	-960.31	1.8	-643.25	2.12	-761.78
139	140	48.60	-2345.74	191.27	258.51	0	-837.49	1.8	-680.52	1.8	-602.10	2.12	-687.69
140	140	48.60	-2345.92	190.68	258.56	0	-837.49	1.8	-680.59	1.8	-602.16	2.12	-687.76
140	141	50.00	-2345.92	207.36	-24.05	0	-1186.87	1.8	-350.66	1.8	-561.46	2.12	-615.81
141	1141	50.00	-2345.71	-207.45	-24.04	0	-1186.81	1.8	-350.60	1.8	-561.41	2.12	-615.76
141	142	51.40	-2345.71	-190.77	258.68	0	-837.32	1.8	-680.56	1.8	-602.13	2.12	-687.76
142	142	51.40	-2345.10	-191.34	258.63	0	-837.17	1.8	-680.36	1.8	-601.96	2.12	-687.58
142	143	52.80	-2345.10	-193.85	528.08	0	-514.10	1.8	-962.15	1.8	-644.84	2.12	-763.40
143	143	52.80	-2619.68	-193.79	356.71	0	-1006.93	1.8	-784.07	1.8	-644.58	2.12	-763.15
143	144	54.20	-2614.86	-218.68	640.44	0	-679.10	1.8	-1034.12	1.8	-694.08	2.12	-851.66
144	144	54.20	-1701.11	-218.18	201.32	0	-822.60	1.8	-624.67	1.8	-338.46	2.12	-410.67
144	145	55.60	-1701.11	-208.32	498.80	0	-493.48	1.8	-845.85	1.8	-397.00	2.12	-514.18
145	145	55.60	-2055.42	-207.90	289.15	0	-1110.56	1.8	-642.02	1.8	-397.03	2.12	-514.22
145	146	57.00	-2055.42	-210.05	586.57	0	-792.02	1.8	-828.80	1.8	-459.84	2.12	-625.28
146	146	57.00	-1128.92	-206.76	146.87	0	-1061.51	1.8	-68.60	1.8	-92.74	2.12	-182.75
146	147	58.40	-1133.95	-166.18	407.33	0	-792.74	1.8	-270.33	1.8	-124.93	2.12	-246.18
147	147	58.40	-1458.36	-167.70	226.99	0	-1368.20	1.8	-132.97	1.8	-125.93	2.12	-242.14
147	148	59.80	-1458.36	-123.78	425.84	0	-1169.33	1.8	-281.26	1.8	-150.94	2.12	-290.24
148	148	59.80	-1458.36	-123.84	425.72	0	-1169.44	1.8	-281.24	1.8	-150.92	2.12	-290.20
148	149	61.20	-1458.36	-75.25	564.45	0	-1031.68	1.8	-381.71	1.8	-168.61	2.12	-324.21
149	149	61.20	-1458.36	-75.36	564.35	0	-1031.76	1.8	-381.69	1.8	-168.59	2.12	-324.18
149	150	62.60	-1458.36	-38.60	645.11	0	-953.36	1.8	-434.78	1.8	-179.32	2.12	-344.80
150	150	62.60	-1458.36	-38.74	645.08	0	-953.39	1.8	-434.77	1.8	-179.31	2.12	-344.79
150	151	64.00	-1456.62	10.40	662.81	0	-937.05	1.8	-438.03	1.8	-182.22	2.12	-350.38
151	151	64.00	-1456.62	10.27	662.82	0	-937.05	1.8	-438.03	1.8	-182.22	2.12	-350.39
151	152	65.40	-1456.62	53.80	623.94	0	-980.37	1.8	-395.61	1.8	-178.40	2.12	-343.03
152	152	65.40	-1456.62	53.66	623.99	0	-980.33	1.8	-395.62	1.8	-178.41	2.12	-343.05
152	153	66.80	-1456.62	90.43	522.24	0	-1087.01	1.8	-304.86	1.8	-166.79	2.12	-320.71
153	153	66.80	-1456.62	90.34	522.34	0	-1086.92	1.8	-304.88	1.8	-166.81	2.12	-320.75
153	154	68.20	-1456.62	138.90	362.30	0	-1253.24	1.8	-166.57	1.8	-148.18	2.12	-284.93
154	154	68.20	-1456.62	138.86	362.43	0	-1253.13	1.8	-166.60	1.8	-148.20	2.12	-284.97
154	155	69.60	-1456.62	182.81	142.49	0	-1480.35	1.8	19.41	1.8	-122.29	2.12	-235.14
155	155	69.60	-1126.45	178.93	322.84	0	-900.73	1.8	-113.25	1.8	-121.32	2.12	-239.05
155	156	71.00	-1122.96	220.21	41.36	0	-1199.09	1.8	124.62	1.8	-88.22	2.12	-173.84
156	156	71.00	-2055.42	225.14	481.06	0	-889.03	1.8	-814.74	1.8	-431.05	2.12	-574.39
156	157	72.40	-2055.42	214.81	162.16	0	-1227.32	1.8	-625.03	1.8	-362.40	2.12	-452.98
157	157	72.40	-1701.11	215.33	371.72	0	-610.34	1.8	-828.84	1.8	-362.35	2.12	-452.90
157	158	73.80	-1701.11	222.53	67.62	0	-944.85	1.8	-609.06	1.8	-301.72	2.12	-345.69
158	158	73.80	-2614.86	222.80	506.81	0	-801.27	1.8	-1018.52	1.8	-657.35	2.12	-786.71
158	159	75.20	-2614.86	192.45	223.52	0	-1126.17	1.8	-770.46	1.8	-606.26	2.12	-696.38
159	159	75.20	-2339.29	191.66	395.07	0	-632.86	1.8	-948.28	1.8	-606.30	2.12	-696.45
159	160	76.60	-2343.12	195.07	122.41	0	-959.20	1.8	-670.07	1.8	-563.21	2.12	-619.47
160	160	76.60	-2343.06	194.49	122.45	0	-959.14	1.8	-670.06	1.8	-563.21	2.12	-619.48
160	161	78.00	-2343.06	212.12	-165.22	0	-1312.41	1.8	-341.99	1.8	-520.82	2.12	-544.52
161	1161	78.00	-2303.37	-216.81	-139.16	0	-1239.34	1.8	-370.96	1.8	-520.73	2.12	-544.43
161	162	79.10	-2303.37	-202.81	94.53	0	-963.81	1.8	-600.14	1.8	-559.81	2.12	-613.54
162	162	79.10	-2302.99	-203.25	94.50	0	-963.72	1.8	-600.02	1.8	-559.71	2.12	-613.43
162	163	80.20	-2302.99	-209.16	321.59	0	-702.96	1.8	-799.93	1.8	-600.52	2.12	-685.60
163	163	80.20	-2578.03	-209.29	147.61	0	-1200.17	1.8	-615.65	1.8	-600.43	2.12	-685.54
163	164	81.30	-2578.03	-216.43	382.98	0	-937.90	1.8	-796.70	1.8	-645.99	2.12	-766.11
164	164	81.30	-2577.33	-216.21	383.13	0	-937.54	1.8	-796.53	1.8	-645.84	2.12	-765.99
164	165	82.40	-2577.33	-228.65	635.05	0	-665.76	1.8	-961.21	1.8	-698.24	2.12	-858.63
165	165	82.40	-1859.54	-228.32	74.87	0	-1158.71	1.8	-428.90	1.8	-342.24	2.12	-417.14
165	166	83.50	-1859.54	-211.89	319.77	0	-900.22	1.8	-570.30	1.8	-395.50	2.12	-511.32
166	166	83.50	-1858.58	-211.57	319.47	0	-963.58	1.8	-508.10	1.8	-341.47	2.12	-437.91
166	167	84.60	-1858.58	-204.99	554.48	0	-743.60	1.8	-603.54	1.8	-375.84	2.12	-506.45
167	167	84.60	-917.40	-196.22	114.81	0	-938.68	1.8	171.29	1.8	-92.40	2.12	-182.08
167	168	85.70	-920.89	-162.54	316.57	0	-722.85	1.8	-10.94	1.8	-115.27	2.12	-227.14
168	168	85.70	-1141.67	-169.91	197.93	0	-1113.59	1.8	70.53	1.8	-116.20	2.12	-223.43
168	169	86.80	-1141.67	-136.07	361.72	0	-941.01	1.8	-78.15	1.8	-134.69	2.12	-258.99
169	169	86.80	-1141.67	-135.95	361.61	0	-941.11	1.8	-78.13	1.8	-134.67	2.12	-258.95
169	170	87.90	-1141.67	-102.27	490.35	0	-804.56	1.8	-197.73	1.8	-148.99	2.12	-286.49
170	170	87.90	-1141.67	-102.11	490.29	0	-804.61	1.8	-197.72	1.8	-148.98	2.12	-286.47
170	171	89.00	-1141.67	-68.29	580.41	0	-707.03	1.8	-287.48	1.8	-158.53	2.12	-304.82

11/09/03



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CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-234.68	-198.37	0	-732.89	1.8	41.72	1.8	0.11	2.12	0.22
1	2	1.10	-517.71	-90.53	-87.22	0	-582.15	1.8	-126.32	1.8	-6.73	2.12	-13.27
2	2	1.10	-822.30	-90.75	-279.75	0	-1132.11	1.8	77.25	1.8	-6.73	2.12	-13.26
2	3	2.20	-822.30	-72.81	-189.79	0	-1011.57	1.8	-65.75	1.8	-11.94	2.12	-23.53
3	3	2.20	-822.30	-73.04	-189.82	0	-1011.60	1.8	-65.74	1.8	-11.93	2.12	-23.52
3	4	3.30	-822.30	-55.06	-119.36	0	-915.51	1.8	-182.71	1.8	-15.62	2.12	-30.78
4	4	3.30	-1039.86	-55.30	-252.56	0	-1301.42	1.8	-47.40	1.8	-15.62	2.12	-30.77
4	5	4.40	-1039.86	-37.36	-201.61	0	-1229.77	1.8	-138.31	1.8	-17.79	2.12	-35.05
5	5	4.40	-1039.86	-37.62	-201.63	0	-1229.79	1.8	-138.31	1.8	-17.78	2.12	-35.04
5	6	5.50	-1039.86	-19.65	-170.15	0	-1182.52	1.8	-203.24	1.8	-18.43	2.12	-36.32
6	6	5.50	-1257.42	-19.93	-301.15	0	-1564.97	1.8	-73.00	1.8	-18.42	2.12	-36.31
6	7	6.60	-1257.42	-1.97	-289.07	0	-1542.03	1.8	-111.98	1.8	-17.56	2.12	-34.61
7	7	6.60	-1257.42	-2.29	-289.12	0	-1540.06	1.8	-129.46	1.8	-17.70	2.12	-34.04
7	8	7.70	-1257.42	15.66	-296.47	0	-1541.32	1.8	-142.41	1.8	-15.31	2.12	-29.45
8	8	7.70	-1257.42	15.35	-296.50	0	-1541.34	1.8	-142.40	1.8	-15.31	2.12	-29.44
8	9	8.80	-1257.42	33.54	-323.27	0	-1565.86	1.8	-129.26	1.8	-11.40	2.12	-21.92
9	9	8.80	-1257.42	33.10	-323.30	0	-1565.89	1.8	-129.25	1.8	-11.39	2.12	-21.91
9	10	9.90	-1257.42	51.16	-369.62	0	-1613.76	1.8	-90.01	1.8	-5.94	2.12	-11.42
10	10	9.90	-1257.42	50.76	-369.63	0	-1613.77	1.8	-90.01	1.8	-5.94	2.12	-11.42
10	11	11.00	-1257.42	68.71	-435.36	0	-1684.88	1.8	-24.72	1.8	1.04	2.12	1.99
11	11	11.00	-1257.42	68.27	-435.37	0	-1684.89	1.8	-24.72	1.8	1.04	2.12	2.00
11	12	12.10	-1257.42	86.25	-520.36	0	-1779.14	1.8	66.64	1.8	9.51	2.12	18.28
12	12	12.10	-1257.42	85.81	-520.39	0	-1779.16	1.8	66.64	1.8	9.51	2.12	18.29
12	13	13.20	-1257.42	103.81	-624.75	0	-1896.63	1.8	184.10	1.8	19.49	2.12	37.48
13	13	13.20	-1257.42	103.36	-624.76	0	-1896.64	1.8	184.10	1.8	19.49	2.12	37.48
13	14	14.30	-1257.42	121.35	-748.35	0	-2037.18	1.8	327.51	1.8	30.97	2.12	59.55
14	14	14.30	-1016.08	110.63	-617.40	0	-1651.81	1.8	233.66	1.8	30.72	2.12	60.53
14	15	15.40	-1016.27	131.08	-759.44	0	-1818.94	1.8	400.83	1.8	43.58	2.12	85.88
15	15	15.40	-1871.02	139.40	-361.78	0	-1622.01	1.8	-377.97	1.8	-211.41	2.12	-201.68
15	16	16.50	-1871.02	189.79	-530.30	0	-1784.70	1.8	-295.01	1.8	-187.87	2.12	-154.74
16	16	16.50	-1871.02	189.49	-530.21	0	-1806.38	1.8	-273.80	1.8	-169.45	2.12	-129.70
16	17	17.60	-1871.02	218.40	-752.69	0	-2043.43	1.8	-138.06	1.8	-121.97	2.12	-45.75
17	17	17.60	-2480.19	217.87	-221.26	0	-1526.49	1.8	-644.98	1.8	-443.86	2.12	-444.99
17	18	18.70	-2480.19	260.19	-483.75	0	-1808.50	1.8	-477.22	1.8	-388.79	2.12	-347.61
18	18	18.70	-2480.18	259.71	-483.34	0	-1808.10	1.8	-477.33	1.8	-388.89	2.12	-347.80
18	19	19.80	-2480.18	306.85	-793.65	0	-2142.89	1.8	-274.44	1.8	-324.36	2.12	-233.69
19	19	19.80	-2175.60	306.45	-600.62	0	-1592.45	1.8	-478.16	1.8	-324.49	2.12	-233.93
19	20	20.90	-2175.60	365.49	-975.53	0	-1996.28	1.8	-235.16	1.8	-246.26	2.12	-95.60
20	20	20.90	-2175.60	365.29	-975.51	0	-1996.26	1.8	-235.17	1.8	-246.27	2.12	-95.61
20	21	22.00	-2175.60	419.33	-1406.01	0	-2462.27	1.8	51.36	1.8	-157.37	2.12	61.58
21	1021	22.00	-2219.11	-441.28	-1434.73	0	-2542.83	1.8	83.46	1.8	-157.39	2.12	61.54
21	22	23.40	-2219.11	-383.43	-862.30	0	-1913.97	1.8	-327.59	1.8	-271.86	2.12	-140.85
22	22	23.40	-2219.11	-383.67	-862.17	0	-1913.85	1.8	-327.62	1.8	-271.89	2.12	-140.91
22	23	24.80	-2219.11	-321.42	-368.78	0	-1375.07	1.8	-671.34	1.8	-371.86	2.12	-317.69
23	23	24.80	-2523.70	-320.12	-558.23	0	-1920.15	1.8	-474.85	1.8	-371.86	2.12	-317.69
23	24	26.20	-2523.70	-246.73	-170.52	0	-1494.19	1.8	-753.34	1.8	-449.38	2.12	-454.76
24	24	26.20	-1696.97	-246.62	-568.77	0	-1624.95	1.8	-382.61	1.8	-127.39	2.12	-55.34
24	25	27.60	-1696.97	-190.83	-263.21	0	-1289.02	1.8	-602.82	1.8	-188.39	2.12	-163.20
25	25	27.60	-2088.58	-191.36	-495.60	0	-1971.70	1.8	-377.33	1.8	-188.25	2.12	-162.94
25	26	29.00	-2088.58	-115.65	-300.50	0	-1753.22	1.8	-530.96	1.8	-225.58	2.12	-228.95
26	26	29.00	-1242.90	-111.46	-698.24	0	-1990.60	1.8	342.88	1.8	22.63	2.12	44.59
26	27	30.40	-1243.14	-85.36	-553.49	0	-1807.25	1.8	133.03	1.8	12.61	2.12	24.84
27	27	30.40	-1606.18	-91.71	-752.65	0	-2404.24	1.8	282.76	1.8	12.72	2.12	24.46
27	28	31.80	-1606.18	-68.78	-640.30	0	-2264.64	1.8	116.58	1.8	5.13	2.12	9.87
28	28	31.80	-1606.18	-69.38	-640.36	0	-2264.68	1.8	116.59	1.8	5.14	2.12	9.89
28	29	33.20	-1606.18	-46.54	-559.21	0	-2162.52	1.8	-7.47	1.8	-0.02	2.12	-0.03
29	29	33.20	-1606.18	-47.09	-559.22	0	-2162.53	1.8	-7.47	1.8	-0.02	2.12	-0.03
29	30	34.60	-1606.18	-22.98	-510.41	0	-2098.76	1.8	-89.09	1.8	-2.56	2.12	-4.93
30	30	34.60	-1606.18	-23.52	-510.48	0	-2098.82	1.8	-89.08	1.8	-2.55	2.12	-4.91
30	31	36.00	-1606.18	3.02	-496.75	0	-2075.68	1.8	-127.76	1.8	-2.02	2.12	-3.88
31	31	36.00	-1606.18	2.49	-496.76	0	-2075.69	1.8	-127.76	1.8	-2.02	2.12	-3.88
31	32	37.40	-1606.18	25.45	-516.26	0	-2091.67	1.8	-123.87	1.8	1.28	2.12	2.46
32	32	37.40	-1606.18	24.85	-516.27	0	-2091.68	1.8	-123.86	1.8	1.28	2.12	2.47
32	33	38.80	-1606.18	47.71	-567.05	0	-2145.18	1.8	-77.75	1.8	7.01	2.12	13.49
33	33	38.80	-1606.18	47.12	-567.05	0	-2145.18	1.8	-77.75	1.8	7.01	2.12	13.49
33	34	40.20	-1606.18	69.98	-649.03	0	-2236.16	1.8	10.56	1.8	15.17	2.12	29.17
34	34	40.20	-1606.18	69.37	-649.00	0	-2236.13	1.8	10.55	1.8	15.16	2.12	29.16
34	35	41.60	-1606.18	92.32	-762.14	0	-2364.52	1.8	141.03	1.8	25.73	2.12	49.48
35	35	41.60	-1249.48	87.58	-563.00	0	-1776.63	1.8	-14.03	1.8	25.52	2.12	50.28
35	36	43.00	-1249.32	113.27	-707.30	0	-1947.92	1.8	157.39	1.8	38.48	2.12	75.82
36	36	43.00	-2088.58	115.79	-309.56	0	-1767.10	1.8	-511.64	1.8	-225.36	2.12	-228.57
36	37	44.40	-2088.58	185.24	-507.34	0	-1989.19	1.8	-353.89	1.8	-187.77	2.12	-162.10
37	37	44.40	-1696.97	184.65	-275.04	0	-1306.61	1.8	-579.35	1.8	-187.89	2.12	-162.31
37	38	45.80	-1696.97	237.55	-567.56	0	-1630.94	1.8	-359.61	1.8	-130.61	2.12	-61.02
38	38	45.80	-2523.70	237.09	-169.21	0	-1500.08	1.8	-730.37	1.8	-452.62	2.12	-460.48

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Programa DINTEL PACADAR S.A.
FRECUENTEST.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	295.94	-538.48	0	-1909.21	1.8	-453.92	1.8	-380.19	2.12	-332.40
39	39	47.20	-2219.11	295.15	-348.64	0	-1363.75	1.8	-650.52	1.8	-380.28	2.12	-332.58
39	40	48.60	-2212.66	371.48	-817.63	0	-1877.95	1.8	-308.60	1.8	-285.17	2.12	-165.73
40	40	48.60	-2212.49	371.19	-817.71	0	-1877.98	1.8	-308.52	1.8	-285.11	2.12	-165.65
40	41	50.00	-2212.49	431.70	-1376.34	0	-2494.50	1.8	101.84	1.8	-174.55	2.12	29.84
41	1041	50.00	-2212.70	-431.62	-1376.34	0	-2494.57	1.8	101.77	1.8	-174.61	2.12	29.78
41	42	51.40	-2212.70	-371.12	-817.83	0	-1878.15	1.8	-308.55	1.8	-285.13	2.12	-165.65
42	42	51.40	-2213.30	-371.40	-817.76	0	-1878.28	1.8	-308.76	1.8	-285.31	2.12	-165.84
42	43	52.80	-2213.30	-295.56	-348.78	0	-1362.10	1.8	-648.69	1.8	-378.69	2.12	-330.96
43	43	52.80	-2518.88	-296.30	-538.52	0	-1907.76	1.8	-452.43	1.8	-378.89	2.12	-331.10
43	44	54.20	-2523.70	-237.09	-169.19	0	-1500.06	1.8	-730.37	1.8	-452.62	2.12	-460.49
44	44	54.20	-1696.97	-237.55	-567.56	0	-1630.94	1.8	-359.61	1.8	-130.61	2.12	-61.02
44	45	55.60	-1696.97	-184.64	-275.01	0	-1306.58	1.8	-579.36	1.8	-187.90	2.12	-162.32
45	45	55.60	-2088.58	-185.24	-507.33	0	-1989.18	1.8	-353.90	1.8	-187.78	2.12	-162.11
45	46	57.00	-2088.58	-115.78	-309.52	0	-1767.06	1.8	-511.65	1.8	-225.37	2.12	-228.59
46	46	57.00	-1249.32	-113.28	-707.29	0	-1947.90	1.8	157.36	1.8	38.47	2.12	75.81
46	47	58.40	-1251.27	-88.50	-562.10	0	-1776.72	1.8	-17.58	1.8	25.52	2.12	50.28
47	47	58.40	-1608.20	-92.25	-761.24	0	-2364.80	1.8	137.31	1.8	25.73	2.12	49.48
47	48	59.80	-1608.20	-69.31	-648.17	0	-2236.51	1.8	7.00	1.8	15.16	2.12	29.15
48	48	59.80	-1608.20	-69.91	-648.19	0	-2236.53	1.8	7.01	1.8	15.16	2.12	29.16
48	49	61.20	-1608.20	-47.05	-566.32	0	-2145.72	1.8	-81.09	1.8	7.01	2.12	13.49
49	49	61.20	-1608.20	-47.65	-566.32	0	-2145.72	1.8	-81.09	1.8	7.01	2.12	13.49
49	50	62.60	-1608.20	-24.80	-515.60	0	-2092.31	1.8	-127.04	1.8	1.28	2.12	2.46
50	50	62.60	-1608.20	-25.39	-515.61	0	-2092.31	1.8	-127.04	1.8	1.28	2.12	2.46
50	51	64.00	-1609.94	-2.40	-496.19	0	-2077.89	1.8	-132.14	1.8	-2.02	2.12	-3.88
51	51	64.00	-1609.94	-2.94	-496.19	0	-2077.89	1.8	-132.14	1.8	-2.02	2.12	-3.88
51	52	65.40	-1609.94	23.61	-510.03	0	-2101.20	1.8	-93.20	1.8	-2.55	2.12	-4.91
52	52	65.40	-1609.94	23.06	-509.98	0	-2101.15	1.8	-93.21	1.8	-2.56	2.12	-4.92
52	53	66.80	-1609.94	47.17	-558.86	0	-2165.07	1.8	-11.34	1.8	-0.02	2.12	-0.03
53	53	66.80	-1609.94	46.63	-558.86	0	-2165.06	1.8	-11.34	1.8	-0.02	2.12	-0.04
53	54	68.20	-1609.94	69.46	-640.11	0	-2267.38	1.8	112.96	1.8	5.14	2.12	9.88
54	54	68.20	-1609.94	68.86	-640.08	0	-2267.36	1.8	112.96	1.8	5.14	2.12	9.88
54	55	69.60	-1609.94	91.79	-752.53	0	-2407.11	1.8	279.39	1.8	12.72	2.12	24.46
55	55	69.60	-1246.39	87.25	-553.38	0	-1809.73	1.8	130.07	1.8	12.61	2.12	24.85
55	56	71.00	-1242.90	111.47	-698.25	0	-1990.61	1.8	342.90	1.8	22.63	2.12	44.59
56	56	71.00	-2088.58	115.65	-300.50	0	-1753.22	1.8	-530.96	1.8	-225.58	2.12	-228.95
56	57	72.40	-2088.58	191.36	-495.60	0	-1971.70	1.8	-377.33	1.8	-188.25	2.12	-162.94
57	57	72.40	-1696.97	190.85	-263.21	0	-1289.03	1.8	-602.81	1.8	-188.39	2.12	-163.19
57	58	73.80	-1696.97	246.65	-568.78	0	-1624.95	1.8	-382.61	1.8	-127.39	2.12	-55.33
58	58	73.80	-2523.70	246.73	-170.52	0	-1494.19	1.8	-753.34	1.8	-449.38	2.12	-454.75
58	59	75.20	-2523.70	320.12	-558.25	0	-1920.17	1.8	-474.84	1.8	-371.86	2.12	-317.68
59	59	75.20	-2219.11	321.41	-368.77	0	-1375.06	1.8	-671.34	1.8	-371.87	2.12	-317.69
59	60	76.60	-2215.29	384.13	-862.69	0	-1913.17	1.8	-326.29	1.8	-270.73	2.12	-139.66
60	60	76.60	-2215.34	383.92	-862.91	0	-1913.40	1.8	-326.24	1.8	-270.69	2.12	-139.57
60	61	78.00	-2215.34	441.80	-1436.04	0	-2542.94	1.8	85.01	1.8	-156.05	2.12	63.14
61	1061	78.00	-2172.15	-419.48	-1407.38	0	-2462.54	1.8	52.82	1.8	-156.10	2.12	63.12
61	62	79.10	-2172.15	-365.44	-976.71	0	-1996.36	1.8	-233.76	1.8	-245.04	2.12	-94.15
62	62	79.10	-2172.53	-365.66	-976.74	0	-1996.51	1.8	-233.86	1.8	-245.13	2.12	-94.23
62	63	80.20	-2172.53	-306.62	-601.63	0	-1592.48	1.8	-476.92	1.8	-323.42	2.12	-232.66
63	63	80.20	-2477.65	-307.02	-794.63	0	-2143.06	1.8	-273.37	1.8	-323.43	2.12	-232.58
63	64	81.30	-2477.65	-259.88	-484.14	0	-1808.09	1.8	-476.32	1.8	-388.01	2.12	-346.76
64	64	81.30	-2478.35	-260.34	-484.50	0	-1808.66	1.8	-476.43	1.8	-388.11	2.12	-346.79
64	65	82.40	-2478.35	-218.01	-221.83	0	-1526.47	1.8	-644.24	1.8	-443.22	2.12	-444.24
65	65	82.40	-1870.06	-218.50	-752.74	0	-2042.92	1.8	-138.62	1.8	-121.59	2.12	-45.27
65	66	83.50	-1870.06	-189.59	-530.59	0	-1806.45	1.8	-273.39	1.8	-169.10	2.12	-129.27
66	66	83.50	-1871.02	-189.81	-530.56	0	-1784.93	1.8	-294.96	1.8	-187.83	2.12	-154.66
66	67	84.60	-1871.02	-139.42	-362.03	0	-1622.22	1.8	-377.93	1.8	-211.37	2.12	-201.60
67	67	84.60	-1016.26	-131.08	-759.70	0	-1819.32	1.8	401.39	1.8	43.59	2.12	85.89
67	68	85.70	-1019.75	-113.08	-616.29	0	-1653.11	1.8	228.05	1.8	30.72	2.12	60.53
68	68	85.70	-1261.85	-121.28	-747.25	0	-2039.10	1.8	321.28	1.8	30.97	2.12	59.56
68	69	86.80	-1261.85	-103.28	-623.73	0	-1898.68	1.8	178.05	1.8	19.50	2.12	37.49
69	69	86.80	-1261.85	-103.75	-623.72	0	-1898.66	1.8	178.05	1.8	19.49	2.12	37.48
69	70	87.90	-1261.85	-85.74	-519.47	0	-1781.36	1.8	60.84	1.8	9.52	2.12	18.30
70	70	87.90	-1261.85	-86.18	-519.45	0	-1781.34	1.8	60.84	1.8	9.51	2.12	18.29
70	71	89.00	-1261.85	-68.20	-434.54	0	-1687.22	1.8	-30.31	1.8	1.04	2.12	2.00
71	71	89.00	-1261.85	-68.64	-434.52	0	-1687.21	1.8	-30.32	1.8	1.04	2.12	2.00
71	72	90.10	-1261.85	-50.69	-368.88	0	-1616.22	1.8	-95.43	1.8	-5.93	2.12	-11.41
72	72	90.10	-1261.85	-51.09	-368.86	0	-1616.21	1.8	-95.43	1.8	-5.94	2.12	-11.42
72	73	91.20	-1261.85	-33.04	-322.64	0	-1568.47	1.8	-134.47	1.8	-11.39	2.12	-21.90
73	73	91.20	-1261.85	-33.47	-322.59	0	-1568.43	1.8	-134.48	1.8	-11.40	2.12	-21.91
73	74	92.30	-1261.85	-15.28	-295.90	0	-1544.04	1.8	-147.42	1.8	-15.31	2.12	-29.43
74	74	92.30	-1261.85	-15.59	-295.88	0	-1544.03	1.8	-147.43	1.8	-15.31	2.12	-29.44
74	75	93.40	-1261.85	2.36	-288.60	0	-1542.89	1.8	-134.28	1.8	-17.70	2.12	-34.04
75	75	93.40	-1261.85	2.03	-288.57	0	-1544.77	1.8	-116.72	1.8	-17.56	2.12	-34.60
75	76	94.50	-1261.85	19.99	-300.72	0	-1567.82	1.8	-77.57	1.8	-18.42	2.12	-36.30

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	19.72	-169.70	0	-1185.36	1.8	-207.81	1.8	-18.43	2.12	-36.32
76	77	95.60	-1044.29	37.68	-201.30	0	-1232.78	1.8	-142.68	1.8	-17.78	2.12	-35.03
77	77	95.60	-1044.29	37.43	-201.27	0	-1232.76	1.8	-142.68	1.8	-17.78	2.12	-35.04
77	78	96.70	-1044.29	55.37	-252.32	0	-1304.58	1.8	-51.52	1.8	-15.61	2.12	-30.77
78	78	96.70	-826.73	55.13	-119.15	0	-918.67	1.8	-186.83	1.8	-15.62	2.12	-30.78
78	79	97.80	-826.73	73.10	-189.66	0	-1014.88	1.8	-69.67	1.8	-11.93	2.12	-23.52
79	79	97.80	-826.73	72.86	-189.62	0	-1014.86	1.8	-69.67	1.8	-11.94	2.12	-23.53
79	80	98.90	-826.73	90.80	-279.66	0	-1135.52	1.8	73.51	1.8	-6.73	2.12	-13.26
80	80	98.90	-522.14	90.59	-87.13	0	-585.56	1.8	-130.06	1.8	-6.73	2.12	-13.27
80	81	100.00	-522.14	234.66	-198.37	0	-732.89	1.8	41.72	1.8	0.11	2.12	0.22
101	101	0.00	-522.14	-231.66	-198.43	0	-732.94	1.8	41.73	1.8	0.12	2.12	0.24
101	102	1.10	-517.71	-86.70	-91.57	0	-585.92	1.8	-125.47	1.8	-6.00	2.12	-11.82
102	102	1.10	-822.30	-87.02	-283.88	0	-1135.67	1.8	78.05	1.8	-6.03	2.12	-11.89
102	103	2.20	-822.30	-69.50	-197.81	0	-1018.50	1.8	-64.20	1.8	-10.59	2.12	-20.87
103	103	2.20	-822.30	-69.74	-197.63	0	-1018.34	1.8	-64.23	1.8	-10.62	2.12	-20.93
103	104	3.30	-822.30	-52.23	-130.58	0	-925.18	1.8	-180.54	1.8	-13.74	2.12	-27.07
104	104	3.30	-1039.86	-52.36	-263.56	0	-1310.92	1.8	-45.27	1.8	-13.77	2.12	-27.13
104	105	4.40	-1039.86	-34.87	-215.59	0	-1241.83	1.8	-135.63	1.8	-15.43	2.12	-30.41
105	105	4.40	-1039.86	-34.95	-215.47	0	-1241.72	1.8	-135.65	1.8	-15.45	2.12	-30.45
105	106	5.50	-1039.86	-17.44	-186.67	0	-1196.77	1.8	-200.06	1.8	-15.65	2.12	-30.84
106	106	5.50	-1257.42	-17.41	-317.51	0	-1579.08	1.8	-69.86	1.8	-15.67	2.12	-30.88
106	107	6.60	-1257.42	0.11	-307.99	0	-1558.36	1.8	-108.31	1.8	-14.38	2.12	-28.34
107	107	6.60	-1257.42	0.18	-307.89	0	-1555.42	1.8	-125.80	1.8	-14.52	2.12	-27.92
107	108	7.70	-1257.42	17.68	-317.72	0	-1558.70	1.8	-138.26	1.8	-11.71	2.12	-22.52
108	108	7.70	-1257.42	17.80	-317.63	0	-1558.63	1.8	-138.28	1.8	-11.73	2.12	-22.55
108	109	8.80	-1257.42	35.30	-346.82	0	-1585.13	1.8	-124.66	1.8	-7.41	2.12	-14.24
109	109	8.80	-1257.42	35.43	-346.76	0	-1585.07	1.8	-124.67	1.8	-7.42	2.12	-14.26
109	110	9.90	-1257.42	52.93	-395.39	0	-1634.84	1.8	-84.98	1.8	-1.57	2.12	-3.02
110	110	9.90	-1257.42	53.10	-395.35	0	-1634.81	1.8	-84.99	1.8	-1.58	2.12	-3.03
110	111	11.00	-1257.42	70.62	-463.37	0	-1707.79	1.8	-19.25	1.8	5.78	2.12	11.12
111	111	11.00	-1257.42	70.84	-463.35	0	-1707.78	1.8	-19.26	1.8	5.78	2.12	11.12
111	112	12.10	-1257.42	88.34	-550.93	0	-1804.14	1.8	72.60	1.8	14.69	2.12	28.24
112	112	12.10	-1257.42	88.58	-550.92	0	-1804.13	1.8	72.60	1.8	14.69	2.12	28.24
112	113	13.20	-1257.42	106.07	-658.01	0	-1923.83	1.8	190.57	1.8	25.13	2.12	48.32
113	113	13.20	-1257.42	106.33	-658.05	0	-1923.86	1.8	190.57	1.8	25.14	2.12	48.33
113	114	14.30	-1257.42	123.87	-784.65	0	-2066.88	1.8	334.59	1.8	37.12	2.12	71.38
114	114	14.30	-1016.08	113.91	-653.74	0	-1683.18	1.8	240.69	1.8	36.83	2.12	72.57
114	115	15.40	-1016.27	134.10	-799.15	0	-1853.22	1.8	408.51	1.8	50.26	2.12	99.04
115	115	15.40	-1871.02	143.22	-401.59	0	-1656.30	1.8	-370.51	1.8	-204.92	2.12	-188.75
115	116	16.50	-1871.02	187.82	-574.25	0	-1822.56	1.8	-286.77	1.8	-180.71	2.12	-140.46
116	116	16.50	-1871.02	188.06	-574.36	0	-1849.11	1.8	-260.93	1.8	-158.27	2.12	-109.94
116	117	17.60	-1871.02	215.59	-794.82	0	-2084.21	1.8	-125.78	1.8	-111.31	2.12	-26.89
117	117	17.60	-2480.18	215.71	-263.62	0	-1567.48	1.8	-632.63	1.8	-433.13	2.12	-426.03
117	118	18.70	-2480.18	265.65	-529.52	0	-1852.80	1.8	-463.87	1.8	-377.20	2.12	-327.13
118	118	18.70	-2480.18	265.91	-529.26	0	-1852.54	1.8	-463.95	1.8	-377.27	2.12	-327.25
118	119	19.80	-2480.18	322.57	-851.66	0	-2199.04	1.8	-257.53	1.8	-309.68	2.12	-207.73
119	119	19.80	-2175.60	323.25	-658.97	0	-1648.92	1.8	-461.16	1.8	-309.73	2.12	-207.82
119	120	20.90	-2175.60	393.84	-1060.70	0	-2078.71	1.8	-210.35	1.8	-224.71	2.12	-57.48
120	120	20.90	-2175.60	394.79	-1060.65	0	-2078.66	1.8	-210.36	1.8	-224.72	2.12	-57.51
120	121	22.00	-2175.60	445.32	-1519.28	0	-2571.90	1.8	84.37	1.8	-128.70	2.12	112.27
121	1121	22.00	-2219.11	-465.62	-1548.08	0	-2652.54	1.8	116.50	1.8	-128.70	2.12	112.27
121	122	23.40	-2219.11	-404.00	-942.94	0	-1992.02	1.8	-304.09	1.8	-251.45	2.12	-104.76
122	122	23.40	-2219.11	-402.74	-943.03	0	-1992.11	1.8	-304.06	1.8	-251.42	2.12	-104.72
122	123	24.80	-2219.11	-337.96	-425.50	0	-1429.96	1.8	-654.81	1.8	-357.51	2.12	-292.31
123	123	24.80	-2523.70	-336.49	-614.94	0	-1975.03	1.8	-458.32	1.8	-357.51	2.12	-292.31
123	124	26.20	-2523.70	-253.39	-212.06	0	-1534.40	1.8	-741.23	1.8	-438.87	2.12	-436.16
124	124	26.20	-1696.97	-253.04	-610.14	0	-1664.99	1.8	-370.56	1.8	-116.92	2.12	-36.82
124	125	27.60	-1696.97	-193.82	-299.24	0	-1323.90	1.8	-592.32	1.8	-179.27	2.12	-147.07
125	125	27.60	-2088.58	-193.78	-531.41	0	-2006.35	1.8	-366.90	1.8	-179.19	2.12	-146.92
125	126	29.00	-2088.58	-118.04	-328.48	0	-1780.30	1.8	-522.81	1.8	-218.50	2.12	-216.43
126	126	29.00	-1242.90	-112.78	-726.04	0	-2014.60	1.8	348.28	1.8	27.30	2.12	53.80
126	127	30.40	-1243.14	-87.78	-578.55	0	-1828.88	1.8	137.88	1.8	16.82	2.12	33.14
127	127	30.40	-1606.18	-93.09	-777.59	0	-2424.64	1.8	287.63	1.8	16.95	2.12	32.59
127	128	31.80	-1606.18	-70.67	-663.02	0	-2283.22	1.8	121.02	1.8	8.98	2.12	17.27
128	128	31.80	-1606.18	-70.19	-662.96	0	-2283.17	1.8	121.00	1.8	8.97	2.12	17.25
128	129	33.20	-1606.18	-47.93	-580.22	0	-2179.70	1.8	-3.39	1.8	3.55	2.12	6.82
129	129	33.20	-1606.18	-47.49	-580.18	0	-2179.67	1.8	-3.40	1.8	3.54	2.12	6.81
129	130	34.60	-1606.18	-24.05	-530.14	0	-2114.90	1.8	-85.24	1.8	0.78	2.12	1.50
130	130	34.60	-1606.18	-23.60	-530.16	0	-2114.92	1.8	-85.23	1.8	0.78	2.12	1.51
130	131	36.00	-1606.18	3.12	-516.37	0	-2091.72	1.8	-123.95	1.8	1.31	2.12	2.51
131	131	36.00	-1606.18	3.58	-516.36	0	-2091.71	1.8	-123.95	1.8	1.31	2.12	2.51
131	132	37.40	-1606.18	25.90	-536.99	0	-2108.63	1.8	-119.80	1.8	4.79	2.12	9.22
132	132	37.40	-1606.18	26.35	-537.00	0	-2108.64	1.8	-119.80	1.8	4.79	2.12	9.22
132	133	38.80	-1606.18	48.63	-589.49	0	-2163.55	1.8	-73.35	1.8	10.82	2.12	20.80
133	133	38.80	-1606.18	49.12	-589.52	0	-2163.57	1.8	-73.35	1.8	10.82	2.12	20.81

Combi_to.xls

Programa DINTEL PACADAR S.A.
FRECUENTEST.T0.MZ-

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.T0.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	71.41	-673.87	0	-2256.48	1.8	15.41	1.8	19.38	2.12	37.26
134	134	40.20	-1606.18	71.88	-673.92	0	-2256.51	1.8	15.42	1.8	19.39	2.12	37.28
134	135	41.60	-1606.18	94.31	-790.23	0	-2387.49	1.8	146.52	1.8	30.49	2.12	58.63
135	135	41.60	-1249.48	90.63	-591.18	0	-1800.95	1.8	-8.58	1.8	30.25	2.12	59.61
135	136	43.00	-1249.32	115.41	-739.27	0	-1975.52	1.8	163.57	1.8	43.85	2.12	86.41
136	136	43.00	-2088.58	119.12	-341.69	0	-1798.19	1.8	-502.27	1.8	-217.23	2.12	-214.19
136	137	44.40	-2088.58	186.76	-546.58	0	-2027.18	1.8	-342.46	1.8	-177.84	2.12	-144.54
137	137	44.40	-1696.97	186.93	-314.55	0	-1344.84	1.8	-567.84	1.8	-177.89	2.12	-144.63
137	138	45.80	-1696.97	243.33	-612.44	0	-1674.37	1.8	-346.53	1.8	-119.25	2.12	-40.93
138	138	45.80	-2523.70	243.49	-214.27	0	-1543.69	1.8	-717.24	1.8	-441.22	2.12	-440.32
138	139	47.20	-2523.70	309.00	-597.45	0	-1966.28	1.8	-436.74	1.8	-365.26	2.12	-306.02
139	139	47.20	-2219.11	309.54	-407.81	0	-1421.01	1.8	-633.28	1.8	-365.31	2.12	-306.10
139	140	48.60	-2212.66	391.39	-903.42	0	-1960.98	1.8	-283.60	1.8	-263.46	2.12	-127.34
140	140	48.60	-2212.49	392.67	-903.39	0	-1960.90	1.8	-283.55	1.8	-263.42	2.12	-127.30
140	141	50.00	-2212.49	457.14	-1496.27	0	-2610.57	1.8	136.79	1.8	-144.20	2.12	83.51
141	1141	50.00	-2212.71	-457.07	-1496.27	0	-2610.64	1.8	136.72	1.8	-144.26	2.12	83.45
141	142	51.40	-2212.71	-392.58	-903.50	0	-1961.07	1.8	-283.59	1.8	-263.45	2.12	-127.31
142	142	51.40	-2213.30	-391.30	-903.54	0	-1961.29	1.8	-283.76	1.8	-263.60	2.12	-127.45
142	143	52.80	-2213.30	-309.94	-407.93	0	-1419.34	1.8	-631.45	1.8	-363.72	2.12	-304.49
143	143	52.80	-2518.88	-309.37	-597.46	0	-1964.81	1.8	-435.25	1.8	-363.97	2.12	-304.72
143	144	54.20	-2523.70	-243.48	-214.26	0	-1543.68	1.8	-717.24	1.8	-441.22	2.12	-440.32
144	144	54.20	-1696.97	-243.34	-612.42	0	-1674.35	1.8	-346.54	1.8	-119.25	2.12	-40.94
144	145	55.60	-1696.97	-186.94	-314.50	0	-1344.80	1.8	-567.85	1.8	-177.90	2.12	-144.65
145	145	55.60	-2088.58	-186.76	-546.55	0	-2027.15	1.8	-342.46	1.8	-177.85	2.12	-144.55
145	146	57.00	-2088.58	-119.12	-341.67	0	-1798.18	1.8	-502.28	1.8	-217.24	2.12	-214.20
146	146	57.00	-1249.32	-115.42	-739.26	0	-1975.50	1.8	163.57	1.8	43.85	2.12	86.40
146	147	58.40	-1251.27	-91.56	-590.26	0	-1801.02	1.8	-12.15	1.8	30.25	2.12	59.61
147	147	58.40	-1608.20	-94.25	-789.30	0	-2387.74	1.8	142.76	1.8	30.49	2.12	58.63
147	148	59.80	-1608.20	-71.83	-673.12	0	-2256.92	1.8	11.87	1.8	19.39	2.12	37.28
148	148	59.80	-1608.20	-71.36	-673.05	0	-2256.87	1.8	11.86	1.8	19.38	2.12	37.26
148	149	61.20	-1608.20	-49.06	-588.77	0	-2164.08	1.8	-76.71	1.8	10.82	2.12	20.80
149	149	61.20	-1608.20	-48.58	-588.76	0	-2164.07	1.8	-76.71	1.8	10.82	2.12	20.80
149	150	62.60	-1608.20	-26.29	-536.33	0	-2109.26	1.8	-122.99	1.8	4.79	2.12	9.22
150	150	62.60	-1608.20	-25.84	-536.33	0	-2109.26	1.8	-122.99	1.8	4.79	2.12	9.22
150	151	64.00	-1609.94	-3.50	-515.82	0	-2093.95	1.8	-128.31	1.8	1.31	2.12	2.52
151	151	64.00	-1609.94	-3.04	-515.82	0	-2093.95	1.8	-128.31	1.8	1.31	2.12	2.52
151	152	65.40	-1609.94	23.68	-529.73	0	-2117.31	1.8	-89.36	1.8	0.79	2.12	1.52
152	152	65.40	-1609.94	24.13	-529.70	0	-2117.28	1.8	-89.36	1.8	0.78	2.12	1.51
152	153	66.80	-1609.94	47.56	-579.86	0	-2182.23	1.8	-7.26	1.8	3.54	2.12	6.81
153	153	66.80	-1609.94	48.01	-579.90	0	-2182.26	1.8	-7.26	1.8	3.55	2.12	6.82
153	154	68.20	-1609.94	70.27	-662.76	0	-2285.91	1.8	117.40	1.8	8.98	2.12	17.26
154	154	68.20	-1609.94	70.75	-662.81	0	-2285.95	1.8	117.41	1.8	8.99	2.12	17.28
154	155	69.60	-1609.94	93.17	-777.49	0	-2427.54	1.8	284.29	1.8	16.95	2.12	32.59
155	155	69.60	-1246.39	89.65	-578.45	0	-1831.37	1.8	134.94	1.8	16.82	2.12	33.15
155	156	71.00	-1242.90	112.78	-726.06	0	-2014.63	1.8	348.31	1.8	27.30	2.12	53.80
156	156	71.00	-2088.58	118.05	-328.50	0	-1780.32	1.8	-522.80	1.8	-218.49	2.12	-216.42
156	157	72.40	-2088.58	193.79	-531.41	0	-2006.36	1.8	-366.89	1.8	-179.19	2.12	-146.92
157	157	72.40	-1696.97	193.83	-299.24	0	-1323.89	1.8	-592.32	1.8	-179.27	2.12	-147.07
157	158	73.80	-1696.97	253.05	-610.16	0	-1665.01	1.8	-370.55	1.8	-116.92	2.12	-36.81
158	158	73.80	-2523.70	253.39	-212.08	0	-1534.41	1.8	-741.23	1.8	-438.86	2.12	-436.16
158	159	75.20	-2523.70	336.51	-614.95	0	-1975.04	1.8	-458.32	1.8	-357.51	2.12	-292.31
159	159	75.20	-2219.11	337.94	-425.51	0	-1429.96	1.8	-654.81	1.8	-357.51	2.12	-292.30
159	160	76.60	-2215.29	403.21	-943.56	0	-1991.43	1.8	-302.73	1.8	-250.27	2.12	-103.47
160	160	76.60	-2215.34	404.49	-943.58	0	-1991.47	1.8	-302.74	1.8	-250.27	2.12	-103.47
160	161	78.00	-2215.34	466.13	-1549.40	0	-2652.65	1.8	118.04	1.8	-127.36	2.12	113.87
161	1161	78.00	-2172.15	-445.47	-1520.65	0	-2572.16	1.8	85.83	1.8	-127.43	2.12	113.81
161	162	79.10	-2172.15	-394.96	-1061.84	0	-2078.75	1.8	-208.95	1.8	-223.50	2.12	-56.05
162	162	79.10	-2172.53	-393.99	-1061.91	0	-2078.93	1.8	-209.04	1.8	-223.58	2.12	-56.12
162	163	80.20	-2172.53	-323.42	-659.98	0	-1648.95	1.8	-459.91	1.8	-308.65	2.12	-206.54
163	163	80.20	-2477.65	-322.73	-852.65	0	-2199.21	1.8	-256.47	1.8	-308.75	2.12	-206.61
163	164	81.30	-2477.65	-266.08	-530.06	0	-1852.54	1.8	-462.94	1.8	-376.39	2.12	-326.21
164	164	81.30	-2478.35	-265.80	-530.26	0	-1852.95	1.8	-463.09	1.8	-376.52	2.12	-326.31
164	165	82.40	-2478.35	-215.85	-264.20	0	-1567.48	1.8	-631.90	1.8	-432.50	2.12	-425.28
165	165	82.40	-1870.06	-215.69	-794.87	0	-2083.69	1.8	-126.35	1.8	-110.93	2.12	-26.42
165	166	83.50	-1870.06	-188.16	-574.75	0	-1849.19	1.8	-260.53	1.8	-157.92	2.12	-109.51
166	166	83.50	-1871.02	-187.85	-574.53	0	-1822.80	1.8	-286.72	1.8	-180.67	2.12	-140.37
166	167	84.60	-1871.02	-143.25	-401.84	0	-1656.52	1.8	-370.46	1.8	-204.88	2.12	-188.67
167	167	84.60	-1016.26	-134.10	-799.42	0	-1853.60	1.8	409.08	1.8	50.27	2.12	99.05
167	168	85.70	-1019.75	-116.37	-652.64	0	-1684.49	1.8	235.08	1.8	36.83	2.12	72.58
168	168	85.70	-1261.85	-123.81	-783.56	0	-2068.81	1.8	328.37	1.8	37.13	2.12	71.39
168	169	86.80	-1261.85	-106.27	-657.03	0	-1925.91	1.8	184.55	1.8	25.14	2.12	48.34
169	169	86.80	-1261.85	-106.00	-657.00	0	-1925.88	1.8	184.55	1.8	25.13	2.12	48.33
169	170	87.90	-1261.85	-88.51	-549.99	0	-1806.32	1.8	66.78	1.8	14.69	2.12	28.25
170	170	87.90	-1261.85	-88.27	-549.99	0	-1806.32	1.8	66.78	1.8	14.69	2.12	28.25
170	171	89.00	-1261.85	-70.77	-462.51	0	-1710.09	1.8	-24.88	1.8	5.78	2.12	11.12

CÁLCULO TENSIONAL

Hipótesis de cálculo:

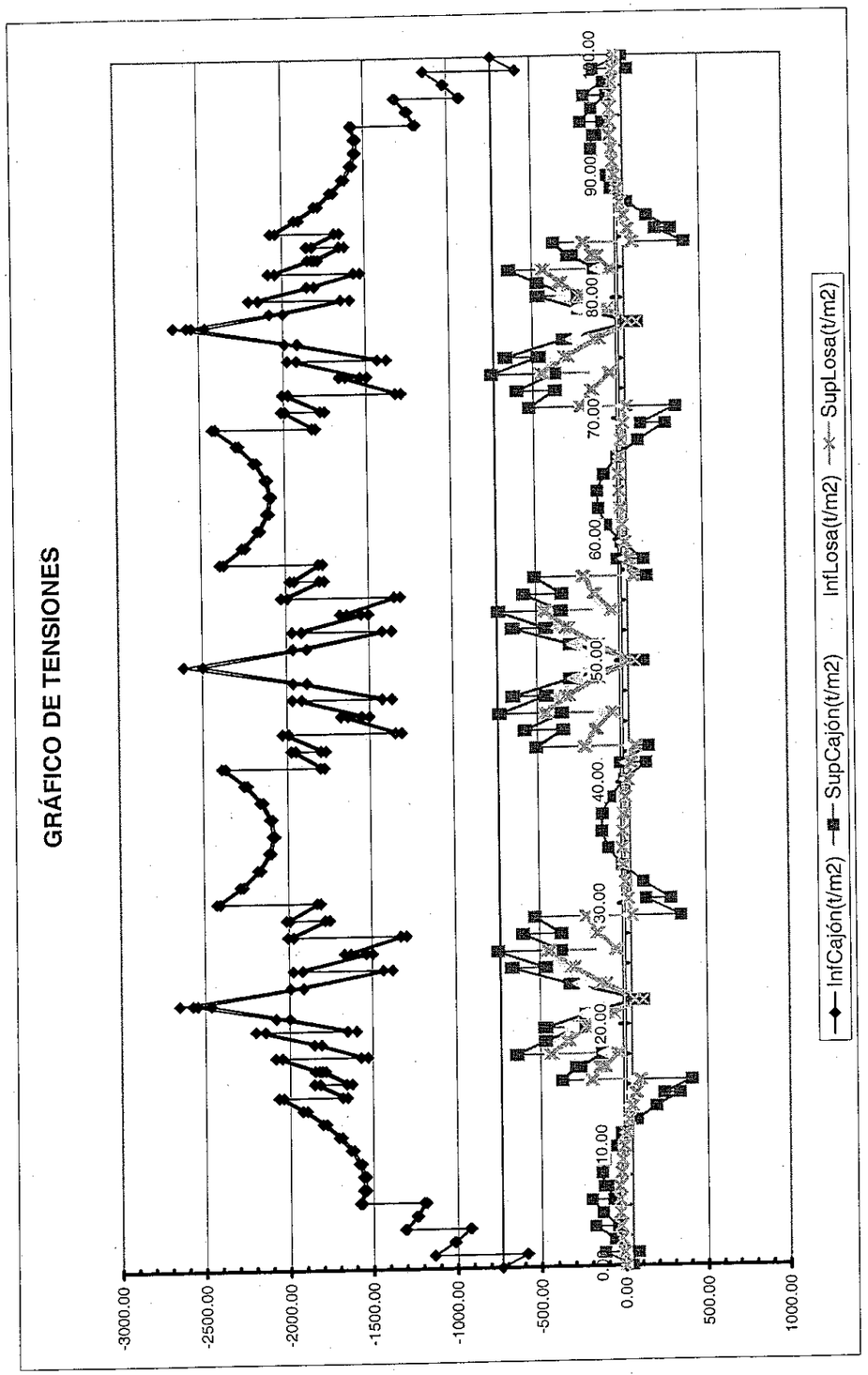
FRECUENTEST.T0.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1261.85	-70.55	-462.52	0	-1710.10	1.8	-24.88	1.8	5.79	2.12	11.13
171	172	90.10	-1261.85	-53.04	-394.58	0	-1637.25	1.8	-90.41	1.8	-1.58	2.12	-3.03
172	172	90.10	-1261.85	-52.85	-394.62	0	-1637.28	1.8	-90.40	1.8	-1.57	2.12	-3.02
172	173	91.20	-1261.85	-35.35	-346.10	0	-1587.66	1.8	-129.89	1.8	-7.41	2.12	-14.25
173	173	91.20	-1261.85	-35.24	-346.16	0	-1587.71	1.8	-129.88	1.8	-7.40	2.12	-14.23
173	174	92.30	-1261.85	-17.73	-317.04	0	-1561.33	1.8	-143.30	1.8	-11.72	2.12	-22.54
174	174	92.30	-1261.85	-17.61	-317.13	0	-1561.40	1.8	-143.28	1.8	-11.71	2.12	-22.51
174	175	93.40	-1261.85	-0.12	-307.38	0	-1558.25	1.8	-130.62	1.8	-14.52	2.12	-27.91
175	175	93.40	-1261.85	-0.05	-307.49	0	-1561.09	1.8	-113.06	1.8	-14.38	2.12	-28.34
175	176	94.50	-1261.85	17.47	-317.08	0	-1581.94	1.8	-74.40	1.8	-15.67	2.12	-30.88
176	176	94.50	-1044.29	17.50	-186.23	0	-1199.63	1.8	-204.61	1.8	-15.65	2.12	-30.84
176	177	95.60	-1044.29	35.01	-215.12	0	-1244.72	1.8	-140.00	1.8	-15.45	2.12	-30.45
177	177	95.60	-1044.29	34.94	-215.27	0	-1244.84	1.8	-139.97	1.8	-15.43	2.12	-30.40
177	178	96.70	-1044.29	52.44	-263.33	0	-1314.09	1.8	-49.39	1.8	-13.76	2.12	-27.12
178	178	96.70	-826.73	52.28	-130.32	0	-928.32	1.8	-184.67	1.8	-13.74	2.12	-27.07
178	179	97.80	-826.73	69.80	-197.47	0	-1021.63	1.8	-68.15	1.8	-10.62	2.12	-20.93
179	179	97.80	-826.73	69.57	-197.65	0	-1021.78	1.8	-68.12	1.8	-10.59	2.12	-20.87
179	180	98.90	-826.73	87.09	-263.79	0	-1139.08	1.8	74.31	1.8	-6.03	2.12	-11.89
180	180	98.90	-522.14	86.77	-91.49	0	-589.32	1.8	-129.22	1.8	-6.00	2.12	-11.82
180	181	100.00	-522.14	231.65	-198.43	0	-732.94	1.8	41.73	1.8	0.12	2.12	0.24



CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTESG.T0.MZ+

C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-138.19	-178.73	0	-662.45	1.8	37.60	1.8	-0.03	2.12	-0.05
1	2	1.10	-476.85	-166.99	18.81	0	-443.29	1.8	-157.02	1.8	-21.17	2.12	-41.72
2	2	1.10	-752.42	-166.78	-155.42	0	-940.90	1.8	27.17	1.8	-21.16	2.12	-41.70
2	3	2.20	-752.42	-142.76	14.17	0	-750.68	1.8	-134.02	1.8	-39.54	2.12	-77.92
3	3	2.20	-752.42	-142.58	14.10	0	-750.74	1.8	-134.01	1.8	-39.53	2.12	-77.90
3	4	3.30	-752.42	-118.54	156.63	0	-591.48	1.8	-267.70	1.8	-55.12	2.12	-108.62
4	4	3.30	-949.26	-118.37	36.12	0	-940.65	1.8	-145.28	1.8	-55.11	2.12	-108.60
4	5	4.40	-949.26	-93.12	151.61	0	-812.34	1.8	-251.45	1.8	-67.91	2.12	-133.82
5	5	4.40	-949.26	-92.97	151.57	0	-812.38	1.8	-251.45	1.8	-67.91	2.12	-133.81
5	6	5.50	-949.26	-68.52	241.56	0	-713.66	1.8	-330.47	1.8	-78.18	2.12	-154.04
6	6	5.50	-1146.10	-68.39	123.03	0	-1059.69	1.8	-212.64	1.8	-78.17	2.12	-154.03
6	7	6.60	-1146.10	-44.35	186.15	0	-991.76	1.8	-264.26	1.8	-85.67	2.12	-168.81
7	7	6.60	-1146.10	-44.24	186.13	0	-1011.02	1.8	-281.07	1.8	-86.37	2.12	-166.08
7	8	7.70	-1146.10	-20.22	222.35	0	-975.71	1.8	-305.30	1.8	-91.15	2.12	-175.27
8	8	7.70	-1146.10	-20.09	222.34	0	-975.72	1.8	-305.30	1.8	-91.15	2.12	-175.27
8	9	8.80	-1146.10	3.88	231.44	0	-969.98	1.8	-301.93	1.8	-93.10	2.12	-179.02
9	9	8.80	-1146.10	4.01	231.45	0	-969.97	1.8	-301.94	1.8	-93.10	2.12	-179.02
9	10	9.90	-1146.10	28.01	215.06	0	-992.45	1.8	-271.31	1.8	-92.50	2.12	-177.87
10	10	9.90	-1146.10	28.15	215.07	0	-992.44	1.8	-271.31	1.8	-92.50	2.12	-177.87
10	11	11.00	-1146.10	52.20	171.90	0	-1044.18	1.8	-213.20	1.8	-89.13	2.12	-171.39
11	11	11.00	-1146.10	52.33	171.93	0	-1044.16	1.8	-213.21	1.8	-89.14	2.12	-171.40
11	12	12.10	-1146.10	76.37	101.90	0	-1125.24	1.8	-127.56	1.8	-82.98	2.12	-159.57
12	12	12.10	-1146.10	76.54	101.94	0	-1125.21	1.8	-127.56	1.8	-82.99	2.12	-159.58
12	13	13.20	-1146.10	100.50	4.90	0	-1235.77	1.8	-14.31	1.8	-74.03	2.12	-142.35
13	13	13.20	-1146.10	100.68	4.94	0	-1235.74	1.8	-14.32	1.8	-74.04	2.12	-142.37
13	14	14.30	-1146.10	124.75	-118.02	0	-1374.85	1.8	126.18	1.8	-62.45	2.12	-120.08
14	14	14.30	-924.56	119.96	0.52	0	-997.91	1.8	44.84	1.8	-61.94	2.12	-122.06
14	15	15.40	-917.39	141.52	-151.22	0	-1168.45	1.8	223.30	1.8	-47.72	2.12	-94.02
15	15	15.40	-1858.58	150.36	288.35	0	-972.85	1.8	-553.62	1.8	-332.49	2.12	-419.99
15	16	16.50	-1858.58	142.19	115.63	0	-1139.16	1.8	-469.87	1.8	-308.27	2.12	-371.68
16	16	16.50	-1858.58	142.28	115.61	0	-1097.52	1.8	-510.52	1.8	-343.57	2.12	-419.70
16	17	17.60	-1858.58	158.93	-51.17	0	-1280.64	1.8	-391.09	1.8	-310.18	2.12	-360.65
17	17	17.60	-2575.51	159.07	509.15	0	-787.04	1.8	-923.96	1.8	-665.88	2.12	-801.80
17	18	18.70	-2575.51	171.21	325.70	0	-992.56	1.8	-779.23	1.8	-630.82	2.12	-739.80
18	18	18.70	-2575.50	171.36	325.62	0	-992.64	1.8	-779.20	1.8	-630.80	2.12	-739.76
18	19	19.80	-2575.50	184.60	129.53	0	-1216.89	1.8	-609.60	1.8	-595.17	2.12	-676.77
19	19	19.80	-2299.92	184.75	303.57	0	-719.45	1.8	-793.74	1.8	-595.14	2.12	-676.72
19	20	20.90	-2299.92	197.99	92.99	0	-964.24	1.8	-598.63	1.8	-558.50	2.12	-611.93
20	20	20.90	-2299.92	198.07	93.01	0	-964.22	1.8	-598.63	1.8	-558.51	2.12	-611.94
20	21	22.00	-2299.92	217.27	-135.54	0	-1234.78	1.8	-370.95	1.8	-520.72	2.12	-545.13
21	1021	22.00	-2339.29	-226.20	-161.62	0	-1307.76	1.8	-341.88	1.8	-520.72	2.12	-545.12
21	22	23.40	-2339.29	-199.54	137.51	0	-943.41	1.8	-673.29	1.8	-566.01	2.12	-625.21
22	22	23.40	-2339.29	-199.44	137.46	0	-943.45	1.8	-673.27	1.8	-566.00	2.12	-625.18
22	23	24.80	-2339.29	-181.85	404.71	0	-623.53	1.8	-951.09	1.8	-608.74	2.12	-700.76
23	23	24.80	-2614.86	-181.77	233.26	0	-1116.74	1.8	-773.30	1.8	-608.73	2.12	-700.74
23	24	26.20	-2614.86	-170.82	479.08	0	-828.11	1.8	-1010.44	1.8	-650.33	2.12	-774.31
24	24	26.20	-1701.11	-170.83	39.70	0	-971.87	1.8	-600.92	1.8	-294.65	2.12	-333.20
24	25	27.60	-1701.11	-152.22	265.10	0	-713.53	1.8	-797.77	1.8	-335.36	2.12	-405.18
25	25	27.60	-2055.42	-152.09	55.46	0	-1330.59	1.8	-593.94	1.8	-335.39	2.12	-405.23
25	26	29.00	-2055.42	-158.54	292.26	0	-1071.75	1.8	-759.72	1.8	-383.27	2.12	-489.90
26	26	29.00	-1122.96	-153.47	-147.30	0	-1361.91	1.8	161.10	1.8	-56.50	2.12	-111.33
26	27	30.40	-1129.71	-125.28	51.92	0	-1137.15	1.8	-63.72	1.8	-75.75	2.12	-149.26
27	27	30.40	-1460.38	-127.18	-128.28	0	-1704.82	1.8	68.93	1.8	-76.37	2.12	-146.84
27	28	31.80	-1460.38	-96.39	27.11	0	-1530.32	1.8	-104.71	1.8	-91.32	2.12	-175.60
28	28	31.80	-1460.38	-96.20	27.07	0	-1530.35	1.8	-104.71	1.8	-91.32	2.12	-175.59
28	29	33.20	-1460.38	-64.47	139.45	0	-1402.95	1.8	-233.93	1.8	-101.85	2.12	-195.83
29	29	33.20	-1460.38	-64.30	139.43	0	-1402.97	1.8	-233.93	1.8	-101.84	2.12	-195.83
29	30	34.60	-1460.38	-35.01	209.13	0	-1322.42	1.8	-318.69	1.8	-108.01	2.12	-207.68
30	30	34.60	-1460.38	-34.85	209.11	0	-1322.44	1.8	-318.68	1.8	-108.00	2.12	-207.67
30	31	36.00	-1460.38	-4.19	235.23	0	-1289.47	1.8	-358.85	1.8	-109.64	2.12	-210.83
31	31	36.00	-1460.38	-4.05	235.24	0	-1289.46	1.8	-358.85	1.8	-109.65	2.12	-210.84
31	32	37.40	-1460.38	27.78	219.05	0	-1303.05	1.8	-354.67	1.8	-106.98	2.12	-205.71
32	32	37.40	-1460.38	27.93	219.07	0	-1303.03	1.8	-354.67	1.8	-106.99	2.12	-205.72
32	33	38.80	-1460.38	57.22	159.28	0	-1364.22	1.8	-305.87	1.8	-99.80	2.12	-191.90
33	33	38.80	-1460.38	57.40	159.30	0	-1364.20	1.8	-305.87	1.8	-99.80	2.12	-191.91
33	34	40.20	-1460.38	89.14	56.84	0	-1472.23	1.8	-212.63	1.8	-88.25	2.12	-169.70
34	34	40.20	-1460.38	89.33	56.88	0	-1472.20	1.8	-212.64	1.8	-88.26	2.12	-169.71
34	35	41.60	-1460.38	120.12	-88.64	0	-1627.39	1.8	-74.90	1.8	-72.28	2.12	-138.98
35	35	41.60	-1135.74	119.79	91.54	0	-1066.19	1.8	-212.55	1.8	-71.69	2.12	-141.27
35	36	43.00	-1128.92	148.18	-98.98	0	-1273.71	1.8	-21.01	1.8	-51.41	2.12	-101.30
36	36	43.00	-2055.42	151.73	340.60	0	-1030.08	1.8	-757.12	1.8	-397.58	2.12	-515.20
36	37	44.40	-2055.42	146.11	120.15	0	-1274.11	1.8	-592.77	1.8	-354.26	2.12	-438.59
37	37	44.40	-1701.11	146.28	329.80	0	-657.04	1.8	-796.60	1.8	-354.23	2.12	-438.55
37	38	45.80	-1701.11	165.60	111.69	0	-909.35	1.8	-598.55	1.8	-315.78	2.12	-370.55
38	38	45.80	-2614.86	165.70	551.05	0	-765.62	1.8	-1008.06	1.8	-671.45	2.12	-811.65

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTESG.T0.MZ+

C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	178.37	310.89	0	-1049.79	1.8	-769.24	1.8	-631.70	2.12	-741.36
39	39	47.20	-2339.29	178.62	482.24	0	-556.67	1.8	-947.00	1.8	-631.68	2.12	-741.33
39	40	48.60	-2345.74	194.16	221.26	0	-873.54	1.8	-669.66	1.8	-592.67	2.12	-671.02
40	40	48.60	-2345.92	194.27	221.35	0	-873.51	1.8	-669.74	1.8	-592.74	2.12	-671.11
40	41	50.00	-2345.92	220.73	-70.44	0	-1231.77	1.8	-337.14	1.8	-549.72	2.12	-595.05
41	1041	50.00	-2345.70	-220.81	-70.43	0	-1231.70	1.8	-337.08	1.8	-549.67	2.12	-594.99
41	42	51.40	-2345.70	-194.36	221.48	0	-873.31	1.8	-669.72	1.8	-592.72	2.12	-671.11
42	42	51.40	-2345.10	-194.25	221.39	0	-873.21	1.8	-669.51	1.8	-592.53	2.12	-670.91
42	43	52.80	-2345.10	-178.21	482.40	0	-558.32	1.8	-948.83	1.8	-633.28	2.12	-742.96
43	43	52.80	-2619.68	-178.01	310.93	0	-1051.23	1.8	-770.73	1.8	-633.00	2.12	-742.66
43	44	54.20	-2614.86	-165.70	551.04	0	-765.63	1.8	-1008.06	1.8	-671.45	2.12	-811.65
44	44	54.20	-1701.11	-165.60	111.68	0	-909.36	1.8	-598.55	1.8	-315.78	2.12	-370.55
44	45	55.60	-1701.11	-146.28	329.82	0	-657.02	1.8	-796.61	1.8	-354.24	2.12	-438.56
45	45	55.60	-2055.42	-146.11	120.15	0	-1274.11	1.8	-592.77	1.8	-354.26	2.12	-438.59
45	46	57.00	-2055.42	-151.73	340.61	0	-1030.07	1.8	-757.12	1.8	-397.59	2.12	-515.21
46	46	57.00	-1128.92	-148.19	-98.96	0	-1273.68	1.8	-21.04	1.8	-51.41	2.12	-101.31
46	47	58.40	-1133.95	-118.88	90.66	0	-1066.08	1.8	-209.01	1.8	-71.69	2.12	-141.27
47	47	58.40	-1458.36	-120.18	-89.53	0	-1627.11	1.8	-71.17	1.8	-72.28	2.12	-138.98
47	48	59.80	-1458.36	-89.39	56.09	0	-1471.78	1.8	-209.10	1.8	-88.26	2.12	-169.72
48	48	59.80	-1458.36	-89.19	56.05	0	-1471.81	1.8	-209.09	1.8	-88.26	2.12	-169.71
48	49	61.20	-1458.36	-57.46	158.56	0	-1363.69	1.8	-302.49	1.8	-99.80	2.12	-191.91
49	49	61.20	-1458.36	-57.28	158.53	0	-1363.72	1.8	-302.49	1.8	-99.80	2.12	-191.90
49	50	62.60	-1458.36	-27.99	218.42	0	-1302.38	1.8	-351.50	1.8	-106.99	2.12	-205.72
50	50	62.60	-1458.36	-27.83	218.41	0	-1302.40	1.8	-351.50	1.8	-106.99	2.12	-205.72
50	51	64.00	-1456.62	3.98	234.68	0	-1287.25	1.8	-354.47	1.8	-109.65	2.12	-210.84
51	51	64.00	-1456.62	4.11	234.68	0	-1287.25	1.8	-354.47	1.8	-109.65	2.12	-210.84
51	52	65.40	-1456.62	34.76	208.67	0	-1320.05	1.8	-314.56	1.8	-108.00	2.12	-207.68
52	52	65.40	-1456.62	34.93	208.68	0	-1320.04	1.8	-314.56	1.8	-108.01	2.12	-207.68
52	53	66.80	-1456.62	64.22	139.11	0	-1400.40	1.8	-230.06	1.8	-101.85	2.12	-195.83
53	53	66.80	-1456.62	64.40	139.13	0	-1400.39	1.8	-230.07	1.8	-101.85	2.12	-195.84
53	54	68.20	-1456.62	96.12	26.87	0	-1527.60	1.8	-101.13	1.8	-91.32	2.12	-175.60
54	54	68.20	-1456.62	96.31	26.91	0	-1527.57	1.8	-101.13	1.8	-91.33	2.12	-175.61
54	55	69.60	-1456.62	127.10	-128.37	0	-1701.91	1.8	72.25	1.8	-76.37	2.12	-146.85
55	55	69.60	-1126.45	123.42	51.83	0	-1134.64	1.8	-60.81	1.8	-75.75	2.12	-149.27
55	56	71.00	-1122.96	153.48	-147.29	0	-1361.92	1.8	161.11	1.8	-56.50	2.12	-111.34
56	56	71.00	-2055.42	158.54	292.27	0	-1071.74	1.8	-759.72	1.8	-383.27	2.12	-489.90
56	57	72.40	-2055.42	152.09	55.47	0	-1330.57	1.8	-593.94	1.8	-335.39	2.12	-405.24
57	57	72.40	-1701.11	152.24	265.11	0	-713.52	1.8	-797.77	1.8	-335.36	2.12	-405.19
57	58	73.80	-1701.11	170.84	39.70	0	-971.87	1.8	-600.92	1.8	-294.65	2.12	-333.19
58	58	73.80	-2614.86	170.82	479.08	0	-828.11	1.8	-1010.44	1.8	-650.33	2.12	-774.30
58	59	75.20	-2614.86	181.77	233.25	0	-1116.76	1.8	-773.30	1.8	-608.72	2.12	-700.73
59	59	75.20	-2339.29	181.85	404.71	0	-623.53	1.8	-951.09	1.8	-608.74	2.12	-700.76
59	60	76.60	-2343.12	198.96	137.97	0	-944.14	1.8	-674.60	1.8	-567.15	2.12	-626.44
60	60	76.60	-2343.06	199.05	138.10	0	-944.00	1.8	-674.62	1.8	-567.17	2.12	-626.48
60	61	78.00	-2343.06	225.71	-160.33	0	-1307.68	1.8	-343.42	1.8	-522.05	2.12	-546.71
61	1061	78.00	-2303.37	-217.12	-134.22	0	-1234.57	1.8	-372.40	1.8	-521.98	2.12	-546.64
61	62	79.10	-2303.37	-197.92	94.15	0	-964.18	1.8	-600.03	1.8	-559.72	2.12	-613.37
62	62	79.10	-2302.99	-197.84	94.13	0	-964.08	1.8	-599.91	1.8	-559.61	2.12	-613.26
62	63	80.20	-2302.99	-184.59	304.55	0	-719.45	1.8	-794.97	1.8	-596.21	2.12	-677.98
63	63	80.20	-2578.03	-184.44	130.49	0	-1216.74	1.8	-610.66	1.8	-596.09	2.12	-677.88
63	64	81.30	-2578.03	-171.20	326.40	0	-992.67	1.8	-780.21	1.8	-631.67	2.12	-740.79
64	64	81.30	-2577.33	-171.06	326.41	0	-992.44	1.8	-780.00	1.8	-631.49	2.12	-740.61
64	65	82.40	-2577.33	-158.92	509.71	0	-787.06	1.8	-924.68	1.8	-666.51	2.12	-802.54
65	65	82.40	-1859.54	-158.83	-50.32	0	-1279.87	1.8	-392.42	1.8	-310.55	2.12	-361.11
65	66	83.50	-1859.54	-142.17	115.98	0	-1097.46	1.8	-510.92	1.8	-343.92	2.12	-420.12
66	66	83.50	-1858.58	-142.18	115.88	0	-1138.95	1.8	-469.91	1.8	-308.31	2.12	-371.77
66	67	84.60	-1858.58	-150.36	288.59	0	-972.64	1.8	-553.66	1.8	-332.53	2.12	-420.07
67	67	84.60	-917.40	-141.50	-150.97	0	-1168.09	1.8	222.74	1.8	-47.72	2.12	-94.03
67	68	85.70	-920.89	-117.47	-0.58	0	-996.60	1.8	50.45	1.8	-61.95	2.12	-122.07
68	68	85.70	-1141.67	-124.84	-119.13	0	-1372.94	1.8	132.41	1.8	-62.45	2.12	-120.08
68	69	86.80	-1141.67	-100.76	3.92	0	-1233.68	1.8	-8.32	1.8	-74.04	2.12	-142.37
69	69	86.80	-1141.67	-100.59	3.89	0	-1233.71	1.8	-8.31	1.8	-74.03	2.12	-142.36
69	70	87.90	-1141.67	-76.62	100.98	0	-1123.06	1.8	-121.71	1.8	-82.99	2.12	-159.58
70	70	87.90	-1141.67	-76.46	100.95	0	-1123.08	1.8	-121.71	1.8	-82.99	2.12	-159.57
70	71	89.00	-1141.67	-52.42	171.06	0	-1041.87	1.8	-207.56	1.8	-89.14	2.12	-171.40
71	71	89.00	-1141.67	-52.29	171.04	0	-1041.88	1.8	-207.56	1.8	-89.13	2.12	-171.39
71	72	90.10	-1141.67	-28.24	214.31	0	-989.99	1.8	-265.89	1.8	-92.51	2.12	-177.88
72	72	90.10	-1141.67	-28.10	214.30	0	-990.00	1.8	-265.89	1.8	-92.50	2.12	-177.87
72	73	91.20	-1141.67	-4.10	230.77	0	-967.39	1.8	-296.72	1.8	-93.10	2.12	-179.03
73	73	91.20	-1141.67	-3.98	230.77	0	-967.40	1.8	-296.72	1.8	-93.10	2.12	-179.03
73	74	92.30	-1141.67	19.99	221.75	0	-973.01	1.8	-300.28	1.8	-91.15	2.12	-175.27
74	74	92.30	-1141.67	20.12	221.76	0	-973.01	1.8	-300.28	1.8	-91.15	2.12	-175.27
74	75	93.40	-1141.67	44.15	185.63	0	-1008.18	1.8	-276.25	1.8	-86.38	2.12	-166.09
75	75	93.40	-1141.67	44.26	185.64	0	-989.02	1.8	-259.52	1.8	-85.67	2.12	-168.82
75	76	94.50	-1141.67	68.30	122.61	0	-1056.82	1.8	-208.11	1.8	-78.17	2.12	-154.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.T0.MZ+
5. Frecuentes dominante GRAD
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	68.44	241.14	0	-710.79	1.8	-325.94	1.8	-78.18	2.12	-154.04
76	77	95.60	-944.83	92.88	151.24	0	-809.36	1.8	-247.12	1.8	-67.91	2.12	-133.81
77	77	95.60	-944.83	93.03	151.29	0	-809.32	1.8	-247.13	1.8	-67.92	2.12	-133.83
77	78	96.70	-944.83	118.27	35.85	0	-937.54	1.8	-141.11	1.8	-55.11	2.12	-108.60
78	78	96.70	-747.99	118.45	156.38	0	-588.35	1.8	-263.53	1.8	-55.12	2.12	-108.62
78	79	97.80	-747.99	142.48	13.91	0	-747.49	1.8	-130.04	1.8	-39.53	2.12	-77.90
79	79	97.80	-747.99	142.66	13.99	0	-747.43	1.8	-130.05	1.8	-39.54	2.12	-77.92
79	80	98.90	-747.99	166.68	-155.50	0	-937.49	1.8	30.91	1.8	-21.16	2.12	-41.70
80	80	98.90	-472.42	166.90	18.73	0	-439.88	1.8	-153.27	1.8	-21.17	2.12	-41.72
80	81	100.00	-472.42	138.18	-178.73	0	-662.45	1.8	37.60	1.8	-0.03	2.12	-0.05
101	101	0.00	-472.42	-156.14	-178.67	0	-662.40	1.8	37.59	1.8	-0.04	2.12	-0.07
101	102	1.10	-476.85	-162.30	13.31	0	-448.04	1.8	-155.95	1.8	-20.25	2.12	-39.90
102	102	1.10	-752.42	-162.37	-160.82	0	-945.56	1.8	28.22	1.8	-20.25	2.12	-39.91
102	103	2.20	-752.42	-138.95	4.07	0	-759.40	1.8	-132.07	1.8	-37.85	2.12	-74.58
103	103	2.20	-752.42	-139.01	4.10	0	-759.37	1.8	-132.07	1.8	-37.85	2.12	-74.58
103	104	3.30	-752.42	-115.60	142.81	0	-603.41	1.8	-265.02	1.8	-52.80	2.12	-104.03
104	104	3.30	-949.26	-115.63	22.36	0	-952.53	1.8	-142.61	1.8	-52.80	2.12	-104.04
104	105	4.40	-949.26	-92.22	134.99	0	-826.68	1.8	-248.26	1.8	-65.12	2.12	-128.31
105	105	4.40	-949.26	-92.27	134.99	0	-826.68	1.8	-248.26	1.8	-65.12	2.12	-128.32
105	106	5.50	-949.26	-66.89	223.10	0	-729.59	1.8	-326.92	1.8	-75.07	2.12	-147.92
106	106	5.50	-1146.10	-66.95	104.62	0	-1075.58	1.8	-209.09	1.8	-75.07	2.12	-147.93
106	107	6.60	-1146.10	-43.52	166.68	0	-1008.56	1.8	-260.50	1.8	-82.40	2.12	-162.36
107	107	6.60	-1146.10	-43.57	166.68	0	-1026.93	1.8	-277.28	1.8	-83.08	2.12	-159.75
107	108	7.70	-1146.10	-20.17	202.63	0	-991.84	1.8	-301.45	1.8	-87.81	2.12	-168.84
108	108	7.70	-1146.10	-20.22	202.63	0	-991.85	1.8	-301.45	1.8	-87.81	2.12	-168.84
108	109	8.80	-1146.10	3.19	212.47	0	-985.49	1.8	-298.23	1.8	-89.89	2.12	-172.84
109	109	8.80	-1146.10	3.13	212.47	0	-985.49	1.8	-298.23	1.8	-89.89	2.12	-172.84
109	110	9.90	-1146.10	26.53	197.50	0	-1006.81	1.8	-267.88	1.8	-89.53	2.12	-172.14
110	110	9.90	-1146.10	26.47	197.48	0	-1006.83	1.8	-267.88	1.8	-89.52	2.12	-172.14
110	111	11.00	-1146.10	49.90	156.70	0	-1056.62	1.8	-210.24	1.8	-86.55	2.12	-166.43
111	111	11.00	-1146.10	49.81	156.67	0	-1056.64	1.8	-210.23	1.8	-86.55	2.12	-166.42
111	112	12.10	-1146.10	73.24	89.88	0	-1135.08	1.8	-125.21	1.8	-80.95	2.12	-155.65
112	112	12.10	-1146.10	73.14	89.85	0	-1135.10	1.8	-125.20	1.8	-80.94	2.12	-155.64
112	113	13.20	-1146.10	96.52	-2.90	0	-1242.15	1.8	-12.81	1.8	-72.71	2.12	-139.81
113	113	13.20	-1146.10	96.40	-2.93	0	-1242.18	1.8	-12.80	1.8	-72.70	2.12	-139.80
113	114	14.30	-1146.10	119.83	-120.72	0	-1377.06	1.8	126.72	1.8	-61.99	2.12	-119.20
114	114	14.30	-924.56	114.74	-2.25	0	-1000.31	1.8	45.38	1.8	-61.48	2.12	-121.14
114	115	15.40	-917.39	135.65	-147.73	0	-1165.44	1.8	222.63	1.8	-48.30	2.12	-95.18
115	115	15.40	-1858.58	144.11	291.76	0	-969.92	1.8	-554.25	1.8	-333.04	2.12	-421.09
115	116	16.50	-1858.58	140.70	126.54	0	-1129.77	1.8	-471.91	1.8	-310.04	2.12	-375.23
116	116	16.50	-1858.58	140.68	126.55	0	-1086.93	1.8	-513.70	1.8	-346.34	2.12	-424.59
116	117	17.60	-1858.58	157.05	-38.29	0	-1268.17	1.8	-394.84	1.8	-313.44	2.12	-366.42
117	117	17.60	-2575.50	157.01	522.08	0	-774.53	1.8	-927.72	1.8	-669.15	2.12	-807.59
117	118	18.70	-2575.50	166.15	342.54	0	-976.27	1.8	-784.13	1.8	-635.08	2.12	-747.33
118	118	18.70	-2575.50	166.07	342.45	0	-976.35	1.8	-784.11	1.8	-635.06	2.12	-747.29
118	119	19.80	-2575.50	176.54	153.73	0	-1193.47	1.8	-616.65	1.8	-601.30	2.12	-687.60
119	119	19.80	-2299.92	176.34	327.81	0	-695.99	1.8	-800.80	1.8	-601.28	2.12	-687.57
119	120	20.90	-2299.92	187.13	127.83	0	-930.53	1.8	-608.78	1.8	-567.32	2.12	-627.52
120	120	20.90	-2299.92	186.84	127.81	0	-930.54	1.8	-608.78	1.8	-567.31	2.12	-627.51
120	121	22.00	-2299.92	206.73	-89.37	0	-1190.10	1.8	-384.41	1.8	-532.41	2.12	-565.79
121	1121	22.00	-2339.29	-215.98	-115.44	0	-1263.07	1.8	-355.34	1.8	-532.41	2.12	-565.79
121	122	23.40	-2339.29	-190.72	170.00	0	-911.96	1.8	-682.76	1.8	-574.23	2.12	-639.75
122	122	23.40	-2339.29	-191.06	170.04	0	-911.93	1.8	-682.77	1.8	-574.24	2.12	-639.76
122	123	24.80	-2339.29	-174.49	426.46	0	-602.49	1.8	-957.42	1.8	-614.24	2.12	-710.49
123	123	24.80	-2614.86	-174.87	255.07	0	-1095.63	1.8	-779.66	1.8	-614.25	2.12	-710.50
123	124	26.20	-2614.86	-166.87	492.44	0	-815.19	1.8	-1014.34	1.8	-653.71	2.12	-780.28
124	124	26.20	-1701.11	-166.97	53.05	0	-958.95	1.8	-604.81	1.8	-298.03	2.12	-339.17
124	125	27.60	-1701.11	-149.55	274.02	0	-704.90	1.8	-800.36	1.8	-337.62	2.12	-409.17
125	125	27.60	-2055.42	-149.58	64.36	0	-1321.97	1.8	-596.53	1.8	-337.64	2.12	-409.22
125	126	29.00	-2055.42	-153.03	291.66	0	-1072.33	1.8	-759.54	1.8	-383.12	2.12	-489.63
126	126	29.00	-1122.96	-148.43	-147.80	0	-1362.35	1.8	161.21	1.8	-56.42	2.12	-111.17
126	127	30.40	-1129.71	-120.94	44.64	0	-1143.43	1.8	-62.31	1.8	-74.53	2.12	-146.85
127	127	30.40	-1460.38	-123.23	-135.46	0	-1710.69	1.8	70.33	1.8	-75.15	2.12	-144.50
127	128	31.80	-1460.38	-93.18	14.70	0	-1540.47	1.8	-102.29	1.8	-89.22	2.12	-171.56
128	128	31.80	-1460.38	-93.34	14.74	0	-1540.44	1.8	-102.30	1.8	-89.23	2.12	-171.57
128	129	33.20	-1460.38	-62.17	123.50	0	-1415.99	1.8	-230.84	1.8	-99.14	2.12	-190.63
129	129	33.20	-1460.38	-62.31	123.52	0	-1415.97	1.8	-230.84	1.8	-99.14	2.12	-190.64
129	130	34.60	-1460.38	-34.07	191.19	0	-1337.09	1.8	-315.19	1.8	-104.97	2.12	-201.83
130	130	34.60	-1460.38	-34.21	191.21	0	-1337.07	1.8	-315.19	1.8	-104.97	2.12	-201.84
130	131	36.00	-1460.38	-4.28	216.66	0	-1304.66	1.8	-355.25	1.8	-106.50	2.12	-204.77
131	131	36.00	-1460.38	-4.41	216.66	0	-1304.66	1.8	-355.25	1.8	-106.49	2.12	-204.77
131	132	37.40	-1460.38	26.93	201.41	0	-1317.48	1.8	-351.21	1.8	-103.99	2.12	-199.97
132	132	37.40	-1460.38	26.78	201.39	0	-1317.50	1.8	-351.20	1.8	-103.99	2.12	-199.96
132	133	38.80	-1460.38	55.02	143.88	0	-1376.82	1.8	-302.84	1.8	-97.19	2.12	-186.89
133	133	38.80	-1460.38	54.87	143.87	0	-1376.83	1.8	-302.84	1.8	-97.19	2.12	-186.88

CÁLCULO TENSIONAL

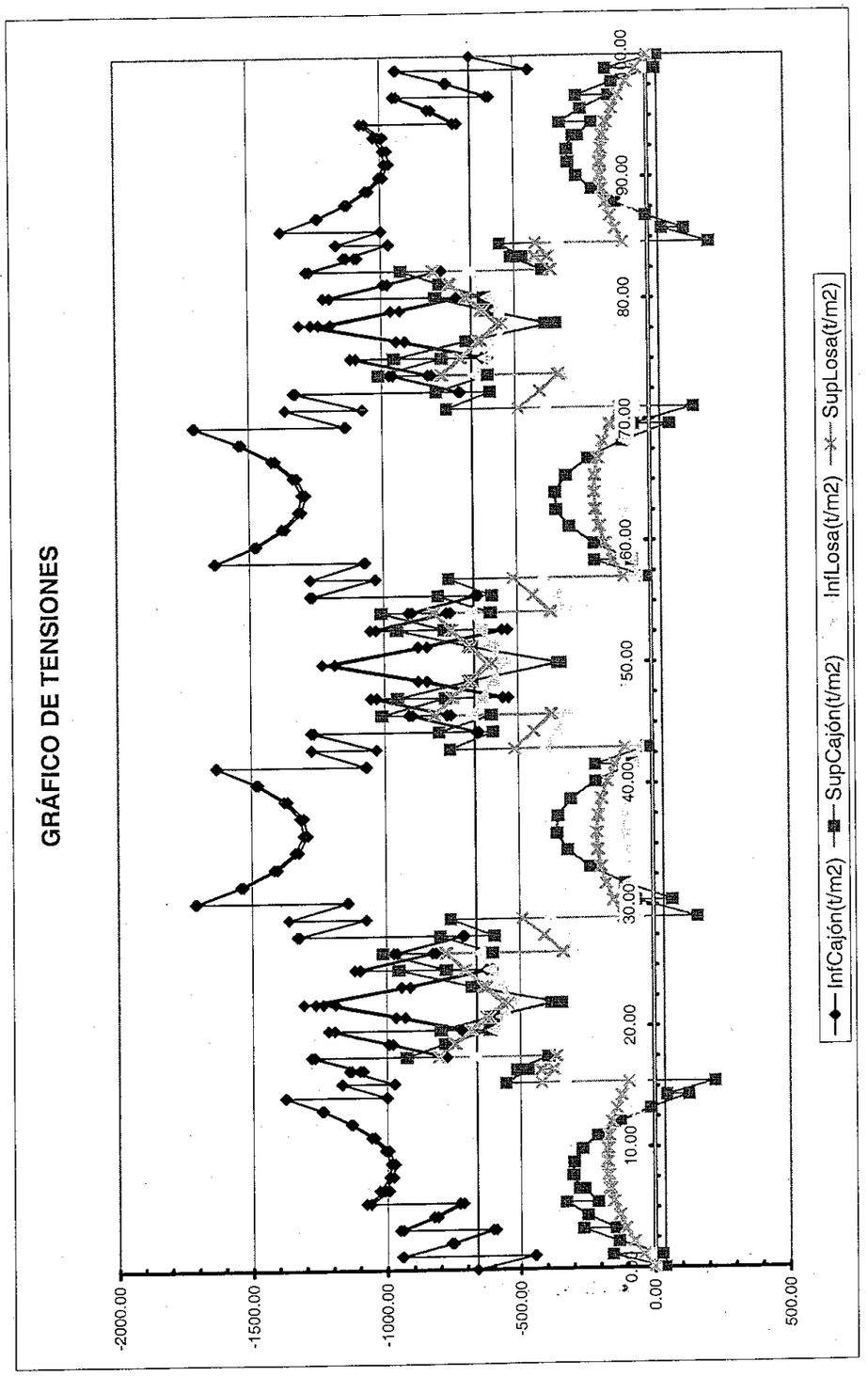
Hipótesis de cálculo:
FRECUENTESG.T0.MZ+
C. Frecuentes dominante GRAD
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	86.05	45.38	0	-1481.61	1.8	-210.39	1.8	-86.31	2.12	-165.96
134	134	40.20	-1460.38	85.89	45.34	0	-1481.64	1.8	-210.39	1.8	-86.30	2.12	-165.95
134	135	41.60	-1460.38	115.91	-94.63	0	-1632.29	1.8	-73.73	1.8	-71.26	2.12	-137.02
135	135	41.60	-1135.74	115.17	85.47	0	-1071.43	1.8	-211.38	1.8	-70.67	2.12	-139.25
135	136	43.00	-1128.92	142.82	-97.86	0	-1272.74	1.8	-21.23	1.8	-51.60	2.12	-101.68
136	136	43.00	-2055.42	145.87	341.60	0	-1029.11	1.8	-757.41	1.8	-397.84	2.12	-515.65
136	137	44.40	-2055.42	143.78	130.14	0	-1264.44	1.8	-595.68	1.8	-356.78	2.12	-443.06
137	137	44.40	-1701.11	143.74	339.80	0	-647.37	1.8	-799.52	1.8	-356.76	2.12	-443.02
137	138	45.80	-1701.11	161.81	126.19	0	-895.32	1.8	-602.77	1.8	-319.45	2.12	-377.04
138	138	45.80	-2614.86	161.77	565.55	0	-751.58	1.8	-1012.29	1.8	-675.13	2.12	-818.15
138	139	47.20	-2614.86	171.23	333.76	0	-1027.65	1.8	-775.90	1.8	-637.49	2.12	-751.59
139	139	47.20	-2339.29	171.07	505.10	0	-534.55	1.8	-953.66	1.8	-637.47	2.12	-751.56
139	140	48.60	-2345.74	185.55	255.76	0	-840.15	1.8	-679.72	1.8	-601.40	2.12	-686.47
140	140	48.60	-2345.92	185.17	255.79	0	-840.17	1.8	-679.78	1.8	-601.46	2.12	-686.53
140	141	50.00	-2345.92	210.20	-21.94	0	-1184.84	1.8	-351.28	1.8	-562.00	2.12	-616.75
141	1141	50.00	-2345.71	-210.29	-21.94	0	-1184.77	1.8	-351.22	1.8	-561.94	2.12	-616.70
141	142	51.40	-2345.71	-185.26	255.92	0	-839.99	1.8	-679.76	1.8	-601.44	2.12	-686.53
142	142	51.40	-2345.10	-185.62	255.89	0	-839.82	1.8	-679.56	1.8	-601.27	2.12	-686.35
142	143	52.80	-2345.10	-170.64	505.25	0	-536.19	1.8	-955.49	1.8	-639.06	2.12	-753.19
143	143	52.80	-2619.68	-170.87	333.81	0	-1029.09	1.8	-777.40	1.8	-638.79	2.12	-752.90
143	144	54.20	-2614.86	-161.77	565.55	0	-751.59	1.8	-1012.29	1.8	-675.12	2.12	-818.14
144	144	54.20	-1701.11	-161.82	126.19	0	-895.32	1.8	-602.77	1.8	-319.45	2.12	-377.04
144	145	55.60	-1701.11	-143.75	339.81	0	-647.36	1.8	-799.52	1.8	-356.76	2.12	-443.03
145	145	55.60	-2055.42	-143.79	130.14	0	-1264.44	1.8	-595.68	1.8	-356.79	2.12	-443.06
145	146	57.00	-2055.42	-145.87	341.62	0	-1029.09	1.8	-757.42	1.8	-397.84	2.12	-515.66
146	146	57.00	-1128.92	-142.83	-97.83	0	-1272.72	1.8	-21.24	1.8	-51.60	2.12	-101.68
146	147	58.40	-1133.95	-114.27	84.61	0	-1071.30	1.8	-207.85	1.8	-70.67	2.12	-139.26
147	147	58.40	-1458.36	-115.98	-95.50	0	-1631.99	1.8	-70.03	1.8	-71.26	2.12	-137.03
147	148	59.80	-1458.36	-85.95	44.54	0	-1481.23	1.8	-206.84	1.8	-86.31	2.12	-165.96
148	148	59.80	-1458.36	-86.11	44.58	0	-1481.20	1.8	-206.85	1.8	-86.31	2.12	-165.97
148	149	61.20	-1458.36	-54.93	143.15	0	-1376.30	1.8	-299.48	1.8	-97.19	2.12	-186.89
149	149	61.20	-1458.36	-55.08	143.17	0	-1376.28	1.8	-299.49	1.8	-97.20	2.12	-186.89
149	150	62.60	-1458.36	-26.84	200.77	0	-1316.82	1.8	-348.06	1.8	-104.00	2.12	-199.97
150	150	62.60	-1458.36	-26.98	200.79	0	-1316.81	1.8	-348.06	1.8	-104.00	2.12	-199.97
150	151	64.00	-1456.62	4.33	216.11	0	-1302.45	1.8	-350.84	1.8	-106.50	2.12	-204.78
151	151	64.00	-1456.62	4.20	216.11	0	-1302.44	1.8	-350.84	1.8	-106.50	2.12	-204.78
151	152	65.40	-1456.62	34.13	190.77	0	-1334.69	1.8	-311.07	1.8	-104.97	2.12	-201.84
152	152	65.40	-1456.62	33.99	190.76	0	-1334.70	1.8	-311.07	1.8	-104.97	2.12	-201.84
152	153	66.80	-1456.62	62.22	123.20	0	-1413.40	1.8	-226.98	1.8	-99.15	2.12	-190.65
153	153	66.80	-1456.62	62.09	123.18	0	-1413.42	1.8	-226.98	1.8	-99.14	2.12	-190.64
153	154	68.20	-1456.62	93.26	14.53	0	-1537.71	1.8	-98.70	1.8	-89.23	2.12	-171.58
154	154	68.20	-1456.62	93.10	14.49	0	-1537.74	1.8	-98.69	1.8	-89.22	2.12	-171.56
154	155	69.60	-1456.62	123.15	-135.56	0	-1707.79	1.8	73.68	1.8	-75.15	2.12	-144.51
155	155	69.60	-1126.45	119.06	44.55	0	-1140.93	1.8	-59.38	1.8	-74.53	2.12	-146.86
155	156	71.00	-1122.96	148.43	-147.79	0	-1362.35	1.8	161.23	1.8	-56.42	2.12	-111.18
156	156	71.00	-2055.42	153.04	291.68	0	-1072.31	1.8	-759.55	1.8	-383.12	2.12	-489.63
156	157	72.40	-2055.42	149.58	64.38	0	-1321.95	1.8	-596.54	1.8	-337.65	2.12	-409.23
157	157	72.40	-1701.11	149.56	274.03	0	-704.88	1.8	-800.37	1.8	-337.62	2.12	-409.18
157	158	73.80	-1701.11	166.98	53.05	0	-958.95	1.8	-604.81	1.8	-298.03	2.12	-339.17
158	158	73.80	-2614.86	166.87	492.43	0	-815.20	1.8	-1014.33	1.8	-653.71	2.12	-780.28
158	159	75.20	-2614.86	174.87	255.06	0	-1095.64	1.8	-779.65	1.8	-614.25	2.12	-710.50
159	159	75.20	-2339.29	174.48	426.47	0	-602.48	1.8	-957.43	1.8	-614.24	2.12	-710.49
159	160	76.60	-2343.12	190.59	170.55	0	-912.61	1.8	-684.09	1.8	-575.40	2.12	-641.02
160	160	76.60	-2343.06	190.22	170.59	0	-912.55	1.8	-684.09	1.8	-575.39	2.12	-641.02
160	161	78.00	-2343.06	215.48	-114.15	0	-1262.98	1.8	-356.88	1.8	-533.74	2.12	-567.38
161	1161	78.00	-2303.37	-206.58	-88.06	0	-1189.89	1.8	-385.85	1.8	-533.66	2.12	-567.30
161	162	79.10	-2303.37	-186.70	128.96	0	-930.49	1.8	-610.17	1.8	-568.53	2.12	-628.95
162	162	79.10	-2302.99	-186.97	128.97	0	-930.37	1.8	-610.06	1.8	-568.43	2.12	-628.85
162	163	80.20	-2302.99	-176.19	328.79	0	-695.99	1.8	-802.03	1.8	-602.35	2.12	-688.82
163	163	80.20	-2578.03	-176.38	154.67	0	-1193.33	1.8	-617.70	1.8	-602.22	2.12	-688.70
163	164	81.30	-2578.03	-165.90	343.23	0	-976.38	1.8	-785.12	1.8	-635.93	2.12	-748.32
164	164	81.30	-2577.33	-166.00	343.25	0	-976.14	1.8	-784.91	1.8	-635.75	2.12	-748.14
164	165	82.40	-2577.33	-156.86	522.64	0	-774.55	1.8	-928.45	1.8	-669.79	2.12	-808.33
165	165	82.40	-1859.54	-156.95	-37.42	0	-1267.38	1.8	-396.18	1.8	-313.82	2.12	-366.89
165	166	83.50	-1859.54	-140.58	126.92	0	-1086.87	1.8	-514.10	1.8	-346.69	2.12	-425.01
166	166	83.50	-1858.58	-140.69	126.79	0	-1129.55	1.8	-471.96	1.8	-310.08	2.12	-375.31
166	167	84.60	-1858.58	-144.11	292.01	0	-969.70	1.8	-554.30	1.8	-333.08	2.12	-421.17
167	167	84.60	-917.40	-135.63	-147.48	0	-1165.08	1.8	222.07	1.8	-48.30	2.12	-95.18
167	168	85.70	-920.89	-112.26	-3.38	0	-999.01	1.8	50.99	1.8	-61.48	2.12	-121.14
168	168	85.70	-1141.67	-119.92	-121.85	0	-1375.16	1.8	132.94	1.8	-61.99	2.12	-119.20
168	169	86.80	-1141.67	-96.49	-3.96	0	-1240.13	1.8	-6.78	1.8	-72.70	2.12	-139.80
169	169	86.80	-1141.67	-96.60	-3.94	0	-1240.11	1.8	-6.78	1.8	-72.71	2.12	-139.81
169	170	87.90	-1141.67	-73.24	88.91	0	-1132.93	1.8	-119.38	1.8	-80.94	2.12	-155.64
170	170	87.90	-1141.67	-73.32	88.93	0	-1132.91	1.8	-119.38	1.8	-80.95	2.12	-155.65
170	171	89.00	-1141.67	-49.91	155.81	0	-1054.33	1.8	-204.61	1.8	-86.55	2.12	-166.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.T0.MZ+
1. Frecuentes dominante GRAD
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1I3.ISO.To + [.95; 1.05]eje1I3.HIP.To + [.95; 1.05]eje2I3.ISO.To + [.95; 1.05]eje2I3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	-49.99	155.84	0	-1054.31	1.8	-204.61	1.8	-86.56	2.12	-166.43
171	172	90.10	-1141.67	-26.56	196.71	0	-1004.39	1.8	-262.46	1.8	-89.52	2.12	-172.14
172	172	90.10	-1141.67	-26.63	196.73	0	-1004.38	1.8	-262.46	1.8	-89.53	2.12	-172.14
172	173	91.20	-1141.67	-3.22	211.77	0	-982.94	1.8	-293.01	1.8	-89.88	2.12	-172.83
173	173	91.20	-1141.67	-3.29	211.79	0	-982.93	1.8	-293.01	1.8	-89.89	2.12	-172.84
173	174	92.30	-1141.67	20.12	202.04	0	-989.14	1.8	-296.43	1.8	-87.81	2.12	-168.85
174	174	92.30	-1141.67	20.08	202.03	0	-989.15	1.8	-296.43	1.8	-87.81	2.12	-168.84
174	175	93.40	-1141.67	43.48	166.17	0	-1024.10	1.8	-272.45	1.8	-83.08	2.12	-159.75
175	175	93.40	-1141.67	43.44	166.16	0	-1005.84	1.8	-255.75	1.8	-82.40	2.12	-162.36
175	176	94.50	-1141.67	66.86	104.19	0	-1072.71	1.8	-204.55	1.8	-75.07	2.12	-147.93
176	176	94.50	-944.83	66.80	222.69	0	-726.71	1.8	-322.37	1.8	-75.07	2.12	-147.93
176	177	95.60	-944.83	92.18	134.67	0	-823.67	1.8	-243.91	1.8	-65.12	2.12	-128.32
177	177	95.60	-944.83	92.13	134.65	0	-823.69	1.8	-243.91	1.8	-65.12	2.12	-128.32
177	178	96.70	-944.83	115.55	22.09	0	-949.41	1.8	-138.44	1.8	-52.80	2.12	-104.04
178	178	96.70	-747.99	115.50	142.54	0	-600.29	1.8	-260.85	1.8	-52.80	2.12	-104.03
178	179	97.80	-747.99	138.92	3.91	0	-756.12	1.8	-128.10	1.8	-37.85	2.12	-74.58
179	179	97.80	-747.99	138.86	3.89	0	-756.14	1.8	-128.10	1.8	-37.85	2.12	-74.58
179	180	98.90	-747.99	162.28	-160.91	0	-942.15	1.8	31.96	1.8	-20.26	2.12	-39.91
180	180	98.90	-472.42	162.20	13.23	0	-444.62	1.8	-152.21	1.8	-20.25	2.12	-39.90
180	181	100.00	-472.42	156.12	-178.67	0	-662.40	1.8	37.59	1.8	-0.04	2.12	-0.07



CÁLCULO TENSIONAL

Hipótesis de cálculo:

FP UENTESG.T0.MZ-

C. cuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-184.58	-197.93	0	-732.51	1.8	41.63	1.8	0.04	2.12	0.07
1	2	1.10	-517.71	-103.22	-73.67	0	-570.46	1.8	-128.94	1.8	-9.01	2.12	-17.76
2	2	1.10	-822.30	-103.12	-266.23	0	-1120.44	1.8	74.64	1.8	-9.00	2.12	-17.74
2	3	2.20	-822.30	-85.90	-162.26	0	-987.81	1.8	-71.08	1.8	-16.57	2.12	-32.64
3	3	2.20	-822.30	-85.82	-162.32	0	-987.87	1.8	-71.07	1.8	-16.56	2.12	-32.62
3	4	3.30	-822.30	-68.57	-77.42	0	-879.29	1.8	-190.83	1.8	-22.67	2.12	-44.68
4	4	3.30	-1039.86	-68.52	-210.62	0	-1265.23	1.8	-55.52	1.8	-22.67	2.12	-44.66
4	5	4.40	-1039.86	-51.29	-144.75	0	-1180.69	1.8	-149.32	1.8	-27.34	2.12	-53.88
5	5	4.40	-1039.86	-51.26	-144.79	0	-1180.73	1.8	-149.31	1.8	-27.34	2.12	-53.87
5	6	5.50	-1039.86	-34.02	-97.90	0	-1120.16	1.8	-217.22	1.8	-30.58	2.12	-60.25
6	6	5.50	-1257.42	-34.00	-228.91	0	-1502.61	1.8	-86.99	1.8	-30.57	2.12	-60.24
6	7	6.60	-1257.42	-16.77	-200.96	0	-1465.97	1.8	-129.03	1.8	-32.38	2.12	-63.80
7	7	6.60	-1257.42	-16.78	-200.99	0	-1467.98	1.8	-146.66	1.8	-32.64	2.12	-62.76
7	8	7.70	-1257.42	0.45	-192.01	0	-1455.87	1.8	-162.80	1.8	-33.02	2.12	-63.49
8	8	7.70	-1257.42	0.44	-192.03	0	-1455.89	1.8	-162.79	1.8	-33.02	2.12	-63.48
8	9	8.80	-1257.42	17.74	-202.02	0	-1466.68	1.8	-152.92	1.8	-31.95	2.12	-61.44
9	9	8.80	-1257.42	17.69	-202.02	0	-1466.68	1.8	-152.92	1.8	-31.95	2.12	-61.44
9	10	9.90	-1257.42	34.95	-230.97	0	-1500.35	1.8	-117.07	1.8	-29.44	2.12	-56.61
10	10	9.90	-1257.42	34.91	-230.97	0	-1500.35	1.8	-117.07	1.8	-29.44	2.12	-56.61
10	11	11.00	-1257.42	52.14	-278.85	0	-1556.86	1.8	-55.26	1.8	-25.49	2.12	-49.02
11	11	11.00	-1257.42	52.09	-278.84	0	-1556.85	1.8	-55.27	1.8	-25.50	2.12	-49.02
11	12	12.10	-1257.42	69.34	-345.63	0	-1636.21	1.8	32.53	1.8	-20.11	2.12	-38.67
12	12	12.10	-1257.42	69.30	-345.62	0	-1636.20	1.8	32.53	1.8	-20.11	2.12	-38.68
12	13	13.20	-1257.42	86.54	-431.37	0	-1738.45	1.8	146.36	1.8	-13.29	2.12	-25.55
13	13	13.20	-1257.42	86.51	-431.35	0	-1738.43	1.8	146.35	1.8	-13.29	2.12	-25.56
13	14	14.30	-1257.42	103.77	-535.99	0	-1863.47	1.8	286.06	1.8	-5.03	2.12	-9.67
14	14	14.30	-1016.08	93.49	-404.99	0	-1468.47	1.8	192.54	1.8	-4.99	2.12	-9.84
14	15	15.40	-1016.27	113.18	-527.75	0	-1618.96	1.8	355.98	1.8	4.63	2.12	9.12
15	15	15.40	-1871.02	121.97	-130.05	0	-1422.39	1.8	-421.44	1.8	-249.16	2.12	-276.97
15	16	16.50	-1871.02	171.43	-278.86	0	-1568.11	1.8	-342.18	1.8	-228.83	2.12	-236.43
16	16	16.50	-1871.02	171.58	-278.77	0	-1563.04	1.8	-347.07	1.8	-233.08	2.12	-242.22
16	17	17.60	-1871.02	194.67	-480.05	0	-1779.56	1.8	-217.51	1.8	-190.97	2.12	-167.76
17	17	17.60	-2480.19	194.79	51.29	0	-1262.70	1.8	-724.40	1.8	-512.84	2.12	-566.96
17	18	18.70	-2480.19	221.23	-177.41	0	-1512.02	1.8	-566.49	1.8	-466.32	2.12	-484.71
18	18	18.70	-2480.18	221.38	-177.25	0	-1511.86	1.8	-566.53	1.8	-466.36	2.12	-484.78
18	19	19.80	-2480.18	249.04	-435.65	0	-1796.41	1.8	-378.76	1.8	-414.97	2.12	-393.90
19	19	19.80	-2175.60	249.24	-242.98	0	-1246.32	1.8	-582.38	1.8	-415.01	2.12	-393.98
19	20	20.90	-2175.60	279.86	-535.34	0	-1570.26	1.8	-363.44	1.8	-357.67	2.12	-292.60
20	20	20.90	-2175.60	280.13	-535.30	0	-1570.22	1.8	-363.45	1.8	-357.68	2.12	-292.61
20	21	22.00	-2175.60	313.63	-861.62	0	-1935.40	1.8	-107.28	1.8	-295.15	2.12	-182.05
21	1021	22.00	-2219.11	-323.86	-890.41	0	-2016.03	1.8	-75.15	1.8	-295.16	2.12	-182.06
21	22	23.40	-2219.11	-283.96	-466.15	0	-1530.57	1.8	-443.03	1.8	-372.12	2.12	-318.14
22	22	23.40	-2219.11	-283.63	-466.17	0	-1530.59	1.8	-443.02	1.8	-372.11	2.12	-318.13
22	23	24.80	-2219.11	-247.87	-94.16	0	-1109.28	1.8	-751.36	1.8	-441.37	2.12	-440.59
23	23	24.80	-2523.70	-247.16	-283.69	0	-1654.44	1.8	-554.85	1.8	-441.35	2.12	-440.55
23	24	26.20	-2523.70	-208.64	33.09	0	-1297.13	1.8	-812.67	1.8	-500.91	2.12	-545.87
24	24	26.20	-1696.97	-208.29	-364.81	0	-1427.55	1.8	-442.05	1.8	-179.01	2.12	-146.61
24	25	27.60	-1696.97	-174.14	-97.26	0	-1128.42	1.8	-651.18	1.8	-230.39	2.12	-237.46
25	25	27.60	-2088.58	-174.00	-329.33	0	-1810.78	1.8	-425.78	1.8	-230.33	2.12	-237.36
25	26	29.00	-2088.58	-115.03	-147.26	0	-1604.91	1.8	-575.62	1.8	-264.36	2.12	-297.53
26	26	29.00	-1242.90	-110.22	-545.00	0	-1858.33	1.8	313.22	1.8	-3.13	2.12	-6.18
26	27	30.40	-1243.14	-86.06	-400.33	0	-1675.05	1.8	103.38	1.8	-13.14	2.12	-25.90
27	27	30.40	-1606.18	-91.87	-599.50	0	-2278.97	1.8	252.87	1.8	-13.24	2.12	-25.46
27	28	31.80	-1606.18	-69.92	-486.26	0	-2138.64	1.8	86.52	1.8	-20.98	2.12	-40.34
28	28	31.80	-1606.18	-69.99	-486.31	0	-2138.68	1.8	86.53	1.8	-20.97	2.12	-40.32
28	29	33.20	-1606.18	-48.06	-403.66	0	-2035.28	1.8	-37.83	1.8	-26.38	2.12	-50.73
29	29	33.20	-1606.18	-48.14	-403.69	0	-2035.31	1.8	-37.82	1.8	-26.38	2.12	-50.72
29	30	34.60	-1606.18	-25.88	-351.94	0	-1969.14	1.8	-120.02	1.8	-29.43	2.12	-56.58
30	30	34.60	-1606.18	-25.96	-351.98	0	-1969.17	1.8	-120.01	1.8	-29.42	2.12	-56.57
30	31	36.00	-1606.18	-3.11	-331.78	0	-1940.74	1.8	-159.96	1.8	-29.98	2.12	-57.66
31	31	36.00	-1606.18	-3.19	-331.78	0	-1940.74	1.8	-159.96	1.8	-29.98	2.12	-57.66
31	32	37.40	-1606.18	18.78	-342.68	0	-1949.68	1.8	-157.74	1.8	-28.14	2.12	-54.12
32	32	37.40	-1606.18	18.68	-342.67	0	-1949.67	1.8	-157.75	1.8	-28.15	2.12	-54.12
32	33	38.80	-1606.18	40.62	-384.17	0	-1995.59	1.8	-113.45	1.8	-23.99	2.12	-46.12
33	33	38.80	-1606.18	40.54	-384.14	0	-1995.57	1.8	-113.45	1.8	-23.99	2.12	-46.13
33	34	40.20	-1606.18	62.48	-456.26	0	-2078.48	1.8	-27.06	1.8	-17.51	2.12	-33.67
34	34	40.20	-1606.18	62.40	-456.22	0	-2078.44	1.8	-27.07	1.8	-17.52	2.12	-33.68
34	35	41.60	-1606.18	84.36	-558.94	0	-2198.31	1.8	101.37	1.8	-8.71	2.12	-16.75
35	35	41.60	-1249.48	80.18	-359.78	0	-1601.22	1.8	-53.37	1.8	-8.65	2.12	-17.05
35	36	43.00	-1249.32	104.13	-492.78	0	-1762.76	1.8	115.86	1.8	2.41	2.12	4.75
36	36	43.00	-2088.58	107.29	-95.04	0	-1559.49	1.8	-574.15	1.8	-279.66	2.12	-324.57
36	37	44.40	-2088.58	165.45	-273.10	0	-1762.50	1.8	-422.15	1.8	-247.06	2.12	-266.93
37	37	44.40	-1696.97	165.60	-41.06	0	-1080.16	1.8	-647.53	1.8	-247.11	2.12	-267.02
37	38	45.80	-1696.97	199.02	-295.51	0	-1367.64	1.8	-438.89	1.8	-199.46	2.12	-182.77
38	38	45.80	-2523.70	199.23	102.42	0	-1237.19	1.8	-809.52	1.8	-521.37	2.12	-582.04

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTESG.T0.MZ-

C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	34.09	-97.46	0	-1123.00	1.8	-221.79	1.8	-30.58	2.12	-60.25
76	77	95.60	-1044.29	51.33	-144.44	0	-1183.71	1.8	-153.68	1.8	-27.34	2.12	-53.87
77	77	95.60	-1044.29	51.36	-144.39	0	-1183.67	1.8	-153.69	1.8	-27.35	2.12	-53.88
77	78	96.70	-1044.29	68.59	-210.38	0	-1268.38	1.8	-59.64	1.8	-22.67	2.12	-44.66
78	78	96.70	-826.73	68.64	-77.17	0	-882.44	1.8	-194.95	1.8	-22.68	2.12	-44.68
78	79	97.80	-826.73	85.89	-162.16	0	-991.15	1.8	-74.99	1.8	-16.56	2.12	-32.62
79	79	97.80	-826.73	85.96	-162.10	0	-991.10	1.8	-75.00	1.8	-16.57	2.12	-32.64
79	80	98.90	-826.73	103.18	-266.14	0	-1123.85	1.8	70.89	1.8	-9.00	2.12	-17.74
80	80	98.90	-522.14	103.29	-73.58	0	-573.87	1.8	-132.69	1.8	-9.01	2.12	-17.76
80	81	100.00	-522.14	184.56	-197.93	0	-732.51	1.8	41.63	1.8	0.04	2.12	0.07
101	101	0.00	-522.14	-155.05	-197.87	0	-732.46	1.8	41.62	1.8	0.03	2.12	0.05
101	102	1.10	-517.71	-97.72	-79.97	0	-575.90	1.8	-127.72	1.8	-7.95	2.12	-15.67
102	102	1.10	-822.30	-97.96	-272.36	0	-1125.74	1.8	75.82	1.8	-7.97	2.12	-15.70
102	103	2.20	-822.30	-81.32	-173.77	0	-997.74	1.8	-68.85	1.8	-14.63	2.12	-28.83
103	103	2.20	-822.30	-81.51	-173.67	0	-997.66	1.8	-68.87	1.8	-14.65	2.12	-28.87
103	104	3.30	-822.30	-64.87	-93.18	0	-892.89	1.8	-187.78	1.8	-20.03	2.12	-39.46
104	104	3.30	-1039.86	-65.00	-226.24	0	-1278.71	1.8	-52.50	1.8	-20.04	2.12	-39.49
104	105	4.40	-1039.86	-48.38	-163.89	0	-1197.20	1.8	-145.64	1.8	-24.13	2.12	-47.54
105	105	4.40	-1039.86	-48.50	-163.82	0	-1197.14	1.8	-145.65	1.8	-24.14	2.12	-47.56
105	106	5.50	-1039.86	-31.86	-119.64	0	-1138.91	1.8	-213.04	1.8	-26.92	2.12	-53.05
106	106	5.50	-1257.42	-31.93	-250.54	0	-1521.28	1.8	-82.82	1.8	-26.93	2.12	-53.07
106	107	6.60	-1257.42	-15.29	-224.56	0	-1486.35	1.8	-124.46	1.8	-28.41	2.12	-55.98
107	107	6.60	-1257.42	-15.34	-224.51	0	-1487.22	1.8	-142.07	1.8	-28.65	2.12	-55.10
107	108	7.70	-1257.42	1.29	-216.79	0	-1476.14	1.8	-157.96	1.8	-28.82	2.12	-55.42
108	108	7.70	-1257.42	1.25	-216.75	0	-1476.11	1.8	-157.97	1.8	-28.83	2.12	-55.43
108	109	8.80	-1257.42	17.89	-227.29	0	-1487.35	1.8	-147.99	1.8	-27.67	2.12	-53.20
109	109	8.80	-1257.42	17.86	-227.26	0	-1487.33	1.8	-148.00	1.8	-27.67	2.12	-53.21
109	110	9.90	-1257.42	34.49	-256.08	0	-1520.89	1.8	-112.17	1.8	-25.19	2.12	-48.43
110	110	9.90	-1257.42	34.48	-256.08	0	-1520.89	1.8	-112.17	1.8	-25.19	2.12	-48.43
110	111	11.00	-1257.42	51.11	-303.14	0	-1576.73	1.8	-50.52	1.8	-21.38	2.12	-41.10
111	111	11.00	-1257.42	51.11	-303.15	0	-1576.74	1.8	-50.52	1.8	-21.37	2.12	-41.10
111	112	12.10	-1257.42	67.75	-368.54	0	-1654.95	1.8	37.00	1.8	-16.23	2.12	-31.20
112	112	12.10	-1257.42	67.74	-368.56	0	-1654.97	1.8	37.01	1.8	-16.22	2.12	-31.20
112	113	13.20	-1257.42	84.36	-452.23	0	-1755.51	1.8	150.41	1.8	-9.75	2.12	-18.75
113	113	13.20	-1257.42	84.34	-452.27	0	-1755.54	1.8	150.41	1.8	-9.74	2.12	-18.74
113	114	14.30	-1257.42	101.00	-554.20	0	-1878.37	1.8	289.61	1.8	-1.94	2.12	-3.73
114	114	14.30	-1016.08	90.74	-423.28	0	-1484.25	1.8	196.08	1.8	-1.92	2.12	-3.78
114	115	15.40	-1016.27	109.88	-542.69	0	-1631.85	1.8	358.87	1.8	7.14	2.12	14.07
115	115	15.40	-1871.02	118.65	-145.09	0	-1435.35	1.8	-418.62	1.8	-246.71	2.12	-272.08
115	116	16.50	-1871.02	162.08	-290.05	0	-1577.75	1.8	-340.08	1.8	-227.01	2.12	-232.79
116	116	16.50	-1871.02	161.92	-290.15	0	-1574.04	1.8	-343.76	1.8	-230.21	2.12	-237.13
116	117	17.60	-1871.02	183.77	-480.21	0	-1779.72	1.8	-217.46	1.8	-190.93	2.12	-167.69
117	117	17.60	-2480.18	183.54	50.95	0	-1263.03	1.8	-724.30	1.8	-512.75	2.12	-566.81
117	118	18.70	-2480.18	210.98	-166.33	0	-1501.29	1.8	-569.71	1.8	-469.13	2.12	-489.67
118	118	18.70	-2480.18	210.78	-166.32	0	-1501.28	1.8	-569.71	1.8	-469.13	2.12	-489.67
118	119	19.80	-2480.18	239.90	-413.87	0	-1775.33	1.8	-385.11	1.8	-420.48	2.12	-403.65
119	119	19.80	-2175.60	239.77	-221.37	0	-1225.40	1.8	-588.68	1.8	-420.48	2.12	-403.65
119	120	20.90	-2175.60	272.38	-504.91	0	-1540.80	1.8	-372.31	1.8	-365.38	2.12	-306.22
120	120	20.90	-2175.60	272.30	-504.91	0	-1540.81	1.8	-372.30	1.8	-365.37	2.12	-306.21
120	121	22.00	-2175.60	304.02	-821.04	0	-1896.13	1.8	-119.10	1.8	-305.42	2.12	-200.21
121	1121	22.00	-2219.11	-314.18	-849.85	0	-1976.77	1.8	-86.98	1.8	-305.42	2.12	-200.21
121	122	23.40	-2219.11	-274.48	-438.70	0	-1504.00	1.8	-451.03	1.8	-379.07	2.12	-330.43
122	122	23.40	-2219.11	-274.55	-438.67	0	-1503.98	1.8	-451.03	1.8	-379.07	2.12	-330.44
122	123	24.80	-2219.11	-239.31	-79.20	0	-1094.80	1.8	-755.72	1.8	-445.16	2.12	-447.29
123	123	24.80	-2523.70	-239.30	-268.55	0	-1639.79	1.8	-559.26	1.8	-445.18	2.12	-447.33
123	124	26.20	-2523.70	-199.50	36.09	0	-1294.23	1.8	-813.55	1.8	-501.67	2.12	-547.22
124	124	26.20	-1696.97	-199.73	-361.58	0	-1424.42	1.8	-442.99	1.8	-179.83	2.12	-148.06
124	125	27.60	-1696.97	-165.86	-106.13	0	-1137.00	1.8	-648.59	1.8	-228.15	2.12	-233.50
125	125	27.60	-2088.58	-166.14	-337.94	0	-1819.12	1.8	-423.27	1.8	-228.15	2.12	-233.50
125	126	29.00	-2088.58	-111.69	-160.04	0	-1617.28	1.8	-571.89	1.8	-261.13	2.12	-291.81
126	126	29.00	-1242.90	-106.85	-557.61	0	-1869.23	1.8	315.68	1.8	-1.02	2.12	-2.00
126	127	30.40	-1243.14	-83.59	-417.00	0	-1689.44	1.8	106.61	1.8	-10.34	2.12	-20.37
127	127	30.40	-1606.18	-89.33	-616.05	0	-2292.51	1.8	256.10	1.8	-10.44	2.12	-20.07
127	128	31.80	-1606.18	-68.12	-505.87	0	-2154.67	1.8	90.34	1.8	-17.66	2.12	-33.95
128	128	31.80	-1606.18	-68.08	-505.81	0	-2154.63	1.8	90.33	1.8	-17.66	2.12	-33.97
128	129	33.20	-1606.18	-46.92	-425.29	0	-2052.97	1.8	-33.63	1.8	-22.72	2.12	-43.68
129	129	33.20	-1606.18	-46.87	-425.25	0	-2052.94	1.8	-33.64	1.8	-22.72	2.12	-43.69
129	130	34.60	-1606.18	-25.40	-374.69	0	-1987.74	1.8	-115.58	1.8	-25.57	2.12	-49.17
130	130	34.60	-1606.18	-25.34	-374.68	0	-1987.73	1.8	-115.58	1.8	-25.57	2.12	-49.17
130	131	36.00	-1606.18	-3.06	-354.93	0	-1959.67	1.8	-155.46	1.8	-26.06	2.12	-50.11
131	131	36.00	-1606.18	-3.00	-354.93	0	-1959.66	1.8	-155.46	1.8	-26.06	2.12	-50.11
131	132	37.40	-1606.18	18.19	-365.57	0	-1968.41	1.8	-153.25	1.8	-24.27	2.12	-46.66
132	132	37.40	-1606.18	18.24	-365.58	0	-1968.42	1.8	-153.25	1.8	-24.26	2.12	-46.65
132	133	38.80	-1606.18	39.43	-405.95	0	-2013.41	1.8	-109.17	1.8	-20.30	2.12	-39.03
133	133	38.80	-1606.18	39.48	-405.98	0	-2013.44	1.8	-109.17	1.8	-20.29	2.12	-39.01

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRE[illegible]ENTESG.T0.MZ-

C. [illegible]uentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	60.65	-476.06	0	-2094.67	1.8	-23.20	1.8	-14.15	2.12	-27.21
134	134	40.20	-1606.18	60.69	-476.11	0	-2094.71	1.8	-23.19	1.8	-14.14	2.12	-27.20
134	135	41.60	-1606.18	81.90	-575.92	0	-2212.20	1.8	104.69	1.8	-5.84	2.12	-11.22
135	135	41.60	-1249.48	77.78	-376.87	0	-1615.97	1.8	-50.06	1.8	-5.78	2.12	-11.38
135	136	43.00	-1249.32	100.88	-505.96	0	-1774.13	1.8	118.41	1.8	4.63	2.12	9.11
136	136	43.00	-2088.58	104.09	-108.37	0	-1572.39	1.8	-570.26	1.8	-276.28	2.12	-318.60
136	137	44.40	-2088.58	157.18	-281.44	0	-1770.56	1.8	-419.72	1.8	-244.95	2.12	-263.20
137	137	44.40	-1696.97	156.94	-49.67	0	-1088.49	1.8	-645.03	1.8	-244.93	2.12	-263.17
137	138	45.80	-1696.97	190.09	-291.77	0	-1364.02	1.8	-439.98	1.8	-200.41	2.12	-184.44
138	138	45.80	-2523.70	189.80	105.92	0	-1233.80	1.8	-810.55	1.8	-522.25	2.12	-583.61
138	139	47.20	-2523.70	225.22	-183.70	0	-1565.84	1.8	-557.31	1.8	-469.98	2.12	-491.18
139	139	47.20	-2219.11	224.98	5.72	0	-1020.79	1.8	-753.79	1.8	-469.97	2.12	-491.17
139	140	48.60	-2212.66	264.86	-338.60	0	-1414.34	1.8	-448.19	1.8	-406.41	2.12	-380.11
140	140	48.60	-2212.49	264.78	-338.69	0	-1414.37	1.8	-448.11	1.8	-406.35	2.12	-380.02
140	141	50.00	-2212.49	305.20	-737.16	0	-1875.89	1.8	-84.42	1.8	-336.33	2.12	-256.21
141	1141	50.00	-2212.71	-305.12	-737.17	0	-1875.96	1.8	-84.49	1.8	-336.38	2.12	-256.27
141	142	51.40	-2212.71	-264.70	-338.81	0	-1414.55	1.8	-448.15	1.8	-406.37	2.12	-380.03
142	142	51.40	-2213.30	-264.77	-338.73	0	-1414.66	1.8	-448.35	1.8	-406.55	2.12	-380.22
2	143	52.80	-2213.30	-225.39	5.59	0	-1019.13	1.8	-751.96	1.8	-468.38	2.12	-489.55
143	143	52.80	-2518.88	-225.59	-183.72	0	-1564.38	1.8	-555.82	1.8	-468.69	2.12	-489.88
143	144	54.20	-2523.70	-189.80	105.92	0	-1233.81	1.8	-810.54	1.8	-522.25	2.12	-583.61
144	144	54.20	-1696.97	-190.10	-291.76	0	-1364.01	1.8	-439.98	1.8	-200.41	2.12	-184.44
144	145	55.60	-1696.97	-156.95	-49.65	0	-1088.47	1.8	-645.03	1.8	-244.94	2.12	-263.18
145	145	55.60	-2088.58	-157.18	-281.43	0	-1770.55	1.8	-419.72	1.8	-244.95	2.12	-263.20
145	146	57.00	-2088.58	-104.09	-108.36	0	-1572.38	1.8	-570.27	1.8	-276.28	2.12	-318.61
146	146	57.00	-1249.32	-100.89	-505.95	0	-1774.13	1.8	118.41	1.8	4.62	2.12	9.11
146	147	58.40	-1251.27	-78.71	-375.95	0	-1616.04	1.8	-53.64	1.8	-5.78	2.12	-11.39
147	147	58.40	-1608.20	-81.84	-575.00	0	-2212.45	1.8	100.93	1.8	-5.84	2.12	-11.22
147	148	59.80	-1608.20	-60.63	-475.30	0	-2095.11	1.8	-26.73	1.8	-14.14	2.12	-27.20
148	148	59.80	-1608.20	-60.59	-475.24	0	-2095.06	1.8	-26.75	1.8	-14.15	2.12	-27.21
148	149	61.20	-1608.20	-39.42	-405.24	0	-2013.95	1.8	-112.53	1.8	-20.29	2.12	-39.02
149	149	61.20	-1608.20	-39.37	-405.21	0	-2013.93	1.8	-112.53	1.8	-20.30	2.12	-39.03
149	150	62.60	-1608.20	-18.19	-364.91	0	-1969.05	1.8	-156.45	1.8	-24.26	2.12	-46.66
150	150	62.60	-1608.20	-18.13	-364.89	0	-1969.03	1.8	-156.45	1.8	-24.27	2.12	-46.66
150	151	64.00	-1609.94	3.08	-354.37	0	-1961.88	1.8	-159.82	1.8	-26.06	2.12	-50.11
151	151	64.00	-1609.94	3.14	-354.37	0	-1961.88	1.8	-159.82	1.8	-26.06	2.12	-50.11
151	152	65.40	-1609.94	25.42	-374.23	0	-1990.12	1.8	-119.71	1.8	-25.57	2.12	-49.17
152	152	65.40	-1609.94	25.48	-374.23	0	-1990.12	1.8	-119.70	1.8	-25.57	2.12	-49.17
152	153	66.80	-1609.94	46.94	-424.91	0	-2055.48	1.8	-37.50	1.8	-22.72	2.12	-43.69
153	153	66.80	-1609.94	47.00	-424.95	0	-2055.51	1.8	-37.50	1.8	-22.72	2.12	-43.68
153	154	68.20	-1609.94	68.16	-505.59	0	-2157.35	1.8	86.73	1.8	-17.66	2.12	-33.97
154	154	68.20	-1609.94	68.20	-505.64	0	-2157.39	1.8	86.74	1.8	-17.66	2.12	-33.95
154	155	69.60	-1609.94	89.41	-615.93	0	-2295.39	1.8	252.76	1.8	-10.44	2.12	-20.07
55	155	69.60	-1246.39	85.46	-416.88	0	-1691.92	1.8	103.67	1.8	-10.34	2.12	-20.37
155	156	71.00	-1242.90	106.85	-557.62	0	-1869.24	1.8	315.70	1.8	-1.02	2.12	-2.00
156	156	71.00	-2088.58	111.69	-160.04	0	-1617.28	1.8	-571.89	1.8	-261.13	2.12	-291.81
156	157	72.40	-2088.58	166.15	-337.93	0	-1819.10	1.8	-423.28	1.8	-228.16	2.12	-233.51
157	157	72.40	-1696.97	165.87	-106.11	0	-1136.98	1.8	-648.60	1.8	-228.15	2.12	-233.50
157	158	73.80	-1696.97	199.74	-361.58	0	-1424.43	1.8	-442.99	1.8	-179.83	2.12	-148.06
158	158	73.80	-2523.70	199.50	36.08	0	-1294.24	1.8	-813.54	1.8	-501.67	2.12	-547.21
158	159	75.20	-2523.70	239.31	-268.56	0	-1639.80	1.8	-559.26	1.8	-445.18	2.12	-447.32
159	159	75.20	-2219.11	239.30	-79.19	0	-1094.79	1.8	-755.73	1.8	-445.16	2.12	-447.29
159	160	76.60	-2215.29	275.02	-439.19	0	-1503.30	1.8	-449.71	1.8	-377.92	2.12	-329.18
160	160	76.60	-2215.34	274.97	-439.32	0	-1503.44	1.8	-449.68	1.8	-377.90	2.12	-329.14
160	161	78.00	-2215.34	314.67	-851.15	0	-1976.87	1.8	-85.43	1.8	-304.09	2.12	-198.62
161	1161	78.00	-2172.15	-304.17	-822.38	0	-1896.36	1.8	-117.65	1.8	-304.16	2.12	-198.68
161	162	79.10	-2172.15	-272.46	-506.09	0	-1540.88	1.8	-370.90	1.8	-364.15	2.12	-304.76
162	162	79.10	-2172.53	-272.54	-506.09	0	-1541.00	1.8	-371.02	1.8	-364.25	2.12	-304.86
162	163	80.20	-2172.53	-239.94	-222.37	0	-1225.43	1.8	-587.44	1.8	-419.41	2.12	-402.38
163	163	80.20	-2477.65	-240.06	-414.84	0	-1775.49	1.8	-384.05	1.8	-419.56	2.12	-402.54
163	164	81.30	-2477.65	-210.94	-167.11	0	-1501.27	1.8	-568.70	1.8	-468.25	2.12	-488.64
164	164	81.30	-2478.35	-211.13	-167.06	0	-1501.43	1.8	-568.93	1.8	-468.45	2.12	-488.85
164	165	82.40	-2478.35	-183.69	50.39	0	-1263.01	1.8	-723.57	1.8	-512.12	2.12	-566.07
165	165	82.40	-1870.06	-183.87	-480.24	0	-1779.19	1.8	-218.03	1.8	-190.56	2.12	-167.22
165	166	83.50	-1870.06	-162.02	-290.51	0	-1574.10	1.8	-343.36	1.8	-229.86	2.12	-236.71
166	166	83.50	-1871.02	-162.11	-290.32	0	-1577.98	1.8	-340.03	1.8	-226.97	2.12	-232.71
166	167	84.60	-1871.02	-118.68	-145.33	0	-1435.55	1.8	-418.58	1.8	-246.67	2.12	-272.00
167	167	84.60	-1016.26	-109.88	-542.93	0	-1632.21	1.8	359.43	1.8	7.14	2.12	14.08
167	168	85.70	-1019.75	-93.20	-422.17	0	-1485.56	1.8	190.47	1.8	-1.92	2.12	-3.78
168	168	85.70	-1261.85	-100.93	-553.09	0	-1880.29	1.8	283.39	1.8	-1.94	2.12	-3.73
168	169	86.80	-1261.85	-84.28	-451.24	0	-1757.58	1.8	144.39	1.8	-9.74	2.12	-18.74
169	169	86.80	-1261.85	-84.29	-451.20	0	-1757.55	1.8	144.38	1.8	-9.75	2.12	-18.75
169	170	87.90	-1261.85	-67.67	-367.62	0	-1657.14	1.8	31.18	1.8	-16.22	2.12	-31.20
170	170	87.90	-1261.85	-67.68	-367.60	0	-1657.12	1.8	31.18	1.8	-16.23	2.12	-31.20
170	171	89.00	-1261.85	-51.04	-302.30	0	-1579.04	1.8	-56.15	1.8	-21.37	2.12	-41.10

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.T0.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-153.41	-177.98	0	-661.80	1.8	37.46	1.8	-0.15	2.12	-0.30
1	2	1.10	-476.85	-262.66	129.63	0	-347.64	1.8	-178.47	1.8	-39.81	2.12	-78.44
2	2	1.10	-752.42	-263.15	-44.33	0	-845.01	1.8	5.67	1.8	-39.84	2.12	-78.50
2	3	2.20	-752.42	-227.60	222.29	0	-571.04	1.8	-174.31	1.8	-74.53	2.12	-146.87
3	3	2.20	-752.42	-228.00	222.46	0	-570.90	1.8	-174.34	1.8	-74.56	2.12	-146.92
3	4	3.30	-752.42	-192.51	448.43	0	-339.61	1.8	-324.18	1.8	-104.18	2.12	-205.28
4	4	3.30	-949.26	-192.79	328.17	0	-688.57	1.8	-201.81	1.8	-104.21	2.12	-205.35
4	5	4.40	-949.26	-151.15	513.27	0	-500.18	1.8	-321.46	1.8	-128.72	2.12	-253.64
5	5	4.40	-949.26	-151.33	513.44	0	-500.03	1.8	-321.49	1.8	-128.75	2.12	-253.69
5	6	5.50	-949.26	-113.74	665.11	0	-348.08	1.8	-412.46	1.8	-149.38	2.12	-294.36
6	6	5.50	-1146.10	-113.91	546.73	0	-693.98	1.8	-294.66	1.8	-149.40	2.12	-294.40
6	7	6.60	-1146.10	-78.29	657.92	0	-584.55	1.8	-355.59	1.8	-164.99	2.12	-325.10
7	7	6.60	-1146.10	-78.43	658.03	0	-625.01	1.8	-373.17	1.8	-166.37	2.12	-319.90
7	8	7.70	-1146.10	-42.90	728.64	0	-561.58	1.8	-404.11	1.8	-176.97	2.12	-340.29
8	8	7.70	-1146.10	-42.92	728.72	0	-561.51	1.8	-404.13	1.8	-176.99	2.12	-340.32
8	9	8.80	-1146.10	-7.71	757.60	0	-539.59	1.8	-404.62	1.8	-182.29	2.12	-350.52
9	9	8.80	-1146.10	-7.67	757.66	0	-539.55	1.8	-404.64	1.8	-182.30	2.12	-350.54
9	10	9.90	-1146.10	27.75	752.73	0	-552.65	1.8	-376.25	1.8	-183.64	2.12	-353.12
10	10	9.90	-1146.10	27.81	752.74	0	-552.64	1.8	-376.25	1.8	-183.64	2.12	-353.12
10	11	11.00	-1146.10	63.47	707.63	0	-605.97	1.8	-317.76	1.8	-179.94	2.12	-346.01
11	11	11.00	-1146.10	63.49	707.64	0	-605.96	1.8	-317.77	1.8	-179.95	2.12	-346.01
11	12	12.10	-1146.10	99.07	622.06	0	-699.76	1.8	-229.08	1.8	-171.16	2.12	-329.11
12	12	12.10	-1146.10	99.16	622.03	0	-699.79	1.8	-229.07	1.8	-171.15	2.12	-329.10
12	13	13.20	-1146.10	134.41	495.34	0	-834.61	1.8	-110.03	1.8	-157.17	2.12	-302.21
13	13	13.20	-1146.10	134.47	495.28	0	-834.66	1.8	-110.02	1.8	-157.16	2.12	-302.19
13	14	14.30	-1146.10	170.11	332.80	0	-1006.09	1.8	38.20	1.8	-138.87	2.12	-267.02
14	14	14.30	-924.56	165.18	451.19	0	-608.92	1.8	-42.40	1.8	-137.71	2.12	-271.36
14	15	15.40	-917.39	198.24	247.13	0	-824.62	1.8	146.19	1.8	-114.69	2.12	-225.99
15	15	15.40	-1858.58	206.87	686.54	0	-629.85	1.8	-628.31	1.8	-397.36	2.12	-549.35
15	16	16.50	-1858.58	209.93	448.52	0	-852.41	1.8	-532.31	1.8	-362.50	2.12	-479.83
16	16	16.50	-1858.58	209.73	448.27	0	-775.56	1.8	-607.45	1.8	-427.76	2.12	-568.57
16	17	17.60	-1858.58	225.02	204.98	0	-1032.73	1.8	-465.73	1.8	-375.01	2.12	-475.29
17	17	17.60	-2575.51	224.99	764.99	0	-539.44	1.8	-998.51	1.8	-730.63	2.12	-916.30
17	18	18.70	-2575.51	217.73	512.48	0	-811.79	1.8	-833.66	1.8	-678.09	2.12	-823.39
18	18	18.70	-2575.50	217.69	511.89	0	-812.36	1.8	-833.49	1.8	-677.94	2.12	-823.12
18	19	19.80	-2575.50	215.89	271.84	0	-1079.16	1.8	-651.07	1.8	-631.19	2.12	-740.46
19	19	19.80	-2299.92	215.77	445.27	0	-582.31	1.8	-835.03	1.8	-631.01	2.12	-740.13
19	20	20.90	-2299.92	214.02	208.56	0	-852.39	1.8	-632.31	1.8	-587.75	2.12	-663.65
20	20	20.90	-2299.92	213.48	208.58	0	-852.37	1.8	-632.31	1.8	-587.76	2.12	-663.66
20	21	22.00	-2299.92	219.56	-30.16	0	-1132.79	1.8	-401.66	1.8	-547.39	2.12	-592.29
21	1021	22.00	-2339.29	-215.63	-56.23	0	-1205.76	1.8	-372.59	1.8	-547.39	2.12	-592.29
21	22	23.40	-2339.29	-196.82	237.97	0	-846.18	1.8	-702.56	1.8	-591.44	2.12	-670.16
22	22	23.40	-2339.29	-197.41	237.90	0	-846.25	1.8	-702.54	1.8	-591.42	2.12	-670.13
22	23	24.80	-2339.29	-196.08	515.04	0	-516.75	1.8	-983.24	1.8	-636.66	2.12	-750.13
23	23	24.80	-2614.86	-196.76	343.65	0	-1009.90	1.8	-805.47	1.8	-636.67	2.12	-750.14
23	24	26.20	-2614.86	-228.45	636.39	0	-675.87	1.8	-1056.28	1.8	-690.14	2.12	-844.70
24	24	26.20	-1701.11	-229.42	197.80	0	-818.86	1.8	-646.99	1.8	-334.66	2.12	-403.95
24	25	27.60	-1701.11	-222.98	510.71	0	-475.82	1.8	-869.34	1.8	-397.53	2.12	-515.10
25	25	27.60	-2055.42	-223.08	301.82	0	-1092.15	1.8	-665.73	1.8	-397.74	2.12	-515.49
25	26	29.00	-2055.42	-235.91	638.28	0	-736.86	1.8	-860.55	1.8	-470.85	2.12	-644.75
26	26	29.00	-1122.96	-230.96	199.07	0	-1062.95	1.8	94.05	1.8	-114.73	2.12	-226.08
26	27	30.40	-1129.71	-190.21	494.79	0	-754.89	1.8	-149.45	1.8	-150.21	2.12	-295.98
27	27	30.40	-1460.38	-192.21	314.86	0	-1342.34	1.8	-17.56	1.8	-151.48	2.12	-291.28
27	28	31.80	-1460.38	-145.98	546.15	0	-1105.76	1.8	-206.02	1.8	-179.31	2.12	-344.78
28	28	31.80	-1460.38	-145.80	546.32	0	-1105.62	1.8	-206.05	1.8	-179.34	2.12	-344.84
28	29	33.20	-1460.38	-94.84	714.25	0	-932.78	1.8	-346.12	1.8	-199.28	2.12	-383.19
29	29	33.20	-1460.38	-94.61	714.41	0	-932.64	1.8	-346.15	1.8	-199.31	2.12	-383.24
29	30	34.60	-1460.38	-55.87	820.67	0	-822.20	1.8	-438.04	1.8	-211.67	2.12	-407.01
30	30	34.60	-1460.38	-55.61	820.74	0	-822.14	1.8	-438.06	1.8	-211.68	2.12	-407.03
30	31	36.00	-1460.38	-10.01	860.62	0	-777.92	1.8	-480.91	1.8	-215.66	2.12	-414.67
31	31	36.00	-1460.38	-9.80	860.63	0	-777.91	1.8	-480.91	1.8	-215.66	2.12	-414.68
31	32	37.40	-1460.38	41.64	840.40	0	-794.80	1.8	-475.94	1.8	-212.31	2.12	-408.24
32	32	37.40	-1460.38	41.88	840.35	0	-794.84	1.8	-475.93	1.8	-212.30	2.12	-408.22
32	33	38.80	-1460.38	80.61	753.64	0	-878.04	1.8	-421.87	1.8	-200.55	2.12	-385.63
33	33	38.80	-1460.38	80.85	753.51	0	-878.15	1.8	-421.84	1.8	-200.53	2.12	-385.59
33	34	40.20	-1460.38	131.85	605.25	0	-1023.65	1.8	-319.66	1.8	-181.22	2.12	-348.45
34	34	40.20	-1460.38	132.03	605.08	0	-1023.78	1.8	-319.63	1.8	-181.19	2.12	-348.40
34	35	41.60	-1460.38	178.27	393.27	0	-1233.20	1.8	-168.95	1.8	-153.97	2.12	-296.05
35	35	41.60	-1135.74	177.82	573.16	0	-650.48	1.8	-305.78	1.8	-152.66	2.12	-300.82
35	36	43.00	-1128.92	219.09	295.59	0	-933.13	1.8	-97.39	1.8	-117.75	2.12	-232.02
36	36	43.00	-2055.42	222.49	734.84	0	-648.52	1.8	-872.01	1.8	-497.36	2.12	-691.64
36	37	44.40	-2055.42	217.76	418.22	0	-985.64	1.8	-679.63	1.8	-429.70	2.12	-571.98
37	37	44.40	-1701.11	217.76	627.20	0	-369.21	1.8	-883.27	1.8	-429.50	2.12	-571.64
37	38	45.80	-1701.11	227.81	316.20	0	-711.42	1.8	-658.14	1.8	-367.54	2.12	-462.08
38	38	45.80	-2614.86	227.36	754.66	0	-568.56	1.8	-1067.40	1.8	-722.99	2.12	-902.78

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.T0.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2614.86	204.24	456.00	0	-909.34	1.8	-811.53	1.8	-668.43	2.12	-806.30
39	39	47.20	-2339.29	204.43	626.88	0	-416.69	1.8	-989.15	1.8	-668.29	2.12	-806.06
39	40	48.60	-2345.74	197.58	344.29	0	-754.47	1.8	-705.52	1.8	-623.81	2.12	-726.08
40	40	48.60	-2345.92	196.98	344.39	0	-754.42	1.8	-705.60	1.8	-623.88	2.12	-726.17
40	41	50.00	-2345.92	214.72	49.76	0	-1115.45	1.8	-372.17	1.8	-580.14	2.12	-648.83
41	1041	50.00	-2345.70	-214.81	49.76	0	-1115.38	1.8	-372.11	1.8	-580.09	2.12	-648.78
41	42	51.40	-2345.70	-197.07	344.51	0	-754.24	1.8	-705.57	1.8	-623.86	2.12	-726.17
42	42	51.40	-2345.10	-197.67	344.42	0	-754.14	1.8	-705.36	1.8	-623.67	2.12	-725.97
42	43	52.80	-2345.10	-204.02	627.02	0	-418.34	1.8	-990.98	1.8	-669.88	2.12	-807.68
43	43	52.80	-2619.68	-203.87	456.04	0	-910.80	1.8	-813.02	1.8	-669.72	2.12	-807.60
43	44	54.20	-2614.86	-227.36	754.66	0	-568.55	1.8	-1067.40	1.8	-722.99	2.12	-902.78
44	44	54.20	-1701.11	-227.81	316.20	0	-711.42	1.8	-658.14	1.8	-367.54	2.12	-462.08
44	45	55.60	-1701.11	-217.77	627.24	0	-369.18	1.8	-883.28	1.8	-429.51	2.12	-571.66
45	45	55.60	-2055.42	-217.76	418.23	0	-985.63	1.8	-679.63	1.8	-429.70	2.12	-571.99
45	46	57.00	-2055.42	-222.49	734.86	0	-648.50	1.8	-872.01	1.8	-497.37	2.12	-691.65
46	46	57.00	-1128.92	-219.10	295.63	0	-933.10	1.8	-97.42	1.8	-117.75	2.12	-232.03
46	47	58.40	-1133.95	-176.91	572.29	0	-650.36	1.8	-302.24	1.8	-152.67	2.12	-300.83
47	47	58.40	-1458.36	-178.33	392.39	0	-1232.91	1.8	-165.23	1.8	-153.97	2.12	-296.06
47	48	59.80	-1458.36	-132.09	604.31	0	-1023.35	1.8	-316.10	1.8	-181.20	2.12	-348.41
48	48	59.80	-1458.36	-131.91	604.48	0	-1023.21	1.8	-316.13	1.8	-181.22	2.12	-348.47
48	49	61.20	-1458.36	-80.90	752.77	0	-877.64	1.8	-418.47	1.8	-200.53	2.12	-385.59
49	49	61.20	-1458.36	-80.67	752.88	0	-877.55	1.8	-418.49	1.8	-200.55	2.12	-385.63
49	50	62.60	-1458.36	-41.94	839.72	0	-794.18	1.8	-472.76	1.8	-212.31	2.12	-408.23
50	50	62.60	-1458.36	-41.69	839.79	0	-794.12	1.8	-472.77	1.8	-212.32	2.12	-408.25
50	51	64.00	-1456.62	9.72	860.08	0	-775.70	1.8	-476.53	1.8	-215.66	2.12	-414.68
51	51	64.00	-1456.62	9.93	860.08	0	-775.70	1.8	-476.53	1.8	-215.66	2.12	-414.68
51	52	65.40	-1456.62	55.52	820.31	0	-819.75	1.8	-433.94	1.8	-211.68	2.12	-407.04
52	52	65.40	-1456.62	55.78	820.22	0	-819.81	1.8	-433.92	1.8	-211.67	2.12	-407.01
52	53	66.80	-1456.62	94.53	714.12	0	-930.06	1.8	-342.29	1.8	-199.32	2.12	-383.26
53	53	66.80	-1456.62	94.76	713.96	0	-930.19	1.8	-342.26	1.8	-199.29	2.12	-383.21
53	54	68.20	-1456.62	145.72	546.15	0	-1102.85	1.8	-202.47	1.8	-179.34	2.12	-344.85
54	54	68.20	-1456.62	145.90	545.99	0	-1102.98	1.8	-202.44	1.8	-179.32	2.12	-344.80
54	55	69.60	-1456.62	192.13	314.77	0	-1339.42	1.8	-14.24	1.8	-151.49	2.12	-291.29
55	55	69.60	-1126.45	188.35	494.71	0	-752.37	1.8	-146.54	1.8	-150.21	2.12	-295.99
55	56	71.00	-1122.96	230.99	199.08	0	-1062.94	1.8	94.07	1.8	-114.74	2.12	-226.09
56	56	71.00	-2055.42	235.90	638.30	0	-736.84	1.8	-860.56	1.8	-470.85	2.12	-644.76
56	57	72.40	-2055.42	223.08	301.85	0	-1092.13	1.8	-665.74	1.8	-397.75	2.12	-515.50
57	57	72.40	-1701.11	223.00	510.73	0	-475.80	1.8	-869.35	1.8	-397.53	2.12	-515.11
57	58	73.80	-1701.11	229.43	197.79	0	-818.87	1.8	-646.99	1.8	-334.66	2.12	-403.94
58	58	73.80	-2614.86	228.44	636.37	0	-675.88	1.8	-1056.28	1.8	-690.14	2.12	-844.70
58	59	75.20	-2614.86	196.77	343.64	0	-1009.91	1.8	-805.47	1.8	-636.66	2.12	-750.14
59	59	75.20	-2339.29	196.07	515.03	0	-516.76	1.8	-983.24	1.8	-636.66	2.12	-750.13
59	60	76.60	-2343.12	196.94	238.40	0	-846.94	1.8	-703.87	1.8	-592.57	2.12	-671.38
60	60	76.60	-2343.06	196.33	238.55	0	-846.78	1.8	-703.89	1.8	-592.59	2.12	-671.43
60	61	78.00	-2343.06	215.14	-54.94	0	-1205.68	1.8	-374.13	1.8	-548.73	2.12	-593.87
61	1061	78.00	-2303.37	-219.41	-28.85	0	-1132.58	1.8	-403.11	1.8	-548.65	2.12	-593.80
61	62	79.10	-2303.37	-213.33	209.72	0	-852.32	1.8	-633.71	1.8	-588.97	2.12	-665.09
62	62	79.10	-2302.99	-213.87	209.70	0	-852.23	1.8	-633.59	1.8	-588.86	2.12	-664.98
62	63	80.20	-2302.99	-215.62	446.26	0	-582.30	1.8	-836.26	1.8	-632.08	2.12	-741.40
63	63	80.20	-2578.03	-215.73	272.80	0	-1079.01	1.8	-652.13	1.8	-632.11	2.12	-741.57
63	64	81.30	-2578.03	-217.53	512.68	0	-812.38	1.8	-834.50	1.8	-678.82	2.12	-824.16
64	64	81.30	-2577.33	-217.58	513.19	0	-811.67	1.8	-834.43	1.8	-678.76	2.12	-824.19
64	65	82.40	-2577.33	-224.84	765.55	0	-539.46	1.8	-999.24	1.8	-731.26	2.12	-917.03
65	65	82.40	-1859.54	-224.93	205.83	0	-1031.96	1.8	-467.07	1.8	-375.38	2.12	-475.75
65	66	83.50	-1859.54	-209.63	448.65	0	-775.49	1.8	-607.86	1.8	-428.12	2.12	-569.00
66	66	83.50	-1858.58	-209.93	448.79	0	-852.18	1.8	-532.36	1.8	-362.54	2.12	-479.92
66	67	84.60	-1858.58	-206.87	686.81	0	-629.62	1.8	-628.36	1.8	-397.40	2.12	-549.44
67	67	84.60	-917.40	-198.22	247.42	0	-824.22	1.8	145.62	1.8	-114.70	2.12	-226.01
67	68	85.70	-920.89	-162.69	450.13	0	-607.58	1.8	-36.79	1.8	-137.72	2.12	-271.38
68	68	85.70	-1141.67	-170.20	331.71	0	-1004.16	1.8	44.42	1.8	-138.87	2.12	-267.03
68	69	86.80	-1141.67	-134.56	494.29	0	-832.58	1.8	-104.02	1.8	-157.16	2.12	-302.20
69	69	86.80	-1141.67	-134.51	494.37	0	-832.51	1.8	-104.04	1.8	-157.18	2.12	-302.23
69	70	87.90	-1141.67	-99.25	621.10	0	-697.61	1.8	-223.23	1.8	-171.16	2.12	-329.11
70	70	87.90	-1141.67	-99.15	621.15	0	-697.57	1.8	-223.24	1.8	-171.17	2.12	-329.13
70	71	89.00	-1141.67	-63.61	706.80	0	-603.65	1.8	-312.12	1.8	-179.95	2.12	-346.02
71	71	89.00	-1141.67	-63.55	706.81	0	-603.64	1.8	-312.13	1.8	-179.95	2.12	-346.02
71	72	90.10	-1141.67	-27.90	752.02	0	-550.16	1.8	-370.84	1.8	-183.65	2.12	-353.14
72	72	90.10	-1141.67	-27.85	752.00	0	-550.18	1.8	-370.84	1.8	-183.65	2.12	-353.13
72	73	91.20	-1141.67	7.57	757.03	0	-536.93	1.8	-399.43	1.8	-182.31	2.12	-350.56
73	73	91.20	-1141.67	7.61	756.97	0	-536.98	1.8	-399.41	1.8	-182.30	2.12	-350.54
73	74	92.30	-1141.67	42.84	728.17	0	-558.78	1.8	-399.12	1.8	-177.00	2.12	-340.34
74	74	92.30	-1141.67	42.79	728.08	0	-558.85	1.8	-399.10	1.8	-176.98	2.12	-340.31
74	75	93.40	-1141.67	78.34	657.57	0	-622.14	1.8	-368.36	1.8	-166.38	2.12	-319.92
75	75	93.40	-1141.67	78.20	657.43	0	-581.80	1.8	-350.84	1.8	-164.99	2.12	-325.11
75	76	94.50	-1141.67	113.82	546.34	0	-691.08	1.8	-290.14	1.8	-149.41	2.12	-294.41

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.T0.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	113.65	664.72	0	-345.18	1.8	-407.94	1.8	-149.39	2.12	-294.37
76	77	95.60	-944.83	151.24	513.14	0	-496.99	1.8	-317.18	1.8	-128.75	2.12	-253.71
77	77	95.60	-944.83	151.05	512.98	0	-497.13	1.8	-317.14	1.8	-128.72	2.12	-253.65
77	78	96.70	-944.83	192.70	327.89	0	-685.47	1.8	-197.64	1.8	-104.21	2.12	-205.35
78	78	96.70	-747.99	192.42	448.19	0	-336.47	1.8	-320.02	1.8	-104.18	2.12	-205.29
78	79	97.80	-747.99	227.91	222.26	0	-567.66	1.8	-170.37	1.8	-74.56	2.12	-146.92
79	79	97.80	-747.99	227.51	222.10	0	-567.79	1.8	-170.34	1.8	-74.53	2.12	-146.87
79	80	98.90	-747.99	263.06	-44.42	0	-841.61	1.8	9.41	1.8	-39.84	2.12	-78.50
80	80	98.90	-472.42	262.57	129.54	0	-344.23	1.8	-174.73	1.8	-39.81	2.12	-78.44
80	81	100.00	-472.42	153.40	-177.98	0	-661.80	1.8	37.46	1.8	-0.15	2.12	-0.30
101	101	0.00	-472.42	-166.28	-178.08	0	-661.89	1.8	37.48	1.8	-0.13	2.12	-0.27
101	102	1.10	-476.85	-284.23	153.75	0	-326.81	1.8	-183.14	1.8	-43.86	2.12	-86.43
102	102	1.10	-752.42	-283.03	-20.82	0	-824.72	1.8	1.12	1.8	-43.79	2.12	-86.29
102	103	2.20	-752.42	-245.73	265.87	0	-533.43	1.8	-182.74	1.8	-81.86	2.12	-161.30
103	103	2.20	-752.42	-244.70	265.48	0	-533.76	1.8	-182.67	1.8	-81.79	2.12	-161.18
103	104	3.30	-752.42	-207.49	507.62	0	-288.53	1.8	-335.64	1.8	-114.13	2.12	-224.89
104	104	3.30	-949.26	-206.59	386.80	0	-637.97	1.8	-213.16	1.8	-114.07	2.12	-224.78
104	105	4.40	-949.26	-169.27	585.14	0	-438.14	1.8	-335.39	1.8	-140.80	2.12	-277.44
105	105	4.40	-949.26	-168.57	584.79	0	-438.44	1.8	-335.32	1.8	-140.74	2.12	-277.33
105	106	5.50	-949.26	-121.50	747.25	0	-277.18	1.8	-428.38	1.8	-163.19	2.12	-321.57
106	106	5.50	-1146.10	-120.99	628.47	0	-623.42	1.8	-310.50	1.8	-163.14	2.12	-321.47
106	107	6.60	-1146.10	-83.64	747.46	0	-507.27	1.8	-372.92	1.8	-180.04	2.12	-354.76
107	107	6.60	-1146.10	-83.20	747.26	0	-552.02	1.8	-390.59	1.8	-181.49	2.12	-348.98
107	108	7.70	-1146.10	-45.95	822.78	0	-484.58	1.8	-422.49	1.8	-192.93	2.12	-370.98
108	108	7.70	-1146.10	-45.58	822.66	0	-484.67	1.8	-422.47	1.8	-192.91	2.12	-370.94
108	109	8.80	-1146.10	-8.35	854.75	0	-460.12	1.8	-423.59	1.8	-198.76	2.12	-382.19
109	109	8.80	-1146.10	-8.06	854.71	0	-460.16	1.8	-423.58	1.8	-198.75	2.12	-382.17
109	110	9.90	-1146.10	29.20	849.87	0	-473.19	1.8	-395.21	1.8	-200.11	2.12	-384.78
110	110	9.90	-1146.10	29.46	849.82	0	-473.23	1.8	-395.20	1.8	-200.10	2.12	-384.77
110	111	11.00	-1146.10	66.82	802.90	0	-528.04	1.8	-336.36	1.8	-196.09	2.12	-377.06
111	111	11.00	-1146.10	67.04	802.92	0	-528.02	1.8	-336.36	1.8	-196.10	2.12	-377.07
111	112	12.10	-1146.10	104.33	713.16	0	-625.25	1.8	-246.86	1.8	-186.60	2.12	-358.80
112	112	12.10	-1146.10	104.56	713.25	0	-625.17	1.8	-246.87	1.8	-186.62	2.12	-358.83
112	113	13.20	-1146.10	141.70	580.66	0	-764.81	1.8	-126.71	1.8	-171.63	2.12	-330.02
113	113	13.20	-1146.10	141.91	580.77	0	-764.72	1.8	-126.73	1.8	-171.65	2.12	-330.05
113	114	14.30	-1146.10	179.22	409.82	0	-943.09	1.8	23.17	1.8	-151.92	2.12	-292.13
114	114	14.30	-924.56	174.50	528.50	0	-542.19	1.8	-57.36	1.8	-150.71	2.12	-296.97
114	115	15.40	-917.39	209.16	314.19	0	-766.74	1.8	133.21	1.8	-125.96	2.12	-248.21
115	115	15.40	-1858.58	218.00	753.93	0	-571.80	1.8	-640.95	1.8	-408.34	2.12	-571.25
115	116	16.50	-1858.58	227.91	503.63	0	-804.94	1.8	-542.64	1.8	-371.48	2.12	-497.74
116	116	16.50	-1858.58	228.47	503.91	0	-721.72	1.8	-623.67	1.8	-441.85	2.12	-593.47
116	117	17.60	-1858.58	244.91	239.66	0	-999.17	1.8	-475.84	1.8	-383.79	2.12	-490.81
117	117	17.60	-2575.50	245.44	800.21	0	-505.35	1.8	-1008.77	1.8	-739.55	2.12	-932.06
117	118	18.70	-2575.50	225.81	531.97	0	-792.92	1.8	-839.34	1.8	-683.02	2.12	-832.11
118	118	18.70	-2575.50	226.16	531.71	0	-793.18	1.8	-839.26	1.8	-682.96	2.12	-831.99
118	119	19.80	-2575.50	213.13	288.61	0	-1062.93	1.8	-655.95	1.8	-635.43	2.12	-747.96
119	119	19.80	-2299.92	213.00	462.50	0	-565.64	1.8	-840.05	1.8	-635.37	2.12	-747.84
119	120	20.90	-2299.92	201.55	234.19	0	-827.58	1.8	-639.78	1.8	-594.24	2.12	-675.12
120	120	20.90	-2299.92	201.04	234.19	0	-827.58	1.8	-639.78	1.8	-594.24	2.12	-675.12
120	121	22.00	-2299.92	213.08	2.83	0	-1100.86	1.8	-411.28	1.8	-555.74	2.12	-607.05
121	1121	22.00	-2339.29	-209.77	-23.23	0	-1173.83	1.8	-382.21	1.8	-555.74	2.12	-607.05
121	122	23.40	-2339.29	-194.69	263.72	0	-821.26	1.8	-710.07	1.8	-597.95	2.12	-681.69
122	122	23.40	-2339.29	-195.31	263.76	0	-821.22	1.8	-710.08	1.8	-597.96	2.12	-681.71
122	123	24.80	-2339.29	-195.67	540.10	0	-492.50	1.8	-990.54	1.8	-643.00	2.12	-761.35
123	123	24.80	-2614.86	-196.59	368.52	0	-985.84	1.8	-812.72	1.8	-642.96	2.12	-761.27
123	124	26.20	-2614.86	-239.73	664.71	0	-648.45	1.8	-1064.54	1.8	-697.31	2.12	-857.38
124	124	26.20	-1701.11	-239.31	225.58	0	-791.98	1.8	-655.09	1.8	-341.69	2.12	-416.38
124	125	27.60	-1701.11	-235.52	554.94	0	-433.01	1.8	-882.23	1.8	-408.72	2.12	-534.89
125	125	27.60	-2055.42	-234.83	345.41	0	-1049.96	1.8	-678.43	1.8	-408.78	2.12	-534.99
125	126	29.00	-2055.42	-247.43	692.43	0	-684.46	1.8	-876.33	1.8	-484.55	2.12	-668.98
126	126	29.00	-1122.96	-242.41	252.65	0	-1016.70	1.8	83.70	1.8	-123.74	2.12	-243.83
126	127	30.40	-1129.71	-199.03	561.52	0	-697.29	1.8	-162.37	1.8	-161.43	2.12	-318.09
127	127	30.40	-1460.38	-201.07	381.11	0	-1288.15	1.8	-30.49	1.8	-162.71	2.12	-312.88
127	128	31.80	-1460.38	-152.47	622.06	0	-1043.67	1.8	-220.83	1.8	-192.17	2.12	-369.52
128	128	31.80	-1460.38	-152.47	621.85	0	-1043.84	1.8	-220.79	1.8	-192.14	2.12	-369.46
128	129	33.20	-1460.38	-98.11	796.71	0	-865.32	1.8	-362.23	1.8	-213.26	2.12	-410.06
129	129	33.20	-1460.38	-98.21	796.56	0	-865.44	1.8	-362.20	1.8	-213.23	2.12	-410.01
129	130	34.60	-1460.38	-58.60	907.43	0	-751.22	1.8	-454.98	1.8	-226.38	2.12	-435.29
130	130	34.60	-1460.38	-58.72	907.37	0	-751.27	1.8	-454.96	1.8	-226.37	2.12	-435.27
130	131	36.00	-1460.38	-10.65	948.48	0	-706.05	1.8	-498.08	1.8	-230.55	2.12	-443.31
131	131	36.00	-1460.38	-10.79	948.45	0	-706.07	1.8	-498.07	1.8	-230.54	2.12	-443.30
131	132	37.40	-1460.38	44.33	927.57	0	-723.51	1.8	-492.93	1.8	-227.09	2.12	-436.65
132	132	37.40	-1460.38	44.19	927.61	0	-723.47	1.8	-492.94	1.8	-227.09	2.12	-436.67
132	133	38.80	-1460.38	83.77	836.83	0	-810.00	1.8	-438.09	1.8	-214.66	2.12	-412.75
133	133	38.80	-1460.38	83.68	837.00	0	-809.87	1.8	-438.12	1.8	-214.68	2.12	-412.80

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.T0.MZ+

C. Infrecuentes dominante tren Mz+

[1. ...PVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	138.06	682.53	0	-960.44	1.8	-334.75	1.8	-194.31	2.12	-373.64
134	134	40.20	-1460.38	138.03	682.72	0	-960.28	1.8	-334.78	1.8	-194.35	2.12	-373.70
134	135	41.60	-1460.38	186.56	461.93	0	-1177.04	1.8	-182.35	1.8	-165.60	2.12	-318.43
135	135	41.60	-1135.74	186.09	642.33	0	-590.78	1.8	-319.17	1.8	-164.29	2.12	-323.73
135	136	43.00	-1128.92	229.77	352.56	0	-883.97	1.8	-108.42	1.8	-127.33	2.12	-250.89
136	136	43.00	-2055.42	233.17	792.34	0	-592.87	1.8	-888.76	1.8	-511.92	2.12	-717.37
136	137	44.40	-2055.42	230.96	463.90	0	-941.42	1.8	-692.94	1.8	-441.26	2.12	-592.43
137	137	44.40	-1701.11	231.56	673.54	0	-324.36	1.8	-896.77	1.8	-441.23	2.12	-592.38
137	138	45.80	-1701.11	238.67	345.73	0	-682.84	1.8	-666.75	1.8	-375.01	2.12	-475.29
138	138	45.80	-2614.86	239.38	784.78	0	-539.41	1.8	-1076.18	1.8	-730.61	2.12	-916.25
138	139	47.20	-2614.86	203.51	481.25	0	-884.91	1.8	-818.88	1.8	-674.81	2.12	-817.60
139	139	47.20	-2339.29	203.74	652.51	0	-391.89	1.8	-996.61	1.8	-674.78	2.12	-817.53
139	140	48.60	-2345.74	194.90	373.98	0	-725.74	1.8	-714.17	1.8	-631.32	2.12	-739.37
140	140	48.60	-2345.92	194.24	374.03	0	-725.73	1.8	-714.24	1.8	-631.38	2.12	-739.44
140	141	50.00	-2345.92	208.14	87.40	0	-1079.02	1.8	-383.14	1.8	-589.67	2.12	-665.68
141	1141	50.00	-2345.71	-208.22	87.40	0	-1078.95	1.8	-383.08	1.8	-589.62	2.12	-665.63
141	142	51.40	-2345.71	-194.32	374.15	0	-725.56	1.8	-714.21	1.8	-631.36	2.12	-739.44
142	142	51.40	-2345.10	-194.97	374.10	0	-725.42	1.8	-714.01	1.8	-631.18	2.12	-739.25
142	143	52.80	-2345.10	-203.31	652.65	0	-393.54	1.8	-998.45	1.8	-676.37	2.12	-819.15
143	143	52.80	-2619.68	-203.15	481.30	0	-886.35	1.8	-820.38	1.8	-676.12	2.12	-818.91
143	144	54.20	-2614.86	-239.38	784.78	0	-539.41	1.8	-1076.18	1.8	-730.61	2.12	-916.25
144	144	54.20	-1701.11	-238.69	345.74	0	-682.84	1.8	-666.75	1.8	-375.01	2.12	-475.30
144	145	55.60	-1701.11	-231.57	673.57	0	-324.33	1.8	-896.78	1.8	-441.24	2.12	-592.39
145	145	55.60	-2055.42	-230.99	463.92	0	-941.40	1.8	-692.95	1.8	-441.26	2.12	-592.44
145	146	57.00	-2055.42	-233.17	792.40	0	-592.81	1.8	-888.78	1.8	-511.93	2.12	-717.40
146	146	57.00	-1128.92	-229.79	352.62	0	-883.91	1.8	-108.43	1.8	-127.34	2.12	-250.91
146	147	58.40	-1133.95	-185.21	641.50	0	-590.62	1.8	-315.65	1.8	-164.30	2.12	-323.75
147	147	58.40	-1458.36	-186.66	461.08	0	-1176.72	1.8	-178.65	1.8	-165.61	2.12	-318.45
147	148	59.80	-1458.36	-138.11	681.95	0	-959.84	1.8	-331.25	1.8	-194.36	2.12	-373.72
148	148	59.80	-1458.36	-138.13	681.77	0	-959.99	1.8	-331.21	1.8	-194.32	2.12	-373.66
148	149	61.20	-1458.36	-83.74	836.30	0	-809.32	1.8	-434.77	1.8	-214.69	2.12	-412.82
149	149	61.20	-1458.36	-83.84	836.16	0	-809.43	1.8	-434.74	1.8	-214.67	2.12	-412.77
149	150	62.60	-1458.36	-44.24	927.05	0	-722.74	1.8	-489.81	1.8	-227.11	2.12	-436.70
150	150	62.60	-1458.36	-44.38	926.99	0	-722.79	1.8	-489.79	1.8	-227.10	2.12	-436.68
150	151	64.00	-1456.62	10.71	947.94	0	-703.82	1.8	-493.68	1.8	-230.55	2.12	-443.32
151	151	64.00	-1456.62	10.57	947.96	0	-703.81	1.8	-493.68	1.8	-230.56	2.12	-443.33
151	152	65.40	-1456.62	58.64	906.96	0	-748.87	1.8	-450.85	1.8	-226.37	2.12	-435.28
152	152	65.40	-1456.62	58.50	907.03	0	-748.81	1.8	-450.86	1.8	-226.38	2.12	-435.30
152	153	66.80	-1456.62	98.11	796.29	0	-862.84	1.8	-358.35	1.8	-213.24	2.12	-410.04
153	153	66.80	-1456.62	98.04	796.44	0	-862.71	1.8	-358.38	1.8	-213.27	2.12	-410.09
153	154	68.20	-1456.62	152.39	621.68	0	-1041.07	1.8	-217.20	1.8	-192.15	2.12	-369.48
154	154	68.20	-1456.62	152.39	621.86	0	-1040.92	1.8	-217.23	1.8	-192.18	2.12	-369.54
154	155	69.60	-1456.62	200.98	381.04	0	-1285.23	1.8	-27.15	1.8	-162.72	2.12	-312.89
155	155	69.60	-1126.45	197.16	561.46	0	-694.76	1.8	-159.44	1.8	-161.44	2.12	-318.11
155	156	71.00	-1122.96	242.41	252.69	0	-1016.68	1.8	83.71	1.8	-123.75	2.12	-243.85
156	156	71.00	-2055.42	247.45	692.46	0	-684.43	1.8	-876.34	1.8	-484.56	2.12	-668.99
156	157	72.40	-2055.42	234.83	345.43	0	-1049.95	1.8	-678.44	1.8	-408.78	2.12	-535.00
157	157	72.40	-1701.11	235.53	554.96	0	-432.99	1.8	-882.23	1.8	-408.73	2.12	-534.90
157	158	73.80	-1701.11	239.32	225.56	0	-791.99	1.8	-655.08	1.8	-341.69	2.12	-416.37
158	158	73.80	-2614.86	239.73	664.70	0	-648.47	1.8	-1064.53	1.8	-697.31	2.12	-857.37
158	159	75.20	-2614.86	196.59	368.50	0	-985.85	1.8	-812.71	1.8	-642.96	2.12	-761.26
159	159	75.20	-2339.29	195.66	540.11	0	-492.49	1.8	-990.54	1.8	-643.01	2.12	-761.35
159	160	76.60	-2343.12	194.84	264.27	0	-821.91	1.8	-711.41	1.8	-599.12	2.12	-682.96
160	160	76.60	-2343.06	194.19	264.31	0	-821.85	1.8	-711.40	1.8	-599.11	2.12	-682.96
160	161	78.00	-2343.06	209.28	-21.93	0	-1173.73	1.8	-383.75	1.8	-557.08	2.12	-608.65
161	1161	78.00	-2303.37	-212.93	4.13	0	-1100.66	1.8	-412.72	1.8	-557.00	2.12	-608.56
161	162	79.10	-2303.37	-200.90	235.35	0	-827.52	1.8	-641.18	1.8	-595.46	2.12	-676.56
162	162	79.10	-2302.99	-201.39	235.32	0	-827.44	1.8	-641.05	1.8	-595.35	2.12	-676.45
162	163	80.20	-2302.99	-212.86	463.47	0	-565.64	1.8	-841.28	1.8	-636.44	2.12	-749.10
163	163	80.20	-2578.03	-212.98	289.54	0	-1062.80	1.8	-657.01	1.8	-636.35	2.12	-749.06
163	164	81.30	-2578.03	-225.99	532.50	0	-793.19	1.8	-840.27	1.8	-683.84	2.12	-833.03
164	164	81.30	-2577.33	-225.66	532.69	0	-792.79	1.8	-840.11	1.8	-683.70	2.12	-832.92
164	165	82.40	-2577.33	-245.29	800.78	0	-505.36	1.8	-1009.50	1.8	-740.18	2.12	-932.80
165	165	82.40	-1859.54	-244.82	240.55	0	-998.36	1.8	-477.19	1.8	-384.17	2.12	-491.29
165	166	83.50	-1859.54	-228.38	504.30	0	-721.63	1.8	-624.08	1.8	-442.20	2.12	-593.90
166	166	83.50	-1858.58	-227.91	503.94	0	-804.68	1.8	-542.70	1.8	-371.53	2.12	-497.84
166	167	84.60	-1858.58	-218.00	754.20	0	-571.56	1.8	-641.00	1.8	-408.38	2.12	-571.33
167	167	84.60	-917.40	-209.13	314.47	0	-766.35	1.8	132.64	1.8	-125.97	2.12	-248.22
167	168	85.70	-920.89	-172.02	527.43	0	-540.86	1.8	-51.76	1.8	-150.72	2.12	-296.99
168	168	85.70	-1141.67	-179.30	408.73	0	-941.16	1.8	29.39	1.8	-151.93	2.12	-292.14
168	169	86.80	-1141.67	-141.98	579.80	0	-762.63	1.8	-120.71	1.8	-171.66	2.12	-330.07
169	169	86.80	-1141.67	-141.79	579.65	0	-762.76	1.8	-120.68	1.8	-171.63	2.12	-330.02
169	170	87.90	-1141.67	-104.66	712.34	0	-622.98	1.8	-241.06	1.8	-186.62	2.12	-358.85
170	170	87.90	-1141.67	-104.42	712.25	0	-623.05	1.8	-241.04	1.8	-186.61	2.12	-358.82
170	171	89.00	-1141.67	-67.14	802.10	0	-525.69	1.8	-330.74	1.8	-196.10	2.12	-377.08

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.T0.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-258.67	-198.52	0	-733.02	1.8	41.75	1.8	0.13	2.12	0.27
1	2	1.10	-517.71	-86.29	-91.73	0	-586.05	1.8	-125.44	1.8	-5.97	2.12	-11.77
2	2	1.10	-822.30	-86.62	-284.26	0	-1136.00	1.8	78.13	1.8	-5.97	2.12	-11.76
2	3	2.20	-822.30	-68.44	-198.96	0	-1019.49	1.8	-63.97	1.8	-10.40	2.12	-20.49
3	3	2.20	-822.30	-68.77	-198.98	0	-1019.51	1.8	-63.97	1.8	-10.39	2.12	-20.48
3	4	3.30	-822.30	-50.56	-133.37	0	-927.58	1.8	-180.00	1.8	-13.27	2.12	-26.15
4	4	3.30	-1039.86	-50.90	-266.54	0	-1313.49	1.8	-44.70	1.8	-13.27	2.12	-26.14
4	5	4.40	-1039.86	-32.72	-220.56	0	-1246.13	1.8	-134.64	1.8	-14.60	2.12	-28.77
5	5	4.40	-1039.86	-33.07	-220.58	0	-1246.14	1.8	-134.64	1.8	-14.60	2.12	-28.76
5	6	5.50	-1039.86	-14.87	-194.23	0	-1203.30	1.8	-198.57	1.8	-14.38	2.12	-28.34
6	6	5.50	-1257.42	-15.23	-325.23	0	-1585.75	1.8	-68.34	1.8	-14.38	2.12	-28.33
6	7	6.60	-1257.42	2.97	-318.44	0	-1567.38	1.8	-106.29	1.8	-12.63	2.12	-24.88
7	7	6.60	-1257.42	2.54	-318.49	0	-1564.09	1.8	-123.73	1.8	-12.72	2.12	-24.46
7	8	7.70	-1257.42	20.73	-331.28	0	-1569.80	1.8	-135.61	1.8	-9.41	2.12	-18.10
8	8	7.70	-1257.42	20.32	-331.32	0	-1569.82	1.8	-135.61	1.8	-9.41	2.12	-18.09
8	9	8.80	-1257.42	38.81	-363.69	0	-1598.92	1.8	-121.37	1.8	-4.55	2.12	-8.74
9	9	8.80	-1257.42	38.24	-363.73	0	-1598.96	1.8	-121.36	1.8	-4.54	2.12	-8.73
9	10	9.90	-1257.42	56.57	-415.84	0	-1651.57	1.8	-80.99	1.8	1.89	2.12	3.64
10	10	9.90	-1257.42	56.04	-415.85	0	-1651.58	1.8	-80.99	1.8	1.90	2.12	3.65
10	11	11.00	-1257.42	74.23	-487.53	0	-1727.55	1.8	-14.54	1.8	9.88	2.12	19.00
11	11	11.00	-1257.42	73.67	-487.55	0	-1727.57	1.8	-14.53	1.8	9.88	2.12	19.00
11	12	12.10	-1257.42	91.89	-578.61	0	-1826.78	1.8	78.00	1.8	19.38	2.12	37.27
12	12	12.10	-1257.42	91.31	-578.65	0	-1826.81	1.8	78.01	1.8	19.39	2.12	37.28
12	13	13.20	-1257.42	109.57	-689.21	0	-1949.35	1.8	196.68	1.8	30.42	2.12	58.49
13	13	13.20	-1257.42	108.98	-689.23	0	-1949.37	1.8	196.68	1.8	30.42	2.12	58.50
13	14	14.30	-1257.42	127.21	-819.14	0	-2095.08	1.8	341.32	1.8	42.97	2.12	82.62
14	14	14.30	-1016.08	116.35	-688.20	0	-1712.92	1.8	247.36	1.8	42.62	2.12	83.98
14	15	15.40	-1016.27	137.04	-836.67	0	-1885.61	1.8	415.78	1.8	56.57	2.12	111.47
15	15	15.40	-1871.02	145.20	-439.02	0	-1688.54	1.8	-363.48	1.8	-198.82	2.12	-176.59
15	16	16.50	-1871.02	195.91	-614.11	0	-1856.90	1.8	-279.29	1.8	-174.22	2.12	-127.51
16	16	16.50	-1871.02	195.45	-614.02	0	-1887.50	1.8	-249.38	1.8	-148.24	2.12	-92.19
16	17	17.60	-1871.02	226.31	-843.57	0	-2131.38	1.8	-111.58	1.8	-98.97	2.12	-5.08
17	17	17.60	-2480.19	225.56	-312.11	0	-1614.41	1.8	-618.50	1.8	-420.86	2.12	-404.33
17	18	18.70	-2480.19	273.17	-585.87	0	-1907.33	1.8	-447.46	1.8	-362.94	2.12	-301.92
18	18	18.70	-2480.18	272.48	-585.38	0	-1906.85	1.8	-447.60	1.8	-363.07	2.12	-302.13
18	19	19.80	-2480.18	326.12	-912.98	0	-2258.38	1.8	-239.67	1.8	-294.16	2.12	-180.29
19	19	19.80	-2175.60	325.52	-719.84	0	-1707.83	1.8	-443.42	1.8	-294.32	2.12	-180.58
19	20	20.90	-2175.60	394.03	-1122.27	0	-2138.29	1.8	-192.40	1.8	-209.12	2.12	-29.93
20	20	20.90	-2175.60	393.67	-1122.24	0	-2138.27	1.8	-192.41	1.8	-209.13	2.12	-29.94
20	21	22.00	-2175.60	454.57	-1587.47	0	-2637.89	1.8	104.24	1.8	-111.44	2.12	142.79
21	1021	22.00	-2219.11	-480.42	-1616.17	0	-2718.43	1.8	136.34	1.8	-111.47	2.12	142.74
21	22	23.40	-2219.11	-416.58	-994.35	0	-2041.78	1.8	-289.10	1.8	-238.43	2.12	-81.76
22	22	23.40	-2219.11	-417.02	-994.17	0	-2041.60	1.8	-289.16	1.8	-238.48	2.12	-81.84
22	23	24.80	-2219.11	-345.94	-460.32	0	-1463.66	1.8	-644.66	1.8	-348.70	2.12	-276.72
23	23	24.80	-2523.70	-344.43	-649.74	0	-2008.71	1.8	-448.18	1.8	-348.70	2.12	-276.74
23	24	26.20	-2523.70	-259.43	-238.38	0	-1559.87	1.8	-733.56	1.8	-432.20	2.12	-424.38
24	24	26.20	-1696.97	-259.40	-636.75	0	-1690.74	1.8	-362.80	1.8	-110.19	2.12	-24.91
24	25	27.60	-1696.97	-196.39	-318.52	0	-1342.56	1.8	-586.70	1.8	-174.39	2.12	-138.44
25	25	27.60	-2088.58	-197.14	-551.03	0	-2025.34	1.8	-361.18	1.8	-174.22	2.12	-138.14
25	26	29.00	-2088.58	-115.85	-351.58	0	-1802.65	1.8	-516.08	1.8	-212.65	2.12	-206.09
26	26	29.00	-1242.90	-111.88	-749.33	0	-2034.70	1.8	352.77	1.8	31.22	2.12	61.51
26	27	30.40	-1243.14	-85.13	-604.54	0	-1851.32	1.8	142.91	1.8	21.19	2.12	41.76
27	27	30.40	-1606.18	-91.66	-803.70	0	-2446.00	1.8	292.73	1.8	21.37	2.12	41.10
27	28	31.80	-1606.18	-68.40	-691.65	0	-2306.64	1.8	126.60	1.8	13.84	2.12	26.61
28	28	31.80	-1606.18	-69.17	-691.71	0	-2306.69	1.8	126.61	1.8	13.85	2.12	26.62
28	29	33.20	-1606.18	-46.03	-611.06	0	-2204.93	1.8	2.65	1.8	8.77	2.12	16.87
29	29	33.20	-1606.18	-46.75	-611.06	0	-2204.93	1.8	2.65	1.8	8.77	2.12	16.87
29	30	34.60	-1606.18	-22.01	-563.24	0	-2141.97	1.8	-78.78	1.8	6.39	2.12	12.29
30	30	34.60	-1606.18	-22.70	-563.32	0	-2142.04	1.8	-78.76	1.8	6.40	2.12	12.32
30	31	36.00	-1606.18	5.06	-551.74	0	-2120.66	1.8	-117.03	1.8	7.30	2.12	14.04
31	31	36.00	-1606.18	4.38	-551.76	0	-2120.67	1.8	-117.02	1.8	7.30	2.12	14.04
31	32	37.40	-1606.18	27.67	-574.12	0	-2138.99	1.8	-112.57	1.8	11.09	2.12	21.32
32	32	37.40	-1606.18	26.91	-574.14	0	-2139.01	1.8	-112.57	1.8	11.09	2.12	21.33
32	33	38.80	-1606.18	50.07	-628.01	0	-2195.05	1.8	-65.86	1.8	17.35	2.12	33.36
33	33	38.80	-1606.18	49.31	-628.02	0	-2195.05	1.8	-65.85	1.8	17.35	2.12	33.36
33	34	40.20	-1606.18	72.48	-713.29	0	-2288.72	1.8	23.10	1.8	26.06	2.12	50.11
34	34	40.20	-1606.18	71.69	-713.26	0	-2288.69	1.8	23.09	1.8	26.06	2.12	50.10
34	35	41.60	-1606.18	94.97	-829.87	0	-2419.93	1.8	154.25	1.8	37.21	2.12	71.56
35	35	41.60	-1249.48	90.04	-630.75	0	-1835.10	1.8	-0.92	1.8	36.91	2.12	72.72
35	36	43.00	-1249.32	116.32	-778.81	0	-2009.64	1.8	171.23	1.8	50.50	2.12	99.51
36	36	43.00	-2088.58	118.62	-381.06	0	-1836.30	1.8	-490.80	1.8	-207.27	2.12	-196.57
36	37	44.40	-2088.58	191.83	-585.41	0	-2064.76	1.8	-331.14	1.8	-168.01	2.12	-127.16
37	37	44.40	-1696.97	191.00	-353.04	0	-1382.10	1.8	-556.62	1.8	-168.15	2.12	-127.40
37	38	45.80	-1696.97	250.40	-658.25	0	-1718.70	1.8	-333.19	1.8	-107.65	2.12	-20.43
38	38	45.80	-2523.70	249.71	-259.75	0	-1587.70	1.8	-703.99	1.8	-429.70	2.12	-419.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.T0.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	316.54	-651.32	0	-2018.42	1.8	-421.04	1.8	-351.63	2.12	-281.91
39	39	47.20	-2219.11	315.43	-461.41	0	-1472.89	1.8	-617.66	1.8	-351.74	2.12	-282.11
39	40	48.60	-2212.66	403.99	-967.87	0	-2023.36	1.8	-264.82	1.8	-247.15	2.12	-98.49
40	40	48.60	-2212.49	403.49	-967.98	0	-2023.40	1.8	-264.73	1.8	-247.08	2.12	-98.40
40	41	50.00	-2212.49	470.65	-1575.62	0	-2687.36	1.8	159.91	1.8	-124.12	2.12	119.02
41	1041	50.00	-2212.70	-470.56	-1575.62	0	-2687.43	1.8	159.85	1.8	-124.17	2.12	118.96
41	42	51.40	-2212.70	-403.42	-968.09	0	-2023.58	1.8	-264.77	1.8	-247.10	2.12	-98.40
42	42	51.40	-2213.30	-403.91	-968.01	0	-2023.69	1.8	-264.97	1.8	-247.28	2.12	-98.60
42	43	52.80	-2213.30	-315.85	-461.55	0	-1471.23	1.8	-615.83	1.8	-350.15	2.12	-280.49
43	43	52.80	-2518.88	-316.90	-651.35	0	-2016.97	1.8	-419.55	1.8	-350.33	2.12	-280.60
43	44	54.20	-2523.70	-249.71	-259.73	0	-1587.68	1.8	-703.99	1.8	-429.71	2.12	-419.97
44	44	54.20	-1696.97	-250.40	-658.24	0	-1718.70	1.8	-333.19	1.8	-107.65	2.12	-20.43
44	45	55.60	-1696.97	-190.99	-353.01	0	-1382.07	1.8	-556.63	1.8	-168.16	2.12	-127.42
45	45	55.60	-2088.58	-191.83	-585.40	0	-2064.74	1.8	-331.14	1.8	-168.02	2.12	-127.17
45	46	57.00	-2088.58	-118.61	-381.01	0	-1836.25	1.8	-490.81	1.8	-207.28	2.12	-196.59
46	46	57.00	-1249.32	-116.33	-778.79	0	-2009.62	1.8	171.20	1.8	50.50	2.12	99.50
46	47	58.40	-1251.27	-90.97	-629.84	0	-1835.19	1.8	-4.47	1.8	36.90	2.12	72.72
47	47	58.40	-1608.20	-94.90	-828.98	0	-2420.20	1.8	150.53	1.8	37.21	2.12	71.56
47	48	59.80	-1608.20	-71.64	-712.43	0	-2289.08	1.8	19.55	1.8	26.05	2.12	50.10
48	48	59.80	-1608.20	-72.41	-712.44	0	-2289.09	1.8	19.55	1.8	26.06	2.12	50.10
48	49	61.20	-1608.20	-49.24	-627.29	0	-2195.59	1.8	-69.19	1.8	17.35	2.12	33.36
49	49	61.20	-1608.20	-50.01	-627.29	0	-2195.58	1.8	-69.19	1.8	17.35	2.12	33.36
49	50	62.60	-1608.20	-26.85	-573.47	0	-2139.64	1.8	-115.74	1.8	11.09	2.12	21.32
50	50	62.60	-1608.20	-27.61	-573.48	0	-2139.65	1.8	-115.74	1.8	11.09	2.12	21.33
50	51	64.00	-1609.94	-4.29	-551.18	0	-2122.87	1.8	-121.41	1.8	7.30	2.12	14.04
51	51	64.00	-1609.94	-4.98	-551.18	0	-2122.87	1.8	-121.41	1.8	7.30	2.12	14.04
51	52	65.40	-1609.94	22.80	-562.87	0	-2144.42	1.8	-82.89	1.8	6.41	2.12	12.32
52	52	65.40	-1609.94	22.09	-562.81	0	-2144.36	1.8	-82.90	1.8	6.39	2.12	12.30
52	53	66.80	-1609.94	46.83	-610.73	0	-2207.48	1.8	-1.22	1.8	8.77	2.12	16.87
53	53	66.80	-1609.94	46.12	-610.71	0	-2207.47	1.8	-1.22	1.8	8.77	2.12	16.86
53	54	68.20	-1609.94	69.25	-691.46	0	-2309.38	1.8	122.98	1.8	13.84	2.12	26.62
54	54	68.20	-1609.94	68.48	-691.44	0	-2309.36	1.8	122.98	1.8	13.84	2.12	26.61
54	55	69.60	-1609.94	91.74	-803.58	0	-2448.87	1.8	289.36	1.8	21.37	2.12	41.10
55	55	69.60	-1246.39	87.01	-604.44	0	-1853.80	1.8	139.95	1.8	21.20	2.12	41.77
55	56	71.00	-1242.90	111.88	-749.33	0	-2034.71	1.8	352.79	1.8	31.22	2.12	61.51
56	56	71.00	-2088.58	115.85	-351.58	0	-1802.66	1.8	-516.08	1.8	-212.65	2.12	-206.09
56	57	72.40	-2088.58	197.14	-551.03	0	-2025.35	1.8	-361.18	1.8	-174.22	2.12	-138.14
57	57	72.40	-1696.97	196.41	-318.53	0	-1342.57	1.8	-586.69	1.8	-174.39	2.12	-138.44
57	58	73.80	-1696.97	259.42	-636.76	0	-1690.75	1.8	-362.80	1.8	-110.18	2.12	-24.91
58	58	73.80	-2523.70	259.43	-238.39	0	-1559.87	1.8	-733.56	1.8	-432.20	2.12	-424.38
58	59	75.20	-2523.70	344.43	-649.77	0	-2008.74	1.8	-448.17	1.8	-348.70	2.12	-276.72
59	59	75.20	-2219.11	345.93	-460.31	0	-1463.65	1.8	-644.66	1.8	-348.70	2.12	-276.73
59	60	76.60	-2215.29	417.48	-994.69	0	-2040.92	1.8	-287.83	1.8	-237.32	2.12	-80.58
60	60	76.60	-2215.34	417.08	-994.96	0	-2041.20	1.8	-287.76	1.8	-237.27	2.12	-80.47
60	61	78.00	-2215.34	480.94	-1617.48	0	-2718.54	1.8	137.88	1.8	-110.13	2.12	144.34
61	1061	78.00	-2172.15	-454.72	-1588.86	0	-2638.17	1.8	105.71	1.8	-110.17	2.12	144.33
61	62	79.10	-2172.15	-393.82	-1123.45	0	-2138.37	1.8	-191.00	1.8	-207.90	2.12	-28.48
62	62	79.10	-2172.53	-394.20	-1123.48	0	-2138.53	1.8	-191.10	1.8	-207.99	2.12	-28.56
62	63	80.20	-2172.53	-325.69	-720.84	0	-1707.86	1.8	-442.18	1.8	-293.24	2.12	-179.30
63	63	80.20	-2477.65	-326.30	-913.96	0	-2258.55	1.8	-238.60	1.8	-293.23	2.12	-179.17
63	64	81.30	-2477.65	-272.66	-586.18	0	-1906.85	1.8	-446.58	1.8	-362.18	2.12	-301.10
64	64	81.30	-2478.35	-273.32	-586.62	0	-1907.49	1.8	-446.67	1.8	-362.26	2.12	-301.09
64	65	82.40	-2478.35	-225.71	-312.68	0	-1614.40	1.8	-617.77	1.8	-420.23	2.12	-403.58
65	65	82.40	-1870.06	-226.41	-843.63	0	-2130.88	1.8	-112.14	1.8	-98.59	2.12	-4.60
65	66	83.50	-1870.06	-195.56	-614.40	0	-1887.57	1.8	-248.97	1.8	-147.88	2.12	-91.76
66	66	83.50	-1871.02	-195.93	-614.38	0	-1857.13	1.8	-279.24	1.8	-174.17	2.12	-127.43
66	67	84.60	-1871.02	-145.23	-439.27	0	-1688.76	1.8	-363.44	1.8	-198.78	2.12	-176.50
67	67	84.60	-1016.26	-137.04	-836.94	0	-1885.98	1.8	416.34	1.8	56.57	2.12	111.47
67	68	85.70	-1019.75	-118.80	-687.10	0	-1714.23	1.8	241.75	1.8	42.62	2.12	83.99
68	68	85.70	-1261.85	-127.13	-818.04	0	-2097.01	1.8	335.10	1.8	42.97	2.12	82.63
68	69	86.80	-1261.85	-108.90	-688.21	0	-1951.42	1.8	190.64	1.8	30.43	2.12	58.50
69	69	86.80	-1261.85	-109.50	-688.18	0	-1951.40	1.8	190.63	1.8	30.42	2.12	58.50
69	70	87.90	-1261.85	-91.25	-577.73	0	-1829.02	1.8	72.21	1.8	19.39	2.12	37.29
70	70	87.90	-1261.85	-91.82	-577.69	0	-1828.98	1.8	72.21	1.8	19.38	2.12	37.27
70	71	89.00	-1261.85	-73.60	-486.72	0	-1729.91	1.8	-20.13	1.8	9.89	2.12	19.01
71	71	89.00	-1261.85	-74.17	-486.69	0	-1729.88	1.8	-20.14	1.8	9.88	2.12	19.00
71	72	90.10	-1261.85	-55.97	-415.11	0	-1654.03	1.8	-86.41	1.8	1.90	2.12	3.66
72	72	90.10	-1261.85	-56.50	-415.08	0	-1654.01	1.8	-86.41	1.8	1.90	2.12	3.65
72	73	91.20	-1261.85	-38.18	-363.08	0	-1601.55	1.8	-126.58	1.8	-4.53	2.12	-8.72
73	73	91.20	-1261.85	-38.74	-363.01	0	-1601.50	1.8	-126.59	1.8	-4.54	2.12	-8.74
73	74	92.30	-1261.85	-20.25	-330.73	0	-1572.53	1.8	-140.63	1.8	-9.40	2.12	-18.08
74	74	92.30	-1261.85	-20.66	-330.70	0	-1572.51	1.8	-140.63	1.8	-9.41	2.12	-18.09
74	75	93.40	-1261.85	-2.47	-317.98	0	-1566.92	1.8	-128.55	1.8	-12.72	2.12	-24.46
75	75	93.40	-1261.85	-2.90	-317.95	0	-1570.12	1.8	-111.04	1.8	-12.62	2.12	-24.87
75	76	94.50	-1261.85	15.30	-324.80	0	-1588.61	1.8	-72.91	1.8	-14.37	2.12	-28.32

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.T0.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	14.94	-193.79	0	-1206.15	1.8	-203.15	1.8	-14.38	2.12	-28.34
76	77	95.60	-1044.29	33.14	-220.25	0	-1249.14	1.8	-139.01	1.8	-14.59	2.12	-28.75
77	77	95.60	-1044.29	32.79	-220.22	0	-1249.12	1.8	-139.01	1.8	-14.60	2.12	-28.76
77	78	96.70	-1044.29	50.97	-266.30	0	-1316.65	1.8	-48.82	1.8	-13.26	2.12	-26.14
78	78	96.70	-826.73	50.63	-133.14	0	-930.75	1.8	-184.12	1.8	-13.27	2.12	-26.14
78	79	97.80	-826.73	68.84	-198.82	0	-1022.79	1.8	-67.89	1.8	-10.39	2.12	-20.48
79	79	97.80	-826.73	68.49	-198.80	0	-1022.77	1.8	-67.90	1.8	-10.40	2.12	-20.49
79	80	98.90	-826.73	86.68	-284.17	0	-1139.41	1.8	74.38	1.8	-5.97	2.12	-11.76
80	80	98.90	-522.14	86.36	-91.65	0	-589.46	1.8	-129.19	1.8	-5.97	2.12	-11.77
80	81	100.00	-522.14	258.64	-198.52	0	-733.02	1.8	41.75	1.8	0.13	2.12	0.27
101	101	0.00	-522.14	-264.49	-198.62	0	-733.11	1.8	41.77	1.8	0.15	2.12	0.30
101	102	1.10	-517.71	-83.03	-95.44	0	-589.25	1.8	-124.72	1.8	-5.35	2.12	-10.54
102	102	1.10	-822.30	-83.38	-287.71	0	-1138.99	1.8	78.80	1.8	-5.39	2.12	-10.62
102	103	2.20	-822.30	-65.56	-205.83	0	-1025.41	1.8	-62.64	1.8	-9.24	2.12	-18.21
103	103	2.20	-822.30	-65.82	-205.61	0	-1025.23	1.8	-62.69	1.8	-9.28	2.12	-18.28
103	104	3.30	-822.30	-48.02	-143.05	0	-935.94	1.8	-178.13	1.8	-11.64	2.12	-22.94
104	104	3.30	-1039.86	-48.14	-276.00	0	-1321.66	1.8	-42.86	1.8	-11.67	2.12	-23.00
104	105	4.40	-1039.86	-30.37	-232.83	0	-1256.70	1.8	-132.29	1.8	-12.53	2.12	-24.70
105	105	4.40	-1039.86	-30.43	-232.69	0	-1256.58	1.8	-132.32	1.8	-12.56	2.12	-24.75
105	106	5.50	-1039.86	-12.63	-209.01	0	-1216.06	1.8	-195.73	1.8	-11.89	2.12	-23.44
106	106	5.50	-1257.42	-12.56	-339.84	0	-1598.35	1.8	-65.54	1.8	-11.92	2.12	-23.49
106	107	6.60	-1257.42	5.25	-335.81	0	-1582.37	1.8	-102.93	1.8	-9.71	2.12	-19.13
107	107	6.60	-1257.42	5.36	-335.68	0	-1578.15	1.8	-120.37	1.8	-9.81	2.12	-18.86
107	108	7.70	-1257.42	23.14	-351.37	0	-1586.22	1.8	-131.69	1.8	-6.01	2.12	-11.55
108	108	7.70	-1257.42	23.31	-351.25	0	-1586.13	1.8	-131.72	1.8	-6.03	2.12	-11.59
108	109	8.80	-1257.42	41.10	-386.67	0	-1617.72	1.8	-116.89	1.8	-0.65	2.12	-1.25
109	109	8.80	-1257.42	41.28	-386.59	0	-1617.66	1.8	-116.90	1.8	-0.66	2.12	-1.28
109	110	9.90	-1257.42	59.07	-441.83	0	-1672.82	1.8	-75.92	1.8	6.30	2.12	12.11
110	110	9.90	-1257.42	59.31	-441.78	0	-1672.78	1.8	-75.93	1.8	6.29	2.12	12.10
110	111	11.00	-1257.42	77.12	-516.78	0	-1751.48	1.8	-8.83	1.8	14.84	2.12	28.53
111	111	11.00	-1257.42	77.41	-516.75	0	-1751.46	1.8	-8.83	1.8	14.83	2.12	28.52
111	112	12.10	-1257.42	95.21	-611.72	0	-1853.86	1.8	84.47	1.8	24.99	2.12	48.06
112	112	12.10	-1257.42	95.53	-611.71	0	-1853.85	1.8	84.46	1.8	24.99	2.12	48.06
112	113	13.20	-1257.42	113.30	-726.60	0	-1979.94	1.8	203.96	1.8	36.76	2.12	70.68
113	113	13.20	-1257.42	113.65	-726.64	0	-1979.97	1.8	203.96	1.8	36.76	2.12	70.69
113	114	14.30	-1257.42	131.50	-861.47	0	-2129.71	1.8	349.58	1.8	50.14	2.12	96.42
114	114	14.30	-1016.08	121.64	-730.57	0	-1749.48	1.8	255.56	1.8	49.74	2.12	98.02
114	115	15.40	-1016.27	142.17	-884.64	0	-1927.01	1.8	425.06	1.8	64.63	2.12	127.36
115	115	15.40	-1871.02	151.42	-487.09	0	-1729.95	1.8	-354.47	1.8	-190.99	2.12	-160.97
115	116	16.50	-1871.02	196.40	-668.99	0	-1904.17	1.8	-269.00	1.8	-165.28	2.12	-109.69
116	116	16.50	-1871.02	196.77	-669.10	0	-1940.80	1.8	-233.33	1.8	-134.29	2.12	-67.54
116	117	17.60	-1871.02	226.20	-899.69	0	-2185.70	1.8	-95.22	1.8	-84.76	2.12	20.04
117	117	17.60	-2480.18	226.43	-368.48	0	-1668.97	1.8	-602.07	1.8	-406.60	2.12	-379.10
117	118	18.70	-2480.18	283.87	-650.59	0	-1969.97	1.8	-428.60	1.8	-346.56	2.12	-272.95
118	118	18.70	-2480.18	284.29	-650.24	0	-1969.63	1.8	-428.70	1.8	-346.65	2.12	-273.10
118	119	19.80	-2480.18	350.12	-997.59	0	-2340.27	1.8	-215.01	1.8	-272.74	2.12	-142.42
119	119	19.80	-2175.60	351.07	-804.83	0	-1790.09	1.8	-418.65	1.8	-272.81	2.12	-142.54
119	120	20.90	-2175.60	434.32	-1245.96	0	-2258.01	1.8	-156.36	1.8	-177.82	2.12	25.43
120	120	20.90	-2175.60	435.63	-1245.89	0	-2257.94	1.8	-156.38	1.8	-177.84	2.12	25.39
120	121	22.00	-2175.60	492.42	-1752.03	0	-2797.16	1.8	152.19	1.8	-69.79	2.12	216.43
121	1121	22.00	-2219.11	-516.10	-1780.83	0	-2877.79	1.8	184.32	1.8	-69.80	2.12	216.43
121	122	23.40	-2219.11	-447.17	-1111.03	0	-2154.70	1.8	-255.10	1.8	-208.90	2.12	-29.54
122	122	23.40	-2219.11	-445.47	-1111.15	0	-2154.82	1.8	-255.07	1.8	-208.87	2.12	-29.49
122	123	24.80	-2219.11	-370.84	-540.93	0	-1541.68	1.8	-621.17	1.8	-328.29	2.12	-240.65
123	123	24.80	-2523.70	-368.89	-730.41	0	-2086.78	1.8	-424.67	1.8	-328.29	2.12	-240.64
123	124	26.20	-2523.70	-271.35	-294.78	0	-1614.45	1.8	-717.13	1.8	-417.93	2.12	-399.14
124	124	26.20	-1696.97	-270.82	-692.99	0	-1745.17	1.8	-346.41	1.8	-95.95	2.12	0.26
124	125	27.60	-1696.97	-203.13	-363.61	0	-1386.19	1.8	-573.56	1.8	-162.98	2.12	-118.27
125	125	27.60	-2088.58	-202.99	-595.89	0	-2068.76	1.8	-348.10	1.8	-162.87	2.12	-118.06
125	126	29.00	-2088.58	-120.16	-384.63	0	-1834.64	1.8	-506.45	1.8	-204.29	2.12	-191.30
126	126	29.00	-1242.90	-114.76	-782.18	0	-2063.06	1.8	359.15	1.8	36.74	2.12	72.40
126	127	30.40	-1243.14	-89.18	-632.39	0	-1875.36	1.8	148.30	1.8	25.87	2.12	50.98
127	127	30.40	-1606.18	-94.35	-831.43	0	-2468.68	1.8	298.14	1.8	26.07	2.12	50.14
127	128	31.80	-1606.18	-71.53	-715.40	0	-2326.07	1.8	131.24	1.8	17.86	2.12	34.35
128	128	31.80	-1606.18	-70.90	-715.34	0	-2326.02	1.8	131.23	1.8	17.85	2.12	34.33
128	129	33.20	-1606.18	-48.27	-631.87	0	-2221.94	1.8	6.69	1.8	12.30	2.12	23.65
129	129	33.20	-1606.18	-47.70	-631.83	0	-2221.91	1.8	6.68	1.8	12.29	2.12	23.64
129	130	34.60	-1606.18	-23.60	-581.96	0	-2157.28	1.8	-75.13	1.8	9.56	2.12	18.39
130	130	34.60	-1606.18	-23.02	-581.99	0	-2157.31	1.8	-75.12	1.8	9.57	2.12	18.40
130	131	36.00	-1606.18	5.18	-570.18	0	-2135.74	1.8	-113.45	1.8	10.43	2.12	20.05
131	131	36.00	-1606.18	5.78	-570.17	0	-2135.73	1.8	-113.45	1.8	10.43	2.12	20.05
131	132	37.40	-1606.18	28.46	-594.14	0	-2155.37	1.8	-108.64	1.8	14.48	2.12	27.84
132	132	37.40	-1606.18	29.05	-594.14	0	-2155.38	1.8	-108.64	1.8	14.48	2.12	27.84
132	133	38.80	-1606.18	51.70	-650.67	0	-2213.59	1.8	-61.41	1.8	21.19	2.12	40.74
133	133	38.80	-1606.18	52.33	-650.70	0	-2213.61	1.8	-61.41	1.8	21.19	2.12	40.75

CULO TENSIONAL

sis de cálculo:

CUEN ST.T0.MZ-

ecue, dominante tren Mz-

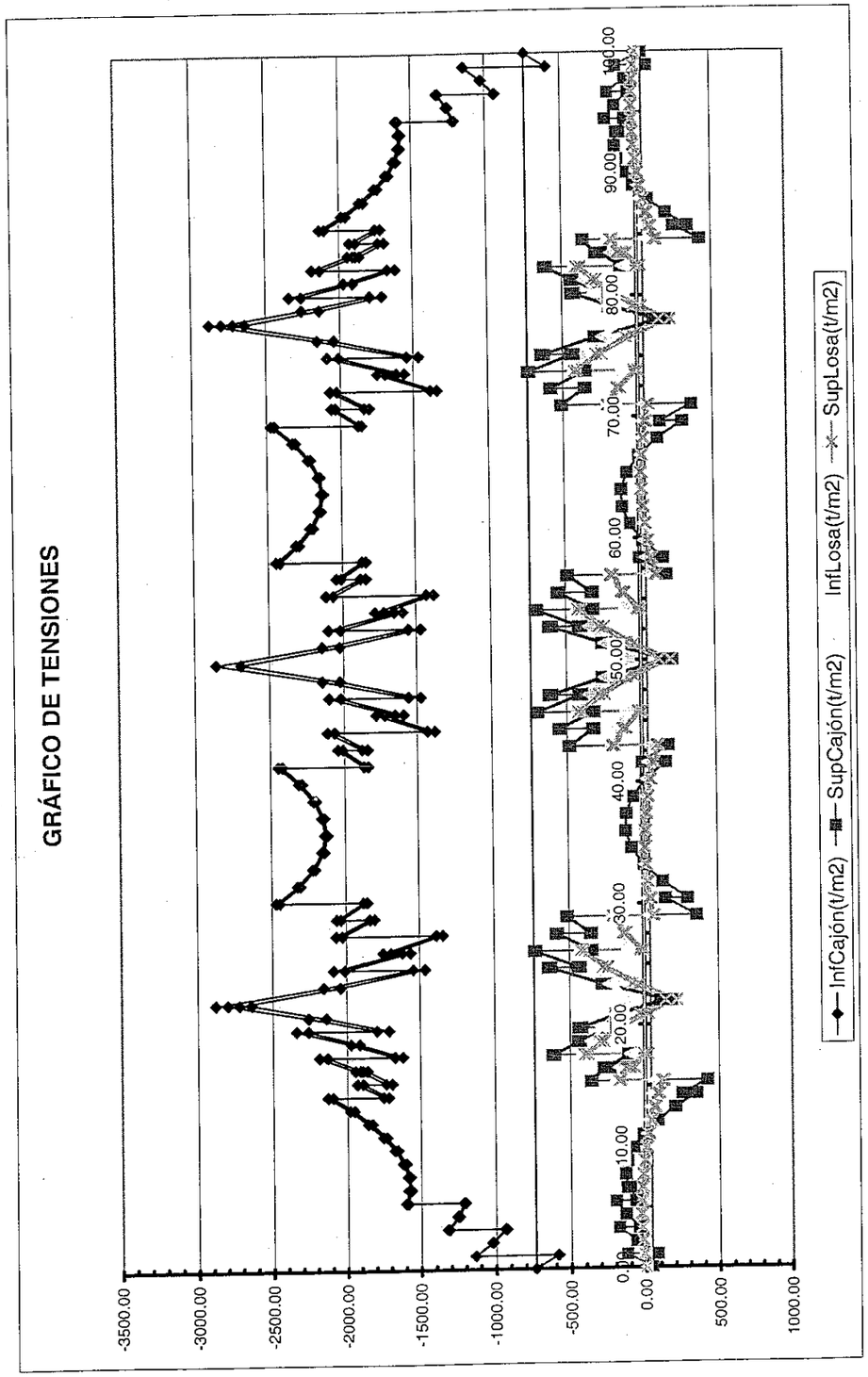
F1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME ; 1.3]CME

	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)	osa /m2)
33	134	40.20	-1606.18	75.00	-739.81	0	-2310.41	1.8	28.28	1.8	30.56	2.12	58.76	28.53
34	134	40.20	-1606.18	75.62	-739.86	0	-2310.45	1.8	28.29	1.8	30.56	2.12	58.77	12.10
34	135	41.60	-1606.18	98.44	-861.66	0	-2445.93	1.8	160.46	1.8	42.60	2.12	81.92	12.12
35	135	41.60	-1249.48	94.92	-662.61	0	-1862.61	1.8	5.25	1.8	42.26	2.12	83.28	-1.27
35	136	43.00	-1249.32	120.26	-817.04	0	-2042.65	1.8	178.63	1.8	56.93	2.12	112.17	-1.24
36	136	43.00	-2088.58	124.14	-419.46	0	-1873.46	1.8	-479.61	1.8	-197.55	2.12	-179.38	11.58
36	137	44.40	-2088.58	196.62	-634.97	0	-2112.72	1.8	-316.70	1.8	-155.47	2.12	-104.98	11.55
37	137	44.40	-1696.97	196.92	-402.84	0	-1430.29	1.8	-542.11	1.8	-155.55	2.12	-105.12	18.86
37	138	45.80	-1696.97	261.08	-719.33	0	-1777.82	1.8	-315.39	1.8	-92.19	2.12	6.90	19.12
38	138	45.80	-2523.70	261.38	-321.00	0	-1646.98	1.8	-686.14	1.8	-414.20	2.12	-392.55	23.49
38	139	47.20	-2523.70	336.93	-735.36	0	-2099.76	1.8	-396.55	1.8	-330.36	2.12	-244.29	23.44
39	139	47.20	-2219.11	337.72	-545.65	0	-1554.42	1.8	-593.11	1.8	-330.42	2.12	-244.41	24.75
39	140	48.60	-2212.66	433.57	-1091.69	0	-2143.19	1.8	-228.74	1.8	-215.81	2.12	-43.08	24.69
40	140	48.60	-2212.49	435.30	-1091.63	0	-2143.08	1.8	-228.70	1.8	-215.78	2.12	-43.06	23.00
40	141	50.00	-2212.49	507.79	-1749.30	0	-2855.46	1.8	210.52	1.8	-80.16	2.12	196.75	22.94
41	1141	50.00	-2212.71	-507.72	-1749.31	0	-2855.53	1.8	210.46	1.8	-80.22	2.12	196.69	18.28
41	142	51.40	-2212.71	-435.21	-1091.73	0	-2143.24	1.8	-228.74	1.8	-215.81	2.12	-43.07	18.21
42	142	51.40	-2213.30	-433.48	-1091.81	0	-2143.50	1.8	-228.90	1.8	-215.95	2.12	-43.20	10.62
42	143	52.80	-2213.30	-338.13	-545.77	0	-1552.74	1.8	-591.29	1.8	-328.84	2.12	-242.80	10.54
43	143	52.80	-2518.88	-337.29	-735.37	0	-2098.28	1.8	-395.06	1.8	-329.07	2.12	-243.00	0.30
43	144	54.20	-2523.70	-261.37	-320.99	0	-1646.97	1.8	-686.14	1.8	-414.21	2.12	-392.56	
44	144	54.20	-1696.97	-261.09	-719.30	0	-1777.79	1.8	-315.39	1.8	-92.20	2.12	6.89	
44	145	55.60	-1696.97	-196.93	-402.79	0	-1430.25	1.8	-542.12	1.8	-155.56	2.12	-105.14	
45	145	55.60	-2088.58	-196.62	-634.93	0	-2112.68	1.8	-316.71	1.8	-155.48	2.12	-105.00	
45	146	57.00	-2088.58	-124.14	-419.44	0	-1873.45	1.8	-479.62	1.8	-197.55	2.12	-179.39	
46	146	57.00	-1249.32	-120.27	-817.02	0	-2042.63	1.8	178.63	1.8	56.92	2.12	112.17	
46	147	58.40	-1251.27	-95.84	-661.70	0	-1862.68	1.8	1.68	1.8	42.26	2.12	83.28	
47	147	58.40	-1608.20	-98.38	-860.74	0	-2446.17	1.8	156.70	1.8	42.60	2.12	81.91	
47	148	59.80	-1608.20	-75.56	-739.06	0	-2310.86	1.8	24.74	1.8	30.57	2.12	58.78	
48	148	59.80	-1608.20	-74.94	-738.99	0	-2310.80	1.8	24.73	1.8	30.56	2.12	58.75	
48	149	61.20	-1608.20	-52.27	-649.94	0	-2214.12	1.8	-64.77	1.8	21.19	2.12	40.74	
49	149	61.20	-1608.20	-51.65	-649.94	0	-2214.11	1.8	-64.77	1.8	21.19	2.12	40.74	
49	150	62.60	-1608.20	-29.00	-593.48	0	-2156.00	1.8	-111.84	1.8	14.48	2.12	27.84	
50	150	62.60	-1608.20	-28.41	-593.47	0	-2156.00	1.8	-111.84	1.8	14.48	2.12	27.84	
50	151	64.00	-1609.94	-5.70	-569.64	0	-2137.97	1.8	-117.81	1.8	10.43	2.12	20.06	
51	151	64.00	-1609.94	-5.10	-569.64	0	-2137.97	1.8	-117.81	1.8	10.43	2.12	20.06	
51	152	65.40	-1609.94	23.10	-581.57	0	-2159.71	1.8	-79.24	1.8	9.58	2.12	18.41	
52	152	65.40	-1609.94	23.68	-581.52	0	-2159.67	1.8	-79.25	1.8	9.57	2.12	18.40	
52	153	66.80	-1609.94	47.77	-631.51	0	-2224.48	1.8	2.82	1.8	12.30	2.12	23.65	
53	153	66.80	-1609.94	48.35	-631.55	0	-2224.51	1.8	2.83	1.8	12.30	2.12	23.66	
53	154	68.20	-1609.94	70.98	-715.15	0	-2328.77	1.8	127.63	1.8	17.86	2.12	34.34	
54	154	68.20	-1609.94	71.61	-715.20	0	-2328.81	1.8	127.64	1.8	17.87	2.12	34.36	
54	155	69.60	-1609.94	94.43	-831.34	0	-2471.59	1.8	294.80	1.8	26.08	2.12	50.15	
55	155	69.60	-1246.39	91.04	-632.30	0	-1877.86	1.8	145.37	1.8	25.88	2.12	50.99	
55	156	71.00	-1242.90	114.75	-782.21	0	-2063.09	1.8	359.18	1.8	36.74	2.12	72.40	
56	156	71.00	-2088.58	120.17	-384.66	0	-1834.67	1.8	-506.44	1.8	-204.28	2.12	-191.28	
56	157	72.40	-2088.58	203.01	-595.91	0	-2068.78	1.8	-348.10	1.8	-162.86	2.12	-118.06	
57	157	72.40	-1696.97	203.14	-363.61	0	-1386.20	1.8	-573.56	1.8	-162.98	2.12	-118.26	
57	158	73.80	-1696.97	270.83	-693.02	0	-1745.20	1.8	-346.40	1.8	-95.95	2.12	0.27	
58	158	73.80	-2523.70	271.35	-294.79	0	-1614.46	1.8	-717.12	1.8	-417.93	2.12	-399.14	
58	159	75.20	-2523.70	368.91	-730.41	0	-2086.79	1.8	-424.67	1.8	-328.29	2.12	-240.63	
59	159	75.20	-2219.11	370.81	-540.95	0	-1541.69	1.8	-621.17	1.8	-328.29	2.12	-240.64	
59	160	76.60	-2215.29	445.94	-1111.68	0	-2154.15	1.8	-253.74	1.8	-207.72	2.12	-28.23	
60	160	76.60	-2215.34	447.67	-1111.67	0	-2154.15	1.8	-253.76	1.8	-207.73	2.12	-28.25	
60	161	78.00	-2215.34	516.61	-1782.16	0	-2877.91	1.8	185.87	1.8	-68.45	2.12	218.03	
61	1161	78.00	-2172.15	-492.57	-1753.40	0	-2797.42	1.8	153.66	1.8	-68.52	2.12	217.97	
61	162	79.10	-2172.15	-435.79	-1247.09	0	-2258.04	1.8	-154.97	1.8	-176.61	2.12	26.85	
62	162	79.10	-2172.53	-434.48	-1247.19	0	-2258.25	1.8	-155.05	1.8	-176.69	2.12	26.80	
62	163	80.20	-2172.53	-351.24	-805.85	0	-1790.13	1.8	-417.41	1.8	-271.73	2.12	-141.26	
63	163	80.20	-2477.65	-350.29	-998.59	0	-2340.45	1.8	-213.94	1.8	-271.81	2.12	-141.30	
63	164	81.30	-2477.65	-284.45	-651.04	0	-1969.63	1.8	-427.68	1.8	-345.77	2.12	-272.07	
64	164	81.30	-2478.35	-284.02	-651.33	0	-1970.12	1.8	-427.81	1.8	-345.88	2.12	-272.13	
64	165	82.40	-2478.35	-226.58	-369.06	0	-1668.96	1.8	-601.34	1.8	-405.96	2.12	-378.35	
65	165	82.40	-1870.06	-226.30	-899.74	0	-2185.19	1.8	-95.79	1.8	-84.39	2.12	20.51	
65	166	83.50	-1870.06	-196.87	-669.49	0	-1940.89	1.8	-232.92	1.8	-133.94	2.12	-67.11	
66	166	83.50	-1871.02	-196.43	-669.26	0	-1904.41	1.8	-268.95	1.8	-165.23	2.12	-109.60	
66	167	84.60	-1871.02	-151.44	-487.34	0	-1730.17	1.8	-354.42	1.8	-190.95	2.12	-160.89	
67	167	84.60	-1016.26	-142.17	-884.92	0	-1927.40	1.8	425.63	1.8	64.64	2.12	127.37	
67	168	85.70	-1019.75	-124.10	-729.47	0	-1750.80	1.8	249.95	1.8	49.75	2.12	98.03	
68	168	85.70	-1261.85	-131.44	-860.39	0	-2131.64	1.8	343.36	1.8	50.15	2.12	96.43	
68	169	86.80	-1261.85	-113.60	-725.62	0	-1982.02	1.8	197.94	1.8	36.77	2.12	70.70	
69	169	86.80	-1261.85	-113.24	-725.59	0	-1981.99	1.8	197.93	1.8	36.76	2.12	70.69	
69	170	87.90	-1261.85	-95.46	-610.78	0	-1856.04	1.8	78.64	1.8	25.00	2.12	48.06	
70	170	87.90	-1261.85	-95.13	-610.79	0	-1856.05	1.8	78.64	1.8	25.00	2.12	48.06	
70	171	89.00	-1261.85	-77.34	-515.91	0	-1753.78	1.8	-14.45	1.8	14.84	2.12	28.53	

11/09/03

Programa DINTEL PACADAR S.A.
INFRECUENTEST.T0.MZ-

GRÁFICO DE TENSIONES



Combi_to.xls

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ+

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-472.42	-155.80	-178.17	0	-661.96	1.8	37.49	1.8	-0.12	2.12	-0.24
1	2	1.10	-476.85	-244.94	108.74	0	-365.67	1.8	-174.43	1.8	-36.29	2.12	-71.52
2	2	1.10	-752.42	-245.25	-65.29	0	-863.10	1.8	9.72	1.8	-36.32	2.12	-71.56
2	3	2.20	-752.42	-212.59	183.89	0	-604.19	1.8	-166.87	1.8	-68.08	2.12	-134.15
3	3	2.20	-752.42	-212.84	184.00	0	-604.09	1.8	-166.90	1.8	-68.10	2.12	-134.18
3	4	3.30	-752.42	-180.22	395.93	0	-384.94	1.8	-314.02	1.8	-95.35	2.12	-187.89
4	4	3.30	-949.26	-180.38	275.60	0	-733.95	1.8	-191.63	1.8	-95.38	2.12	-187.94
4	5	4.40	-949.26	-142.84	450.11	0	-554.70	1.8	-309.23	1.8	-118.10	2.12	-232.71
5	5	4.40	-949.26	-142.94	450.23	0	-554.59	1.8	-309.26	1.8	-118.12	2.12	-232.75
5	6	5.50	-949.26	-108.63	593.30	0	-410.07	1.8	-398.56	1.8	-137.31	2.12	-270.57
6	6	5.50	-1146.10	-108.72	474.88	0	-756.00	1.8	-280.75	1.8	-137.32	2.12	-270.59
6	7	6.60	-1146.10	-76.00	580.86	0	-651.06	1.8	-340.67	1.8	-152.03	2.12	-299.57
7	7	6.60	-1146.10	-76.08	580.94	0	-688.07	1.8	-358.13	1.8	-153.30	2.12	-294.77
7	8	7.70	-1146.10	-43.42	649.76	0	-626.10	1.8	-388.72	1.8	-163.60	2.12	-314.58
8	8	7.70	-1146.10	-43.41	649.82	0	-626.05	1.8	-388.73	1.8	-163.61	2.12	-314.60
8	9	8.80	-1146.10	-11.01	680.57	0	-602.60	1.8	-389.59	1.8	-169.23	2.12	-325.41
9	9	8.80	-1146.10	-10.95	680.62	0	-602.56	1.8	-389.60	1.8	-169.24	2.12	-325.43
9	10	9.90	-1146.10	21.62	679.64	0	-612.43	1.8	-361.98	1.8	-171.25	2.12	-329.30
10	10	9.90	-1146.10	21.71	679.65	0	-612.42	1.8	-361.99	1.8	-171.26	2.12	-329.30
10	11	11.00	-1146.10	54.46	641.83	0	-659.79	1.8	-304.92	1.8	-168.79	2.12	-324.56
11	11	11.00	-1146.10	54.51	641.85	0	-659.77	1.8	-304.93	1.8	-168.79	2.12	-324.57
11	12	12.10	-1146.10	87.20	566.98	0	-744.82	1.8	-218.32	1.8	-161.82	2.12	-311.16
12	12	12.10	-1146.10	87.31	566.96	0	-744.84	1.8	-218.32	1.8	-161.82	2.12	-311.15
12	13	13.20	-1146.10	119.74	454.49	0	-868.02	1.8	-102.06	1.8	-150.24	2.12	-288.90
13	13	13.20	-1146.10	119.83	454.46	0	-868.05	1.8	-102.05	1.8	-150.24	2.12	-288.88
13	14	14.30	-1146.10	152.58	308.67	0	-1025.83	1.8	42.91	1.8	-134.78	2.12	-259.16
14	14	14.30	-924.56	147.69	427.10	0	-629.71	1.8	-37.73	1.8	-133.66	2.12	-263.38
14	15	15.40	-917.39	177.87	242.93	0	-828.24	1.8	147.01	1.8	-113.98	2.12	-224.60
15	15	15.40	-1858.58	186.55	682.39	0	-633.43	1.8	-627.53	1.8	-396.68	2.12	-548.00
15	16	16.50	-1858.58	186.80	467.50	0	-836.06	1.8	-535.87	1.8	-365.59	2.12	-486.00
16	16	16.50	-1858.58	186.67	467.31	0	-757.14	1.8	-613.00	1.8	-432.58	2.12	-577.09
16	17	17.60	-1858.58	202.30	249.96	0	-989.20	1.8	-478.84	1.8	-386.39	2.12	-495.42
17	17	17.60	-2575.51	202.31	810.05	0	-495.83	1.8	-1011.64	1.8	-742.04	2.12	-936.46
17	18	18.70	-2575.51	199.90	581.61	0	-744.88	1.8	-853.81	1.8	-695.59	2.12	-854.33
18	18	18.70	-2575.50	199.91	581.15	0	-745.33	1.8	-853.67	1.8	-695.47	2.12	-854.12
18	19	19.80	-2575.50	201.87	358.90	0	-994.89	1.8	-676.44	1.8	-653.23	2.12	-779.42
19	19	19.80	-2299.92	201.82	532.49	0	-497.90	1.8	-860.45	1.8	-653.08	2.12	-779.16
19	20	20.90	-2299.92	203.82	309.12	0	-755.06	1.8	-661.61	1.8	-613.20	2.12	-708.65
20	20	20.90	-2299.92	203.44	309.15	0	-755.04	1.8	-661.62	1.8	-613.21	2.12	-708.66
20	21	22.00	-2299.92	212.80	79.76	0	-1026.40	1.8	-433.70	1.8	-575.21	2.12	-641.48
21	1021	22.00	-2339.29	-216.81	53.69	0	-1099.38	1.8	-404.62	1.8	-575.21	2.12	-641.48
21	22	23.40	-2339.29	-196.04	347.08	0	-740.58	1.8	-734.36	1.8	-619.05	2.12	-718.99
22	22	23.40	-2339.29	-196.46	347.01	0	-740.65	1.8	-734.34	1.8	-619.03	2.12	-718.96
22	23	24.80	-2339.29	-191.06	619.63	0	-415.52	1.8	-1013.72	1.8	-663.13	2.12	-796.94
23	23	24.80	-2614.86	-191.55	448.23	0	-908.69	1.8	-835.94	1.8	-663.13	2.12	-796.94
23	24	26.20	-2614.86	-212.58	727.19	0	-587.99	1.8	-1082.74	1.8	-713.13	2.12	-885.34
24	24	26.20	-1701.11	-213.31	288.40	0	-731.17	1.8	-673.39	1.8	-357.59	2.12	-444.49
24	25	27.60	-1701.11	-203.83	577.39	0	-411.29	1.8	-888.77	1.8	-414.40	2.12	-544.94
25	25	27.60	-2055.42	-203.87	368.31	0	-1027.80	1.8	-685.10	1.8	-414.57	2.12	-545.24
25	26	29.00	-2055.42	-215.11	677.81	0	-698.61	1.8	-872.07	1.8	-480.85	2.12	-662.44
26	26	29.00	-1122.96	-210.13	238.50	0	-1028.91	1.8	86.41	1.8	-121.36	2.12	-239.14
26	27	30.40	-1129.71	-172.52	508.05	0	-743.44	1.8	-152.02	1.8	-152.44	2.12	-300.37
27	27	30.40	-1460.38	-174.49	328.06	0	-1331.55	1.8	-20.13	1.8	-153.72	2.12	-295.58
27	28	31.80	-1460.38	-132.12	538.32	0	-1112.16	1.8	-204.49	1.8	-177.98	2.12	-342.23
28	28	31.80	-1460.38	-131.93	538.44	0	-1112.07	1.8	-204.51	1.8	-178.00	2.12	-342.27
28	29	33.20	-1460.38	-85.79	690.44	0	-952.25	1.8	-341.47	1.8	-195.24	2.12	-375.43
29	29	33.20	-1460.38	-85.57	690.56	0	-952.16	1.8	-341.49	1.8	-195.26	2.12	-375.46
29	30	34.60	-1460.38	-49.19	785.62	0	-850.86	1.8	-431.20	1.8	-205.73	2.12	-395.58
30	30	34.60	-1460.38	-48.96	785.67	0	-850.82	1.8	-431.21	1.8	-205.74	2.12	-395.60
30	31	36.00	-1460.38	-7.09	820.06	0	-811.10	1.8	-472.99	1.8	-208.78	2.12	-401.45
31	31	36.00	-1460.38	-6.90	820.07	0	-811.09	1.8	-472.99	1.8	-208.78	2.12	-401.46
31	32	37.40	-1460.38	39.64	798.81	0	-828.82	1.8	-467.82	1.8	-205.26	2.12	-394.68
32	32	37.40	-1460.38	39.86	798.78	0	-828.84	1.8	-467.81	1.8	-205.25	2.12	-394.67
32	33	38.80	-1460.38	76.23	716.75	0	-908.22	1.8	-414.67	1.8	-194.30	2.12	-373.61
33	33	38.80	-1460.38	76.45	716.66	0	-908.30	1.8	-414.65	1.8	-194.28	2.12	-373.58
33	34	40.20	-1460.38	122.64	577.80	0	-1046.10	1.8	-314.31	1.8	-176.56	2.12	-339.50
34	34	40.20	-1460.38	122.82	577.68	0	-1046.20	1.8	-314.28	1.8	-176.54	2.12	-339.46
34	35	41.60	-1460.38	165.20	380.40	0	-1243.73	1.8	-166.44	1.8	-151.78	2.12	-291.86
35	35	41.60	-1135.74	164.77	560.36	0	-661.53	1.8	-303.30	1.8	-150.51	2.12	-296.58
35	36	43.00	-1128.92	202.82	302.51	0	-927.17	1.8	-98.73	1.8	-118.91	2.12	-234.31
36	36	43.00	-2055.42	206.26	741.84	0	-641.75	1.8	-874.04	1.8	-499.13	2.12	-694.77
36	37	44.40	-2055.42	201.31	447.21	0	-957.58	1.8	-688.08	1.8	-437.03	2.12	-584.96
37	37	44.40	-1701.11	201.35	656.36	0	-340.99	1.8	-891.77	1.8	-436.88	2.12	-584.69
37	38	45.80	-1701.11	213.71	366.54	0	-662.71	1.8	-672.81	1.8	-380.28	2.12	-484.60
38	38	45.80	-2614.86	213.41	805.22	0	-519.62	1.8	-1082.13	1.8	-735.78	2.12	-925.40

Combi_to.xls

Programa DINTEL PACADAR S.A.
INFRECUENTESG.T0.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ+

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-944.83	108.54	592.89	0	-407.18	1.8	-394.03	1.8	-137.31	2.12	-270.57
76	77	95.60	-944.83	142.85	449.92	0	-551.56	1.8	-304.94	1.8	-118.12	2.12	-232.76
77	77	95.60	-944.83	142.73	449.81	0	-551.65	1.8	-304.92	1.8	-118.11	2.12	-232.73
77	78	96.70	-944.83	180.28	275.33	0	-730.84	1.8	-187.46	1.8	-95.37	2.12	-187.93
78	78	96.70	-747.99	180.12	395.68	0	-381.80	1.8	-309.86	1.8	-95.36	2.12	-187.90
78	79	97.80	-747.99	212.74	183.80	0	-600.85	1.8	-162.92	1.8	-68.09	2.12	-134.18
79	79	97.80	-747.99	212.49	183.70	0	-600.94	1.8	-162.90	1.8	-68.08	2.12	-134.14
79	80	98.90	-747.99	245.15	-65.37	0	-859.70	1.8	13.47	1.8	-36.32	2.12	-71.56
80	80	98.90	-472.42	244.84	108.65	0	-362.26	1.8	-170.68	1.8	-36.29	2.12	-71.52
80	81	100.00	-472.42	155.78	-178.17	0	-661.96	1.8	37.49	1.8	-0.12	2.12	-0.24
101	101	0.00	-472.42	-169.94	-178.23	0	-662.02	1.8	37.50	1.8	-0.11	2.12	-0.22
101	102	1.10	-476.85	-259.94	125.46	0	-351.24	1.8	-177.66	1.8	-39.10	2.12	-77.05
102	102	1.10	-752.42	-259.06	-49.01	0	-849.05	1.8	6.57	1.8	-39.05	2.12	-76.95
102	103	2.20	-752.42	-225.23	214.05	0	-578.16	1.8	-172.71	1.8	-73.15	2.12	-144.14
103	103	2.20	-752.42	-224.48	213.77	0	-578.40	1.8	-172.66	1.8	-73.10	2.12	-144.04
103	104	3.30	-752.42	-190.72	436.86	0	-349.60	1.8	-321.94	1.8	-102.23	2.12	-201.45
104	104	3.30	-949.26	-190.05	316.13	0	-698.97	1.8	-199.48	1.8	-102.19	2.12	-201.36
104	105	4.40	-949.26	-156.21	499.85	0	-511.75	1.8	-318.88	1.8	-126.46	2.12	-249.19
105	105	4.40	-949.26	-155.69	499.59	0	-511.98	1.8	-318.83	1.8	-126.42	2.12	-249.10
105	106	5.50	-949.26	-114.04	650.28	0	-360.88	1.8	-409.61	1.8	-146.89	2.12	-289.44
106	106	5.50	-1146.10	-113.67	531.58	0	-707.05	1.8	-291.74	1.8	-146.85	2.12	-289.37
106	107	6.60	-1146.10	-79.81	643.15	0	-597.30	1.8	-352.73	1.8	-162.50	2.12	-320.21
107	107	6.60	-1146.10	-79.48	643.00	0	-637.31	1.8	-370.24	1.8	-163.82	2.12	-315.00
107	108	7.70	-1146.10	-45.70	715.44	0	-572.38	1.8	-401.54	1.8	-174.74	2.12	-335.99
108	108	7.70	-1146.10	-45.43	715.35	0	-572.45	1.8	-401.52	1.8	-174.72	2.12	-335.96
108	109	8.80	-1146.10	-11.65	748.69	0	-546.88	1.8	-402.89	1.8	-180.78	2.12	-347.62
109	109	8.80	-1146.10	-11.46	748.66	0	-546.90	1.8	-402.88	1.8	-180.78	2.12	-347.61
109	110	9.90	-1146.10	22.34	748.10	0	-556.43	1.8	-375.35	1.8	-182.86	2.12	-351.61
110	110	9.90	-1146.10	22.52	748.06	0	-556.47	1.8	-375.34	1.8	-182.85	2.12	-351.60
110	111	11.00	-1146.10	56.39	709.48	0	-604.45	1.8	-318.13	1.8	-180.26	2.12	-346.61
111	111	11.00	-1146.10	56.54	709.50	0	-604.44	1.8	-318.13	1.8	-180.26	2.12	-346.62
111	112	12.10	-1146.10	90.36	632.29	0	-691.40	1.8	-231.07	1.8	-172.89	2.12	-332.44
112	112	12.10	-1146.10	90.52	632.35	0	-691.35	1.8	-231.08	1.8	-172.90	2.12	-332.46
112	113	13.20	-1146.10	124.21	516.54	0	-817.26	1.8	-114.19	1.8	-160.76	2.12	-309.12
113	113	13.20	-1146.10	124.34	516.61	0	-817.20	1.8	-114.20	1.8	-160.77	2.12	-309.14
113	114	14.30	-1146.10	158.18	365.76	0	-979.13	1.8	31.77	1.8	-144.46	2.12	-277.77
114	114	14.30	-924.56	153.37	484.39	0	-580.26	1.8	-48.82	1.8	-143.30	2.12	-282.36
114	115	15.40	-917.39	184.59	294.10	0	-784.08	1.8	137.10	1.8	-122.58	2.12	-241.55
115	115	15.40	-1858.58	193.33	733.78	0	-589.16	1.8	-637.17	1.8	-405.05	2.12	-564.70
115	116	16.50	-1858.58	199.92	511.56	0	-798.11	1.8	-544.13	1.8	-372.77	2.12	-500.31
116	116	16.50	-1858.58	200.33	511.77	0	-714.10	1.8	-625.96	1.8	-443.84	2.12	-596.99
116	117	17.60	-1858.58	216.75	279.19	0	-960.91	1.8	-487.36	1.8	-393.79	2.12	-508.50
117	117	17.60	-2575.50	217.14	839.69	0	-467.14	1.8	-1020.28	1.8	-749.54	2.12	-949.73
117	118	18.70	-2575.50	204.70	600.44	0	-726.66	1.8	-859.29	1.8	-700.35	2.12	-862.75
118	118	18.70	-2575.50	204.94	600.22	0	-726.87	1.8	-859.23	1.8	-700.30	2.12	-862.65
118	119	19.80	-2575.50	197.79	377.53	0	-976.87	1.8	-681.86	1.8	-657.94	2.12	-787.76
119	119	19.80	-2299.92	197.64	551.47	0	-479.53	1.8	-865.98	1.8	-657.88	2.12	-787.66
119	120	20.90	-2299.92	191.75	337.06	0	-728.02	1.8	-669.75	1.8	-620.27	2.12	-721.16
120	120	20.90	-2299.92	191.30	337.06	0	-728.03	1.8	-669.75	1.8	-620.27	2.12	-721.16
120	121	22.00	-2299.92	205.30	116.05	0	-991.29	1.8	-444.27	1.8	-584.40	2.12	-657.72
121	1121	22.00	-2339.29	-209.86	89.99	0	-1064.25	1.8	-415.20	1.8	-584.40	2.12	-657.72
121	122	23.40	-2339.29	-192.23	374.52	0	-714.03	1.8	-742.35	1.8	-625.99	2.12	-731.27
122	122	23.40	-2339.29	-192.78	374.55	0	-713.99	1.8	-742.36	1.8	-626.00	2.12	-731.29
122	123	24.80	-2339.29	-188.92	643.86	0	-392.08	1.8	-1020.78	1.8	-669.27	2.12	-807.79
123	123	24.80	-2614.86	-189.70	472.33	0	-885.37	1.8	-842.97	1.8	-669.23	2.12	-807.73
123	124	26.20	-2614.86	-220.05	751.77	0	-564.20	1.8	-1089.91	1.8	-719.35	2.12	-896.34
124	124	26.20	-1701.11	-219.77	312.57	0	-707.78	1.8	-680.44	1.8	-363.71	2.12	-455.31
124	125	27.60	-1701.11	-212.57	612.79	0	-377.03	1.8	-899.09	1.8	-423.36	2.12	-560.78
125	125	27.60	-2055.42	-212.05	403.23	0	-994.01	1.8	-695.28	1.8	-423.41	2.12	-560.87
125	126	29.00	-2055.42	-222.36	718.26	0	-659.45	1.8	-883.86	1.8	-491.09	2.12	-680.54
126	126	29.00	-1122.96	-217.45	278.57	0	-994.33	1.8	78.68	1.8	-128.10	2.12	-252.42
126	127	30.40	-1129.71	-178.05	556.28	0	-701.81	1.8	-161.35	1.8	-160.54	2.12	-316.35
127	127	30.40	-1460.38	-180.15	375.95	0	-1292.37	1.8	-29.48	1.8	-161.84	2.12	-311.19
127	128	31.80	-1460.38	-136.19	592.16	0	-1068.13	1.8	-214.99	1.8	-187.11	2.12	-359.78
128	128	31.80	-1460.38	-136.23	592.01	0	-1068.25	1.8	-214.97	1.8	-187.08	2.12	-359.73
128	129	33.20	-1460.38	-87.66	748.30	0	-904.92	1.8	-352.78	1.8	-205.05	2.12	-394.28
129	129	33.20	-1460.38	-87.78	748.19	0	-905.01	1.8	-352.76	1.8	-205.03	2.12	-394.25
129	130	34.60	-1460.38	-51.00	846.21	0	-801.30	1.8	-443.03	1.8	-216.00	2.12	-415.33
130	130	34.60	-1460.38	-51.13	846.17	0	-801.33	1.8	-443.02	1.8	-215.99	2.12	-415.32
130	131	36.00	-1460.38	-7.60	881.31	0	-760.99	1.8	-484.97	1.8	-219.16	2.12	-421.42
131	131	36.00	-1460.38	-7.73	881.29	0	-761.00	1.8	-484.96	1.8	-219.16	2.12	-421.41
131	132	37.40	-1460.38	41.44	859.77	0	-778.96	1.8	-479.70	1.8	-215.60	2.12	-414.56
132	132	37.40	-1460.38	41.30	859.80	0	-778.93	1.8	-479.70	1.8	-215.60	2.12	-414.57
132	133	38.80	-1460.38	78.05	775.30	0	-860.34	1.8	-426.08	1.8	-204.22	2.12	-392.69
133	133	38.80	-1460.38	77.94	775.41	0	-860.24	1.8	-426.10	1.8	-204.24	2.12	-392.73

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ+
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1460.38	126.52	632.89	0	-1001.04	1.8	-325.06	1.8	-185.90	2.12	-357.46
134	134	40.20	-1460.38	126.46	633.03	0	-1000.93	1.8	-325.08	1.8	-185.92	2.12	-357.50
134	135	41.60	-1460.38	170.36	430.39	0	-1202.83	1.8	-176.20	1.8	-160.26	2.12	-308.15
135	135	41.60	-1135.74	169.82	610.72	0	-618.06	1.8	-313.05	1.8	-158.98	2.12	-313.26
135	136	43.00	-1128.92	209.49	345.51	0	-890.05	1.8	-107.06	1.8	-126.14	2.12	-248.56
136	136	43.00	-2055.42	212.80	785.22	0	-599.77	1.8	-886.68	1.8	-510.11	2.12	-714.18
136	137	44.40	-2055.42	210.63	483.97	0	-922.00	1.8	-698.79	1.8	-446.34	2.12	-601.41
137	137	44.40	-1701.11	211.07	693.62	0	-304.94	1.8	-902.62	1.8	-446.31	2.12	-601.36
137	138	45.80	-1701.11	220.91	392.31	0	-637.76	1.8	-680.32	1.8	-386.80	2.12	-496.14
138	138	45.80	-2614.86	221.44	831.44	0	-494.25	1.8	-1089.77	1.8	-742.42	2.12	-937.13
138	139	47.20	-2614.86	196.90	543.79	0	-824.38	1.8	-837.11	1.8	-690.64	2.12	-845.59
139	139	47.20	-2339.29	197.03	715.07	0	-331.34	1.8	-1014.85	1.8	-690.61	2.12	-845.53
139	140	48.60	-2345.74	194.02	441.79	0	-660.10	1.8	-733.93	1.8	-648.49	2.12	-769.72
140	140	48.60	-2345.92	193.43	441.84	0	-660.11	1.8	-734.00	1.8	-648.55	2.12	-769.79
140	141	50.00	-2345.92	210.11	155.39	0	-1013.22	1.8	-402.95	1.8	-606.88	2.12	-696.11
141	1141	50.00	-2345.71	-210.20	155.39	0	-1013.15	1.8	-402.89	1.8	-606.83	2.12	-696.06
141	142	51.40	-2345.71	-193.52	441.96	0	-659.94	1.8	-733.97	1.8	-648.52	2.12	-769.78
142	142	51.40	-2345.10	-194.10	441.91	0	-659.79	1.8	-733.77	1.8	-648.35	2.12	-769.60
142	143	52.80	-2345.10	-196.61	715.22	0	-332.98	1.8	-1016.68	1.8	-692.20	2.12	-847.15
143	143	52.80	-2619.68	-196.54	543.84	0	-825.81	1.8	-838.61	1.8	-691.95	2.12	-846.90
143	144	54.20	-2614.86	-221.44	831.44	0	-494.25	1.8	-1089.77	1.8	-742.42	2.12	-937.13
144	144	54.20	-1701.11	-220.93	392.32	0	-637.76	1.8	-680.32	1.8	-386.80	2.12	-496.14
144	145	55.60	-1701.11	-211.08	693.64	0	-304.91	1.8	-902.63	1.8	-446.32	2.12	-601.37
145	145	55.60	-2055.42	-210.65	483.99	0	-921.99	1.8	-698.79	1.8	-446.34	2.12	-601.42
145	146	57.00	-2055.42	-212.80	785.27	0	-599.72	1.8	-886.70	1.8	-510.13	2.12	-714.20
146	146	57.00	-1128.92	-209.51	345.56	0	-890.00	1.8	-107.07	1.8	-126.15	2.12	-248.58
146	147	58.40	-1133.95	-168.94	609.89	0	-617.91	1.8	-309.53	1.8	-158.98	2.12	-313.28
147	147	58.40	-1458.36	-170.45	429.54	0	-1202.52	1.8	-172.50	1.8	-160.26	2.12	-308.17
147	148	59.80	-1458.36	-126.54	632.25	0	-1000.50	1.8	-321.55	1.8	-185.93	2.12	-357.52
148	148	59.80	-1458.36	-126.59	632.12	0	-1000.60	1.8	-321.52	1.8	-185.91	2.12	-357.48
148	149	61.20	-1458.36	-78.00	774.71	0	-859.70	1.8	-422.75	1.8	-204.25	2.12	-392.74
149	149	61.20	-1458.36	-78.11	774.61	0	-859.78	1.8	-422.73	1.8	-204.23	2.12	-392.71
149	150	62.60	-1458.36	-41.35	859.23	0	-778.22	1.8	-476.57	1.8	-215.61	2.12	-414.59
150	150	62.60	-1458.36	-41.50	859.19	0	-778.25	1.8	-476.56	1.8	-215.61	2.12	-414.58
150	151	64.00	-1456.62	7.65	880.78	0	-758.76	1.8	-480.57	1.8	-219.17	2.12	-421.43
151	151	64.00	-1456.62	7.52	880.79	0	-758.75	1.8	-480.57	1.8	-219.17	2.12	-421.43
151	152	65.40	-1456.62	51.05	845.75	0	-798.93	1.8	-438.90	1.8	-216.00	2.12	-415.33
152	152	65.40	-1456.62	50.91	845.80	0	-798.89	1.8	-438.91	1.8	-216.01	2.12	-415.35
152	153	66.80	-1456.62	87.68	747.91	0	-902.41	1.8	-348.91	1.8	-205.04	2.12	-394.27
153	153	66.80	-1456.62	87.59	748.02	0	-902.32	1.8	-348.93	1.8	-205.06	2.12	-394.30
153	154	68.20	-1456.62	136.15	591.83	0	-1065.49	1.8	-211.37	1.8	-187.09	2.12	-359.75
154	154	68.20	-1456.62	136.11	591.96	0	-1065.39	1.8	-211.39	1.8	-187.11	2.12	-359.79
154	155	69.60	-1456.62	180.06	375.87	0	-1289.45	1.8	-26.14	1.8	-161.85	2.12	-311.21
155	155	69.60	-1126.45	176.17	556.22	0	-699.29	1.8	-158.43	1.8	-160.55	2.12	-316.37
155	156	71.00	-1122.96	217.45	278.60	0	-994.32	1.8	78.69	1.8	-128.11	2.12	-252.43
156	156	71.00	-2055.42	222.38	718.30	0	-659.42	1.8	-883.87	1.8	-491.10	2.12	-680.56
156	157	72.40	-2055.42	212.06	403.25	0	-993.99	1.8	-695.28	1.8	-423.41	2.12	-560.88
157	157	72.40	-1701.11	212.58	612.81	0	-377.01	1.8	-899.09	1.8	-423.37	2.12	-560.79
157	158	73.80	-1701.11	219.78	312.56	0	-707.79	1.8	-680.43	1.8	-363.71	2.12	-455.31
158	158	73.80	-2614.86	220.05	751.75	0	-564.21	1.8	-1089.90	1.8	-719.34	2.12	-896.33
158	159	75.20	-2614.86	189.70	472.32	0	-885.38	1.8	-842.96	1.8	-669.23	2.12	-807.72
159	159	75.20	-2339.29	188.91	643.87	0	-392.07	1.8	-1020.78	1.8	-669.27	2.12	-807.79
159	160	76.60	-2343.12	192.32	375.06	0	-714.68	1.8	-743.69	1.8	-627.16	2.12	-732.54
160	160	76.60	-2343.06	191.74	375.11	0	-714.62	1.8	-743.69	1.8	-627.15	2.12	-732.55
160	161	78.00	-2343.06	209.37	91.29	0	-1064.15	1.8	-416.74	1.8	-585.74	2.12	-659.31
161	1161	78.00	-2303.37	-205.15	117.36	0	-991.08	1.8	-445.71	1.8	-585.65	2.12	-659.23
161	162	79.10	-2303.37	-191.15	338.21	0	-727.98	1.8	-671.15	1.8	-621.49	2.12	-722.59
162	162	79.10	-2302.99	-191.59	338.18	0	-727.88	1.8	-671.03	1.8	-621.38	2.12	-722.48
162	163	80.20	-2302.99	-197.50	552.44	0	-479.53	1.8	-867.21	1.8	-658.95	2.12	-788.92
163	163	80.20	-2578.03	-197.64	378.47	0	-976.74	1.8	-682.92	1.8	-658.86	2.12	-788.86
163	164	81.30	-2578.03	-204.78	601.01	0	-726.89	1.8	-860.24	1.8	-701.18	2.12	-863.69
164	164	81.30	-2577.33	-204.55	601.16	0	-726.53	1.8	-860.06	1.8	-701.03	2.12	-863.57
164	165	82.40	-2577.33	-216.99	840.26	0	-467.15	1.8	-1021.01	1.8	-750.17	2.12	-950.47
165	165	82.40	-1859.54	-216.66	280.08	0	-960.10	1.8	-488.70	1.8	-394.17	2.12	-508.98
165	166	83.50	-1859.54	-200.24	512.16	0	-714.03	1.8	-626.37	1.8	-444.19	2.12	-597.42
166	166	83.50	-1858.58	-199.91	511.85	0	-797.86	1.8	-544.19	1.8	-372.82	2.12	-500.41
166	167	84.60	-1858.58	-193.34	734.04	0	-588.93	1.8	-637.22	1.8	-405.10	2.12	-564.79
167	167	84.60	-917.40	-184.57	294.37	0	-783.70	1.8	136.53	1.8	-122.59	2.12	-241.56
167	168	85.70	-920.89	-150.89	483.30	0	-578.94	1.8	-43.21	1.8	-143.30	2.12	-282.37
168	168	85.70	-1141.67	-158.26	364.66	0	-977.21	1.8	37.99	1.8	-144.46	2.12	-277.77
168	169	86.80	-1141.67	-124.42	515.62	0	-815.13	1.8	-108.19	1.8	-160.78	2.12	-309.16
169	169	86.80	-1141.67	-124.30	515.51	0	-815.22	1.8	-108.17	1.8	-160.76	2.12	-309.12
169	170	87.90	-1141.67	-90.61	631.43	0	-689.16	1.8	-225.26	1.8	-172.91	2.12	-332.47
170	170	87.90	-1141.67	-90.45	631.37	0	-689.21	1.8	-225.25	1.8	-172.90	2.12	-332.45
170	171	89.00	-1141.67	-56.64	708.66	0	-602.12	1.8	-312.51	1.8	-180.27	2.12	-346.62

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ+
C. Infrecuentes dominante GRAD

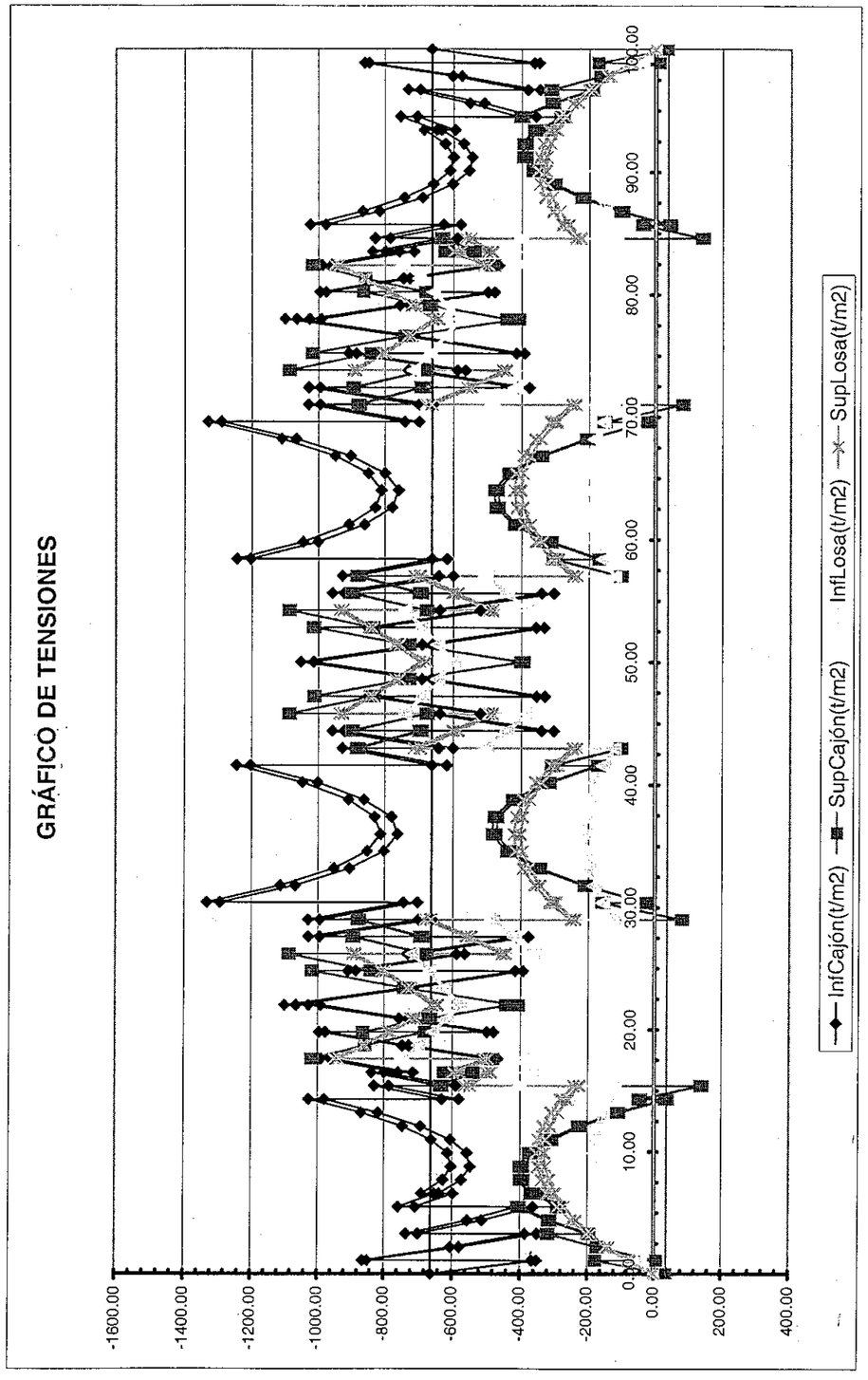
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1141.67	-56.49	708.64	0	-602.13	1.8	-312.50	1.8	-180.26	2.12	-346.62
171	172	90.10	-1141.67	-22.61	747.30	0	-554.02	1.8	-369.92	1.8	-182.86	2.12	-351.60
172	172	90.10	-1141.67	-22.45	747.34	0	-553.99	1.8	-369.93	1.8	-182.86	2.12	-351.61
172	173	91.20	-1141.67	11.36	747.97	0	-544.34	1.8	-397.66	1.8	-180.78	2.12	-347.60
173	173	91.20	-1141.67	11.54	748.03	0	-544.30	1.8	-397.67	1.8	-180.79	2.12	-347.62
173	174	92.30	-1141.67	45.32	714.78	0	-569.73	1.8	-396.51	1.8	-174.73	2.12	-335.97
174	174	92.30	-1141.67	45.61	714.87	0	-569.66	1.8	-396.52	1.8	-174.74	2.12	-336.00
174	175	93.40	-1141.67	79.40	642.51	0	-634.46	1.8	-365.42	1.8	-163.82	2.12	-315.01
175	175	93.40	-1141.67	79.73	642.65	0	-594.56	1.8	-347.98	1.8	-162.51	2.12	-320.21
175	176	94.50	-1141.67	113.59	531.18	0	-704.16	1.8	-287.20	1.8	-146.86	2.12	-289.39
176	176	94.50	-944.83	113.95	649.89	0	-357.98	1.8	-405.07	1.8	-146.90	2.12	-289.46
176	177	95.60	-944.83	155.59	499.28	0	-508.95	1.8	-314.49	1.8	-126.42	2.12	-249.11
177	177	95.60	-944.83	156.11	499.52	0	-508.75	1.8	-314.54	1.8	-126.46	2.12	-249.19
177	178	96.70	-944.83	189.96	315.87	0	-695.84	1.8	-195.31	1.8	-102.19	2.12	-201.37
178	178	96.70	-747.99	190.61	436.60	0	-346.48	1.8	-317.78	1.8	-102.24	2.12	-201.45
178	179	97.80	-747.99	224.38	213.57	0	-575.16	1.8	-168.69	1.8	-73.10	2.12	-144.04
179	179	97.80	-747.99	225.13	213.86	0	-574.90	1.8	-168.74	1.8	-73.15	2.12	-144.14
179	180	98.90	-747.99	258.96	-49.09	0	-845.64	1.8	10.32	1.8	-39.05	2.12	-76.96
180	180	98.90	-472.42	259.84	125.37	0	-347.83	1.8	-173.92	1.8	-39.10	2.12	-77.05
180	181	100.00	-472.42	169.92	-178.23	0	-662.02	1.8	37.50	1.8	-0.11	2.12	-0.22

Programa DINTEL PACADAR S.A.
INFRECUENTESG.T0.MZ+

GRÁFICO DE TENSIONES



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ-

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-522.14	-246.34	-198.37	0	-732.89	1.8	41.72	1.8	0.11	2.12	0.22
1	2	1.10	-517.71	-90.53	-87.22	0	-582.15	1.8	-126.32	1.8	-6.73	2.12	-13.27
2	2	1.10	-822.30	-90.75	-279.75	0	-1132.11	1.8	77.25	1.8	-6.73	2.12	-13.26
2	3	2.20	-822.30	-72.81	-189.79	0	-1011.57	1.8	-65.75	1.8	-11.94	2.12	-23.53
3	3	2.20	-822.30	-73.04	-189.82	0	-1011.60	1.8	-65.74	1.8	-11.93	2.12	-23.52
3	4	3.30	-822.30	-55.06	-119.38	0	-915.51	1.8	-182.71	1.8	-15.62	2.12	-30.78
4	4	3.30	-1039.86	-55.30	-252.56	0	-1301.42	1.8	-47.40	1.8	-15.62	2.12	-30.77
4	5	4.40	-1039.86	-37.36	-201.61	0	-1229.77	1.8	-138.31	1.8	-17.79	2.12	-35.05
5	5	4.40	-1039.86	-37.62	-201.63	0	-1229.79	1.8	-138.31	1.8	-17.78	2.12	-35.04
5	6	5.50	-1039.86	-19.65	-170.15	0	-1182.52	1.8	-203.24	1.8	-18.43	2.12	-36.32
6	6	5.50	-1257.42	-19.93	-301.15	0	-1564.97	1.8	-73.00	1.8	-18.42	2.12	-36.31
6	7	6.60	-1257.42	-1.97	-289.07	0	-1542.03	1.8	-111.98	1.8	-17.56	2.12	-34.61
7	7	6.60	-1257.42	-2.29	-289.12	0	-1540.06	1.8	-129.46	1.8	-17.70	2.12	-34.04
7	8	7.70	-1257.42	15.66	-296.47	0	-1541.32	1.8	-142.41	1.8	-15.31	2.12	-29.45
8	8	7.70	-1257.42	15.35	-296.50	0	-1541.34	1.8	-142.40	1.8	-15.31	2.12	-29.44
8	9	8.80	-1257.42	33.54	-323.27	0	-1565.86	1.8	-129.26	1.8	-11.40	2.12	-21.92
9	9	8.80	-1257.42	33.10	-323.30	0	-1565.89	1.8	-129.25	1.8	-11.39	2.12	-21.91
9	10	9.90	-1257.42	51.16	-369.62	0	-1613.76	1.8	-90.01	1.8	-5.94	2.12	-11.42
10	10	9.90	-1257.42	50.76	-369.63	0	-1613.77	1.8	-90.01	1.8	-5.94	2.12	-11.42
10	11	11.00	-1257.42	68.71	-435.36	0	-1684.88	1.8	-24.72	1.8	1.04	2.12	1.99
11	11	11.00	-1257.42	68.27	-435.37	0	-1684.89	1.8	-24.72	1.8	1.04	2.12	2.00
11	12	12.10	-1257.42	86.25	-520.36	0	-1779.14	1.8	66.64	1.8	9.51	2.12	18.28
12	12	12.10	-1257.42	85.81	-520.39	0	-1779.16	1.8	66.64	1.8	9.51	2.12	18.29
12	13	13.20	-1257.42	103.81	-624.75	0	-1896.63	1.8	184.10	1.8	19.49	2.12	37.48
13	13	13.20	-1257.42	103.36	-624.76	0	-1896.64	1.8	184.10	1.8	19.49	2.12	37.48
13	14	14.30	-1257.42	121.35	-748.35	0	-2037.18	1.8	327.51	1.8	30.97	2.12	59.55
14	14	14.30	-1016.08	110.63	-617.40	0	-1651.81	1.8	233.66	1.8	30.72	2.12	60.53
14	15	15.40	-1016.27	131.08	-759.44	0	-1818.94	1.8	400.83	1.8	43.58	2.12	85.88
15	15	15.40	-1871.02	139.40	-361.78	0	-1622.01	1.8	-377.97	1.8	-211.41	2.12	-201.68
15	16	16.50	-1871.02	189.79	-530.30	0	-1784.70	1.8	-295.01	1.8	-187.87	2.12	-154.74
16	16	16.50	-1871.02	189.49	-530.21	0	-1806.38	1.8	-273.80	1.8	-169.45	2.12	-129.70
16	17	17.60	-1871.02	218.40	-752.69	0	-2043.43	1.8	-138.06	1.8	-121.97	2.12	-45.75
17	17	17.60	-2480.19	217.87	-221.26	0	-1526.49	1.8	-644.98	1.8	-443.86	2.12	-444.99
17	18	18.70	-2480.19	260.19	-483.75	0	-1808.50	1.8	-477.22	1.8	-388.79	2.12	-347.61
18	18	18.70	-2480.18	259.71	-483.34	0	-1808.10	1.8	-477.33	1.8	-388.89	2.12	-347.80
18	19	19.80	-2480.18	306.85	-793.65	0	-2142.89	1.8	-274.44	1.8	-324.36	2.12	-233.69
19	19	19.80	-2175.60	306.45	-600.62	0	-1592.45	1.8	-478.16	1.8	-324.49	2.12	-233.93
19	20	20.90	-2175.60	365.49	-975.53	0	-1996.28	1.8	-235.16	1.8	-246.26	2.12	-95.60
20	20	20.90	-2175.60	365.29	-975.51	0	-1996.26	1.8	-235.17	1.8	-246.27	2.12	-95.61
20	21	22.00	-2175.60	419.33	-1406.01	0	-2462.27	1.8	51.36	1.8	-157.37	2.12	61.58
21	1021	22.00	-2219.11	-441.28	-1434.73	0	-2542.83	1.8	83.46	1.8	-157.39	2.12	61.54
21	22	23.40	-2219.11	-383.43	-862.30	0	-1913.97	1.8	-327.59	1.8	-271.86	2.12	-140.85
22	22	23.40	-2219.11	-383.67	-862.17	0	-1913.85	1.8	-327.62	1.8	-271.89	2.12	-140.91
22	23	24.80	-2219.11	-321.42	-368.78	0	-1375.07	1.8	-671.34	1.8	-371.86	2.12	-317.69
23	23	24.80	-2523.70	-320.12	-558.23	0	-1920.15	1.8	-474.85	1.8	-371.86	2.12	-317.69
23	24	26.20	-2523.70	-246.73	-170.52	0	-1494.19	1.8	-753.34	1.8	-449.38	2.12	-454.76
24	24	26.20	-1696.97	-246.62	-568.77	0	-1624.95	1.8	-382.61	1.8	-127.39	2.12	-55.34
24	25	27.60	-1696.97	-190.83	-263.21	0	-1289.02	1.8	-602.82	1.8	-188.39	2.12	-163.20
25	25	27.60	-2088.58	-191.36	-495.60	0	-1971.70	1.8	-377.33	1.8	-188.25	2.12	-162.94
25	26	29.00	-2088.58	-115.65	-300.50	0	-1753.22	1.8	-530.96	1.8	-225.58	2.12	-228.95
26	26	29.00	-1242.90	-111.46	-698.24	0	-1990.60	1.8	342.88	1.8	22.63	2.12	44.59
26	27	30.40	-1243.14	-85.36	-553.49	0	-1807.25	1.8	133.03	1.8	12.61	2.12	24.84
27	27	30.40	-1606.18	-91.71	-752.65	0	-2404.24	1.8	282.76	1.8	12.72	2.12	24.46
27	28	31.80	-1606.18	-68.78	-640.30	0	-2264.64	1.8	116.58	1.8	5.13	2.12	9.87
28	28	31.80	-1606.18	-69.38	-640.36	0	-2264.68	1.8	116.59	1.8	5.14	2.12	9.89
28	29	33.20	-1606.18	-46.54	-559.21	0	-2162.52	1.8	-7.47	1.8	-0.02	2.12	-0.03
29	29	33.20	-1606.18	-47.09	-559.22	0	-2162.53	1.8	-7.47	1.8	-0.02	2.12	-0.03
29	30	34.60	-1606.18	-22.98	-510.41	0	-2098.76	1.8	-89.09	1.8	-2.56	2.12	-4.93
30	30	34.60	-1606.18	-23.52	-510.48	0	-2098.82	1.8	-89.08	1.8	-2.55	2.12	-4.91
30	31	36.00	-1606.18	3.02	-496.75	0	-2075.68	1.8	-127.76	1.8	-2.02	2.12	-3.88
31	31	36.00	-1606.18	2.49	-496.76	0	-2075.69	1.8	-127.76	1.8	-2.02	2.12	-3.88
31	32	37.40	-1606.18	25.45	-516.26	0	-2091.67	1.8	-123.87	1.8	1.28	2.12	2.46
32	32	37.40	-1606.18	24.85	-516.27	0	-2091.68	1.8	-123.86	1.8	1.28	2.12	2.47
32	33	38.80	-1606.18	47.71	-567.05	0	-2145.18	1.8	-77.75	1.8	7.01	2.12	13.49
33	33	38.80	-1606.18	47.12	-567.05	0	-2145.18	1.8	-77.75	1.8	7.01	2.12	13.49
33	34	40.20	-1606.18	69.98	-649.03	0	-2236.16	1.8	10.56	1.8	15.17	2.12	29.17
34	34	40.20	-1606.18	69.37	-649.00	0	-2236.13	1.8	10.55	1.8	15.16	2.12	29.16
34	35	41.60	-1606.18	92.32	-762.14	0	-2364.52	1.8	141.03	1.8	25.73	2.12	49.48
35	35	41.60	-1249.48	87.58	-563.00	0	-1776.63	1.8	-14.03	1.8	25.52	2.12	50.28
35	36	43.00	-1249.32	113.27	-707.30	0	-1947.92	1.8	157.39	1.8	38.48	2.12	75.82
36	36	43.00	-2088.58	115.79	-309.56	0	-1767.10	1.8	-511.64	1.8	-225.36	2.12	-228.57
36	37	44.40	-2088.58	185.24	-507.34	0	-1989.19	1.8	-353.89	1.8	-187.77	2.12	-162.10
37	37	44.40	-1696.97	184.65	-275.04	0	-1306.61	1.8	-579.35	1.8	-187.89	2.12	-162.31
37	38	45.80	-1696.97	237.55	-567.56	0	-1630.94	1.8	-359.61	1.8	-130.61	2.12	-61.02
38	38	45.80	-2523.70	237.09	-169.21	0	-1500.08	1.8	-730.37	1.8	-452.62	2.12	-460.48

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ-
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2523.70	295.94	-538.48	0	-1909.21	1.8	-453.92	1.8	-380.19	2.12	-332.40
39	39	47.20	-2219.11	295.15	-348.64	0	-1363.75	1.8	-650.52	1.8	-380.28	2.12	-332.58
39	40	48.60	-2212.66	371.48	-817.63	0	-1877.95	1.8	-308.60	1.8	-285.17	2.12	-165.73
40	40	48.60	-2212.49	371.19	-817.71	0	-1877.98	1.8	-308.52	1.8	-285.11	2.12	-165.65
40	41	50.00	-2212.49	431.70	-1376.34	0	-2494.50	1.8	101.84	1.8	-174.55	2.12	29.84
41	1041	50.00	-2212.70	-431.62	-1376.34	0	-2494.57	1.8	101.77	1.8	-174.61	2.12	29.78
41	42	51.40	-2212.70	-371.12	-817.83	0	-1878.15	1.8	-308.55	1.8	-285.13	2.12	-165.65
42	42	51.40	-2213.30	-371.40	-817.76	0	-1878.28	1.8	-308.76	1.8	-285.31	2.12	-165.84
42	43	52.80	-2213.30	-295.56	-348.78	0	-1362.10	1.8	-648.69	1.8	-378.69	2.12	-330.96
43	43	52.80	-2518.88	-296.30	-538.52	0	-1907.76	1.8	-452.43	1.8	-378.89	2.12	-331.10
43	44	54.20	-2523.70	-237.09	-169.19	0	-1500.06	1.8	-730.37	1.8	-452.62	2.12	-460.49
44	44	54.20	-1696.97	-237.55	-567.56	0	-1630.94	1.8	-359.61	1.8	-130.61	2.12	-61.02
44	45	55.60	-1696.97	-184.64	-275.01	0	-1306.58	1.8	-579.36	1.8	-187.90	2.12	-162.32
45	45	55.60	-2088.58	-185.24	-507.33	0	-1989.18	1.8	-353.90	1.8	-187.78	2.12	-162.11
45	46	57.00	-2088.58	-115.78	-309.52	0	-1767.06	1.8	-511.65	1.8	-225.37	2.12	-228.59
46	46	57.00	-1249.32	-113.28	-707.29	0	-1947.90	1.8	157.36	1.8	38.47	2.12	75.81
46	47	58.40	-1251.27	-88.50	-562.10	0	-1776.72	1.8	-17.58	1.8	25.52	2.12	50.28
47	47	58.40	-1608.20	-92.25	-761.24	0	-2364.80	1.8	137.31	1.8	25.73	2.12	49.48
47	48	59.80	-1608.20	-69.31	-648.17	0	-2236.51	1.8	7.00	1.8	15.16	2.12	29.15
48	48	59.80	-1608.20	-69.91	-648.19	0	-2236.53	1.8	7.01	1.8	15.16	2.12	29.16
48	49	61.20	-1608.20	-47.05	-566.32	0	-2145.72	1.8	-81.09	1.8	7.01	2.12	13.49
49	49	61.20	-1608.20	-47.65	-566.32	0	-2145.72	1.8	-81.09	1.8	7.01	2.12	13.49
49	50	62.60	-1608.20	-24.80	-515.60	0	-2092.31	1.8	-127.04	1.8	1.28	2.12	2.46
50	50	62.60	-1608.20	-25.39	-515.61	0	-2092.31	1.8	-127.04	1.8	1.28	2.12	2.46
50	51	64.00	-1609.94	-2.40	-496.19	0	-2077.89	1.8	-132.14	1.8	-2.02	2.12	-3.88
51	51	64.00	-1609.94	-2.94	-496.19	0	-2077.89	1.8	-132.14	1.8	-2.02	2.12	-3.88
51	52	65.40	-1609.94	23.61	-510.03	0	-2101.20	1.8	-93.20	1.8	-2.55	2.12	-4.91
52	52	65.40	-1609.94	23.06	-509.98	0	-2101.15	1.8	-93.21	1.8	-2.56	2.12	-4.92
52	53	66.80	-1609.94	47.17	-558.88	0	-2165.07	1.8	-11.34	1.8	-0.02	2.12	-0.03
53	53	66.80	-1609.94	46.63	-558.86	0	-2165.06	1.8	-11.34	1.8	-0.02	2.12	-0.04
53	54	68.20	-1609.94	69.46	-640.11	0	-2267.38	1.8	112.96	1.8	5.14	2.12	9.88
54	54	68.20	-1609.94	68.86	-640.08	0	-2267.36	1.8	112.96	1.8	5.14	2.12	9.88
54	55	69.60	-1609.94	91.79	-752.53	0	-2407.11	1.8	279.39	1.8	12.72	2.12	24.46
55	55	69.60	-1246.39	87.25	-553.38	0	-1809.73	1.8	130.07	1.8	12.61	2.12	24.85
55	56	71.00	-1242.90	111.47	-698.25	0	-1990.61	1.8	342.90	1.8	22.63	2.12	44.59
56	56	71.00	-2088.58	115.65	-300.50	0	-1753.22	1.8	-530.96	1.8	-225.58	2.12	-228.95
56	57	72.40	-2088.58	191.36	-495.60	0	-1971.70	1.8	-377.33	1.8	-188.25	2.12	-162.94
57	57	72.40	-1696.97	190.85	-263.21	0	-1289.03	1.8	-602.81	1.8	-188.39	2.12	-163.19
57	58	73.80	-1696.97	246.65	-568.78	0	-1624.95	1.8	-382.61	1.8	-127.39	2.12	-55.33
58	58	73.80	-2523.70	246.73	-170.52	0	-1494.19	1.8	-753.34	1.8	-449.38	2.12	-454.75
58	59	75.20	-2523.70	320.12	-558.25	0	-1920.17	1.8	-474.84	1.8	-371.86	2.12	-317.68
59	59	75.20	-2219.11	321.41	-368.77	0	-1375.06	1.8	-671.34	1.8	-371.87	2.12	-317.69
59	60	76.60	-2215.29	384.13	-862.69	0	-1913.17	1.8	-326.29	1.8	-270.73	2.12	-139.66
60	60	76.60	-2215.34	383.92	-862.91	0	-1913.40	1.8	-326.24	1.8	-270.69	2.12	-139.57
60	61	78.00	-2215.34	441.80	-1436.04	0	-2542.94	1.8	85.01	1.8	-156.05	2.12	63.14
61	1061	78.00	-2172.15	-419.48	-1407.38	0	-2462.54	1.8	52.82	1.8	-156.10	2.12	63.12
61	62	79.10	-2172.15	-365.44	-976.71	0	-1996.36	1.8	-233.76	1.8	-245.04	2.12	-94.15
62	62	79.10	-2172.53	-365.66	-976.74	0	-1996.51	1.8	-233.86	1.8	-245.13	2.12	-94.23
62	63	80.20	-2172.53	-306.62	-601.63	0	-1592.48	1.8	-476.92	1.8	-323.42	2.12	-232.66
63	63	80.20	-2477.65	-307.02	-794.63	0	-2143.06	1.8	-273.37	1.8	-323.43	2.12	-232.58
63	64	81.30	-2477.65	-259.88	-484.14	0	-1808.09	1.8	-476.32	1.8	-388.01	2.12	-346.76
64	64	81.30	-2478.35	-260.34	-484.50	0	-1808.66	1.8	-476.43	1.8	-388.11	2.12	-346.79
64	65	82.40	-2478.35	-218.01	-221.83	0	-1526.47	1.8	-644.24	1.8	-443.22	2.12	-444.24
65	65	82.40	-1870.06	-218.50	-752.74	0	-2042.92	1.8	-138.62	1.8	-121.59	2.12	-45.27
65	66	83.50	-1870.06	-189.59	-530.59	0	-1806.45	1.8	-273.39	1.8	-169.10	2.12	-129.27
66	66	83.50	-1871.02	-189.81	-530.56	0	-1784.93	1.8	-294.96	1.8	-187.83	2.12	-154.66
66	67	84.60	-1871.02	-139.42	-362.03	0	-1622.22	1.8	-377.93	1.8	-211.37	2.12	-201.60
67	67	84.60	-1016.26	-131.08	-759.70	0	-1819.32	1.8	401.39	1.8	43.59	2.12	85.89
67	68	85.70	-1019.75	-113.08	-616.29	0	-1653.11	1.8	228.05	1.8	30.72	2.12	60.53
68	68	85.70	-1261.85	-121.28	-747.25	0	-2039.10	1.8	321.28	1.8	30.97	2.12	59.56
68	69	86.80	-1261.85	-103.28	-623.73	0	-1898.68	1.8	178.05	1.8	19.50	2.12	37.49
69	69	86.80	-1261.85	-103.75	-623.72	0	-1898.66	1.8	178.05	1.8	19.49	2.12	37.48
69	70	87.90	-1261.85	-85.74	-519.47	0	-1781.36	1.8	60.84	1.8	9.52	2.12	18.30
70	70	87.90	-1261.85	-86.18	-519.45	0	-1781.34	1.8	60.84	1.8	9.51	2.12	18.29
70	71	89.00	-1261.85	-68.20	-434.54	0	-1687.22	1.8	-30.31	1.8	1.04	2.12	2.00
71	71	89.00	-1261.85	-68.64	-434.52	0	-1687.21	1.8	-30.32	1.8	1.04	2.12	2.00
71	72	90.10	-1261.85	-50.69	-368.88	0	-1616.22	1.8	-95.43	1.8	-5.93	2.12	-11.41
72	72	90.10	-1261.85	-51.09	-368.86	0	-1616.21	1.8	-95.43	1.8	-5.94	2.12	-11.42
72	73	91.20	-1261.85	-33.04	-322.64	0	-1568.47	1.8	-134.47	1.8	-11.39	2.12	-21.90
73	73	91.20	-1261.85	-33.47	-322.59	0	-1568.43	1.8	-134.48	1.8	-11.40	2.12	-21.91
73	74	92.30	-1261.85	-15.28	-295.90	0	-1544.04	1.8	-147.42	1.8	-15.31	2.12	-29.43
74	74	92.30	-1261.85	-15.59	-295.88	0	-1544.03	1.8	-147.43	1.8	-15.31	2.12	-29.44
74	75	93.40	-1261.85	2.36	-288.60	0	-1542.89	1.8	-134.28	1.8	-17.70	2.12	-34.04
75	75	93.40	-1261.85	2.03	-288.57	0	-1544.77	1.8	-116.72	1.8	-17.56	2.12	-34.60
75	76	94.50	-1261.85	19.99	-300.72	0	-1567.82	1.8	-77.57	1.8	-18.42	2.12	-36.30

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ-
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-1044.29	19.72	-169.70	0	-1185.36	1.8	-207.81	1.8	-18.43	2.12	-36.32
76	77	95.60	-1044.29	37.68	-201.30	0	-1232.78	1.8	-142.68	1.8	-17.78	2.12	-35.03
77	77	95.60	-1044.29	37.43	-201.27	0	-1232.76	1.8	-142.68	1.8	-17.78	2.12	-35.04
77	78	96.70	-1044.29	55.37	-252.32	0	-1304.58	1.8	-51.52	1.8	-15.61	2.12	-30.77
78	78	96.70	-826.73	55.13	-119.15	0	-918.67	1.8	-186.83	1.8	-15.62	2.12	-30.78
78	79	97.80	-826.73	73.10	-189.66	0	-1014.88	1.8	-69.67	1.8	-11.93	2.12	-23.52
79	79	97.80	-826.73	72.86	-189.62	0	-1014.86	1.8	-69.67	1.8	-11.94	2.12	-23.53
79	80	98.90	-826.73	90.80	-279.66	0	-1135.52	1.8	73.51	1.8	-6.73	2.12	-13.26
80	80	98.90	-522.14	90.59	-87.13	0	-585.56	1.8	-130.06	1.8	-6.73	2.12	-13.27
80	81	100.00	-522.14	246.31	-198.37	0	-732.89	1.8	41.72	1.8	0.11	2.12	0.22
101	101	0.00	-522.14	-243.33	-198.43	0	-732.94	1.8	41.73	1.8	0.12	2.12	0.24
101	102	1.10	-517.71	-86.70	-91.57	0	-585.92	1.8	-125.47	1.8	-6.00	2.12	-11.82
102	102	1.10	-822.30	-87.02	-283.88	0	-1135.67	1.8	78.05	1.8	-6.03	2.12	-11.89
102	103	2.20	-822.30	-69.50	-197.81	0	-1018.50	1.8	-64.20	1.8	-10.59	2.12	-20.87
103	103	2.20	-822.30	-69.74	-197.63	0	-1018.34	1.8	-64.23	1.8	-10.62	2.12	-20.93
103	104	3.30	-822.30	-52.23	-130.58	0	-925.18	1.8	-180.54	1.8	-13.74	2.12	-27.07
104	104	3.30	-1039.86	-52.36	-263.56	0	-1310.92	1.8	-45.27	1.8	-13.77	2.12	-27.13
104	105	4.40	-1039.86	-34.87	-215.59	0	-1241.83	1.8	-135.63	1.8	-15.43	2.12	-30.41
105	105	4.40	-1039.86	-34.95	-215.47	0	-1241.72	1.8	-135.65	1.8	-15.45	2.12	-30.45
105	106	5.50	-1039.86	-17.44	-186.67	0	-1196.77	1.8	-200.06	1.8	-15.65	2.12	-30.84
106	106	5.50	-1257.42	-17.41	-317.51	0	-1579.08	1.8	-69.86	1.8	-15.67	2.12	-30.88
106	107	6.60	-1257.42	0.11	-307.99	0	-1558.36	1.8	-108.31	1.8	-14.38	2.12	-28.34
107	107	6.60	-1257.42	0.18	-307.89	0	-1555.42	1.8	-125.80	1.8	-14.52	2.12	-27.92
107	108	7.70	-1257.42	17.68	-317.72	0	-1558.70	1.8	-138.26	1.8	-11.71	2.12	-22.52
108	108	7.70	-1257.42	17.80	-317.63	0	-1558.63	1.8	-138.28	1.8	-11.73	2.12	-22.55
108	109	8.80	-1257.42	35.30	-346.82	0	-1585.13	1.8	-124.66	1.8	-7.41	2.12	-14.24
109	109	8.80	-1257.42	35.43	-346.76	0	-1585.07	1.8	-124.67	1.8	-7.42	2.12	-14.26
109	110	9.90	-1257.42	52.93	-395.39	0	-1634.84	1.8	-84.98	1.8	-1.57	2.12	-3.02
110	110	9.90	-1257.42	53.10	-395.35	0	-1634.81	1.8	-84.99	1.8	-1.58	2.12	-3.03
110	111	11.00	-1257.42	70.62	-463.37	0	-1707.79	1.8	-19.25	1.8	5.78	2.12	11.12
111	111	11.00	-1257.42	70.84	-463.35	0	-1707.78	1.8	-19.26	1.8	5.78	2.12	11.12
111	112	12.10	-1257.42	88.34	-550.93	0	-1804.14	1.8	72.60	1.8	14.69	2.12	28.24
112	112	12.10	-1257.42	88.58	-550.92	0	-1804.13	1.8	72.60	1.8	14.69	2.12	28.24
112	113	13.20	-1257.42	106.07	-658.01	0	-1923.83	1.8	190.57	1.8	25.13	2.12	48.32
113	113	13.20	-1257.42	106.33	-658.05	0	-1923.86	1.8	190.57	1.8	25.14	2.12	48.33
113	114	14.30	-1257.42	123.87	-784.65	0	-2066.88	1.8	334.59	1.8	37.12	2.12	71.38
114	114	14.30	-1016.08	113.91	-653.74	0	-1683.18	1.8	240.69	1.8	36.83	2.12	72.57
114	115	15.40	-1016.27	134.10	-799.15	0	-1853.22	1.8	408.51	1.8	50.26	2.12	99.04
115	115	15.40	-1871.02	143.22	-401.59	0	-1656.30	1.8	-370.51	1.8	-204.92	2.12	-188.75
115	116	16.50	-1871.02	187.82	-574.25	0	-1822.56	1.8	-286.77	1.8	-180.71	2.12	-140.46
116	116	16.50	-1871.02	188.06	-574.36	0	-1849.11	1.8	-260.93	1.8	-158.27	2.12	-109.94
116	117	17.60	-1871.02	215.59	-794.82	0	-2084.21	1.8	-125.78	1.8	-111.31	2.12	-26.89
117	117	17.60	-2480.18	215.71	-263.62	0	-1567.48	1.8	-632.63	1.8	-433.13	2.12	-426.03
117	118	18.70	-2480.18	265.65	-529.52	0	-1852.80	1.8	-463.87	1.8	-377.20	2.12	-327.13
118	118	18.70	-2480.18	265.91	-529.26	0	-1852.54	1.8	-463.95	1.8	-377.27	2.12	-327.25
118	119	19.80	-2480.18	322.57	-851.66	0	-2199.04	1.8	-257.53	1.8	-309.68	2.12	-207.73
119	119	19.80	-2175.60	323.25	-658.97	0	-1648.92	1.8	-461.16	1.8	-309.73	2.12	-207.82
119	120	20.90	-2175.60	393.84	-1060.70	0	-2078.71	1.8	-210.35	1.8	-224.71	2.12	-57.48
120	120	20.90	-2175.60	394.79	-1060.65	0	-2078.66	1.8	-210.36	1.8	-224.72	2.12	-57.51
120	121	22.00	-2175.60	445.32	-1519.28	0	-2571.90	1.8	84.37	1.8	-128.70	2.12	112.27
121	1121	22.00	-2219.11	-465.62	-1548.08	0	-2652.54	1.8	116.50	1.8	-128.70	2.12	112.27
121	122	23.40	-2219.11	-404.00	-942.94	0	-1992.02	1.8	-304.09	1.8	-251.45	2.12	-104.76
122	122	23.40	-2219.11	-402.74	-943.03	0	-1992.11	1.8	-304.06	1.8	-251.42	2.12	-104.72
122	123	24.80	-2219.11	-337.96	-425.50	0	-1429.96	1.8	-654.81	1.8	-357.51	2.12	-292.31
123	123	24.80	-2523.70	-336.49	-614.94	0	-1975.03	1.8	-458.32	1.8	-357.51	2.12	-292.31
123	124	26.20	-2523.70	-253.39	-212.06	0	-1534.40	1.8	-741.23	1.8	-438.87	2.12	-436.16
124	124	26.20	-1696.97	-253.04	-610.14	0	-1664.99	1.8	-370.56	1.8	-116.92	2.12	-36.82
124	125	27.60	-1696.97	-193.82	-299.24	0	-1323.90	1.8	-592.32	1.8	-179.27	2.12	-147.07
125	125	27.60	-2088.58	-193.78	-531.41	0	-2006.35	1.8	-366.90	1.8	-179.19	2.12	-146.92
125	126	29.00	-2088.58	-118.04	-328.48	0	-1780.30	1.8	-522.81	1.8	-218.50	2.12	-216.43
126	126	29.00	-1242.90	-112.78	-726.04	0	-2014.60	1.8	348.28	1.8	27.30	2.12	53.80
126	127	30.40	-1243.14	-87.78	-578.55	0	-1828.88	1.8	137.88	1.8	16.82	2.12	33.14
127	127	30.40	-1606.18	-93.09	-777.59	0	-2424.64	1.8	287.63	1.8	16.95	2.12	32.59
127	128	31.80	-1606.18	-70.67	-663.02	0	-2283.22	1.8	121.02	1.8	8.98	2.12	17.27
128	128	31.80	-1606.18	-70.19	-662.96	0	-2283.17	1.8	121.00	1.8	8.97	2.12	17.25
128	129	33.20	-1606.18	-47.93	-580.22	0	-2179.70	1.8	-3.39	1.8	3.55	2.12	6.82
129	129	33.20	-1606.18	-47.49	-580.18	0	-2179.67	1.8	-3.40	1.8	3.54	2.12	6.81
129	130	34.60	-1606.18	-24.05	-530.14	0	-2114.90	1.8	-85.24	1.8	0.78	2.12	1.50
130	130	34.60	-1606.18	-23.60	-530.16	0	-2114.92	1.8	-85.23	1.8	0.78	2.12	1.51
130	131	36.00	-1606.18	3.12	-516.37	0	-2091.72	1.8	-123.95	1.8	1.31	2.12	2.51
131	131	36.00	-1606.18	3.58	-516.36	0	-2091.71	1.8	-123.95	1.8	1.31	2.12	2.51
131	132	37.40	-1606.18	25.90	-536.99	0	-2108.63	1.8	-119.80	1.8	4.79	2.12	9.22
132	132	37.40	-1606.18	26.35	-537.00	0	-2108.64	1.8	-119.80	1.8	4.79	2.12	9.22
132	133	38.80	-1606.18	48.63	-589.49	0	-2163.55	1.8	-73.35	1.8	10.82	2.12	20.80
133	133	38.80	-1606.18	49.12	-589.52	0	-2163.57	1.8	-73.35	1.8	10.82	2.12	20.81

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.T0.MZ-

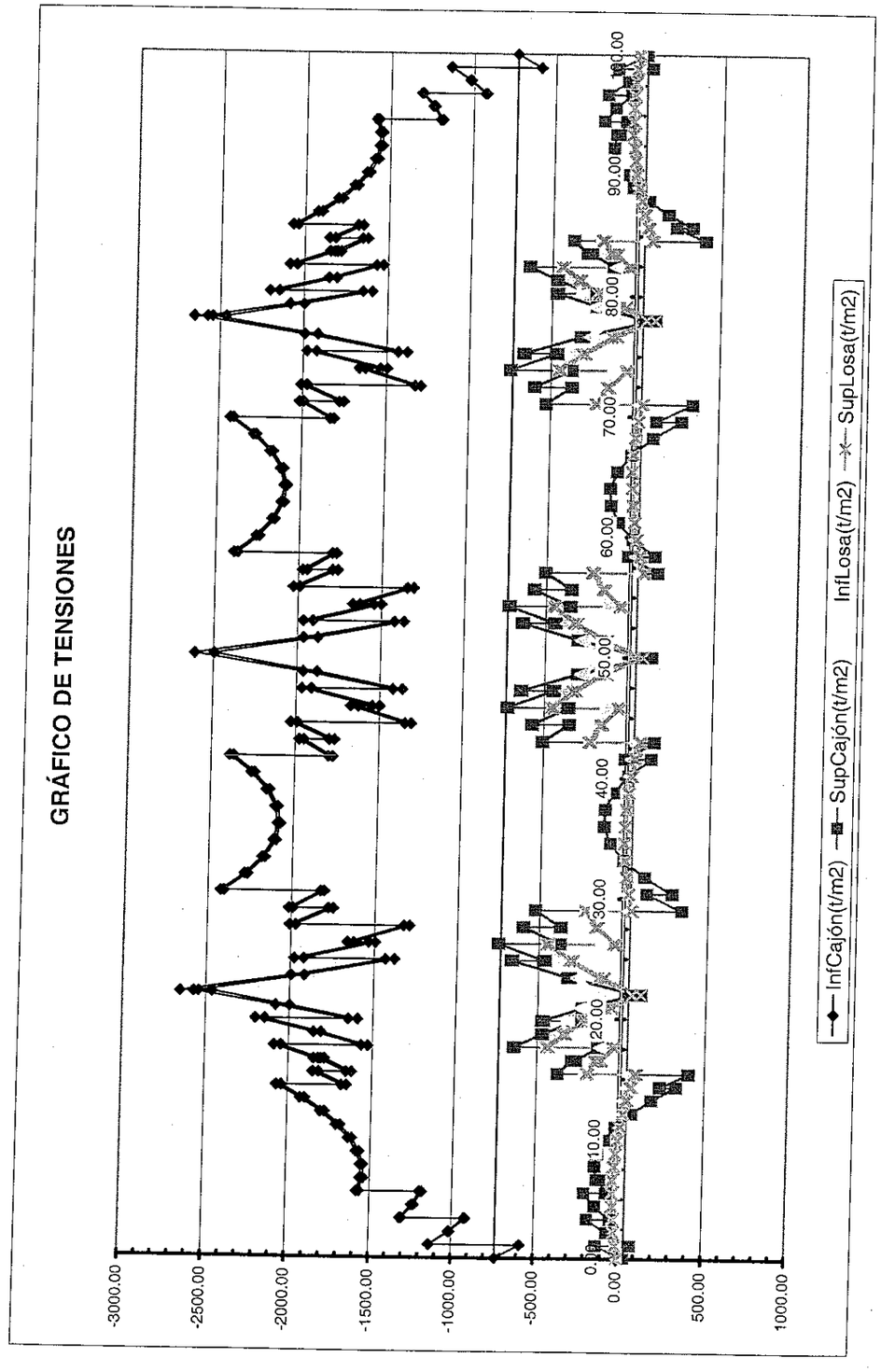
Infrecuentes dominante GRAD

1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1606.18	71.41	-673.87	0	-2256.48	1.8	15.41	1.8	19.38	2.12	37.26
134	134	40.20	-1606.18	71.88	-673.92	0	-2256.51	1.8	15.42	1.8	19.39	2.12	37.28
134	135	41.60	-1606.18	94.31	-790.23	0	-2387.49	1.8	146.52	1.8	30.49	2.12	58.63
135	135	41.60	-1249.48	90.63	-591.18	0	-1800.95	1.8	-8.58	1.8	30.25	2.12	59.61
135	136	43.00	-1249.32	115.41	-739.27	0	-1975.52	1.8	163.57	1.8	43.85	2.12	86.41
136	136	43.00	-2088.58	119.12	-341.69	0	-1798.19	1.8	-502.27	1.8	-217.23	2.12	-214.19
136	137	44.40	-2088.58	186.76	-546.58	0	-2027.18	1.8	-342.46	1.8	-177.84	2.12	-144.54
137	137	44.40	-1696.97	186.93	-314.55	0	-1344.84	1.8	-567.84	1.8	-177.89	2.12	-144.63
137	138	45.80	-1696.97	243.33	-612.44	0	-1674.37	1.8	-346.53	1.8	-119.25	2.12	-40.93
138	138	45.80	-2523.70	243.49	-214.27	0	-1543.69	1.8	-717.24	1.8	-441.22	2.12	-440.32
138	139	47.20	-2523.70	309.00	-597.45	0	-1966.28	1.8	-436.74	1.8	-365.26	2.12	-306.02
139	139	47.20	-2219.11	309.54	-407.81	0	-1421.01	1.8	-633.28	1.8	-365.31	2.12	-306.10
139	140	48.60	-2212.66	391.39	-903.42	0	-1960.98	1.8	-283.60	1.8	-263.46	2.12	-127.34
140	140	48.60	-2212.49	392.67	-903.39	0	-1960.90	1.8	-283.55	1.8	-263.42	2.12	-127.30
140	141	50.00	-2212.49	457.14	-1496.27	0	-2610.57	1.8	136.79	1.8	-144.20	2.12	83.51
141	1141	50.00	-2212.71	-457.07	-1496.27	0	-2610.64	1.8	136.72	1.8	-144.26	2.12	83.45
141	142	51.40	-2212.71	-392.58	-903.50	0	-1961.07	1.8	-283.59	1.8	-263.45	2.12	-127.31
142	142	51.40	-2213.30	-391.30	-903.54	0	-1961.29	1.8	-283.76	1.8	-263.60	2.12	-127.45
142	143	52.80	-2213.30	-309.94	-407.93	0	-1419.34	1.8	-631.45	1.8	-363.72	2.12	-304.49
143	143	52.80	-2518.88	-309.37	-597.46	0	-1964.81	1.8	-435.25	1.8	-363.97	2.12	-304.72
143	144	54.20	-2523.70	-243.48	-214.26	0	-1543.68	1.8	-717.24	1.8	-441.22	2.12	-440.32
144	144	54.20	-1696.97	-243.34	-612.42	0	-1674.35	1.8	-346.54	1.8	-119.25	2.12	-40.94
144	145	55.60	-1696.97	-186.94	-314.50	0	-1344.80	1.8	-567.85	1.8	-177.90	2.12	-144.65
145	145	55.60	-2088.58	-186.76	-546.55	0	-2027.15	1.8	-342.46	1.8	-177.85	2.12	-144.55
145	146	57.00	-2088.58	-119.12	-341.67	0	-1798.18	1.8	-502.28	1.8	-217.24	2.12	-214.20
146	146	57.00	-1249.32	-115.42	-739.26	0	-1975.50	1.8	163.57	1.8	43.85	2.12	86.40
146	147	58.40	-1251.27	-91.56	-590.26	0	-1801.02	1.8	-12.15	1.8	30.25	2.12	59.61
147	147	58.40	-1608.20	-94.25	-789.30	0	-2387.74	1.8	142.76	1.8	30.49	2.12	58.63
147	148	59.80	-1608.20	-71.83	-673.12	0	-2256.92	1.8	11.87	1.8	19.39	2.12	37.28
148	148	59.80	-1608.20	-71.36	-673.05	0	-2256.87	1.8	11.86	1.8	19.38	2.12	37.26
148	149	61.20	-1608.20	-49.06	-588.77	0	-2164.08	1.8	-76.71	1.8	10.82	2.12	20.80
149	149	61.20	-1608.20	-48.58	-588.76	0	-2164.07	1.8	-76.71	1.8	10.82	2.12	20.80
149	150	62.60	-1608.20	-26.29	-536.33	0	-2109.26	1.8	-122.99	1.8	4.79	2.12	9.22
150	150	62.60	-1608.20	-25.84	-536.33	0	-2109.26	1.8	-122.99	1.8	4.79	2.12	9.22
150	151	64.00	-1609.94	-3.50	-515.82	0	-2093.95	1.8	-128.31	1.8	1.31	2.12	2.52
151	151	64.00	-1609.94	-3.04	-515.82	0	-2093.95	1.8	-128.31	1.8	1.31	2.12	2.52
151	152	65.40	-1609.94	23.68	-529.73	0	-2117.31	1.8	-89.36	1.8	0.79	2.12	1.52
152	152	65.40	-1609.94	24.13	-529.70	0	-2117.28	1.8	-89.36	1.8	0.78	2.12	1.51
152	153	66.80	-1609.94	47.56	-579.86	0	-2182.23	1.8	-7.26	1.8	3.54	2.12	6.81
153	153	66.80	-1609.94	48.01	-579.90	0	-2182.26	1.8	-7.26	1.8	3.55	2.12	6.82
153	154	68.20	-1609.94	70.27	-662.76	0	-2285.91	1.8	117.40	1.8	8.98	2.12	17.26
154	154	68.20	-1609.94	70.75	-662.81	0	-2285.95	1.8	117.41	1.8	8.99	2.12	17.28
154	155	69.60	-1609.94	93.17	-777.49	0	-2427.54	1.8	284.29	1.8	16.95	2.12	32.59
155	155	69.60	-1246.39	89.65	-578.45	0	-1831.37	1.8	134.94	1.8	16.82	2.12	33.15
155	156	71.00	-1242.90	112.78	-726.06	0	-2014.63	1.8	348.31	1.8	27.30	2.12	53.80
156	156	71.00	-2088.58	118.05	-328.50	0	-1780.32	1.8	-522.80	1.8	-218.49	2.12	-216.42
156	157	72.40	-2088.58	193.79	-531.41	0	-2006.36	1.8	-366.89	1.8	-179.19	2.12	-146.92
157	157	72.40	-1696.97	193.83	-299.24	0	-1323.89	1.8	-592.32	1.8	-179.27	2.12	-147.07
157	158	73.80	-1696.97	253.05	-610.16	0	-1665.01	1.8	-370.55	1.8	-116.92	2.12	-36.81
158	158	73.80	-2523.70	253.39	-212.08	0	-1534.41	1.8	-741.23	1.8	-438.86	2.12	-436.16
158	159	75.20	-2523.70	336.51	-614.95	0	-1975.04	1.8	-458.32	1.8	-357.51	2.12	-292.31
159	159	75.20	-2219.11	337.94	-425.51	0	-1429.96	1.8	-654.81	1.8	-357.51	2.12	-292.30
159	160	76.60	-2215.29	403.21	-943.56	0	-1991.43	1.8	-302.73	1.8	-250.27	2.12	-103.47
160	160	76.60	-2215.34	404.49	-943.58	0	-1991.47	1.8	-302.74	1.8	-250.27	2.12	-103.47
160	161	78.00	-2215.34	466.13	-1549.40	0	-2652.65	1.8	118.04	1.8	-127.36	2.12	113.87
161	1161	78.00	-2172.15	-445.47	-1520.65	0	-2572.16	1.8	85.83	1.8	-127.43	2.12	113.81
161	162	79.10	-2172.15	-394.96	-1061.84	0	-2078.75	1.8	-208.95	1.8	-223.50	2.12	-56.05
162	162	79.10	-2172.53	-393.99	-1061.91	0	-2078.93	1.8	-209.04	1.8	-223.58	2.12	-56.12
162	163	80.20	-2172.53	-323.42	-659.98	0	-1648.95	1.8	-459.91	1.8	-308.65	2.12	-206.54
163	163	80.20	-2477.65	-322.73	-852.65	0	-2199.21	1.8	-256.47	1.8	-308.75	2.12	-206.61
163	164	81.30	-2477.65	-266.08	-530.06	0	-1852.54	1.8	-462.94	1.8	-376.39	2.12	-326.21
164	164	81.30	-2478.35	-265.80	-530.26	0	-1852.95	1.8	-463.09	1.8	-376.52	2.12	-326.31
164	165	82.40	-2478.35	-215.85	-264.20	0	-1567.48	1.8	-631.90	1.8	-432.50	2.12	-425.28
165	165	82.40	-1870.06	-215.69	-794.87	0	-2083.69	1.8	-126.35	1.8	-110.93	2.12	-26.42
165	166	83.50	-1870.06	-188.16	-574.75	0	-1849.19	1.8	-260.53	1.8	-157.92	2.12	-109.51
166	166	83.50	-1871.02	-187.85	-574.53	0	-1822.80	1.8	-286.72	1.8	-180.67	2.12	-140.37
166	167	84.60	-1871.02	-143.25	-401.84	0	-1656.52	1.8	-370.46	1.8	-204.88	2.12	-188.67
167	167	84.60	-1016.26	-134.10	-799.42	0	-1853.60	1.8	409.08	1.8	50.27	2.12	99.05
167	168	85.70	-1019.75	-116.37	-652.64	0	-1684.49	1.8	235.08	1.8	36.83	2.12	72.58
168	168	85.70	-1261.85	-123.81	-783.56	0	-2068.81	1.8	328.37	1.8	37.13	2.12	71.39
168	169	86.80	-1261.85	-105.27	-657.03	0	-1925.91	1.8	184.55	1.8	25.14	2.12	48.34
169	169	86.80	-1261.85	-106.00	-657.00	0	-1925.88	1.8	184.55	1.8	25.13	2.12	48.33
169	170	87.90	-1261.85	-88.51	-549.99	0	-1806.32	1.8	66.78	1.8	14.69	2.12	28.25
170	170	87.90	-1261.85	-88.27	-549.99	0	-1806.32	1.8	66.78	1.8	14.69	2.12	28.25
170	171	89.00	-1261.85	-70.77	-462.51	0	-1710.09	1.8	-24.88	1.8	5.78	2.12	11.12

11/09/03



Combi_to.xls

TENSIONES EN ESTADOS COMBINADOS

TIEMPO inf

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-150.30	-86.06	0	-493.08	1.8	-30.80	1.8	-36.62	2.12	37.22
1	2	1.10	-395.79	-160.40	102.25	0	-341.68	1.8	-55.13	1.8	-64.37	2.12	-19.73
2	2	1.10	-624.09	-160.00	-5.89	0	-674.29	1.8	-70.87	1.8	-78.31	2.12	18.21
2	3	2.20	-624.09	-138.81	158.46	0	-538.16	1.8	-91.96	1.8	-102.04	2.12	-31.54
3	3	2.20	-624.08	-138.48	158.33	0	-538.27	1.8	-91.93	1.8	-102.02	2.12	-31.50
3	4	3.30	-624.08	-117.28	298.98	0	-421.56	1.8	-110.18	1.8	-122.39	2.12	-74.16
4	4	3.30	-787.15	-117.00	224.98	0	-656.63	1.8	-121.55	1.8	-132.77	2.12	-47.96
4	5	4.40	-787.15	-95.81	342.02	0	-559.26	1.8	-136.98	1.8	-149.79	2.12	-83.55
5	5	4.40	-787.15	-95.58	341.93	0	-559.34	1.8	-136.96	1.8	-149.77	2.12	-83.53
5	6	5.50	-787.15	-74.38	435.39	0	-481.29	1.8	-149.57	1.8	-163.45	2.12	-112.06
6	6	5.50	-950.22	-74.17	363.06	0	-715.05	1.8	-161.01	1.8	-174.03	2.12	-86.33
6	7	6.60	-950.22	-52.98	433.01	0	-656.27	1.8	-170.81	1.8	-184.37	2.12	-107.83
7	7	6.60	-950.22	-52.81	432.96	0	-545.88	1.8	-140.46	1.8	-174.28	2.12	-126.65
7	8	7.70	-950.22	-31.62	479.38	0	-512.08	1.8	-148.14	1.8	-181.63	2.12	-140.63
8	8	7.70	-950.22	-31.45	479.34	0	-512.11	1.8	-148.13	1.8	-181.63	2.12	-140.62
8	9	8.80	-950.22	-10.25	502.27	0	-494.26	1.8	-152.30	1.8	-185.20	2.12	-147.71
9	9	8.80	-950.22	-10.11	502.26	0	-494.27	1.8	-152.30	1.8	-185.20	2.12	-147.70
9	10	9.90	-950.22	11.08	501.72	0	-492.34	1.8	-152.97	1.8	-185.00	2.12	-147.89
10	10	9.90	-950.22	11.24	501.73	0	-492.33	1.8	-152.97	1.8	-185.00	2.12	-147.89
10	11	11.00	-950.22	32.43	477.71	0	-506.34	1.8	-150.13	1.8	-181.03	2.12	-141.17
11	11	11.00	-950.22	32.59	477.74	0	-506.32	1.8	-150.14	1.8	-181.04	2.12	-141.18
11	12	12.10	-950.22	53.79	430.22	0	-536.27	1.8	-143.79	1.8	-173.29	2.12	-127.56
12	12	12.10	-950.22	53.97	430.27	0	-536.24	1.8	-143.80	1.8	-173.30	2.12	-127.57
12	13	13.20	-950.22	75.17	359.24	0	-582.14	1.8	-133.94	1.8	-161.78	2.12	-107.04
13	13	13.20	-950.22	75.37	359.31	0	-582.09	1.8	-133.95	1.8	-161.79	2.12	-107.06
13	14	14.30	-950.22	96.58	264.73	0	-643.98	1.8	-120.57	1.8	-146.48	2.12	-79.60
14	14	14.30	-780.33	97.44	337.07	0	-515.88	1.8	-144.55	1.8	-149.31	2.12	-90.02
14	15	15.40	-775.77	116.17	217.35	0	-600.21	1.8	-128.93	1.8	-130.61	2.12	-54.79
15	15	15.40	-1554.62	118.63	588.73	0	-568.94	1.8	-345.28	1.8	-334.91	2.12	-301.46
15	16	16.50	-1554.62	107.68	451.69	0	-680.59	1.8	-329.98	1.8	-319.30	2.12	-265.19
16	16	16.50	-1554.62	107.85	451.74	0	-680.55	1.8	-329.98	1.8	-319.30	2.12	-265.20
16	17	17.60	-1554.62	124.89	323.40	0	-784.63	1.8	-316.48	1.8	-304.46	2.12	-230.99
17	17	17.60	-2163.46	125.07	768.95	0	-461.29	1.8	-541.65	1.8	-506.32	2.12	-521.24
17	18	18.70	-2163.46	142.10	622.01	0	-580.41	1.8	-526.46	1.8	-489.17	2.12	-481.88
18	18	18.70	-2163.46	142.30	622.06	0	-580.37	1.8	-526.47	1.8	-489.17	2.12	-481.90
18	19	19.80	-2163.46	159.34	456.16	0	-714.83	1.8	-509.56	1.8	-469.67	2.12	-437.28
19	19	19.80	-1935.17	159.55	564.21	0	-381.30	1.8	-494.33	1.8	-456.44	2.12	-475.98
19	20	20.90	-1935.17	176.58	379.33	0	-531.12	1.8	-475.71	1.8	-434.58	2.12	-426.10
20	20	20.90	-1935.17	176.81	379.34	0	-531.11	1.8	-475.71	1.8	-434.58	2.12	-426.10
20	21	22.00	-1935.17	195.21	174.72	0	-696.72	1.8	-455.52	1.8	-410.25	2.12	-370.74
21	1021	22.00	-1967.78	-218.67	158.30	0	-745.13	1.8	-457.65	1.8	-412.01	2.12	-364.93
21	22	23.40	-1967.78	-195.25	448.05	0	-509.89	1.8	-486.15	1.8	-446.99	2.12	-444.09
22	22	23.40	-1967.78	-194.97	448.01	0	-509.92	1.8	-486.15	1.8	-446.98	2.12	-444.08
22	23	24.80	-1967.78	-173.28	705.78	0	-300.26	1.8	-512.09	1.8	-477.96	2.12	-514.36
23	23	24.80	-2196.07	-173.01	599.99	0	-632.04	1.8	-527.43	1.8	-491.49	2.12	-476.31
23	24	26.20	-2196.07	-151.32	827.00	0	-447.26	1.8	-550.60	1.8	-518.65	2.12	-538.06
24	24	26.20	-1424.17	-151.10	455.66	0	-534.68	1.8	-314.41	1.8	-306.94	2.12	-274.59
24	25	27.60	-1424.17	-129.41	652.02	0	-374.69	1.8	-334.81	1.8	-330.29	2.12	-327.85
25	25	27.60	-1717.69	-129.21	524.80	0	-794.41	1.8	-354.92	1.8	-348.87	2.12	-281.46
25	26	29.00	-1717.69	-134.01	729.46	0	-626.96	1.8	-377.47	1.8	-372.83	2.12	-336.54
26	26	29.00	-941.07	-132.51	358.04	0	-653.66	1.8	-165.13	1.8	-170.62	2.12	-92.84
26	27	30.40	-945.20	-107.40	526.32	0	-528.26	1.8	-186.93	1.8	-196.31	2.12	-142.85
27	27	30.40	-1210.45	-106.35	418.41	0	-763.14	1.8	-165.55	1.8	-199.79	2.12	-125.73
27	28	31.80	-1210.45	-79.38	548.40	0	-675.94	1.8	-184.44	1.8	-220.78	2.12	-163.83
28	28	31.80	-1210.45	-79.18	548.31	0	-676.00	1.8	-184.43	1.8	-220.77	2.12	-163.80
28	29	33.20	-1210.45	-52.19	640.27	0	-614.61	1.8	-197.65	1.8	-235.66	2.12	-190.72
29	29	33.20	-1210.45	-52.05	640.20	0	-614.66	1.8	-197.63	1.8	-235.65	2.12	-190.70
29	30	34.60	-1210.45	-25.08	694.20	0	-579.02	1.8	-205.19	1.8	-244.44	2.12	-206.46
30	30	34.60	-1210.45	-24.92	694.16	0	-579.04	1.8	-205.18	1.8	-244.43	2.12	-206.45
30	31	36.00	-1210.45	2.05	710.18	0	-569.18	1.8	-207.06	1.8	-247.12	2.12	-211.05
31	31	36.00	-1210.45	2.17	710.19	0	-569.17	1.8	-207.06	1.8	-247.12	2.12	-211.06
31	32	37.40	-1210.45	29.14	688.24	0	-585.07	1.8	-203.28	1.8	-243.71	2.12	-204.50
32	32	37.40	-1210.45	29.29	688.29	0	-585.03	1.8	-203.28	1.8	-243.71	2.12	-204.51
32	33	38.80	-1210.45	56.26	628.40	0	-626.67	1.8	-193.84	1.8	-234.20	2.12	-186.81
33	33	38.80	-1210.45	56.44	628.48	0	-626.62	1.8	-193.85	1.8	-234.21	2.12	-186.83
33	34	40.20	-1210.45	83.42	530.57	0	-694.05	1.8	-178.72	1.8	-218.60	2.12	-157.94
34	34	40.20	-1210.45	83.60	530.67	0	-693.98	1.8	-178.74	1.8	-218.61	2.12	-157.97
34	35	41.60	-1210.45	110.57	394.75	0	-787.21	1.8	-157.94	1.8	-196.88	2.12	-117.92
35	35	41.60	-946.85	112.07	502.65	0	-567.02	1.8	-179.41	1.8	-193.40	2.12	-132.97
35	36	43.00	-942.63	137.30	327.33	0	-701.87	1.8	-155.77	1.8	-166.86	2.12	-80.39
36	36	43.00	-1717.69	138.42	698.77	0	-655.32	1.8	-372.79	1.8	-368.03	2.12	-326.34
36	37	44.40	-1717.69	132.64	496.16	0	-821.66	1.8	-350.34	1.8	-344.04	2.12	-271.38
37	37	44.40	-1424.17	132.85	623.37	0	-401.95	1.8	-330.23	1.8	-325.46	2.12	-317.78
37	38	45.80	-1424.17	154.53	422.24	0	-566.47	1.8	-309.06	1.8	-301.30	2.12	-262.84
38	38	45.80	-2196.07	154.77	793.59	0	-479.05	1.8	-545.25	1.8	-513.01	2.12	-526.31

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	176.45	561.74	0	-668.43	1.8	-521.30	1.8	-485.03	2.12	-462.86
39	39	47.20	-1967.78	176.72	667.52	0	-336.66	1.8	-505.97	1.8	-471.50	2.12	-500.91
39	40	48.60	-1974.23	197.90	405.55	0	-552.21	1.8	-480.94	1.8	-441.23	2.12	-430.52
40	40	48.60	-1974.41	198.19	405.65	0	-552.18	1.8	-481.00	1.8	-441.28	2.12	-430.58
40	41	50.00	-1974.41	221.63	111.78	0	-791.42	1.8	-451.81	1.8	-405.57	2.12	-349.92
41	1041	50.00	-1974.19	-221.72	111.79	0	-791.36	1.8	-451.76	1.8	-405.53	2.12	-349.87
41	42	51.40	-1974.19	-198.27	405.77	0	-552.02	1.8	-480.96	1.8	-441.25	2.12	-430.57
42	42	51.40	-1973.59	-197.98	405.68	0	-551.92	1.8	-480.80	1.8	-441.10	2.12	-430.41
42	43	52.80	-1973.59	-176.29	667.67	0	-338.18	1.8	-507.44	1.8	-472.82	2.12	-502.22
43	43	52.80	-2200.88	-176.09	561.78	0	-669.76	1.8	-522.51	1.8	-486.12	2.12	-463.92
43	44	54.20	-2196.07	-154.77	793.59	0	-479.05	1.8	-545.25	1.8	-513.01	2.12	-526.31
44	44	54.20	-1424.17	-154.53	422.23	0	-566.49	1.8	-309.06	1.8	-301.29	2.12	-262.84
44	45	55.60	-1424.17	-132.85	623.39	0	-401.93	1.8	-330.23	1.8	-325.46	2.12	-317.78
45	45	55.60	-1717.69	-132.64	496.18	0	-821.64	1.8	-350.34	1.8	-344.04	2.12	-271.39
45	46	57.00	-1717.69	-138.42	698.76	0	-655.33	1.8	-372.79	1.8	-368.03	2.12	-326.33
46	46	57.00	-942.63	-137.31	327.35	0	-701.86	1.8	-155.77	1.8	-166.86	2.12	-80.40
46	47	58.40	-945.05	-111.15	501.76	0	-566.13	1.8	-179.14	1.8	-192.99	2.12	-132.64
47	47	58.40	-1208.44	-110.63	393.85	0	-786.14	1.8	-157.64	1.8	-196.44	2.12	-117.57
47	48	59.80	-1208.44	-83.66	529.88	0	-692.84	1.8	-178.46	1.8	-218.19	2.12	-157.66
48	48	59.80	-1208.43	-83.46	529.79	0	-692.91	1.8	-178.44	1.8	-218.17	2.12	-157.63
48	49	61.20	-1208.43	-56.49	627.73	0	-625.45	1.8	-193.57	1.8	-233.80	2.12	-186.52
49	49	61.20	-1208.44	-56.32	627.67	0	-625.49	1.8	-193.56	1.8	-233.79	2.12	-186.51
49	50	62.60	-1208.44	-29.34	687.63	0	-583.81	1.8	-203.02	1.8	-243.32	2.12	-204.24
50	50	62.60	-1208.44	-29.20	687.59	0	-583.84	1.8	-203.01	1.8	-243.31	2.12	-204.22
50	51	64.00	-1206.69	-2.24	709.60	0	-566.46	1.8	-206.65	1.8	-246.49	2.12	-210.73
51	51	64.00	-1206.69	-2.12	709.61	0	-566.46	1.8	-206.65	1.8	-246.49	2.12	-210.73
51	52	65.40	-1206.69	24.85	693.71	0	-576.25	1.8	-204.78	1.8	-243.82	2.12	-206.17
52	52	65.40	-1206.69	25.00	693.72	0	-576.24	1.8	-204.78	1.8	-243.82	2.12	-206.17
52	53	66.80	-1206.69	51.97	639.87	0	-611.79	1.8	-197.25	1.8	-235.06	2.12	-190.45
53	53	66.80	-1206.69	52.12	639.93	0	-611.74	1.8	-197.26	1.8	-235.07	2.12	-190.47
53	54	68.20	-1206.69	79.10	548.09	0	-673.05	1.8	-184.06	1.8	-220.20	2.12	-163.58
54	54	68.20	-1206.69	79.30	548.19	0	-672.99	1.8	-184.07	1.8	-220.21	2.12	-163.61
54	55	69.60	-1206.69	106.27	418.29	0	-760.13	1.8	-165.18	1.8	-199.23	2.12	-125.54
55	55	69.60	-941.94	105.53	526.20	0	-525.66	1.8	-186.62	1.8	-195.82	2.12	-142.68
55	56	71.00	-941.07	132.52	358.05	0	-653.65	1.8	-165.13	1.8	-170.62	2.12	-92.84
56	56	71.00	-1717.69	134.02	729.47	0	-626.95	1.8	-377.47	1.8	-372.83	2.12	-336.54
56	57	72.40	-1717.69	129.21	524.81	0	-794.40	1.8	-354.92	1.8	-348.87	2.12	-281.46
57	57	72.40	-1424.17	129.41	652.01	0	-374.70	1.8	-334.81	1.8	-330.29	2.12	-327.85
57	58	73.80	-1424.17	151.10	455.65	0	-534.68	1.8	-314.41	1.8	-306.94	2.12	-274.59
58	58	73.80	-2196.08	151.34	826.99	0	-447.27	1.8	-550.60	1.8	-518.65	2.12	-538.06
58	59	75.20	-2196.08	173.02	599.98	0	-632.05	1.8	-527.43	1.8	-491.49	2.12	-476.31
59	59	75.20	-1967.78	173.28	705.78	0	-300.26	1.8	-512.09	1.8	-477.96	2.12	-514.36
59	60	76.60	-1971.61	194.49	448.53	0	-510.57	1.8	-487.17	1.8	-447.90	2.12	-445.05
60	60	76.60	-1971.55	194.75	448.65	0	-510.46	1.8	-487.17	1.8	-447.90	2.12	-445.07
60	61	78.00	-1971.55	218.17	159.60	0	-745.12	1.8	-458.76	1.8	-413.00	2.12	-366.10
61	1061	78.00	-1938.62	-195.06	176.06	0	-696.59	1.8	-456.55	1.8	-411.18	2.12	-371.85
61	62	79.10	-1938.62	-176.66	380.49	0	-531.13	1.8	-476.72	1.8	-435.49	2.12	-427.16
62	62	79.10	-1938.24	-176.43	380.48	0	-531.04	1.8	-476.62	1.8	-435.40	2.12	-427.08
62	63	80.20	-1938.24	-159.39	565.18	0	-381.37	1.8	-495.22	1.8	-457.24	2.12	-476.91
63	63	80.20	-2165.99	-159.17	457.12	0	-714.76	1.8	-510.32	1.8	-470.34	2.12	-438.09
63	64	81.30	-2165.99	-142.13	622.84	0	-580.45	1.8	-527.20	1.8	-489.83	2.12	-482.66
64	64	81.30	-2165.29	-141.95	622.73	0	-580.33	1.8	-527.01	1.8	-489.66	2.12	-482.48
64	65	82.40	-2165.29	-124.92	769.51	0	-461.34	1.8	-542.18	1.8	-506.79	2.12	-521.79
65	65	82.40	-1555.58	-124.79	324.19	0	-784.26	1.8	-316.80	1.8	-304.77	2.12	-231.42
65	66	83.50	-1555.58	-107.75	452.08	0	-680.54	1.8	-330.27	1.8	-319.56	2.12	-265.50
66	66	83.50	-1554.62	-107.67	451.94	0	-680.39	1.8	-330.01	1.8	-319.33	2.12	-265.25
66	67	84.60	-1554.62	-118.63	588.96	0	-568.74	1.8	-345.31	1.8	-334.94	2.12	-301.53
67	67	84.60	-775.78	-116.16	217.58	0	-600.07	1.8	-128.96	1.8	-130.65	2.12	-54.86
67	68	85.70	-776.65	-94.97	335.95	0	-513.59	1.8	-144.07	1.8	-148.60	2.12	-89.54
68	68	85.70	-945.78	-96.67	263.60	0	-641.08	1.8	-120.02	1.8	-145.66	2.12	-79.09
68	69	86.80	-945.78	-75.46	358.27	0	-579.13	1.8	-133.41	1.8	-160.98	2.12	-106.57
69	69	86.80	-945.79	-75.25	358.20	0	-579.18	1.8	-133.40	1.8	-160.97	2.12	-106.55
69	70	87.90	-945.79	-54.05	429.31	0	-533.22	1.8	-143.27	1.8	-172.51	2.12	-127.11
70	70	87.90	-945.79	-53.87	429.26	0	-533.26	1.8	-143.26	1.8	-172.50	2.12	-127.09
70	71	89.00	-945.79	-32.68	476.87	0	-503.25	1.8	-149.62	1.8	-180.26	2.12	-140.74
71	71	89.00	-945.79	-32.53	476.85	0	-503.26	1.8	-149.62	1.8	-180.26	2.12	-140.74
71	72	90.10	-945.79	-11.33	500.97	0	-489.19	1.8	-152.47	1.8	-184.25	2.12	-147.46
72	72	90.10	-945.79	-11.17	500.94	0	-489.21	1.8	-152.47	1.8	-184.24	2.12	-147.47
72	73	91.20	-945.79	10.02	501.56	0	-491.08	1.8	-151.81	1.8	-184.45	2.12	-147.31
73	73	91.20	-945.79	10.16	501.58	0	-491.07	1.8	-151.81	1.8	-184.46	2.12	-147.32
73	74	92.30	-945.79	31.36	478.73	0	-508.87	1.8	-147.65	1.8	-180.90	2.12	-140.26
74	74	92.30	-945.79	31.53	478.76	0	-508.85	1.8	-147.65	1.8	-180.90	2.12	-140.27
74	75	93.40	-945.79	52.72	432.43	0	-542.58	1.8	-139.98	1.8	-173.57	2.12	-126.31
75	75	93.40	-945.79	52.89	432.50	0	-652.39	1.8	-170.31	1.8	-183.67	2.12	-107.63
75	76	94.50	-945.79	74.08	362.62	0	-711.12	1.8	-160.51	1.8	-173.34	2.12	-86.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	74.30	434.96	0	-477.35	1.8	-149.08	1.8	-162.76	2.12	-111.88
76	77	95.60	-782.72	95.50	341.58	0	-555.33	1.8	-136.47	1.8	-149.09	2.12	-83.37
77	77	95.60	-782.72	95.72	341.69	0	-555.24	1.8	-136.49	1.8	-149.11	2.12	-83.40
77	78	96.70	-782.72	116.91	224.72	0	-652.55	1.8	-121.06	1.8	-132.10	2.12	-47.83
78	78	96.70	-619.65	117.20	298.74	0	-417.47	1.8	-109.70	1.8	-121.73	2.12	-74.03
78	79	97.80	-619.65	138.39	158.15	0	-534.13	1.8	-91.45	1.8	-101.36	2.12	-31.39
79	79	97.80	-619.65	138.73	158.28	0	-534.02	1.8	-91.47	1.8	-101.38	2.12	-31.43
79	80	98.90	-619.65	159.93	-5.98	0	-670.08	1.8	-70.39	1.8	-77.66	2.12	18.30
80	80	98.90	-391.36	160.31	102.16	0	-337.47	1.8	-54.65	1.8	-63.72	2.12	-19.65
80	81	100.00	-391.36	150.29	-86.06	0	-493.08	1.8	-30.80	1.8	-36.62	2.12	37.22
101	101	0.00	-391.36	-169.52	-85.96	0	-493.00	1.8	-30.82	1.8	-36.63	2.12	37.19
101	102	1.10	-395.79	-149.14	89.34	0	-352.52	1.8	-52.98	1.8	-62.44	2.12	-15.74
102	102	1.10	-624.09	-149.53	-18.53	0	-684.91	1.8	-68.77	1.8	-76.42	2.12	22.11
102	103	2.20	-624.09	-129.52	134.95	0	-557.92	1.8	-88.05	1.8	-98.54	2.12	-24.28
103	103	2.20	-624.08	-129.85	135.08	0	-557.80	1.8	-88.07	1.8	-98.56	2.12	-24.32
103	104	3.30	-624.08	-109.86	266.89	0	-448.52	1.8	-104.86	1.8	-117.61	2.12	-64.24
104	104	3.30	-787.15	-110.12	193.12	0	-683.39	1.8	-116.26	1.8	-128.02	2.12	-38.12
104	105	4.40	-787.15	-90.15	303.29	0	-591.80	1.8	-130.55	1.8	-144.02	2.12	-71.59
105	105	4.40	-787.15	-90.39	303.37	0	-591.73	1.8	-130.56	1.8	-144.03	2.12	-71.61
105	106	5.50	-787.15	-70.40	391.79	0	-517.91	1.8	-142.33	1.8	-156.95	2.12	-98.59
106	106	5.50	-950.22	-70.59	319.61	0	-751.55	1.8	-153.79	1.8	-167.56	2.12	-72.91
106	107	6.60	-950.22	-50.61	386.28	0	-695.52	1.8	-163.05	1.8	-177.41	2.12	-93.39
107	107	6.60	-950.22	-50.78	386.33	0	-578.43	1.8	-132.43	1.8	-167.10	2.12	-112.98
107	108	7.70	-950.22	-30.80	431.17	0	-545.73	1.8	-139.84	1.8	-174.21	2.12	-126.51
108	108	7.70	-950.22	-30.95	431.21	0	-545.71	1.8	-139.85	1.8	-174.21	2.12	-126.52
108	109	8.80	-950.22	-10.96	454.25	0	-527.78	1.8	-144.04	1.8	-177.81	2.12	-133.63
109	109	8.80	-950.22	-11.10	454.25	0	-527.78	1.8	-144.04	1.8	-177.81	2.12	-133.63
109	110	9.90	-950.22	8.88	455.48	0	-524.62	1.8	-145.01	1.8	-177.88	2.12	-134.34
110	110	9.90	-950.22	8.73	455.47	0	-524.62	1.8	-145.01	1.8	-177.88	2.12	-134.34
110	111	11.00	-950.22	28.71	434.87	0	-536.24	1.8	-142.76	1.8	-174.44	2.12	-128.62
111	111	11.00	-950.22	28.57	434.83	0	-536.27	1.8	-142.75	1.8	-174.43	2.12	-128.61
111	112	12.10	-950.22	48.55	392.41	0	-562.66	1.8	-137.28	1.8	-167.47	2.12	-116.48
112	112	12.10	-950.22	48.38	392.35	0	-562.71	1.8	-137.27	1.8	-167.46	2.12	-116.46
112	113	13.20	-950.22	68.37	328.15	0	-603.85	1.8	-128.59	1.8	-156.99	2.12	-97.93
113	113	13.20	-950.22	68.17	328.08	0	-603.89	1.8	-128.58	1.8	-156.98	2.12	-97.91
113	114	14.30	-950.22	88.16	242.09	0	-659.79	1.8	-116.68	1.8	-143.00	2.12	-72.97
114	114	14.30	-780.33	88.59	314.28	0	-535.03	1.8	-140.76	1.8	-145.91	2.12	-82.98
114	115	15.40	-775.77	106.10	204.95	0	-610.63	1.8	-126.87	1.8	-128.76	2.12	-50.96
115	115	15.40	-1554.62	108.03	576.14	0	-579.36	1.8	-343.69	1.8	-333.49	2.12	-298.13
115	116	16.50	-1554.62	101.32	451.55	0	-680.71	1.8	-329.96	1.8	-319.28	2.12	-265.15
116	116	16.50	-1554.62	101.17	451.50	0	-680.75	1.8	-329.95	1.8	-319.28	2.12	-265.14
116	117	17.60	-1554.62	117.57	330.87	0	-778.44	1.8	-317.42	1.8	-305.30	2.12	-232.97
117	117	17.60	-2163.46	117.38	776.32	0	-455.19	1.8	-542.58	1.8	-507.15	2.12	-523.20
117	118	18.70	-2163.46	133.76	638.20	0	-567.01	1.8	-528.50	1.8	-491.00	2.12	-486.17
118	118	18.70	-2163.46	133.56	638.15	0	-567.05	1.8	-528.49	1.8	-490.99	2.12	-486.16
118	119	19.80	-2163.46	149.95	482.22	0	-693.26	1.8	-512.85	1.8	-472.61	2.12	-444.18
119	119	19.80	-1935.17	149.73	590.20	0	-359.79	1.8	-497.60	1.8	-459.38	2.12	-482.86
119	120	20.90	-1935.17	166.12	416.48	0	-500.36	1.8	-480.39	1.8	-438.78	2.12	-435.94
120	120	20.90	-1935.17	165.89	416.47	0	-500.37	1.8	-480.39	1.8	-438.78	2.12	-435.94
120	121	22.00	-1935.17	183.66	224.20	0	-655.75	1.8	-461.75	1.8	-415.84	2.12	-383.85
121	1121	22.00	-1967.78	-207.35	207.79	0	-704.16	1.8	-463.88	1.8	-417.60	2.12	-378.05
121	122	23.40	-1967.78	-184.74	482.23	0	-481.59	1.8	-490.46	1.8	-450.85	2.12	-453.15
122	122	23.40	-1967.78	-185.02	482.27	0	-481.56	1.8	-490.46	1.8	-450.85	2.12	-453.16
122	123	24.80	-1967.78	-164.17	726.70	0	-282.94	1.8	-514.73	1.8	-480.32	2.12	-519.90
123	123	24.80	-2196.07	-164.43	621.04	0	-614.60	1.8	-530.08	1.8	-493.87	2.12	-481.89
123	124	26.20	-2196.07	-143.57	836.62	0	-439.30	1.8	-551.81	1.8	-519.74	2.12	-540.61
124	124	26.20	-1424.17	-143.80	465.41	0	-526.61	1.8	-315.64	1.8	-308.04	2.12	-277.18
124	125	27.60	-1424.17	-122.93	652.12	0	-374.61	1.8	-334.83	1.8	-330.30	2.12	-327.88
125	125	27.60	-1717.69	-123.12	525.04	0	-794.21	1.8	-354.95	1.8	-348.90	2.12	-281.52
125	126	29.00	-1717.69	-124.25	715.17	0	-638.79	1.8	-375.67	1.8	-371.21	2.12	-332.75
126	126	29.00	-941.08	-123.35	344.03	0	-665.43	1.8	-162.81	1.8	-168.53	2.12	-88.51
126	127	30.40	-945.21	-99.77	500.53	0	-549.92	1.8	-182.65	1.8	-192.46	2.12	-134.88
127	127	30.40	-1210.45	-99.20	392.85	0	-780.98	1.8	-161.15	1.8	-195.85	2.12	-118.24
127	128	31.80	-1210.45	-73.75	513.91	0	-700.01	1.8	-178.51	1.8	-215.47	2.12	-153.72
128	128	31.80	-1210.45	-73.94	514.01	0	-699.95	1.8	-178.53	1.8	-215.49	2.12	-153.75
128	129	33.20	-1210.45	-48.51	599.71	0	-642.92	1.8	-190.67	1.8	-229.41	2.12	-178.84
129	129	33.20	-1210.45	-48.66	599.78	0	-642.87	1.8	-190.68	1.8	-229.42	2.12	-178.86
129	130	34.60	-1210.45	-23.21	650.07	0	-609.82	1.8	-197.60	1.8	-237.64	2.12	-193.53
130	130	34.60	-1210.45	-23.35	650.10	0	-609.80	1.8	-197.60	1.8	-237.65	2.12	-193.54
130	131	36.00	-1210.45	2.10	664.98	0	-600.73	1.8	-199.29	1.8	-240.16	2.12	-197.81
131	131	36.00	-1210.45	1.96	664.98	0	-600.73	1.8	-199.29	1.8	-240.16	2.12	-197.81
131	132	37.40	-1210.45	27.41	644.40	0	-615.67	1.8	-195.74	1.8	-236.95	2.12	-191.65
132	132	37.40	-1210.45	27.27	644.37	0	-615.69	1.8	-195.73	1.8	-236.95	2.12	-191.64
132	133	38.80	-1210.45	52.73	588.38	0	-654.60	1.8	-186.95	1.8	-228.04	2.12	-175.08
133	133	38.80	-1210.45	52.56	588.32	0	-654.65	1.8	-186.94	1.8	-228.03	2.12	-175.06

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	78.00	496.93	0	-717.53	1.8	-172.94	1.8	-213.41	2.12	-148.09
134	134	40.20	-1210.45	77.81	496.84	0	-717.59	1.8	-172.92	1.8	-213.40	2.12	-148.06
134	135	41.60	-1210.45	103.25	370.09	0	-804.43	1.8	-153.69	1.8	-193.08	2.12	-110.69
135	135	41.60	-946.85	104.23	477.77	0	-587.92	1.8	-175.28	1.8	-189.69	2.12	-125.28
135	136	43.00	-942.63	127.92	314.50	0	-712.64	1.8	-153.64	1.8	-164.95	2.12	-76.43
136	136	43.00	-1717.69	128.42	685.65	0	-666.18	1.8	-371.14	1.8	-366.55	2.12	-322.86
136	137	44.40	-1717.69	126.43	497.24	0	-820.76	1.8	-350.47	1.8	-344.16	2.12	-271.67
137	137	44.40	-1424.16	126.22	624.30	0	-401.18	1.8	-330.34	1.8	-325.56	2.12	-318.02
137	138	45.80	-1424.16	147.08	432.99	0	-557.57	1.8	-310.41	1.8	-302.51	2.12	-265.69
138	138	45.80	-2196.07	146.85	804.21	0	-470.26	1.8	-546.59	1.8	-514.21	2.12	-529.12
138	139	47.20	-2196.07	167.69	584.03	0	-649.97	1.8	-524.11	1.8	-487.55	2.12	-468.77
139	139	47.20	-1967.78	167.43	689.69	0	-318.30	1.8	-508.76	1.8	-474.01	2.12	-506.78
139	140	48.60	-1974.23	187.80	441.29	0	-522.62	1.8	-485.45	1.8	-445.27	2.12	-439.99
140	140	48.60	-1974.41	187.50	441.33	0	-522.64	1.8	-485.50	1.8	-445.31	2.12	-440.04
140	141	50.00	-1974.41	210.12	163.01	0	-749.00	1.8	-458.27	1.8	-411.36	2.12	-363.50
141	1141	50.00	-1974.19	-210.19	163.02	0	-748.94	1.8	-458.22	1.8	-411.31	2.12	-363.45
141	142	51.40	-1974.19	-187.58	441.45	0	-522.47	1.8	-485.46	1.8	-445.28	2.12	-440.02
142	142	51.40	-1973.59	-187.88	441.43	0	-522.32	1.8	-485.31	1.8	-445.14	2.12	-439.89
142	143	52.80	-1973.59	-167.01	689.84	0	-319.83	1.8	-510.23	1.8	-475.33	2.12	-508.10
143	143	52.80	-2200.88	-167.34	584.06	0	-651.30	1.8	-525.32	1.8	-488.64	2.12	-469.83
143	144	54.20	-2196.07	-146.85	804.18	0	-470.28	1.8	-546.58	1.8	-514.20	2.12	-529.12
144	144	54.20	-1424.17	-147.09	432.97	0	-557.59	1.8	-310.41	1.8	-302.51	2.12	-265.68
144	145	55.60	-1424.17	-126.23	624.29	0	-401.18	1.8	-330.34	1.8	-325.56	2.12	-318.02
145	145	55.60	-1717.69	-126.43	497.24	0	-820.77	1.8	-350.47	1.8	-344.16	2.12	-271.67
145	146	57.00	-1717.69	-128.42	685.64	0	-666.19	1.8	-371.14	1.8	-366.54	2.12	-322.86
146	146	57.00	-942.63	-127.93	314.50	0	-712.65	1.8	-153.64	1.8	-164.95	2.12	-76.43
146	147	58.40	-945.05	-103.32	476.88	0	-587.04	1.8	-175.01	1.8	-189.28	2.12	-124.95
147	147	58.40	-1208.44	-103.30	369.21	0	-803.35	1.8	-153.40	1.8	-192.65	2.12	-110.35
147	148	59.80	-1208.44	-77.86	496.02	0	-716.48	1.8	-172.64	1.8	-212.98	2.12	-147.74
148	148	59.80	-1208.45	-78.06	496.11	0	-716.41	1.8	-172.65	1.8	-212.99	2.12	-147.76
148	149	61.20	-1208.45	-52.62	587.57	0	-653.49	1.8	-186.67	1.8	-227.62	2.12	-174.76
149	149	61.20	-1208.44	-52.78	587.63	0	-653.44	1.8	-186.68	1.8	-227.63	2.12	-174.77
149	150	62.60	-1208.44	-27.33	643.72	0	-614.46	1.8	-195.47	1.8	-236.55	2.12	-191.37
150	150	62.60	-1208.44	-27.47	643.77	0	-614.43	1.8	-195.48	1.8	-236.56	2.12	-191.38
150	151	64.00	-1206.69	-2.04	664.42	0	-598.01	1.8	-198.87	1.8	-239.53	2.12	-197.49
151	151	64.00	-1206.69	-2.18	664.41	0	-598.01	1.8	-198.87	1.8	-239.53	2.12	-197.49
151	152	65.40	-1206.69	23.27	649.64	0	-607.01	1.8	-197.20	1.8	-237.04	2.12	-193.25
152	152	65.40	-1206.69	23.13	649.61	0	-607.03	1.8	-197.19	1.8	-237.03	2.12	-193.25
152	153	66.80	-1206.69	48.57	599.44	0	-640.01	1.8	-190.29	1.8	-228.83	2.12	-178.60
153	153	66.80	-1206.69	48.43	599.37	0	-640.05	1.8	-190.28	1.8	-228.82	2.12	-178.58
153	154	68.20	-1206.69	73.86	513.77	0	-697.01	1.8	-178.15	1.8	-214.91	2.12	-153.53
154	154	68.20	-1206.69	73.66	513.68	0	-697.07	1.8	-178.14	1.8	-214.90	2.12	-153.50
154	155	69.60	-1206.69	99.11	392.75	0	-777.96	1.8	-160.79	1.8	-195.30	2.12	-118.05
155	155	69.60	-941.94	97.89	500.41	0	-547.32	1.8	-182.34	1.8	-191.98	2.12	-134.71
155	156	71.00	-941.07	123.34	344.03	0	-665.42	1.8	-162.80	1.8	-168.53	2.12	-88.51
156	156	71.00	-1717.69	124.24	715.19	0	-638.77	1.8	-375.67	1.8	-371.22	2.12	-332.76
156	157	72.40	-1717.69	123.13	525.06	0	-794.19	1.8	-354.95	1.8	-348.90	2.12	-281.52
157	157	72.40	-1424.17	122.93	652.12	0	-374.61	1.8	-334.83	1.8	-330.30	2.12	-327.87
157	158	73.80	-1424.17	143.81	465.41	0	-526.60	1.8	-315.64	1.8	-308.04	2.12	-277.18
158	158	73.80	-2196.07	143.58	836.61	0	-439.30	1.8	-551.81	1.8	-519.73	2.12	-540.61
158	159	75.20	-2196.07	164.42	621.03	0	-614.62	1.8	-530.08	1.8	-493.87	2.12	-481.88
159	159	75.20	-1967.78	164.16	726.71	0	-282.94	1.8	-514.73	1.8	-480.32	2.12	-519.90
159	160	76.60	-1971.61	184.55	482.79	0	-482.20	1.8	-491.49	1.8	-451.77	2.12	-454.13
160	160	76.60	-1971.55	184.24	482.84	0	-482.15	1.8	-491.48	1.8	-451.76	2.12	-454.13
160	161	78.00	-1971.55	206.86	209.08	0	-704.15	1.8	-464.99	1.8	-418.59	2.12	-379.21
161	1161	78.00	-1938.62	-183.51	225.53	0	-655.62	1.8	-462.78	1.8	-416.77	2.12	-384.96
161	162	79.10	-1938.62	-165.75	417.61	0	-500.40	1.8	-481.40	1.8	-439.68	2.12	-437.00
162	162	79.10	-1938.23	-165.96	417.62	0	-500.28	1.8	-481.30	1.8	-439.60	2.12	-436.92
162	163	80.20	-1938.23	-149.58	591.18	0	-359.84	1.8	-498.49	1.8	-460.18	2.12	-483.80
163	163	80.20	-2165.99	-149.79	483.17	0	-693.18	1.8	-513.60	1.8	-473.29	2.12	-444.99
163	164	81.30	-2165.99	-133.40	638.92	0	-567.12	1.8	-529.22	1.8	-491.65	2.12	-486.92
164	164	81.30	-2165.29	-133.61	638.91	0	-566.93	1.8	-529.05	1.8	-491.49	2.12	-486.76
164	165	82.40	-2165.29	-117.23	776.87	0	-455.25	1.8	-543.11	1.8	-507.63	2.12	-523.75
165	165	82.40	-1555.58	-117.46	331.66	0	-778.07	1.8	-317.74	1.8	-305.61	2.12	-233.40
165	166	83.50	-1555.58	-101.06	451.83	0	-680.74	1.8	-330.24	1.8	-319.53	2.12	-265.43
166	166	83.50	-1554.62	-101.31	451.78	0	-680.52	1.8	-329.99	1.8	-319.31	2.12	-265.21
166	167	84.60	-1554.62	-108.02	576.38	0	-579.16	1.8	-343.72	1.8	-333.52	2.12	-298.19
167	167	84.60	-775.78	-106.08	205.18	0	-610.48	1.8	-126.90	1.8	-128.81	2.12	-51.03
167	168	85.70	-776.65	-86.11	313.13	0	-532.76	1.8	-140.28	1.8	-145.20	2.12	-82.49
168	168	85.70	-945.79	-88.24	240.96	0	-656.89	1.8	-116.13	1.8	-142.18	2.12	-72.45
168	169	86.80	-945.79	-68.25	327.04	0	-600.93	1.8	-128.04	1.8	-156.17	2.12	-97.42
169	169	86.80	-945.79	-68.46	327.10	0	-600.89	1.8	-128.05	1.8	-156.19	2.12	-97.44
169	170	87.90	-945.79	-48.47	391.40	0	-559.68	1.8	-136.75	1.8	-166.67	2.12	-116.00
170	170	87.90	-945.79	-48.63	391.45	0	-559.65	1.8	-136.76	1.8	-166.68	2.12	-116.02
170	171	89.00	-945.79	-28.66	433.97	0	-533.19	1.8	-142.24	1.8	-173.66	2.12	-128.17

CÁLCULO TENSIONAL

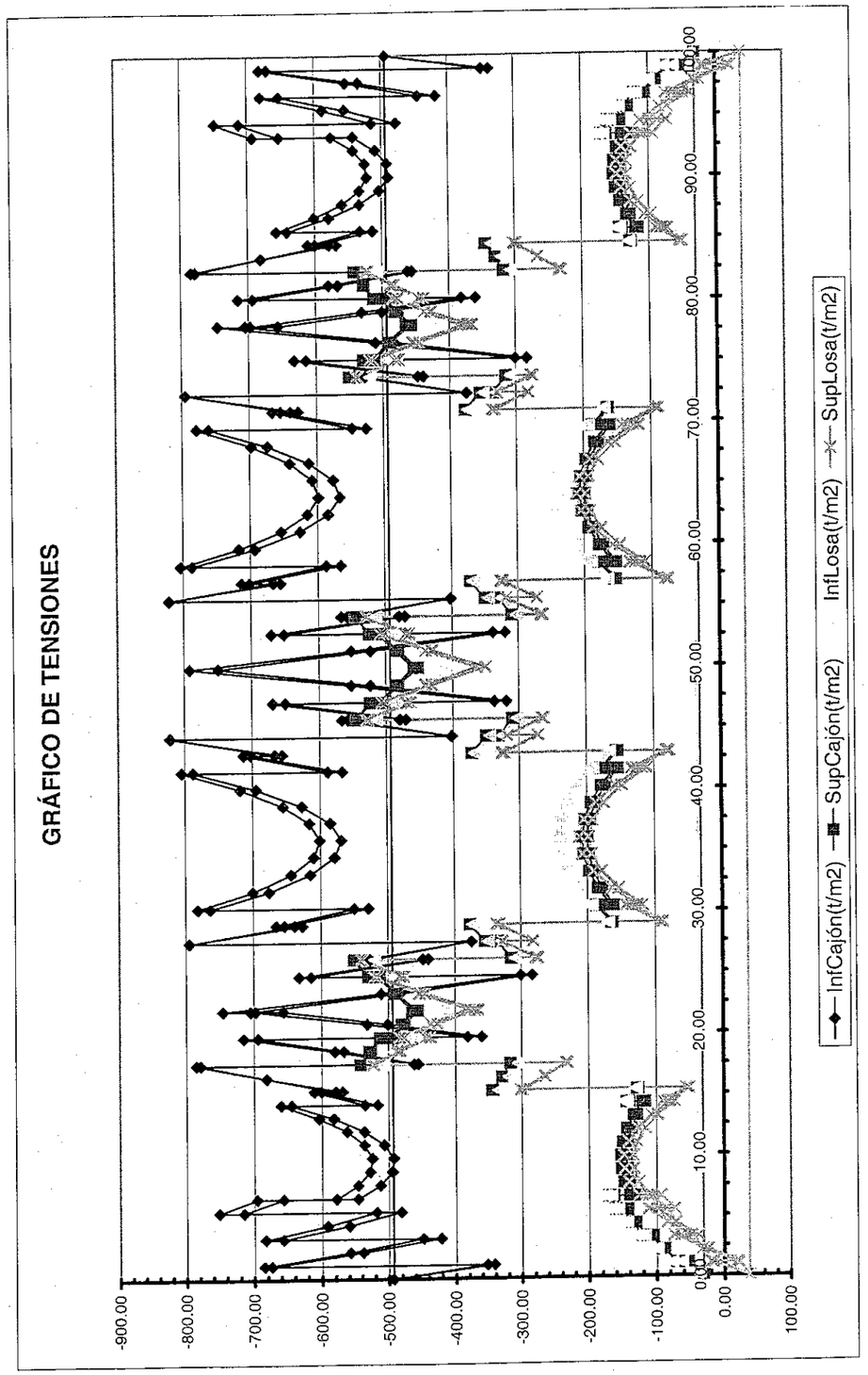
Hipótesis de cálculo:
PERM1.Tinf.MZ+

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-28.82	434.01	0	-533.16	1.8	-142.25	1.8	-173.66	2.12	-128.18
171	172	90.10	-945.79	-8.82	454.69	0	-521.49	1.8	-144.51	1.8	-177.12	2.12	-133.92
172	172	90.10	-945.79	-8.96	454.70	0	-521.49	1.8	-144.51	1.8	-177.12	2.12	-133.92
172	173	91.20	-945.79	11.02	453.55	0	-524.59	1.8	-143.55	1.8	-177.06	2.12	-133.25
173	173	91.20	-945.79	10.86	453.55	0	-524.59	1.8	-143.55	1.8	-177.06	2.12	-133.25
173	174	92.30	-945.79	30.86	430.60	0	-542.46	1.8	-139.37	1.8	-173.48	2.12	-126.16
174	174	92.30	-945.79	30.71	430.56	0	-542.49	1.8	-139.36	1.8	-173.48	2.12	-126.15
174	175	93.40	-945.79	50.69	385.80	0	-575.12	1.8	-131.96	1.8	-166.39	2.12	-112.65
175	175	93.40	-945.79	50.52	385.76	0	-691.65	1.8	-162.55	1.8	-176.71	2.12	-93.19
175	176	94.50	-945.79	70.50	319.16	0	-747.64	1.8	-153.29	1.8	-166.87	2.12	-72.72
176	176	94.50	-782.72	70.31	391.36	0	-513.98	1.8	-141.84	1.8	-156.26	2.12	-98.41
176	177	95.60	-782.72	90.30	303.03	0	-587.72	1.8	-130.07	1.8	-143.35	2.12	-71.45
177	177	95.60	-782.72	90.06	302.93	0	-587.80	1.8	-130.06	1.8	-143.34	2.12	-71.43
177	178	96.70	-782.72	110.04	192.85	0	-679.32	1.8	-115.77	1.8	-127.35	2.12	-37.98
178	178	96.70	-619.65	109.77	266.64	0	-444.44	1.8	-104.37	1.8	-116.95	2.12	-64.11
178	179	97.80	-619.65	129.76	134.90	0	-553.67	1.8	-87.59	1.8	-97.90	2.12	-24.21
179	179	97.80	-619.66	129.44	134.77	0	-553.78	1.8	-87.57	1.8	-97.88	2.12	-24.17
179	180	98.90	-619.66	149.45	-18.63	0	-680.71	1.8	-68.29	1.8	-75.78	2.12	22.20
180	180	98.90	-391.36	149.05	89.27	0	-348.30	1.8	-52.51	1.8	-61.80	2.12	-15.67
180	181	100.00	-391.36	169.51	-85.96	0	-493.00	1.8	-30.82	1.8	-36.63	2.12	37.19



CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-181.97	-104.92	0	-556.08	1.8	-34.92	1.8	-41.22	2.12	41.98
1	2	1.10	-436.66	-131.70	49.60	0	-424.43	1.8	-52.83	1.8	-62.69	2.12	-4.44
2	2	1.10	-693.96	-131.49	-76.81	0	-799.56	1.8	-70.54	1.8	-78.35	2.12	38.37
2	3	2.20	-693.96	-114.45	58.46	0	-687.79	1.8	-86.94	1.8	-97.77	2.12	-2.43
3	3	2.20	-693.96	-114.28	58.39	0	-687.85	1.8	-86.93	1.8	-97.76	2.12	-2.40
3	4	3.30	-693.96	-97.23	174.71	0	-591.52	1.8	-101.27	1.8	-114.53	2.12	-37.57
4	4	3.30	-877.74	-97.08	88.07	0	-856.62	1.8	-114.07	1.8	-126.18	2.12	-8.02
4	5	4.40	-877.74	-80.05	185.49	0	-775.67	1.8	-126.38	1.8	-140.30	2.12	-37.58
5	5	4.40	-877.74	-79.93	185.45	0	-775.71	1.8	-126.37	1.8	-140.29	2.12	-37.56
5	6	5.50	-877.74	-62.89	263.98	0	-710.14	1.8	-136.64	1.8	-151.77	2.12	-61.51
6	6	5.50	-1061.53	-62.77	179.21	0	-973.78	1.8	-149.51	1.8	-163.66	2.12	-32.49
6	7	6.60	-1061.53	-45.74	238.91	0	-923.54	1.8	-157.75	1.8	-172.49	2.12	-50.85
7	7	6.60	-1061.53	-45.65	238.88	0	-769.75	1.8	-120.89	1.8	-159.15	2.12	-74.20
7	8	7.70	-1061.53	-28.62	279.72	0	-739.81	1.8	-127.68	1.8	-165.62	2.12	-86.55
8	8	7.70	-1061.53	-28.53	279.69	0	-739.83	1.8	-127.67	1.8	-165.62	2.12	-86.54
8	9	8.80	-1061.53	-11.49	301.70	0	-722.56	1.8	-131.75	1.8	-169.03	2.12	-93.36
9	9	8.80	-1061.54	-11.41	301.69	0	-722.57	1.8	-131.75	1.8	-169.03	2.12	-93.35
9	10	9.90	-1061.54	5.62	304.86	0	-717.99	1.8	-133.13	1.8	-169.38	2.12	-94.62
10	10	9.90	-1061.53	5.71	304.87	0	-717.98	1.8	-133.13	1.8	-169.38	2.12	-94.63
10	11	11.00	-1061.53	22.74	289.22	0	-726.09	1.8	-131.79	1.8	-166.68	2.12	-90.36
11	11	11.00	-1061.53	22.83	289.23	0	-726.08	1.8	-131.80	1.8	-166.69	2.12	-90.36
11	12	12.10	-1061.53	39.87	254.74	0	-746.89	1.8	-127.75	1.8	-160.93	2.12	-80.55
12	12	12.10	-1061.53	39.96	254.77	0	-746.87	1.8	-127.76	1.8	-160.93	2.12	-80.56
12	13	13.20	-1061.53	57.01	201.42	0	-780.37	1.8	-121.01	1.8	-152.11	2.12	-65.21
13	13	13.20	-1061.53	57.12	201.46	0	-780.34	1.8	-121.01	1.8	-152.12	2.12	-65.22
13	14	14.30	-1061.53	74.17	129.25	0	-826.56	1.8	-111.55	1.8	-140.24	2.12	-44.31
14	14	14.30	-871.84	69.64	214.03	0	-703.29	1.8	-139.93	1.8	-144.53	2.12	-54.30
14	15	15.40	-874.66	89.13	124.25	0	-768.82	1.8	-129.89	1.8	-131.37	2.12	-28.61
15	15	15.40	-1567.05	91.64	453.73	0	-750.42	1.8	-320.29	1.8	-313.39	2.12	-246.83
15	16	16.50	-1567.05	140.81	338.46	0	-844.05	1.8	-307.74	1.8	-300.24	2.12	-216.32
16	16	16.50	-1567.05	141.12	338.55	0	-843.97	1.8	-307.75	1.8	-300.25	2.12	-216.34
16	17	17.60	-1567.05	162.32	171.29	0	-980.28	1.8	-289.35	1.8	-281.00	2.12	-171.82
17	17	17.60	-2068.15	162.66	587.74	0	-636.83	1.8	-486.07	1.8	-457.37	2.12	-435.31
17	18	18.70	-2068.15	183.85	397.17	0	-792.08	1.8	-465.38	1.8	-435.29	2.12	-384.39
18	18	18.70	-2068.15	184.21	397.25	0	-792.01	1.8	-465.39	1.8	-435.30	2.12	-384.41
18	19	19.80	-2068.15	205.41	182.96	0	-966.54	1.8	-442.39	1.8	-410.33	2.12	-326.97
19	19	19.80	-1810.85	205.81	309.37	0	-590.43	1.8	-425.20	1.8	-395.39	2.12	-370.56
19	20	20.90	-1810.85	226.99	71.31	0	-784.28	1.8	-399.88	1.8	-367.52	2.12	-306.59
20	20	20.90	-1810.85	227.42	71.34	0	-784.26	1.8	-399.89	1.8	-367.53	2.12	-306.60
20	21	22.00	-1810.85	249.98	-191.24	0	-997.86	1.8	-372.39	1.8	-336.65	2.12	-235.88
21	1021	22.00	-1847.60	-272.91	-210.41	0	-1052.45	1.8	-374.79	1.8	-338.63	2.12	-229.33
21	22	23.40	-1847.60	-244.19	151.57	0	-757.40	1.8	-412.40	1.8	-381.77	2.12	-327.63
22	22	23.40	-1847.60	-243.67	151.50	0	-757.46	1.8	-412.39	1.8	-381.76	2.12	-327.61
22	23	24.80	-1847.60	-216.70	473.75	0	-494.41	1.8	-446.46	1.8	-420.02	2.12	-414.98
23	23	24.80	-2104.90	-216.19	349.87	0	-868.56	1.8	-463.76	1.8	-435.30	2.12	-372.11
23	24	26.20	-2104.90	-189.22	633.64	0	-636.78	1.8	-494.08	1.8	-468.87	2.12	-448.91
24	24	26.20	-1420.02	-188.80	304.09	0	-714.22	1.8	-284.92	1.8	-281.38	2.12	-215.58
24	25	27.60	-1420.02	-161.81	549.53	0	-513.60	1.8	-311.50	1.8	-310.28	2.12	-281.84
25	25	27.60	-1750.84	-161.44	400.17	0	-986.90	1.8	-334.21	1.8	-331.25	2.12	-229.58
25	26	29.00	-1750.84	-108.01	568.38	0	-849.64	1.8	-352.17	1.8	-351.08	2.12	-275.00
26	26	29.00	-1061.02	-106.59	238.88	0	-863.30	1.8	-165.38	1.8	-170.63	2.12	-59.19
26	27	30.40	-1058.63	-83.02	374.41	0	-760.13	1.8	-181.13	1.8	-190.52	2.12	-98.80
27	27	30.40	-1356.26	-85.73	247.59	0	-997.88	1.8	-154.62	1.8	-192.70	2.12	-81.46
27	28	31.80	-1356.26	-64.05	352.42	0	-928.26	1.8	-169.17	1.8	-209.83	2.12	-112.18
28	28	31.80	-1356.26	-63.94	352.37	0	-928.30	1.8	-169.16	1.8	-209.82	2.12	-112.17
28	29	33.20	-1356.26	-42.25	426.70	0	-879.22	1.8	-179.32	1.8	-222.01	2.12	-133.93
29	29	33.20	-1356.26	-42.18	426.66	0	-879.25	1.8	-179.32	1.8	-222.00	2.12	-133.92
29	30	34.60	-1356.26	-20.49	470.54	0	-850.70	1.8	-185.10	1.8	-229.24	2.12	-146.72
30	30	34.60	-1356.26	-20.40	470.52	0	-850.71	1.8	-185.10	1.8	-229.23	2.12	-146.71
30	31	36.00	-1356.26	1.27	483.91	0	-842.69	1.8	-186.51	1.8	-231.52	2.12	-150.54
31	31	36.00	-1356.26	1.33	483.92	0	-842.69	1.8	-186.51	1.8	-231.52	2.12	-150.54
31	32	37.40	-1356.26	23.02	466.84	0	-855.20	1.8	-183.54	1.8	-228.87	2.12	-145.41
32	32	37.40	-1356.26	23.10	466.87	0	-855.18	1.8	-183.54	1.8	-228.87	2.12	-145.42
32	33	38.80	-1356.26	44.78	419.36	0	-888.20	1.8	-176.20	1.8	-221.27	2.12	-131.34
33	33	38.80	-1356.26	44.88	419.40	0	-888.17	1.8	-176.21	1.8	-221.28	2.12	-131.35
33	34	40.20	-1356.26	66.57	341.38	0	-941.75	1.8	-164.48	1.8	-208.73	2.12	-108.30
34	34	40.20	-1356.26	66.66	341.43	0	-941.71	1.8	-164.49	1.8	-208.73	2.12	-108.31
34	35	41.60	-1356.26	88.34	232.93	0	-1015.82	1.8	-148.38	1.8	-191.24	2.12	-76.29
35	35	41.60	-1060.58	86.14	359.74	0	-792.23	1.8	-174.97	1.8	-189.07	2.12	-91.67
35	36	43.00	-1063.03	109.56	221.66	0	-901.78	1.8	-158.01	1.8	-169.08	2.12	-50.84
36	36	43.00	-1750.84	110.48	551.17	0	-866.83	1.8	-349.19	1.8	-347.81	2.12	-268.37
36	37	44.40	-1750.84	164.94	371.19	0	-1014.44	1.8	-329.58	1.8	-326.37	2.12	-219.41
37	37	44.40	-1420.02	165.32	520.54	0	-541.14	1.8	-306.87	1.8	-305.40	2.12	-271.67
37	38	45.80	-1420.02	192.29	270.26	0	-746.37	1.8	-279.51	1.8	-275.69	2.12	-203.71
38	38	45.80	-2104.90	192.73	599.81	0	-668.92	1.8	-488.68	1.8	-463.18	2.12	-437.05

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	219.71	311.10	0	-905.38	1.8	-457.57	1.8	-428.78	2.12	-358.53
39	39	47.20	-1847.60	220.20	434.97	0	-531.24	1.8	-440.27	1.8	-413.51	2.12	-401.39
39	40	48.60	-1841.15	247.67	107.23	0	-797.60	1.8	-403.73	1.8	-372.92	2.12	-310.74
40	40	48.60	-1840.98	248.23	107.23	0	-797.55	1.8	-403.69	1.8	-372.88	2.12	-310.71
40	41	50.00	-1840.98	276.97	-260.41	0	-1097.88	1.8	-365.21	1.8	-328.83	2.12	-210.49
41	1041	50.00	-1841.19	-276.88	-260.42	0	-1097.94	1.8	-365.26	1.8	-328.88	2.12	-210.54
41	42	51.40	-1841.19	-248.15	107.10	0	-797.72	1.8	-403.72	1.8	-372.91	2.12	-310.72
42	42	51.40	-1841.79	-247.58	107.08	0	-797.90	1.8	-403.87	1.8	-373.04	2.12	-310.85
42	43	52.80	-1841.79	-220.61	434.82	0	-529.72	1.8	-438.79	1.8	-412.19	2.12	-400.08
43	43	52.80	-2100.09	-220.07	311.05	0	-904.06	1.8	-456.36	1.8	-427.70	2.12	-357.46
43	44	54.20	-2104.90	-192.73	599.80	0	-668.93	1.8	-488.68	1.8	-463.18	2.12	-437.05
44	44	54.20	-1420.02	-192.29	270.24	0	-746.38	1.8	-279.51	1.8	-275.69	2.12	-203.71
44	45	55.60	-1420.02	-165.32	520.56	0	-541.12	1.8	-306.88	1.8	-305.41	2.12	-271.68
45	45	55.60	-1750.84	-164.93	371.21	0	-1014.42	1.8	-329.58	1.8	-326.38	2.12	-219.42
45	46	57.00	-1750.84	-110.47	551.17	0	-866.84	1.8	-349.18	1.8	-347.81	2.12	-268.37
46	46	57.00	-1063.03	-109.56	221.67	0	-901.77	1.8	-158.01	1.8	-169.08	2.12	-50.84
46	47	58.40	-1062.37	-87.06	360.64	0	-793.12	1.8	-175.25	1.8	-189.47	2.12	-92.01
47	47	58.40	-1358.27	-88.28	233.82	0	-1016.89	1.8	-148.67	1.8	-191.67	2.12	-76.63
47	48	59.80	-1358.27	-66.61	342.27	0	-942.82	1.8	-164.78	1.8	-209.16	2.12	-108.64
48	48	59.80	-1358.27	-66.50	342.22	0	-942.85	1.8	-164.76	1.8	-209.15	2.12	-108.62
48	49	61.20	-1358.27	-44.82	420.12	0	-889.35	1.8	-176.48	1.8	-221.68	2.12	-131.65
49	49	61.20	-1358.27	-44.73	420.09	0	-889.37	1.8	-176.47	1.8	-221.68	2.12	-131.64
49	50	62.60	-1358.27	-23.04	467.53	0	-856.41	1.8	-183.81	1.8	-229.27	2.12	-145.70
50	50	62.60	-1358.27	-22.96	467.50	0	-856.43	1.8	-183.80	1.8	-229.26	2.12	-145.69
50	51	64.00	-1360.02	-1.25	484.46	0	-845.43	1.8	-186.92	1.8	-232.15	2.12	-150.86
51	51	64.00	-1360.02	-1.18	484.47	0	-845.42	1.8	-186.92	1.8	-232.15	2.12	-150.86
51	52	65.40	-1360.02	20.49	470.96	0	-853.51	1.8	-185.50	1.8	-229.84	2.12	-147.00
52	52	65.40	-1360.02	20.57	470.97	0	-853.51	1.8	-185.50	1.8	-229.84	2.12	-147.00
52	53	66.80	-1360.02	42.26	427.00	0	-882.12	1.8	-179.70	1.8	-222.59	2.12	-134.17
53	53	66.80	-1360.02	42.34	427.04	0	-882.09	1.8	-179.71	1.8	-222.60	2.12	-134.18
53	54	68.20	-1360.02	64.02	352.61	0	-931.23	1.8	-169.53	1.8	-210.40	2.12	-112.40
54	54	68.20	-1360.02	64.13	352.66	0	-931.19	1.8	-169.54	1.8	-210.41	2.12	-112.41
54	55	69.60	-1360.02	85.81	247.71	0	-1000.90	1.8	-154.98	1.8	-193.25	2.12	-81.64
55	55	69.60	-1061.89	84.90	374.52	0	-762.74	1.8	-181.44	1.8	-191.00	2.12	-98.97
55	56	71.00	-1061.02	106.59	238.88	0	-863.30	1.8	-165.38	1.8	-170.63	2.12	-59.19
56	56	71.00	-1750.84	108.02	568.38	0	-849.64	1.8	-352.17	1.8	-351.08	2.12	-275.00
56	57	72.40	-1750.84	161.44	400.19	0	-986.89	1.8	-334.21	1.8	-331.25	2.12	-229.58
57	57	72.40	-1420.02	161.82	549.52	0	-513.61	1.8	-311.50	1.8	-310.28	2.12	-281.84
57	58	73.80	-1420.02	188.81	304.09	0	-714.23	1.8	-284.92	1.8	-281.38	2.12	-215.57
58	58	73.80	-2104.91	189.23	633.63	0	-636.79	1.8	-494.08	1.8	-468.87	2.12	-448.91
58	59	75.20	-2104.91	216.21	349.85	0	-868.57	1.8	-463.76	1.8	-435.30	2.12	-372.11
59	59	75.20	-1847.60	216.69	473.75	0	-494.41	1.8	-446.46	1.8	-420.02	2.12	-414.98
59	60	76.60	-1843.78	244.13	150.99	0	-756.80	1.8	-411.37	1.8	-380.85	2.12	-326.64
60	60	76.60	-1843.83	244.68	150.97	0	-756.83	1.8	-411.38	1.8	-380.86	2.12	-326.64
60	61	78.00	-1843.83	273.40	-211.70	0	-1052.45	1.8	-373.69	1.8	-337.64	2.12	-228.16
61	1061	78.00	-1807.39	-250.13	-192.56	0	-997.97	1.8	-371.36	1.8	-335.73	2.12	-234.77
61	62	79.10	-1807.39	-227.57	70.17	0	-784.25	1.8	-398.88	1.8	-366.62	2.12	-305.53
62	62	79.10	-1807.77	-227.17	70.14	0	-784.38	1.8	-398.97	1.8	-366.70	2.12	-305.61
62	63	80.20	-1807.77	-205.98	308.37	0	-590.39	1.8	-424.30	1.8	-394.59	2.12	-369.62
63	63	80.20	-2065.61	-205.58	182.00	0	-966.62	1.8	-441.63	1.8	-409.65	2.12	-326.16
63	64	81.30	-2065.61	-184.38	396.47	0	-791.94	1.8	-464.66	1.8	-434.64	2.12	-383.65
64	64	81.30	-2066.31	-183.99	396.45	0	-792.16	1.8	-464.83	1.8	-434.80	2.12	-383.80
64	65	82.40	-2066.31	-162.80	587.19	0	-636.77	1.8	-485.54	1.8	-456.90	2.12	-434.77
65	65	82.40	-1566.09	-162.42	171.18	0	-980.11	1.8	-289.06	1.8	-280.78	2.12	-171.59
65	66	83.50	-1566.09	-141.23	338.18	0	-844.01	1.8	-307.46	1.8	-299.99	2.12	-216.03
66	66	83.50	-1567.05	-140.84	338.20	0	-844.26	1.8	-307.70	1.8	-300.21	2.12	-216.25
66	67	84.60	-1567.05	-91.67	453.49	0	-750.62	1.8	-320.26	1.8	-313.36	2.12	-246.76
67	67	84.60	-874.65	-89.14	124.01	0	-768.98	1.8	-129.86	1.8	-131.33	2.12	-28.54
67	68	85.70	-875.52	-72.11	215.15	0	-705.59	1.8	-140.40	1.8	-145.24	2.12	-54.78
68	68	85.70	-1065.95	-74.10	130.36	0	-829.48	1.8	-112.09	1.8	-141.05	2.12	-44.82
68	69	86.80	-1065.95	-57.05	202.49	0	-783.31	1.8	-121.54	1.8	-152.92	2.12	-65.70
69	69	86.80	-1065.96	-56.93	202.46	0	-783.34	1.8	-121.54	1.8	-152.92	2.12	-65.69
69	70	87.90	-1065.96	-39.89	255.70	0	-749.90	1.8	-128.28	1.8	-161.72	2.12	-81.02
70	70	87.90	-1065.96	-39.79	255.68	0	-749.92	1.8	-128.27	1.8	-161.71	2.12	-81.01
70	71	89.00	-1065.96	-22.76	290.08	0	-729.17	1.8	-132.31	1.8	-167.46	2.12	-90.79
71	71	89.00	-1065.96	-22.68	290.08	0	-729.17	1.8	-132.30	1.8	-167.46	2.12	-90.79
71	72	90.10	-1065.96	-5.64	305.66	0	-721.11	1.8	-133.63	1.8	-170.15	2.12	-95.04
72	72	90.10	-1065.96	-5.55	305.63	0	-721.13	1.8	-133.62	1.8	-170.14	2.12	-95.03
72	73	91.20	-1065.96	11.48	302.36	0	-725.77	1.8	-132.24	1.8	-169.77	2.12	-93.73
73	73	91.20	-1065.96	11.55	302.38	0	-725.76	1.8	-132.24	1.8	-169.77	2.12	-93.74
73	74	92.30	-1065.96	28.59	280.29	0	-743.08	1.8	-128.15	1.8	-166.35	2.12	-86.90
74	74	92.30	-1065.96	28.69	280.30	0	-743.07	1.8	-128.16	1.8	-166.35	2.12	-86.91
74	75	93.40	-1065.96	45.72	239.39	0	-773.07	1.8	-121.36	1.8	-159.87	2.12	-74.54
75	75	93.40	-1065.96	45.81	239.43	0	-927.41	1.8	-158.25	1.8	-173.19	2.12	-51.05
75	76	94.50	-1065.96	62.84	179.64	0	-977.73	1.8	-150.01	1.8	-164.35	2.12	-32.66

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	62.97	264.41	0	-714.08	1.8	-137.13	1.8	-152.46	2.12	-61.69
76	77	95.60	-882.17	80.01	185.79	0	-779.72	1.8	-126.86	1.8	-140.97	2.12	-37.72
77	77	95.60	-882.17	80.12	185.85	0	-779.67	1.8	-126.87	1.8	-140.98	2.12	-37.74
77	78	96.70	-882.17	97.15	88.33	0	-860.70	1.8	-114.55	1.8	-126.85	2.12	-8.15
78	78	96.70	-698.39	97.31	174.97	0	-595.59	1.8	-101.76	1.8	-115.20	2.12	-37.70
78	79	97.80	-698.39	114.35	58.56	0	-692.00	1.8	-87.41	1.8	-98.41	2.12	-2.51
79	79	97.80	-698.38	114.53	58.63	0	-691.94	1.8	-87.41	1.8	-98.42	2.12	-2.53
79	80	98.90	-698.38	131.57	-76.73	0	-803.77	1.8	-71.01	1.8	-78.99	2.12	38.29
80	80	98.90	-441.09	131.77	49.69	0	-428.64	1.8	-53.31	1.8	-63.33	2.12	-4.52
80	81	100.00	-441.09	181.96	-104.92	0	-556.08	1.8	-34.92	1.8	-41.22	2.12	41.98
101	101	0.00	-441.09	-143.60	-104.82	0	-555.99	1.8	-34.94	1.8	-41.23	2.12	41.95
101	102	1.10	-436.66	-125.64	42.65	0	-430.27	1.8	-51.68	1.8	-61.65	2.12	-2.29
102	102	1.10	-693.96	-125.85	-83.61	0	-805.27	1.8	-69.41	1.8	-77.33	2.12	40.47
102	103	2.20	-693.96	-109.45	45.80	0	-698.43	1.8	-84.84	1.8	-95.88	2.12	1.49
103	103	2.20	-693.96	-109.63	45.87	0	-698.37	1.8	-84.85	1.8	-95.89	2.12	1.47
103	104	3.30	-693.96	-93.24	157.42	0	-606.04	1.8	-98.40	1.8	-111.95	2.12	-32.23
104	104	3.30	-877.74	-93.38	70.92	0	-871.03	1.8	-111.22	1.8	-123.62	2.12	-2.72
104	105	4.40	-877.74	-77.01	164.65	0	-793.18	1.8	-122.92	1.8	-137.19	2.12	-31.13
105	105	4.40	-877.74	-77.14	164.69	0	-793.15	1.8	-122.92	1.8	-137.20	2.12	-31.15
105	106	5.50	-877.74	-60.75	240.51	0	-729.85	1.8	-132.74	1.8	-148.27	2.12	-54.26
106	106	5.50	-1061.53	-60.85	155.82	0	-993.43	1.8	-145.63	1.8	-160.17	2.12	-25.26
106	107	6.60	-1061.53	-44.47	213.75	0	-944.68	1.8	-153.57	1.8	-168.74	2.12	-43.07
107	107	6.60	-1061.53	-44.55	213.77	0	-787.29	1.8	-116.57	1.8	-155.28	2.12	-66.85
107	108	7.70	-1061.53	-28.17	253.75	0	-757.93	1.8	-123.21	1.8	-161.62	2.12	-78.94
108	108	7.70	-1061.53	-28.26	253.77	0	-757.92	1.8	-123.21	1.8	-161.62	2.12	-78.95
108	109	8.80	-1061.53	-11.87	275.83	0	-740.61	1.8	-127.30	1.8	-165.05	2.12	-85.78
109	109	8.80	-1061.53	-11.94	275.83	0	-740.62	1.8	-127.30	1.8	-165.04	2.12	-85.77
109	110	9.90	-1061.53	4.44	279.96	0	-735.37	1.8	-128.84	1.8	-165.55	2.12	-87.33
110	110	9.90	-1061.53	4.36	279.96	0	-735.37	1.8	-128.84	1.8	-165.55	2.12	-87.33
110	111	11.00	-1061.53	20.74	266.15	0	-742.20	1.8	-127.82	1.8	-163.13	2.12	-83.60
111	111	11.00	-1061.53	20.67	266.12	0	-742.22	1.8	-127.82	1.8	-163.13	2.12	-83.59
111	112	12.10	-1061.53	37.05	234.37	0	-761.10	1.8	-124.25	1.8	-157.79	2.12	-74.59
112	112	12.10	-1061.53	36.95	234.34	0	-761.13	1.8	-124.24	1.8	-157.79	2.12	-74.57
112	113	13.20	-1061.53	53.34	184.68	0	-792.06	1.8	-118.13	1.8	-149.53	2.12	-60.30
113	113	13.20	-1061.53	53.23	184.65	0	-792.08	1.8	-118.12	1.8	-149.53	2.12	-60.29
113	114	14.30	-1061.53	69.62	117.06	0	-835.07	1.8	-109.45	1.8	-138.36	2.12	-40.74
114	114	14.30	-871.84	64.88	201.76	0	-713.60	1.8	-137.89	1.8	-142.70	2.12	-50.51
114	115	15.40	-874.66	83.71	117.57	0	-774.43	1.8	-128.78	1.8	-130.38	2.12	-26.54
115	115	15.40	-1567.05	85.93	446.95	0	-756.03	1.8	-319.44	1.8	-312.62	2.12	-245.03
115	116	16.50	-1567.05	129.00	338.20	0	-844.26	1.8	-307.70	1.8	-300.21	2.12	-216.25
116	116	16.50	-1567.05	128.72	338.10	0	-844.34	1.8	-307.69	1.8	-300.20	2.12	-216.22
116	117	17.60	-1567.05	148.72	185.14	0	-968.80	1.8	-291.09	1.8	-282.56	2.12	-175.49
117	117	17.60	-2068.15	148.38	601.42	0	-625.51	1.8	-487.79	1.8	-458.92	2.12	-438.94
117	118	18.70	-2068.15	168.36	427.22	0	-767.20	1.8	-469.17	1.8	-438.69	2.12	-392.35
118	118	18.70	-2068.15	167.99	427.13	0	-767.27	1.8	-469.16	1.8	-438.68	2.12	-392.33
118	119	19.80	-2068.15	187.98	231.35	0	-926.48	1.8	-448.49	1.8	-415.79	2.12	-339.79
119	119	19.80	-1810.85	187.58	357.63	0	-550.48	1.8	-431.28	1.8	-400.85	2.12	-383.35
119	120	20.90	-1810.85	207.57	140.29	0	-727.16	1.8	-408.57	1.8	-375.32	2.12	-324.87
120	120	20.90	-1810.85	207.14	140.27	0	-727.18	1.8	-408.57	1.8	-375.32	2.12	-324.86
120	121	22.00	-1810.85	228.52	-99.37	0	-921.79	1.8	-383.96	1.8	-347.03	2.12	-260.22
121	1121	22.00	-1847.60	-251.89	-118.52	0	-976.37	1.8	-386.37	1.8	-349.01	2.12	-253.68
121	122	23.40	-1847.60	-224.68	215.06	0	-704.83	1.8	-420.40	1.8	-388.95	2.12	-344.45
122	122	23.40	-1847.60	-225.21	215.12	0	-704.78	1.8	-420.40	1.8	-388.95	2.12	-344.47
122	123	24.80	-1847.60	-199.78	512.62	0	-462.23	1.8	-451.35	1.8	-424.42	2.12	-425.28
123	123	24.80	-2104.90	-200.26	388.97	0	-836.18	1.8	-468.69	1.8	-439.72	2.12	-382.48
123	124	26.20	-2104.90	-174.82	651.50	0	-622.00	1.8	-496.33	1.8	-470.89	2.12	-453.64
124	124	26.20	-1420.02	-175.25	322.20	0	-699.23	1.8	-287.20	1.8	-283.42	2.12	-220.37
124	125	27.60	-1420.02	-149.78	549.72	0	-513.44	1.8	-311.53	1.8	-310.30	2.12	-281.89
125	125	27.60	-1750.84	-150.15	400.62	0	-986.53	1.8	-334.27	1.8	-331.30	2.12	-229.70
125	126	29.00	-1750.84	-102.76	560.68	0	-856.01	1.8	-351.20	1.8	-350.21	2.12	-272.96
126	126	29.00	-1061.03	-101.66	231.32	0	-869.65	1.8	-164.13	1.8	-169.51	2.12	-56.86
126	127	30.40	-1058.64	-78.91	360.52	0	-771.80	1.8	-178.83	1.8	-188.45	2.12	-94.51
127	127	30.40	-1356.26	-81.88	233.82	0	-1007.49	1.8	-152.25	1.8	-190.58	2.12	-77.42
127	128	31.80	-1356.26	-61.02	333.84	0	-941.22	1.8	-165.97	1.8	-206.97	2.12	-106.74
128	128	31.80	-1356.26	-61.12	333.90	0	-941.19	1.8	-165.98	1.8	-206.98	2.12	-106.76
128	129	33.20	-1356.26	-40.27	404.86	0	-894.47	1.8	-175.57	1.8	-218.64	2.12	-127.53
129	129	33.20	-1356.26	-40.35	404.90	0	-894.45	1.8	-175.57	1.8	-218.65	2.12	-127.54
129	130	34.60	-1356.26	-19.49	446.77	0	-867.29	1.8	-181.02	1.8	-225.58	2.12	-139.75
130	130	34.60	-1356.26	-19.56	446.78	0	-867.28	1.8	-181.02	1.8	-225.58	2.12	-139.75
130	131	36.00	-1356.26	1.30	459.57	0	-859.69	1.8	-182.32	1.8	-227.77	2.12	-143.41
131	131	36.00	-1356.26	1.22	459.57	0	-859.68	1.8	-182.32	1.8	-227.77	2.12	-143.41
131	132	37.40	-1356.26	22.09	443.23	0	-871.68	1.8	-179.48	1.8	-225.23	2.12	-138.50
132	132	37.40	-1356.26	22.02	443.22	0	-871.69	1.8	-179.48	1.8	-225.23	2.12	-138.49
132	133	38.80	-1356.26	42.88	397.80	0	-903.25	1.8	-172.49	1.8	-217.95	2.12	-125.03
133	133	38.80	-1356.26	42.79	397.77	0	-903.27	1.8	-172.49	1.8	-217.95	2.12	-125.01

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	63.65	323.27	0	-954.39	1.8	-161.36	1.8	-205.94	2.12	-102.99
134	134	40.20	-1356.26	63.54	323.22	0	-954.42	1.8	-161.36	1.8	-205.93	2.12	-102.98
134	135	41.60	-1356.26	84.40	219.64	0	-1025.09	1.8	-146.09	1.8	-189.19	2.12	-72.40
135	135	41.60	-1060.58	81.92	346.34	0	-803.49	1.8	-172.75	1.8	-187.07	2.12	-87.53
135	136	43.00	-1063.03	104.51	214.75	0	-907.58	1.8	-156.86	1.8	-168.05	2.12	-48.70
136	136	43.00	-1750.84	105.09	544.10	0	-872.68	1.8	-348.29	1.8	-347.01	2.12	-266.50
136	137	44.40	-1750.84	153.40	373.17	0	-1012.80	1.8	-329.83	1.8	-326.60	2.12	-219.94
137	137	44.40	-1420.02	153.02	522.24	0	-539.73	1.8	-307.09	1.8	-305.59	2.12	-272.12
137	138	45.80	-1420.02	178.46	290.21	0	-729.84	1.8	-282.03	1.8	-277.94	2.12	-209.00
138	138	45.80	-2104.90	178.02	619.52	0	-652.60	1.8	-491.16	1.8	-465.41	2.12	-442.27
138	139	47.20	-2104.90	203.46	352.47	0	-871.12	1.8	-462.79	1.8	-433.46	2.12	-369.49
139	139	47.20	-1847.60	202.96	476.13	0	-497.16	1.8	-445.45	1.8	-418.16	2.12	-412.30
139	140	48.60	-1841.15	228.91	173.57	0	-742.66	1.8	-412.09	1.8	-380.41	2.12	-328.33
140	140	48.60	-1840.98	228.38	173.46	0	-742.71	1.8	-412.03	1.8	-380.36	2.12	-328.26
140	141	50.00	-1840.98	255.59	-165.30	0	-1019.12	1.8	-377.19	1.8	-339.58	2.12	-235.70
141	1141	50.00	-1841.18	-255.50	-165.31	0	-1019.19	1.8	-377.24	1.8	-339.62	2.12	-235.74
141	142	51.40	-1841.18	-228.29	173.34	0	-742.87	1.8	-412.07	1.8	-380.39	2.12	-328.27
142	142	51.40	-1841.79	-228.83	173.45	0	-742.94	1.8	-412.23	1.8	-380.54	2.12	-328.43
142	143	52.80	-1841.79	-203.38	475.98	0	-495.64	1.8	-443.98	1.8	-416.84	2.12	-410.98
143	143	52.80	-2100.09	-203.83	352.42	0	-869.80	1.8	-461.58	1.8	-432.38	2.12	-368.43
143	144	54.20	-2104.90	-178.02	619.49	0	-652.63	1.8	-491.16	1.8	-465.41	2.12	-442.26
144	144	54.20	-1420.02	-178.47	290.20	0	-729.86	1.8	-282.02	1.8	-277.94	2.12	-209.00
144	145	55.60	-1420.02	-153.03	522.25	0	-539.73	1.8	-307.09	1.8	-305.60	2.12	-272.13
145	145	55.60	-1750.84	-153.40	373.18	0	-1012.79	1.8	-329.83	1.8	-326.60	2.12	-219.94
145	146	57.00	-1750.84	-105.09	544.10	0	-872.69	1.8	-348.29	1.8	-347.01	2.12	-266.50
146	146	57.00	-1063.03	-104.52	214.74	0	-907.59	1.8	-156.86	1.8	-168.05	2.12	-48.70
146	147	58.40	-1062.37	-82.85	347.24	0	-804.38	1.8	-173.02	1.8	-187.48	2.12	-87.87
147	147	58.40	-1358.27	-84.34	220.55	0	-1026.15	1.8	-146.39	1.8	-189.63	2.12	-72.75
147	148	59.80	-1358.27	-63.48	324.03	0	-955.55	1.8	-161.64	1.8	-206.35	2.12	-103.30
148	148	59.80	-1358.28	-63.59	324.08	0	-955.51	1.8	-161.65	1.8	-206.36	2.12	-103.31
148	149	61.20	-1358.28	-42.73	398.49	0	-904.46	1.8	-172.76	1.8	-218.36	2.12	-125.31
149	149	61.20	-1358.27	-42.82	398.52	0	-904.43	1.8	-172.76	1.8	-218.36	2.12	-125.32
149	150	62.60	-1358.27	-21.96	443.88	0	-872.92	1.8	-179.74	1.8	-225.63	2.12	-138.77
150	150	62.60	-1358.27	-22.03	443.91	0	-872.90	1.8	-179.75	1.8	-225.63	2.12	-138.78
150	151	64.00	-1360.02	-1.14	460.13	0	-862.41	1.8	-182.74	1.8	-228.40	2.12	-143.73
151	151	64.00	-1360.02	-1.22	460.12	0	-862.42	1.8	-182.73	1.8	-228.40	2.12	-143.73
151	152	65.40	-1360.02	19.64	447.23	0	-870.08	1.8	-181.42	1.8	-226.19	2.12	-140.04
152	152	65.40	-1360.02	19.57	447.21	0	-870.09	1.8	-181.41	1.8	-226.18	2.12	-140.04
152	153	66.80	-1360.02	40.42	405.24	0	-897.31	1.8	-175.96	1.8	-219.24	2.12	-127.79
153	153	66.80	-1360.02	40.35	405.20	0	-897.34	1.8	-175.95	1.8	-219.23	2.12	-127.78
153	154	68.20	-1360.02	61.20	334.12	0	-944.13	1.8	-166.35	1.8	-207.55	2.12	-106.98
154	154	68.20	-1360.02	61.09	334.07	0	-944.17	1.8	-166.35	1.8	-207.54	2.12	-106.96
154	155	69.60	-1360.02	81.95	233.95	0	-1010.50	1.8	-152.61	1.8	-191.14	2.12	-77.61
155	155	69.60	-1061.89	80.78	360.63	0	-774.40	1.8	-179.14	1.8	-188.93	2.12	-94.68
155	156	71.00	-1061.02	101.65	231.33	0	-869.64	1.8	-164.13	1.8	-169.51	2.12	-56.86
156	156	71.00	-1750.84	102.75	560.69	0	-856.00	1.8	-351.20	1.8	-350.22	2.12	-272.96
156	157	72.40	-1750.84	150.16	400.65	0	-986.51	1.8	-334.27	1.8	-331.30	2.12	-229.70
157	157	72.40	-1420.02	149.79	549.72	0	-513.44	1.8	-311.53	1.8	-310.30	2.12	-281.89
157	158	73.80	-1420.02	175.25	322.20	0	-699.23	1.8	-287.20	1.8	-283.42	2.12	-220.37
158	158	73.80	-2104.90	174.82	651.49	0	-622.01	1.8	-496.33	1.8	-470.89	2.12	-453.64
158	159	75.20	-2104.90	200.25	388.95	0	-836.20	1.8	-468.69	1.8	-439.71	2.12	-382.47
159	159	75.20	-1847.60	199.77	512.63	0	-462.23	1.8	-451.36	1.8	-424.42	2.12	-425.28
159	160	76.60	-1843.78	225.68	214.62	0	-704.11	1.8	-419.38	1.8	-388.04	2.12	-343.50
160	160	76.60	-1843.83	225.18	214.46	0	-704.26	1.8	-419.38	1.8	-388.03	2.12	-343.47
160	161	78.00	-1843.83	252.38	-119.82	0	-976.37	1.8	-385.26	1.8	-348.02	2.12	-252.51
161	1161	78.00	-1807.39	-228.67	-100.68	0	-921.90	1.8	-382.94	1.8	-346.11	2.12	-259.12
161	162	79.10	-1807.39	-207.31	139.09	0	-727.18	1.8	-407.56	1.8	-374.41	2.12	-323.80
162	162	79.10	-1807.77	-207.73	139.11	0	-727.27	1.8	-407.66	1.8	-374.50	2.12	-323.88
162	163	80.20	-1807.77	-187.75	356.64	0	-550.43	1.8	-430.38	1.8	-400.04	2.12	-382.41
163	163	80.20	-2065.60	-188.14	230.38	0	-926.56	1.8	-447.73	1.8	-415.11	2.12	-338.98
163	164	81.30	-2065.60	-168.15	426.34	0	-767.21	1.8	-468.42	1.8	-438.02	2.12	-391.56
164	164	81.30	-2066.31	-168.51	426.49	0	-767.28	1.8	-468.62	1.8	-438.19	2.12	-391.76
164	165	82.40	-2066.31	-148.53	600.86	0	-625.45	1.8	-487.26	1.8	-458.44	2.12	-438.39
165	165	82.40	-1566.09	-148.82	185.05	0	-968.63	1.8	-290.81	1.8	-282.35	2.12	-175.26
165	166	83.50	-1566.09	-128.82	337.73	0	-844.38	1.8	-307.41	1.8	-299.94	2.12	-215.91
166	166	83.50	-1567.05	-129.03	337.91	0	-844.50	1.8	-307.67	1.8	-300.17	2.12	-216.17
166	167	84.60	-1567.05	-85.96	446.72	0	-756.22	1.8	-319.41	1.8	-312.60	2.12	-244.97
167	167	84.60	-874.65	-83.71	117.34	0	-774.58	1.8	-128.75	1.8	-130.34	2.12	-26.47
167	168	85.70	-875.52	-67.34	202.86	0	-715.91	1.8	-138.36	1.8	-143.41	2.12	-50.98
168	168	85.70	-1065.96	-69.55	118.17	0	-837.99	1.8	-109.99	1.8	-139.18	2.12	-41.25
168	169	86.80	-1065.96	-53.16	185.67	0	-795.05	1.8	-118.65	1.8	-150.33	2.12	-60.77
169	169	86.80	-1065.96	-53.28	185.71	0	-795.03	1.8	-118.66	1.8	-150.34	2.12	-60.79
169	170	87.90	-1065.96	-36.89	235.29	0	-764.15	1.8	-124.77	1.8	-158.58	2.12	-75.04
170	170	87.90	-1065.96	-36.97	235.32	0	-764.13	1.8	-124.77	1.8	-158.58	2.12	-75.04
170	171	89.00	-1065.96	-20.60	266.98	0	-745.29	1.8	-128.33	1.8	-163.90	2.12	-84.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

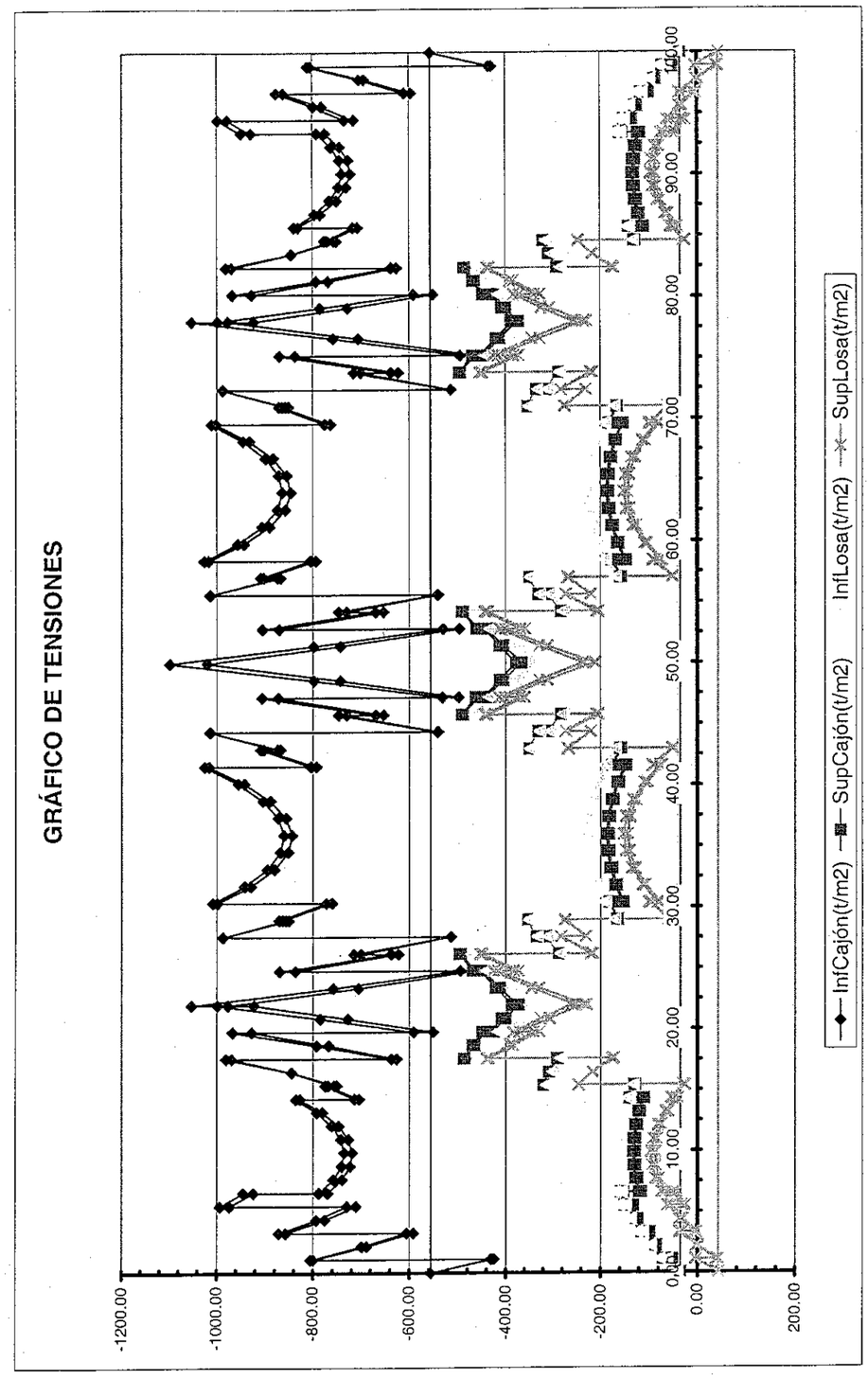
PERM1.Tinf.MZ-

C. Permanentes sin gradiente

[1; 1]PPVF1 + [.95; 1.05]eje1I1.ISO.To + [.95; 1.05]eje2I1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1I3.ISO.To + [.95; 1.05]eje1I3.HIP.To + [.95; 1.05]eje2I3.ISO.To + [.95; 1.05]eje2I3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

						Fibra	InfCajón	Fibra	SupCajón	Fibra	InfLosa	Fibra	SupLosa
Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)	y fibra	sig (t/m2)
171	171	89.00	-1065.96	-20.69	267.01	0	-745.27	1.8	-128.34	1.8	-163.91	2.12	-84.03
171	172	90.10	-1065.96	-4.29	280.73	0	-738.51	1.8	-129.34	1.8	-166.31	2.12	-87.73
172	172	90.10	-1065.96	-4.36	280.73	0	-738.51	1.8	-129.34	1.8	-166.31	2.12	-87.73
172	173	91.20	-1065.96	12.02	276.51	0	-743.82	1.8	-127.79	1.8	-165.79	2.12	-86.16
173	173	91.20	-1065.96	11.93	276.51	0	-743.81	1.8	-127.79	1.8	-165.79	2.12	-86.16
173	174	92.30	-1065.96	28.32	254.37	0	-761.17	1.8	-123.69	1.8	-162.35	2.12	-79.31
174	174	92.30	-1065.96	28.25	254.35	0	-761.18	1.8	-123.69	1.8	-162.35	2.12	-79.30
174	175	93.40	-1065.96	44.63	214.28	0	-790.59	1.8	-117.04	1.8	-156.00	2.12	-67.18
175	175	93.40	-1065.96	44.53	214.26	0	-948.56	1.8	-154.07	1.8	-169.44	2.12	-43.27
175	176	94.50	-1065.96	60.91	156.23	0	-997.39	1.8	-146.12	1.8	-160.86	2.12	-25.43
176	176	94.50	-882.17	60.81	240.93	0	-733.80	1.8	-133.24	1.8	-148.96	2.12	-54.44
176	177	95.60	-882.17	77.20	165.03	0	-797.16	1.8	-123.41	1.8	-137.88	2.12	-31.30
177	177	95.60	-882.17	77.07	164.98	0	-797.20	1.8	-123.41	1.8	-137.87	2.12	-31.29
177	178	96.70	-882.17	93.45	71.17	0	-875.11	1.8	-111.71	1.8	-124.29	2.12	-2.85
178	178	96.70	-698.39	93.30	157.69	0	-610.11	1.8	-98.89	1.8	-112.62	2.12	-32.36
178	179	97.80	-698.39	109.69	46.03	0	-702.52	1.8	-85.33	1.8	-96.55	2.12	1.36
179	179	97.80	-698.40	109.53	45.96	0	-702.58	1.8	-85.32	1.8	-96.54	2.12	1.38
179	180	98.90	-698.40	125.93	-83.54	0	-809.49	1.8	-69.88	1.8	-77.98	2.12	40.39
180	180	98.90	-441.09	125.71	42.75	0	-434.48	1.8	-52.15	1.8	-62.30	2.12	-2.38
180	181	100.00	-441.09	143.59	-104.82	0	-555.99	1.8	-34.94	1.8	-41.23	2.12	41.95



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-153.74	-85.87	0	-492.92	1.8	-30.84	1.8	-36.65	2.12	37.15
1	2	1.10	-395.79	-186.87	132.76	0	-315.35	1.8	-61.03	1.8	-69.49	2.12	-29.84
2	2	1.10	-624.09	-186.65	24.69	0	-647.90	1.8	-76.79	1.8	-83.45	2.12	8.08
2	3	2.20	-624.09	-162.57	216.10	0	-488.41	1.8	-103.11	1.8	-111.73	2.12	-50.64
3	3	2.20	-624.08	-162.39	216.03	0	-488.47	1.8	-103.10	1.8	-111.72	2.12	-50.62
3	4	3.30	-624.08	-138.33	380.35	0	-351.33	1.8	-125.93	1.8	-136.07	2.12	-101.11
4	4	3.30	-787.15	-138.15	306.41	0	-586.34	1.8	-137.31	1.8	-146.46	2.12	-74.94
4	5	4.40	-787.15	-112.87	443.66	0	-471.53	1.8	-156.65	1.8	-166.87	2.12	-117.23
5	5	4.40	-787.15	-112.72	443.62	0	-471.56	1.8	-156.65	1.8	-166.87	2.12	-117.22
5	6	5.50	-787.15	-88.24	555.31	0	-377.78	1.8	-172.79	1.8	-183.61	2.12	-151.79
6	6	5.50	-950.22	-88.10	483.02	0	-611.51	1.8	-184.23	1.8	-194.20	2.12	-126.07
6	7	6.60	-950.22	-64.02	567.79	0	-539.94	1.8	-196.90	1.8	-207.03	2.12	-152.48
7	7	6.60	-950.22	-63.91	567.77	0	-435.60	1.8	-166.77	1.8	-197.14	2.12	-170.59
7	8	7.70	-950.22	-39.84	625.59	0	-392.49	1.8	-176.67	1.8	-206.42	2.12	-188.29
8	8	7.70	-950.22	-39.71	625.57	0	-392.50	1.8	-176.67	1.8	-206.41	2.12	-188.28
8	9	8.80	-950.22	-15.70	656.26	0	-368.30	1.8	-182.36	1.8	-211.30	2.12	-197.90
9	9	8.80	-950.22	-15.58	656.26	0	-368.30	1.8	-182.36	1.8	-211.31	2.12	-197.90
9	10	9.90	-950.22	8.46	661.39	0	-361.74	1.8	-184.13	1.8	-212.07	2.12	-199.93
10	10	9.90	-950.22	8.61	661.40	0	-361.72	1.8	-184.13	1.8	-212.07	2.12	-199.93
10	11	11.00	-950.22	32.70	639.70	0	-373.83	1.8	-181.75	1.8	-208.49	2.12	-193.97
11	11	11.00	-950.22	32.83	639.73	0	-373.82	1.8	-181.75	1.8	-208.50	2.12	-193.98
11	12	12.10	-950.22	56.91	591.12	0	-404.66	1.8	-175.19	1.8	-200.57	2.12	-180.00
12	12	12.10	-950.22	57.07	591.16	0	-404.63	1.8	-175.20	1.8	-200.57	2.12	-180.01
12	13	13.20	-950.22	81.09	515.52	0	-454.31	1.8	-164.44	1.8	-188.27	2.12	-157.98
13	13	13.20	-950.22	81.27	515.56	0	-454.28	1.8	-164.44	1.8	-188.28	2.12	-157.99
13	14	14.30	-950.22	105.37	413.91	0	-521.96	1.8	-149.69	1.8	-171.77	2.12	-128.23
14	14	14.30	-780.33	106.20	486.22	0	-387.15	1.8	-173.42	1.8	-174.38	2.12	-139.43
14	15	15.40	-775.77	127.80	356.21	0	-480.35	1.8	-155.81	1.8	-153.96	2.12	-100.80
15	15	15.40	-1554.62	130.21	727.56	0	-449.35	1.8	-371.32	1.8	-357.53	2.12	-346.57
15	16	16.50	-1554.62	122.06	576.99	0	-572.65	1.8	-353.48	1.8	-339.71	2.12	-305.90
16	16	16.50	-1554.62	122.16	576.98	0	-559.34	1.8	-366.48	1.8	-351.00	2.12	-321.25
16	17	17.60	-1554.62	138.86	432.33	0	-679.20	1.8	-348.23	1.8	-332.02	2.12	-279.74
17	17	17.60	-2163.46	139.00	877.79	0	-355.94	1.8	-573.37	1.8	-533.87	2.12	-569.96
17	18	18.70	-2163.46	151.18	716.40	0	-489.06	1.8	-553.97	1.8	-513.06	2.12	-524.12
18	18	18.70	-2163.46	151.33	716.32	0	-489.14	1.8	-553.94	1.8	-513.03	2.12	-524.08
18	19	19.80	-2163.46	164.61	542.24	0	-631.52	1.8	-534.65	1.8	-491.45	2.12	-475.80
19	19	19.80	-1935.17	164.75	650.14	0	-298.14	1.8	-519.36	1.8	-478.19	2.12	-514.43
19	20	20.90	-1935.17	178.04	461.52	0	-451.57	1.8	-499.66	1.8	-455.39	2.12	-462.88
20	20	20.90	-1935.17	178.11	461.54	0	-451.56	1.8	-499.66	1.8	-455.39	2.12	-462.89
20	21	22.00	-1935.17	193.23	257.18	0	-616.91	1.8	-479.54	1.8	-431.12	2.12	-407.64
21	1021	22.00	-1967.78	-215.43	240.76	0	-665.33	1.8	-481.68	1.8	-432.88	2.12	-401.83
21	22	23.40	-1967.78	-193.96	528.43	0	-432.09	1.8	-509.58	1.8	-467.33	2.12	-480.06
22	22	23.40	-1967.78	-193.86	528.39	0	-432.13	1.8	-509.57	1.8	-467.33	2.12	-480.05
22	23	24.80	-1967.78	-176.24	787.79	0	-220.90	1.8	-535.99	1.8	-498.71	2.12	-551.06
23	23	24.80	-2196.07	-176.15	682.01	0	-552.66	1.8	-551.33	1.8	-512.25	2.12	-513.01
23	24	26.20	-2196.07	-165.13	919.91	0	-357.34	1.8	-577.67	1.8	-542.16	2.12	-579.64
24	24	26.20	-1424.17	-165.15	548.77	0	-444.57	1.8	-341.54	1.8	-330.50	2.12	-316.26
24	25	27.60	-1424.17	-146.50	766.16	0	-264.22	1.8	-368.08	1.8	-359.18	2.12	-378.93
25	25	27.60	-1717.69	-146.35	639.13	0	-683.76	1.8	-388.24	1.8	-377.81	2.12	-332.62
25	26	29.00	-1717.69	-152.75	867.86	0	-493.01	1.8	-417.80	1.8	-407.86	2.12	-398.48
26	26	29.00	-941.07	-151.28	496.53	0	-534.13	1.8	-191.94	1.8	-193.90	2.12	-138.72
26	27	30.40	-945.20	-123.03	688.09	0	-388.63	1.8	-218.25	1.8	-223.50	2.12	-196.44
27	27	30.40	-1210.45	-122.00	580.25	0	-630.76	1.8	-197.13	1.8	-227.22	2.12	-178.48
27	28	31.80	-1210.45	-91.18	728.37	0	-528.73	1.8	-219.57	1.8	-251.29	2.12	-222.49
28	28	31.80	-1210.45	-90.98	728.33	0	-528.75	1.8	-219.56	1.8	-251.29	2.12	-222.48
28	29	33.20	-1210.45	-59.18	833.34	0	-456.68	1.8	-235.33	1.8	-268.39	2.12	-253.65
29	29	33.20	-1210.45	-59.03	833.31	0	-456.70	1.8	-235.32	1.8	-268.38	2.12	-253.64
29	30	34.60	-1210.45	-29.69	895.61	0	-414.27	1.8	-244.50	1.8	-278.58	2.12	-272.11
30	30	34.60	-1210.45	-29.51	895.59	0	-414.28	1.8	-244.49	1.8	-278.58	2.12	-272.11
30	31	36.00	-1210.45	1.19	914.20	0	-402.29	1.8	-246.88	1.8	-281.70	2.12	-277.56
31	31	36.00	-1210.45	1.33	914.21	0	-402.28	1.8	-246.88	1.8	-281.70	2.12	-277.56
31	32	37.40	-1210.45	33.21	890.42	0	-419.69	1.8	-242.74	1.8	-277.98	2.12	-270.40
32	32	37.40	-1210.45	33.38	890.44	0	-419.67	1.8	-242.74	1.8	-277.98	2.12	-270.41
32	33	38.80	-1210.45	62.71	822.99	0	-467.50	1.8	-231.81	1.8	-267.19	2.12	-250.23
33	33	38.80	-1210.45	62.90	823.02	0	-467.48	1.8	-231.82	1.8	-267.19	2.12	-250.24
33	34	40.20	-1210.45	94.70	712.83	0	-544.97	1.8	-214.29	1.8	-249.49	2.12	-217.35
34	34	40.20	-1210.45	94.88	712.87	0	-544.95	1.8	-214.30	1.8	-249.49	2.12	-217.36
34	35	41.60	-1210.45	125.71	559.54	0	-652.42	1.8	-190.10	1.8	-224.82	2.12	-171.63
35	35	41.60	-946.85	127.18	667.36	0	-424.85	1.8	-211.30	1.8	-221.09	2.12	-187.54
35	36	43.00	-942.63	155.63	469.44	0	-579.21	1.8	-183.28	1.8	-190.75	2.12	-127.47
36	36	43.00	-1717.69	156.72	840.80	0	-517.86	1.8	-414.18	1.8	-403.97	2.12	-389.90
36	37	44.40	-1717.69	151.16	613.30	0	-708.29	1.8	-384.47	1.8	-373.69	2.12	-323.81
37	37	44.40	-1424.17	151.33	740.34	0	-288.74	1.8	-364.31	1.8	-355.06	2.12	-370.12
37	38	45.80	-1424.17	170.68	515.15	0	-476.56	1.8	-336.13	1.8	-324.81	2.12	-304.42
38	38	45.80	-2196.07	170.78	886.28	0	-389.35	1.8	-572.26	1.8	-536.47	2.12	-567.79

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	183.52	638.95	0	-593.70	1.8	-543.81	1.8	-504.58	2.12	-497.42
39	39	47.20	-1967.78	183.77	744.61	0	-262.05	1.8	-528.43	1.8	-491.01	2.12	-535.41
39	40	48.60	-1974.23	199.36	476.41	0	-483.64	1.8	-501.59	1.8	-459.17	2.12	-462.23
40	40	48.60	-1974.41	199.47	476.51	0	-483.60	1.8	-501.65	1.8	-459.22	2.12	-462.29
40	41	50.00	-1974.41	220.73	181.08	0	-724.35	1.8	-472.01	1.8	-423.11	2.12	-380.93
41	1041	50.00	-1974.19	-220.82	181.09	0	-724.29	1.8	-471.96	1.8	-423.07	2.12	-380.89
41	42	51.40	-1974.19	-199.55	476.62	0	-483.45	1.8	-501.61	1.8	-459.18	2.12	-462.27
42	42	51.40	-1973.59	-199.44	476.53	0	-483.35	1.8	-501.45	1.8	-459.04	2.12	-462.12
42	43	52.80	-1973.59	-183.35	744.76	0	-263.57	1.8	-529.91	1.8	-492.33	2.12	-536.72
43	43	52.80	-2200.88	-183.15	638.99	0	-595.03	1.8	-545.01	1.8	-505.66	2.12	-498.48
43	44	54.20	-2196.07	-170.78	886.27	0	-389.35	1.8	-572.26	1.8	-536.47	2.12	-567.79
44	44	54.20	-1424.17	-170.68	515.14	0	-476.57	1.8	-336.13	1.8	-324.81	2.12	-304.42
44	45	55.60	-1424.17	-151.33	740.37	0	-288.72	1.8	-364.32	1.8	-355.07	2.12	-370.13
45	45	55.60	-1717.69	-151.15	613.32	0	-708.27	1.8	-384.47	1.8	-373.69	2.12	-323.81
45	46	57.00	-1717.69	-156.71	840.79	0	-517.87	1.8	-414.18	1.8	-403.97	2.12	-389.90
46	46	57.00	-942.63	-155.64	469.46	0	-579.19	1.8	-183.28	1.8	-190.75	2.12	-127.48
46	47	58.40	-945.05	-126.26	666.48	0	-423.96	1.8	-211.02	1.8	-220.68	2.12	-187.20
47	47	58.40	-1208.44	-125.77	558.64	0	-651.35	1.8	-189.80	1.8	-224.38	2.12	-171.28
47	48	59.80	-1208.44	-94.94	712.08	0	-543.80	1.8	-214.02	1.8	-249.08	2.12	-217.04
48	48	59.80	-1208.43	-94.74	712.04	0	-543.82	1.8	-214.01	1.8	-249.07	2.12	-217.03
48	49	61.20	-1208.43	-62.95	822.28	0	-466.31	1.8	-231.54	1.8	-266.78	2.12	-249.93
49	49	61.20	-1208.44	-62.77	822.25	0	-466.33	1.8	-231.54	1.8	-266.78	2.12	-249.93
49	50	62.60	-1208.44	-33.43	889.79	0	-418.45	1.8	-242.48	1.8	-277.58	2.12	-270.13
50	50	62.60	-1208.44	-33.26	889.77	0	-418.46	1.8	-242.47	1.8	-277.58	2.12	-270.12
50	51	64.00	-1206.69	-1.41	913.63	0	-399.58	1.8	-246.47	1.8	-281.07	2.12	-277.23
51	51	64.00	-1206.69	-1.27	913.64	0	-399.57	1.8	-246.47	1.8	-281.07	2.12	-277.23
51	52	65.40	-1206.69	29.44	895.14	0	-411.49	1.8	-244.09	1.8	-277.97	2.12	-271.82
52	52	65.40	-1206.69	29.61	895.13	0	-411.49	1.8	-244.09	1.8	-277.97	2.12	-271.82
52	53	66.80	-1206.69	58.95	832.98	0	-453.82	1.8	-234.94	1.8	-267.79	2.12	-253.39
53	53	66.80	-1206.69	59.11	833.01	0	-453.81	1.8	-234.94	1.8	-267.80	2.12	-253.40
53	54	68.20	-1206.69	90.90	728.12	0	-525.80	1.8	-219.19	1.8	-250.72	2.12	-222.26
54	54	68.20	-1206.69	91.10	728.17	0	-525.77	1.8	-219.20	1.8	-250.72	2.12	-222.27
54	55	69.60	-1206.69	121.92	580.13	0	-627.75	1.8	-196.77	1.8	-226.66	2.12	-178.29
55	55	69.60	-941.94	121.16	687.97	0	-386.03	1.8	-217.93	1.8	-223.02	2.12	-196.27
55	56	71.00	-941.07	151.29	496.54	0	-534.11	1.8	-191.94	1.8	-193.90	2.12	-138.72
56	56	71.00	-1717.69	152.75	867.87	0	-493.00	1.8	-417.80	1.8	-407.86	2.12	-398.48
56	57	72.40	-1717.69	146.35	639.14	0	-683.75	1.8	-388.24	1.8	-377.81	2.12	-332.62
57	57	72.40	-1424.17	146.50	766.16	0	-264.23	1.8	-368.08	1.8	-359.18	2.12	-378.93
57	58	73.80	-1424.17	165.15	548.75	0	-444.58	1.8	-341.54	1.8	-330.50	2.12	-316.26
58	58	73.80	-2196.08	165.14	919.90	0	-357.35	1.8	-577.67	1.8	-542.16	2.12	-579.64
58	59	75.20	-2196.08	176.17	682.00	0	-552.66	1.8	-551.33	1.8	-512.25	2.12	-513.01
59	59	75.20	-1967.78	176.23	787.79	0	-220.90	1.8	-535.99	1.8	-498.71	2.12	-551.06
59	60	76.60	-1971.61	193.38	528.91	0	-432.78	1.8	-510.59	1.8	-468.24	2.12	-481.02
60	60	76.60	-1971.55	193.47	529.03	0	-432.67	1.8	-510.59	1.8	-468.25	2.12	-481.05
60	61	78.00	-1971.55	214.93	242.06	0	-665.32	1.8	-482.79	1.8	-433.87	2.12	-403.00
61	1061	78.00	-1938.62	-193.08	258.51	0	-616.78	1.8	-480.58	1.8	-432.05	2.12	-408.75
61	62	79.10	-1938.62	-177.96	462.69	0	-451.58	1.8	-500.67	1.8	-456.29	2.12	-463.95
62	62	79.10	-1938.24	-177.88	462.67	0	-451.48	1.8	-500.58	1.8	-456.20	2.12	-463.86
62	63	80.20	-1938.24	-164.60	651.11	0	-298.21	1.8	-520.26	1.8	-478.99	2.12	-515.36
63	63	80.20	-2165.99	-164.45	543.19	0	-631.45	1.8	-535.40	1.8	-492.13	2.12	-476.61
63	64	81.30	-2165.99	-151.17	717.10	0	-489.22	1.8	-554.67	1.8	-513.69	2.12	-524.84
64	64	81.30	-2165.29	-151.03	717.12	0	-488.98	1.8	-554.52	1.8	-513.55	2.12	-524.72
64	65	82.40	-2165.29	-138.85	878.36	0	-356.00	1.8	-573.90	1.8	-534.34	2.12	-570.51
65	65	82.40	-1555.58	-138.76	433.12	0	-678.84	1.8	-348.54	1.8	-332.34	2.12	-280.16
65	66	83.50	-1555.58	-122.06	577.33	0	-559.32	1.8	-366.77	1.8	-351.26	2.12	-321.55
66	66	83.50	-1554.62	-122.06	577.25	0	-572.45	1.8	-353.51	1.8	-339.74	2.12	-305.96
66	67	84.60	-1554.62	-130.20	727.79	0	-449.15	1.8	-371.35	1.8	-357.56	2.12	-346.63
67	67	84.60	-775.78	-127.79	356.46	0	-480.20	1.8	-155.84	1.8	-154.00	2.12	-100.87
67	68	85.70	-776.65	-103.73	485.10	0	-384.85	1.8	-172.94	1.8	-173.67	2.12	-138.95
68	68	85.70	-945.78	-105.46	412.78	0	-519.06	1.8	-149.14	1.8	-170.95	2.12	-127.71
68	69	86.80	-945.78	-81.36	514.53	0	-451.31	1.8	-163.91	1.8	-187.47	2.12	-157.50
69	69	86.80	-945.79	-81.18	514.49	0	-451.34	1.8	-163.91	1.8	-187.47	2.12	-157.49
69	70	87.90	-945.79	-57.16	590.20	0	-401.62	1.8	-174.67	1.8	-199.78	2.12	-179.55
70	70	87.90	-945.79	-56.99	590.17	0	-401.64	1.8	-174.67	1.8	-199.78	2.12	-179.54
70	71	89.00	-945.79	-32.92	638.86	0	-370.74	1.8	-181.24	1.8	-207.72	2.12	-193.54
71	71	89.00	-945.79	-32.80	638.85	0	-370.75	1.8	-181.24	1.8	-207.72	2.12	-193.54
71	72	90.10	-945.79	-8.70	660.65	0	-358.57	1.8	-183.63	1.8	-211.31	2.12	-199.53
72	72	90.10	-945.79	-8.55	660.62	0	-358.60	1.8	-183.63	1.8	-211.31	2.12	-199.52
72	73	91.20	-945.79	15.49	655.57	0	-365.11	1.8	-181.87	1.8	-210.56	2.12	-197.51
73	73	91.20	-945.79	15.61	655.57	0	-365.10	1.8	-181.87	1.8	-210.56	2.12	-197.51
73	74	92.30	-945.79	39.62	624.98	0	-389.24	1.8	-176.19	1.8	-205.69	2.12	-187.93
74	74	92.30	-945.79	39.75	624.98	0	-389.24	1.8	-176.19	1.8	-205.69	2.12	-187.93
74	75	93.40	-945.79	63.82	567.25	0	-432.30	1.8	-166.30	1.8	-196.42	2.12	-170.25
75	75	93.40	-945.79	63.93	567.28	0	-536.06	1.8	-196.40	1.8	-206.33	2.12	-152.28
75	76	94.50	-945.79	88.01	482.58	0	-607.58	1.8	-183.73	1.8	-193.51	2.12	-125.89

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	88.16	554.88	0	-373.84	1.8	-172.29	1.8	-182.92	2.12	-151.61
76	77	95.60	-782.72	112.64	443.28	0	-467.55	1.8	-156.16	1.8	-166.19	2.12	-117.06
77	77	95.60	-782.72	112.78	443.34	0	-467.51	1.8	-156.16	1.8	-166.20	2.12	-117.08
77	78	96.70	-782.72	138.06	306.15	0	-582.27	1.8	-136.83	1.8	-145.79	2.12	-74.81
78	78	96.70	-619.65	138.24	380.11	0	-347.24	1.8	-125.45	1.8	-135.41	2.12	-100.99
78	79	97.80	-619.65	162.30	215.85	0	-484.33	1.8	-102.62	1.8	-111.06	2.12	-50.51
79	79	97.80	-619.65	162.49	215.92	0	-484.27	1.8	-102.63	1.8	-111.07	2.12	-50.53
79	80	98.90	-619.65	186.57	24.59	0	-643.69	1.8	-76.31	1.8	-82.80	2.12	8.17
80	80	98.90	-391.36	186.78	132.67	0	-311.13	1.8	-60.56	1.8	-68.85	2.12	-29.76
80	81	100.00	-391.36	153.73	-85.87	0	-492.92	1.8	-30.84	1.8	-36.65	2.12	37.15
101	101	0.00	-391.36	-171.69	-85.81	0	-492.87	1.8	-30.85	1.8	-36.65	2.12	37.14
101	102	1.10	-395.79	-182.17	127.26	0	-319.80	1.8	-60.32	1.8	-68.82	2.12	-28.31
102	102	1.10	-624.09	-182.24	19.28	0	-652.28	1.8	-76.09	1.8	-82.78	2.12	9.59
102	103	2.20	-624.09	-158.77	206.01	0	-496.58	1.8	-101.81	1.8	-110.49	2.12	-47.82
103	103	2.20	-624.08	-158.83	206.04	0	-496.56	1.8	-101.81	1.8	-110.49	2.12	-47.82
103	104	3.30	-624.08	-135.39	366.51	0	-362.53	1.8	-124.14	1.8	-134.36	2.12	-97.25
104	104	3.30	-787.15	-135.42	292.65	0	-597.49	1.8	-135.53	1.8	-144.75	2.12	-71.09
104	105	4.40	-787.15	-111.97	427.05	0	-484.98	1.8	-154.50	1.8	-164.82	2.12	-112.58
105	105	4.40	-787.15	-112.02	427.04	0	-484.98	1.8	-154.50	1.8	-164.82	2.12	-112.58
105	106	5.50	-787.15	-86.60	536.85	0	-392.70	1.8	-170.42	1.8	-181.34	2.12	-146.65
106	106	5.50	-950.22	-86.65	464.60	0	-626.40	1.8	-181.86	1.8	-191.94	2.12	-120.94
106	107	6.60	-950.22	-63.19	548.31	0	-555.67	1.8	-194.42	1.8	-204.65	2.12	-147.07
107	107	6.60	-950.22	-63.23	548.31	0	-445.93	1.8	-164.05	1.8	-194.56	2.12	-165.78
107	108	7.70	-950.22	-39.79	605.85	0	-402.85	1.8	-173.94	1.8	-203.82	2.12	-183.44
108	108	7.70	-950.22	-39.84	605.85	0	-402.85	1.8	-173.94	1.8	-203.82	2.12	-183.44
108	109	8.80	-950.22	-16.39	637.27	0	-378.07	1.8	-179.76	1.8	-208.83	2.12	-193.29
109	109	8.80	-950.22	-16.45	637.25	0	-378.09	1.8	-179.76	1.8	-208.83	2.12	-193.28
109	110	9.90	-950.22	6.99	643.82	0	-370.56	1.8	-181.77	1.8	-209.81	2.12	-195.73
110	110	9.90	-950.22	6.93	643.81	0	-370.57	1.8	-181.77	1.8	-209.81	2.12	-195.72
110	111	11.00	-950.22	30.39	624.48	0	-381.15	1.8	-179.77	1.8	-206.58	2.12	-190.42
111	111	11.00	-950.22	30.33	624.45	0	-381.17	1.8	-179.76	1.8	-206.57	2.12	-190.41
111	112	12.10	-950.22	53.77	579.09	0	-409.96	1.8	-173.72	1.8	-199.12	2.12	-177.33
112	112	12.10	-950.22	53.68	579.06	0	-409.98	1.8	-173.71	1.8	-199.11	2.12	-177.32
112	113	13.20	-950.22	77.11	507.70	0	-456.97	1.8	-163.63	1.8	-187.43	2.12	-156.45
113	113	13.20	-950.22	76.99	507.67	0	-456.99	1.8	-163.63	1.8	-187.42	2.12	-156.45
113	114	14.30	-950.22	100.45	411.20	0	-521.46	1.8	-149.68	1.8	-171.66	2.12	-128.09
114	114	14.30	-780.33	100.98	483.44	0	-389.02	1.8	-173.51	1.8	-174.35	2.12	-139.02
114	115	15.40	-775.77	121.93	359.71	0	-477.05	1.8	-156.83	1.8	-154.78	2.12	-102.23
115	115	15.40	-1554.62	123.95	730.96	0	-446.00	1.8	-372.73	1.8	-358.71	2.12	-348.43
115	116	16.50	-1554.62	120.57	587.91	0	-563.25	1.8	-355.54	1.8	-341.50	2.12	-309.45
116	116	16.50	-1554.62	120.57	587.92	0	-548.72	1.8	-369.71	1.8	-353.80	2.12	-326.19
116	117	17.60	-1554.62	136.98	445.24	0	-667.75	1.8	-350.75	1.8	-334.25	2.12	-284.15
117	117	17.60	-2163.46	136.93	890.74	0	-344.45	1.8	-575.92	1.8	-536.11	2.12	-574.40
117	118	18.70	-2163.46	146.12	733.25	0	-475.01	1.8	-556.20	1.8	-515.05	2.12	-528.71
118	118	18.70	-2163.46	146.03	733.16	0	-475.10	1.8	-556.18	1.8	-515.04	2.12	-528.68
118	119	19.80	-2163.46	156.55	566.44	0	-611.75	1.8	-537.39	1.8	-493.93	2.12	-481.87
119	119	19.80	-1935.17	156.34	674.37	0	-278.32	1.8	-522.13	1.8	-480.68	2.12	-520.53
119	120	20.90	-1935.17	167.17	496.38	0	-423.03	1.8	-503.67	1.8	-459.00	2.12	-471.70
120	120	20.90	-1935.17	166.89	496.37	0	-423.04	1.8	-503.67	1.8	-459.00	2.12	-471.70
120	121	22.00	-1935.17	182.69	303.36	0	-579.14	1.8	-484.82	1.8	-435.88	2.12	-419.28
121	1121	22.00	-1967.78	-205.20	286.95	0	-627.54	1.8	-486.95	1.8	-437.64	2.12	-413.47
121	122	23.40	-1967.78	-185.13	560.93	0	-405.42	1.8	-513.39	1.8	-470.77	2.12	-488.37
122	122	23.40	-1967.78	-185.48	560.96	0	-405.39	1.8	-513.40	1.8	-470.77	2.12	-488.37
122	123	24.80	-1967.78	-168.87	809.54	0	-202.77	1.8	-538.87	1.8	-501.29	2.12	-556.97
123	123	24.80	-2196.07	-169.26	703.83	0	-534.48	1.8	-554.21	1.8	-514.82	2.12	-518.93
123	124	26.20	-2196.07	-161.18	933.27	0	-345.76	1.8	-579.97	1.8	-544.20	2.12	-583.86
124	124	26.20	-1424.17	-161.29	562.12	0	-433.01	1.8	-343.82	1.8	-332.52	2.12	-320.46
124	125	27.60	-1424.17	-143.82	775.09	0	-255.60	1.8	-370.66	1.8	-361.43	2.12	-382.91
125	125	27.60	-1717.69	-143.84	648.04	0	-675.17	1.8	-390.80	1.8	-380.03	2.12	-336.56
125	126	29.00	-1717.69	-147.25	867.26	0	-491.60	1.8	-419.99	1.8	-409.71	2.12	-400.81
126	126	29.00	-941.08	-146.24	496.03	0	-534.23	1.8	-192.23	1.8	-194.09	2.12	-138.87
126	127	30.40	-945.21	-118.69	680.80	0	-394.32	1.8	-217.55	1.8	-222.77	2.12	-194.60
127	127	30.40	-1210.45	-118.06	573.05	0	-633.59	1.8	-196.32	1.8	-226.39	2.12	-176.97
127	128	31.80	-1210.45	-87.97	715.96	0	-534.74	1.8	-217.95	1.8	-249.72	2.12	-219.58
128	128	31.80	-1210.45	-88.12	715.99	0	-534.73	1.8	-217.95	1.8	-249.73	2.12	-219.59
128	129	33.20	-1210.45	-56.89	817.38	0	-464.87	1.8	-233.15	1.8	-266.31	2.12	-249.78
129	129	33.20	-1210.45	-57.04	817.40	0	-464.86	1.8	-233.16	1.8	-266.31	2.12	-249.79
129	130	34.60	-1210.45	-28.74	877.65	0	-423.66	1.8	-242.01	1.8	-276.22	2.12	-267.71
130	130	34.60	-1210.45	-28.87	877.66	0	-423.66	1.8	-242.02	1.8	-276.22	2.12	-267.72
130	131	36.00	-1210.45	1.11	895.61	0	-412.08	1.8	-244.30	1.8	-279.25	2.12	-272.98
131	131	36.00	-1210.45	0.97	895.61	0	-412.08	1.8	-244.30	1.8	-279.25	2.12	-272.98
131	132	37.40	-1210.45	32.36	872.78	0	-428.86	1.8	-240.31	1.8	-275.67	2.12	-266.09
132	132	37.40	-1210.45	32.23	872.76	0	-428.87	1.8	-240.31	1.8	-275.67	2.12	-266.09
132	133	38.80	-1210.45	60.52	807.61	0	-475.28	1.8	-229.74	1.8	-265.20	2.12	-246.54
133	133	38.80	-1210.45	60.36	807.59	0	-475.28	1.8	-229.74	1.8	-265.20	2.12	-246.53

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	91.60	701.37	0	-550.30	1.8	-212.84	1.8	-248.07	2.12	-214.72
134	134	40.20	-1210.45	91.44	701.34	0	-550.32	1.8	-212.83	1.8	-248.06	2.12	-214.71
134	135	41.60	-1210.45	121.51	553.53	0	-654.37	1.8	-189.50	1.8	-224.18	2.12	-170.48
135	135	41.60	-946.85	122.56	661.29	0	-429.52	1.8	-210.81	1.8	-220.54	2.12	-186.08
135	136	43.00	-942.63	150.26	470.57	0	-577.93	1.8	-183.85	1.8	-191.19	2.12	-128.13
136	136	43.00	-1717.69	150.85	841.80	0	-515.06	1.8	-416.64	1.8	-406.07	2.12	-392.74
136	137	44.40	-1717.69	148.83	623.30	0	-698.76	1.8	-387.21	1.8	-376.07	2.12	-328.09
137	137	44.40	-1424.16	148.78	750.36	0	-279.18	1.8	-367.08	1.8	-357.47	2.12	-374.43
137	138	45.80	-1424.16	166.90	529.66	0	-464.02	1.8	-338.58	1.8	-326.97	2.12	-308.95
138	138	45.80	-2196.07	166.85	900.80	0	-376.78	1.8	-574.73	1.8	-538.65	2.12	-572.35
138	139	47.20	-2196.07	176.36	661.83	0	-574.67	1.8	-546.79	1.8	-507.25	2.12	-503.59
139	139	47.20	-1967.78	176.20	767.48	0	-243.02	1.8	-531.43	1.8	-493.70	2.12	-541.60
139	140	48.60	-1974.23	190.74	510.94	0	-455.21	1.8	-505.74	1.8	-462.90	2.12	-471.16
140	140	48.60	-1974.41	190.37	510.98	0	-455.23	1.8	-505.79	1.8	-462.94	2.12	-471.21
140	141	50.00	-1974.41	210.20	229.60	0	-684.56	1.8	-477.67	1.8	-428.21	2.12	-393.29
141	1141	50.00	-1974.19	-210.28	229.60	0	-684.49	1.8	-477.62	1.8	-428.17	2.12	-393.25
141	142	51.40	-1974.19	-190.45	511.10	0	-455.06	1.8	-505.75	1.8	-462.91	2.12	-471.19
142	142	51.40	-1973.59	-190.82	511.08	0	-454.92	1.8	-505.60	1.8	-462.77	2.12	-471.05
142	143	52.80	-1973.59	-175.78	767.63	0	-244.54	1.8	-532.90	1.8	-495.01	2.12	-542.91
143	143	52.80	-2200.88	-176.01	661.87	0	-576.00	1.8	-547.99	1.8	-508.33	2.12	-504.65
143	144	54.20	-2196.07	-166.85	900.77	0	-376.80	1.8	-574.73	1.8	-538.65	2.12	-572.34
144	144	54.20	-1424.17	-166.91	529.64	0	-464.03	1.8	-338.58	1.8	-326.97	2.12	-308.95
144	145	55.60	-1424.17	-148.79	750.36	0	-279.18	1.8	-367.08	1.8	-357.47	2.12	-374.44
145	145	55.60	-1717.69	-148.83	623.30	0	-698.76	1.8	-387.21	1.8	-376.07	2.12	-328.09
145	146	57.00	-1717.69	-150.85	841.80	0	-515.05	1.8	-416.64	1.8	-406.07	2.12	-392.74
146	146	57.00	-942.63	-150.28	470.57	0	-577.93	1.8	-183.85	1.8	-191.19	2.12	-128.13
146	147	58.40	-945.05	-121.66	660.41	0	-428.62	1.8	-210.54	1.8	-220.14	2.12	-185.75
147	147	58.40	-1208.44	-121.57	552.66	0	-653.29	1.8	-189.21	1.8	-223.75	2.12	-170.14
147	148	59.80	-1208.44	-91.50	700.52	0	-549.20	1.8	-212.55	1.8	-247.64	2.12	-214.39
148	148	59.80	-1208.45	-91.66	700.56	0	-549.18	1.8	-212.56	1.8	-247.65	2.12	-214.40
148	149	61.20	-1208.45	-60.42	806.85	0	-474.12	1.8	-229.46	1.8	-264.79	2.12	-246.23
149	149	61.20	-1208.44	-60.58	806.87	0	-474.11	1.8	-229.47	1.8	-264.79	2.12	-246.24
149	150	62.60	-1208.44	-32.28	872.13	0	-427.63	1.8	-240.05	1.8	-275.27	2.12	-265.82
150	150	62.60	-1208.44	-32.42	872.15	0	-427.61	1.8	-240.05	1.8	-275.28	2.12	-265.83
150	151	64.00	-1206.69	-1.05	895.05	0	-409.35	1.8	-243.89	1.8	-278.63	2.12	-272.67
151	151	64.00	-1206.69	-1.19	895.05	0	-409.35	1.8	-243.89	1.8	-278.62	2.12	-272.67
151	152	65.40	-1206.69	28.79	877.21	0	-420.86	1.8	-241.62	1.8	-275.61	2.12	-267.43
152	152	65.40	-1206.69	28.66	877.20	0	-420.87	1.8	-241.61	1.8	-275.61	2.12	-267.43
152	153	66.80	-1206.69	56.94	817.07	0	-461.98	1.8	-232.77	1.8	-265.72	2.12	-249.54
153	153	66.80	-1206.69	56.81	817.05	0	-461.99	1.8	-232.77	1.8	-265.72	2.12	-249.54
153	154	68.20	-1206.69	88.04	715.77	0	-531.78	1.8	-217.58	1.8	-249.16	2.12	-219.37
154	154	68.20	-1206.69	87.88	715.73	0	-531.80	1.8	-217.57	1.8	-249.15	2.12	-219.36
154	155	69.60	-1206.69	117.97	572.95	0	-630.56	1.8	-195.96	1.8	-225.84	2.12	-176.79
155	155	69.60	-941.94	116.81	680.70	0	-391.71	1.8	-217.24	1.8	-222.29	2.12	-194.43
155	156	71.00	-941.07	146.23	496.05	0	-534.21	1.8	-192.23	1.8	-194.09	2.12	-138.87
156	156	71.00	-1717.69	147.24	867.28	0	-491.58	1.8	-419.99	1.8	-409.71	2.12	-400.82
156	157	72.40	-1717.69	143.84	648.06	0	-675.15	1.8	-390.80	1.8	-380.03	2.12	-336.57
157	157	72.40	-1424.17	143.82	775.08	0	-255.60	1.8	-370.66	1.8	-361.43	2.12	-382.91
157	158	73.80	-1424.17	161.29	562.12	0	-433.01	1.8	-343.82	1.8	-332.52	2.12	-320.46
158	158	73.80	-2196.07	161.19	933.26	0	-345.76	1.8	-579.97	1.8	-544.20	2.12	-583.86
158	159	75.20	-2196.07	169.25	703.81	0	-534.50	1.8	-554.20	1.8	-514.82	2.12	-518.93
159	159	75.20	-1967.78	168.86	809.55	0	-202.77	1.8	-538.87	1.8	-501.29	2.12	-556.97
159	160	76.60	-1971.61	185.01	561.49	0	-406.04	1.8	-514.42	1.8	-471.69	2.12	-489.35
160	160	76.60	-1971.55	184.63	561.53	0	-405.99	1.8	-514.41	1.8	-471.68	2.12	-489.35
160	161	78.00	-1971.55	204.70	288.24	0	-627.54	1.8	-488.06	1.8	-438.63	2.12	-414.64
161	1161	78.00	-1938.62	-182.55	304.69	0	-579.00	1.8	-485.85	1.8	-436.80	2.12	-420.39
161	162	79.10	-1938.62	-166.75	497.51	0	-423.07	1.8	-504.68	1.8	-459.90	2.12	-472.76
162	162	79.10	-1938.23	-167.01	497.52	0	-422.96	1.8	-504.58	1.8	-459.82	2.12	-472.67
162	163	80.20	-1938.23	-156.19	675.35	0	-278.38	1.8	-523.02	1.8	-481.48	2.12	-521.47
163	163	80.20	-2165.99	-156.39	567.39	0	-611.68	1.8	-538.14	1.8	-494.60	2.12	-482.68
163	164	81.30	-2165.99	-145.87	733.94	0	-475.17	1.8	-556.91	1.8	-515.69	2.12	-529.44
164	164	81.30	-2165.29	-145.97	733.97	0	-474.94	1.8	-556.75	1.8	-515.55	2.12	-529.30
164	165	82.40	-2165.29	-136.79	891.29	0	-344.50	1.8	-576.45	1.8	-536.59	2.12	-574.95
165	165	82.40	-1555.58	-136.88	446.05	0	-667.37	1.8	-351.07	1.8	-334.56	2.12	-284.59
165	166	83.50	-1555.58	-120.46	588.26	0	-548.70	1.8	-369.99	1.8	-354.06	2.12	-326.49
166	166	83.50	-1554.62	-120.56	588.15	0	-563.05	1.8	-355.57	1.8	-341.52	2.12	-309.51
166	167	84.60	-1554.62	-123.95	731.21	0	-445.79	1.8	-372.76	1.8	-358.74	2.12	-348.49
167	167	84.60	-775.78	-121.91	359.95	0	-476.89	1.8	-156.86	1.8	-154.83	2.12	-102.30
167	168	85.70	-776.65	-98.50	482.30	0	-386.74	1.8	-173.03	1.8	-173.64	2.12	-138.53
168	168	85.70	-945.79	-100.54	410.08	0	-518.55	1.8	-149.14	1.8	-170.84	2.12	-127.58
168	169	86.80	-945.79	-77.08	506.64	0	-454.02	1.8	-163.10	1.8	-186.62	2.12	-155.96
169	169	86.80	-945.79	-77.20	506.67	0	-454.01	1.8	-163.10	1.8	-186.62	2.12	-155.97
169	170	87.90	-945.79	-53.77	578.12	0	-406.95	1.8	-173.19	1.8	-198.32	2.12	-176.86
170	170	87.90	-945.79	-53.85	578.14	0	-406.94	1.8	-173.20	1.8	-198.33	2.12	-176.87
170	171	89.00	-945.79	-30.42	623.59	0	-378.08	1.8	-179.25	1.8	-205.80	2.12	-189.98

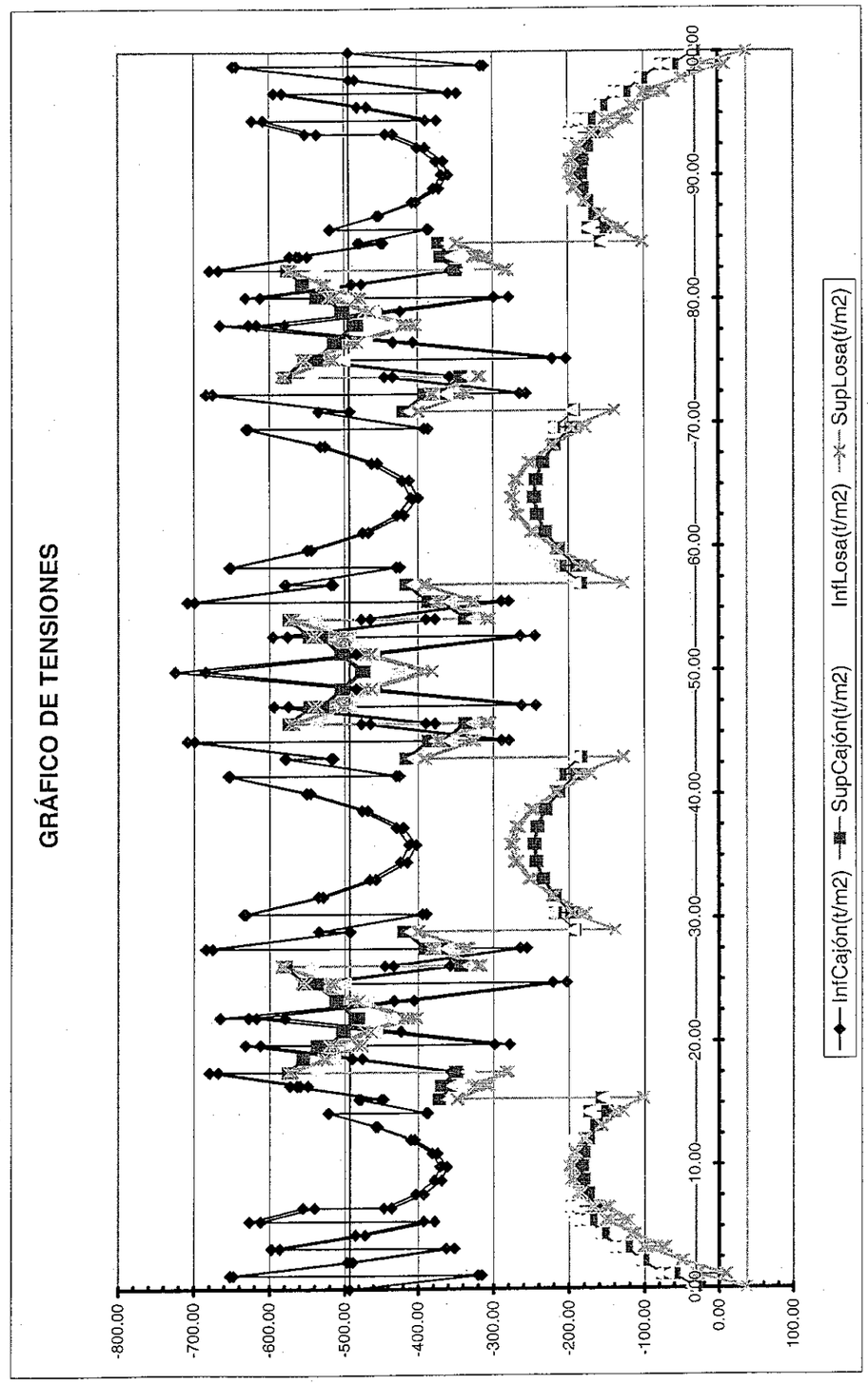
CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ+
C. Cuasipermanentes Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-30.50	623.62	0	-378.06	1.8	-179.26	1.8	-205.80	2.12	-189.99
171	172	90.10	-945.79	-7.02	643.03	0	-367.43	1.8	-181.27	1.8	-209.05	2.12	-195.31
172	172	90.10	-945.79	-7.08	643.04	0	-367.42	1.8	-181.27	1.8	-209.05	2.12	-195.32
172	173	91.20	-945.79	16.37	636.56	0	-374.90	1.8	-179.27	1.8	-208.08	2.12	-192.90
173	173	91.20	-945.79	16.29	636.57	0	-374.89	1.8	-179.27	1.8	-208.08	2.12	-192.90
173	174	92.30	-945.79	39.75	605.26	0	-399.60	1.8	-173.46	1.8	-203.09	2.12	-183.09
174	174	92.30	-945.79	39.71	605.25	0	-399.60	1.8	-173.46	1.8	-203.09	2.12	-183.08
174	175	93.40	-945.79	63.15	547.79	0	-442.62	1.8	-163.58	1.8	-193.84	2.12	-165.45
175	175	93.40	-945.79	63.10	547.79	0	-551.79	1.8	-193.91	1.8	-203.95	2.12	-146.87
175	176	94.50	-945.79	86.56	464.16	0	-622.48	1.8	-181.36	1.8	-191.24	2.12	-120.76
176	176	94.50	-782.72	86.51	536.43	0	-388.76	1.8	-169.92	1.8	-180.65	2.12	-146.47
176	177	95.60	-782.72	111.92	426.70	0	-480.97	1.8	-154.01	1.8	-164.14	2.12	-112.43
177	177	95.60	-782.72	111.87	426.70	0	-480.97	1.8	-154.01	1.8	-164.14	2.12	-112.43
177	178	96.70	-782.72	135.33	292.38	0	-593.41	1.8	-135.04	1.8	-144.08	2.12	-70.96
178	178	96.70	-619.65	135.29	366.27	0	-358.45	1.8	-123.66	1.8	-133.70	2.12	-97.12
178	179	97.80	-619.65	158.73	205.85	0	-492.42	1.8	-101.33	1.8	-109.83	2.12	-47.71
179	179	97.80	-619.66	158.69	205.83	0	-492.45	1.8	-101.33	1.8	-109.83	2.12	-47.71
179	180	98.90	-619.66	182.16	19.18	0	-648.07	1.8	-75.61	1.8	-82.13	2.12	9.68
180	180	98.90	-391.36	182.08	127.18	0	-315.58	1.8	-59.85	1.8	-68.17	2.12	-28.23
180	181	100.00	-391.36	171.68	-85.81	0	-492.87	1.8	-30.85	1.8	-36.65	2.12	37.14



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ-
C. Cuasipermanentes Mz-
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-200.13	-105.06	0	-556.20	1.8	-34.89	1.8	-41.19	2.12	42.03
1	2	1.10	-436.66	-127.47	45.09	0	-428.33	1.8	-51.96	1.8	-61.93	2.12	-2.94
2	2	1.10	-693.96	-127.37	-81.32	0	-803.45	1.8	-69.67	1.8	-77.59	2.12	39.86
2	3	2.20	-693.96	-110.09	49.29	0	-695.71	1.8	-85.16	1.8	-96.23	2.12	0.61
3	3	2.20	-693.96	-110.01	49.23	0	-695.76	1.8	-85.15	1.8	-96.22	2.12	0.63
3	4	3.30	-693.96	-92.73	160.72	0	-603.59	1.8	-98.57	1.8	-112.18	2.12	-32.94
4	4	3.30	-877.74	-92.68	74.10	0	-868.68	1.8	-111.36	1.8	-123.83	2.12	-3.39
4	5	4.40	-877.74	-75.41	166.54	0	-792.03	1.8	-122.71	1.8	-137.11	2.12	-31.30
5	5	4.40	-877.74	-75.38	166.50	0	-792.07	1.8	-122.70	1.8	-137.11	2.12	-31.26
5	6	5.50	-877.74	-58.10	239.90	0	-730.92	1.8	-131.98	1.8	-147.72	2.12	-53.53
6	6	5.50	-1061.53	-58.08	155.13	0	-994.57	1.8	-144.85	1.8	-159.61	2.12	-24.51
6	7	6.60	-1061.53	-40.81	209.54	0	-948.89	1.8	-152.06	1.8	-167.55	2.12	-41.12
7	7	6.60	-1061.53	-40.82	209.51	0	-793.78	1.8	-115.16	1.8	-154.17	2.12	-64.63
7	8	7.70	-1061.53	-23.55	244.90	0	-768.29	1.8	-120.88	1.8	-159.72	2.12	-75.20
8	8	7.70	-1061.53	-23.56	244.87	0	-768.31	1.8	-120.88	1.8	-159.71	2.12	-75.19
8	9	8.80	-1061.53	-6.22	261.28	0	-755.62	1.8	-123.86	1.8	-162.18	2.12	-80.18
9	9	8.80	-1061.54	-6.27	261.26	0	-755.64	1.8	-123.86	1.8	-162.18	2.12	-80.18
9	10	9.90	-1061.54	11.03	258.65	0	-755.79	1.8	-124.11	1.8	-161.55	2.12	-79.56
10	10	9.90	-1061.53	10.99	258.65	0	-755.79	1.8	-124.11	1.8	-161.55	2.12	-79.56
10	11	11.00	-1061.53	28.27	237.05	0	-768.76	1.8	-121.61	1.8	-157.84	2.12	-73.35
11	11	11.00	-1061.53	28.22	237.06	0	-768.76	1.8	-121.61	1.8	-157.84	2.12	-73.35
11	12	12.10	-1061.53	45.51	196.50	0	-794.53	1.8	-116.39	1.8	-151.05	2.12	-61.57
12	12	12.10	-1061.53	45.47	196.51	0	-794.52	1.8	-116.39	1.8	-151.06	2.12	-61.57
12	13	13.20	-1061.53	62.76	136.97	0	-833.09	1.8	-108.43	1.8	-141.19	2.12	-44.20
13	13	13.20	-1061.53	62.74	136.99	0	-833.08	1.8	-108.43	1.8	-141.19	2.12	-44.20
13	14	14.30	-1061.53	80.03	58.46	0	-884.47	1.8	-97.73	1.8	-128.24	2.12	-21.24
14	14	14.30	-871.84	75.36	143.23	0	-764.40	1.8	-126.22	1.8	-132.63	2.12	-30.84
14	15	15.40	-874.66	95.10	47.02	0	-835.49	1.8	-114.94	1.8	-118.39	2.12	-3.02
15	15	15.40	-1567.05	97.45	376.49	0	-816.95	1.8	-305.81	1.8	-300.81	2.12	-221.73
15	16	16.50	-1567.05	146.93	254.65	0	-916.24	1.8	-292.02	1.8	-286.58	2.12	-189.09
16	16	16.50	-1567.05	147.09	254.74	0	-925.09	1.8	-283.33	1.8	-279.03	2.12	-178.84
16	17	17.60	-1567.05	170.23	80.41	0	-1068.23	1.8	-262.86	1.8	-258.00	2.12	-131.14
17	17	17.60	-2068.15	170.35	496.89	0	-724.76	1.8	-459.60	1.8	-434.38	2.12	-394.66
17	18	18.70	-2068.15	196.83	295.05	0	-890.91	1.8	-435.62	1.8	-409.44	2.12	-338.69
18	18	18.70	-2068.15	196.99	295.22	0	-890.76	1.8	-435.66	1.8	-409.48	2.12	-338.75
18	19	19.80	-2068.15	224.68	63.63	0	-1082.04	1.8	-407.62	1.8	-380.12	2.12	-273.57
19	19	19.80	-1810.85	224.88	190.16	0	-705.81	1.8	-390.46	1.8	-365.22	2.12	-317.21
19	20	20.90	-1810.85	255.54	-75.42	0	-926.29	1.8	-357.12	1.8	-330.39	2.12	-240.92
20	20	20.90	-1810.85	255.81	-75.39	0	-926.27	1.8	-357.13	1.8	-330.39	2.12	-240.93
20	21	22.00	-1810.85	285.22	-372.71	0	-1173.48	1.8	-319.51	1.8	-290.72	2.12	-154.67
21	1021	22.00	-1847.60	-312.05	-391.85	0	-1228.05	1.8	-321.92	1.8	-292.71	2.12	-148.13
21	22	23.40	-1847.60	-277.35	19.52	0	-885.20	1.8	-373.92	1.8	-348.35	2.12	-268.53
22	22	23.40	-1847.60	-277.02	19.50	0	-885.21	1.8	-373.92	1.8	-348.36	2.12	-268.54
22	23	24.80	-1847.60	-241.22	382.21	0	-583.01	1.8	-419.78	1.8	-396.86	2.12	-374.01
23	23	24.80	-2104.90	-240.51	258.36	0	-957.13	1.8	-437.09	1.8	-412.14	2.12	-331.16
23	24	26.20	-2104.90	-201.92	565.77	0	-702.47	1.8	-474.30	1.8	-451.69	2.12	-418.53
24	24	26.20	-1420.02	-201.58	236.11	0	-780.02	1.8	-265.11	1.8	-264.17	2.12	-185.15
24	25	27.60	-1420.02	-167.38	494.22	0	-567.13	1.8	-295.39	1.8	-296.28	2.12	-257.08
25	25	27.60	-1750.84	-167.23	344.75	0	-1040.54	1.8	-318.06	1.8	-317.22	2.12	-204.77
25	26	29.00	-1750.84	-108.21	517.30	0	-899.07	1.8	-337.28	1.8	-338.16	2.12	-252.14
26	26	29.00	-1061.02	-107.01	187.80	0	-907.40	1.8	-155.49	1.8	-162.04	2.12	-42.27
26	27	30.40	-1058.63	-82.79	323.36	0	-804.19	1.8	-171.25	1.8	-181.94	2.12	-81.89
27	27	30.40	-1356.26	-85.67	196.54	0	-1039.64	1.8	-144.66	1.8	-184.05	2.12	-64.82
27	28	31.80	-1356.26	-63.67	301.07	0	-970.26	1.8	-159.15	1.8	-201.13	2.12	-95.45
28	28	31.80	-1356.26	-63.74	301.02	0	-970.30	1.8	-159.14	1.8	-201.12	2.12	-95.43
28	29	33.20	-1356.26	-41.74	374.85	0	-921.63	1.8	-169.20	1.8	-213.22	2.12	-117.03
29	29	33.20	-1356.26	-41.83	374.82	0	-921.66	1.8	-169.20	1.8	-213.21	2.12	-117.02
29	30	34.60	-1356.26	-19.53	417.71	0	-893.90	1.8	-174.79	1.8	-220.28	2.12	-129.50
30	30	34.60	-1356.26	-19.59	417.68	0	-893.93	1.8	-174.79	1.8	-220.28	2.12	-129.49
30	31	36.00	-1356.26	3.31	428.92	0	-887.67	1.8	-175.78	1.8	-222.20	2.12	-132.62
31	31	36.00	-1356.26	3.22	428.92	0	-887.68	1.8	-175.78	1.8	-222.20	2.12	-132.62
31	32	37.40	-1356.26	25.24	408.98	0	-902.53	1.8	-172.25	1.8	-219.06	2.12	-126.56
32	32	37.40	-1356.26	25.16	409.00	0	-902.52	1.8	-172.25	1.8	-219.06	2.12	-126.56
32	33	38.80	-1356.26	47.15	358.39	0	-938.07	1.8	-164.30	1.8	-210.94	2.12	-111.47
33	33	38.80	-1356.26	47.07	358.43	0	-938.05	1.8	-164.31	1.8	-210.94	2.12	-111.48
33	34	40.20	-1356.26	69.07	277.12	0	-994.31	1.8	-151.94	1.8	-197.84	2.12	-87.35
34	34	40.20	-1356.26	68.99	277.17	0	-994.28	1.8	-151.95	1.8	-197.84	2.12	-87.36
34	35	41.60	-1356.26	90.99	165.20	0	-1071.23	1.8	-135.16	1.8	-179.75	2.12	-54.21
35	35	41.60	-1060.58	88.60	292.00	0	-850.70	1.8	-161.86	1.8	-177.68	2.12	-69.23
35	36	43.00	-1063.03	112.61	150.16	0	-963.50	1.8	-144.16	1.8	-157.06	2.12	-27.15
36	36	43.00	-1750.84	113.31	479.67	0	-936.03	1.8	-328.35	1.8	-329.71	2.12	-236.37
36	37	44.40	-1750.84	171.53	293.11	0	-1090.01	1.8	-306.83	1.8	-306.61	2.12	-184.47
37	37	44.40	-1420.02	171.67	442.55	0	-616.62	1.8	-284.15	1.8	-285.66	2.12	-236.77
37	38	45.80	-1420.02	205.13	179.57	0	-834.13	1.8	-253.09	1.8	-252.74	2.12	-163.13
38	38	45.80	-2104.90	205.35	509.27	0	-756.55	1.8	-462.29	1.8	-440.27	2.12	-396.53

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ-
C. Cuasipermanentes Mz-
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	240.31	198.26	0	-1014.58	1.8	-424.69	1.8	-400.23	2.12	-308.03
39	39	47.20	-1847.60	240.48	322.20	0	-640.38	1.8	-407.41	1.8	-384.97	2.12	-350.93
39	40	48.60	-1841.15	280.18	-43.02	0	-943.01	1.8	-359.95	1.8	-334.89	2.12	-243.51
40	40	48.60	-1840.98	280.53	-43.03	0	-942.98	1.8	-359.90	1.8	-334.85	2.12	-243.46
40	41	50.00	-1840.98	315.91	-459.69	0	-1290.74	1.8	-307.13	1.8	-278.39	2.12	-121.31
41	1041	50.00	-1841.19	-315.83	-459.70	0	-1290.81	1.8	-307.19	1.8	-278.44	2.12	-121.36
41	42	51.40	-1841.19	-280.45	-43.16	0	-943.15	1.8	-359.93	1.8	-334.88	2.12	-243.47
42	42	51.40	-1841.79	-280.09	-43.16	0	-943.31	1.8	-360.09	1.8	-335.02	2.12	-243.61
42	43	52.80	-1841.79	-240.89	322.05	0	-638.86	1.8	-405.93	1.8	-383.65	2.12	-349.61
43	43	52.80	-2100.09	-240.67	198.21	0	-1013.26	1.8	-423.48	1.8	-399.14	2.12	-306.97
43	44	54.20	-2104.90	-205.35	509.27	0	-756.55	1.8	-462.30	1.8	-440.27	2.12	-396.53
44	44	54.20	-1420.02	-205.13	179.56	0	-834.14	1.8	-253.08	1.8	-252.73	2.12	-163.13
44	45	55.60	-1420.02	-171.67	442.57	0	-616.60	1.8	-284.15	1.8	-285.67	2.12	-236.78
45	45	55.60	-1750.84	-171.52	293.13	0	-1089.98	1.8	-306.83	1.8	-306.62	2.12	-184.48
45	46	57.00	-1750.84	-113.30	479.67	0	-936.03	1.8	-328.35	1.8	-329.71	2.12	-236.37
46	46	57.00	-1063.03	-112.61	150.16	0	-963.49	1.8	-144.17	1.8	-157.06	2.12	-27.15
46	47	58.40	-1062.37	-89.52	292.90	0	-851.59	1.8	-162.13	1.8	-178.08	2.12	-69.57
47	47	58.40	-1358.27	-90.93	166.09	0	-1072.30	1.8	-135.45	1.8	-180.19	2.12	-54.56
47	48	59.80	-1358.27	-68.93	278.01	0	-995.38	1.8	-152.23	1.8	-198.27	2.12	-87.69
48	48	59.80	-1358.27	-69.00	277.96	0	-995.41	1.8	-152.22	1.8	-198.26	2.12	-87.68
48	49	61.20	-1358.27	-47.01	359.15	0	-939.22	1.8	-164.58	1.8	-211.35	2.12	-111.77
49	49	61.20	-1358.27	-47.09	359.13	0	-939.24	1.8	-164.58	1.8	-211.35	2.12	-111.77
49	50	62.60	-1358.27	-25.10	409.66	0	-903.74	1.8	-172.51	1.8	-219.46	2.12	-126.84
50	50	62.60	-1358.27	-25.18	409.64	0	-903.76	1.8	-172.51	1.8	-219.45	2.12	-126.83
50	51	64.00	-1360.02	-3.14	429.47	0	-890.41	1.8	-176.19	1.8	-222.83	2.12	-132.93
51	51	64.00	-1360.02	-3.22	429.48	0	-890.40	1.8	-176.19	1.8	-222.83	2.12	-132.94
51	52	65.40	-1360.02	19.68	418.13	0	-896.73	1.8	-175.19	1.8	-220.89	2.12	-129.77
52	52	65.40	-1360.02	19.61	418.14	0	-896.72	1.8	-175.19	1.8	-220.89	2.12	-129.78
52	53	66.80	-1360.02	41.91	375.16	0	-924.53	1.8	-169.58	1.8	-213.80	2.12	-117.27
53	53	66.80	-1360.02	41.83	375.19	0	-924.50	1.8	-169.59	1.8	-213.81	2.12	-117.28
53	54	68.20	-1360.02	63.82	301.26	0	-973.23	1.8	-159.51	1.8	-201.69	2.12	-95.66
54	54	68.20	-1360.02	63.75	301.31	0	-973.20	1.8	-159.52	1.8	-201.70	2.12	-95.67
54	55	69.60	-1360.02	85.75	196.65	0	-1042.66	1.8	-145.01	1.8	-184.60	2.12	-65.00
55	55	69.60	-1061.89	84.66	323.46	0	-806.81	1.8	-171.56	1.8	-182.42	2.12	-82.05
55	56	71.00	-1061.02	107.01	187.80	0	-907.39	1.8	-155.49	1.8	-162.04	2.12	-42.27
56	56	71.00	-1750.84	108.22	517.30	0	-899.07	1.8	-337.28	1.8	-338.16	2.12	-252.14
56	57	72.40	-1750.84	167.23	344.76	0	-1040.54	1.8	-318.06	1.8	-317.22	2.12	-204.77
57	57	72.40	-1420.02	167.38	494.20	0	-567.15	1.8	-295.38	1.8	-296.28	2.12	-257.08
57	58	73.80	-1420.02	201.59	236.10	0	-780.03	1.8	-265.10	1.8	-264.17	2.12	-185.15
58	58	73.80	-2104.91	201.93	565.76	0	-702.48	1.8	-474.31	1.8	-451.69	2.12	-418.53
58	59	75.20	-2104.91	240.52	258.34	0	-957.14	1.8	-437.09	1.8	-412.14	2.12	-331.16
59	59	75.20	-1847.60	241.21	382.22	0	-583.00	1.8	-419.78	1.8	-396.86	2.12	-374.01
59	60	76.60	-1843.78	277.48	18.99	0	-884.55	1.8	-372.90	1.8	-347.44	2.12	-267.57
60	60	76.60	-1843.83	277.84	18.92	0	-884.63	1.8	-372.90	1.8	-347.44	2.12	-267.55
60	61	78.00	-1843.83	312.54	-393.14	0	-1228.05	1.8	-320.81	1.8	-291.72	2.12	-146.96
61	1061	78.00	-1807.39	-285.37	-374.03	0	-1173.60	1.8	-318.48	1.8	-289.80	2.12	-153.56
61	62	79.10	-1807.39	-255.96	-76.57	0	-926.26	1.8	-356.12	1.8	-329.48	2.12	-239.86
62	62	79.10	-1807.77	-255.71	-76.60	0	-926.40	1.8	-356.21	1.8	-329.56	2.12	-239.94
62	63	80.20	-1807.77	-225.05	189.16	0	-705.77	1.8	-389.56	1.8	-364.42	2.12	-316.27
63	63	80.20	-2065.61	-224.85	62.66	0	-1082.12	1.8	-406.86	1.8	-379.45	2.12	-272.75
63	64	81.30	-2065.61	-197.15	294.44	0	-890.70	1.8	-434.92	1.8	-408.82	2.12	-337.99
64	64	81.30	-2066.31	-196.98	294.33	0	-890.99	1.8	-435.07	1.8	-408.95	2.12	-338.10
64	65	82.40	-2066.31	-170.49	496.33	0	-724.70	1.8	-459.07	1.8	-433.91	2.12	-394.11
65	65	82.40	-1566.09	-170.33	80.30	0	-1068.07	1.8	-262.58	1.8	-257.78	2.12	-130.91
65	66	83.50	-1566.09	-147.19	254.37	0	-925.13	1.8	-283.04	1.8	-278.78	2.12	-178.52
66	66	83.50	-1567.05	-146.96	254.39	0	-916.46	1.8	-291.98	1.8	-286.55	2.12	-189.02
66	67	84.60	-1567.05	-97.48	376.24	0	-817.16	1.8	-305.77	1.8	-300.78	2.12	-221.67
67	67	84.60	-874.65	-95.11	46.77	0	-835.64	1.8	-114.91	1.8	-118.35	2.12	-2.95
67	68	85.70	-875.52	-77.83	144.34	0	-766.70	1.8	-126.70	1.8	-133.34	2.12	-31.32
68	68	85.70	-1065.95	-79.96	59.57	0	-887.39	1.8	-98.27	1.8	-129.05	2.12	-21.75
68	69	86.80	-1065.95	-62.66	138.02	0	-836.05	1.8	-108.96	1.8	-141.99	2.12	-44.69
69	69	86.80	-1065.96	-62.69	137.99	0	-836.07	1.8	-108.96	1.8	-141.99	2.12	-44.68
69	70	87.90	-1065.96	-45.39	197.44	0	-797.55	1.8	-116.91	1.8	-151.84	2.12	-62.03
70	70	87.90	-1065.96	-45.43	197.43	0	-797.56	1.8	-116.91	1.8	-151.84	2.12	-62.02
70	71	89.00	-1065.96	-28.15	237.90	0	-771.85	1.8	-122.12	1.8	-158.61	2.12	-73.79
71	71	89.00	-1065.96	-28.21	237.90	0	-771.85	1.8	-122.12	1.8	-158.61	2.12	-73.79
71	72	90.10	-1065.96	-10.93	259.43	0	-758.92	1.8	-124.61	1.8	-162.31	2.12	-79.97
72	72	90.10	-1065.96	-10.96	259.41	0	-758.94	1.8	-124.60	1.8	-162.31	2.12	-79.97
72	73	91.20	-1065.96	6.34	261.93	0	-758.84	1.8	-124.35	1.8	-162.92	2.12	-80.55
73	73	91.20	-1065.96	6.28	261.96	0	-758.82	1.8	-124.35	1.8	-162.92	2.12	-80.56
73	74	92.30	-1065.96	23.62	245.46	0	-771.56	1.8	-121.36	1.8	-160.44	2.12	-75.55
74	74	92.30	-1065.96	23.62	245.48	0	-771.55	1.8	-121.36	1.8	-160.45	2.12	-75.56
74	75	93.40	-1065.96	40.89	210.01	0	-797.10	1.8	-115.63	1.8	-154.89	2.12	-64.96
75	75	93.40	-1065.96	40.88	210.05	0	-952.77	1.8	-152.56	1.8	-168.25	2.12	-41.32
75	76	94.50	-1065.96	58.15	155.55	0	-998.52	1.8	-145.34	1.8	-160.30	2.12	-24.69

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ-
C. Cuasipermanentes Mz-
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	58.18	240.33	0	-734.87	1.8	-132.47	1.8	-148.41	2.12	-53.71
76	77	95.60	-882.17	75.46	166.84	0	-796.08	1.8	-123.19	1.8	-137.79	2.12	-31.44
77	77	95.60	-882.17	75.48	166.89	0	-796.03	1.8	-123.20	1.8	-137.79	2.12	-31.46
77	78	96.70	-882.17	92.75	74.35	0	-872.76	1.8	-111.85	1.8	-124.50	2.12	-3.52
78	78	96.70	-698.39	92.80	160.98	0	-607.66	1.8	-99.05	1.8	-112.84	2.12	-33.07
78	79	97.80	-698.39	110.08	49.39	0	-699.91	1.8	-85.63	1.8	-96.87	2.12	0.53
79	79	97.80	-698.38	110.16	49.45	0	-699.86	1.8	-85.64	1.8	-96.88	2.12	0.51
79	80	98.90	-698.38	127.44	-81.24	0	-807.66	1.8	-70.14	1.8	-78.23	2.12	39.79
80	80	98.90	-441.09	127.54	45.17	0	-432.54	1.8	-52.43	1.8	-62.57	2.12	-3.03
80	81	100.00	-441.09	200.12	-105.06	0	-556.20	1.8	-34.89	1.8	-41.19	2.12	42.03
101	101	0.00	-441.09	-170.60	-105.00	0	-556.16	1.8	-34.90	1.8	-41.20	2.12	42.01
101	102	1.10	-436.66	-121.97	38.78	0	-433.61	1.8	-50.93	1.8	-61.00	2.12	-1.01
102	102	1.10	-693.96	-122.20	-87.45	0	-808.58	1.8	-68.67	1.8	-76.69	2.12	41.74
102	103	2.20	-693.96	-105.51	37.79	0	-705.35	1.8	-83.29	1.8	-94.54	2.12	4.14
103	103	2.20	-693.96	-105.71	37.89	0	-705.26	1.8	-83.30	1.8	-94.55	2.12	4.11
103	104	3.30	-693.96	-89.03	144.96	0	-616.80	1.8	-95.99	1.8	-109.86	2.12	-28.10
104	104	3.30	-877.74	-89.16	58.48	0	-881.77	1.8	-108.81	1.8	-121.53	2.12	1.40
104	105	4.40	-877.74	-72.50	147.41	0	-808.06	1.8	-119.58	1.8	-134.30	2.12	-25.42
105	105	4.40	-877.74	-72.62	147.47	0	-808.01	1.8	-119.59	1.8	-134.31	2.12	-25.44
105	106	5.50	-877.74	-55.94	218.16	0	-749.14	1.8	-128.42	1.8	-144.51	2.12	-46.86
106	106	5.50	-1061.53	-56.01	133.49	0	-1012.70	1.8	-141.31	1.8	-156.42	2.12	-17.86
106	107	6.60	-1061.53	-39.33	185.93	0	-968.69	1.8	-148.19	1.8	-164.07	2.12	-33.86
107	107	6.60	-1061.53	-39.38	185.97	0	-810.02	1.8	-111.15	1.8	-150.57	2.12	-57.79
107	108	7.70	-1061.53	-22.71	220.10	0	-785.45	1.8	-116.64	1.8	-155.92	2.12	-67.98
108	108	7.70	-1061.53	-22.74	220.14	0	-785.42	1.8	-116.65	1.8	-155.92	2.12	-67.99
108	109	8.80	-1061.53	-6.06	235.99	0	-773.21	1.8	-119.53	1.8	-158.29	2.12	-72.79
109	109	8.80	-1061.53	-6.09	235.99	0	-773.20	1.8	-119.53	1.8	-158.29	2.12	-72.79
109	110	9.90	-1061.53	10.58	233.52	0	-773.35	1.8	-119.78	1.8	-157.68	2.12	-72.19
110	110	9.90	-1061.53	10.57	233.53	0	-773.35	1.8	-119.78	1.8	-157.68	2.12	-72.19
110	111	11.00	-1061.53	27.24	212.74	0	-785.88	1.8	-117.40	1.8	-154.08	2.12	-66.19
111	111	11.00	-1061.53	27.25	212.72	0	-785.90	1.8	-117.40	1.8	-154.07	2.12	-66.18
111	112	12.10	-1061.53	43.91	173.58	0	-810.83	1.8	-112.39	1.8	-147.49	2.12	-54.77
112	112	12.10	-1061.53	43.90	173.55	0	-810.85	1.8	-112.38	1.8	-147.48	2.12	-54.76
112	113	13.20	-1061.53	60.58	116.09	0	-848.16	1.8	-104.74	1.8	-137.91	2.12	-37.94
113	113	13.20	-1061.53	60.56	116.05	0	-848.19	1.8	-104.73	1.8	-137.90	2.12	-37.93
113	114	14.30	-1061.53	77.25	40.25	0	-897.90	1.8	-94.46	1.8	-125.34	2.12	-15.70
114	114	14.30	-871.84	72.60	124.94	0	-779.91	1.8	-123.02	1.8	-129.79	2.12	-25.06
114	115	15.40	-874.66	91.78	32.08	0	-848.22	1.8	-112.23	1.8	-116.00	2.12	1.78
115	115	15.40	-1567.05	94.12	361.45	0	-829.68	1.8	-303.40	1.8	-298.70	2.12	-217.25
115	116	16.50	-1567.05	137.58	243.46	0	-925.87	1.8	-289.94	1.8	-284.77	2.12	-185.47
116	116	16.50	-1567.05	137.43	243.37	0	-936.03	1.8	-280.09	1.8	-276.22	2.12	-173.83
116	117	17.60	-1567.05	159.33	80.27	0	-1070.30	1.8	-260.53	1.8	-256.02	2.12	-128.56
117	117	17.60	-2068.15	159.10	496.56	0	-726.99	1.8	-457.24	1.8	-432.38	2.12	-392.01
117	118	18.70	-2068.15	186.58	306.15	0	-884.37	1.8	-433.89	1.8	-408.04	2.12	-338.17
118	118	18.70	-2068.15	186.37	306.15	0	-884.36	1.8	-433.90	1.8	-408.06	2.12	-338.19
118	119	19.80	-2068.15	215.54	85.41	0	-1067.72	1.8	-405.96	1.8	-378.86	2.12	-274.48
119	119	19.80	-1810.85	215.40	211.76	0	-691.65	1.8	-388.77	1.8	-363.93	2.12	-318.07
119	120	20.90	-1810.85	248.05	-44.97	0	-906.46	1.8	-354.59	1.8	-328.43	2.12	-241.96
120	120	20.90	-1810.85	247.98	-44.98	0	-906.47	1.8	-354.59	1.8	-328.43	2.12	-241.96
120	121	22.00	-1810.85	275.62	-332.12	0	-1147.04	1.8	-316.14	1.8	-288.12	2.12	-156.06
121	1121	22.00	-1847.60	-302.37	-351.27	0	-1201.63	1.8	-318.55	1.8	-290.11	2.12	-149.52
121	122	23.40	-1847.60	-267.86	46.98	0	-867.51	1.8	-371.42	1.8	-346.40	2.12	-269.23
122	122	23.40	-1847.60	-267.94	47.00	0	-867.49	1.8	-371.41	1.8	-346.40	2.12	-269.23
122	123	24.80	-1847.60	-232.66	397.19	0	-573.95	1.8	-417.72	1.8	-395.20	2.12	-373.62
123	123	24.80	-2104.90	-232.65	273.51	0	-947.93	1.8	-435.04	1.8	-410.49	2.12	-330.80
123	124	26.20	-2104.90	-192.78	568.78	0	-702.05	1.8	-472.23	1.8	-449.95	2.12	-416.62
124	124	26.20	-1420.02	-193.02	239.34	0	-779.42	1.8	-263.05	1.8	-262.45	2.12	-183.29
124	125	27.60	-1420.02	-159.10	485.35	0	-575.74	1.8	-292.77	1.8	-294.01	2.12	-253.08
125	125	27.60	-1750.84	-159.36	336.14	0	-1048.94	1.8	-315.48	1.8	-314.98	2.12	-200.84
125	126	29.00	-1750.84	-104.88	504.53	0	-910.36	1.8	-334.84	1.8	-336.00	2.12	-247.83
126	126	29.00	-1061.03	-103.63	175.18	0	-918.11	1.8	-153.26	1.8	-160.07	2.12	-38.26
126	127	30.40	-1058.64	-80.31	306.67	0	-818.28	1.8	-168.40	1.8	-179.40	2.12	-76.67
127	127	30.40	-1356.26	-83.13	179.98	0	-1051.54	1.8	-141.74	1.8	-181.45	2.12	-59.87
127	128	31.80	-1356.26	-61.87	281.46	0	-984.07	1.8	-155.75	1.8	-198.09	2.12	-89.67
128	128	31.80	-1356.26	-61.82	281.52	0	-984.03	1.8	-155.76	1.8	-198.10	2.12	-89.68
128	129	33.20	-1356.26	-40.61	353.21	0	-936.72	1.8	-165.49	1.8	-209.89	2.12	-110.69
129	129	33.20	-1356.26	-40.56	353.25	0	-936.69	1.8	-165.49	1.8	-209.89	2.12	-110.71
129	130	34.60	-1356.26	-19.04	394.95	0	-909.68	1.8	-170.90	1.8	-216.79	2.12	-122.86
130	130	34.60	-1356.26	-18.98	394.95	0	-909.67	1.8	-170.90	1.8	-216.79	2.12	-122.86
130	131	36.00	-1356.26	3.36	405.75	0	-903.71	1.8	-171.82	1.8	-218.65	2.12	-125.87
131	131	36.00	-1356.26	3.41	405.76	0	-903.70	1.8	-171.82	1.8	-218.65	2.12	-125.87
131	132	37.40	-1356.26	24.66	386.09	0	-918.42	1.8	-168.33	1.8	-215.54	2.12	-119.87
132	132	37.40	-1356.26	24.72	386.08	0	-918.43	1.8	-168.32	1.8	-215.54	2.12	-119.87
132	133	38.80	-1356.26	45.95	336.62	0	-953.29	1.8	-160.55	1.8	-207.58	2.12	-105.08
133	133	38.80	-1356.26	46.00	336.59	0	-953.31	1.8	-160.55	1.8	-207.58	2.12	-105.07

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CUASIPERM1.Tinf.MZ-
C. Cuasipermanentes Mz-
[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	67.24	257.33	0	-1008.32	1.8	-148.49	1.8	-194.76	2.12	-81.50
134	134	40.20	-1356.26	67.27	257.28	0	-1008.36	1.8	-148.49	1.8	-194.75	2.12	-81.48
134	135	41.60	-1356.26	88.54	148.21	0	-1083.53	1.8	-132.15	1.8	-177.08	2.12	-49.11
135	135	41.60	-1060.58	86.20	274.91	0	-865.15	1.8	-158.92	1.8	-175.06	2.12	-63.87
135	136	43.00	-1063.03	109.35	136.98	0	-974.71	1.8	-141.81	1.8	-154.98	2.12	-22.94
136	136	43.00	-1750.84	110.10	466.33	0	-947.95	1.8	-325.63	1.8	-327.33	2.12	-231.69
136	137	44.40	-1750.84	163.26	284.79	0	-1098.33	1.8	-304.08	1.8	-304.23	2.12	-180.39
137	137	44.40	-1420.02	163.01	433.95	0	-625.18	1.8	-281.36	1.8	-283.25	2.12	-232.61
137	138	45.80	-1420.02	196.21	183.32	0	-833.29	1.8	-250.88	1.8	-250.89	2.12	-161.16
138	138	45.80	-2104.90	195.92	512.79	0	-755.90	1.8	-460.06	1.8	-438.40	2.12	-394.51
138	139	47.20	-2104.90	231.38	214.55	0	-1004.60	1.8	-422.59	1.8	-398.55	2.12	-307.77
139	139	47.20	-1847.60	231.15	338.29	0	-630.57	1.8	-405.28	1.8	-383.27	2.12	-350.61
139	140	48.60	-1841.15	271.09	-14.70	0	-924.88	1.8	-357.22	1.8	-332.76	2.12	-244.07
140	140	48.60	-1840.98	271.01	-14.77	0	-924.88	1.8	-357.18	1.8	-332.72	2.12	-244.02
140	141	50.00	-1840.98	306.23	-418.34	0	-1264.02	1.8	-303.45	1.8	-275.54	2.12	-122.46
141	1141	50.00	-1841.18	-306.14	-418.34	0	-1264.08	1.8	-303.50	1.8	-275.58	2.12	-122.50
141	142	51.40	-1841.18	-270.92	-14.89	0	-925.04	1.8	-357.22	1.8	-332.75	2.12	-244.03
142	142	51.40	-1841.79	-271.00	-14.81	0	-925.15	1.8	-357.37	1.8	-332.89	2.12	-244.18
142	143	52.80	-1841.79	-231.56	338.14	0	-629.05	1.8	-403.81	1.8	-381.95	2.12	-349.30
143	143	52.80	-2100.09	-231.76	214.51	0	-1003.27	1.8	-421.39	1.8	-397.47	2.12	-306.71
143	144	54.20	-2104.90	-195.92	512.76	0	-755.92	1.8	-460.06	1.8	-438.39	2.12	-394.50
144	144	54.20	-1420.02	-196.22	183.31	0	-833.30	1.8	-250.88	1.8	-250.89	2.12	-161.16
144	145	55.60	-1420.02	-163.02	433.96	0	-625.17	1.8	-281.36	1.8	-283.25	2.12	-232.62
145	145	55.60	-1750.84	-163.26	284.80	0	-1098.33	1.8	-304.08	1.8	-304.23	2.12	-180.39
145	146	57.00	-1750.84	-110.10	466.33	0	-947.96	1.8	-325.63	1.8	-327.32	2.12	-231.69
146	146	57.00	-1063.03	-109.36	136.97	0	-974.72	1.8	-141.80	1.8	-154.97	2.12	-22.93
146	147	58.40	-1062.37	-87.13	275.80	0	-866.03	1.8	-159.19	1.8	-175.47	2.12	-64.20
147	147	58.40	-1358.27	-88.47	149.12	0	-1084.58	1.8	-132.45	1.8	-177.52	2.12	-49.46
147	148	59.80	-1358.27	-67.21	258.09	0	-1009.48	1.8	-148.77	1.8	-195.18	2.12	-81.80
148	148	59.80	-1358.28	-67.18	258.14	0	-1009.45	1.8	-148.78	1.8	-195.19	2.12	-81.82
148	149	61.20	-1358.28	-45.95	337.31	0	-954.50	1.8	-160.82	1.8	-207.99	2.12	-105.37
149	149	61.20	-1358.27	-45.89	337.34	0	-954.48	1.8	-160.82	1.8	-207.99	2.12	-105.38
149	150	62.60	-1358.27	-24.66	386.74	0	-919.66	1.8	-168.59	1.8	-215.94	2.12	-120.15
150	150	62.60	-1358.27	-24.60	386.76	0	-919.64	1.8	-168.59	1.8	-215.94	2.12	-120.15
150	151	64.00	-1360.02	-3.33	406.31	0	-906.43	1.8	-172.23	1.8	-219.28	2.12	-126.19
151	151	64.00	-1360.02	-3.28	406.31	0	-906.44	1.8	-172.23	1.8	-219.28	2.12	-126.19
151	152	65.40	-1360.02	19.06	395.39	0	-912.48	1.8	-171.30	1.8	-217.40	2.12	-123.14
152	152	65.40	-1360.02	19.12	395.39	0	-912.48	1.8	-171.30	1.8	-217.40	2.12	-123.14
152	153	66.80	-1360.02	40.63	353.59	0	-939.56	1.8	-165.88	1.8	-210.48	2.12	-110.96
153	153	66.80	-1360.02	40.69	353.55	0	-939.59	1.8	-165.87	1.8	-210.48	2.12	-110.95
153	154	68.20	-1360.02	61.90	281.73	0	-986.99	1.8	-156.13	1.8	-198.67	2.12	-89.90
154	154	68.20	-1360.02	61.95	281.68	0	-987.02	1.8	-156.12	1.8	-198.66	2.12	-89.89
154	155	69.60	-1360.02	83.20	180.10	0	-1054.55	1.8	-142.10	1.8	-182.01	2.12	-60.06
155	155	69.60	-1061.89	82.18	306.78	0	-820.89	1.8	-168.71	1.8	-179.88	2.12	-76.84
155	156	71.00	-1061.02	103.63	175.18	0	-918.10	1.8	-153.26	1.8	-160.07	2.12	-38.26
156	156	71.00	-1750.84	104.87	504.53	0	-910.35	1.8	-334.83	1.8	-336.00	2.12	-247.83
156	157	72.40	-1750.84	159.37	336.15	0	-1048.93	1.8	-315.48	1.8	-314.98	2.12	-200.84
157	157	72.40	-1420.02	159.10	485.35	0	-575.74	1.8	-292.77	1.8	-294.01	2.12	-253.08
157	158	73.80	-1420.02	193.02	239.34	0	-779.42	1.8	-263.05	1.8	-262.45	2.12	-183.29
158	158	73.80	-2104.90	192.79	568.77	0	-702.06	1.8	-472.23	1.8	-449.95	2.12	-416.62
158	159	75.20	-2104.90	232.65	273.49	0	-947.94	1.8	-435.04	1.8	-410.49	2.12	-330.80
159	159	75.20	-1847.60	232.65	397.19	0	-573.95	1.8	-417.72	1.8	-395.20	2.12	-373.62
159	160	76.60	-1843.78	268.41	46.50	0	-866.82	1.8	-370.39	1.8	-345.49	2.12	-268.26
160	160	76.60	-1843.83	268.35	46.37	0	-866.94	1.8	-370.39	1.8	-345.49	2.12	-268.25
160	161	78.00	-1843.83	302.86	-352.57	0	-1201.63	1.8	-317.44	1.8	-289.12	2.12	-148.35
161	1161	78.00	-1807.39	-275.77	-333.44	0	-1147.16	1.8	-315.11	1.8	-287.20	2.12	-154.96
161	162	79.10	-1807.39	-248.14	-46.16	0	-906.47	1.8	-353.58	1.8	-327.52	2.12	-240.89
162	162	79.10	-1807.77	-248.21	-46.16	0	-906.58	1.8	-353.67	1.8	-327.60	2.12	-240.97
162	163	80.20	-1807.77	-215.57	210.77	0	-691.60	1.8	-387.88	1.8	-363.12	2.12	-317.13
163	163	80.20	-2065.60	-215.70	84.44	0	-1067.80	1.8	-405.20	1.8	-378.18	2.12	-273.67
163	164	81.30	-2065.60	-186.53	305.36	0	-884.30	1.8	-433.17	1.8	-407.40	2.12	-337.42
164	164	81.30	-2066.31	-186.73	305.43	0	-884.46	1.8	-433.34	1.8	-407.55	2.12	-337.58
164	165	82.40	-2066.31	-159.25	495.99	0	-726.94	1.8	-456.71	1.8	-431.90	2.12	-391.46
165	165	82.40	-1566.09	-159.43	80.17	0	-1070.13	1.8	-260.25	1.8	-255.80	2.12	-128.33
165	166	83.50	-1566.09	-137.53	242.98	0	-936.08	1.8	-279.80	1.8	-275.96	2.12	-173.51
166	166	83.50	-1567.05	-137.61	243.18	0	-926.11	1.8	-289.90	1.8	-284.74	2.12	-185.40
166	167	84.60	-1567.05	-94.15	361.21	0	-829.88	1.8	-303.37	1.8	-298.67	2.12	-217.19
167	167	84.60	-874.65	-91.79	31.84	0	-848.38	1.8	-112.20	1.8	-115.96	2.12	1.85
167	168	85.70	-875.52	-75.07	126.03	0	-782.22	1.8	-123.49	1.8	-130.49	2.12	-25.53
168	168	85.70	-1065.96	-77.18	41.35	0	-900.83	1.8	-95.00	1.8	-126.16	2.12	-16.21
168	169	86.80	-1065.96	-60.50	117.07	0	-851.16	1.8	-105.26	1.8	-138.70	2.12	-38.42
169	169	86.80	-1065.96	-60.51	117.11	0	-851.14	1.8	-105.27	1.8	-138.71	2.12	-38.43
169	170	87.90	-1065.96	-43.83	174.50	0	-813.87	1.8	-112.90	1.8	-148.27	2.12	-55.22
170	170	87.90	-1065.96	-43.84	174.52	0	-813.86	1.8	-112.91	1.8	-148.27	2.12	-55.23
170	171	89.00	-1065.96	-27.18	213.58	0	-788.98	1.8	-117.91	1.8	-154.85	2.12	-66.62

CÁLCULO TENSIONAL

Hipótesis de cálculo:

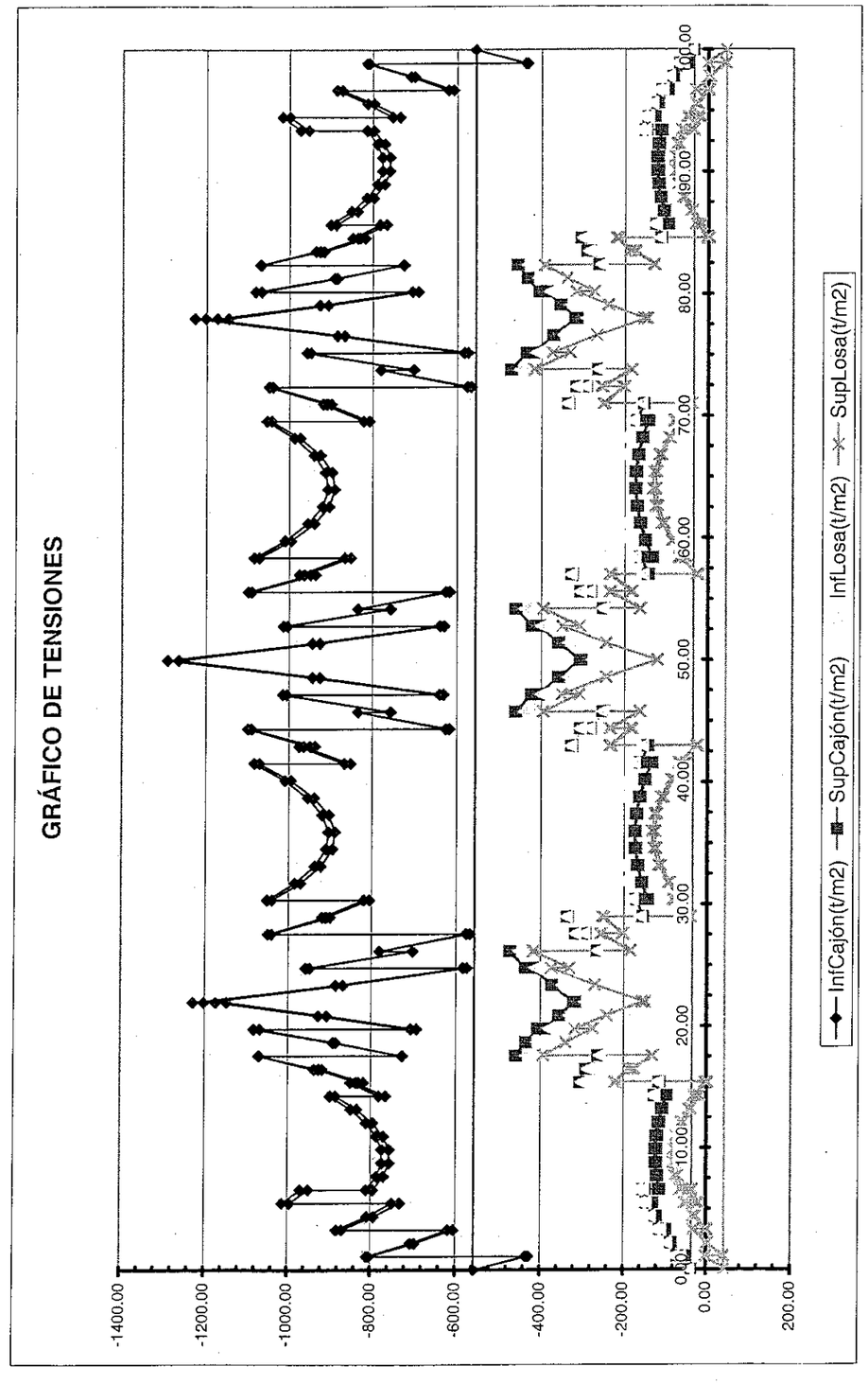
CUASIPERM1.Tinf.MZ-

C. Cuasipermanentes Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Cosf. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1065.96	-27.19	213.60	0	-788.96	1.8	-117.91	1.8	-154.85	2.12	-66.62
171	172	90.10	-1065.96	-10.50	234.30	0	-776.49	1.8	-120.28	1.8	-158.44	2.12	-72.60
172	172	90.10	-1065.96	-10.50	234.29	0	-776.50	1.8	-120.28	1.8	-158.44	2.12	-72.60
172	173	91.20	-1065.96	6.17	236.67	0	-776.40	1.8	-120.02	1.8	-159.04	2.12	-73.17
173	173	91.20	-1065.96	6.13	236.66	0	-776.41	1.8	-120.02	1.8	-159.03	2.12	-73.17
173	174	92.30	-1065.96	22.81	220.74	0	-788.68	1.8	-117.13	1.8	-156.65	2.12	-68.35
174	174	92.30	-1065.96	22.78	220.70	0	-788.70	1.8	-117.12	1.8	-156.65	2.12	-68.34
174	175	93.40	-1065.96	39.45	186.49	0	-813.33	1.8	-111.62	1.8	-151.29	2.12	-58.12
175	175	93.40	-1065.96	39.39	186.45	0	-972.56	1.8	-148.69	1.8	-164.77	2.12	-34.06
175	176	94.50	-1065.96	56.07	133.90	0	-1016.66	1.8	-141.80	1.8	-157.11	2.12	-18.04
176	176	94.50	-882.17	56.00	218.59	0	-753.09	1.8	-128.91	1.8	-145.20	2.12	-47.04
176	177	95.60	-882.17	72.68	147.81	0	-812.02	1.8	-120.08	1.8	-134.98	2.12	-25.60
177	177	95.60	-882.17	72.57	147.74	0	-812.08	1.8	-120.07	1.8	-134.97	2.12	-25.58
177	178	96.70	-882.17	89.23	58.72	0	-885.85	1.8	-109.30	1.8	-122.20	2.12	1.28
178	178	96.70	-698.39	89.09	145.23	0	-620.87	1.8	-96.48	1.8	-110.53	2.12	-28.23
178	179	97.80	-698.39	105.76	38.05	0	-709.41	1.8	-83.78	1.8	-95.21	2.12	4.01
179	179	97.80	-698.40	105.59	37.95	0	-709.50	1.8	-83.77	1.8	-95.19	2.12	4.04
179	180	98.90	-698.40	122.28	-87.38	0	-812.81	1.8	-69.14	1.8	-77.33	2.12	41.66
180	180	98.90	-441.09	122.04	38.88	0	-437.82	1.8	-51.41	1.8	-61.65	2.12	-1.10
180	181	100.00	-441.09	170.59	-105.00	0	-556.16	1.8	-34.90	1.8	-41.20	2.12	42.01



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ+
C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-164.06	-85.30	0	-492.43	1.8	-30.95	1.8	-36.74	2.12	36.97
1	2	1.10	-395.79	-257.53	214.67	0	-244.64	1.8	-76.89	1.8	-83.27	2.12	-56.98
2	2	1.10	-624.09	-257.84	106.80	0	-577.03	1.8	-92.68	1.8	-97.25	2.12	-19.12
2	3	2.20	-624.09	-225.11	369.79	0	-355.76	1.8	-132.86	1.8	-137.57	2.12	-101.55
3	3	2.20	-624.08	-225.37	369.90	0	-355.66	1.8	-132.89	1.8	-137.59	2.12	-101.59
3	4	3.30	-624.08	-192.71	595.59	0	-165.55	1.8	-167.60	1.8	-172.26	2.12	-172.42
4	4	3.30	-787.15	-192.88	521.84	0	-400.40	1.8	-179.01	1.8	-182.67	2.12	-146.31
4	5	4.40	-787.15	-155.30	710.09	0	-241.56	1.8	-208.23	1.8	-211.67	2.12	-205.49
5	5	4.40	-787.15	-155.40	710.21	0	-241.46	1.8	-208.25	1.8	-211.69	2.12	-205.53
5	6	5.50	-787.15	-121.05	866.96	0	-108.79	1.8	-233.11	1.8	-236.00	2.12	-255.03
6	6	5.50	-950.22	-121.14	794.78	0	-342.42	1.8	-244.58	1.8	-246.62	2.12	-229.36
6	7	6.60	-950.22	-88.38	914.40	0	-240.76	1.8	-263.99	1.8	-265.31	2.12	-267.31
7	7	6.60	-950.22	-88.46	914.48	0	-152.00	1.8	-234.44	1.8	-255.91	2.12	-283.60
7	8	7.70	-950.22	-55.76	996.89	0	-88.77	1.8	-249.14	1.8	-269.36	2.12	-309.31
8	8	7.70	-950.22	-55.75	996.94	0	-88.73	1.8	-249.15	1.8	-269.37	2.12	-309.33
8	9	8.80	-950.22	-23.30	1041.26	0	-53.38	1.8	-257.50	1.8	-276.57	2.12	-323.39
9	9	8.80	-950.22	-23.25	1041.29	0	-53.35	1.8	-257.51	1.8	-276.57	2.12	-323.40
9	10	9.90	-950.22	9.36	1053.82	0	-40.74	1.8	-260.72	1.8	-278.59	2.12	-327.84
10	10	9.90	-950.22	9.45	1053.83	0	-40.73	1.8	-260.72	1.8	-278.59	2.12	-327.84
10	11	11.00	-950.22	42.24	1029.48	0	-55.01	1.8	-257.82	1.8	-274.57	2.12	-321.02
11	11	11.00	-950.22	42.29	1029.49	0	-55.00	1.8	-257.82	1.8	-274.57	2.12	-321.02
11	12	12.10	-950.22	75.02	968.02	0	-96.37	1.8	-248.75	1.8	-264.46	2.12	-302.85
12	12	12.10	-950.22	75.13	968.00	0	-96.39	1.8	-248.75	1.8	-264.45	2.12	-302.84
12	13	13.20	-950.22	107.62	868.92	0	-165.24	1.8	-233.41	1.8	-248.18	2.12	-273.17
13	13	13.20	-950.22	107.71	868.88	0	-165.28	1.8	-233.40	1.8	-248.17	2.12	-273.15
13	14	14.30	-950.22	140.49	736.39	0	-258.18	1.8	-212.62	1.8	-226.44	2.12	-233.34
14	14	14.30	-780.33	141.20	808.59	0	-108.90	1.8	-235.82	1.8	-228.58	2.12	-246.22
14	15	15.40	-775.77	171.44	638.14	0	-237.01	1.8	-210.38	1.8	-201.36	2.12	-194.20
15	15	15.40	-1554.62	173.68	1009.37	0	-206.59	1.8	-424.18	1.8	-403.44	2.12	-438.12
15	16	16.50	-1554.62	173.97	808.62	0	-373.13	1.8	-396.93	1.8	-377.45	2.12	-381.15
16	16	16.50	-1554.62	173.84	808.44	0	-335.33	1.8	-433.93	1.8	-409.58	2.12	-424.83
16	17	17.60	-1554.62	189.52	605.21	0	-511.89	1.8	-398.60	1.8	-375.78	2.12	-357.10
17	17	17.60	-2163.46	189.53	1050.43	0	-188.86	1.8	-623.68	1.8	-577.56	2.12	-647.22
17	18	18.70	-2163.46	187.16	836.04	0	-373.27	1.8	-588.83	1.8	-543.34	2.12	-577.67
18	18	18.70	-2163.46	187.17	835.59	0	-373.72	1.8	-588.69	1.8	-543.22	2.12	-577.46
18	19	19.80	-2163.46	189.17	627.33	0	-549.17	1.8	-559.44	1.8	-512.99	2.12	-513.88
19	19	19.80	-1935.17	189.12	734.77	0	-216.23	1.8	-544.03	1.8	-499.61	2.12	-552.31
19	20	20.90	-1935.17	191.15	525.36	0	-389.79	1.8	-518.26	1.8	-471.54	2.12	-491.45
20	20	20.90	-1935.17	190.77	525.38	0	-389.77	1.8	-518.27	1.8	-471.54	2.12	-491.46
20	21	22.00	-1935.17	196.04	312.17	0	-563.69	1.8	-495.57	1.8	-445.04	2.12	-432.25
21	1021	22.00	-1967.78	-207.75	295.75	0	-612.10	1.8	-497.70	1.8	-446.80	2.12	-426.44
21	22	23.40	-1967.78	-192.18	580.09	0	-382.10	1.8	-524.63	1.8	-480.41	2.12	-503.18
22	22	23.40	-1967.78	-192.60	580.03	0	-382.15	1.8	-524.62	1.8	-480.40	2.12	-503.16
22	23	24.80	-1967.78	-187.16	847.21	0	-163.38	1.8	-553.31	1.8	-513.75	2.12	-577.65
23	23	24.80	-2196.07	-187.65	741.48	0	-495.10	1.8	-568.66	1.8	-527.30	2.12	-539.63
23	24	26.20	-2196.07	-208.61	1014.93	0	-265.38	1.8	-605.36	1.8	-566.21	2.12	-622.16
24	24	26.20	-1424.17	-209.36	644.37	0	-352.04	1.8	-369.40	1.8	-354.70	2.12	-359.05
24	25	27.60	-1424.17	-199.82	927.77	0	-107.81	1.8	-415.17	1.8	-400.09	2.12	-451.26
25	25	27.60	-1717.69	-199.85	801.30	0	-526.80	1.8	-435.50	1.8	-418.85	2.12	-405.20
25	26	29.00	-1717.69	-211.04	1105.14	0	-263.37	1.8	-486.95	1.8	-467.91	2.12	-504.66
26	26	29.00	-941.07	-209.66	734.06	0	-329.10	1.8	-237.92	1.8	-233.84	2.12	-217.41
26	27	30.40	-945.20	-171.99	998.36	0	-120.82	1.8	-278.31	1.8	-275.67	2.12	-299.23
27	27	30.40	-1210.45	-171.04	890.72	0	-376.81	1.8	-257.73	1.8	-279.85	2.12	-279.67
27	28	31.80	-1210.45	-128.63	1096.13	0	-227.91	1.8	-291.35	1.8	-313.63	2.12	-342.36
28	28	31.80	-1210.45	-128.43	1096.25	0	-227.81	1.8	-291.37	1.8	-313.65	2.12	-342.40
28	29	33.20	-1210.45	-82.22	1243.28	0	-121.36	1.8	-315.34	1.8	-337.88	2.12	-387.27
29	29	33.20	-1210.45	-82.02	1243.39	0	-121.26	1.8	-315.36	1.8	-337.90	2.12	-387.31
29	30	34.60	-1210.45	-45.59	1333.46	0	-56.11	1.8	-329.95	1.8	-352.80	2.12	-414.83
30	30	34.60	-1210.45	-45.34	1333.51	0	-56.07	1.8	-329.96	1.8	-352.81	2.12	-414.85
30	31	36.00	-1210.45	-3.43	1362.81	0	-35.34	1.8	-334.44	1.8	-357.75	2.12	-423.78
31	31	36.00	-1210.45	-3.24	1362.82	0	-35.34	1.8	-334.44	1.8	-357.75	2.12	-423.78
31	32	37.40	-1210.45	43.35	1336.36	0	-54.92	1.8	-329.77	1.8	-353.57	2.12	-415.75
32	32	37.40	-1210.45	43.58	1336.33	0	-54.95	1.8	-329.77	1.8	-353.57	2.12	-415.74
32	33	38.80	-1210.45	80.00	1249.05	0	-118.99	1.8	-314.97	1.8	-339.41	2.12	-389.10
33	33	38.80	-1210.45	80.23	1248.97	0	-119.07	1.8	-314.95	1.8	-339.39	2.12	-389.07
33	34	40.20	-1210.45	126.47	1104.78	0	-224.36	1.8	-290.79	1.8	-315.93	2.12	-345.11
34	34	40.20	-1210.45	126.65	1104.67	0	-224.46	1.8	-290.77	1.8	-315.91	2.12	-345.06
34	35	41.60	-1210.45	169.07	901.98	0	-372.31	1.8	-256.93	1.8	-282.86	2.12	-283.24
35	35	41.60	-946.85	170.44	1009.59	0	-129.46	1.8	-277.54	1.8	-278.62	2.12	-300.91
35	36	43.00	-942.63	208.55	746.75	0	-339.85	1.8	-236.96	1.8	-237.37	2.12	-219.34
36	36	43.00	-1717.69	209.53	1117.85	0	-249.72	1.8	-494.91	1.8	-474.10	2.12	-513.89
36	37	44.40	-1717.69	204.63	818.58	0	-509.61	1.8	-444.29	1.8	-425.64	2.12	-415.68
37	37	44.40	-1424.17	204.68	945.13	0	-90.55	1.8	-423.99	1.8	-406.89	2.12	-461.77
37	38	45.80	-1424.17	217.08	650.63	0	-345.44	1.8	-375.61	1.8	-359.10	2.12	-365.05
38	38	45.80	-2196.07	216.77	1021.08	0	-258.88	1.8	-611.54	1.8	-570.58	2.12	-628.12

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ+
C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	202.66	730.25	0	-505.34	1.8	-570.41	1.8	-527.68	2.12	-538.27
39	39	47.20	-1967.78	202.87	835.55	0	-174.04	1.8	-554.93	1.8	-514.03	2.12	-576.10
39	40	48.60	-1974.23	201.67	551.49	0	-410.96	1.8	-523.47	1.8	-478.17	2.12	-495.83
40	40	48.60	-1974.41	201.24	551.60	0	-410.92	1.8	-523.53	1.8	-478.22	2.12	-495.90
40	41	50.00	-1974.41	215.97	254.40	0	-653.39	1.8	-493.38	1.8	-441.67	2.12	-413.75
41	1041	50.00	-1974.19	-216.06	254.41	0	-653.32	1.8	-493.32	1.8	-441.62	2.12	-413.70
41	42	51.40	-1974.19	-201.33	551.71	0	-410.77	1.8	-523.49	1.8	-478.19	2.12	-495.88
42	42	51.40	-1973.59	-201.74	551.62	0	-410.68	1.8	-523.33	1.8	-478.04	2.12	-495.72
42	43	52.80	-1973.59	-202.45	835.69	0	-175.57	1.8	-556.40	1.8	-515.35	2.12	-577.41
43	43	52.80	-2200.88	-202.29	730.27	0	-506.68	1.8	-571.61	1.8	-528.76	2.12	-539.33
43	44	54.20	-2196.07	-216.77	1021.08	0	-258.88	1.8	-611.54	1.8	-570.59	2.12	-628.12
44	44	54.20	-1424.17	-217.08	650.62	0	-345.44	1.8	-375.61	1.8	-359.10	2.12	-365.05
44	45	55.60	-1424.17	-204.69	945.16	0	-90.52	1.8	-423.99	1.8	-406.90	2.12	-461.78
45	45	55.60	-1717.69	-204.63	818.62	0	-509.58	1.8	-444.30	1.8	-425.65	2.12	-415.69
45	46	57.00	-1717.69	-209.52	1117.85	0	-249.72	1.8	-494.92	1.8	-474.10	2.12	-513.89
46	46	57.00	-942.63	-208.56	746.77	0	-339.84	1.8	-236.96	1.8	-237.38	2.12	-219.35
46	47	58.40	-945.05	-169.53	1008.71	0	-128.56	1.8	-277.27	1.8	-278.22	2.12	-300.58
47	47	58.40	-1208.44	-169.13	901.09	0	-371.23	1.8	-256.64	1.8	-282.43	2.12	-282.90
47	48	59.80	-1208.44	-126.71	1103.90	0	-223.31	1.8	-290.49	1.8	-315.49	2.12	-344.76
48	48	59.80	-1208.43	-126.52	1104.02	0	-223.20	1.8	-290.51	1.8	-315.51	2.12	-344.79
48	49	61.20	-1208.43	-80.27	1248.23	0	-117.90	1.8	-314.67	1.8	-338.98	2.12	-388.77
49	49	61.20	-1208.44	-80.06	1248.31	0	-117.82	1.8	-314.69	1.8	-339.00	2.12	-388.80
49	50	62.60	-1208.44	-43.64	1335.69	0	-53.72	1.8	-329.50	1.8	-353.17	2.12	-415.47
50	50	62.60	-1208.44	-43.40	1335.73	0	-53.67	1.8	-329.51	1.8	-353.18	2.12	-415.48
50	51	64.00	-1206.69	3.16	1362.24	0	-32.62	1.8	-334.02	1.8	-357.12	2.12	-423.46
51	51	64.00	-1206.69	3.35	1362.25	0	-32.62	1.8	-334.02	1.8	-357.12	2.12	-423.46
51	52	65.40	-1206.69	45.26	1333.07	0	-53.27	1.8	-329.56	1.8	-352.20	2.12	-414.56
52	52	65.40	-1206.69	45.50	1333.00	0	-53.33	1.8	-329.55	1.8	-352.19	2.12	-414.54
52	53	66.80	-1206.69	81.94	1243.09	0	-118.36	1.8	-314.98	1.8	-337.31	2.12	-387.07
53	53	66.80	-1206.69	82.14	1242.98	0	-118.46	1.8	-314.96	1.8	-337.29	2.12	-387.03
53	54	68.20	-1206.69	128.35	1096.06	0	-224.83	1.8	-291.00	1.8	-313.09	2.12	-342.19
54	54	68.20	-1206.69	128.55	1095.95	0	-224.93	1.8	-290.98	1.8	-313.07	2.12	-342.15
54	55	69.60	-1206.69	170.96	890.61	0	-373.79	1.8	-257.37	1.8	-279.29	2.12	-279.49
55	55	69.60	-941.94	170.12	998.26	0	-118.21	1.8	-278.00	1.8	-275.19	2.12	-299.06
55	56	71.00	-941.07	209.68	734.08	0	-329.08	1.8	-237.92	1.8	-233.84	2.12	-217.42
56	56	71.00	-1717.69	211.04	1105.16	0	-263.36	1.8	-486.95	1.8	-467.91	2.12	-504.67
56	57	72.40	-1717.69	199.85	801.32	0	-526.79	1.8	-435.50	1.8	-418.86	2.12	-405.20
57	57	72.40	-1424.17	199.82	927.77	0	-107.81	1.8	-415.17	1.8	-400.09	2.12	-451.26
57	58	73.80	-1424.17	209.35	644.35	0	-352.05	1.8	-369.40	1.8	-354.70	2.12	-359.04
58	58	73.80	-2196.08	208.62	1014.91	0	-265.40	1.8	-605.36	1.8	-566.21	2.12	-622.15
58	59	75.20	-2196.08	187.68	741.48	0	-495.11	1.8	-568.66	1.8	-527.30	2.12	-539.63
59	59	75.20	-1967.78	187.16	847.20	0	-163.39	1.8	-553.30	1.8	-513.75	2.12	-577.65
59	60	76.60	-1971.61	192.12	580.54	0	-382.81	1.8	-525.64	1.8	-481.31	2.12	-504.13
60	60	76.60	-1971.55	191.69	580.68	0	-382.68	1.8	-525.65	1.8	-481.32	2.12	-504.16
60	61	78.00	-1971.55	207.26	297.05	0	-612.10	1.8	-498.81	1.8	-447.79	2.12	-427.61
61	1061	78.00	-1938.62	-195.89	313.50	0	-563.57	1.8	-496.60	1.8	-445.96	2.12	-433.36
61	62	79.10	-1938.62	-190.62	526.53	0	-389.79	1.8	-519.27	1.8	-472.45	2.12	-492.52
62	62	79.10	-1938.24	-191.00	526.51	0	-389.70	1.8	-519.18	1.8	-472.36	2.12	-492.43
62	63	80.20	-1938.24	-188.96	735.75	0	-216.30	1.8	-544.92	1.8	-500.41	2.12	-553.24
63	63	80.20	-2165.99	-189.01	628.28	0	-549.10	1.8	-560.20	1.8	-513.67	2.12	-514.69
63	64	81.30	-2165.99	-187.01	836.37	0	-373.78	1.8	-589.42	1.8	-543.87	2.12	-578.22
64	64	81.30	-2165.29	-187.01	836.77	0	-373.19	1.8	-589.38	1.8	-543.83	2.12	-578.26
64	65	82.40	-2165.29	-189.38	1050.99	0	-188.92	1.8	-624.21	1.8	-578.04	2.12	-647.77
65	65	82.40	-1555.58	-189.43	606.00	0	-511.52	1.8	-398.92	1.8	-376.09	2.12	-357.53
65	66	83.50	-1555.58	-173.74	808.80	0	-335.30	1.8	-434.22	1.8	-409.84	2.12	-425.14
66	66	83.50	-1554.62	-173.96	808.89	0	-372.91	1.8	-396.97	1.8	-377.48	2.12	-381.22
66	67	84.60	-1554.62	-173.68	1009.62	0	-206.39	1.8	-424.21	1.8	-403.47	2.12	-438.19
67	67	84.60	-775.78	-171.42	638.41	0	-236.83	1.8	-210.42	1.8	-201.40	2.12	-194.28
67	68	85.70	-776.65	-138.73	807.50	0	-106.58	1.8	-235.35	1.8	-227.88	2.12	-245.75
68	68	85.70	-945.78	-140.58	735.28	0	-255.26	1.8	-212.08	1.8	-225.62	2.12	-232.83
68	69	86.80	-945.78	-107.80	867.87	0	-162.29	1.8	-232.87	1.8	-247.37	2.12	-272.67
69	69	86.80	-945.79	-107.71	867.92	0	-162.24	1.8	-232.89	1.8	-247.38	2.12	-272.69
69	70	87.90	-945.79	-75.22	967.07	0	-93.35	1.8	-248.23	1.8	-263.67	2.12	-302.39
70	70	87.90	-945.79	-75.10	967.10	0	-93.32	1.8	-248.23	1.8	-263.67	2.12	-302.40
70	71	89.00	-945.79	-42.40	1028.64	0	-51.91	1.8	-257.31	1.8	-273.79	2.12	-320.59
71	71	89.00	-945.79	-42.34	1028.65	0	-51.90	1.8	-257.32	1.8	-273.80	2.12	-320.59
71	72	90.10	-945.79	-9.54	1053.10	0	-37.55	1.8	-260.23	1.8	-277.84	2.12	-327.45
72	72	90.10	-945.79	-9.45	1053.07	0	-37.58	1.8	-260.23	1.8	-277.83	2.12	-327.44
72	73	91.20	-945.79	23.15	1040.64	0	-50.13	1.8	-257.02	1.8	-275.83	2.12	-323.02
73	73	91.20	-945.79	23.21	1040.60	0	-50.16	1.8	-257.01	1.8	-275.83	2.12	-323.01
73	74	92.30	-945.79	55.66	996.37	0	-85.45	1.8	-248.68	1.8	-268.64	2.12	-308.98
74	74	92.30	-945.79	55.66	996.31	0	-85.51	1.8	-248.66	1.8	-268.63	2.12	-308.96
74	75	93.40	-945.79	88.37	913.99	0	-148.68	1.8	-233.97	1.8	-255.20	2.12	-283.27
75	75	93.40	-945.79	88.29	913.91	0	-236.87	1.8	-263.50	1.8	-264.61	2.12	-267.11
75	76	94.50	-945.79	121.05	794.37	0	-338.47	1.8	-244.08	1.8	-245.93	2.12	-229.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.Tinf.MZ+

C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	120.97	866.55	0	-104.83	1.8	-232.62	1.8	-235.32	2.12	-254.86
76	77	95.60	-782.72	155.32	709.89	0	-237.43	1.8	-207.77	1.8	-211.02	2.12	-205.38
77	77	95.60	-782.72	155.20	709.79	0	-237.52	1.8	-207.74	1.8	-211.00	2.12	-205.35
77	78	96.70	-782.72	192.79	521.57	0	-396.33	1.8	-178.53	1.8	-182.00	2.12	-146.17
78	78	96.70	-619.65	192.62	595.36	0	-161.45	1.8	-167.12	1.8	-171.60	2.12	-172.30
78	79	97.80	-619.65	225.28	369.71	0	-351.53	1.8	-132.40	1.8	-136.93	2.12	-101.48
79	79	97.80	-619.65	225.03	369.61	0	-351.62	1.8	-132.38	1.8	-136.91	2.12	-101.44
79	80	98.90	-619.65	257.76	106.71	0	-572.82	1.8	-92.20	1.8	-96.60	2.12	-19.03
80	80	98.90	-391.36	257.44	214.58	0	-240.43	1.8	-76.41	1.8	-82.62	2.12	-56.90
80	81	100.00	-391.36	164.05	-85.30	0	-492.43	1.8	-30.95	1.8	-36.74	2.12	36.97
101	101	0.00	-391.36	-178.20	-85.37	0	-492.49	1.8	-30.93	1.8	-36.73	2.12	36.99
101	102	1.10	-395.79	-272.53	231.39	0	-229.92	1.8	-80.48	1.8	-86.32	2.12	-62.80
102	102	1.10	-624.09	-271.65	123.08	0	-562.68	1.8	-96.18	1.8	-100.23	2.12	-24.80
102	103	2.20	-624.09	-237.76	399.94	0	-329.19	1.8	-139.35	1.8	-143.09	2.12	-112.07
103	103	2.20	-624.08	-237.00	399.67	0	-329.43	1.8	-139.29	1.8	-143.04	2.12	-111.97
103	104	3.30	-624.08	-203.21	636.52	0	-129.48	1.8	-176.41	1.8	-179.76	2.12	-186.69
104	104	3.30	-787.15	-202.54	562.37	0	-364.68	1.8	-187.74	1.8	-190.10	2.12	-160.44
104	105	4.40	-787.15	-168.66	759.85	0	-197.72	1.8	-218.93	1.8	-220.77	2.12	-222.84
105	105	4.40	-787.15	-168.15	759.58	0	-197.95	1.8	-218.87	1.8	-220.73	2.12	-222.75
105	106	5.50	-787.15	-126.46	923.95	0	-58.58	1.8	-245.35	1.8	-246.42	2.12	-274.88
106	106	5.50	-950.22	-126.10	851.48	0	-292.47	1.8	-256.75	1.8	-256.98	2.12	-249.11
106	107	6.60	-950.22	-92.19	976.68	0	-185.92	1.8	-277.34	1.8	-276.67	2.12	-288.98
107	107	6.60	-950.22	-91.86	976.53	0	-95.65	1.8	-247.63	1.8	-247.15	2.12	-305.36
107	108	7.70	-950.22	-58.04	1062.55	0	-29.28	1.8	-263.07	1.8	-281.23	2.12	-332.30
108	108	7.70	-950.22	-57.77	1062.47	0	-29.35	1.8	-263.05	1.8	-281.22	2.12	-332.27
108	109	8.80	-950.22	-23.95	1109.36	0	8.08	1.8	-271.90	1.8	-288.85	2.12	-347.16
109	109	8.80	-950.22	-23.75	1109.31	0	8.05	1.8	-271.89	1.8	-288.85	2.12	-347.15
109	110	9.90	-950.22	10.08	1122.28	0	20.81	1.8	-275.15	1.8	-290.91	2.12	-351.68
110	110	9.90	-950.22	10.26	1122.24	0	20.78	1.8	-275.15	1.8	-290.91	2.12	-351.67
110	111	11.00	-950.22	44.18	1097.11	0	5.45	1.8	-272.01	1.8	-286.69	2.12	-344.47
111	111	11.00	-950.22	44.34	1097.11	0	5.46	1.8	-272.01	1.8	-286.70	2.12	-344.48
111	112	12.10	-950.22	78.19	1033.33	0	-38.41	1.8	-262.37	1.8	-276.12	2.12	-325.39
112	112	12.10	-950.22	78.34	1033.38	0	-38.36	1.8	-262.39	1.8	-276.12	2.12	-325.40
112	113	13.20	-950.22	112.09	930.95	0	-110.77	1.8	-246.24	1.8	-259.17	2.12	-294.41
113	113	13.20	-950.22	112.21	931.02	0	-110.70	1.8	-246.25	1.8	-259.19	2.12	-294.44
113	114	14.30	-950.22	146.09	793.47	0	-208.77	1.8	-224.29	1.8	-236.46	2.12	-252.69
114	114	14.30	-780.33	146.89	865.88	0	-58.92	1.8	-247.54	1.8	-238.65	2.12	-265.71
114	115	15.40	-775.77	178.15	689.31	0	-192.55	1.8	-220.63	1.8	-210.20	2.12	-211.43
115	115	15.40	-1554.62	180.46	1060.75	0	-161.91	1.8	-434.59	1.8	-412.44	2.12	-455.57
115	116	16.50	-1554.62	187.07	852.69	0	-335.16	1.8	-405.21	1.8	-384.63	2.12	-395.47
116	116	16.50	-1554.62	187.50	852.90	0	-292.26	1.8	-446.93	1.8	-420.87	2.12	-444.77
116	117	17.60	-1554.62	203.97	634.47	0	-484.61	1.8	-405.90	1.8	-382.14	2.12	-368.84
117	117	17.60	-2163.46	204.35	1080.09	0	-161.19	1.8	-631.10	1.8	-584.04	2.12	-659.15
117	118	18.70	-2163.46	191.95	854.89	0	-357.29	1.8	-591.65	1.8	-545.84	2.12	-583.15
118	118	18.70	-2163.46	192.19	854.66	0	-357.50	1.8	-591.59	1.8	-545.79	2.12	-583.05
118	119	19.80	-2163.46	185.08	645.95	0	-534.79	1.8	-560.56	1.8	-514.05	2.12	-517.46
119	119	19.80	-1935.17	184.93	753.75	0	-201.50	1.8	-545.26	1.8	-500.77	2.12	-556.06
119	120	20.90	-1935.17	179.08	553.31	0	-367.93	1.8	-520.26	1.8	-473.41	2.12	-497.18
120	120	20.90	-1935.17	178.63	553.31	0	-367.93	1.8	-520.27	1.8	-473.41	2.12	-497.18
120	121	22.00	-1935.17	188.55	348.46	0	-535.48	1.8	-497.96	1.8	-447.30	2.12	-439.47
121	1121	22.00	-1967.78	-200.80	332.05	0	-583.89	1.8	-500.10	1.8	-449.05	2.12	-433.66
121	122	23.40	-1967.78	-188.36	607.53	0	-360.32	1.8	-526.97	1.8	-482.56	2.12	-509.22
122	122	23.40	-1967.78	-188.92	607.57	0	-360.29	1.8	-526.98	1.8	-482.57	2.12	-509.23
122	123	24.80	-1967.78	-185.01	871.45	0	-142.86	1.8	-556.91	1.8	-516.96	2.12	-584.68
123	123	24.80	-2196.07	-185.80	765.59	0	-474.71	1.8	-572.20	1.8	-530.45	2.12	-546.57
123	124	26.20	-2196.07	-216.09	1039.52	0	-242.93	1.8	-610.94	1.8	-571.09	2.12	-631.41
124	124	26.20	-1424.17	-215.80	668.55	0	-330.00	1.8	-374.83	1.8	-359.45	2.12	-368.09
124	125	27.60	-1424.17	-208.56	963.18	0	-73.56	1.8	-425.47	1.8	-409.03	2.12	-467.08
125	125	27.60	-1717.69	-208.03	836.22	0	-493.04	1.8	-445.63	1.8	-427.66	2.12	-420.78
125	126	29.00	-1717.69	-218.30	1145.60	0	-222.22	1.8	-501.10	1.8	-480.15	2.12	-525.38
126	126	29.00	-941.08	-216.99	774.13	0	-294.19	1.8	-246.06	1.8	-240.84	2.12	-231.00
126	127	30.40	-945.21	-177.52	1046.58	0	-78.61	1.8	-288.35	1.8	-284.27	2.12	-315.78
127	127	30.40	-1210.45	-176.70	938.60	0	-334.57	1.8	-267.66	1.8	-288.36	2.12	-296.12
127	128	31.80	-1210.45	-132.69	1149.96	0	-179.74	1.8	-302.65	1.8	-323.29	2.12	-361.04
128	128	31.80	-1210.45	-132.73	1149.81	0	-179.87	1.8	-302.62	1.8	-323.26	2.12	-360.99
128	129	33.20	-1210.45	-84.10	1301.13	0	-69.18	1.8	-327.57	1.8	-348.31	2.12	-407.46
129	129	33.20	-1210.45	-84.22	1301.02	0	-69.27	1.8	-327.55	1.8	-348.29	2.12	-407.43
129	130	34.60	-1210.45	-47.39	1394.04	0	-1.27	1.8	-342.80	1.8	-363.75	2.12	-436.03
130	130	34.60	-1210.45	-47.52	1393.99	0	-1.32	1.8	-342.79	1.8	-363.75	2.12	-436.01
130	131	36.00	-1210.45	-3.93	1424.04	0	20.16	1.8	-347.43	1.8	-368.83	2.12	-445.22
131	131	36.00	-1210.45	-4.07	1424.02	0	20.15	1.8	-347.43	1.8	-368.83	2.12	-445.22
131	132	37.40	-1210.45	45.16	1397.32	0	0.20	1.8	-342.69	1.8	-364.58	2.12	-437.07
132	132	37.40	-1210.45	45.02	1397.35	0	0.24	1.8	-342.69	1.8	-364.59	2.12	-437.08
132	133	38.80	-1210.45	81.82	1307.61	0	-66.29	1.8	-327.33	1.8	-349.96	2.12	-409.51
133	133	38.80	-1210.45	81.71	1307.73	0	-66.19	1.8	-327.35	1.8	-349.98	2.12	-409.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FRECUENTEST.Tinf.MZ+

C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	130.35	1159.88	0	-175.25	1.8	-302.33	1.8	-325.79	2.12	-364.17
134	134	40.20	-1210.45	130.29	1160.02	0	-175.13	1.8	-302.35	1.8	-325.82	2.12	-364.22
134	135	41.60	-1210.45	174.25	951.97	0	-328.46	1.8	-267.26	1.8	-291.72	2.12	-300.35
135	135	41.60	-946.85	175.50	1059.95	0	-85.42	1.8	-287.97	1.8	-287.57	2.12	-318.15
135	136	43.00	-942.63	215.22	789.75	0	-302.43	1.8	-245.64	1.8	-244.85	2.12	-233.87
136	136	43.00	-1717.69	216.07	1161.22	0	-205.91	1.8	-509.72	1.8	-486.91	2.12	-535.69
136	137	44.40	-1717.69	213.95	855.36	0	-474.17	1.8	-454.83	1.8	-434.80	2.12	-431.94
137	137	44.40	-1424.16	214.39	982.40	0	-54.61	1.8	-434.69	1.8	-416.19	2.12	-478.28
137	138	45.80	-1424.16	224.28	676.41	0	-321.99	1.8	-381.34	1.8	-364.12	2.12	-374.62
138	138	45.80	-2196.07	224.80	1047.31	0	-234.98	1.8	-617.43	1.8	-575.73	2.12	-637.92
138	139	47.20	-2196.07	200.31	754.90	0	-484.59	1.8	-573.91	1.8	-530.80	2.12	-545.24
139	139	47.20	-1967.78	200.44	860.50	0	-153.00	1.8	-558.53	1.8	-517.24	2.12	-583.22
139	140	48.60	-1974.23	197.50	582.41	0	-386.04	1.8	-526.57	1.8	-480.99	2.12	-503.14
140	140	48.60	-1974.41	196.91	582.48	0	-386.03	1.8	-526.63	1.8	-481.04	2.12	-503.20
140	141	50.00	-1974.41	208.39	294.78	0	-621.47	1.8	-496.67	1.8	-444.71	2.12	-422.46
141	1141	50.00	-1974.19	-208.47	294.78	0	-621.41	1.8	-496.61	1.8	-444.66	2.12	-422.42
141	142	51.40	-1974.19	-196.99	582.59	0	-385.87	1.8	-526.59	1.8	-481.00	2.12	-503.18
142	142	51.40	-1973.59	-197.58	582.55	0	-385.75	1.8	-526.43	1.8	-480.86	2.12	-503.04
142	143	52.80	-1973.59	-200.03	860.63	0	-154.53	1.8	-560.00	1.8	-518.55	2.12	-584.53
143	143	52.80	-2200.88	-199.95	754.94	0	-485.92	1.8	-575.12	1.8	-531.88	2.12	-546.30
143	144	54.20	-2196.07	-224.80	1047.29	0	-235.00	1.8	-617.42	1.8	-575.73	2.12	-637.91
144	144	54.20	-1424.17	-224.30	676.40	0	-322.00	1.8	-381.35	1.8	-364.12	2.12	-374.62
144	145	55.60	-1424.17	-214.40	982.41	0	-54.59	1.8	-434.70	1.8	-416.20	2.12	-478.29
145	145	55.60	-1717.69	-213.97	855.37	0	-474.16	1.8	-454.83	1.8	-434.80	2.12	-431.94
145	146	57.00	-1717.69	-216.07	1161.26	0	-205.88	1.8	-509.73	1.8	-486.92	2.12	-535.71
146	146	57.00	-942.63	-215.24	789.79	0	-302.41	1.8	-245.64	1.8	-244.85	2.12	-233.88
146	147	58.40	-945.05	-174.61	1059.09	0	-84.50	1.8	-287.71	1.8	-287.17	2.12	-317.83
147	147	58.40	-1208.44	-174.32	951.11	0	-327.37	1.8	-266.97	1.8	-291.29	2.12	-300.02
147	148	59.80	-1208.44	-130.36	1159.23	0	-173.99	1.8	-302.08	1.8	-325.40	2.12	-363.91
148	148	59.80	-1208.45	-130.42	1159.10	0	-174.11	1.8	-302.05	1.8	-325.38	2.12	-363.86
148	149	61.20	-1208.45	-81.77	1307.00	0	-65.01	1.8	-327.08	1.8	-349.57	2.12	-409.25
149	149	61.20	-1208.44	-81.89	1306.90	0	-65.10	1.8	-327.06	1.8	-349.55	2.12	-409.22
149	150	62.60	-1208.44	-45.08	1396.76	0	1.51	1.8	-342.44	1.8	-364.20	2.12	-436.82
150	150	62.60	-1208.44	-45.21	1396.73	0	1.48	1.8	-342.43	1.8	-364.20	2.12	-436.81
150	151	64.00	-1206.69	3.99	1423.50	0	22.90	1.8	-347.02	1.8	-368.20	2.12	-444.91
151	151	64.00	-1206.69	3.85	1423.50	0	22.91	1.8	-347.03	1.8	-368.20	2.12	-444.91
151	152	65.40	-1206.69	47.44	1393.56	0	1.50	1.8	-342.39	1.8	-363.14	2.12	-435.73
152	152	65.40	-1206.69	47.30	1393.61	0	1.54	1.8	-342.40	1.8	-363.15	2.12	-435.75
152	153	66.80	-1206.69	84.12	1300.73	0	-66.36	1.8	-327.17	1.8	-347.71	2.12	-407.19
153	153	66.80	-1206.69	84.03	1300.84	0	-66.27	1.8	-327.19	1.8	-347.73	2.12	-407.22
153	154	68.20	-1206.69	132.65	1149.62	0	-176.90	1.8	-302.25	1.8	-322.70	2.12	-360.78
154	154	68.20	-1206.69	132.61	1149.75	0	-176.79	1.8	-302.28	1.8	-322.72	2.12	-360.82
154	155	69.60	-1206.69	176.60	938.52	0	-331.54	1.8	-267.31	1.8	-287.81	2.12	-295.94
155	155	69.60	-941.94	175.64	1046.50	0	-75.97	1.8	-288.05	1.8	-283.79	2.12	-315.62
155	156	71.00	-941.07	216.98	774.16	0	-294.16	1.8	-246.07	1.8	-240.85	2.12	-231.01
156	156	71.00	-1717.69	218.31	1145.63	0	-222.19	1.8	-501.11	1.8	-480.16	2.12	-525.39
156	157	72.40	-1717.69	208.03	836.24	0	-493.02	1.8	-445.64	1.8	-427.66	2.12	-420.79
157	157	72.40	-1424.17	208.56	963.18	0	-73.56	1.8	-425.47	1.8	-409.03	2.12	-467.08
157	158	73.80	-1424.17	215.81	668.54	0	-330.01	1.8	-374.83	1.8	-359.45	2.12	-368.08
158	158	73.80	-2196.07	216.09	1039.50	0	-242.94	1.8	-610.93	1.8	-571.08	2.12	-631.40
158	159	75.20	-2196.07	185.80	765.57	0	-474.73	1.8	-572.20	1.8	-530.45	2.12	-546.57
159	159	75.20	-1967.78	185.01	871.45	0	-142.85	1.8	-556.91	1.8	-516.96	2.12	-584.68
159	160	76.60	-1971.61	188.46	608.09	0	-360.93	1.8	-528.00	1.8	-483.48	2.12	-510.21
160	160	76.60	-1971.55	187.87	608.14	0	-360.88	1.8	-527.99	1.8	-483.48	2.12	-510.21
160	161	78.00	-1971.55	200.31	333.36	0	-583.87	1.8	-501.21	1.8	-450.05	2.12	-434.83
161	1161	78.00	-1938.62	-188.41	349.79	0	-535.36	1.8	-498.99	1.8	-448.22	2.12	-440.57
161	162	79.10	-1938.62	-178.49	554.46	0	-367.95	1.8	-521.27	1.8	-474.32	2.12	-498.24
162	162	79.10	-1938.23	-178.92	554.43	0	-367.87	1.8	-521.17	1.8	-474.22	2.12	-498.14
162	163	80.20	-1938.23	-184.79	754.73	0	-201.56	1.8	-546.15	1.8	-501.57	2.12	-556.99
163	163	80.20	-2165.99	-184.93	646.90	0	-534.73	1.8	-561.31	1.8	-514.73	2.12	-518.26
163	164	81.30	-2165.99	-192.03	855.46	0	-357.56	1.8	-592.32	1.8	-546.45	2.12	-583.82
164	164	81.30	-2165.29	-191.81	855.61	0	-357.21	1.8	-592.20	1.8	-546.33	2.12	-583.74
164	165	82.40	-2165.29	-204.21	1080.66	0	-161.24	1.8	-631.63	1.8	-584.51	2.12	-659.70
165	165	82.40	-1555.58	-203.87	635.28	0	-484.22	1.8	-406.22	1.8	-382.46	2.12	-369.27
165	166	83.50	-1555.58	-187.40	853.27	0	-292.23	1.8	-447.22	1.8	-421.13	2.12	-445.09
166	166	83.50	-1554.62	-187.07	852.97	0	-334.93	1.8	-405.24	1.8	-384.67	2.12	-395.55
166	167	84.60	-1554.62	-180.46	1061.03	0	-161.68	1.8	-434.63	1.8	-412.47	2.12	-455.64
167	167	84.60	-775.78	-178.13	689.58	0	-192.38	1.8	-220.66	1.8	-210.24	2.12	-211.51
167	168	85.70	-776.65	-144.41	864.77	0	-56.61	1.8	-247.07	1.8	-237.94	2.12	-265.24
168	168	85.70	-945.79	-146.16	792.38	0	-205.84	1.8	-223.75	1.8	-235.65	2.12	-252.19
168	169	86.80	-945.79	-112.29	930.03	0	-107.70	1.8	-245.73	1.8	-258.39	2.12	-293.96
169	169	86.80	-945.79	-112.18	929.92	0	-107.80	1.8	-245.71	1.8	-258.37	2.12	-293.93
169	170	87.90	-945.79	-78.44	1032.47	0	-35.31	1.8	-261.87	1.8	-275.34	2.12	-324.95
170	170	87.90	-945.79	-78.26	1032.41	0	-35.37	1.8	-261.86	1.8	-275.33	2.12	-324.93
170	171	89.00	-945.79	-44.43	1096.28	0	8.56	1.8	-271.51	1.8	-285.93	2.12	-344.05

CÁLCULO TENSIONAL

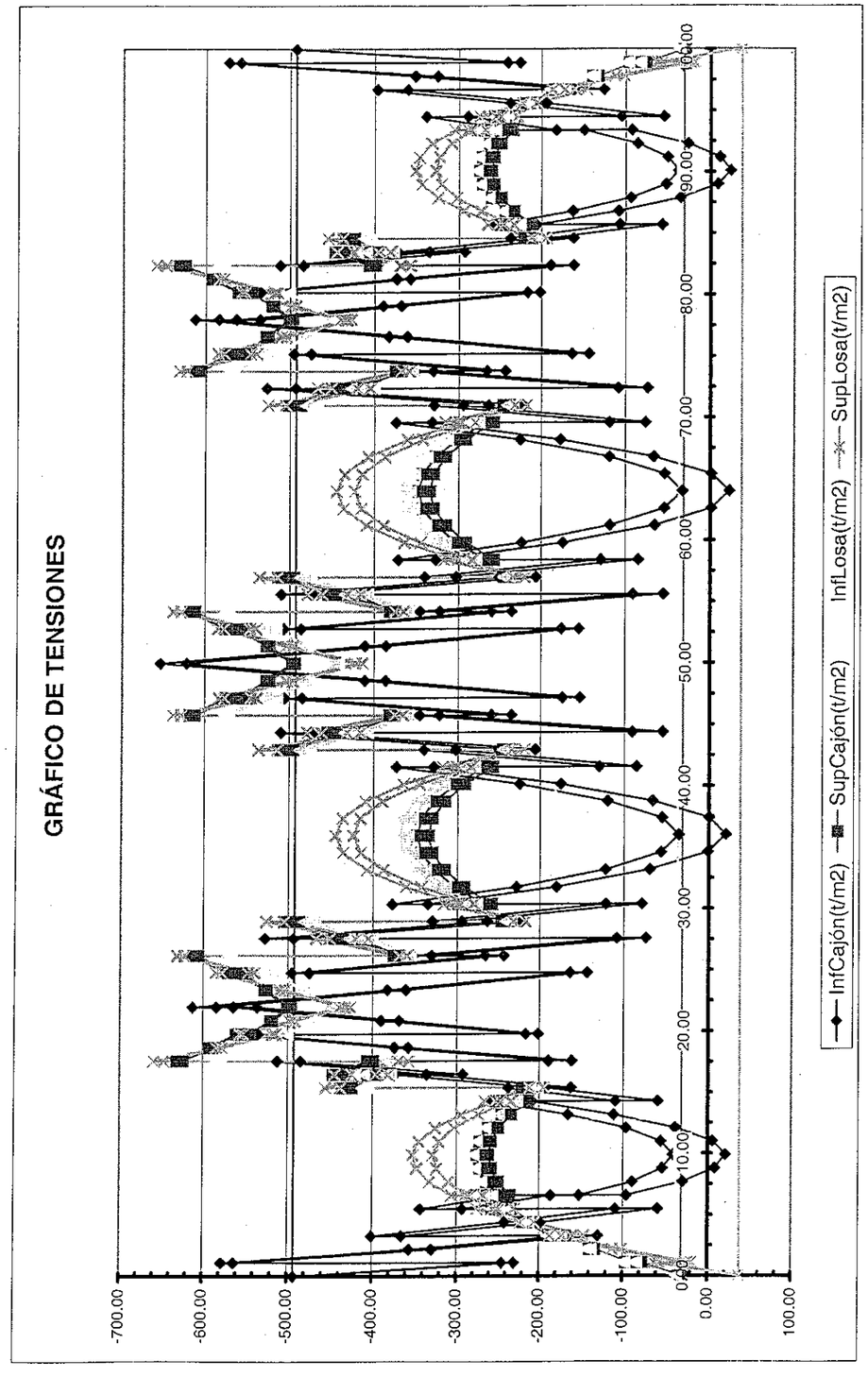
Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ+

C. Frecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-44.29	1096.26	0	8.54	1.8	-271.50	1.8	-285.92	2.12	-344.04
171	172	90.10	-945.79	-10.35	1121.48	0	23.93	1.8	-274.65	1.8	-290.15	2.12	-351.26
172	172	90.10	-945.79	-10.18	1121.51	0	23.95	1.8	-274.65	1.8	-290.15	2.12	-351.27
172	173	91.20	-945.79	23.66	1108.63	0	11.24	1.8	-271.40	1.8	-288.10	2.12	-346.77
173	173	91.20	-945.79	23.84	1108.69	0	11.29	1.8	-271.41	1.8	-288.11	2.12	-346.79
173	174	92.30	-945.79	57.66	1061.89	0	-26.09	1.8	-262.58	1.8	-280.49	2.12	-331.92
174	174	92.30	-945.79	57.96	1061.98	0	-26.01	1.8	-262.60	1.8	-280.51	2.12	-331.95
174	175	93.40	-945.79	91.78	976.04	0	-92.32	1.8	-247.16	1.8	-266.44	2.12	-305.03
175	175	93.40	-945.79	92.11	976.18	0	-182.03	1.8	-276.84	1.8	-275.97	2.12	-288.78
175	176	94.50	-945.79	126.01	851.07	0	-288.52	1.8	-256.26	1.8	-256.29	2.12	-248.93
176	176	94.50	-782.72	126.37	923.54	0	-54.62	1.8	-244.86	1.8	-245.73	2.12	-274.71
176	177	95.60	-782.72	168.06	759.25	0	-193.93	1.8	-218.38	1.8	-220.05	2.12	-222.60
177	177	95.60	-782.72	168.56	759.50	0	-193.71	1.8	-218.44	1.8	-220.10	2.12	-222.68
177	178	96.70	-782.72	202.46	562.12	0	-360.60	1.8	-187.25	1.8	-189.43	2.12	-160.31
178	178	96.70	-619.65	203.11	636.28	0	-125.39	1.8	-175.93	1.8	-179.09	2.12	-186.57
178	179	97.80	-619.65	236.91	399.48	0	-325.30	1.8	-138.81	1.8	-142.38	2.12	-111.86
179	179	97.80	-619.66	237.67	399.77	0	-325.04	1.8	-138.87	1.8	-142.44	2.12	-111.96
179	180	98.90	-619.66	271.57	122.99	0	-558.48	1.8	-95.71	1.8	-99.58	2.12	-24.71
180	180	98.90	-391.36	272.44	231.30	0	-225.70	1.8	-80.00	1.8	-85.68	2.12	-62.72
180	181	100.00	-391.36	178.19	-85.37	0	-492.49	1.8	-30.93	1.8	-36.73	2.12	36.99



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-254.60	-105.50	0	-556.59	1.8	-34.81	1.8	-41.12	2.12	42.18
1	2	1.10	-436.66	-114.78	31.54	0	-440.02	1.8	-49.34	1.8	-59.65	2.12	1.54
2	2	1.10	-693.96	-115.00	-94.84	0	-815.12	1.8	-67.05	1.8	-75.31	2.12	44.34
2	3	2.20	-693.96	-96.99	21.77	0	-719.47	1.8	-79.84	1.8	-91.60	2.12	9.73
3	3	2.20	-693.96	-97.22	21.73	0	-719.49	1.8	-79.83	1.8	-91.60	2.12	9.74
3	4	3.30	-693.96	-79.22	118.76	0	-639.81	1.8	-90.44	1.8	-105.12	2.12	-19.04
4	4	3.30	-877.74	-79.46	32.16	0	-904.88	1.8	-103.24	1.8	-116.78	2.12	10.51
4	5	4.40	-877.74	-61.48	109.68	0	-841.11	1.8	-111.70	1.8	-127.55	2.12	-12.46
5	5	4.40	-877.74	-61.74	109.66	0	-841.13	1.8	-111.70	1.8	-127.55	2.12	-12.45
5	6	5.50	-877.74	-43.74	167.65	0	-793.28	1.8	-117.99	1.8	-135.57	2.12	-29.60
6	6	5.50	-1061.53	-44.01	82.89	0	-1056.92	1.8	-130.87	1.8	-147.47	2.12	-0.58
6	7	6.60	-1061.53	-26.01	121.43	0	-1024.94	1.8	-135.01	1.8	-152.74	2.12	-11.93
7	7	6.60	-1061.53	-26.33	121.38	0	-865.86	1.8	-97.96	1.8	-139.23	2.12	-35.91
7	8	7.70	-1061.53	-8.34	140.44	0	-853.73	1.8	-100.50	1.8	-142.01	2.12	-41.16
8	8	7.70	-1061.53	-8.65	140.41	0	-853.75	1.8	-100.49	1.8	-142.01	2.12	-41.15
8	9	8.80	-1061.53	9.58	140.03	0	-854.80	1.8	-100.20	1.8	-141.62	2.12	-40.66
9	9	8.80	-1061.54	9.14	139.98	0	-854.84	1.8	-100.19	1.8	-141.62	2.12	-40.65
9	10	9.90	-1061.54	27.24	120.00	0	-869.21	1.8	-97.05	1.8	-138.05	2.12	-34.37
10	10	9.90	-1061.53	26.85	119.99	0	-869.21	1.8	-97.04	1.8	-138.04	2.12	-34.36
10	11	11.00	-1061.53	44.84	80.55	0	-896.78	1.8	-91.07	1.8	-131.31	2.12	-22.34
11	11	11.00	-1061.53	44.40	80.53	0	-896.80	1.8	-91.06	1.8	-131.31	2.12	-22.33
11	12	12.10	-1061.53	62.42	21.77	0	-937.45	1.8	-82.28	1.8	-121.44	2.12	-4.61
12	12	12.10	-1061.53	61.98	21.74	0	-937.48	1.8	-82.28	1.8	-121.43	2.12	-4.61
12	13	13.20	-1061.53	80.04	-56.41	0	-991.27	1.8	-70.69	1.8	-108.41	2.12	18.83
13	13	13.20	-1061.53	79.59	-56.42	0	-991.29	1.8	-70.68	1.8	-108.40	2.12	18.84
13	14	14.30	-1061.53	97.61	-153.90	0	-1058.17	1.8	-56.29	1.8	-92.24	2.12	47.98
14	14	14.30	-871.84	92.50	-69.18	0	-947.74	1.8	-85.11	1.8	-96.92	2.12	39.52
14	15	15.40	-874.66	112.99	-184.67	0	-1035.47	1.8	-70.09	1.8	-79.44	2.12	73.73
15	15	15.40	-1567.05	114.87	144.76	0	-1016.57	1.8	-262.34	1.8	-263.06	2.12	-146.45
15	16	16.50	-1567.05	165.29	3.21	0	-1132.84	1.8	-244.85	1.8	-245.62	2.12	-107.40
16	16	16.50	-1567.05	165.00	3.30	0	-1168.43	1.8	-210.06	1.8	-215.40	2.12	-66.31
16	17	17.60	-1567.05	193.96	-192.23	0	-1332.10	1.8	-183.41	1.8	-188.99	2.12	-9.13
17	17	17.60	-2068.15	193.43	224.33	0	-988.54	1.8	-380.17	1.8	-365.40	2.12	-272.68
17	18	18.70	-2068.15	235.79	-11.29	0	-1187.40	1.8	-346.35	1.8	-331.91	2.12	-201.59
18	18	18.70	-2068.15	235.31	-10.88	0	-1187.01	1.8	-346.46	1.8	-332.00	2.12	-201.76
18	19	19.80	-2068.15	282.49	-294.36	0	-1428.51	1.8	-303.29	1.8	-289.52	2.12	-113.35
19	19	19.80	-1810.85	282.09	-167.48	0	-1051.94	1.8	-286.24	1.8	-274.70	2.12	-157.16
19	20	20.90	-1810.85	341.16	-515.62	0	-1352.32	1.8	-228.85	1.8	-218.98	2.12	-43.92
20	20	20.90	-1810.85	340.96	-515.60	0	-1352.31	1.8	-228.85	1.8	-218.98	2.12	-43.93
20	21	22.00	-1810.85	390.92	-917.10	0	-1700.36	1.8	-160.87	1.8	-152.94	2.12	88.96
21	1021	22.00	-1847.60	-429.47	-936.16	0	-1754.85	1.8	-163.30	1.8	-154.95	2.12	95.46
21	22	23.40	-1847.60	-376.82	-376.63	0	-1268.61	1.8	-258.47	1.8	-248.09	2.12	-91.25
22	22	23.40	-1847.60	-377.06	-376.49	0	-1268.46	1.8	-258.53	1.8	-248.13	2.12	-91.32
22	23	24.80	-1847.60	-314.77	107.59	0	-848.79	1.8	-339.76	1.8	-327.35	2.12	-251.11
23	23	24.80	-2104.90	-313.47	-16.18	0	-1222.83	1.8	-357.09	1.8	-342.65	2.12	-208.30
23	24	26.20	-2104.90	-240.01	362.17	0	-899.52	1.8	-414.97	1.8	-400.16	2.12	-327.42
24	24	26.20	-1420.02	-239.91	32.15	0	-977.41	1.8	-205.67	1.8	-212.55	2.12	-93.87
24	25	27.60	-1420.02	-184.07	328.27	0	-727.74	1.8	-247.03	1.8	-254.28	2.12	-182.82
25	25	27.60	-1750.84	-184.58	178.48	0	-1201.47	1.8	-269.61	1.8	-275.14	2.12	-130.36
25	26	29.00	-1750.84	-108.82	364.06	0	-1047.38	1.8	-292.63	1.8	-299.37	2.12	-183.56
26	26	29.00	-1061.02	-108.24	34.55	0	-1039.67	1.8	-125.83	1.8	-136.28	2.12	8.50
26	27	30.40	-1058.63	-82.08	170.20	0	-936.39	1.8	-141.60	1.8	-156.19	2.12	-31.15
27	27	30.40	-1356.26	-85.51	43.39	0	-1164.91	1.8	-114.76	1.8	-158.09	2.12	-14.90
27	28	31.80	-1356.26	-62.54	147.03	0	-1096.27	1.8	-129.08	1.8	-175.02	2.12	-45.24
28	28	31.80	-1356.26	-63.13	146.97	0	-1096.30	1.8	-129.07	1.8	-175.01	2.12	-45.22
28	29	33.20	-1356.26	-40.22	219.31	0	-1048.87	1.8	-138.85	1.8	-186.85	2.12	-66.33
29	29	33.20	-1356.26	-40.79	219.29	0	-1048.88	1.8	-138.84	1.8	-186.85	2.12	-66.32
29	30	34.60	-1356.26	-16.63	259.25	0	-1023.53	1.8	-143.87	1.8	-193.42	2.12	-77.85
30	30	34.60	-1356.26	-17.15	259.17	0	-1023.58	1.8	-143.85	1.8	-193.41	2.12	-77.82
30	31	36.00	-1356.26	9.43	263.96	0	-1022.61	1.8	-143.58	1.8	-194.24	2.12	-78.85
31	31	36.00	-1356.26	8.90	263.94	0	-1022.63	1.8	-143.58	1.8	-194.23	2.12	-78.84
31	32	37.40	-1356.26	31.91	235.40	0	-1044.52	1.8	-138.37	1.8	-189.63	2.12	-69.98
32	32	37.40	-1356.26	31.33	235.40	0	-1044.52	1.8	-138.37	1.8	-189.63	2.12	-69.97
32	33	38.80	-1356.26	54.23	175.51	0	-1087.66	1.8	-128.61	1.8	-179.94	2.12	-51.86
33	33	38.80	-1356.26	53.65	175.52	0	-1087.66	1.8	-128.61	1.8	-179.94	2.12	-51.86
33	34	40.20	-1356.26	76.57	84.35	0	-1151.99	1.8	-114.31	1.8	-165.16	2.12	-24.52
34	34	40.20	-1356.26	75.95	84.39	0	-1151.97	1.8	-114.32	1.8	-165.16	2.12	-24.53
34	35	41.60	-1356.26	98.94	-38.01	0	-1237.44	1.8	-95.50	1.8	-145.31	2.12	12.02
35	35	41.60	-1060.58	96.00	88.77	0	-1026.12	1.8	-122.52	1.8	-143.51	2.12	-1.91
35	36	43.00	-1063.03	121.75	-64.36	0	-1148.66	1.8	-102.64	1.8	-120.99	2.12	43.92
36	36	43.00	-1750.84	121.81	265.16	0	-1143.64	1.8	-265.84	1.8	-275.42	2.12	-140.37
36	37	44.40	-1750.84	191.32	58.88	0	-1316.70	1.8	-238.57	1.8	-247.33	2.12	-79.65
37	37	44.40	-1420.02	190.73	208.56	0	-843.08	1.8	-215.96	1.8	-226.44	2.12	-132.06
37	38	45.80	-1420.02	243.67	-92.48	0	-1097.43	1.8	-173.81	1.8	-183.88	2.12	-41.38
38	38	45.80	-2104.90	243.21	237.64	0	-1019.43	1.8	-383.14	1.8	-371.52	2.12	-274.97

Combi_ti.xls Programa DINTEL PACADAR S.A. 11/09/03
FRECUENTEST.Tinf.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	302.11	-140.25	0	-1342.20	1.8	-326.05	1.8	-314.55	2.12	-156.54
39	39	47.20	-1847.60	301.33	-16.10	0	-967.79	1.8	-308.82	1.8	-299.35	2.12	-199.53
39	40	48.60	-1841.15	377.71	-493.75	0	-1379.24	1.8	-228.60	1.8	-220.81	2.12	-41.79
40	40	48.60	-1840.98	377.42	-493.82	0	-1379.26	1.8	-228.53	1.8	-220.75	2.12	-41.72
40	41	50.00	-1840.98	432.74	-1057.53	0	-1869.34	1.8	-132.92	1.8	-127.08	2.12	146.24
41	1041	50.00	-1841.19	-432.66	-1057.54	0	-1869.41	1.8	-132.97	1.8	-127.13	2.12	146.19
41	42	51.40	-1841.19	-377.34	-493.95	0	-1379.43	1.8	-228.57	1.8	-220.79	2.12	-41.73
42	42	51.40	-1841.79	-377.62	-493.89	0	-1379.54	1.8	-228.74	1.8	-220.94	2.12	-41.89
42	43	52.80	-1841.79	-301.74	-16.24	0	-966.27	1.8	-307.35	1.8	-298.03	2.12	-198.22
43	43	52.80	-2100.09	-302.48	-140.29	0	-1340.87	1.8	-324.84	1.8	-313.47	2.12	-155.48
43	44	54.20	-2104.90	-243.21	237.66	0	-1019.42	1.8	-383.15	1.8	-371.53	2.12	-274.98
44	44	54.20	-1420.02	-243.67	-92.49	0	-1097.43	1.8	-173.81	1.8	-183.88	2.12	-41.38
44	45	55.60	-1420.02	-190.72	208.59	0	-843.05	1.8	-215.97	1.8	-226.45	2.12	-132.07
45	45	55.60	-1750.84	-191.31	58.91	0	-1316.67	1.8	-238.58	1.8	-247.34	2.12	-79.66
45	46	57.00	-1750.84	-121.79	265.18	0	-1143.62	1.8	-265.85	1.8	-275.42	2.12	-140.38
46	46	57.00	-1063.03	-121.76	-64.36	0	-1148.66	1.8	-102.64	1.8	-120.99	2.12	43.92
46	47	58.40	-1062.37	-96.92	89.67	0	-1027.00	1.8	-122.79	1.8	-143.92	2.12	-2.24
47	47	58.40	-1358.27	-98.88	-37.12	0	-1238.51	1.8	-95.79	1.8	-145.75	2.12	11.68
47	48	59.80	-1358.27	-75.90	85.23	0	-1153.07	1.8	-114.61	1.8	-165.59	2.12	-24.86
48	48	59.80	-1358.27	-76.49	85.20	0	-1153.08	1.8	-114.60	1.8	-165.59	2.12	-24.85
48	49	61.20	-1358.27	-53.58	176.24	0	-1088.84	1.8	-128.88	1.8	-180.34	2.12	-52.16
49	49	61.20	-1358.27	-54.17	176.25	0	-1088.83	1.8	-128.88	1.8	-180.35	2.12	-52.16
49	50	62.60	-1358.27	-31.27	236.05	0	-1045.75	1.8	-138.63	1.8	-190.03	2.12	-70.25
50	50	62.60	-1358.27	-31.85	236.04	0	-1045.75	1.8	-138.63	1.8	-190.03	2.12	-70.25
50	51	64.00	-1360.02	-8.82	264.50	0	-1025.35	1.8	-143.99	1.8	-194.86	2.12	-79.16
51	51	64.00	-1360.02	-9.35	264.50	0	-1025.35	1.8	-143.99	1.8	-194.86	2.12	-79.16
51	52	65.40	-1360.02	17.25	259.61	0	-1026.39	1.8	-144.25	1.8	-194.02	2.12	-78.11
52	52	65.40	-1360.02	16.71	259.66	0	-1026.35	1.8	-144.26	1.8	-194.02	2.12	-78.12
52	53	66.80	-1360.02	40.87	219.63	0	-1051.75	1.8	-139.23	1.8	-187.44	2.12	-66.58
53	53	66.80	-1360.02	40.31	219.65	0	-1051.73	1.8	-139.23	1.8	-187.44	2.12	-66.58
53	54	68.20	-1360.02	63.21	147.21	0	-1099.24	1.8	-129.45	1.8	-175.58	2.12	-45.45
54	54	68.20	-1360.02	62.62	147.24	0	-1099.22	1.8	-129.45	1.8	-175.59	2.12	-45.46
54	55	69.60	-1360.02	85.59	43.49	0	-1167.94	1.8	-115.12	1.8	-158.64	2.12	-15.08
55	55	69.60	-1061.89	83.96	170.28	0	-939.03	1.8	-141.91	1.8	-156.67	2.12	-31.31
55	56	71.00	-1061.02	108.24	34.55	0	-1039.67	1.8	-125.83	1.8	-136.28	2.12	8.50
56	56	71.00	-1750.84	108.83	364.06	0	-1047.38	1.8	-292.63	1.8	-299.37	2.12	-183.56
56	57	72.40	-1750.84	184.58	178.48	0	-1201.47	1.8	-269.61	1.8	-275.14	2.12	-130.36
57	57	72.40	-1420.02	184.08	328.24	0	-727.77	1.8	-247.02	1.8	-254.27	2.12	-182.81
57	58	73.80	-1420.02	239.92	32.13	0	-977.43	1.8	-205.67	1.8	-212.55	2.12	-93.87
58	58	73.80	-2104.91	240.02	362.15	0	-899.53	1.8	-414.97	1.8	-400.16	2.12	-327.41
58	59	75.20	-2104.91	313.48	-16.20	0	-1222.84	1.8	-357.09	1.8	-342.65	2.12	-208.29
59	59	75.20	-1847.60	314.76	107.60	0	-848.78	1.8	-339.76	1.8	-327.35	2.12	-251.12
59	60	76.60	-1843.76	377.52	-377.01	0	-1267.81	1.8	-257.50	1.8	-247.21	2.12	-90.35
60	60	76.60	-1843.83	377.31	-377.24	0	-1268.04	1.8	-257.45	1.8	-247.17	2.12	-90.26
60	61	78.00	-1843.83	429.98	-937.46	0	-1754.86	1.8	-162.19	1.8	-153.95	2.12	96.63
61	1061	78.00	-1807.39	-391.07	-918.45	0	-1700.50	1.8	-159.83	1.8	-152.01	2.12	90.08
61	62	79.10	-1807.39	-341.12	-516.78	0	-1352.31	1.8	-227.83	1.8	-218.07	2.12	-42.85
62	62	79.10	-1807.77	-341.34	-516.82	0	-1352.45	1.8	-227.92	1.8	-218.15	2.12	-42.93
62	63	80.20	-1807.77	-282.26	-168.50	0	-1051.92	1.8	-285.34	1.8	-273.90	2.12	-156.21
63	63	80.20	-2065.61	-282.66	-295.35	0	-1428.61	1.8	-302.53	1.8	-288.83	2.12	-112.53
63	64	81.30	-2065.61	-235.48	-11.68	0	-1186.96	1.8	-345.72	1.8	-331.34	2.12	-200.99
64	64	81.30	-2066.31	-235.93	-12.03	0	-1187.49	1.8	-345.80	1.8	-331.41	2.12	-200.99
64	65	82.40	-2066.31	-193.57	223.77	0	-988.49	1.8	-379.64	1.8	-364.92	2.12	-272.13
65	65	82.40	-1566.09	-194.06	-192.35	0	-1331.94	1.8	-183.13	1.8	-188.77	2.12	-8.90
65	66	83.50	-1566.09	-165.10	2.92	0	-1168.49	1.8	-209.76	1.8	-215.13	2.12	-65.99
66	66	83.50	-1567.05	-165.32	2.94	0	-1133.06	1.8	-244.82	1.8	-245.59	2.12	-107.33
66	67	84.60	-1567.05	-114.90	144.51	0	-1016.78	1.8	-262.31	1.8	-263.03	2.12	-146.38
67	67	84.60	-874.65	-113.00	-184.94	0	-1035.64	1.8	-70.05	1.8	-79.39	2.12	73.81
67	68	85.70	-875.52	-94.97	-68.08	0	-950.05	1.8	-85.58	1.8	-97.62	2.12	39.05
68	68	85.70	-1065.95	-97.53	-152.81	0	-1061.11	1.8	-56.82	1.8	-93.05	2.12	47.48
68	69	86.80	-1065.95	-79.51	-55.41	0	-994.27	1.8	-71.21	1.8	-109.20	2.12	18.36
69	69	86.80	-1065.96	-79.96	-55.40	0	-994.26	1.8	-71.21	1.8	-109.21	2.12	18.35
69	70	87.90	-1065.96	-61.90	22.66	0	-940.52	1.8	-82.79	1.8	-122.21	2.12	-5.06
70	70	87.90	-1065.96	-62.34	22.68	0	-940.50	1.8	-82.80	1.8	-122.22	2.12	-5.07
70	71	89.00	-1065.96	-44.33	81.35	0	-899.90	1.8	-91.57	1.8	-132.08	2.12	-22.76
71	71	89.00	-1065.96	-44.78	81.39	0	-899.88	1.8	-91.57	1.8	-132.08	2.12	-22.77
71	72	90.10	-1065.96	-26.78	120.74	0	-872.36	1.8	-97.54	1.8	-138.80	2.12	-34.77
72	72	90.10	-1065.96	-27.17	120.75	0	-872.36	1.8	-97.54	1.8	-138.80	2.12	-34.77
72	73	91.20	-1065.96	-9.08	140.63	0	-858.06	1.8	-100.67	1.8	-142.35	2.12	-41.02
73	73	91.20	-1065.96	-9.52	140.69	0	-858.01	1.8	-100.69	1.8	-142.36	2.12	-41.03
73	74	92.30	-1065.96	8.71	140.99	0	-857.02	1.8	-100.96	1.8	-142.73	2.12	-41.50
74	74	92.30	-1065.96	8.41	141.01	0	-857.00	1.8	-100.97	1.8	-142.74	2.12	-41.50
74	75	93.40	-1065.96	26.40	121.88	0	-869.19	1.8	-98.43	1.8	-139.95	2.12	-36.23
75	75	93.40	-1065.96	26.08	121.92	0	-1028.84	1.8	-135.50	1.8	-153.44	2.12	-12.12
75	76	94.50	-1065.96	44.07	83.30	0	-1060.88	1.8	-131.36	1.8	-148.15	2.12	-0.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ-
C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	43.82	168.08	0	-797.23	1.8	-118.49	1.8	-136.26	2.12	-29.78
76	77	95.60	-882.17	61.82	109.98	0	-845.15	1.8	-112.18	1.8	-128.23	2.12	-12.60
77	77	95.60	-882.17	61.55	110.02	0	-845.12	1.8	-112.19	1.8	-128.23	2.12	-12.61
77	78	96.70	-882.17	79.53	32.40	0	-908.97	1.8	-103.73	1.8	-117.45	2.12	10.38
78	78	96.70	-698.39	79.29	119.01	0	-643.89	1.8	-90.93	1.8	-105.79	2.12	-19.16
78	79	97.80	-698.39	97.29	21.90	0	-723.64	1.8	-80.31	1.8	-92.25	2.12	9.64
79	79	97.80	-698.38	97.06	21.93	0	-723.61	1.8	-80.31	1.8	-92.25	2.12	9.63
79	80	98.90	-698.38	115.06	-94.76	0	-819.33	1.8	-67.52	1.8	-75.96	2.12	44.26
80	80	98.90	-441.09	114.84	31.63	0	-444.24	1.8	-49.81	1.8	-60.30	2.12	1.46
80	81	100.00	-441.09	254.58	-105.50	0	-556.59	1.8	-34.81	1.8	-41.12	2.12	42.18
101	101	0.00	-441.09	-251.59	-105.57	0	-556.64	1.8	-34.79	1.8	-41.11	2.12	42.20
101	102	1.10	-436.66	-110.95	27.18	0	-443.62	1.8	-48.68	1.8	-59.05	2.12	2.83
102	102	1.10	-693.96	-111.27	-98.96	0	-818.52	1.8	-66.44	1.8	-74.75	2.12	45.56
102	103	2.20	-693.96	-93.69	13.74	0	-726.10	1.8	-78.63	1.8	-90.49	2.12	12.11
103	103	2.20	-693.96	-93.93	13.93	0	-725.94	1.8	-78.66	1.8	-90.52	2.12	12.05
103	104	3.30	-693.96	-76.39	107.56	0	-649.08	1.8	-88.75	1.8	-103.57	2.12	-15.71
104	104	3.30	-877.74	-76.52	21.16	0	-913.98	1.8	-101.59	1.8	-115.26	2.12	13.77
104	105	4.40	-877.74	-58.99	95.70	0	-852.69	1.8	-109.57	1.8	-125.60	2.12	-8.29
105	105	4.40	-877.74	-59.07	95.82	0	-852.59	1.8	-109.59	1.8	-125.62	2.12	-8.33
105	106	5.50	-877.74	-41.52	151.13	0	-807.00	1.8	-115.44	1.8	-133.24	2.12	-24.65
106	106	5.50	-1061.53	-41.49	66.52	0	-1070.51	1.8	-128.34	1.8	-145.16	2.12	4.33
106	107	6.60	-1061.53	-23.93	102.50	0	-1040.70	1.8	-132.04	1.8	-150.04	2.12	-6.21
107	107	6.60	-1061.53	-23.85	102.60	0	-878.22	1.8	-94.87	1.8	-136.44	2.12	-30.61
107	108	7.70	-1061.53	-6.32	119.17	0	-868.01	1.8	-96.94	1.8	-138.81	2.12	-35.08
108	108	7.70	-1061.53	-6.20	119.27	0	-867.94	1.8	-96.96	1.8	-138.82	2.12	-35.11
108	109	8.80	-1061.53	11.34	116.45	0	-870.99	1.8	-96.20	1.8	-138.03	2.12	-33.82
109	109	8.80	-1061.53	11.47	116.50	0	-870.95	1.8	-96.21	1.8	-138.04	2.12	-33.84
109	110	9.90	-1061.53	29.01	94.22	0	-887.30	1.8	-92.59	1.8	-134.06	2.12	-26.78
110	110	9.90	-1061.53	29.19	94.26	0	-887.27	1.8	-92.60	1.8	-134.07	2.12	-26.80
110	111	11.00	-1061.53	46.74	52.51	0	-916.94	1.8	-86.13	1.8	-126.92	2.12	-13.96
111	111	11.00	-1061.53	46.98	52.52	0	-916.93	1.8	-86.13	1.8	-126.92	2.12	-13.97
111	112	12.10	-1061.53	64.50	-8.80	0	-960.01	1.8	-76.79	1.8	-116.57	2.12	4.68
112	112	12.10	-1061.53	64.75	-8.81	0	-960.02	1.8	-76.79	1.8	-116.57	2.12	4.68
112	113	13.20	-1061.53	82.29	-89.69	0	-1016.48	1.8	-64.58	1.8	-103.03	2.12	29.13
113	113	13.20	-1061.53	82.55	-89.72	0	-1016.51	1.8	-64.57	1.8	-103.02	2.12	29.14
113	114	14.30	-1061.53	100.12	-190.21	0	-1086.41	1.8	-49.48	1.8	-86.28	2.12	59.41
114	114	14.30	-871.84	95.78	-105.53	0	-978.83	1.8	-78.41	1.8	-91.04	2.12	51.29
114	115	15.40	-874.66	116.00	-224.38	0	-1069.59	1.8	-62.59	1.8	-72.89	2.12	86.74
115	115	15.40	-1567.05	118.69	104.95	0	-1050.64	1.8	-255.29	1.8	-256.91	2.12	-133.92
115	116	16.50	-1567.05	163.32	-40.74	0	-1170.68	1.8	-236.63	1.8	-238.47	2.12	-93.14
116	116	16.50	-1567.05	163.57	-40.85	0	-1211.10	1.8	-197.26	1.8	-204.28	2.12	-46.63
116	117	17.60	-1567.05	191.15	-234.34	0	-1374.78	1.8	-168.85	1.8	-176.40	2.12	12.24
117	117	17.60	-2068.15	191.26	181.99	0	-1031.44	1.8	-365.57	1.8	-352.76	2.12	-251.23
117	118	18.70	-2068.15	241.25	-57.05	0	-1235.88	1.8	-328.05	1.8	-316.12	2.12	-175.63
118	118	18.70	-2068.15	241.51	-56.79	0	-1235.62	1.8	-328.14	1.8	-316.20	2.12	-175.76
118	119	19.80	-2068.15	298.21	-352.38	0	-1491.43	1.8	-278.38	1.8	-268.06	2.12	-78.56
119	119	19.80	-1810.85	298.88	-225.83	0	-1115.16	1.8	-261.25	1.8	-253.17	2.12	-122.24
119	120	20.90	-1810.85	369.51	-600.76	0	-1444.37	1.8	-192.63	1.8	-187.76	2.12	6.77
120	120	20.90	-1810.85	370.47	-600.71	0	-1444.32	1.8	-192.64	1.8	-187.78	2.12	6.74
120	121	22.00	-1810.85	416.91	-1030.36	0	-1822.82	1.8	-112.67	1.8	-111.40	2.12	156.42
121	1121	22.00	-1847.60	-453.81	-1049.50	0	-1877.39	1.8	-115.08	1.8	-113.39	2.12	162.95
121	122	23.40	-1847.60	-397.38	-457.27	0	-1355.53	1.8	-224.47	1.8	-218.78	2.12	-43.57
122	122	23.40	-1847.60	-396.13	-457.36	0	-1355.62	1.8	-224.44	1.8	-218.75	2.12	-43.52
122	123	24.80	-1847.60	-331.30	50.88	0	-909.11	1.8	-316.80	1.8	-307.55	2.12	-218.64
123	123	24.80	-2104.90	-329.84	-72.89	0	-1283.18	1.8	-334.10	1.8	-322.82	2.12	-175.78
123	124	26.20	-2104.90	-246.67	320.63	0	-942.22	1.8	-399.91	1.8	-387.15	2.12	-305.57
124	124	26.20	-1420.02	-246.33	-9.22	0	-1019.98	1.8	-190.62	1.8	-199.54	2.12	-72.06
124	125	27.60	-1420.02	-187.05	292.24	0	-762.64	1.8	-236.50	1.8	-245.13	2.12	-166.66
125	125	27.60	-1750.84	-187.00	142.68	0	-1236.18	1.8	-259.10	1.8	-266.01	2.12	-114.26
125	126	29.00	-1750.84	-111.23	336.08	0	-1073.38	1.8	-285.75	1.8	-293.37	2.12	-172.45
126	126	29.00	-1061.03	-109.56	6.75	0	-1063.48	1.8	-120.66	1.8	-131.75	2.12	17.54
126	127	30.40	-1058.64	-84.50	145.13	0	-957.71	1.8	-137.13	1.8	-152.24	2.12	-23.16
127	127	30.40	-1356.26	-86.89	18.44	0	-1183.67	1.8	-110.21	1.8	-154.07	2.12	-7.22
127	128	31.80	-1356.26	-64.43	124.31	0	-1112.62	1.8	-125.08	1.8	-171.45	2.12	-38.44
128	128	31.80	-1356.26	-63.94	124.37	0	-1112.57	1.8	-125.09	1.8	-171.46	2.12	-38.46
128	129	33.20	-1356.26	-41.62	198.28	0	-1063.45	1.8	-135.25	1.8	-183.62	2.12	-60.19
129	129	33.20	-1356.26	-41.18	198.32	0	-1063.42	1.8	-135.25	1.8	-183.63	2.12	-60.21
129	130	34.60	-1356.26	-17.69	239.50	0	-1036.83	1.8	-140.56	1.8	-190.44	2.12	-72.19
130	130	34.60	-1356.26	-17.23	239.47	0	-1036.86	1.8	-140.56	1.8	-190.44	2.12	-72.18
130	131	36.00	-1356.26	9.54	244.31	0	-1035.76	1.8	-140.31	1.8	-191.29	2.12	-73.25
131	131	36.00	-1356.26	9.99	244.33	0	-1035.75	1.8	-140.31	1.8	-191.29	2.12	-73.25
131	132	37.40	-1356.26	32.37	214.66	0	-1058.65	1.8	-134.87	1.8	-186.48	2.12	-64.00
132	132	37.40	-1356.26	32.83	214.67	0	-1058.64	1.8	-134.87	1.8	-186.49	2.12	-64.00
132	133	38.80	-1356.26	55.16	153.08	0	-1103.42	1.8	-124.73	1.8	-176.47	2.12	-45.26
133	133	38.80	-1356.26	55.64	153.06	0	-1103.44	1.8	-124.73	1.8	-176.47	2.12	-45.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ-
C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	78.00	59.52	0	-1170.13	1.8	-109.89	1.8	-161.23	2.12	-17.02
134	134	40.20	-1356.26	78.47	59.47	0	-1170.16	1.8	-109.88	1.8	-161.22	2.12	-17.01
134	135	41.60	-1356.26	100.94	-66.10	0	-1258.83	1.8	-90.32	1.8	-140.75	2.12	20.74
135	135	41.60	-1060.58	99.06	60.60	0	-1050.12	1.8	-117.44	1.8	-139.03	2.12	7.13
135	136	43.00	-1063.03	123.89	-96.33	0	-1176.09	1.8	-96.64	1.8	-115.75	2.12	54.36
136	136	43.00	-1750.84	125.14	233.02	0	-1173.76	1.8	-257.64	1.8	-268.27	2.12	-127.28
136	137	44.40	-1750.84	192.84	19.64	0	-1354.95	1.8	-226.81	1.8	-237.12	2.12	-61.73
137	137	44.40	-1420.02	193.00	169.08	0	-881.53	1.8	-204.17	1.8	-216.21	2.12	-114.07
137	138	45.80	-1420.02	249.46	-137.35	0	-1143.64	1.8	-157.43	1.8	-169.73	2.12	-17.66
138	138	45.80	-2104.90	249.60	192.60	0	-1065.79	1.8	-366.75	1.8	-357.36	2.12	-251.21
138	139	47.20	-2104.90	315.16	-199.20	0	-1405.04	1.8	-302.02	1.8	-293.84	2.12	-122.61
139	139	47.20	-1847.60	315.70	-75.25	0	-1030.80	1.8	-284.78	1.8	-278.61	2.12	-165.54
139	140	48.60	-1841.15	397.62	-579.51	0	-1471.52	1.8	-192.63	1.8	-189.81	2.12	8.70
140	140	48.60	-1840.98	398.90	-579.48	0	-1471.42	1.8	-192.62	1.8	-189.80	2.12	8.70
140	141	50.00	-1840.98	458.17	-1177.44	0	-1998.69	1.8	-82.24	1.8	-83.41	2.12	217.26
141	1141	50.00	-1841.18	-458.09	-1177.45	0	-1998.76	1.8	-82.29	1.8	-83.46	2.12	217.22
141	142	51.40	-1841.18	-398.81	-579.58	0	-1471.56	1.8	-192.66	1.8	-189.83	2.12	8.68
142	142	51.40	-1841.79	-397.53	-579.62	0	-1471.79	1.8	-192.78	1.8	-189.94	2.12	8.59
142	143	52.80	-1841.79	-316.12	-75.38	0	-1029.26	1.8	-283.31	1.8	-277.30	2.12	-164.24
143	143	52.80	-2100.09	-315.53	-199.23	0	-1403.70	1.8	-300.82	1.8	-292.76	2.12	-121.55
143	144	54.20	-2104.90	-249.59	192.58	0	-1065.79	1.8	-366.76	1.8	-357.36	2.12	-251.21
144	144	54.20	-1420.02	-249.47	-137.34	0	-1143.64	1.8	-157.44	1.8	-169.73	2.12	-17.66
144	145	55.60	-1420.02	-193.01	169.11	0	-881.50	1.8	-204.18	1.8	-216.22	2.12	-114.09
145	145	55.60	-1750.84	-192.84	19.67	0	-1354.92	1.8	-226.82	1.8	-237.13	2.12	-61.74
145	146	57.00	-1750.84	-125.14	233.02	0	-1173.76	1.8	-257.64	1.8	-268.28	2.12	-127.28
146	146	57.00	-1063.03	-123.90	-96.34	0	-1176.10	1.8	-96.64	1.8	-115.75	2.12	54.36
146	147	58.40	-1062.37	-99.98	61.50	0	-1051.01	1.8	-117.71	1.8	-139.44	2.12	6.79
147	147	58.40	-1358.27	-100.88	-65.18	0	-1259.88	1.8	-90.62	1.8	-141.19	2.12	20.39
147	148	59.80	-1358.27	-78.41	60.27	0	-1171.30	1.8	-110.16	1.8	-161.64	2.12	-17.32
148	148	59.80	-1358.28	-77.94	60.33	0	-1171.25	1.8	-110.17	1.8	-161.65	2.12	-17.35
148	149	61.20	-1358.28	-55.58	153.78	0	-1104.62	1.8	-125.00	1.8	-176.88	2.12	-45.55
149	149	61.20	-1358.27	-55.10	153.79	0	-1104.62	1.8	-125.00	1.8	-176.87	2.12	-45.55
149	150	62.60	-1358.27	-32.77	215.32	0	-1059.88	1.8	-135.13	1.8	-186.88	2.12	-64.27
150	150	62.60	-1358.27	-32.31	215.33	0	-1059.87	1.8	-135.13	1.8	-186.88	2.12	-64.27
150	151	64.00	-1360.02	-9.91	244.86	0	-1038.49	1.8	-140.72	1.8	-191.91	2.12	-73.56
151	151	64.00	-1360.02	-9.46	244.85	0	-1038.50	1.8	-140.72	1.8	-191.91	2.12	-73.56
151	152	65.40	-1360.02	17.31	239.89	0	-1039.68	1.8	-140.95	1.8	-191.04	2.12	-72.46
152	152	65.40	-1360.02	17.77	239.92	0	-1039.65	1.8	-140.96	1.8	-191.05	2.12	-72.47
152	153	66.80	-1360.02	41.25	198.64	0	-1066.31	1.8	-135.64	1.8	-184.22	2.12	-60.45
153	153	66.80	-1360.02	41.70	198.60	0	-1066.33	1.8	-135.63	1.8	-184.21	2.12	-60.44
153	154	68.20	-1360.02	64.02	124.56	0	-1115.55	1.8	-125.45	1.8	-172.03	2.12	-38.67
154	154	68.20	-1360.02	64.50	124.51	0	-1115.59	1.8	-125.44	1.8	-172.02	2.12	-38.66
154	155	69.60	-1360.02	86.96	18.54	0	-1186.70	1.8	-110.57	1.8	-154.62	2.12	-7.40
155	155	69.60	-1061.89	86.36	145.22	0	-960.34	1.8	-137.44	1.8	-152.72	2.12	-23.31
155	156	71.00	-1061.02	109.55	6.74	0	-1063.49	1.8	-120.65	1.8	-131.75	2.12	17.55
156	156	71.00	-1750.84	111.22	336.07	0	-1073.40	1.8	-285.74	1.8	-293.36	2.12	-172.44
156	157	72.40	-1750.84	187.01	142.67	0	-1236.19	1.8	-259.09	1.8	-266.01	2.12	-114.25
157	157	72.40	-1420.02	187.05	292.22	0	-762.66	1.8	-236.49	1.8	-245.13	2.12	-166.65
157	158	73.80	-1420.02	246.33	-9.23	0	-1020.00	1.8	-190.62	1.8	-199.54	2.12	-72.05
158	158	73.80	-2104.90	246.68	320.61	0	-942.23	1.8	-399.91	1.8	-387.15	2.12	-305.56
158	159	75.20	-2104.90	329.86	-72.90	0	-1283.19	1.8	-334.10	1.8	-322.82	2.12	-175.78
159	159	75.20	-1847.60	331.28	50.87	0	-909.12	1.8	-316.80	1.8	-307.55	2.12	-218.63
159	160	76.60	-1843.78	396.60	-457.87	0	-1354.96	1.8	-223.42	1.8	-217.84	2.12	-42.54
160	160	76.60	-1843.83	397.87	-457.89	0	-1354.98	1.8	-223.45	1.8	-217.86	2.12	-42.57
160	161	78.00	-1843.83	454.31	-1050.82	0	-1877.42	1.8	-113.96	1.8	-112.39	2.12	164.14
161	1161	78.00	-1807.39	-417.07	-1031.70	0	-1822.95	1.8	-111.63	1.8	-110.47	2.12	157.53
161	162	79.10	-1807.39	-370.64	-601.91	0	-1444.34	1.8	-191.63	1.8	-186.87	2.12	7.82
162	162	79.10	-1807.77	-369.67	-601.98	0	-1444.51	1.8	-191.69	1.8	-186.93	2.12	7.78
162	163	80.20	-1807.77	-299.05	-226.84	0	-1115.13	1.8	-260.35	1.8	-252.37	2.12	-121.29
163	163	80.20	-2065.60	-298.37	-353.36	0	-1491.52	1.8	-277.62	1.8	-267.37	2.12	-77.74
163	164	81.30	-2065.60	-241.67	-57.59	0	-1235.57	1.8	-327.40	1.8	-315.54	2.12	-174.99
164	164	81.30	-2066.31	-241.40	-57.78	0	-1235.97	1.8	-327.50	1.8	-315.63	2.12	-175.03
164	165	82.40	-2066.31	-191.41	181.41	0	-1031.40	1.8	-365.03	1.8	-352.28	2.12	-250.67
165	165	82.40	-1566.09	-191.25	-234.45	0	-1374.63	1.8	-168.57	1.8	-176.17	2.12	12.47
165	166	83.50	-1566.09	-163.67	-41.26	0	-1211.17	1.8	-196.97	1.8	-204.02	2.12	-46.31
166	166	83.50	-1567.05	-163.35	-41.03	0	-1170.93	1.8	-236.59	1.8	-238.44	2.12	-93.06
166	167	84.60	-1567.05	-118.72	104.70	0	-1050.84	1.8	-255.26	1.8	-256.88	2.12	-133.85
167	167	84.60	-874.65	-116.01	-224.65	0	-1069.77	1.8	-62.55	1.8	-72.84	2.12	86.82
167	168	85.70	-875.52	-98.24	-104.44	0	-981.15	1.8	-78.88	1.8	-91.75	2.12	50.82
168	168	85.70	-1065.96	-100.06	-189.12	0	-1089.34	1.8	-50.02	1.8	-87.09	2.12	58.91
168	169	86.80	-1065.96	-82.49	-88.71	0	-1019.49	1.8	-65.10	1.8	-103.82	2.12	28.66
169	169	86.80	-1065.96	-82.22	-88.68	0	-1019.47	1.8	-65.11	1.8	-103.83	2.12	28.65
169	170	87.90	-1065.96	-64.68	-7.88	0	-963.05	1.8	-77.31	1.8	-117.36	2.12	4.22
170	170	87.90	-1065.96	-64.43	-7.87	0	-963.05	1.8	-77.31	1.8	-117.36	2.12	4.22
170	171	89.00	-1065.96	-46.91	53.37	0	-920.03	1.8	-86.64	1.8	-127.69	2.12	-14.40

CÁLCULO TENSIONAL

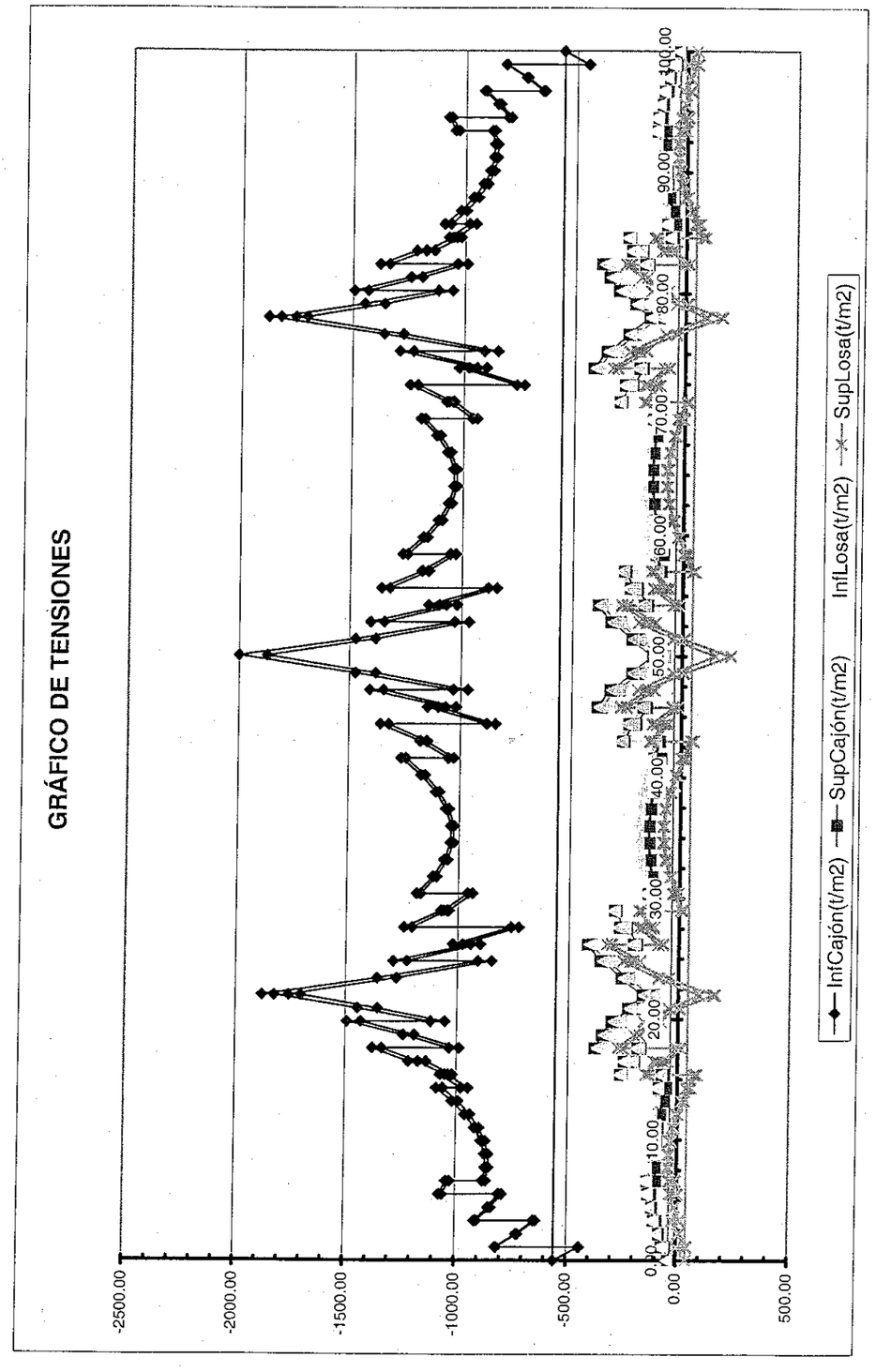
Hipótesis de cálculo:
FRECUENTEST.Tinf.MZ-

C. Frecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1065.96	-46.69	53.37	0	-920.03	1.8	-86.64	1.8	-127.69	2.12	-14.40
171	172	90.10	-1065.96	-29.12	95.03	0	-890.41	1.8	-93.10	1.8	-134.83	2.12	-27.21
172	172	90.10	-1065.96	-28.93	94.98	0	-890.45	1.8	-93.09	1.8	-134.82	2.12	-27.19
172	173	91.20	-1065.96	-11.39	117.16	0	-874.16	1.8	-96.69	1.8	-138.78	2.12	-34.22
173	173	91.20	-1065.96	-11.28	117.10	0	-874.20	1.8	-96.68	1.8	-138.77	2.12	-34.20
173	174	92.30	-1065.96	6.27	119.85	0	-871.20	1.8	-97.44	1.8	-139.55	2.12	-35.46
174	174	92.30	-1065.96	6.39	119.76	0	-871.27	1.8	-97.42	1.8	-139.54	2.12	-35.43
174	175	93.40	-1065.96	23.92	103.10	0	-881.54	1.8	-95.34	1.8	-137.15	2.12	-30.94
175	175	93.40	-1065.96	23.99	103.00	0	-1044.59	1.8	-132.54	1.8	-150.74	2.12	-6.42
175	176	94.50	-1065.96	41.55	66.93	0	-1074.47	1.8	-128.84	1.8	-145.85	2.12	4.15
176	176	94.50	-882.17	41.58	151.55	0	-810.95	1.8	-115.93	1.8	-133.93	2.12	-24.83
176	177	95.60	-882.17	59.13	96.15	0	-856.61	1.8	-110.08	1.8	-126.30	2.12	-8.49
177	177	95.60	-882.17	59.06	96.02	0	-856.72	1.8	-110.06	1.8	-126.28	2.12	-8.44
177	178	96.70	-882.17	76.59	21.39	0	-918.08	1.8	-102.07	1.8	-115.92	2.12	13.65
178	178	96.70	-698.39	76.44	107.83	0	-653.14	1.8	-89.24	1.8	-104.24	2.12	-15.85
178	179	97.80	-698.39	93.98	14.09	0	-730.09	1.8	-79.14	1.8	-91.18	2.12	11.95
179	179	97.80	-698.40	93.77	13.91	0	-730.25	1.8	-79.11	1.8	-91.15	2.12	12.00
179	180	98.90	-698.40	111.35	-98.89	0	-822.75	1.8	-66.91	1.8	-75.39	2.12	45.48
180	180	98.90	-441.09	111.02	27.27	0	-447.83	1.8	-49.16	1.8	-59.70	2.12	2.75
180	181	100.00	-441.09	251.57	-105.57	0	-556.64	1.8	-34.79	1.8	-41.11	2.12	42.20



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ+
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-153.74	-85.87	0	-492.92	1.8	-30.84	1.8	-36.65	2.12	37.15
1	2	1.10	-395.79	-191.24	137.57	0	-311.19	1.8	-61.96	1.8	-70.30	2.12	-31.43
2	2	1.10	-624.09	-191.02	29.50	0	-643.75	1.8	-77.72	1.8	-84.25	2.12	6.49
2	3	2.20	-624.09	-166.94	225.73	0	-480.11	1.8	-104.98	1.8	-113.35	2.12	-53.83
3	3	2.20	-624.08	-166.76	225.66	0	-480.16	1.8	-104.97	1.8	-113.34	2.12	-53.80
3	4	3.30	-624.08	-142.70	394.78	0	-338.88	1.8	-128.73	1.8	-138.50	2.12	-105.89
4	4	3.30	-787.15	-142.53	320.84	0	-573.89	1.8	-140.10	1.8	-148.88	2.12	-79.72
4	5	4.40	-787.15	-117.24	462.90	0	-454.93	1.8	-160.38	1.8	-170.11	2.12	-123.60
5	5	4.40	-787.15	-117.09	462.86	0	-454.96	1.8	-160.37	1.8	-170.10	2.12	-123.59
5	6	5.50	-787.15	-92.61	579.36	0	-357.02	1.8	-177.44	1.8	-187.65	2.12	-159.76
6	6	5.50	-950.22	-92.47	507.07	0	-590.75	1.8	-188.88	1.8	-198.25	2.12	-134.04
6	7	6.60	-950.22	-68.39	596.65	0	-515.03	1.8	-202.48	1.8	-211.88	2.12	-162.04
7	7	6.60	-950.22	-68.28	596.63	0	-412.00	1.8	-172.40	1.8	-202.03	2.12	-179.99
7	8	7.70	-950.22	-44.22	659.26	0	-364.94	1.8	-183.24	1.8	-212.13	2.12	-199.26
8	8	7.70	-950.22	-44.09	659.24	0	-364.96	1.8	-183.24	1.8	-212.12	2.12	-199.26
8	9	8.80	-950.22	-20.08	694.74	0	-336.82	1.8	-189.87	1.8	-217.83	2.12	-210.44
9	9	8.80	-950.22	-19.95	694.74	0	-336.83	1.8	-189.87	1.8	-217.83	2.12	-210.44
9	10	9.90	-950.22	4.09	704.68	0	-326.33	1.8	-192.58	1.8	-219.41	2.12	-214.04
10	10	9.90	-950.22	4.24	704.69	0	-326.31	1.8	-192.58	1.8	-219.41	2.12	-214.04
10	11	11.00	-950.22	28.33	687.80	0	-334.49	1.8	-191.13	1.8	-216.65	2.12	-209.65
11	11	11.00	-950.22	28.46	687.83	0	-334.47	1.8	-191.14	1.8	-216.65	2.12	-209.66
11	12	12.10	-950.22	52.54	644.03	0	-361.38	1.8	-185.52	1.8	-209.54	2.12	-197.25
12	12	12.10	-950.22	52.70	644.07	0	-361.36	1.8	-185.52	1.8	-209.54	2.12	-197.26
12	13	13.20	-950.22	76.72	573.24	0	-407.10	1.8	-175.70	1.8	-198.05	2.12	-176.79
13	13	13.20	-950.22	76.90	573.28	0	-407.07	1.8	-175.71	1.8	-198.06	2.12	-176.80
13	14	14.30	-950.22	101.00	476.43	0	-470.82	1.8	-161.89	1.8	-182.37	2.12	-148.61
14	14	14.30	-780.33	101.83	548.74	0	-333.18	1.8	-185.52	1.8	-184.90	2.12	-160.14
14	15	15.40	-775.77	123.43	423.55	0	-422.23	1.8	-168.84	1.8	-165.28	2.12	-123.11
15	15	15.40	-1554.62	125.84	794.89	0	-391.35	1.8	-383.95	1.8	-368.50	2.12	-368.44
15	16	16.50	-1554.62	117.69	649.14	0	-510.51	1.8	-367.02	1.8	-351.47	2.12	-329.33
16	16	16.50	-1554.62	117.79	649.13	0	-489.51	1.8	-387.51	1.8	-369.26	2.12	-353.54
16	17	17.60	-1554.62	134.49	509.28	0	-604.73	1.8	-370.65	1.8	-351.50	2.12	-314.18
17	17	17.60	-2163.46	134.63	954.75	0	-281.47	1.8	-595.80	1.8	-553.35	2.12	-604.40
17	18	18.70	-2163.46	146.81	798.16	0	-409.93	1.8	-577.79	1.8	-533.75	2.12	-560.71
18	18	18.70	-2163.46	146.96	798.09	0	-410.01	1.8	-577.76	1.8	-533.72	2.12	-560.67
18	19	19.80	-2163.46	160.24	628.81	0	-547.74	1.8	-559.87	1.8	-513.36	2.12	-514.54
19	19	19.80	-1935.17	160.38	736.71	0	-214.36	1.8	-544.59	1.8	-500.10	2.12	-553.18
19	20	20.90	-1935.17	173.66	552.90	0	-363.13	1.8	-526.29	1.8	-478.51	2.12	-503.78
20	20	20.90	-1935.17	173.74	552.92	0	-363.12	1.8	-526.29	1.8	-478.52	2.12	-503.78
20	21	22.00	-1935.17	188.86	353.37	0	-523.82	1.8	-507.57	1.8	-455.47	2.12	-450.69
21	1021	22.00	-1967.78	-214.39	336.95	0	-572.23	1.8	-509.71	1.8	-457.22	2.12	-444.88
21	22	23.40	-1967.78	-192.93	623.18	0	-340.40	1.8	-537.19	1.8	-491.31	2.12	-522.46
22	22	23.40	-1967.78	-192.83	623.14	0	-340.43	1.8	-537.18	1.8	-491.31	2.12	-522.45
22	23	24.80	-1967.78	-175.21	881.09	0	-130.60	1.8	-563.18	1.8	-522.33	2.12	-592.81
23	23	24.80	-2196.07	-175.12	775.31	0	-462.36	1.8	-578.52	1.8	-535.86	2.12	-554.77
23	24	26.20	-2196.07	-164.10	1011.77	0	-268.44	1.8	-604.44	1.8	-565.41	2.12	-620.75
24	24	26.20	-1424.17	-164.12	640.62	0	-355.67	1.8	-368.31	1.8	-353.75	2.12	-357.37
24	25	27.60	-1424.17	-145.47	856.57	0	-176.72	1.8	-394.42	1.8	-382.06	2.12	-419.39
25	25	27.60	-1717.69	-145.32	729.54	0	-596.26	1.8	-414.58	1.8	-400.69	2.12	-373.08
25	26	29.00	-1717.69	-151.71	956.82	0	-406.91	1.8	-443.73	1.8	-430.37	2.12	-438.29
26	26	29.00	-941.07	-150.25	585.49	0	-457.34	1.8	-209.16	1.8	-208.86	2.12	-168.19
26	27	30.40	-945.20	-122.00	775.61	0	-313.09	1.8	-235.19	1.8	-238.22	2.12	-225.43
27	27	30.40	-1210.45	-120.97	667.76	0	-559.18	1.8	-214.21	1.8	-242.05	2.12	-207.00
27	28	31.80	-1210.45	-90.14	814.44	0	-458.33	1.8	-236.37	1.8	-265.88	2.12	-250.54
28	28	31.80	-1210.45	-89.94	814.40	0	-458.35	1.8	-236.36	1.8	-265.88	2.12	-250.53
28	29	33.20	-1210.45	-58.15	917.96	0	-387.46	1.8	-251.85	1.8	-282.73	2.12	-281.23
29	29	33.20	-1210.45	-58.00	917.94	0	-387.47	1.8	-251.84	1.8	-282.73	2.12	-281.23
29	30	34.60	-1210.45	-28.66	978.79	0	-346.23	1.8	-260.73	1.8	-292.68	2.12	-299.23
30	30	34.60	-1210.45	-28.48	978.77	0	-346.24	1.8	-260.73	1.8	-292.68	2.12	-299.22
30	31	36.00	-1210.45	2.22	995.94	0	-335.43	1.8	-262.83	1.8	-295.56	2.12	-304.20
31	31	36.00	-1210.45	2.36	995.95	0	-335.43	1.8	-262.84	1.8	-295.56	2.12	-304.20
31	32	37.40	-1210.45	34.24	970.71	0	-354.02	1.8	-258.41	1.8	-291.59	2.12	-296.57
32	32	37.40	-1210.45	34.41	970.74	0	-354.00	1.8	-258.41	1.8	-291.59	2.12	-296.58
32	33	38.80	-1210.45	63.75	901.84	0	-403.01	1.8	-247.20	1.8	-280.55	2.12	-275.93
33	33	38.80	-1210.45	63.93	901.87	0	-402.99	1.8	-247.21	1.8	-280.56	2.12	-275.94
33	34	40.20	-1210.45	95.73	790.23	0	-481.66	1.8	-229.40	1.8	-262.61	2.12	-242.58
34	34	40.20	-1210.45	95.91	790.27	0	-481.64	1.8	-229.41	1.8	-262.61	2.12	-242.59
34	35	41.60	-1210.45	126.74	635.49	0	-590.29	1.8	-204.92	1.8	-237.69	2.12	-196.38
35	35	41.60	-946.85	128.21	743.32	0	-359.29	1.8	-226.00	1.8	-233.86	2.12	-212.70
35	36	43.00	-942.63	156.66	543.95	0	-514.89	1.8	-197.70	1.8	-203.28	2.12	-152.16
36	36	43.00	-1717.69	157.75	915.31	0	-445.75	1.8	-435.89	1.8	-422.83	2.12	-423.24
36	37	44.40	-1717.69	152.19	686.36	0	-637.58	1.8	-405.76	1.8	-392.18	2.12	-356.50
37	37	44.40	-1424.17	152.36	813.41	0	-218.03	1.8	-385.60	1.8	-373.55	2.12	-402.82
37	38	45.80	-1424.17	171.71	586.77	0	-407.24	1.8	-357.00	1.8	-342.94	2.12	-336.47
38	38	45.80	-2196.07	171.82	957.90	0	-320.03	1.8	-593.13	1.8	-554.59	2.12	-599.84

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ+
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	184.55	709.13	0	-525.78	1.8	-564.26	1.8	-522.34	2.12	-528.82
39	39	47.20	-1967.78	184.80	814.79	0	-194.13	1.8	-548.88	1.8	-508.78	2.12	-566.81
39	40	48.60	-1974.23	200.39	545.14	0	-417.12	1.8	-521.62	1.8	-476.56	2.12	-492.99
40	40	48.60	-1974.41	200.50	545.24	0	-417.08	1.8	-521.68	1.8	-476.61	2.12	-493.05
40	41	50.00	-1974.41	221.76	248.37	0	-659.23	1.8	-491.62	1.8	-440.14	2.12	-411.04
41	1041	50.00	-1974.19	-221.85	248.37	0	-659.17	1.8	-491.56	1.8	-440.10	2.12	-411.00
41	42	51.40	-1974.19	-200.58	545.35	0	-416.93	1.8	-521.64	1.8	-476.58	2.12	-493.03
42	42	51.40	-1973.59	-200.47	545.27	0	-416.83	1.8	-521.48	1.8	-476.43	2.12	-492.88
42	43	52.80	-1973.59	-184.38	814.94	0	-195.65	1.8	-550.36	1.8	-510.10	2.12	-568.13
43	43	52.80	-2200.88	-184.19	709.17	0	-527.11	1.8	-565.46	1.8	-523.42	2.12	-529.88
43	44	54.20	-2196.07	-171.82	957.89	0	-320.03	1.8	-593.13	1.8	-554.59	2.12	-599.84
44	44	54.20	-1424.17	-171.71	586.76	0	-407.25	1.8	-357.00	1.8	-342.94	2.12	-336.47
44	45	55.60	-1424.17	-152.36	813.43	0	-218.01	1.8	-385.61	1.8	-373.56	2.12	-402.83
45	45	55.60	-1717.69	-152.18	686.39	0	-637.56	1.8	-405.77	1.8	-392.18	2.12	-356.51
45	46	57.00	-1717.69	-157.74	915.30	0	-445.75	1.8	-435.89	1.8	-422.83	2.12	-423.24
46	46	57.00	-942.63	-156.67	543.97	0	-514.88	1.8	-197.71	1.8	-203.28	2.12	-152.16
46	47	58.40	-945.05	-127.29	742.43	0	-358.40	1.8	-225.73	1.8	-233.45	2.12	-212.37
47	47	58.40	-1208.44	-126.80	634.60	0	-589.22	1.8	-204.63	1.8	-237.25	2.12	-196.04
47	48	59.80	-1208.44	-95.97	789.48	0	-480.49	1.8	-229.13	1.8	-262.20	2.12	-242.27
48	48	59.80	-1208.43	-95.78	789.44	0	-480.51	1.8	-229.12	1.8	-262.19	2.12	-242.26
48	49	61.20	-1208.43	-63.98	901.12	0	-401.82	1.8	-246.93	1.8	-280.14	2.12	-275.63
49	49	61.20	-1208.44	-63.80	901.10	0	-401.83	1.8	-246.93	1.8	-280.14	2.12	-275.63
49	50	62.60	-1208.44	-34.47	970.08	0	-352.77	1.8	-258.15	1.8	-291.20	2.12	-296.30
50	50	62.60	-1208.44	-34.29	970.06	0	-352.78	1.8	-258.14	1.8	-291.19	2.12	-296.30
50	51	64.00	-1206.69	-2.44	995.37	0	-332.72	1.8	-262.42	1.8	-294.93	2.12	-303.87
51	51	64.00	-1206.69	-2.30	995.37	0	-332.71	1.8	-262.42	1.8	-294.93	2.12	-303.88
51	52	65.40	-1206.69	28.40	978.32	0	-343.45	1.8	-260.33	1.8	-292.07	2.12	-298.93
52	52	65.40	-1206.69	28.58	978.31	0	-343.45	1.8	-260.33	1.8	-292.07	2.12	-298.93
52	53	66.80	-1206.69	57.92	917.61	0	-384.60	1.8	-251.46	1.8	-282.14	2.12	-280.98
53	53	66.80	-1206.69	58.08	917.63	0	-384.59	1.8	-251.46	1.8	-282.14	2.12	-280.98
53	54	68.20	-1206.69	89.86	814.19	0	-455.39	1.8	-235.99	1.8	-265.31	2.12	-250.32
54	54	68.20	-1206.69	90.06	814.24	0	-455.36	1.8	-236.00	1.8	-265.31	2.12	-250.33
54	55	69.60	-1206.69	120.89	667.65	0	-556.17	1.8	-213.85	1.8	-241.50	2.12	-206.81
55	55	69.60	-941.94	120.13	775.49	0	-310.49	1.8	-234.87	1.8	-237.73	2.12	-225.26
55	56	71.00	-941.07	150.26	585.50	0	-457.33	1.8	-209.16	1.8	-208.86	2.12	-168.19
56	56	71.00	-1717.69	151.72	956.83	0	-406.90	1.8	-443.73	1.8	-430.37	2.12	-438.29
56	57	72.40	-1717.69	145.32	729.55	0	-596.25	1.8	-414.59	1.8	-400.69	2.12	-373.08
57	57	72.40	-1424.17	145.47	856.56	0	-176.73	1.8	-394.42	1.8	-382.06	2.12	-419.39
57	58	73.80	-1424.17	164.12	640.61	0	-355.68	1.8	-368.31	1.8	-353.75	2.12	-357.36
58	58	73.80	-2196.08	164.11	1011.75	0	-268.45	1.8	-604.44	1.8	-565.41	2.12	-620.74
58	59	75.20	-2196.08	175.13	775.30	0	-462.36	1.8	-578.52	1.8	-535.86	2.12	-554.77
59	59	75.20	-1967.78	175.20	881.09	0	-130.60	1.8	-563.18	1.8	-522.33	2.12	-592.81
59	60	76.60	-1971.61	192.35	623.65	0	-341.09	1.8	-538.20	1.8	-492.22	2.12	-523.43
60	60	76.60	-1971.55	192.44	623.77	0	-340.97	1.8	-538.20	1.8	-492.22	2.12	-523.45
60	61	78.00	-1971.55	213.90	338.25	0	-572.22	1.8	-510.82	1.8	-458.22	2.12	-446.05
61	1061	78.00	-1938.62	-188.71	354.70	0	-523.69	1.8	-508.61	1.8	-456.39	2.12	-451.80
61	62	79.10	-1938.62	-173.59	554.07	0	-363.14	1.8	-527.30	1.8	-479.42	2.12	-504.84
62	62	79.10	-1938.24	-173.51	554.05	0	-363.05	1.8	-527.20	1.8	-479.33	2.12	-504.76
62	63	80.20	-1938.24	-160.23	737.68	0	-214.42	1.8	-545.48	1.8	-500.90	2.12	-554.11
63	63	80.20	-2165.99	-160.08	629.76	0	-547.67	1.8	-560.63	1.8	-514.04	2.12	-515.35
63	64	81.30	-2165.99	-146.80	798.86	0	-410.08	1.8	-578.49	1.8	-534.38	2.12	-561.43
64	64	81.30	-2165.29	-146.66	798.88	0	-409.85	1.8	-578.34	1.8	-534.24	2.12	-561.31
64	65	82.40	-2165.29	-134.48	955.31	0	-281.52	1.8	-596.33	1.8	-553.82	2.12	-604.95
65	65	82.40	-1555.58	-134.39	510.07	0	-604.36	1.8	-370.96	1.8	-351.81	2.12	-314.60
65	66	83.50	-1555.58	-117.69	649.48	0	-489.50	1.8	-387.79	1.8	-369.52	2.12	-353.84
66	66	83.50	-1554.62	-117.69	649.39	0	-510.30	1.8	-367.05	1.8	-351.49	2.12	-329.40
66	67	84.60	-1554.62	-125.83	795.13	0	-391.15	1.8	-383.98	1.8	-368.53	2.12	-368.51
67	67	84.60	-775.78	-123.42	423.79	0	-422.08	1.8	-168.87	1.8	-165.32	2.12	-123.18
67	68	85.70	-776.65	-99.35	547.63	0	-330.88	1.8	-185.05	1.8	-184.19	2.12	-159.66
68	68	85.70	-945.78	-101.09	475.31	0	-467.91	1.8	-161.34	1.8	-181.55	2.12	-148.09
68	69	86.80	-945.78	-76.99	572.25	0	-404.10	1.8	-175.17	1.8	-197.25	2.12	-176.31
69	69	86.80	-945.79	-76.81	572.21	0	-404.13	1.8	-175.17	1.8	-197.25	2.12	-176.31
69	70	87.90	-945.79	-52.78	643.11	0	-358.34	1.8	-185.00	1.8	-208.75	2.12	-196.79
70	70	87.90	-945.79	-52.62	643.08	0	-358.36	1.8	-184.99	1.8	-208.75	2.12	-196.79
70	71	89.00	-945.79	-28.55	686.95	0	-331.40	1.8	-190.62	1.8	-215.87	2.12	-209.22
71	71	89.00	-945.79	-28.42	686.94	0	-331.41	1.8	-190.62	1.8	-215.87	2.12	-209.22
71	72	90.10	-945.79	-4.33	703.93	0	-323.17	1.8	-192.08	1.8	-218.65	2.12	-213.64
72	72	90.10	-945.79	-4.18	703.90	0	-323.19	1.8	-192.08	1.8	-218.65	2.12	-213.63
72	73	91.20	-945.79	19.86	694.05	0	-333.63	1.8	-189.37	1.8	-217.08	2.12	-210.05
73	73	91.20	-945.79	19.98	694.05	0	-333.63	1.8	-189.38	1.8	-217.08	2.12	-210.05
73	74	92.30	-945.79	43.99	658.65	0	-361.70	1.8	-182.76	1.8	-211.39	2.12	-198.90
74	74	92.30	-945.79	44.12	658.65	0	-361.70	1.8	-182.76	1.8	-211.39	2.12	-198.90
74	75	93.40	-945.79	68.19	596.11	0	-408.70	1.8	-171.93	1.8	-201.31	2.12	-179.66
75	75	93.40	-945.79	68.30	596.13	0	-511.15	1.8	-201.98	1.8	-211.18	2.12	-161.84
75	76	94.50	-945.79	92.38	506.63	0	-586.82	1.8	-188.38	1.8	-197.55	2.12	-133.86

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ+
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	92.53	578.93	0	-353.09	1.8	-176.94	1.8	-186.96	2.12	-159.57
76	77	95.60	-782.72	117.02	462.52	0	-450.95	1.8	-159.88	1.8	-169.43	2.12	-123.43
77	77	95.60	-782.72	117.15	462.58	0	-450.90	1.8	-159.89	1.8	-169.43	2.12	-123.45
77	78	96.70	-782.72	142.44	320.58	0	-569.82	1.8	-139.62	1.8	-148.21	2.12	-79.59
78	78	96.70	-619.65	142.61	394.54	0	-334.79	1.8	-128.25	1.8	-137.84	2.12	-105.77
78	79	97.80	-619.65	166.67	225.47	0	-476.03	1.8	-104.48	1.8	-112.68	2.12	-53.69
79	79	97.80	-619.65	166.86	225.54	0	-475.97	1.8	-104.49	1.8	-112.69	2.12	-53.71
79	80	98.90	-619.65	190.94	29.40	0	-639.54	1.8	-77.24	1.8	-83.61	2.12	6.57
80	80	98.90	-391.36	191.15	137.48	0	-306.98	1.8	-61.49	1.8	-69.66	2.12	-31.35
80	81	100.00	-391.36	153.73	-85.87	0	-492.92	1.8	-30.84	1.8	-36.65	2.12	37.15
101	101	0.00	-391.36	-171.69	-85.81	0	-492.87	1.8	-30.85	1.8	-36.65	2.12	37.14
101	102	1.10	-395.79	-186.55	132.06	0	-315.65	1.8	-61.25	1.8	-69.62	2.12	-29.90
102	102	1.10	-624.09	-186.62	24.09	0	-648.13	1.8	-77.02	1.8	-83.59	2.12	8.00
102	103	2.20	-624.09	-163.14	215.63	0	-488.28	1.8	-103.67	1.8	-112.10	2.12	-51.00
103	103	2.20	-624.08	-163.20	215.66	0	-488.25	1.8	-103.67	1.8	-112.10	2.12	-51.01
103	104	3.30	-624.08	-139.76	380.94	0	-350.08	1.8	-126.93	1.8	-136.79	2.12	-102.03
104	104	3.30	-787.15	-139.79	307.08	0	-585.03	1.8	-138.32	1.8	-147.18	2.12	-75.87
104	105	4.40	-787.15	-116.34	446.28	0	-468.37	1.8	-158.23	1.8	-168.06	2.12	-118.96
105	105	4.40	-787.15	-116.39	446.28	0	-468.38	1.8	-158.22	1.8	-168.05	2.12	-118.96
105	106	5.50	-787.15	-90.98	560.90	0	-371.95	1.8	-175.07	1.8	-185.38	2.12	-154.61
106	106	5.50	-950.22	-91.03	488.65	0	-605.65	1.8	-186.51	1.8	-195.98	2.12	-128.91
106	107	6.60	-950.22	-67.56	577.17	0	-530.76	1.8	-200.00	1.8	-209.50	2.12	-156.63
107	107	6.60	-950.22	-67.60	577.17	0	-422.32	1.8	-169.68	1.8	-199.45	2.12	-175.19
107	108	7.70	-950.22	-44.16	639.52	0	-375.31	1.8	-180.51	1.8	-209.53	2.12	-194.42
108	108	7.70	-950.22	-44.21	639.52	0	-375.31	1.8	-180.51	1.8	-209.53	2.12	-194.42
108	109	8.80	-950.22	-20.77	675.74	0	-346.60	1.8	-187.27	1.8	-215.35	2.12	-205.83
109	109	8.80	-950.22	-20.82	675.73	0	-346.61	1.8	-187.27	1.8	-215.35	2.12	-205.83
109	110	9.90	-950.22	2.62	687.11	0	-335.15	1.8	-190.22	1.8	-217.15	2.12	-209.84
110	110	9.90	-950.22	2.56	687.10	0	-335.16	1.8	-190.22	1.8	-217.14	2.12	-209.83
110	111	11.00	-950.22	26.02	672.58	0	-341.81	1.8	-189.16	1.8	-214.73	2.12	-206.10
111	111	11.00	-950.22	25.95	672.54	0	-341.83	1.8	-189.15	1.8	-214.73	2.12	-206.09
111	112	12.10	-950.22	49.40	632.00	0	-366.69	1.8	-184.04	1.8	-208.08	2.12	-194.57
112	112	12.10	-950.22	49.31	631.96	0	-366.71	1.8	-184.04	1.8	-208.08	2.12	-194.56
112	113	13.20	-950.22	72.74	565.42	0	-409.76	1.8	-174.90	1.8	-197.21	2.12	-175.27
113	113	13.20	-950.22	72.62	565.39	0	-409.78	1.8	-174.89	1.8	-197.21	2.12	-175.26
113	114	14.30	-950.22	96.08	473.73	0	-470.32	1.8	-161.88	1.8	-182.26	2.12	-148.47
114	114	14.30	-780.33	96.61	545.97	0	-335.05	1.8	-185.61	1.8	-184.87	2.12	-159.73
114	115	15.40	-775.77	117.56	427.04	0	-418.93	1.8	-169.86	1.8	-166.10	2.12	-124.54
115	115	15.40	-1554.62	119.58	798.29	0	-387.99	1.8	-385.36	1.8	-369.68	2.12	-370.30
115	116	16.50	-1554.62	116.20	660.05	0	-501.10	1.8	-369.07	1.8	-353.25	2.12	-332.89
116	116	16.50	-1554.62	116.20	660.07	0	-478.90	1.8	-390.73	1.8	-372.06	2.12	-358.48
116	117	17.60	-1554.62	132.61	522.20	0	-593.27	1.8	-373.18	1.8	-353.72	2.12	-318.59
117	117	17.60	-2163.46	132.56	967.69	0	-269.97	1.8	-598.35	1.8	-555.59	2.12	-608.84
117	118	18.70	-2163.46	141.75	815.01	0	-395.88	1.8	-580.03	1.8	-535.75	2.12	-565.30
118	118	18.70	-2163.46	141.66	814.92	0	-395.97	1.8	-580.01	1.8	-535.73	2.12	-565.27
118	119	19.80	-2163.46	152.18	653.01	0	-527.96	1.8	-562.62	1.8	-515.84	2.12	-520.62
119	119	19.80	-1935.17	151.97	760.94	0	-194.54	1.8	-547.36	1.8	-502.59	2.12	-559.28
119	120	20.90	-1935.17	162.80	587.76	0	-334.59	1.8	-530.30	1.8	-482.13	2.12	-512.60
120	120	20.90	-1935.17	162.52	587.75	0	-334.60	1.8	-530.30	1.8	-482.13	2.12	-512.59
120	121	22.00	-1935.17	178.32	399.55	0	-486.04	1.8	-512.85	1.8	-460.23	2.12	-462.33
121	1121	22.00	-1967.78	-204.17	383.14	0	-534.44	1.8	-514.98	1.8	-461.98	2.12	-456.52
121	122	23.40	-1967.78	-184.09	655.68	0	-313.72	1.8	-541.00	1.8	-494.75	2.12	-530.77
122	122	23.40	-1967.78	-184.45	655.71	0	-313.69	1.8	-541.01	1.8	-494.75	2.12	-530.78
122	123	24.80	-1967.78	-167.83	902.84	0	-112.47	1.8	-566.06	1.8	-524.90	2.12	-598.73
123	123	24.80	-2196.07	-168.22	797.13	0	-444.18	1.8	-581.39	1.8	-538.43	2.12	-560.69
123	124	26.20	-2196.07	-160.15	1025.12	0	-256.86	1.8	-606.74	1.8	-567.44	2.12	-624.97
124	124	26.20	-1424.17	-160.26	653.97	0	-344.11	1.8	-370.59	1.8	-355.76	2.12	-361.56
124	125	27.60	-1424.17	-142.79	865.49	0	-168.10	1.8	-397.01	1.8	-384.31	2.12	-423.37
125	125	27.60	-1717.69	-142.80	738.45	0	-587.67	1.8	-417.14	1.8	-402.91	2.12	-377.02
125	126	29.00	-1717.69	-146.22	956.22	0	-405.50	1.8	-445.91	1.8	-432.22	2.12	-440.63
126	126	29.00	-941.08	-145.21	585.00	0	-457.44	1.8	-209.45	1.8	-209.05	2.12	-168.34
126	127	30.40	-945.21	-117.66	768.32	0	-318.79	1.8	-234.49	1.8	-237.49	2.12	-223.59
127	127	30.40	-1210.45	-117.02	660.56	0	-562.00	1.8	-213.40	1.8	-241.23	2.12	-205.50
127	128	31.80	-1210.45	-86.94	802.03	0	-464.34	1.8	-234.75	1.8	-264.31	2.12	-247.63
128	128	31.80	-1210.45	-87.09	802.07	0	-464.32	1.8	-234.75	1.8	-264.32	2.12	-247.64
128	129	33.20	-1210.45	-55.86	902.00	0	-395.65	1.8	-249.67	1.8	-280.66	2.12	-277.37
129	129	33.20	-1210.45	-56.00	902.03	0	-395.64	1.8	-249.67	1.8	-280.66	2.12	-277.37
129	130	34.60	-1210.45	-27.71	960.83	0	-355.62	1.8	-258.25	1.8	-290.32	2.12	-294.83
130	130	34.60	-1210.45	-27.84	960.84	0	-355.62	1.8	-258.25	1.8	-290.32	2.12	-294.83
130	131	36.00	-1210.45	2.14	977.34	0	-345.22	1.8	-260.25	1.8	-293.11	2.12	-299.63
131	131	36.00	-1210.45	2.00	977.35	0	-345.22	1.8	-260.25	1.8	-293.11	2.12	-299.63
131	132	37.40	-1210.45	33.40	953.07	0	-363.18	1.8	-255.98	1.8	-289.28	2.12	-292.26
132	132	37.40	-1210.45	33.26	953.05	0	-363.19	1.8	-255.98	1.8	-289.28	2.12	-292.26
132	133	38.80	-1210.45	61.55	886.46	0	-410.78	1.8	-245.13	1.8	-278.57	2.12	-272.24
133	133	38.80	-1210.45	61.40	886.44	0	-410.79	1.8	-245.13	1.8	-278.56	2.12	-272.23

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ+
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	92.64	778.77	0	-486.99	1.8	-227.94	1.8	-261.19	2.12	-239.95
134	134	40.20	-1210.45	92.48	778.74	0	-487.01	1.8	-227.94	1.8	-261.18	2.12	-239.94
134	135	41.60	-1210.45	122.55	629.49	0	-592.24	1.8	-204.32	1.8	-237.06	2.12	-195.24
135	135	41.60	-946.85	123.59	737.25	0	-363.96	1.8	-225.51	1.8	-233.31	2.12	-211.24
135	136	43.00	-942.63	151.30	545.08	0	-513.62	1.8	-198.28	1.8	-203.71	2.12	-152.82
136	136	43.00	-1717.69	151.88	916.31	0	-442.95	1.8	-438.35	1.8	-424.92	2.12	-426.09
136	137	44.40	-1717.69	149.86	696.37	0	-628.05	1.8	-408.50	1.8	-394.56	2.12	-360.78
137	137	44.40	-1424.16	149.81	823.42	0	-208.46	1.8	-388.37	1.8	-375.96	2.12	-407.13
137	138	45.80	-1424.16	167.93	601.28	0	-394.70	1.8	-359.45	1.8	-345.10	2.12	-341.00
138	138	45.80	-2196.07	167.88	972.42	0	-307.46	1.8	-595.60	1.8	-556.78	2.12	-604.40
138	139	47.20	-2196.07	177.40	732.01	0	-506.75	1.8	-567.24	1.8	-525.01	2.12	-534.99
139	139	47.20	-1967.78	177.23	837.66	0	-175.10	1.8	-551.88	1.8	-511.46	2.12	-573.00
139	140	48.60	-1974.23	191.77	579.67	0	-388.70	1.8	-525.77	1.8	-480.29	2.12	-501.91
140	140	48.60	-1974.41	191.40	579.71	0	-388.71	1.8	-525.82	1.8	-480.34	2.12	-501.97
140	141	50.00	-1974.41	211.23	296.88	0	-619.44	1.8	-497.28	1.8	-445.24	2.12	-423.41
141	1141	50.00	-1974.19	-211.31	296.89	0	-619.37	1.8	-497.23	1.8	-445.20	2.12	-423.36
141	142	51.40	-1974.19	-191.48	579.83	0	-388.55	1.8	-525.78	1.8	-480.30	2.12	-501.95
142	142	51.40	-1973.59	-191.85	579.81	0	-388.40	1.8	-525.63	1.8	-480.17	2.12	-501.81
142	143	52.80	-1973.59	-176.81	837.80	0	-176.63	1.8	-553.35	1.8	-512.78	2.12	-574.31
143	143	52.80	-2200.88	-177.04	732.05	0	-508.08	1.8	-568.44	1.8	-526.09	2.12	-536.06
143	144	54.20	-2196.07	-167.88	972.39	0	-307.49	1.8	-595.60	1.8	-556.78	2.12	-604.39
144	144	54.20	-1424.17	-167.94	601.26	0	-394.72	1.8	-359.45	1.8	-345.10	2.12	-341.00
144	145	55.60	-1424.17	-149.82	823.42	0	-208.47	1.8	-388.37	1.8	-375.96	2.12	-407.14
145	145	55.60	-1717.69	-149.86	696.37	0	-628.05	1.8	-408.50	1.8	-394.56	2.12	-360.79
145	146	57.00	-1717.69	-151.88	916.31	0	-442.94	1.8	-438.35	1.8	-424.93	2.12	-426.09
146	146	57.00	-942.63	-151.31	545.08	0	-513.62	1.8	-198.28	1.8	-203.71	2.12	-152.82
146	147	58.40	-945.05	-122.69	736.37	0	-363.06	1.8	-225.24	1.8	-232.91	2.12	-210.91
147	147	58.40	-1208.44	-122.60	628.62	0	-591.15	1.8	-204.03	1.8	-236.62	2.12	-194.90
147	148	59.80	-1208.44	-92.53	777.93	0	-485.88	1.8	-227.66	1.8	-260.76	2.12	-239.62
148	148	59.80	-1208.45	-92.70	777.96	0	-485.87	1.8	-227.66	1.8	-260.77	2.12	-239.63
148	149	61.20	-1208.45	-61.45	885.69	0	-409.63	1.8	-244.85	1.8	-278.16	2.12	-271.93
149	149	61.20	-1208.44	-61.61	885.72	0	-409.61	1.8	-244.85	1.8	-278.16	2.12	-271.93
149	150	62.60	-1208.44	-33.31	952.42	0	-361.95	1.8	-255.72	1.8	-288.88	2.12	-291.99
150	150	62.60	-1208.44	-33.45	952.44	0	-361.93	1.8	-255.72	1.8	-288.89	2.12	-292.00
150	151	64.00	-1206.69	-2.08	976.79	0	-342.49	1.8	-259.84	1.8	-292.48	2.12	-299.31
151	151	64.00	-1206.69	-2.22	976.79	0	-342.49	1.8	-259.84	1.8	-292.48	2.12	-299.31
151	152	65.40	-1206.69	27.76	960.39	0	-352.82	1.8	-257.85	1.8	-289.71	2.12	-294.54
152	152	65.40	-1206.69	27.63	960.38	0	-352.83	1.8	-257.85	1.8	-289.71	2.12	-294.54
152	153	66.80	-1206.69	55.91	901.70	0	-392.76	1.8	-249.29	1.8	-280.07	2.12	-277.12
153	153	66.80	-1206.69	55.78	901.68	0	-392.77	1.8	-249.29	1.8	-280.07	2.12	-277.12
153	154	68.20	-1206.69	87.01	801.84	0	-461.38	1.8	-234.38	1.8	-263.75	2.12	-247.42
154	154	68.20	-1206.69	86.85	801.81	0	-461.39	1.8	-234.37	1.8	-263.74	2.12	-247.41
154	155	69.60	-1206.69	116.93	660.47	0	-558.97	1.8	-213.04	1.8	-240.68	2.12	-205.32
155	155	69.60	-941.94	115.78	768.21	0	-316.17	1.8	-234.18	1.8	-237.00	2.12	-223.43
155	156	71.00	-941.07	145.20	585.01	0	-457.42	1.8	-209.45	1.8	-209.05	2.12	-168.35
156	156	71.00	-1717.69	146.21	956.25	0	-405.47	1.8	-445.92	1.8	-432.23	2.12	-440.64
156	157	72.40	-1717.69	142.81	738.47	0	-587.65	1.8	-417.14	1.8	-402.92	2.12	-377.03
157	157	72.40	-1424.17	142.79	865.49	0	-168.10	1.8	-397.01	1.8	-384.31	2.12	-423.37
157	158	73.80	-1424.17	160.26	653.97	0	-344.11	1.8	-370.59	1.8	-355.76	2.12	-361.56
158	158	73.80	-2196.07	160.16	1025.12	0	-256.87	1.8	-606.74	1.8	-567.44	2.12	-624.97
158	159	75.20	-2196.07	168.22	797.11	0	-444.20	1.8	-581.39	1.8	-538.43	2.12	-560.68
159	159	75.20	-1967.78	167.83	902.85	0	-112.47	1.8	-566.06	1.8	-524.90	2.12	-598.73
159	160	76.60	-1971.61	183.98	656.24	0	-314.34	1.8	-542.03	1.8	-495.67	2.12	-531.75
160	160	76.60	-1971.55	183.60	656.28	0	-314.29	1.8	-542.02	1.8	-495.66	2.12	-531.75
160	161	78.00	-1971.55	203.67	384.44	0	-534.44	1.8	-516.09	1.8	-462.98	2.12	-457.69
161	1161	78.00	-1938.62	-178.18	400.89	0	-485.91	1.8	-513.88	1.8	-461.15	2.12	-463.44
161	162	79.10	-1938.62	-162.38	588.89	0	-334.63	1.8	-531.31	1.8	-483.03	2.12	-513.65
162	162	79.10	-1938.23	-162.64	588.90	0	-334.52	1.8	-531.21	1.8	-482.94	2.12	-513.57
162	163	80.20	-1938.23	-151.82	761.92	0	-194.59	1.8	-548.25	1.8	-503.39	2.12	-560.21
163	163	80.20	-2165.99	-152.02	653.96	0	-527.89	1.8	-563.37	1.8	-516.51	2.12	-521.42
163	164	81.30	-2165.99	-141.50	815.70	0	-396.04	1.8	-580.74	1.8	-536.39	2.12	-566.03
164	164	81.30	-2165.29	-141.60	815.73	0	-395.81	1.8	-580.58	1.8	-536.24	2.12	-565.90
164	165	82.40	-2165.29	-132.42	968.25	0	-270.03	1.8	-598.88	1.8	-556.06	2.12	-609.39
165	165	82.40	-1555.58	-132.51	523.00	0	-592.89	1.8	-373.50	1.8	-354.04	2.12	-319.02
165	166	83.50	-1555.58	-116.09	660.41	0	-478.88	1.8	-391.02	1.8	-372.32	2.12	-358.78
166	166	83.50	-1554.62	-116.19	660.29	0	-500.91	1.8	-369.10	1.8	-353.28	2.12	-332.95
166	167	84.60	-1554.62	-119.58	798.55	0	-387.79	1.8	-385.40	1.8	-369.71	2.12	-370.37
167	167	84.60	-775.78	-117.54	427.29	0	-418.77	1.8	-169.89	1.8	-166.15	2.12	-124.61
167	168	85.70	-776.65	-94.13	544.83	0	-332.77	1.8	-185.13	1.8	-184.15	2.12	-159.24
168	168	85.70	-945.79	-96.17	472.60	0	-467.41	1.8	-161.34	1.8	-181.44	2.12	-147.96
168	169	86.80	-945.79	-72.71	564.36	0	-406.81	1.8	-174.36	1.8	-196.40	2.12	-174.77
169	169	86.80	-945.79	-72.83	564.38	0	-406.80	1.8	-174.36	1.8	-196.41	2.12	-174.78
169	170	87.90	-945.79	-49.40	631.02	0	-363.68	1.8	-183.52	1.8	-207.29	2.12	-194.10
170	170	87.90	-945.79	-49.48	631.05	0	-363.67	1.8	-183.52	1.8	-207.29	2.12	-194.11
170	171	89.00	-945.79	-26.05	671.69	0	-338.74	1.8	-188.64	1.8	-213.95	2.12	-205.66

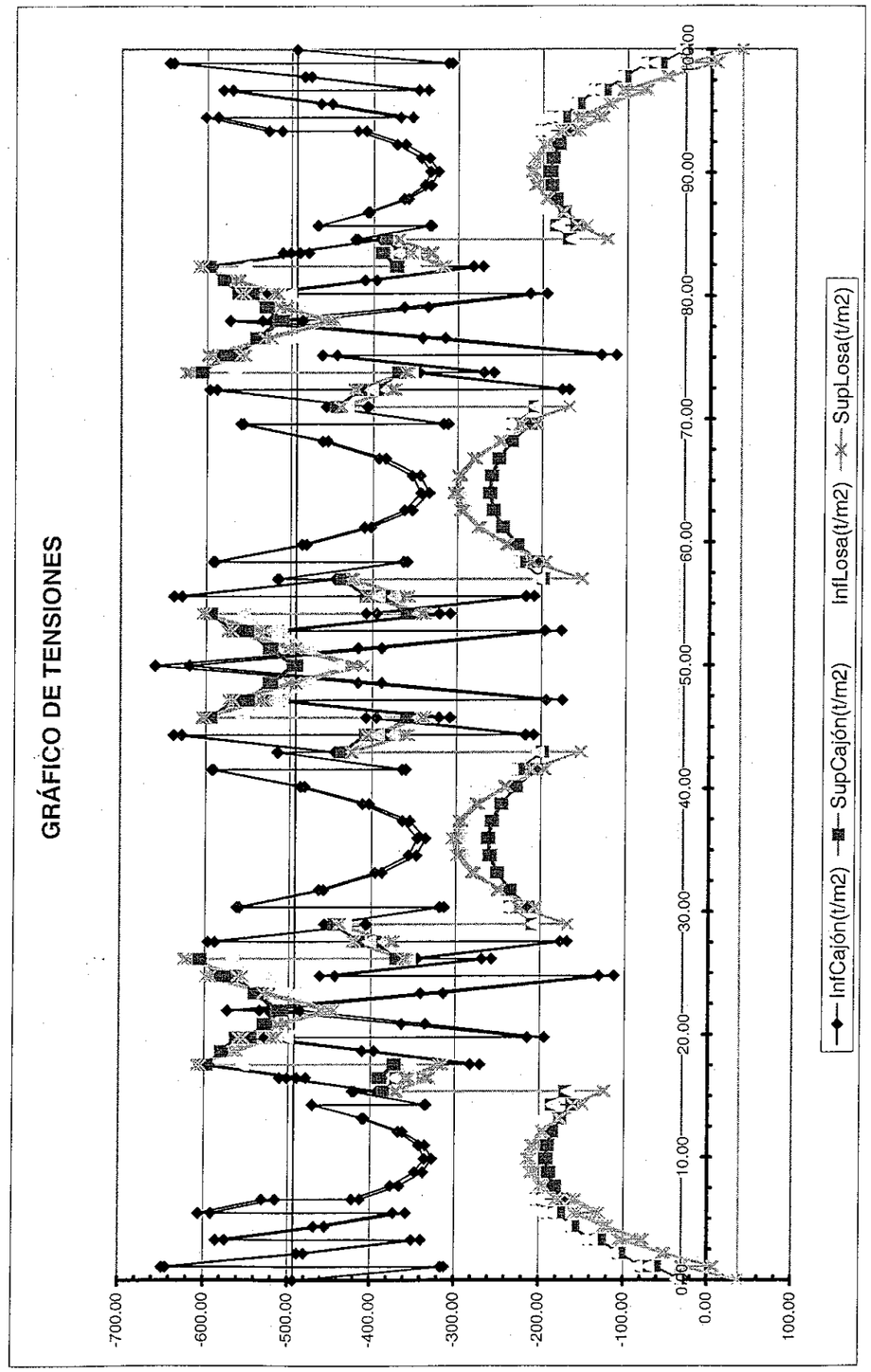
CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ+
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-26.13	671.72	0	-338.72	1.8	-188.64	1.8	-213.96	2.12	-205.66
171	172	90.10	-945.79	-2.65	686.32	0	-332.02	1.8	-189.72	1.8	-216.38	2.12	-209.42
172	172	90.10	-945.79	-2.71	686.33	0	-332.02	1.8	-189.72	1.8	-216.38	2.12	-209.42
172	173	91.20	-945.79	20.74	675.03	0	-343.43	1.8	-186.78	1.8	-214.60	2.12	-205.44
173	173	91.20	-945.79	20.66	675.05	0	-343.41	1.8	-186.78	1.8	-214.61	2.12	-205.44
173	174	92.30	-945.79	44.12	638.92	0	-372.06	1.8	-180.03	1.8	-208.80	2.12	-194.06
174	174	92.30	-945.79	44.08	638.92	0	-372.06	1.8	-180.03	1.8	-208.80	2.12	-194.06
174	175	93.40	-945.79	67.52	576.65	0	-419.02	1.8	-169.21	1.8	-198.74	2.12	-174.85
175	175	93.40	-945.79	67.47	576.65	0	-526.89	1.8	-199.50	1.8	-208.80	2.12	-156.42
175	176	94.50	-945.79	90.93	488.21	0	-601.72	1.8	-186.02	1.8	-195.29	2.12	-128.72
176	176	94.50	-782.72	90.88	560.48	0	-368.00	1.8	-174.58	1.8	-184.69	2.12	-154.43
176	177	95.60	-782.72	116.30	445.94	0	-464.37	1.8	-157.73	1.8	-167.38	2.12	-118.80
177	177	95.60	-782.72	116.24	445.94	0	-464.37	1.8	-157.74	1.8	-167.38	2.12	-118.80
177	178	96.70	-782.72	139.70	306.81	0	-580.96	1.8	-137.83	1.8	-146.51	2.12	-75.74
178	178	96.70	-619.65	139.66	380.70	0	-345.99	1.8	-126.45	1.8	-136.12	2.12	-101.90
178	179	97.80	-619.65	163.10	215.47	0	-484.12	1.8	-103.19	1.8	-111.45	2.12	-50.90
179	179	97.80	-619.66	163.06	215.44	0	-484.14	1.8	-103.19	1.8	-111.45	2.12	-50.89
179	180	98.90	-619.66	186.53	23.99	0	-643.92	1.8	-76.54	1.8	-82.94	2.12	8.08
180	180	98.90	-391.36	186.45	131.99	0	-311.42	1.8	-60.78	1.8	-68.98	2.12	-29.82
180	181	100.00	-391.36	171.68	-85.81	0	-492.87	1.8	-30.85	1.8	-36.65	2.12	37.14



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ-
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-200.13	-105.06	0	-556.20	1.8	-34.89	1.8	-41.19	2.12	42.03
1	2	1.10	-436.66	-127.47	45.09	0	-428.33	1.8	-51.96	1.8	-61.93	2.12	-2.94
2	2	1.10	-693.96	-127.37	-81.32	0	-803.45	1.8	-69.67	1.8	-77.59	2.12	39.86
2	3	2.20	-693.96	-110.09	49.29	0	-695.71	1.8	-85.16	1.8	-96.23	2.12	0.61
3	3	2.20	-693.96	-110.01	49.23	0	-695.76	1.8	-85.15	1.8	-96.22	2.12	0.63
3	4	3.30	-693.96	-92.73	160.72	0	-603.59	1.8	-98.57	1.8	-112.18	2.12	-32.94
4	4	3.30	-877.74	-92.68	74.10	0	-868.68	1.8	-111.36	1.8	-123.83	2.12	-3.39
4	5	4.40	-877.74	-75.41	166.54	0	-792.03	1.8	-122.71	1.8	-137.11	2.12	-31.30
5	5	4.40	-877.74	-75.38	166.50	0	-792.07	1.8	-122.70	1.8	-137.11	2.12	-31.28
5	6	5.50	-877.74	-58.10	239.90	0	-730.92	1.8	-131.98	1.8	-147.72	2.12	-53.53
6	6	5.50	-1061.53	-58.08	155.13	0	-994.57	1.8	-144.85	1.8	-159.61	2.12	-24.51
6	7	6.60	-1061.53	-40.81	209.54	0	-948.89	1.8	-152.06	1.8	-167.55	2.12	-41.12
7	7	6.60	-1061.53	-40.82	209.51	0	-793.78	1.8	-115.16	1.8	-154.17	2.12	-64.63
7	8	7.70	-1061.53	-23.55	244.90	0	-768.29	1.8	-120.88	1.8	-159.72	2.12	-75.20
8	8	7.70	-1061.53	-23.56	244.87	0	-768.31	1.8	-120.88	1.8	-159.71	2.12	-75.19
8	9	8.80	-1061.53	-6.22	261.28	0	-755.62	1.8	-123.86	1.8	-162.18	2.12	-80.18
9	9	8.80	-1061.54	-6.27	261.26	0	-755.64	1.8	-123.86	1.8	-162.18	2.12	-80.18
9	10	9.90	-1061.54	11.03	258.65	0	-755.79	1.8	-124.11	1.8	-161.55	2.12	-79.56
10	10	9.90	-1061.53	10.99	258.65	0	-755.79	1.8	-124.11	1.8	-161.55	2.12	-79.56
10	11	11.00	-1061.53	28.27	237.05	0	-768.76	1.8	-121.61	1.8	-157.84	2.12	-73.35
11	11	11.00	-1061.53	28.22	237.06	0	-768.76	1.8	-121.61	1.8	-157.84	2.12	-73.35
11	12	12.10	-1061.53	45.51	196.50	0	-794.53	1.8	-116.39	1.8	-151.05	2.12	-61.57
12	12	12.10	-1061.53	45.47	196.51	0	-794.52	1.8	-116.39	1.8	-151.06	2.12	-61.57
12	13	13.20	-1061.53	62.76	136.97	0	-833.09	1.8	-108.43	1.8	-141.19	2.12	-44.20
13	13	13.20	-1061.53	62.74	136.99	0	-833.08	1.8	-108.43	1.8	-141.19	2.12	-44.20
13	14	14.30	-1061.53	80.03	58.46	0	-884.47	1.8	-97.73	1.8	-128.24	2.12	-21.24
14	14	14.30	-871.84	75.36	143.23	0	-764.40	1.8	-126.22	1.8	-132.63	2.12	-30.84
14	15	15.40	-874.66	95.10	47.02	0	-835.49	1.8	-114.94	1.8	-118.39	2.12	-3.02
15	15	15.40	-1567.05	97.45	376.49	0	-816.95	1.8	-305.81	1.8	-300.81	2.12	-221.73
15	16	16.50	-1567.05	146.93	254.65	0	-916.24	1.8	-292.02	1.8	-286.58	2.12	-189.09
16	16	16.50	-1567.05	147.09	254.74	0	-925.09	1.8	-283.33	1.8	-279.03	2.12	-178.84
16	17	17.60	-1567.05	170.23	80.41	0	-1068.23	1.8	-262.86	1.8	-258.00	2.12	-131.14
17	17	17.60	-2068.15	170.35	496.89	0	-724.76	1.8	-459.60	1.8	-434.38	2.12	-394.66
17	18	18.70	-2068.15	196.83	295.05	0	-890.91	1.8	-435.62	1.8	-409.44	2.12	-338.69
18	18	18.70	-2068.15	196.99	295.22	0	-890.76	1.8	-435.66	1.8	-409.48	2.12	-338.75
18	19	19.80	-2068.15	224.68	63.63	0	-1082.04	1.8	-407.62	1.8	-380.12	2.12	-273.57
19	19	19.80	-1810.85	224.88	190.16	0	-705.81	1.8	-390.46	1.8	-365.22	2.12	-317.21
19	20	20.90	-1810.85	255.54	-75.42	0	-926.29	1.8	-357.12	1.8	-330.39	2.12	-240.92
20	20	20.90	-1810.85	255.81	-75.39	0	-926.27	1.8	-357.13	1.8	-330.39	2.12	-240.93
20	21	22.00	-1810.85	285.22	-372.71	0	-1173.48	1.8	-319.51	1.8	-290.72	2.12	-154.67
21	1021	22.00	-1847.60	-312.05	-391.85	0	-1228.05	1.8	-321.92	1.8	-292.71	2.12	-148.13
21	22	23.40	-1847.60	-277.35	19.52	0	-885.20	1.8	-373.92	1.8	-348.35	2.12	-268.53
22	22	23.40	-1847.60	-277.02	19.50	0	-885.21	1.8	-373.92	1.8	-348.36	2.12	-268.54
22	23	24.80	-1847.60	-241.22	382.21	0	-583.01	1.8	-419.78	1.8	-396.86	2.12	-374.01
23	23	24.80	-2104.90	-240.51	258.36	0	-957.13	1.8	-437.09	1.8	-412.14	2.12	-331.16
23	24	26.20	-2104.90	-201.92	565.77	0	-702.47	1.8	-474.30	1.8	-451.69	2.12	-418.53
24	24	26.20	-1420.02	-201.58	236.11	0	-780.02	1.8	-265.11	1.8	-264.17	2.12	-185.15
24	25	27.60	-1420.02	-167.38	494.22	0	-567.13	1.8	-295.39	1.8	-296.28	2.12	-257.08
25	25	27.60	-1750.84	-167.23	344.75	0	-1040.54	1.8	-318.06	1.8	-317.22	2.12	-204.77
25	26	29.00	-1750.84	-108.21	517.30	0	-899.07	1.8	-337.28	1.8	-338.16	2.12	-252.14
26	26	29.00	-1061.02	-107.01	187.80	0	-907.40	1.8	-155.49	1.8	-162.04	2.12	-42.27
26	27	30.40	-1058.63	-82.79	323.36	0	-804.19	1.8	-171.25	1.8	-181.94	2.12	-81.89
27	27	30.40	-1356.26	-85.67	196.54	0	-1039.64	1.8	-144.66	1.8	-184.05	2.12	-64.82
27	28	31.80	-1356.26	-63.67	301.07	0	-970.26	1.8	-159.15	1.8	-201.13	2.12	-95.45
28	28	31.80	-1356.26	-63.74	301.02	0	-970.30	1.8	-159.14	1.8	-201.12	2.12	-95.43
28	29	33.20	-1356.26	-41.74	374.85	0	-921.63	1.8	-169.20	1.8	-213.22	2.12	-117.03
29	29	33.20	-1356.26	-41.83	374.82	0	-921.66	1.8	-169.20	1.8	-213.21	2.12	-117.02
29	30	34.60	-1356.26	-19.53	417.71	0	-893.90	1.8	-174.79	1.8	-220.28	2.12	-129.50
30	30	34.60	-1356.26	-19.59	417.68	0	-893.93	1.8	-174.79	1.8	-220.28	2.12	-129.49
30	31	36.00	-1356.26	3.31	428.92	0	-887.67	1.8	-175.78	1.8	-222.20	2.12	-132.62
31	31	36.00	-1356.26	3.22	428.92	0	-887.68	1.8	-175.78	1.8	-222.20	2.12	-132.62
31	32	37.40	-1356.26	25.24	408.98	0	-902.53	1.8	-172.25	1.8	-219.06	2.12	-126.56
32	32	37.40	-1356.26	25.16	409.00	0	-902.52	1.8	-172.25	1.8	-219.06	2.12	-126.56
32	33	38.80	-1356.26	47.15	358.39	0	-938.07	1.8	-164.30	1.8	-210.94	2.12	-111.47
33	33	38.80	-1356.26	47.07	358.43	0	-938.05	1.8	-164.31	1.8	-210.94	2.12	-111.48
33	34	40.20	-1356.26	69.07	277.12	0	-994.31	1.8	-151.94	1.8	-197.84	2.12	-87.35
34	34	40.20	-1356.26	68.99	277.17	0	-994.28	1.8	-151.95	1.8	-197.84	2.12	-87.36
34	35	41.60	-1356.26	90.99	165.20	0	-1071.23	1.8	-135.16	1.8	-179.75	2.12	-54.21
35	35	41.60	-1060.58	88.60	292.00	0	-850.70	1.8	-161.86	1.8	-177.68	2.12	-69.23
35	36	43.00	-1063.03	112.61	150.16	0	-963.50	1.8	-144.16	1.8	-157.06	2.12	-27.15
36	36	43.00	-1750.84	113.31	479.67	0	-936.03	1.8	-328.35	1.8	-329.71	2.12	-236.37
36	37	44.40	-1750.84	171.53	293.11	0	-1090.01	1.8	-306.83	1.8	-306.61	2.12	-184.47
37	37	44.40	-1420.02	171.67	442.55	0	-616.62	1.8	-284.15	1.8	-285.66	2.12	-236.77
37	38	45.80	-1420.02	205.13	179.57	0	-834.13	1.8	-253.09	1.8	-252.74	2.12	-163.13
38	38	45.80	-2104.90	205.35	509.27	0	-756.55	1.8	-462.29	1.8	-440.27	2.12	-396.53

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ-
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	240.31	198.26	0	-1014.58	1.8	-424.69	1.8	-400.23	2.12	-308.03
39	39	47.20	-1847.60	240.48	322.20	0	-640.38	1.8	-407.41	1.8	-384.97	2.12	-350.93
39	40	48.60	-1841.15	280.18	-43.02	0	-943.01	1.8	-359.95	1.8	-334.89	2.12	-243.51
40	40	48.60	-1840.98	280.53	-43.03	0	-942.98	1.8	-359.90	1.8	-334.85	2.12	-243.46
40	41	50.00	-1840.98	315.91	-459.69	0	-1290.74	1.8	-307.13	1.8	-278.39	2.12	-121.31
41	1041	50.00	-1841.19	-315.83	-459.70	0	-1290.81	1.8	-307.19	1.8	-278.44	2.12	-121.36
41	42	51.40	-1841.19	-280.45	-43.16	0	-943.15	1.8	-359.93	1.8	-334.88	2.12	-243.47
42	42	51.40	-1841.79	-280.09	-43.16	0	-943.31	1.8	-360.09	1.8	-335.02	2.12	-243.61
42	43	52.80	-1841.79	-240.89	322.05	0	-638.86	1.8	-405.93	1.8	-383.65	2.12	-349.61
43	43	52.80	-2100.09	-240.67	198.21	0	-1013.26	1.8	-423.48	1.8	-399.14	2.12	-306.97
43	44	54.20	-2104.90	-205.35	509.27	0	-756.55	1.8	-462.30	1.8	-440.27	2.12	-396.53
44	44	54.20	-1420.02	-205.13	179.56	0	-834.14	1.8	-253.08	1.8	-252.73	2.12	-163.13
44	45	55.60	-1420.02	-171.67	442.57	0	-616.60	1.8	-284.15	1.8	-285.67	2.12	-236.78
45	45	55.60	-1750.84	-171.52	293.13	0	-1089.98	1.8	-306.83	1.8	-306.62	2.12	-184.48
45	46	57.00	-1750.84	-113.30	479.67	0	-936.03	1.8	-328.35	1.8	-329.71	2.12	-236.37
46	46	57.00	-1063.03	-112.61	150.16	0	-963.49	1.8	-144.17	1.8	-157.06	2.12	-27.15
46	47	58.40	-1062.37	-89.52	292.90	0	-851.59	1.8	-162.13	1.8	-178.08	2.12	-69.57
47	47	58.40	-1358.27	-90.93	166.09	0	-1072.30	1.8	-135.45	1.8	-180.19	2.12	-54.56
47	48	59.80	-1358.27	-68.93	278.01	0	-995.38	1.8	-152.23	1.8	-198.27	2.12	-87.69
48	48	59.80	-1358.27	-69.00	277.96	0	-995.41	1.8	-152.22	1.8	-198.26	2.12	-87.68
48	49	61.20	-1358.27	-47.01	359.15	0	-939.22	1.8	-164.58	1.8	-211.35	2.12	-111.77
49	49	61.20	-1358.27	-47.09	359.13	0	-939.24	1.8	-164.58	1.8	-211.35	2.12	-111.77
49	50	62.60	-1358.27	-25.10	409.66	0	-903.74	1.8	-172.51	1.8	-219.46	2.12	-126.84
50	50	62.60	-1358.27	-25.18	409.64	0	-903.76	1.8	-172.51	1.8	-219.45	2.12	-126.83
50	51	64.00	-1360.02	-3.14	429.47	0	-890.41	1.8	-176.19	1.8	-222.83	2.12	-132.93
51	51	64.00	-1360.02	-3.22	429.48	0	-890.40	1.8	-176.19	1.8	-222.83	2.12	-132.94
51	52	65.40	-1360.02	19.68	418.13	0	-896.73	1.8	-175.19	1.8	-220.89	2.12	-129.77
52	52	65.40	-1360.02	19.61	418.14	0	-896.72	1.8	-175.19	1.8	-220.89	2.12	-129.78
52	53	66.80	-1360.02	41.91	375.16	0	-924.53	1.8	-169.58	1.8	-213.80	2.12	-117.27
53	53	66.80	-1360.02	41.83	375.19	0	-924.50	1.8	-169.59	1.8	-213.81	2.12	-117.28
53	54	68.20	-1360.02	63.82	301.26	0	-973.23	1.8	-159.51	1.8	-201.69	2.12	-95.66
54	54	68.20	-1360.02	63.75	301.31	0	-973.20	1.8	-159.52	1.8	-201.70	2.12	-95.67
54	55	69.60	-1360.02	85.75	196.65	0	-1042.66	1.8	-145.01	1.8	-184.60	2.12	-65.00
55	55	69.60	-1061.89	84.66	323.46	0	-806.81	1.8	-171.56	1.8	-182.42	2.12	-82.05
55	56	71.00	-1061.02	107.01	187.80	0	-907.39	1.8	-155.49	1.8	-162.04	2.12	-42.27
56	56	71.00	-1750.84	108.22	517.30	0	-899.07	1.8	-337.28	1.8	-338.16	2.12	-252.14
56	57	72.40	-1750.84	167.23	344.76	0	-1040.54	1.8	-318.06	1.8	-317.22	2.12	-204.77
57	57	72.40	-1420.02	167.38	494.20	0	-567.15	1.8	-295.38	1.8	-296.28	2.12	-257.08
57	58	73.80	-1420.02	201.59	236.10	0	-780.03	1.8	-265.10	1.8	-264.17	2.12	-185.15
58	58	73.80	-2104.91	201.93	565.76	0	-702.48	1.8	-474.31	1.8	-451.69	2.12	-418.53
58	59	75.20	-2104.91	240.52	258.34	0	-957.14	1.8	-437.09	1.8	-412.14	2.12	-331.16
59	59	75.20	-1847.60	241.21	382.22	0	-583.00	1.8	-419.78	1.8	-396.86	2.12	-374.01
59	60	76.60	-1843.78	277.48	18.99	0	-884.55	1.8	-372.90	1.8	-347.44	2.12	-267.57
60	60	76.60	-1843.83	277.84	18.92	0	-884.63	1.8	-372.90	1.8	-347.44	2.12	-267.55
60	61	78.00	-1843.83	312.54	-393.14	0	-1228.05	1.8	-320.81	1.8	-291.72	2.12	-146.96
61	1061	78.00	-1807.39	-285.37	-374.03	0	-1173.60	1.8	-318.48	1.8	-289.80	2.12	-153.56
61	62	79.10	-1807.39	-255.96	-76.57	0	-926.26	1.8	-356.12	1.8	-329.48	2.12	-239.86
62	62	79.10	-1807.77	-255.71	-76.60	0	-926.40	1.8	-356.21	1.8	-329.56	2.12	-239.94
62	63	80.20	-1807.77	-225.05	189.16	0	-705.77	1.8	-389.56	1.8	-364.42	2.12	-316.27
63	63	80.20	-2065.61	-224.85	62.66	0	-1082.12	1.8	-406.86	1.8	-379.45	2.12	-272.75
63	64	81.30	-2065.61	-197.15	294.44	0	-890.70	1.8	-434.92	1.8	-408.82	2.12	-337.99
64	64	81.30	-2066.31	-196.98	294.33	0	-890.99	1.8	-435.07	1.8	-408.95	2.12	-338.10
64	65	82.40	-2066.31	-170.49	496.33	0	-724.70	1.8	-459.07	1.8	-433.91	2.12	-394.11
65	65	82.40	-1566.09	-170.33	80.30	0	-1068.07	1.8	-262.58	1.8	-257.78	2.12	-130.91
65	66	83.50	-1566.09	-147.19	254.37	0	-925.13	1.8	-283.04	1.8	-278.78	2.12	-178.52
66	66	83.50	-1567.05	-146.96	254.39	0	-916.46	1.8	-291.98	1.8	-286.55	2.12	-189.02
66	67	84.60	-1567.05	-97.48	376.24	0	-817.16	1.8	-305.77	1.8	-300.78	2.12	-221.67
67	67	84.60	-874.65	-95.11	46.77	0	-835.64	1.8	-114.91	1.8	-118.35	2.12	-2.95
67	68	85.70	-875.52	-77.83	144.34	0	-766.70	1.8	-126.70	1.8	-133.34	2.12	-31.32
68	68	85.70	-1065.95	-79.96	59.57	0	-887.39	1.8	-98.27	1.8	-129.05	2.12	-21.75
68	69	86.80	-1065.95	-62.66	138.02	0	-836.05	1.8	-108.96	1.8	-141.99	2.12	-44.69
69	69	86.80	-1065.96	-62.69	137.99	0	-836.07	1.8	-108.96	1.8	-141.99	2.12	-44.68
69	70	87.90	-1065.96	-45.39	197.44	0	-797.55	1.8	-116.91	1.8	-151.84	2.12	-62.03
70	70	87.90	-1065.96	-45.43	197.43	0	-797.56	1.8	-116.91	1.8	-151.84	2.12	-62.02
70	71	89.00	-1065.96	-28.15	237.90	0	-771.85	1.8	-122.12	1.8	-158.61	2.12	-73.79
71	71	89.00	-1065.96	-28.21	237.90	0	-771.85	1.8	-122.12	1.8	-158.61	2.12	-73.79
71	72	90.10	-1065.96	-10.93	259.43	0	-758.92	1.8	-124.61	1.8	-162.31	2.12	-79.97
72	72	90.10	-1065.96	-10.96	259.41	0	-758.94	1.8	-124.60	1.8	-162.31	2.12	-79.97
72	73	91.20	-1065.96	6.34	261.93	0	-758.84	1.8	-124.35	1.8	-162.92	2.12	-80.55
73	73	91.20	-1065.96	6.28	261.96	0	-758.82	1.8	-124.35	1.8	-162.92	2.12	-80.56
73	74	92.30	-1065.96	23.62	245.46	0	-771.56	1.8	-121.36	1.8	-160.44	2.12	-75.55
74	74	92.30	-1065.96	23.62	245.48	0	-771.55	1.8	-121.36	1.8	-160.45	2.12	-75.56
74	75	93.40	-1065.96	40.89	210.01	0	-797.10	1.8	-115.63	1.8	-154.89	2.12	-64.96
75	75	93.40	-1065.96	40.88	210.05	0	-952.77	1.8	-152.56	1.8	-168.25	2.12	-41.32
75	76	94.50	-1065.96	58.15	155.55	0	-998.52	1.8	-145.34	1.8	-160.30	2.12	-24.69

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ-
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	58.18	240.33	0	-734.87	1.8	-132.47	1.8	-148.41	2.12	-53.71
76	77	95.60	-882.17	75.46	166.84	0	-796.08	1.8	-123.19	1.8	-137.79	2.12	-31.44
77	77	95.60	-882.17	75.48	166.89	0	-796.03	1.8	-123.20	1.8	-137.79	2.12	-31.46
77	78	96.70	-882.17	92.75	74.35	0	-872.76	1.8	-111.85	1.8	-124.50	2.12	-3.52
78	78	96.70	-698.39	92.80	160.98	0	-607.66	1.8	-99.05	1.8	-112.84	2.12	-33.07
78	79	97.80	-698.39	110.08	49.39	0	-699.91	1.8	-85.63	1.8	-96.87	2.12	0.53
79	79	97.80	-698.38	110.16	49.45	0	-699.86	1.8	-85.64	1.8	-96.88	2.12	0.51
79	80	98.90	-698.38	127.44	-81.24	0	-807.66	1.8	-70.14	1.8	-78.23	2.12	39.79
80	80	98.90	-441.09	127.54	45.17	0	-432.54	1.8	-52.43	1.8	-62.57	2.12	-3.03
80	81	100.00	-441.09	200.12	-105.06	0	-556.20	1.8	-34.89	1.8	-41.19	2.12	42.03
101	101	0.00	-441.09	-170.60	-105.00	0	-556.16	1.8	-34.90	1.8	-41.20	2.12	42.01
101	102	1.10	-436.66	-121.97	38.78	0	-433.61	1.8	-50.93	1.8	-61.00	2.12	-1.01
102	102	1.10	-693.96	-122.20	-87.45	0	-808.58	1.8	-68.67	1.8	-76.69	2.12	41.74
102	103	2.20	-693.96	-105.51	37.79	0	-705.35	1.8	-83.29	1.8	-94.54	2.12	4.14
103	103	2.20	-693.96	-105.71	37.89	0	-705.26	1.8	-83.30	1.8	-94.55	2.12	4.11
103	104	3.30	-693.96	-89.03	144.96	0	-616.80	1.8	-95.99	1.8	-109.86	2.12	-28.10
104	104	3.30	-877.74	-89.16	58.48	0	-881.77	1.8	-108.81	1.8	-121.53	2.12	1.40
104	105	4.40	-877.74	-72.50	147.41	0	-808.06	1.8	-119.58	1.8	-134.30	2.12	-25.42
105	105	4.40	-877.74	-72.62	147.47	0	-808.01	1.8	-119.59	1.8	-134.31	2.12	-25.44
105	106	5.50	-877.74	-55.94	218.16	0	-749.14	1.8	-128.42	1.8	-144.51	2.12	-46.86
106	106	5.50	-1061.53	-56.01	133.49	0	-1012.70	1.8	-141.31	1.8	-156.42	2.12	-17.86
106	107	6.60	-1061.53	-39.33	185.93	0	-968.69	1.8	-148.19	1.8	-164.07	2.12	-33.86
107	107	6.60	-1061.53	-39.38	185.97	0	-810.02	1.8	-111.15	1.8	-150.57	2.12	-57.79
107	108	7.70	-1061.53	-22.71	220.10	0	-785.45	1.8	-116.64	1.8	-155.92	2.12	-67.98
108	108	7.70	-1061.53	-22.74	220.14	0	-785.42	1.8	-116.65	1.8	-155.92	2.12	-67.99
108	109	8.80	-1061.53	-6.06	235.99	0	-773.21	1.8	-119.53	1.8	-158.29	2.12	-72.79
109	109	8.80	-1061.53	-6.09	235.99	0	-773.20	1.8	-119.53	1.8	-158.29	2.12	-72.79
109	110	9.90	-1061.53	10.58	233.52	0	-773.35	1.8	-119.78	1.8	-157.68	2.12	-72.19
110	110	9.90	-1061.53	10.57	233.53	0	-773.35	1.8	-119.78	1.8	-157.68	2.12	-72.19
110	111	11.00	-1061.53	27.24	212.74	0	-785.88	1.8	-117.40	1.8	-154.08	2.12	-66.19
111	111	11.00	-1061.53	27.25	212.72	0	-785.90	1.8	-117.40	1.8	-154.07	2.12	-66.18
111	112	12.10	-1061.53	43.91	173.58	0	-810.83	1.8	-112.39	1.8	-147.49	2.12	-54.77
112	112	12.10	-1061.53	43.90	173.55	0	-810.85	1.8	-112.38	1.8	-147.48	2.12	-54.76
112	113	13.20	-1061.53	60.58	116.09	0	-848.16	1.8	-104.74	1.8	-137.91	2.12	-37.94
113	113	13.20	-1061.53	60.56	116.05	0	-848.19	1.8	-104.73	1.8	-137.90	2.12	-37.93
113	114	14.30	-1061.53	77.25	40.25	0	-897.90	1.8	-94.46	1.8	-125.34	2.12	-15.70
114	114	14.30	-871.84	72.60	124.94	0	-779.91	1.8	-123.02	1.8	-129.79	2.12	-25.06
114	115	15.40	-874.66	91.78	32.08	0	-848.22	1.8	-112.23	1.8	-116.00	2.12	1.78
115	115	15.40	-1567.05	94.12	361.45	0	-829.68	1.8	-303.40	1.8	-298.70	2.12	-217.25
115	116	16.50	-1567.05	137.58	243.46	0	-925.87	1.8	-289.94	1.8	-284.77	2.12	-185.47
116	116	16.50	-1567.05	137.43	243.37	0	-936.03	1.8	-280.09	1.8	-276.22	2.12	-173.83
116	117	17.60	-1567.05	159.33	80.27	0	-1070.30	1.8	-260.53	1.8	-256.02	2.12	-128.56
117	117	17.60	-2068.15	159.10	496.56	0	-726.99	1.8	-457.24	1.8	-432.38	2.12	-392.01
117	118	18.70	-2068.15	186.58	306.15	0	-884.37	1.8	-433.89	1.8	-408.04	2.12	-338.17
118	118	18.70	-2068.15	186.37	306.15	0	-884.36	1.8	-433.90	1.8	-408.06	2.12	-338.19
118	119	19.80	-2068.15	215.54	85.41	0	-1067.72	1.8	-405.96	1.8	-378.86	2.12	-274.48
119	119	19.80	-1810.85	215.40	211.76	0	-691.65	1.8	-388.77	1.8	-363.93	2.12	-318.07
119	120	20.90	-1810.85	248.05	-44.97	0	-906.46	1.8	-354.59	1.8	-328.43	2.12	-241.96
120	120	20.90	-1810.85	247.98	-44.98	0	-906.47	1.8	-354.59	1.8	-328.43	2.12	-241.96
120	121	22.00	-1810.85	275.62	-332.12	0	-1147.04	1.8	-316.14	1.8	-288.12	2.12	-156.06
121	1121	22.00	-1847.60	-302.37	-351.27	0	-1201.63	1.8	-318.55	1.8	-290.11	2.12	-149.52
121	122	23.40	-1847.60	-267.86	46.98	0	-867.51	1.8	-371.42	1.8	-346.40	2.12	-269.23
122	122	23.40	-1847.60	-267.94	47.00	0	-867.49	1.8	-371.41	1.8	-346.40	2.12	-269.23
122	123	24.80	-1847.60	-232.66	397.19	0	-573.95	1.8	-417.72	1.8	-395.20	2.12	-373.62
123	123	24.80	-2104.90	-232.65	273.51	0	-947.93	1.8	-435.04	1.8	-410.49	2.12	-330.80
123	124	26.20	-2104.90	-192.78	568.78	0	-702.05	1.8	-472.23	1.8	-449.95	2.12	-416.62
124	124	26.20	-1420.02	-193.02	239.34	0	-779.42	1.8	-263.05	1.8	-262.45	2.12	-183.29
124	125	27.60	-1420.02	-159.10	485.35	0	-575.74	1.8	-292.77	1.8	-294.01	2.12	-253.08
125	125	27.60	-1750.84	-159.36	336.14	0	-1048.94	1.8	-315.48	1.8	-314.98	2.12	-200.84
125	126	29.00	-1750.84	-104.88	504.53	0	-910.36	1.8	-334.84	1.8	-336.00	2.12	-247.83
126	126	29.00	-1061.03	-103.63	175.18	0	-918.11	1.8	-153.26	1.8	-160.07	2.12	-38.26
126	127	30.40	-1058.64	-80.31	306.67	0	-818.28	1.8	-168.40	1.8	-179.40	2.12	-76.67
127	127	30.40	-1356.26	-83.13	179.98	0	-1051.54	1.8	-141.74	1.8	-181.45	2.12	-59.87
127	128	31.80	-1356.26	-61.87	281.46	0	-984.07	1.8	-155.75	1.8	-198.09	2.12	-89.67
128	128	31.80	-1356.26	-61.82	281.52	0	-984.03	1.8	-155.76	1.8	-198.10	2.12	-89.68
128	129	33.20	-1356.26	-40.61	353.21	0	-936.72	1.8	-165.49	1.8	-209.89	2.12	-110.69
129	129	33.20	-1356.26	-40.56	353.25	0	-936.69	1.8	-165.49	1.8	-209.89	2.12	-110.71
129	130	34.60	-1356.26	-19.04	394.95	0	-909.68	1.8	-170.90	1.8	-216.79	2.12	-122.86
130	130	34.60	-1356.26	-18.98	394.95	0	-909.67	1.8	-170.90	1.8	-216.79	2.12	-122.86
130	131	36.00	-1356.26	3.36	405.75	0	-903.71	1.8	-171.82	1.8	-218.65	2.12	-125.87
131	131	36.00	-1356.26	3.41	405.76	0	-903.70	1.8	-171.82	1.8	-218.65	2.12	-125.87
131	132	37.40	-1356.26	24.66	386.09	0	-918.42	1.8	-168.33	1.8	-215.54	2.12	-119.87
132	132	37.40	-1356.26	24.72	386.08	0	-918.43	1.8	-168.32	1.8	-215.54	2.12	-119.87
132	133	38.80	-1356.26	45.95	336.62	0	-953.29	1.8	-160.55	1.8	-207.58	2.12	-105.08
133	133	38.80	-1356.26	46.00	336.59	0	-953.31	1.8	-160.55	1.8	-207.58	2.12	-105.07

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ-
C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	67.24	257.33	0	-1008.32	1.8	-148.49	1.8	-194.76	2.12	-81.50
134	134	40.20	-1356.26	67.27	257.28	0	-1008.36	1.8	-148.49	1.8	-194.75	2.12	-81.48
134	135	41.60	-1356.26	88.54	148.21	0	-1083.53	1.8	-132.15	1.8	-177.08	2.12	-49.11
135	135	41.60	-1060.58	86.20	274.91	0	-865.15	1.8	-158.92	1.8	-175.06	2.12	-63.87
135	136	43.00	-1063.03	109.35	136.98	0	-974.71	1.8	-141.81	1.8	-154.98	2.12	-22.94
136	136	43.00	-1750.84	110.10	466.33	0	-947.95	1.8	-325.63	1.8	-327.33	2.12	-231.69
136	137	44.40	-1750.84	163.26	284.79	0	-1098.33	1.8	-304.08	1.8	-304.23	2.12	-180.39
137	137	44.40	-1420.02	163.01	433.95	0	-625.18	1.8	-281.36	1.8	-283.25	2.12	-232.61
137	138	45.80	-1420.02	196.21	183.32	0	-833.29	1.8	-250.88	1.8	-250.89	2.12	-161.16
138	138	45.80	-2104.90	195.92	512.79	0	-755.90	1.8	-460.06	1.8	-438.40	2.12	-394.51
138	139	47.20	-2104.90	231.38	214.55	0	-1004.60	1.8	-422.59	1.8	-398.55	2.12	-307.77
139	139	47.20	-1847.60	231.15	338.29	0	-630.57	1.8	-405.28	1.8	-383.27	2.12	-350.61
139	140	48.60	-1841.15	271.09	-14.70	0	-924.88	1.8	-357.22	1.8	-332.76	2.12	-244.07
140	140	48.60	-1840.98	271.01	-14.77	0	-924.88	1.8	-357.18	1.8	-332.72	2.12	-244.02
140	141	50.00	-1840.98	306.23	-418.34	0	-1264.02	1.8	-303.45	1.8	-275.54	2.12	-122.46
141	1141	50.00	-1841.18	-306.14	-418.34	0	-1264.08	1.8	-303.50	1.8	-275.58	2.12	-122.50
141	142	51.40	-1841.18	-270.92	-14.89	0	-925.04	1.8	-357.22	1.8	-332.75	2.12	-244.03
142	142	51.40	-1841.79	-271.00	-14.81	0	-925.15	1.8	-357.37	1.8	-332.89	2.12	-244.18
142	143	52.80	-1841.79	-231.56	338.14	0	-629.05	1.8	-403.81	1.8	-381.95	2.12	-349.30
143	143	52.80	-2100.09	-231.76	214.51	0	-1003.27	1.8	-421.39	1.8	-397.47	2.12	-306.71
143	144	54.20	-2104.90	-195.92	512.76	0	-755.92	1.8	-460.06	1.8	-438.39	2.12	-394.50
144	144	54.20	-1420.02	-196.22	183.31	0	-833.30	1.8	-250.88	1.8	-250.89	2.12	-161.16
144	145	55.60	-1420.02	-163.02	433.96	0	-625.17	1.8	-281.36	1.8	-283.25	2.12	-232.62
145	145	55.60	-1750.84	-163.26	284.80	0	-1098.33	1.8	-304.08	1.8	-304.23	2.12	-180.39
145	146	57.00	-1750.84	-110.10	466.33	0	-947.96	1.8	-325.63	1.8	-327.32	2.12	-231.69
146	146	57.00	-1063.03	-109.36	136.97	0	-974.72	1.8	-141.80	1.8	-154.97	2.12	-22.93
146	147	58.40	-1062.37	-87.13	275.80	0	-866.03	1.8	-159.19	1.8	-175.47	2.12	-64.20
147	147	58.40	-1358.27	-88.47	149.12	0	-1084.58	1.8	-132.45	1.8	-177.52	2.12	-49.46
147	148	59.80	-1358.27	-67.21	258.09	0	-1009.48	1.8	-148.77	1.8	-195.18	2.12	-81.80
148	148	59.80	-1358.28	-67.18	258.14	0	-1009.45	1.8	-148.78	1.8	-195.19	2.12	-81.82
148	149	61.20	-1358.28	-45.95	337.31	0	-954.50	1.8	-160.82	1.8	-207.99	2.12	-105.37
149	149	61.20	-1358.27	-45.89	337.34	0	-954.48	1.8	-160.82	1.8	-207.99	2.12	-105.38
149	150	62.60	-1358.27	-24.66	386.74	0	-919.66	1.8	-168.59	1.8	-215.94	2.12	-120.15
150	150	62.60	-1358.27	-24.60	386.76	0	-919.64	1.8	-168.59	1.8	-215.94	2.12	-120.15
150	151	64.00	-1360.02	-3.33	406.31	0	-906.43	1.8	-172.23	1.8	-219.28	2.12	-126.19
151	151	64.00	-1360.02	-3.28	406.31	0	-906.44	1.8	-172.23	1.8	-219.28	2.12	-126.19
151	152	65.40	-1360.02	19.06	395.39	0	-912.48	1.8	-171.30	1.8	-217.40	2.12	-123.14
152	152	65.40	-1360.02	19.12	395.39	0	-912.48	1.8	-171.30	1.8	-217.40	2.12	-123.14
152	153	66.80	-1360.02	40.63	353.59	0	-939.56	1.8	-165.88	1.8	-210.48	2.12	-110.96
153	153	66.80	-1360.02	40.69	353.55	0	-939.59	1.8	-165.87	1.8	-210.48	2.12	-110.95
153	154	68.20	-1360.02	61.90	281.73	0	-986.99	1.8	-156.13	1.8	-198.67	2.12	-89.90
154	154	68.20	-1360.02	61.95	281.68	0	-987.02	1.8	-156.12	1.8	-198.66	2.12	-89.89
154	155	69.60	-1360.02	83.20	180.10	0	-1054.55	1.8	-142.10	1.8	-182.01	2.12	-60.06
155	155	69.60	-1061.89	82.18	306.78	0	-820.89	1.8	-168.71	1.8	-179.88	2.12	-76.84
155	156	71.00	-1061.02	103.63	175.18	0	-918.10	1.8	-153.26	1.8	-160.07	2.12	-38.26
156	156	71.00	-1750.84	104.87	504.53	0	-910.35	1.8	-334.83	1.8	-336.00	2.12	-247.83
156	157	72.40	-1750.84	159.37	336.15	0	-1048.93	1.8	-315.48	1.8	-314.98	2.12	-200.84
157	157	72.40	-1420.02	159.10	485.35	0	-575.74	1.8	-292.77	1.8	-294.01	2.12	-253.08
157	158	73.80	-1420.02	193.02	239.34	0	-779.42	1.8	-263.05	1.8	-262.45	2.12	-183.29
158	158	73.80	-2104.90	192.79	568.77	0	-702.06	1.8	-472.23	1.8	-449.95	2.12	-416.62
158	159	75.20	-2104.90	232.65	273.49	0	-947.94	1.8	-435.04	1.8	-410.49	2.12	-330.80
159	159	75.20	-1847.60	232.65	397.19	0	-573.95	1.8	-417.72	1.8	-395.20	2.12	-373.62
159	160	76.60	-1843.78	268.41	46.50	0	-866.82	1.8	-370.39	1.8	-345.49	2.12	-268.26
160	160	76.60	-1843.83	268.35	46.37	0	-866.94	1.8	-370.39	1.8	-345.49	2.12	-268.25
160	161	78.00	-1843.83	302.86	-352.57	0	-1201.63	1.8	-317.44	1.8	-289.12	2.12	-148.35
161	1161	78.00	-1807.39	-275.77	-333.44	0	-1147.16	1.8	-315.11	1.8	-287.20	2.12	-154.96
161	162	79.10	-1807.39	-248.14	-46.16	0	-906.47	1.8	-353.58	1.8	-327.52	2.12	-240.89
162	162	79.10	-1807.77	-248.21	-46.16	0	-906.58	1.8	-353.67	1.8	-327.60	2.12	-240.97
162	163	80.20	-1807.77	-215.57	210.77	0	-691.60	1.8	-387.88	1.8	-363.12	2.12	-317.13
163	163	80.20	-2065.60	-215.70	84.44	0	-1067.80	1.8	-405.20	1.8	-378.18	2.12	-273.67
163	164	81.30	-2065.60	-186.53	305.36	0	-884.30	1.8	-433.17	1.8	-407.40	2.12	-337.42
164	164	81.30	-2066.31	-186.73	305.43	0	-884.46	1.8	-433.34	1.8	-407.55	2.12	-337.58
164	165	82.40	-2066.31	-159.25	495.99	0	-726.94	1.8	-456.71	1.8	-431.90	2.12	-391.46
165	165	82.40	-1566.09	-159.43	80.17	0	-1070.13	1.8	-260.25	1.8	-255.80	2.12	-128.33
165	166	83.50	-1566.09	-137.53	242.98	0	-936.08	1.8	-279.80	1.8	-275.96	2.12	-173.51
166	166	83.50	-1567.05	-137.61	243.18	0	-926.11	1.8	-289.90	1.8	-284.74	2.12	-185.40
166	167	84.60	-1567.05	-94.15	361.21	0	-829.88	1.8	-303.37	1.8	-298.67	2.12	-217.19
167	167	84.60	-874.65	-91.79	31.84	0	-848.38	1.8	-112.20	1.8	-115.96	2.12	1.85
167	168	85.70	-875.52	-75.07	126.03	0	-782.22	1.8	-123.49	1.8	-130.49	2.12	-25.53
168	168	85.70	-1065.96	-77.18	41.35	0	-900.83	1.8	-95.00	1.8	-126.16	2.12	-16.21
168	169	86.80	-1065.96	-60.50	117.07	0	-851.16	1.8	-105.26	1.8	-138.70	2.12	-38.42
169	169	86.80	-1065.96	-60.51	117.11	0	-851.14	1.8	-105.27	1.8	-138.71	2.12	-38.43
169	170	87.90	-1065.96	-43.83	174.50	0	-813.87	1.8	-112.90	1.8	-148.27	2.12	-55.22
170	170	87.90	-1065.96	-43.84	174.52	0	-813.86	1.8	-112.91	1.8	-148.27	2.12	-55.23
170	171	89.00	-1065.96	-27.18	213.58	0	-788.98	1.8	-117.91	1.8	-154.85	2.12	-66.62

CÁLCULO TENSIONAL

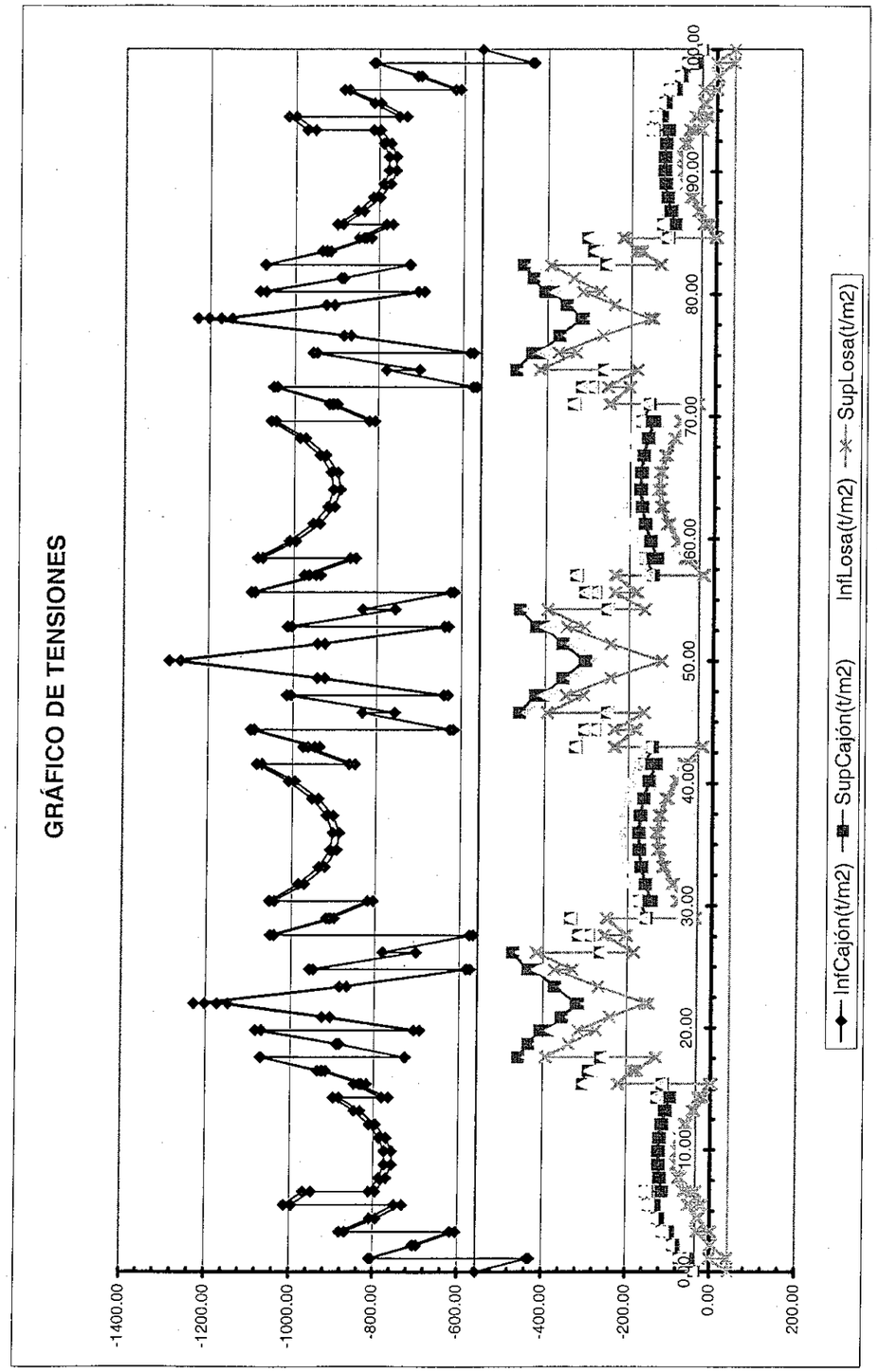
Hipótesis de cálculo:
FRECUENTESG.Tinf.MZ-

C. Frecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1065.96	-27.19	213.60	0	-788.96	1.8	-117.91	1.8	-154.85	2.12	-66.62
171	172	90.10	-1065.96	-10.50	234.30	0	-776.49	1.8	-120.28	1.8	-158.44	2.12	-72.60
172	172	90.10	-1065.96	-10.50	234.29	0	-776.50	1.8	-120.28	1.8	-158.44	2.12	-72.60
172	173	91.20	-1065.96	6.17	236.67	0	-776.40	1.8	-120.02	1.8	-159.04	2.12	-73.17
173	173	91.20	-1065.96	6.13	236.66	0	-776.41	1.8	-120.02	1.8	-159.03	2.12	-73.17
173	174	92.30	-1065.96	22.81	220.74	0	-788.68	1.8	-117.13	1.8	-156.65	2.12	-68.35
174	174	92.30	-1065.96	22.78	220.70	0	-788.70	1.8	-117.12	1.8	-156.65	2.12	-68.34
174	175	93.40	-1065.96	39.45	186.49	0	-813.33	1.8	-111.62	1.8	-151.29	2.12	-58.12
175	175	93.40	-1065.96	39.39	186.45	0	-972.56	1.8	-148.69	1.8	-164.77	2.12	-34.06
175	176	94.50	-1065.96	56.07	133.90	0	-1016.66	1.8	-141.80	1.8	-157.11	2.12	-18.04
176	176	94.50	-882.17	56.00	218.59	0	-753.09	1.8	-128.91	1.8	-145.20	2.12	-47.04
176	177	95.60	-882.17	72.68	147.81	0	-812.02	1.8	-120.08	1.8	-134.98	2.12	-25.60
177	177	95.60	-882.17	72.57	147.74	0	-812.08	1.8	-120.07	1.8	-134.97	2.12	-25.58
177	178	96.70	-882.17	89.23	58.72	0	-885.85	1.8	-109.30	1.8	-122.20	2.12	1.28
178	178	96.70	-698.39	89.09	145.23	0	-620.87	1.8	-96.48	1.8	-110.53	2.12	-28.23
178	179	97.80	-698.39	105.76	38.05	0	-709.41	1.8	-83.78	1.8	-95.21	2.12	4.01
179	179	97.80	-698.40	105.59	37.95	0	-709.50	1.8	-83.77	1.8	-95.19	2.12	4.04
179	180	98.90	-698.40	122.28	-87.38	0	-812.81	1.8	-69.14	1.8	-77.33	2.12	41.66
180	180	98.90	-441.09	122.04	38.88	0	-437.82	1.8	-51.41	1.8	-61.65	2.12	-1.10
180	181	100.00	-441.09	170.59	-105.00	0	-556.16	1.8	-34.90	1.8	-41.20	2.12	42.01



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-167.50	-85.12	0	-492.27	1.8	-30.98	1.8	-36.77	2.12	36.90
1	2	1.10	-395.79	-286.91	248.39	0	-215.54	1.8	-83.41	1.8	-88.93	2.12	-68.15
2	2	1.10	-624.09	-287.40	140.58	0	-547.87	1.8	-99.22	1.8	-102.93	2.12	-30.31
2	3	2.20	-624.09	-251.79	433.84	0	-300.47	1.8	-145.26	1.8	-148.34	2.12	-122.77
3	3	2.20	-624.08	-252.19	434.01	0	-300.32	1.8	-145.30	1.8	-148.37	2.12	-122.83
3	4	3.30	-624.08	-216.67	686.58	0	-87.01	1.8	-185.21	1.8	-187.56	2.12	-202.56
4	4	3.30	-787.15	-216.95	612.89	0	-321.81	1.8	-196.64	1.8	-197.98	2.12	-176.47
4	5	4.40	-787.15	-175.27	824.56	0	-142.76	1.8	-230.38	1.8	-230.91	2.12	-243.41
5	5	4.40	-787.15	-175.45	824.73	0	-142.61	1.8	-230.42	1.8	-230.94	2.12	-243.47
5	6	5.50	-787.15	-137.83	1002.91	0	8.56	1.8	-259.43	1.8	-258.86	2.12	-300.07
6	6	5.50	-950.22	-137.99	930.77	0	-225.04	1.8	-270.90	1.8	-269.48	2.12	-274.41
6	7	6.60	-950.22	-102.33	1068.42	0	-107.82	1.8	-293.81	1.8	-291.20	2.12	-318.33
7	7	6.60	-950.22	-102.47	1068.53	0	-25.99	1.8	-264.50	1.8	-282.02	2.12	-333.81
7	8	7.70	-950.22	-66.90	1165.54	0	49.18	1.8	-282.06	1.8	-297.95	2.12	-364.29
8	8	7.70	-950.22	-66.92	1165.62	0	49.25	1.8	-282.07	1.8	-297.96	2.12	-364.31
8	9	8.80	-950.22	-31.67	1220.90	0	93.56	1.8	-292.56	1.8	-307.02	2.12	-381.94
9	9	8.80	-950.22	-31.63	1220.94	0	93.60	1.8	-292.57	1.8	-307.03	2.12	-381.95
9	10	9.90	-950.22	3.83	1242.35	0	113.48	1.8	-297.52	1.8	-310.55	2.12	-389.29
10	10	9.90	-950.22	3.90	1242.36	0	113.49	1.8	-297.52	1.8	-310.55	2.12	-389.30
10	11	11.00	-950.22	39.59	1223.53	0	103.72	1.8	-295.69	1.8	-307.46	2.12	-384.27
11	11	11.00	-950.22	39.62	1223.54	0	103.73	1.8	-295.69	1.8	-307.46	2.12	-384.27
11	12	12.10	-950.22	75.23	1164.19	0	64.10	1.8	-287.04	1.8	-297.71	2.12	-366.79
12	12	12.10	-950.22	75.33	1164.16	0	64.06	1.8	-287.03	1.8	-297.70	2.12	-366.78
12	13	13.20	-950.22	110.63	1063.67	0	-5.94	1.8	-271.42	1.8	-281.19	2.12	-336.65
13	13	13.20	-950.22	110.69	1063.61	0	-5.99	1.8	-271.41	1.8	-281.18	2.12	-336.62
13	14	14.30	-950.22	146.36	927.25	0	-102.06	1.8	-249.87	1.8	-258.79	2.12	-295.55
14	14	14.30	-780.33	147.05	999.41	0	55.81	1.8	-272.76	1.8	-260.66	2.12	-309.44
14	15	15.40	-775.77	180.15	821.90	0	-78.40	1.8	-245.95	1.8	-232.25	2.12	-255.07
15	15	15.40	-1554.62	182.35	1193.09	0	-48.34	1.8	-458.64	1.8	-433.37	2.12	-497.81
15	16	16.50	-1554.62	185.44	982.02	0	-223.76	1.8	-429.46	1.8	-405.70	2.12	-437.48
16	16	16.50	-1554.62	185.24	981.79	0	-167.56	1.8	-484.45	1.8	-453.46	2.12	-502.41
16	17	17.60	-1554.62	200.58	765.44	0	-356.81	1.8	-445.30	1.8	-416.33	2.12	-428.81
17	17	17.60	-2163.46	200.55	1210.58	0	-33.87	1.8	-670.35	1.8	-618.10	2.12	-718.89
17	18	18.70	-2163.46	193.33	984.94	0	-229.16	1.8	-632.22	1.8	-581.02	2.12	-644.30
18	18	18.70	-2163.46	193.29	984.36	0	-229.73	1.8	-632.04	1.8	-580.87	2.12	-644.03
18	19	19.80	-2163.46	191.53	771.12	0	-410.01	1.8	-601.34	1.8	-549.38	2.12	-578.23
19	19	19.80	-1935.17	191.41	878.41	0	-77.21	1.8	-585.89	1.8	-535.96	2.12	-616.59
19	20	20.90	-1935.17	189.70	668.48	0	-251.27	1.8	-559.97	1.8	-507.77	2.12	-555.50
20	20	20.90	-1935.17	189.16	668.49	0	-251.26	1.8	-559.97	1.8	-507.77	2.12	-555.51
20	21	22.00	-1935.17	191.14	458.75	0	-421.83	1.8	-538.28	1.8	-482.14	2.12	-497.85
21	1021	22.00	-1967.78	-203.82	442.33	0	-470.24	1.8	-540.42	1.8	-483.90	2.12	-492.04
21	22	23.40	-1967.78	-190.21	723.64	0	-243.17	1.8	-566.46	1.8	-516.74	2.12	-567.42
22	22	23.40	-1967.78	-190.80	723.57	0	-243.23	1.8	-566.45	1.8	-516.73	2.12	-567.40
22	23	24.80	-1967.78	-189.43	991.42	0	-23.82	1.8	-595.33	1.8	-550.25	2.12	-642.19
23	23	24.80	-2196.07	-190.11	885.70	0	-355.52	1.8	-610.69	1.8	-563.80	2.12	-604.17
23	24	26.20	-2196.07	-221.73	1169.07	0	-116.20	1.8	-650.28	1.8	-605.22	2.12	-691.14
24	24	26.20	-1424.17	-222.72	798.72	0	-202.66	1.8	-414.38	1.8	-393.76	2.12	-428.12
24	25	27.60	-1424.17	-216.22	1102.19	0	60.99	1.8	-466.00	1.8	-444.23	2.12	-529.31
25	25	27.60	-1717.69	-216.30	975.90	0	-357.82	1.8	-486.38	1.8	-463.05	2.12	-483.33
25	26	29.00	-1717.69	-229.09	1302.85	0	-72.03	1.8	-544.56	1.8	-517.95	2.12	-593.14
26	26	29.00	-941.07	-227.74	931.86	0	-158.38	1.8	-276.20	1.8	-267.09	2.12	-282.94
26	27	30.40	-945.20	-186.93	1218.47	0	69.17	1.8	-320.91	1.8	-312.67	2.12	-372.14
27	27	30.40	-1210.45	-186.01	1110.90	0	-196.70	1.8	-300.70	1.8	-317.17	2.12	-351.44
27	28	31.80	-1210.45	-139.73	1333.48	0	-33.76	1.8	-337.67	1.8	-353.87	2.12	-419.72
28	28	31.80	-1210.45	-139.54	1333.64	0	-33.62	1.8	-337.70	1.8	-353.89	2.12	-419.78
28	29	33.20	-1210.45	-88.52	1492.77	0	82.71	1.8	-364.03	1.8	-380.17	2.12	-468.59
29	29	33.20	-1210.45	-88.31	1492.92	0	82.85	1.8	-364.06	1.8	-380.20	2.12	-468.64
29	30	34.60	-1210.45	-49.52	1590.33	0	153.99	1.8	-380.09	1.8	-396.34	2.12	-498.55
30	30	34.60	-1210.45	-49.25	1590.39	0	154.05	1.8	-380.10	1.8	-396.36	2.12	-498.58
30	31	36.00	-1210.45	-3.59	1621.32	0	176.11	1.8	-384.89	1.8	-401.57	2.12	-508.04
31	31	36.00	-1210.45	-3.39	1621.33	0	176.12	1.8	-384.89	1.8	-401.57	2.12	-508.04
31	32	37.40	-1210.45	48.10	1592.06	0	154.24	1.8	-379.68	1.8	-396.91	2.12	-499.10
32	32	37.40	-1210.45	48.35	1592.02	0	154.20	1.8	-379.67	1.8	-396.91	2.12	-499.08
32	33	38.80	-1210.45	87.14	1496.20	0	83.17	1.8	-363.21	1.8	-381.31	2.12	-469.66
33	33	38.80	-1210.45	87.38	1496.08	0	83.06	1.8	-363.18	1.8	-381.28	2.12	-469.62
33	34	40.20	-1210.45	138.44	1338.64	0	-33.07	1.8	-336.43	1.8	-355.57	2.12	-421.33
34	34	40.20	-1210.45	138.62	1338.47	0	-33.22	1.8	-336.40	1.8	-355.54	2.12	-421.27
34	35	41.60	-1210.45	184.89	1117.40	0	-196.10	1.8	-298.98	1.8	-319.38	2.12	-353.46
35	35	41.60	-946.85	186.24	1224.94	0	56.41	1.8	-319.23	1.8	-314.83	2.12	-372.25
35	36	43.00	-942.63	227.57	938.53	0	-174.32	1.8	-274.08	1.8	-269.62	2.12	-282.87
36	36	43.00	-1717.69	228.51	1309.55	0	-64.19	1.8	-550.78	1.8	-522.61	2.12	-599.68
36	37	44.40	-1717.69	223.84	984.43	0	-349.10	1.8	-492.62	1.8	-467.62	2.12	-489.90
37	37	44.40	-1424.17	223.84	1110.81	0	69.81	1.8	-472.27	1.8	-448.83	2.12	-535.92
37	38	45.80	-1424.17	233.92	791.28	0	-209.31	1.8	-416.60	1.8	-394.70	2.12	-428.00
38	38	45.80	-2196.07	233.48	1161.51	0	-122.97	1.8	-652.46	1.8	-606.13	2.12	-690.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	210.42	854.24	0	-385.33	1.8	-606.54	1.8	-559.07	2.12	-593.76
39	39	47.20	-1967.78	210.61	959.43	0	-54.15	1.8	-591.03	1.8	-545.38	2.12	-631.54
39	40	48.60	-1974.23	203.81	668.17	0	-298.05	1.8	-557.47	1.8	-507.70	2.12	-548.04
40	40	48.60	-1974.41	203.21	668.28	0	-298.00	1.8	-557.53	1.8	-507.75	2.12	-548.11
40	41	50.00	-1974.41	215.76	368.56	0	-542.90	1.8	-526.64	1.8	-470.56	2.12	-464.83
41	1041	50.00	-1974.19	-215.85	368.57	0	-542.84	1.8	-526.59	1.8	-470.52	2.12	-464.79
41	42	51.40	-1974.19	-203.30	668.39	0	-297.85	1.8	-557.49	1.8	-507.72	2.12	-548.09
42	42	51.40	-1973.59	-203.89	668.30	0	-297.76	1.8	-557.33	1.8	-507.57	2.12	-547.94
42	43	52.80	-1973.59	-210.19	959.57	0	-55.68	1.8	-592.50	1.8	-546.70	2.12	-632.85
43	43	52.80	-2200.88	-210.05	854.27	0	-386.68	1.8	-607.75	1.8	-560.15	2.12	-594.82
43	44	54.20	-2196.07	-233.48	1161.52	0	-122.96	1.8	-652.46	1.8	-606.13	2.12	-690.97
44	44	54.20	-1424.17	-233.92	791.28	0	-209.31	1.8	-416.60	1.8	-394.70	2.12	-428.00
44	45	55.60	-1424.17	-223.85	1110.84	0	69.83	1.8	-472.28	1.8	-448.83	2.12	-535.93
45	45	55.60	-1717.69	-223.83	984.47	0	-349.07	1.8	-492.63	1.8	-467.62	2.12	-489.91
45	46	57.00	-1717.69	-228.50	1309.56	0	-64.19	1.8	-550.78	1.8	-522.62	2.12	-599.68
46	46	57.00	-942.63	-227.57	938.56	0	-174.30	1.8	-274.09	1.8	-269.62	2.12	-282.88
46	47	58.40	-945.05	-185.32	1224.06	0	57.32	1.8	-318.96	1.8	-314.43	2.12	-371.92
47	47	58.40	-1208.44	-184.95	1116.52	0	-195.02	1.8	-298.69	1.8	-318.95	2.12	-353.12
47	48	59.80	-1208.44	-138.68	1337.70	0	-32.06	1.8	-336.12	1.8	-355.13	2.12	-420.96
48	48	59.80	-1208.43	-138.49	1337.87	0	-31.91	1.8	-336.16	1.8	-355.15	2.12	-421.02
48	49	61.20	-1208.43	-87.43	1495.34	0	84.24	1.8	-362.90	1.8	-380.87	2.12	-469.32
49	49	61.20	-1208.44	-87.19	1495.46	0	84.34	1.8	-362.93	1.8	-380.89	2.12	-469.36
49	50	62.60	-1208.44	-48.41	1591.37	0	155.43	1.8	-379.41	1.8	-396.51	2.12	-498.81
50	50	62.60	-1208.44	-48.15	1591.44	0	155.49	1.8	-379.42	1.8	-396.52	2.12	-498.83
50	51	64.00	-1206.69	3.30	1620.76	0	178.84	1.8	-384.48	1.8	-400.94	2.12	-507.72
51	51	64.00	-1206.69	3.52	1620.77	0	178.84	1.8	-384.48	1.8	-400.94	2.12	-507.72
51	52	65.40	-1206.69	49.16	1589.95	0	156.85	1.8	-379.70	1.8	-395.75	2.12	-498.29
52	52	65.40	-1206.69	49.42	1589.86	0	156.78	1.8	-379.68	1.8	-395.73	2.12	-498.26
52	53	66.80	-1206.69	88.23	1492.62	0	85.75	1.8	-363.68	1.8	-379.61	2.12	-468.40
53	53	66.80	-1206.69	88.44	1492.47	0	85.61	1.8	-363.65	1.8	-379.58	2.12	-468.35
53	54	68.20	-1206.69	139.46	1333.47	0	-30.64	1.8	-337.34	1.8	-353.33	2.12	-419.57
54	54	68.20	-1206.69	139.65	1333.31	0	-30.78	1.8	-337.31	1.8	-353.30	2.12	-419.52
54	55	69.60	-1206.69	185.93	1110.79	0	-193.68	1.8	-300.34	1.8	-316.62	2.12	-351.26
55	55	69.60	-941.94	185.06	1218.38	0	71.79	1.8	-320.60	1.8	-312.19	2.12	-371.98
55	56	71.00	-941.07	227.76	931.88	0	-158.36	1.8	-276.21	1.8	-267.09	2.12	-282.94
56	56	71.00	-1717.69	229.09	1302.87	0	-72.01	1.8	-544.56	1.8	-517.95	2.12	-593.15
56	57	72.40	-1717.69	216.30	975.93	0	-357.80	1.8	-486.38	1.8	-463.05	2.12	-483.34
57	57	72.40	-1424.17	216.22	1102.19	0	61.00	1.8	-466.00	1.8	-444.23	2.12	-529.31
57	58	73.80	-1424.17	222.70	798.69	0	-202.68	1.8	-414.37	1.8	-393.76	2.12	-428.11
58	58	73.80	-2196.08	221.73	1169.05	0	-116.22	1.8	-650.27	1.8	-605.22	2.12	-691.14
58	59	75.20	-2196.08	190.14	885.70	0	-355.52	1.8	-610.69	1.8	-563.80	2.12	-604.17
59	59	75.20	-1967.78	189.42	991.41	0	-23.83	1.8	-595.33	1.8	-550.25	2.12	-642.18
59	60	76.60	-1971.61	190.33	724.08	0	-243.89	1.8	-567.47	1.8	-517.64	2.12	-568.37
60	60	76.60	-1971.55	189.72	724.22	0	-243.75	1.8	-567.48	1.8	-517.65	2.12	-568.40
60	61	78.00	-1971.55	203.32	443.63	0	-470.23	1.8	-541.53	1.8	-484.89	2.12	-493.22
61	1061	78.00	-1938.62	-190.99	460.08	0	-421.70	1.8	-539.31	1.8	-483.06	2.12	-498.96
61	62	79.10	-1938.62	-189.01	669.65	0	-251.28	1.8	-560.98	1.8	-508.67	2.12	-556.57
62	62	79.10	-1938.24	-189.54	669.63	0	-251.19	1.8	-560.88	1.8	-508.58	2.12	-556.48
62	63	80.20	-1938.24	-191.26	879.38	0	-77.28	1.8	-586.78	1.8	-536.76	2.12	-617.52
63	63	80.20	-2165.99	-191.37	772.07	0	-409.94	1.8	-602.10	1.8	-550.06	2.12	-579.04
63	64	81.30	-2165.99	-193.13	985.15	0	-229.80	1.8	-632.78	1.8	-581.53	2.12	-644.80
64	64	81.30	-2165.29	-193.18	985.66	0	-229.08	1.8	-632.77	1.8	-581.52	2.12	-644.90
64	65	82.40	-2165.29	-200.40	1211.14	0	-33.92	1.8	-670.88	1.8	-618.57	2.12	-719.44
65	65	82.40	-1555.58	-200.49	766.23	0	-356.45	1.8	-445.61	1.8	-416.64	2.12	-429.24
65	66	83.50	-1555.58	-185.14	982.15	0	-167.53	1.8	-484.73	1.8	-453.72	2.12	-502.72
66	66	83.50	-1554.62	-185.43	982.29	0	-223.53	1.8	-429.49	1.8	-405.73	2.12	-437.56
66	67	84.60	-1554.62	-182.34	1193.34	0	-48.13	1.8	-458.67	1.8	-433.40	2.12	-497.88
67	67	84.60	-775.78	-180.14	822.18	0	-78.21	1.8	-245.99	1.8	-232.30	2.12	-255.16
67	68	85.70	-776.65	-144.57	998.34	0	58.14	1.8	-272.29	1.8	-259.96	2.12	-308.98
68	68	85.70	-945.78	-146.45	926.15	0	-99.13	1.8	-249.33	1.8	-257.97	2.12	-295.04
68	69	86.80	-945.78	-110.78	1062.61	0	-3.00	1.8	-270.88	1.8	-280.38	2.12	-336.15
69	69	86.80	-945.79	-110.73	1062.69	0	-2.93	1.8	-270.90	1.8	-280.39	2.12	-336.18
69	70	87.90	-945.79	-75.41	1163.23	0	67.10	1.8	-286.51	1.8	-296.92	2.12	-366.33
70	70	87.90	-945.79	-75.31	1163.28	0	67.15	1.8	-286.52	1.8	-296.93	2.12	-366.34
70	71	89.00	-945.79	-39.73	1222.69	0	106.82	1.8	-295.19	1.8	-306.69	2.12	-383.84
71	71	89.00	-945.79	-39.69	1222.71	0	106.84	1.8	-295.19	1.8	-306.69	2.12	-383.85
71	72	90.10	-945.79	-3.99	1241.64	0	116.66	1.8	-297.03	1.8	-309.80	2.12	-388.90
72	72	90.10	-945.79	-3.93	1241.60	0	116.64	1.8	-297.02	1.8	-309.79	2.12	-388.89
72	73	91.20	-945.79	31.53	1220.30	0	96.83	1.8	-292.08	1.8	-306.29	2.12	-381.58
73	73	91.20	-945.79	31.57	1220.25	0	96.79	1.8	-292.07	1.8	-306.28	2.12	-381.57
73	74	92.30	-945.79	66.83	1165.06	0	52.53	1.8	-281.60	1.8	-297.24	2.12	-363.97
74	74	92.30	-945.79	66.79	1164.98	0	52.46	1.8	-281.58	1.8	-297.22	2.12	-363.94
74	75	93.40	-945.79	102.38	1068.05	0	-22.66	1.8	-264.04	1.8	-281.31	2.12	-333.48
75	75	93.40	-945.79	102.24	1067.93	0	-103.93	1.8	-293.31	1.8	-290.50	2.12	-318.14
75	76	94.50	-945.79	137.90	930.36	0	-221.09	1.8	-270.41	1.8	-268.79	2.12	-274.23

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+
C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	137.75	1002.50	0	12.52	1.8	-258.94	1.8	-258.17	2.12	-299.90
76	77	95.60	-782.72	175.37	824.42	0	-138.58	1.8	-229.93	1.8	-230.27	2.12	-243.32
77	77	95.60	-782.72	175.17	824.26	0	-138.72	1.8	-229.90	1.8	-230.24	2.12	-243.27
77	78	96.70	-782.72	216.86	612.62	0	-317.75	1.8	-196.15	1.8	-197.31	2.12	-176.33
78	78	96.70	-619.65	216.58	686.35	0	-82.91	1.8	-184.73	1.8	-186.90	2.12	-202.44
78	79	97.80	-619.65	252.10	433.82	0	-296.20	1.8	-144.81	1.8	-147.71	2.12	-122.72
79	79	97.80	-619.65	251.71	433.66	0	-296.34	1.8	-144.78	1.8	-147.68	2.12	-122.66
79	80	98.90	-619.65	287.31	140.49	0	-543.66	1.8	-98.74	1.8	-102.28	2.12	-30.23
80	80	98.90	-391.36	286.82	248.30	0	-211.33	1.8	-82.94	1.8	-88.29	2.12	-68.06
80	81	100.00	-391.36	167.49	-85.12	0	-492.27	1.8	-30.98	1.8	-36.77	2.12	36.90
101	101	0.00	-391.36	-180.37	-85.22	0	-492.36	1.8	-30.96	1.8	-36.75	2.12	36.94
101	102	1.10	-395.79	-308.48	272.51	0	-194.42	1.8	-88.44	1.8	-93.24	2.12	-76.43
102	102	1.10	-624.09	-307.28	164.09	0	-527.29	1.8	-104.12	1.8	-107.12	2.12	-38.38
102	103	2.20	-624.09	-269.92	477.42	0	-262.32	1.8	-154.35	1.8	-156.12	2.12	-137.73
103	103	2.20	-624.08	-268.89	477.04	0	-262.65	1.8	-154.27	1.8	-156.05	2.12	-137.60
103	104	3.30	-624.08	-231.65	745.76	0	-35.19	1.8	-197.55	1.8	-198.12	2.12	-222.88
104	104	3.30	-787.15	-230.75	671.52	0	-270.47	1.8	-208.86	1.8	-208.45	2.12	-196.60
104	105	4.40	-787.15	-193.39	896.43	0	-79.83	1.8	-245.36	1.8	-243.74	2.12	-268.09
105	105	4.40	-787.15	-192.70	896.08	0	-80.14	1.8	-245.29	1.8	-243.68	2.12	-267.97
105	106	5.50	-787.15	-145.58	1085.05	0	80.46	1.8	-276.53	1.8	-273.50	2.12	-328.25
106	106	5.50	-950.22	-145.07	1012.51	0	-153.49	1.8	-287.92	1.8	-284.05	2.12	-302.45
106	107	6.60	-950.22	-107.68	1157.95	0	-29.46	1.8	-312.43	1.8	-307.15	2.12	-349.04
107	107	6.60	-950.22	-107.23	1157.75	0	52.58	1.8	-283.00	1.8	-297.87	2.12	-364.43
107	108	7.70	-950.22	-69.95	1259.67	0	131.96	1.8	-301.54	1.8	-314.65	2.12	-396.55
108	108	7.70	-950.22	-69.57	1259.56	0	131.86	1.8	-301.52	1.8	-314.63	2.12	-396.52
108	109	8.80	-950.22	-32.30	1318.03	0	178.77	1.8	-312.63	1.8	-324.23	2.12	-415.18
109	109	8.80	-950.22	-32.02	1317.97	0	178.72	1.8	-312.62	1.8	-324.22	2.12	-415.16
109	110	9.90	-950.22	5.28	1339.48	0	198.48	1.8	-317.55	1.8	-327.73	2.12	-422.47
110	110	9.90	-950.22	5.54	1339.44	0	198.44	1.8	-317.54	1.8	-327.72	2.12	-422.46
110	111	11.00	-950.22	42.94	1318.78	0	186.77	1.8	-315.28	1.8	-324.27	2.12	-416.73
111	111	11.00	-950.22	43.18	1318.80	0	186.79	1.8	-315.28	1.8	-324.27	2.12	-416.73
111	112	12.10	-950.22	80.49	1255.29	0	143.15	1.8	-305.69	1.8	-313.74	2.12	-397.73
112	112	12.10	-950.22	80.73	1255.36	0	143.22	1.8	-305.71	1.8	-313.75	2.12	-397.76
112	113	13.20	-950.22	117.92	1148.99	0	67.58	1.8	-288.79	1.8	-296.13	2.12	-365.48
113	113	13.20	-950.22	118.13	1149.09	0	67.68	1.8	-288.82	1.8	-296.15	2.12	-365.52
113	114	14.30	-950.22	155.47	1004.27	0	-36.35	1.8	-265.43	1.8	-272.20	2.12	-321.40
114	114	14.30	-780.33	156.36	1076.72	0	123.07	1.8	-288.35	1.8	-274.10	2.12	-335.56
114	115	15.40	-775.77	191.06	888.96	0	-20.23	1.8	-259.28	1.8	-243.76	2.12	-277.57
115	115	15.40	-1554.62	193.47	1260.46	0	10.12	1.8	-472.05	1.8	-444.98	2.12	-520.45
115	116	16.50	-1554.62	203.41	1037.15	0	-176.27	1.8	-439.80	1.8	-414.69	2.12	-455.40
116	116	16.50	-1554.62	203.98	1037.42	0	-113.68	1.8	-500.70	1.8	-467.57	2.12	-527.35
116	117	17.60	-1554.62	220.48	800.15	0	-324.27	1.8	-454.18	1.8	-424.07	2.12	-442.98
117	117	17.60	-2163.46	221.00	1245.82	0	-0.80	1.8	-679.40	1.8	-625.98	2.12	-733.31
117	118	18.70	-2163.46	201.40	1004.45	0	-212.54	1.8	-635.23	1.8	-583.69	2.12	-650.08
118	118	18.70	-2163.46	201.75	1004.18	0	-212.80	1.8	-635.16	1.8	-583.63	2.12	-649.97
118	119	19.80	-2163.46	188.77	787.89	0	-397.43	1.8	-601.92	1.8	-549.98	2.12	-580.98
119	119	19.80	-1935.17	188.63	895.63	0	-64.18	1.8	-586.61	1.8	-536.68	2.12	-619.55
119	120	20.90	-1935.17	177.22	694.13	0	-231.64	1.8	-561.30	1.8	-509.05	2.12	-560.20
120	120	20.90	-1935.17	176.72	694.13	0	-231.64	1.8	-561.30	1.8	-509.05	2.12	-560.20
120	121	22.00	-1935.17	184.68	491.75	0	-396.81	1.8	-539.72	1.8	-483.56	2.12	-503.59
121	1121	22.00	-1967.78	-197.96	475.35	0	-445.21	1.8	-541.85	1.8	-485.32	2.12	-497.79
121	122	23.40	-1967.78	-188.07	749.40	0	-223.02	1.8	-568.31	1.8	-518.47	2.12	-572.71
122	122	23.40	-1967.78	-188.69	749.43	0	-222.99	1.8	-568.32	1.8	-518.47	2.12	-572.72
122	123	24.80	-1967.78	-189.02	1016.48	0	-2.49	1.8	-599.17	1.8	-553.66	2.12	-649.58
123	123	24.80	-2196.07	-189.94	910.57	0	-334.39	1.8	-614.45	1.8	-567.15	2.12	-611.46
123	124	26.20	-2196.07	-233.01	1197.40	0	-90.12	1.8	-656.94	1.8	-611.05	2.12	-702.07
124	124	26.20	-1424.17	-232.60	826.50	0	-177.14	1.8	-420.86	1.8	-399.43	2.12	-438.77
124	125	27.60	-1424.17	-228.76	1146.42	0	103.79	1.8	-478.87	1.8	-455.41	2.12	-549.09
125	125	27.60	-1717.69	-228.05	1019.49	0	-315.67	1.8	-499.04	1.8	-474.04	2.12	-502.80
125	126	29.00	-1717.69	-240.61	1356.99	0	-17.62	1.8	-562.70	1.8	-533.66	2.12	-619.98
126	126	29.00	-941.08	-239.19	985.45	0	-111.79	1.8	-286.97	1.8	-276.37	2.12	-301.01
126	127	30.40	-945.21	-195.75	1285.19	0	127.35	1.8	-334.54	1.8	-324.38	2.12	-394.83
127	127	30.40	-1210.45	-194.87	1177.14	0	-139.45	1.8	-314.22	1.8	-328.80	2.12	-373.87
127	128	31.80	-1210.45	-146.22	1409.39	0	32.46	1.8	-353.28	1.8	-367.27	2.12	-445.60
128	128	31.80	-1210.45	-146.22	1409.18	0	32.29	1.8	-353.24	1.8	-367.23	2.12	-445.53
128	129	33.20	-1210.45	-91.80	1575.22	0	155.02	1.8	-381.06	1.8	-394.77	2.12	-496.80
129	129	33.20	-1210.45	-91.90	1575.07	0	154.89	1.8	-381.03	1.8	-394.75	2.12	-496.75
129	130	34.60	-1210.45	-52.23	1677.07	0	230.24	1.8	-398.04	1.8	-411.73	2.12	-528.28
130	130	34.60	-1210.45	-52.35	1677.00	0	230.18	1.8	-398.02	1.8	-411.72	2.12	-528.26
130	131	36.00	-1210.45	-4.24	1709.16	0	253.38	1.8	-403.08	1.8	-417.16	2.12	-538.16
131	131	36.00	-1210.45	-4.38	1709.14	0	253.37	1.8	-403.08	1.8	-417.16	2.12	-538.15
131	132	37.40	-1210.45	50.80	1679.22	0	230.79	1.8	-397.71	1.8	-412.37	2.12	-528.95
132	132	37.40	-1210.45	50.66	1679.28	0	230.84	1.8	-397.72	1.8	-412.38	2.12	-528.97
132	133	38.80	-1210.45	90.30	1579.41	0	156.03	1.8	-380.37	1.8	-396.03	2.12	-498.10
133	133	38.80	-1210.45	90.20	1579.57	0	156.17	1.8	-380.41	1.8	-396.06	2.12	-498.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+
C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	144.64	1415.92	0	34.18	1.8	-352.30	1.8	-369.19	2.12	-447.63
134	134	40.20	-1210.45	144.62	1416.11	0	34.35	1.8	-352.34	1.8	-369.23	2.12	-447.69
134	135	41.60	-1210.45	193.20	1186.05	0	-136.98	1.8	-312.95	1.8	-331.40	2.12	-376.65
135	135	41.60	-946.85	194.52	1294.11	0	116.69	1.8	-333.30	1.8	-326.93	2.12	-395.72
135	136	43.00	-942.63	238.24	995.50	0	-124.85	1.8	-285.46	1.8	-279.44	2.12	-302.03
136	136	43.00	-1717.69	239.18	1367.05	0	-6.71	1.8	-569.70	1.8	-539.00	2.12	-627.80
136	137	44.40	-1717.69	237.04	1030.13	0	-305.03	1.8	-505.76	1.8	-479.03	2.12	-510.15
137	137	44.40	-1424.16	237.63	1157.16	0	114.54	1.8	-485.62	1.8	-460.43	2.12	-556.49
137	138	45.80	-1424.16	244.79	820.82	0	-182.22	1.8	-423.43	1.8	-400.67	2.12	-439.25
138	138	45.80	-2196.07	245.49	1191.64	0	-95.29	1.8	-659.49	1.8	-612.26	2.12	-702.51
138	139	47.20	-2196.07	209.67	879.49	0	-364.01	1.8	-610.21	1.8	-562.33	2.12	-601.00
139	139	47.20	-1967.78	209.90	985.07	0	-32.43	1.8	-594.84	1.8	-548.77	2.12	-638.97
139	140	48.60	-1974.23	201.12	697.88	0	-274.29	1.8	-560.22	1.8	-510.21	2.12	-554.82
140	140	48.60	-1974.41	200.47	697.95	0	-274.27	1.8	-560.28	1.8	-510.26	2.12	-554.88
140	141	50.00	-1974.41	209.17	406.22	0	-513.62	1.8	-529.14	1.8	-472.92	2.12	-472.34
141	1141	50.00	-1974.19	-209.25	406.23	0	-513.55	1.8	-529.09	1.8	-472.87	2.12	-472.29
141	142	51.40	-1974.19	-200.55	698.06	0	-274.12	1.8	-560.23	1.8	-510.23	2.12	-554.86
142	142	51.40	-1973.59	-201.21	698.01	0	-274.00	1.8	-560.07	1.8	-510.08	2.12	-554.71
142	143	52.80	-1973.59	-209.49	985.20	0	-33.97	1.8	-596.30	1.8	-550.08	2.12	-640.28
143	143	52.80	-2200.88	-209.31	879.53	0	-365.34	1.8	-611.42	1.8	-563.42	2.12	-602.06
143	144	54.20	-2196.07	-245.49	1191.63	0	-95.31	1.8	-659.49	1.8	-612.26	2.12	-702.51
144	144	54.20	-1424.17	-244.81	820.81	0	-182.23	1.8	-423.43	1.8	-400.67	2.12	-439.25
144	145	55.60	-1424.17	-237.64	1157.18	0	114.56	1.8	-485.63	1.8	-460.43	2.12	-556.50
145	145	55.60	-1717.69	-237.06	1030.15	0	-305.01	1.8	-505.77	1.8	-479.04	2.12	-510.16
145	146	57.00	-1717.69	-239.18	1367.09	0	-6.67	1.8	-569.72	1.8	-539.02	2.12	-627.83
146	146	57.00	-942.63	-238.27	995.54	0	-124.82	1.8	-285.47	1.8	-279.45	2.12	-302.05
146	147	58.40	-945.05	-193.64	1293.26	0	117.62	1.8	-333.04	1.8	-326.54	2.12	-395.40
147	147	58.40	-1208.44	-193.29	1185.20	0	-135.88	1.8	-312.66	1.8	-330.97	2.12	-376.32
147	148	59.80	-1208.44	-144.69	1415.33	0	35.50	1.8	-352.06	1.8	-368.81	2.12	-447.38
148	148	59.80	-1208.45	-144.71	1415.15	0	35.34	1.8	-352.02	1.8	-368.78	2.12	-447.32
148	149	61.20	-1208.45	-90.27	1578.84	0	157.35	1.8	-380.14	1.8	-395.65	2.12	-497.86
149	149	61.20	-1208.44	-90.36	1578.71	0	157.23	1.8	-380.11	1.8	-395.63	2.12	-497.81
149	150	62.60	-1208.44	-50.72	1678.70	0	232.13	1.8	-397.47	1.8	-412.00	2.12	-528.72
150	150	62.60	-1208.44	-50.86	1678.65	0	232.08	1.8	-397.46	1.8	-411.99	2.12	-528.70
150	151	64.00	-1206.69	4.30	1708.63	0	256.13	1.8	-402.67	1.8	-416.54	2.12	-537.85
151	151	64.00	-1206.69	4.16	1708.63	0	256.14	1.8	-402.68	1.8	-416.54	2.12	-537.85
151	152	65.40	-1206.69	52.27	1676.58	0	233.00	1.8	-397.63	1.8	-411.12	2.12	-527.98
152	152	65.40	-1206.69	52.14	1676.65	0	233.06	1.8	-397.64	1.8	-411.13	2.12	-528.01
152	153	66.80	-1206.69	91.80	1574.79	0	157.81	1.8	-380.66	1.8	-394.17	2.12	-496.51
153	153	66.80	-1206.69	91.73	1574.94	0	157.94	1.8	-380.69	1.8	-394.19	2.12	-496.57
153	154	68.20	-1206.69	146.14	1409.00	0	35.26	1.8	-352.88	1.8	-366.67	2.12	-445.32
154	154	68.20	-1206.69	146.14	1409.18	0	35.42	1.8	-352.91	1.8	-366.70	2.12	-445.38
154	155	69.60	-1206.69	194.77	1177.06	0	-136.41	1.8	-313.87	1.8	-328.25	2.12	-373.70
155	155	69.60	-941.94	193.87	1285.13	0	130.00	1.8	-334.24	1.8	-323.91	2.12	-394.67
155	156	71.00	-941.07	239.19	985.49	0	-111.76	1.8	-286.97	1.8	-276.38	2.12	-301.02
156	156	71.00	-1717.69	240.62	1357.03	0	-17.59	1.8	-562.71	1.8	-533.66	2.12	-620.00
156	157	72.40	-1717.69	228.06	1019.51	0	-315.65	1.8	-499.04	1.8	-474.05	2.12	-502.81
157	157	72.40	-1424.17	228.76	1146.42	0	103.79	1.8	-478.87	1.8	-455.41	2.12	-549.09
157	158	73.80	-1424.17	232.60	826.49	0	-177.15	1.8	-420.86	1.8	-399.43	2.12	-438.77
158	158	73.80	-2196.07	233.02	1197.39	0	-90.14	1.8	-656.94	1.8	-611.04	2.12	-702.06
158	159	75.20	-2196.07	189.94	910.55	0	-334.41	1.8	-614.45	1.8	-567.14	2.12	-611.45
159	159	75.20	-1967.78	189.01	1016.49	0	-2.48	1.8	-599.17	1.8	-553.66	2.12	-649.59
159	160	76.60	-1971.61	188.23	749.96	0	-223.64	1.8	-569.34	1.8	-519.39	2.12	-573.70
160	160	76.60	-1971.55	187.57	750.00	0	-223.58	1.8	-569.33	1.8	-519.38	2.12	-573.70
160	161	78.00	-1971.55	197.47	476.65	0	-445.19	1.8	-542.96	1.8	-486.32	2.12	-498.96
161	1161	78.00	-1938.62	-184.53	493.08	0	-396.68	1.8	-540.75	1.8	-484.48	2.12	-504.70
161	162	79.10	-1938.62	-176.58	695.28	0	-231.66	1.8	-562.31	1.8	-509.96	2.12	-561.26
162	162	79.10	-1938.23	-177.06	695.24	0	-231.59	1.8	-562.20	1.8	-509.86	2.12	-561.16
162	163	80.20	-1938.23	-188.49	896.61	0	-64.24	1.8	-587.50	1.8	-537.48	2.12	-620.49
163	163	80.20	-2165.99	-188.62	788.83	0	-397.36	1.8	-602.67	1.8	-550.65	2.12	-581.78
163	164	81.30	-2165.99	-201.59	1004.98	0	-212.85	1.8	-635.89	1.8	-584.29	2.12	-650.74
164	164	81.30	-2165.29	-201.26	1005.18	0	-212.46	1.8	-635.78	1.8	-584.19	2.12	-650.68
164	165	82.40	-2165.29	-220.85	1246.38	0	-0.84	1.8	-679.93	1.8	-626.46	2.12	-733.86
165	165	82.40	-1555.58	-220.38	800.97	0	-323.87	1.8	-454.50	1.8	-424.39	2.12	-443.42
165	166	83.50	-1555.58	-203.89	1037.79	0	-113.64	1.8	-500.99	1.8	-467.83	2.12	-527.67
166	166	83.50	-1554.62	-203.41	1037.43	0	-176.03	1.8	-439.84	1.8	-414.72	2.12	-455.48
166	167	84.60	-1554.62	-193.47	1260.74	0	10.35	1.8	-472.09	1.8	-445.01	2.12	-520.53
167	167	84.60	-775.78	-191.04	889.24	0	-20.05	1.8	-259.31	1.8	-243.81	2.12	-277.65
167	168	85.70	-776.65	-153.89	1075.63	0	125.38	1.8	-287.88	1.8	-273.39	2.12	-335.09
168	168	85.70	-945.79	-155.54	1003.18	0	-33.41	1.8	-264.89	1.8	-271.38	2.12	-320.90
168	169	86.80	-945.79	-118.20	1148.12	0	70.69	1.8	-288.29	1.8	-295.36	2.12	-365.05
169	169	86.80	-945.79	-118.01	1147.96	0	70.55	1.8	-288.26	1.8	-295.33	2.12	-364.99
169	170	87.90	-945.79	-80.83	1254.45	0	146.27	1.8	-305.19	1.8	-312.97	2.12	-397.31
170	170	87.90	-945.79	-80.57	1254.37	0	146.19	1.8	-305.18	1.8	-312.95	2.12	-397.28
170	171	89.00	-945.79	-43.27	1317.97	0	189.90	1.8	-314.78	1.8	-323.51	2.12	-416.31

CÁLCULO TENSIONAL

Hipótesis de cálculo:

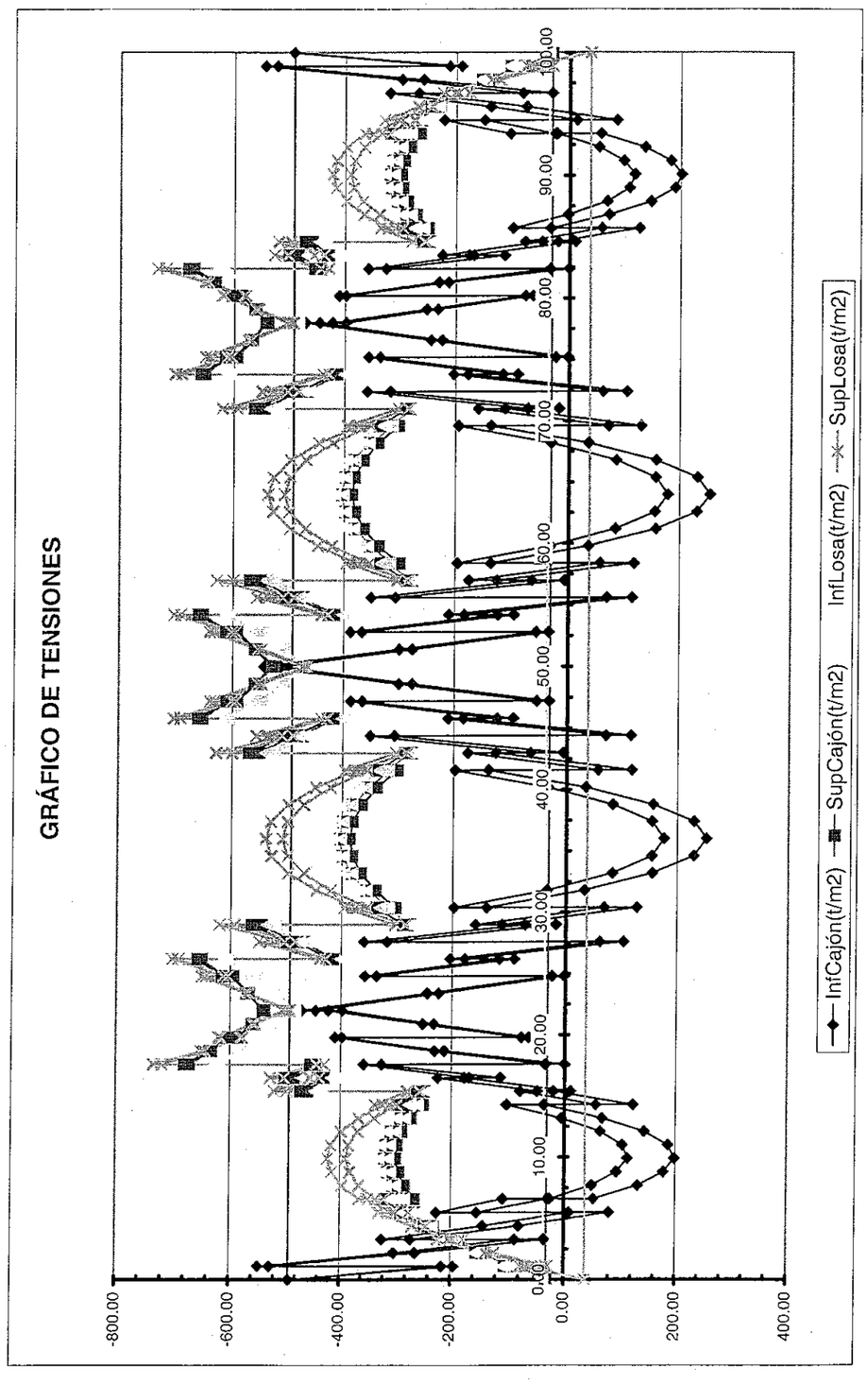
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-43.06	1317.94	0	189.87	1.8	-314.77	1.8	-323.50	2.12	-416.30
171	172	90.10	-945.79	-5.63	1338.68	0	201.59	1.8	-317.04	1.8	-326.97	2.12	-422.06
172	172	90.10	-945.79	-5.39	1338.71	0	201.61	1.8	-317.05	1.8	-326.97	2.12	-422.07
172	173	91.20	-945.79	31.92	1317.29	0	181.92	1.8	-312.13	1.8	-323.47	2.12	-414.78
173	173	91.20	-945.79	32.19	1317.36	0	181.98	1.8	-312.14	1.8	-323.48	2.12	-414.80
173	174	92.30	-945.79	69.46	1258.99	0	135.14	1.8	-301.05	1.8	-313.90	2.12	-396.17
174	174	92.30	-945.79	69.87	1259.11	0	135.24	1.8	-301.07	1.8	-313.93	2.12	-396.21
174	175	93.40	-945.79	107.15	1157.27	0	55.92	1.8	-282.53	1.8	-297.16	2.12	-364.10
175	175	93.40	-945.79	107.60	1157.46	0	-25.57	1.8	-311.93	1.8	-306.45	2.12	-348.84
175	176	94.50	-945.79	144.99	1012.10	0	-149.53	1.8	-287.43	1.8	-283.37	2.12	-302.28
176	176	94.50	-782.72	145.48	1084.65	0	84.43	1.8	-276.04	1.8	-272.82	2.12	-328.08
176	177	95.60	-782.72	192.60	895.76	0	-76.11	1.8	-244.81	1.8	-243.00	2.12	-267.82
177	177	95.60	-782.72	193.29	896.09	0	-75.82	1.8	-244.87	1.8	-243.06	2.12	-267.93
177	178	96.70	-782.72	230.66	671.27	0	-266.38	1.8	-208.38	1.8	-207.78	2.12	-196.47
178	178	96.70	-619.65	231.54	745.52	0	-31.09	1.8	-197.07	1.8	-197.46	2.12	-222.76
178	179	97.80	-619.65	268.79	476.85	0	-258.52	1.8	-153.78	1.8	-155.39	2.12	-137.49
179	179	97.80	-619.66	269.82	477.24	0	-258.17	1.8	-153.87	1.8	-155.46	2.12	-137.63
179	180	98.90	-619.66	307.20	164.00	0	-523.07	1.8	-103.65	1.8	-106.48	2.12	-38.30
180	180	98.90	-391.36	308.38	272.42	0	-190.21	1.8	-87.96	1.8	-92.59	2.12	-76.34
180	181	100.00	-391.36	180.36	-85.22	0	-492.36	1.8	-30.96	1.8	-36.75	2.12	36.94



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-272.76	-105.65	0	-556.71	1.8	-34.78	1.8	-41.09	2.12	42.23
1	2	1.10	-436.66	-110.54	27.02	0	-443.92	1.8	-48.46	1.8	-58.89	2.12	3.04
2	2	1.10	-693.96	-110.87	-99.35	0	-819.01	1.8	-66.18	1.8	-74.56	2.12	45.83
2	3	2.20	-693.96	-92.63	12.59	0	-727.38	1.8	-78.06	1.8	-90.06	2.12	12.77
3	3	2.20	-693.96	-92.96	12.57	0	-727.40	1.8	-78.06	1.8	-90.06	2.12	12.78
3	4	3.30	-693.96	-74.72	104.78	0	-651.88	1.8	-87.74	1.8	-102.77	2.12	-14.40
4	4	3.30	-877.74	-75.06	18.18	0	-916.95	1.8	-100.54	1.8	-114.43	2.12	15.14
4	5	4.40	-877.74	-56.84	90.72	0	-857.47	1.8	-108.03	1.8	-124.37	2.12	-6.18
5	5	4.40	-877.74	-57.19	90.71	0	-857.48	1.8	-108.03	1.8	-124.37	2.12	-6.18
5	6	5.50	-877.74	-38.95	143.57	0	-814.07	1.8	-113.33	1.8	-131.52	2.12	-21.62
6	6	5.50	-1061.53	-39.31	58.81	0	-1077.71	1.8	-126.21	1.8	-143.42	2.12	7.40
6	7	6.60	-1061.53	-21.07	92.06	0	-1050.29	1.8	-129.32	1.8	-147.80	2.12	-2.20
7	7	6.60	-1061.53	-21.50	92.01	0	-889.89	1.8	-92.23	1.8	-134.25	2.12	-26.33
7	8	7.70	-1061.53	-3.27	105.62	0	-882.21	1.8	-93.70	1.8	-136.11	2.12	-29.81
8	8	7.70	-1061.53	-3.68	105.59	0	-882.24	1.8	-93.69	1.8	-136.10	2.12	-29.80
8	9	8.80	-1061.53	14.85	99.61	0	-887.86	1.8	-92.31	1.8	-134.77	2.12	-27.49
9	9	8.80	-1061.54	14.28	99.55	0	-887.91	1.8	-92.30	1.8	-134.76	2.12	-27.47
9	10	9.90	-1061.54	32.65	73.78	0	-907.01	1.8	-88.03	1.8	-130.21	2.12	-19.30
10	10	9.90	-1061.53	32.13	73.77	0	-907.02	1.8	-88.02	1.8	-130.21	2.12	-19.30
10	11	11.00	-1061.53	50.36	28.38	0	-939.45	1.8	-80.88	1.8	-122.47	2.12	-5.34
11	11	11.00	-1061.53	49.79	28.35	0	-939.48	1.8	-80.88	1.8	-122.46	2.12	-5.33
11	12	12.10	-1061.53	68.06	-36.48	0	-985.09	1.8	-70.92	1.8	-111.56	2.12	14.37
12	12	12.10	-1061.53	67.48	-36.52	0	-985.13	1.8	-70.91	1.8	-111.55	2.12	14.38
12	13	13.20	-1061.53	85.80	-120.87	0	-1044.00	1.8	-58.10	1.8	-97.48	2.12	39.84
13	13	13.20	-1061.53	85.21	-120.90	0	-1044.02	1.8	-58.10	1.8	-97.47	2.12	39.85
13	14	14.30	-1061.53	103.47	-224.69	0	-1116.08	1.8	-42.47	1.8	-80.24	2.12	71.05
14	14	14.30	-871.84	98.21	-139.98	0	-1008.85	1.8	-71.40	1.8	-85.01	2.12	62.98
14	15	15.40	-874.66	118.95	-261.90	0	-1102.13	1.8	-55.14	1.8	-66.45	2.12	99.32
15	15	15.40	-1567.05	120.68	67.52	0	-1083.10	1.8	-247.85	1.8	-250.47	2.12	-121.35
15	16	16.50	-1567.05	171.41	-80.61	0	-1205.04	1.8	-229.13	1.8	-231.96	2.12	-80.17
16	16	16.50	-1567.05	170.97	-80.51	0	-1249.55	1.8	-185.63	1.8	-194.18	2.12	-28.80
16	17	17.60	-1567.05	201.87	-283.11	0	-1420.05	1.8	-156.93	1.8	-165.99	2.12	31.54
17	17	17.60	-2068.15	201.12	133.48	0	-1076.47	1.8	-353.70	1.8	-342.40	2.12	-232.02
17	18	18.70	-2068.15	248.78	-113.41	0	-1286.23	1.8	-316.59	1.8	-306.07	2.12	-155.89
18	18	18.70	-2068.15	248.09	-112.91	0	-1285.76	1.8	-316.73	1.8	-306.18	2.12	-156.10
18	19	19.80	-2068.15	301.76	-413.70	0	-1544.00	1.8	-268.52	1.8	-259.31	2.12	-59.95
19	19	19.80	-1810.85	301.16	-286.69	0	-1167.32	1.8	-251.50	1.8	-244.53	2.12	-103.81
19	20	20.90	-1810.85	369.71	-662.35	0	-1494.33	1.8	-186.09	1.8	-181.84	2.12	21.74
20	20	20.90	-1810.85	369.35	-662.33	0	-1494.32	1.8	-186.09	1.8	-181.84	2.12	21.74
20	21	22.00	-1810.85	426.15	-1098.56	0	-1875.98	1.8	-107.99	1.8	-107.01	2.12	170.17
21	1021	22.00	-1847.60	-468.61	-1117.60	0	-1930.45	1.8	-110.43	1.8	-109.03	2.12	176.66
21	22	23.40	-1847.60	-409.97	-508.68	0	-1396.41	1.8	-219.99	1.8	-214.66	2.12	-32.15
22	22	23.40	-1847.60	-410.41	-508.49	0	-1396.21	1.8	-220.06	1.8	-214.72	2.12	-32.25
22	23	24.80	-1847.60	-339.29	16.05	0	-937.38	1.8	-313.08	1.8	-304.18	2.12	-210.15
23	23	24.80	-2104.90	-337.78	-107.70	0	-1311.40	1.8	-330.42	1.8	-319.49	2.12	-167.34
23	24	26.20	-2104.90	-252.71	294.30	0	-965.20	1.8	-395.20	1.8	-382.99	2.12	-297.04
24	24	26.20	-1420.02	-252.69	-35.83	0	-1043.21	1.8	-185.86	1.8	-195.34	2.12	-63.45
24	25	27.60	-1420.02	-189.63	272.95	0	-781.27	1.8	-230.91	1.8	-240.28	2.12	-158.06
25	25	27.60	-1750.84	-190.37	123.05	0	-1255.11	1.8	-253.46	1.8	-261.11	2.12	-105.56
25	26	29.00	-1750.84	-109.03	312.98	0	-1096.82	1.8	-277.74	1.8	-286.44	2.12	-160.70
26	26	29.00	-1061.02	-108.66	-16.54	0	-1083.76	1.8	-115.94	1.8	-127.69	2.12	25.43
26	27	30.40	-1058.63	-81.85	119.14	0	-980.46	1.8	-131.72	1.8	-147.61	2.12	-14.24
27	27	30.40	-1356.26	-85.45	-7.66	0	-1206.67	1.8	-104.80	1.8	-149.43	2.12	1.74
27	28	31.80	-1356.26	-62.16	95.68	0	-1138.27	1.8	-119.06	1.8	-166.31	2.12	-28.50
28	28	31.80	-1356.26	-62.92	95.62	0	-1138.31	1.8	-119.05	1.8	-166.30	2.12	-28.48
28	29	33.20	-1356.26	-39.71	167.46	0	-1091.28	1.8	-128.73	1.8	-178.06	2.12	-49.43
29	29	33.20	-1356.26	-40.44	167.45	0	-1091.28	1.8	-128.72	1.8	-178.06	2.12	-49.43
29	30	34.60	-1356.26	-15.66	206.42	0	-1066.74	1.8	-133.56	1.8	-184.47	2.12	-60.63
30	30	34.60	-1356.26	-16.34	206.34	0	-1066.80	1.8	-133.54	1.8	-184.45	2.12	-60.60
30	31	36.00	-1356.26	11.47	208.97	0	-1067.59	1.8	-132.85	1.8	-184.92	2.12	-60.92
31	31	36.00	-1356.26	10.79	208.95	0	-1067.61	1.8	-132.84	1.8	-184.91	2.12	-60.92
31	32	37.40	-1356.26	34.14	177.54	0	-1091.84	1.8	-127.08	1.8	-179.83	2.12	-51.12
32	32	37.40	-1356.26	33.38	177.53	0	-1091.86	1.8	-127.07	1.8	-179.82	2.12	-51.11
32	33	38.80	-1356.26	56.59	114.55	0	-1137.53	1.8	-116.71	1.8	-169.60	2.12	-31.99
33	33	38.80	-1356.26	55.84	114.55	0	-1137.53	1.8	-116.71	1.8	-169.60	2.12	-31.99
33	34	40.20	-1356.26	79.07	20.10	0	-1204.55	1.8	-101.77	1.8	-154.27	2.12	-3.58
34	34	40.20	-1356.26	78.28	20.13	0	-1204.53	1.8	-101.78	1.8	-154.27	2.12	-3.58
34	35	41.60	-1356.26	101.59	-105.74	0	-1292.85	1.8	-82.28	1.8	-133.83	2.12	34.10
35	35	41.60	-1060.58	98.46	21.03	0	-1084.59	1.8	-109.41	1.8	-132.12	2.12	20.54
35	36	43.00	-1063.03	124.80	-135.87	0	-1210.38	1.8	-88.80	1.8	-108.97	2.12	67.61
36	36	43.00	-1750.84	124.64	193.65	0	-1212.85	1.8	-245.00	1.8	-257.32	2.12	-108.37
36	37	44.40	-1750.84	197.91	-19.20	0	-1392.26	1.8	-215.82	1.8	-227.57	2.12	-44.71
37	37	44.40	-1420.02	197.08	130.57	0	-918.56	1.8	-193.23	1.8	-206.70	2.12	-97.15
37	38	45.80	-1420.02	256.51	-183.17	0	-1185.20	1.8	-147.38	1.8	-160.93	2.12	-0.79
38	38	45.80	-2104.90	255.83	147.10	0	-1107.06	1.8	-356.76	1.8	-348.60	2.12	-234.45

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	322.72	-253.08	0	-1451.40	1.8	-293.17	1.8	-285.99	2.12	-106.05
39	39	47.20	-1847.60	321.61	-128.86	0	-1076.93	1.8	-275.96	1.8	-270.81	2.12	-149.06
39	40	48.60	-1841.15	410.22	-643.99	0	-1524.65	1.8	-184.82	1.8	-182.79	2.12	25.45
40	40	48.60	-1840.98	409.72	-644.09	0	-1524.69	1.8	-184.75	1.8	-182.72	2.12	25.53
40	41	50.00	-1840.98	471.69	-1256.81	0	-2062.21	1.8	-74.85	1.8	-76.65	2.12	235.42
41	1041	50.00	-1841.19	-471.60	-1256.82	0	-2062.28	1.8	-74.90	1.8	-76.69	2.12	235.38
41	42	51.40	-1841.19	-409.64	-644.22	0	-1524.85	1.8	-184.78	1.8	-182.76	2.12	25.52
42	42	51.40	-1841.79	-410.13	-644.14	0	-1524.94	1.8	-184.96	1.8	-182.91	2.12	25.34
42	43	52.80	-1841.79	-322.02	-129.00	0	-1075.40	1.8	-274.49	1.8	-269.49	2.12	-147.75
43	43	52.80	-2100.09	-323.08	-253.12	0	-1450.07	1.8	-291.96	1.8	-284.91	2.12	-104.98
43	44	54.20	-2104.90	-255.83	147.12	0	-1107.04	1.8	-356.76	1.8	-348.61	2.12	-234.46
44	44	54.20	-1420.02	-256.51	-183.17	0	-1185.20	1.8	-147.38	1.8	-160.93	2.12	-0.80
44	45	55.60	-1420.02	-197.07	130.60	0	-918.53	1.8	-193.24	1.8	-206.71	2.12	-97.16
45	45	55.60	-1750.84	-197.90	-19.16	0	-1392.23	1.8	-215.83	1.8	-227.57	2.12	-44.72
45	46	57.00	-1750.84	-124.62	193.68	0	-1212.82	1.8	-245.01	1.8	-257.33	2.12	-108.38
46	46	57.00	-1063.03	-124.80	-135.86	0	-1210.38	1.8	-88.80	1.8	-108.97	2.12	67.61
46	47	58.40	-1062.37	-99.38	21.93	0	-1085.47	1.8	-109.68	1.8	-132.53	2.12	20.20
47	47	58.40	-1358.27	-101.53	-104.85	0	-1293.92	1.8	-82.57	1.8	-134.26	2.12	33.75
47	48	59.80	-1358.27	-78.22	20.96	0	-1205.63	1.8	-102.07	1.8	-154.70	2.12	-3.91
48	48	59.80	-1358.27	-78.99	20.95	0	-1205.64	1.8	-102.06	1.8	-154.69	2.12	-3.91
48	49	61.20	-1358.27	-55.77	115.27	0	-1138.71	1.8	-116.98	1.8	-170.01	2.12	-32.28
49	49	61.20	-1358.27	-56.54	115.29	0	-1138.70	1.8	-116.98	1.8	-170.01	2.12	-32.29
49	50	62.60	-1358.27	-33.33	178.19	0	-1093.08	1.8	-127.34	1.8	-180.22	2.12	-51.39
50	50	62.60	-1358.27	-34.08	178.18	0	-1093.09	1.8	-127.34	1.8	-180.22	2.12	-51.39
50	51	64.00	-1360.02	-10.71	209.51	0	-1070.34	1.8	-133.26	1.8	-185.54	2.12	-61.24
51	51	64.00	-1360.02	-11.39	209.51	0	-1070.33	1.8	-133.26	1.8	-185.54	2.12	-61.24
51	52	65.40	-1360.02	16.44	206.78	0	-1069.61	1.8	-133.94	1.8	-185.06	2.12	-60.88
52	52	65.40	-1360.02	15.74	206.83	0	-1069.57	1.8	-133.95	1.8	-185.07	2.12	-60.90
52	53	66.80	-1360.02	40.52	167.78	0	-1094.16	1.8	-129.11	1.8	-178.65	2.12	-49.68
53	53	66.80	-1360.02	39.80	167.80	0	-1094.15	1.8	-129.11	1.8	-178.65	2.12	-49.68
53	54	68.20	-1360.02	63.00	95.86	0	-1141.24	1.8	-119.42	1.8	-166.88	2.12	-28.71
54	54	68.20	-1360.02	62.24	95.89	0	-1141.23	1.8	-119.43	1.8	-166.88	2.12	-28.72
54	55	69.60	-1360.02	85.53	-7.56	0	-1209.70	1.8	-105.16	1.8	-149.98	2.12	1.56
55	55	69.60	-1061.89	83.73	119.22	0	-983.10	1.8	-132.02	1.8	-148.08	2.12	-14.39
55	56	71.00	-1061.02	108.66	-16.54	0	-1083.76	1.8	-115.94	1.8	-127.69	2.12	25.43
56	56	71.00	-1750.84	109.04	312.98	0	-1096.81	1.8	-277.74	1.8	-286.44	2.12	-160.70
56	57	72.40	-1750.84	190.37	123.05	0	-1255.11	1.8	-253.45	1.8	-261.11	2.12	-105.55
57	57	72.40	-1420.02	189.64	272.92	0	-781.31	1.8	-230.90	1.8	-240.27	2.12	-158.05
57	58	73.80	-1420.02	252.70	-35.86	0	-1043.23	1.8	-185.85	1.8	-195.34	2.12	-63.44
58	58	73.80	-2104.91	252.72	294.28	0	-965.22	1.8	-395.19	1.8	-382.98	2.12	-297.04
58	59	75.20	-2104.91	337.80	-107.71	0	-1311.41	1.8	-330.42	1.8	-319.49	2.12	-167.34
59	59	75.20	-1847.60	339.28	16.07	0	-937.37	1.8	-313.08	1.8	-304.19	2.12	-210.15
59	60	76.60	-1843.78	410.87	-509.01	0	-1395.56	1.8	-219.04	1.8	-213.81	2.12	-31.27
60	60	76.60	-1843.83	410.46	-509.29	0	-1395.84	1.8	-218.97	1.8	-213.75	2.12	-31.16
60	61	78.00	-1843.83	469.13	-1118.90	0	-1930.46	1.8	-109.32	1.8	-108.03	2.12	177.83
61	1061	78.00	-1807.39	-426.30	-1099.93	0	-1876.14	1.8	-106.95	1.8	-106.08	2.12	171.30
61	62	79.10	-1807.39	-369.50	-663.52	0	-1494.33	1.8	-185.07	1.8	-180.93	2.12	22.82
62	62	79.10	-1807.77	-369.88	-663.56	0	-1494.47	1.8	-185.16	1.8	-181.01	2.12	22.74
62	63	80.20	-1807.77	-301.33	-287.72	0	-1167.30	1.8	-250.60	1.8	-243.72	2.12	-102.86
63	63	80.20	-2065.61	-301.93	-414.69	0	-1544.11	1.8	-267.76	1.8	-258.63	2.12	-59.13
63	64	81.30	-2065.61	-248.25	-113.71	0	-1285.71	1.8	-315.99	1.8	-305.52	2.12	-155.33
64	64	81.30	-2066.31	-248.92	-114.15	0	-1286.33	1.8	-316.04	1.8	-305.57	2.12	-155.29
64	65	82.40	-2066.31	-201.27	132.92	0	-1076.42	1.8	-353.16	1.8	-341.93	2.12	-231.47
65	65	82.40	-1566.09	-201.97	-283.23	0	-1419.90	1.8	-156.64	1.8	-165.77	2.12	31.78
65	66	83.50	-1566.09	-171.07	-80.90	0	-1249.60	1.8	-185.34	1.8	-193.92	2.12	-28.48
66	66	83.50	-1567.05	-171.44	-80.87	0	-1205.25	1.8	-229.10	1.8	-231.93	2.12	-80.10
66	67	84.60	-1567.05	-120.71	67.26	0	-1083.32	1.8	-247.82	1.8	-250.44	2.12	-121.29
67	67	84.60	-874.65	-118.96	-262.17	0	-1102.31	1.8	-55.10	1.8	-66.40	2.12	99.40
67	68	85.70	-875.52	-100.68	-138.89	0	-1011.17	1.8	-71.87	1.8	-85.72	2.12	62.51
68	68	85.70	-1065.95	-103.39	-223.61	0	-1119.01	1.8	-43.00	1.8	-81.05	2.12	70.55
68	69	86.80	-1065.95	-85.13	-119.89	0	-1047.01	1.8	-58.62	1.8	-98.27	2.12	39.38
69	69	86.80	-1065.96	-85.72	-119.86	0	-1046.99	1.8	-58.63	1.8	-98.28	2.12	39.37
69	70	87.90	-1065.96	-67.41	-35.60	0	-988.18	1.8	-71.42	1.8	-112.34	2.12	13.93
70	70	87.90	-1065.96	-67.98	-35.56	0	-988.14	1.8	-71.43	1.8	-112.35	2.12	13.92
70	71	89.00	-1065.96	-49.73	29.17	0	-942.59	1.8	-81.38	1.8	-123.23	2.12	-5.75
71	71	89.00	-1065.96	-50.30	29.21	0	-942.55	1.8	-81.39	1.8	-123.24	2.12	-5.76
71	72	90.10	-1065.96	-32.06	74.52	0	-910.18	1.8	-88.52	1.8	-130.96	2.12	-19.70
72	72	90.10	-1065.96	-32.58	74.52	0	-910.17	1.8	-88.52	1.8	-130.97	2.12	-19.70
72	73	91.20	-1065.96	-14.21	100.20	0	-891.14	1.8	-92.78	1.8	-135.50	2.12	-27.84
73	73	91.20	-1065.96	-14.79	100.27	0	-891.08	1.8	-92.80	1.8	-135.51	2.12	-27.86
73	74	92.30	-1065.96	3.74	106.16	0	-885.51	1.8	-94.17	1.8	-136.83	2.12	-30.15
74	74	92.30	-1065.96	3.34	106.19	0	-885.49	1.8	-94.17	1.8	-136.83	2.12	-30.15
74	75	93.40	-1065.96	21.57	92.50	0	-893.22	1.8	-92.69	1.8	-134.97	2.12	-26.66
75	75	93.40	-1065.96	21.14	92.55	0	-1054.19	1.8	-129.82	1.8	-148.50	2.12	-2.39
75	76	94.50	-1065.96	39.38	59.22	0	-1081.67	1.8	-126.70	1.8	-144.10	2.12	7.23

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-
C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	39.03	144.00	0	-818.01	1.8	-113.83	1.8	-132.21	2.12	-21.80
76	77	95.60	-882.17	57.27	91.03	0	-861.51	1.8	-108.52	1.8	-125.04	2.12	-6.32
77	77	95.60	-882.17	56.91	91.06	0	-861.49	1.8	-108.52	1.8	-125.04	2.12	-6.33
77	78	96.70	-882.17	75.13	18.42	0	-921.03	1.8	-101.02	1.8	-115.10	2.12	15.01
78	78	96.70	-698.39	74.79	105.02	0	-655.97	1.8	-88.22	1.8	-103.44	2.12	-14.53
78	79	97.80	-698.39	93.03	12.73	0	-731.55	1.8	-78.54	1.8	-90.71	2.12	12.67
79	79	97.80	-698.38	92.69	12.76	0	-731.53	1.8	-78.54	1.8	-90.71	2.12	12.67
79	80	98.90	-698.38	110.93	-99.27	0	-823.22	1.8	-66.65	1.8	-75.20	2.12	45.76
80	80	98.90	-441.09	110.61	27.11	0	-448.13	1.8	-48.94	1.8	-59.54	2.12	2.96
80	81	100.00	-441.09	272.74	-105.65	0	-556.71	1.8	-34.78	1.8	-41.09	2.12	42.23
101	101	0.00	-441.09	-278.59	-105.76	0	-556.80	1.8	-34.75	1.8	-41.07	2.12	42.26
101	102	1.10	-436.66	-107.28	23.31	0	-446.96	1.8	-47.94	1.8	-58.40	2.12	4.11
102	102	1.10	-693.96	-107.62	-102.80	0	-821.83	1.8	-65.70	1.8	-74.11	2.12	46.83
102	103	2.20	-693.96	-89.75	5.73	0	-733.02	1.8	-77.08	1.8	-89.15	2.12	14.76
103	103	2.20	-693.96	-90.01	5.94	0	-732.83	1.8	-77.12	1.8	-89.18	2.12	14.69
103	104	3.30	-693.96	-72.18	95.09	0	-659.84	1.8	-86.34	1.8	-101.47	2.12	-11.58
104	104	3.30	-877.74	-72.30	8.71	0	-924.72	1.8	-99.18	1.8	-113.17	2.12	17.89
104	105	4.40	-877.74	-54.49	78.47	0	-867.57	1.8	-106.23	1.8	-122.71	2.12	-2.59
105	105	4.40	-877.74	-54.56	78.60	0	-867.45	1.8	-106.26	1.8	-122.73	2.12	-2.63
105	106	5.50	-877.74	-36.71	128.79	0	-826.29	1.8	-111.12	1.8	-129.48	2.12	-17.25
106	106	5.50	-1061.53	-36.64	44.20	0	-1089.78	1.8	-124.02	1.8	-141.41	2.12	11.72
106	107	6.60	-1061.53	-18.79	74.69	0	-1064.71	1.8	-126.65	1.8	-145.36	2.12	3.00
107	107	6.60	-1061.53	-18.67	74.80	0	-900.96	1.8	-89.45	1.8	-131.73	2.12	-21.55
107	108	7.70	-1061.53	-0.85	85.53	0	-895.53	1.8	-90.38	1.8	-133.11	2.12	-24.11
108	108	7.70	-1061.53	-0.68	85.64	0	-895.44	1.8	-90.40	1.8	-133.12	2.12	-24.15
108	109	8.80	-1061.53	17.15	76.60	0	-903.58	1.8	-88.42	1.8	-131.27	2.12	-20.84
109	109	8.80	-1061.53	17.33	76.66	0	-903.53	1.8	-88.43	1.8	-131.28	2.12	-20.86
109	110	9.90	-1061.53	35.16	47.78	0	-925.29	1.8	-83.53	1.8	-126.19	2.12	-11.65
110	110	9.90	-1061.53	35.40	47.84	0	-925.24	1.8	-83.54	1.8	-126.20	2.12	-11.67
110	111	11.00	-1061.53	53.24	-0.90	0	-960.63	1.8	-75.70	1.8	-117.86	2.12	3.44
111	111	11.00	-1061.53	53.55	-0.87	0	-960.61	1.8	-75.71	1.8	-117.87	2.12	3.44
111	112	12.10	-1061.53	71.37	-69.60	0	-1009.74	1.8	-64.92	1.8	-106.26	2.12	24.49
112	112	12.10	-1061.53	71.69	-69.60	0	-1009.74	1.8	-64.92	1.8	-106.26	2.12	24.49
112	113	13.20	-1061.53	89.53	-158.28	0	-1072.59	1.8	-51.19	1.8	-91.40	2.12	51.49
113	113	13.20	-1061.53	89.87	-158.32	0	-1072.62	1.8	-51.18	1.8	-91.39	2.12	51.50
113	114	14.30	-1061.53	107.75	-267.03	0	-1149.25	1.8	-34.49	1.8	-73.25	2.12	84.45
114	114	14.30	-871.84	103.50	-182.35	0	-1045.14	1.8	-63.54	1.8	-78.12	2.12	76.74
114	115	15.40	-874.66	124.08	-309.87	0	-1143.38	1.8	-46.04	1.8	-58.51	2.12	115.06
115	115	15.40	-1567.05	126.89	19.44	0	-1124.29	1.8	-239.25	1.8	-242.98	2.12	-106.14
115	116	16.50	-1567.05	171.90	-135.47	0	-1252.29	1.8	-218.86	1.8	-223.04	2.12	-62.36
116	116	16.50	-1567.05	172.28	-135.59	0	-1302.80	1.8	-169.65	1.8	-180.31	2.12	-4.23
116	117	17.60	-1567.05	201.76	-339.20	0	-1476.28	1.8	-138.29	1.8	-149.85	2.12	59.17
117	117	17.60	-2068.15	201.98	77.13	0	-1132.92	1.8	-335.01	1.8	-326.22	2.12	-204.31
117	118	18.70	-2068.15	259.47	-178.11	0	-1353.05	1.8	-292.77	1.8	-285.48	2.12	-121.45
118	118	18.70	-2068.15	259.89	-177.77	0	-1352.71	1.8	-292.88	1.8	-285.58	2.12	-121.62
118	119	19.80	-2068.15	325.76	-498.31	0	-1632.66	1.8	-235.86	1.8	-231.12	2.12	-13.25
119	119	19.80	-1810.85	326.70	-371.70	0	-1256.33	1.8	-218.75	1.8	-216.26	2.12	-56.96
119	120	20.90	-1810.85	409.99	-786.02	0	-1623.67	1.8	-138.64	1.8	-140.87	2.12	89.68
120	120	20.90	-1810.85	411.30	-785.96	0	-1623.60	1.8	-138.66	1.8	-140.89	2.12	89.65
120	121	22.00	-1810.85	464.01	-1263.11	0	-2048.07	1.8	-44.84	1.8	-52.49	2.12	260.58
121	1121	22.00	-1847.60	-504.29	-1282.25	0	-2102.64	1.8	-47.25	1.8	-54.48	2.12	267.11
121	122	23.40	-1847.60	-440.55	-625.35	0	-1518.20	1.8	-175.49	1.8	-176.24	2.12	31.65
122	122	23.40	-1847.60	-438.85	-625.48	0	-1518.33	1.8	-175.45	1.8	-176.20	2.12	31.72
122	123	24.80	-1847.60	-364.18	-64.55	0	-1020.83	1.8	-283.16	1.8	-278.34	2.12	-166.98
123	123	24.80	-2104.90	-362.24	-188.35	0	-1394.92	1.8	-300.45	1.8	-293.60	2.12	-124.11
123	124	26.20	-2104.90	-264.64	237.91	0	-1022.28	1.8	-375.81	1.8	-366.21	2.12	-268.55
124	124	26.20	-1420.02	-264.10	-92.07	0	-1100.17	1.8	-166.48	1.8	-178.57	2.12	-34.98
124	125	27.60	-1420.02	-196.37	227.87	0	-824.93	1.8	-217.74	1.8	-228.84	2.12	-137.85
125	125	27.60	-1750.84	-196.22	78.19	0	-1298.59	1.8	-240.31	1.8	-249.69	2.12	-85.40
125	126	29.00	-1750.84	-113.34	279.94	0	-1127.72	1.8	-269.39	1.8	-279.16	2.12	-147.32
126	126	29.00	-1061.03	-111.54	-49.39	0	-1111.94	1.8	-109.79	1.8	-122.31	2.12	36.14
126	127	30.40	-1058.64	-85.90	91.28	0	-1004.19	1.8	-126.71	1.8	-143.19	2.12	-5.32
127	127	30.40	-1356.26	-88.14	-35.40	0	-1227.71	1.8	-99.71	1.8	-144.94	2.12	10.33
127	128	31.80	-1356.26	-65.28	71.92	0	-1155.47	1.8	-114.85	1.8	-162.57	2.12	-21.37
128	128	31.80	-1356.26	-64.65	71.99	0	-1155.42	1.8	-114.87	1.8	-162.58	2.12	-21.39
128	129	33.20	-1356.26	-41.96	146.64	0	-1105.69	1.8	-125.17	1.8	-174.87	2.12	-43.36
129	129	33.20	-1356.26	-41.39	146.68	0	-1105.66	1.8	-125.17	1.8	-174.88	2.12	-43.37
129	130	34.60	-1356.26	-17.24	187.68	0	-1079.22	1.8	-130.45	1.8	-181.66	2.12	-55.30
130	130	34.60	-1356.26	-16.65	187.64	0	-1079.25	1.8	-130.44	1.8	-181.65	2.12	-55.29
130	131	36.00	-1356.26	11.60	190.50	0	-1079.78	1.8	-129.81	1.8	-182.16	2.12	-55.71
131	131	36.00	-1356.26	12.19	190.52	0	-1079.76	1.8	-129.81	1.8	-182.17	2.12	-55.71
131	132	37.40	-1356.26	34.94	157.52	0	-1105.39	1.8	-123.72	1.8	-176.80	2.12	-45.37
132	132	37.40	-1356.26	35.53	157.53	0	-1105.38	1.8	-123.72	1.8	-176.80	2.12	-45.37
132	133	38.80	-1356.26	58.23	91.90	0	-1153.47	1.8	-112.79	1.8	-166.10	2.12	-25.32
133	133	38.80	-1356.26	58.85	91.88	0	-1153.48	1.8	-112.79	1.8	-166.09	2.12	-25.31

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-
C. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	81.58	-6.42	0	-1224.07	1.8	-97.02	1.8	-150.05	2.12	4.47
134	134	40.20	-1356.26	82.20	-6.47	0	-1224.10	1.8	-97.01	1.8	-150.04	2.12	4.49
134	135	41.60	-1356.26	105.07	-137.54	0	-1317.26	1.8	-76.38	1.8	-128.64	2.12	44.03
135	135	41.60	-1060.58	103.34	-10.83	0	-1111.78	1.8	-103.61	1.8	-127.02	2.12	30.79
135	136	43.00	-1063.03	128.73	-174.11	0	-1243.22	1.8	-81.59	1.8	-102.67	2.12	80.12
136	136	43.00	-1750.84	130.15	155.25	0	-1249.03	1.8	-234.98	1.8	-248.59	2.12	-92.47
136	137	44.40	-1750.84	202.69	-68.74	0	-1440.49	1.8	-201.06	1.8	-214.75	2.12	-22.17
137	137	44.40	-1420.02	202.99	80.78	0	-966.98	1.8	-178.44	1.8	-193.86	2.12	-74.56
137	138	45.80	-1420.02	267.20	-244.23	0	-1247.09	1.8	-126.28	1.8	-142.67	2.12	30.18
138	138	45.80	-2104.90	267.50	85.86	0	-1169.08	1.8	-335.65	1.8	-330.34	2.12	-203.45
138	139	47.20	-2104.90	343.09	-337.12	0	-1538.52	1.8	-261.83	1.8	-258.93	2.12	-60.89
139	139	47.20	-1847.60	343.89	-213.09	0	-1164.20	1.8	-244.61	1.8	-243.72	2.12	-103.85
139	140	48.60	-1841.15	439.79	-767.79	0	-1653.73	1.8	-137.77	1.8	-142.16	2.12	92.96
140	140	48.60	-1840.98	441.53	-767.72	0	-1653.60	1.8	-137.77	1.8	-142.15	2.12	92.94
140	141	50.00	-1840.98	508.82	-1430.48	0	-2243.59	1.8	-8.51	1.8	-19.37	2.12	330.50
141	1141	50.00	-1841.18	-508.74	-1430.48	0	-2243.65	1.8	-8.56	1.8	-19.41	2.12	330.46
141	142	51.40	-1841.18	-441.44	-767.82	0	-1653.74	1.8	-137.81	1.8	-142.19	2.12	92.92
142	142	51.40	-1841.79	-439.71	-767.89	0	-1654.00	1.8	-137.92	1.8	-142.29	2.12	92.84
142	143	52.80	-1841.79	-344.30	-213.22	0	-1162.66	1.8	-243.14	1.8	-242.41	2.12	-102.55
143	143	52.80	-2100.09	-343.46	-337.14	0	-1537.17	1.8	-260.63	1.8	-257.85	2.12	-59.83
143	144	54.20	-2104.90	-267.48	85.86	0	-1169.09	1.8	-335.65	1.8	-330.35	2.12	-203.45
144	144	54.20	-1420.02	-267.21	-244.23	0	-1247.08	1.8	-126.29	1.8	-142.68	2.12	30.17
144	145	55.60	-1420.02	-203.00	80.82	0	-966.95	1.8	-178.46	1.8	-193.87	2.12	-74.58
145	145	55.60	-1750.84	-202.69	-68.70	0	-1440.45	1.8	-201.07	1.8	-214.76	2.12	-22.19
145	146	57.00	-1750.84	-130.15	155.25	0	-1249.03	1.8	-234.98	1.8	-248.59	2.12	-92.48
146	146	57.00	-1063.03	-128.75	-174.11	0	-1243.22	1.8	-81.59	1.8	-102.67	2.12	80.12
146	147	58.40	-1062.37	-104.27	-9.94	0	-1112.67	1.8	-103.88	1.8	-127.43	2.12	30.46
147	147	58.40	-1358.27	-105.01	-136.62	0	-1318.31	1.8	-76.68	1.8	-129.09	2.12	43.67
147	148	59.80	-1358.27	-82.14	-5.67	0	-1225.24	1.8	-97.29	1.8	-150.46	2.12	4.17
148	148	59.80	-1358.28	-81.53	-5.60	0	-1225.19	1.8	-97.30	1.8	-150.48	2.12	4.15
148	149	61.20	-1358.28	-58.79	92.60	0	-1154.66	1.8	-113.06	1.8	-166.51	2.12	-25.61
149	149	61.20	-1358.27	-58.17	92.61	0	-1154.66	1.8	-113.06	1.8	-166.50	2.12	-25.61
149	150	62.60	-1358.27	-35.47	158.17	0	-1106.62	1.8	-123.98	1.8	-177.19	2.12	-45.65
150	150	62.60	-1358.27	-34.88	158.18	0	-1106.61	1.8	-123.98	1.8	-177.20	2.12	-45.65
150	151	64.00	-1360.02	-12.11	191.05	0	-1082.51	1.8	-130.22	1.8	-182.79	2.12	-56.02
151	151	64.00	-1360.02	-11.52	191.03	0	-1082.53	1.8	-130.22	1.8	-182.79	2.12	-56.02
151	152	65.40	-1360.02	16.73	188.06	0	-1082.08	1.8	-130.83	1.8	-182.25	2.12	-55.56
152	152	65.40	-1360.02	17.32	188.10	0	-1082.04	1.8	-130.84	1.8	-182.26	2.12	-55.58
152	153	66.80	-1360.02	41.46	146.98	0	-1108.56	1.8	-125.56	1.8	-175.46	2.12	-43.62
153	153	66.80	-1360.02	42.04	146.95	0	-1108.58	1.8	-125.55	1.8	-175.46	2.12	-43.61
153	154	68.20	-1360.02	64.73	72.17	0	-1158.40	1.8	-115.23	1.8	-163.15	2.12	-21.60
154	154	68.20	-1360.02	65.36	72.11	0	-1158.44	1.8	-115.22	1.8	-163.14	2.12	-21.58
154	155	69.60	-1360.02	88.21	-35.31	0	-1230.75	1.8	-100.06	1.8	-145.49	2.12	10.15
155	155	69.60	-1061.89	87.76	91.36	0	-1006.82	1.8	-127.01	1.8	-143.66	2.12	-5.47
155	156	71.00	-1061.02	111.53	-49.41	0	-1111.96	1.8	-109.79	1.8	-122.31	2.12	36.15
156	156	71.00	-1750.84	113.34	279.91	0	-1127.75	1.8	-269.38	1.8	-279.15	2.12	-147.31
156	157	72.40	-1750.84	196.23	78.17	0	-1298.61	1.8	-240.30	1.8	-249.69	2.12	-85.39
157	157	72.40	-1420.02	196.37	227.85	0	-824.96	1.8	-217.73	1.8	-228.83	2.12	-137.84
157	158	73.80	-1420.02	264.10	-92.09	0	-1100.19	1.8	-166.47	1.8	-178.57	2.12	-34.97
158	158	73.80	-2104.90	264.64	237.89	0	-1022.29	1.8	-375.81	1.8	-366.21	2.12	-268.54
158	159	75.20	-2104.90	362.26	-188.36	0	-1394.93	1.8	-300.45	1.8	-293.60	2.12	-124.11
159	159	75.20	-1847.60	364.16	-64.57	0	-1020.85	1.8	-283.16	1.8	-278.33	2.12	-166.97
159	160	76.60	-1843.78	439.32	-625.99	0	-1517.67	1.8	-174.42	1.8	-175.28	2.12	32.69
160	160	76.60	-1843.83	441.04	-625.98	0	-1517.65	1.8	-174.47	1.8	-175.32	2.12	32.65
160	161	78.00	-1843.83	504.80	-1283.57	0	-2102.68	1.8	-46.14	1.8	-53.48	2.12	268.30
161	1161	78.00	-1807.39	-464.17	-1264.46	0	-2048.22	1.8	-43.80	1.8	-51.56	2.12	261.70
161	162	79.10	-1807.39	-411.47	-787.16	0	-1623.62	1.8	-137.64	1.8	-139.98	2.12	90.72
162	162	79.10	-1807.77	-410.15	-787.26	0	-1623.83	1.8	-137.70	1.8	-140.04	2.12	90.69
162	163	80.20	-1807.77	-326.88	-372.71	0	-1256.31	1.8	-217.85	1.8	-215.45	2.12	-56.01
163	163	80.20	-2065.60	-325.92	-499.30	0	-1632.76	1.8	-235.09	1.8	-230.44	2.12	-12.43
163	164	81.30	-2065.60	-260.05	-178.57	0	-1352.65	1.8	-292.14	1.8	-284.92	2.12	-120.85
164	164	81.30	-2066.31	-259.62	-178.85	0	-1353.14	1.8	-292.22	1.8	-284.98	2.12	-120.85
164	165	82.40	-2066.31	-202.14	76.54	0	-1132.89	1.8	-334.48	1.8	-325.74	2.12	-203.75
165	165	82.40	-1566.09	-201.86	-339.33	0	-1476.13	1.8	-138.01	1.8	-149.63	2.12	59.41
165	166	83.50	-1566.09	-172.38	-136.00	0	-1302.87	1.8	-169.36	1.8	-180.04	2.12	-3.91
166	166	83.50	-1567.05	-171.93	-135.77	0	-1252.53	1.8	-218.82	1.8	-223.00	2.12	-62.28
166	167	84.60	-1567.05	-126.91	19.20	0	-1124.49	1.8	-239.22	1.8	-242.95	2.12	-106.08
167	167	84.60	-874.65	-124.08	-310.15	0	-1143.56	1.8	-46.00	1.8	-58.47	2.12	115.14
167	168	85.70	-875.52	-105.97	-181.27	0	-1047.46	1.8	-64.01	1.8	-78.83	2.12	76.27
168	168	85.70	-1065.96	-107.69	-265.94	0	-1152.18	1.8	-35.03	1.8	-74.07	2.12	83.95
168	169	86.80	-1065.96	-89.82	-157.31	0	-1075.60	1.8	-51.71	1.8	-92.19	2.12	51.02
169	169	86.80	-1065.96	-89.46	-157.28	0	-1075.58	1.8	-51.72	1.8	-92.20	2.12	51.01
169	170	87.90	-1065.96	-71.63	-68.67	0	-1012.78	1.8	-65.44	1.8	-107.05	2.12	24.04
170	170	87.90	-1065.96	-71.29	-68.67	0	-1012.78	1.8	-65.44	1.8	-107.05	2.12	24.04
170	171	89.00	-1065.96	-53.48	-0.04	0	-963.71	1.8	-76.22	1.8	-118.64	2.12	3.01

CÁLCULO TENSIONAL

Hipótesis de cálculo:

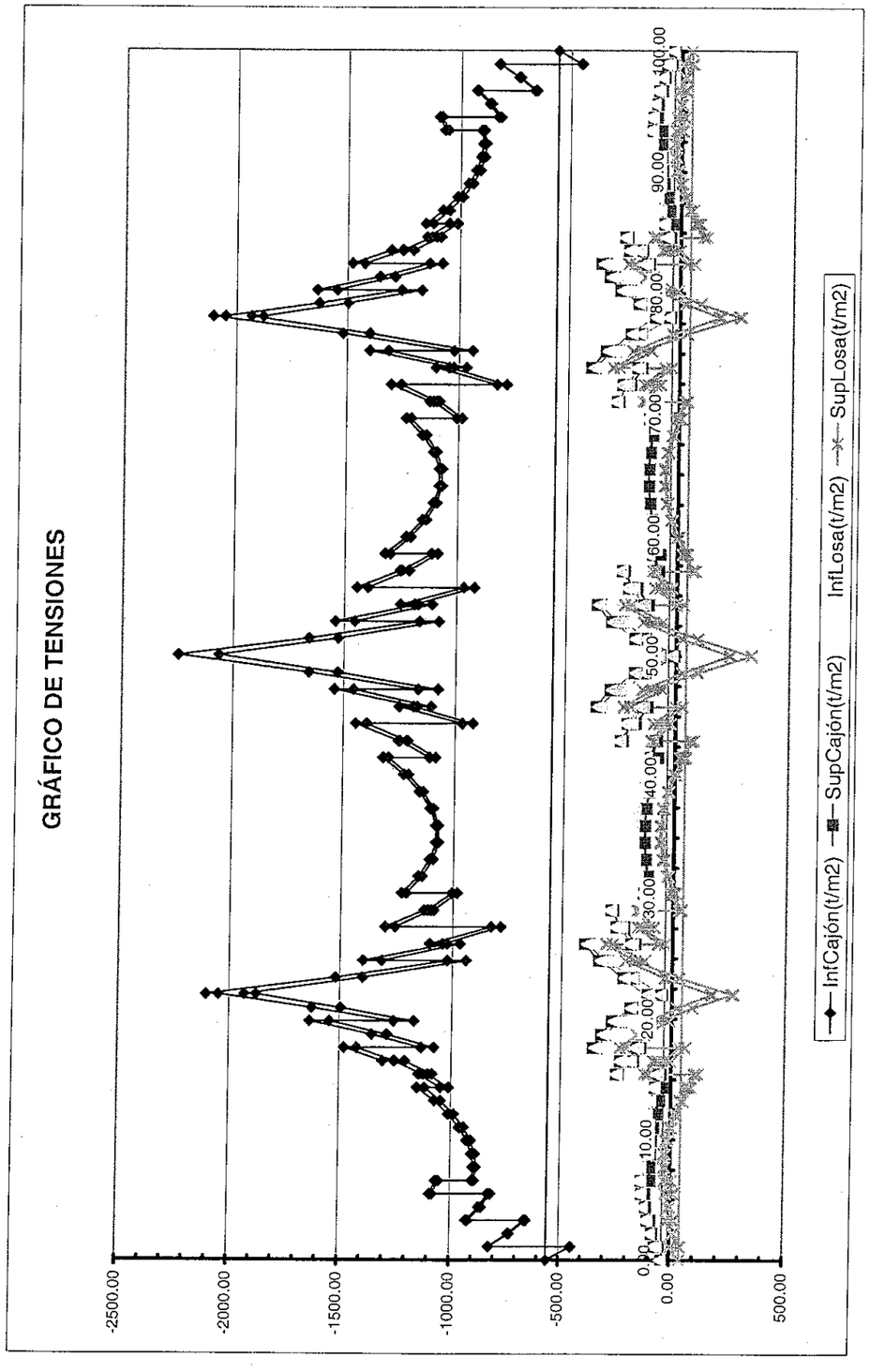
INFRECUENTEST.Tinf.MZ-

3. Infrecuentes dominante tren Mz-

[1; 1]PPVF1 + [.95; 1.05]eje1I1.ISO.To + [.95; 1.05]eje2I1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1I3.ISO.To + [.95; 1.05]eje1I3.HIP.To + [.95; 1.05]eje2I3.ISO.To + [.95; 1.05]eje2I3.HIP.To + [1, 1]HLCV + [.7; 1.3]CMB

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1065.96	-53.19	-0.05	0	-963.72	1.8	-76.21	1.8	-118.64	2.12	3.01
171	172	90.10	-1065.96	-35.33	48.60	0	-928.39	1.8	-84.04	1.8	-126.96	2.12	-12.07
172	172	90.10	-1065.96	-35.07	48.54	0	-928.44	1.8	-84.02	1.8	-126.95	2.12	-12.05
172	173	91.20	-1065.96	-17.24	77.32	0	-906.75	1.8	-88.92	1.8	-132.02	2.12	-21.23
173	173	91.20	-1065.96	-17.08	77.25	0	-906.80	1.8	-88.90	1.8	-132.01	2.12	-21.21
173	174	92.30	-1065.96	0.75	86.22	0	-898.71	1.8	-90.88	1.8	-133.85	2.12	-24.50
174	174	92.30	-1065.96	0.93	86.11	0	-898.79	1.8	-90.86	1.8	-133.83	2.12	-24.47
174	175	93.40	-1065.96	18.75	75.30	0	-904.27	1.8	-89.92	1.8	-132.44	2.12	-21.88
175	175	93.40	-1065.96	18.85	75.19	0	-1068.59	1.8	-127.15	1.8	-146.06	2.12	2.80
175	176	94.50	-1065.96	36.71	44.60	0	-1093.74	1.8	-124.51	1.8	-142.09	2.12	11.55
176	176	94.50	-882.17	36.77	129.21	0	-830.23	1.8	-111.61	1.8	-130.17	2.12	-17.43
176	177	95.60	-882.17	54.61	78.94	0	-871.47	1.8	-106.75	1.8	-123.40	2.12	-2.78
177	177	95.60	-882.17	54.55	78.78	0	-871.60	1.8	-106.72	1.8	-123.38	2.12	-2.73
177	178	96.70	-882.17	72.37	8.94	0	-928.82	1.8	-99.66	1.8	-113.83	2.12	17.77
178	178	96.70	-698.39	72.22	95.37	0	-663.90	1.8	-86.83	1.8	-102.14	2.12	-11.72
178	179	97.80	-698.39	90.06	6.10	0	-736.99	1.8	-77.60	1.8	-89.83	2.12	14.59
179	179	97.80	-698.40	89.83	5.89	0	-737.17	1.8	-77.56	1.8	-89.80	2.12	14.66
179	180	98.90	-698.40	107.70	-102.73	0	-826.06	1.8	-66.17	1.8	-74.75	2.12	46.75
180	180	98.90	-441.09	107.35	23.40	0	-451.17	1.8	-48.41	1.8	-59.05	2.12	4.03
180	181	100.00	-441.09	278.57	-105.76	0	-556.80	1.8	-34.75	1.8	-41.07	2.12	42.26



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-391.36	-164.06	-85.30	0	-492.43	1.8	-30.95	1.8	-36.74	2.12	36.97
1	2	1.10	-395.79	-269.19	227.49	0	-233.58	1.8	-79.37	1.8	-85.42	2.12	-61.23
2	2	1.10	-624.09	-269.50	119.62	0	-565.96	1.8	-95.16	1.8	-99.41	2.12	-23.37
2	3	2.20	-624.09	-236.78	395.44	0	-333.62	1.8	-137.83	1.8	-141.89	2.12	-110.05
3	3	2.20	-624.08	-237.03	395.55	0	-333.52	1.8	-137.85	1.8	-141.90	2.12	-110.09
3	4	3.30	-624.08	-204.37	634.07	0	-132.33	1.8	-175.05	1.8	-178.73	2.12	-185.17
4	4	3.30	-787.15	-204.54	560.32	0	-367.18	1.8	-186.46	1.8	-189.14	2.12	-159.06
4	5	4.40	-787.15	-166.96	761.40	0	-197.28	1.8	-218.16	1.8	-220.29	2.12	-222.49
5	5	4.40	-787.15	-167.06	761.52	0	-197.17	1.8	-218.18	1.8	-220.32	2.12	-222.53
5	6	5.50	-787.15	-132.72	931.09	0	-53.43	1.8	-245.53	1.8	-246.79	2.12	-276.28
6	6	5.50	-950.22	-132.80	858.92	0	-287.06	1.8	-256.99	1.8	-257.40	2.12	-250.60
6	7	6.60	-950.22	-100.04	991.36	0	-174.33	1.8	-278.89	1.8	-278.24	2.12	-292.81
7	7	6.60	-950.22	-100.12	991.44	0	-89.05	1.8	-249.46	1.8	-268.95	2.12	-308.68
7	8	7.70	-950.22	-67.42	1086.67	0	-15.33	1.8	-266.66	1.8	-284.58	2.12	-338.58
8	8	7.70	-950.22	-67.41	1086.72	0	-15.29	1.8	-266.67	1.8	-284.59	2.12	-338.60
8	9	8.80	-950.22	-34.97	1143.87	0	30.55	1.8	-277.52	1.8	-293.96	2.12	-356.83
9	9	8.80	-950.22	-34.91	1143.90	0	30.58	1.8	-277.53	1.8	-293.97	2.12	-356.84
9	10	9.90	-950.22	-2.30	1169.26	0	53.69	1.8	-283.25	1.8	-298.16	2.12	-365.47
10	10	9.90	-950.22	-2.21	1169.27	0	53.70	1.8	-283.25	1.8	-298.16	2.12	-365.47
10	11	11.00	-950.22	30.58	1157.74	0	49.91	1.8	-282.85	1.8	-296.31	2.12	-362.83
11	11	11.00	-950.22	30.64	1157.75	0	49.91	1.8	-282.85	1.8	-296.31	2.12	-362.83
11	12	12.10	-950.22	63.37	1109.11	0	19.04	1.8	-276.29	1.8	-288.37	2.12	-348.84
12	12	12.10	-950.22	63.48	1109.09	0	19.02	1.8	-276.28	1.8	-288.37	2.12	-348.83
12	13	13.20	-950.22	95.96	1022.83	0	-39.34	1.8	-263.45	1.8	-274.27	2.12	-323.33
13	13	13.20	-950.22	96.05	1022.79	0	-39.38	1.8	-263.44	1.8	-274.26	2.12	-323.32
13	14	14.30	-950.22	128.83	903.12	0	-121.80	1.8	-245.17	1.8	-254.70	2.12	-287.69
14	14	14.30	-780.33	129.55	975.32	0	35.02	1.8	-268.09	1.8	-256.61	2.12	-301.46
14	15	15.40	-775.77	159.78	817.70	0	-82.02	1.8	-245.14	1.8	-231.55	2.12	-253.68
15	15	15.40	-1554.62	162.03	1188.93	0	-51.92	1.8	-457.86	1.8	-432.70	2.12	-496.46
15	16	16.50	-1554.62	162.31	1001.01	0	-207.41	1.8	-433.02	1.8	-408.79	2.12	-443.65
16	16	16.50	-1554.62	162.19	1000.83	0	-149.13	1.8	-489.99	1.8	-458.28	2.12	-510.93
16	17	17.60	-1554.62	177.87	810.41	0	-313.28	1.8	-458.40	1.8	-427.72	2.12	-448.94
17	17	17.60	-2163.46	177.88	1255.64	0	9.74	1.8	-683.48	1.8	-629.50	2.12	-739.05
17	18	18.70	-2163.46	175.51	1054.08	0	-162.25	1.8	-652.37	1.8	-598.52	2.12	-675.24
18	18	18.70	-2163.46	175.52	1053.62	0	-162.70	1.8	-652.23	1.8	-598.40	2.12	-675.03
18	19	19.80	-2163.46	177.51	858.19	0	-325.75	1.8	-626.72	1.8	-571.42	2.12	-617.19
19	19	19.80	-1935.17	177.46	965.63	0	7.20	1.8	-611.30	1.8	-558.04	2.12	-655.62
19	20	20.90	-1935.17	179.50	769.04	0	-153.95	1.8	-589.27	1.8	-533.22	2.12	-600.50
20	20	20.90	-1935.17	179.11	769.06	0	-153.94	1.8	-589.28	1.8	-533.22	2.12	-600.51
20	21	22.00	-1935.17	184.38	568.67	0	-315.44	1.8	-570.32	1.8	-509.96	2.12	-547.05
21	1021	22.00	-1967.78	-205.00	552.25	0	-363.85	1.8	-572.45	1.8	-511.72	2.12	-541.24
21	22	23.40	-1967.78	-189.43	832.75	0	-137.57	1.8	-598.26	1.8	-544.35	2.12	-616.25
22	22	23.40	-1967.78	-189.85	832.69	0	-137.62	1.8	-598.24	1.8	-544.34	2.12	-616.23
22	23	24.80	-1967.78	-184.41	1096.01	0	77.41	1.8	-625.81	1.8	-576.72	2.12	-688.99
23	23	24.80	-2196.07	-184.90	990.28	0	-254.31	1.8	-641.16	1.8	-590.27	2.12	-650.97
23	24	26.20	-2196.07	-205.86	1259.87	0	-28.32	1.8	-676.74	1.8	-628.20	2.12	-731.78
24	24	26.20	-1424.17	-206.60	889.32	0	-114.97	1.8	-440.78	1.8	-416.69	2.12	-468.67
24	25	27.60	-1424.17	-197.07	1168.86	0	125.52	1.8	-485.43	1.8	-461.10	2.12	-559.15
25	25	27.60	-1717.69	-197.10	1042.39	0	-293.47	1.8	-505.75	1.8	-479.87	2.12	-513.09
25	26	29.00	-1717.69	-208.28	1342.37	0	-33.77	1.8	-556.08	1.8	-527.95	2.12	-610.83
26	26	29.00	-941.07	-206.91	971.30	0	-124.34	1.8	-283.84	1.8	-273.72	2.12	-296.00
26	27	30.40	-945.20	-169.24	1231.74	0	80.62	1.8	-323.48	1.8	-314.90	2.12	-376.54
27	27	30.40	-1210.45	-168.29	1124.10	0	-185.91	1.8	-303.28	1.8	-319.41	2.12	-355.74
27	28	31.80	-1210.45	-125.87	1325.65	0	-40.17	1.8	-336.14	1.8	-352.54	2.12	-417.17
28	28	31.80	-1210.45	-125.68	1325.77	0	-40.06	1.8	-336.17	1.8	-352.56	2.12	-417.21
28	29	33.20	-1210.45	-79.47	1468.95	0	63.23	1.8	-359.38	1.8	-376.13	2.12	-460.83
29	29	33.20	-1210.45	-79.27	1469.06	0	63.33	1.8	-359.41	1.8	-376.15	2.12	-460.87
29	30	34.60	-1210.45	-42.84	1555.28	0	125.33	1.8	-373.25	1.8	-390.40	2.12	-487.13
30	30	34.60	-1210.45	-42.59	1555.33	0	125.37	1.8	-373.26	1.8	-390.41	2.12	-487.15
30	31	36.00	-1210.45	-0.68	1580.77	0	142.94	1.8	-376.98	1.8	-394.69	2.12	-494.82
31	31	36.00	-1210.45	-0.49	1580.78	0	142.95	1.8	-376.98	1.8	-394.70	2.12	-494.82
31	32	37.40	-1210.45	46.10	1550.47	0	120.21	1.8	-371.56	1.8	-389.86	2.12	-485.54
32	32	37.40	-1210.45	46.33	1550.45	0	120.19	1.8	-371.55	1.8	-389.86	2.12	-485.53
32	33	38.80	-1210.45	82.75	1459.31	0	52.99	1.8	-356.01	1.8	-375.05	2.12	-457.64
33	33	38.80	-1210.45	82.98	1459.22	0	52.91	1.8	-355.99	1.8	-375.04	2.12	-457.61
33	34	40.20	-1210.45	129.23	1311.18	0	-55.53	1.8	-331.08	1.8	-350.92	2.12	-412.38
34	34	40.20	-1210.45	129.40	1311.07	0	-55.63	1.8	-331.05	1.8	-350.90	2.12	-412.34
34	35	41.60	-1210.45	171.82	1104.53	0	-206.63	1.8	-296.47	1.8	-317.20	2.12	-349.26
35	35	41.60	-946.85	173.19	1212.14	0	45.37	1.8	-316.75	1.8	-312.68	2.12	-368.01
35	36	43.00	-942.63	211.31	945.44	0	-168.35	1.8	-275.42	1.8	-270.78	2.12	-285.16
36	36	43.00	-1717.69	212.28	1316.55	0	-57.42	1.8	-552.82	1.8	-524.38	2.12	-602.81
36	37	44.40	-1717.69	207.39	1013.42	0	-321.04	1.8	-501.07	1.8	-474.95	2.12	-502.87
37	37	44.40	-1424.17	207.43	1139.97	0	98.02	1.8	-480.77	1.8	-456.21	2.12	-548.97
37	38	45.80	-1424.17	219.83	841.62	0	-160.59	1.8	-431.27	1.8	-407.44	2.12	-450.52
38	38	45.80	-2196.07	219.53	1212.07	0	-74.04	1.8	-667.20	1.8	-618.92	2.12	-713.59

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2196.07	205.41	917.38	0	-324.23	1.8	-624.94	1.8	-575.05	2.12	-622.02
39	39	47.20	-1967.78	205.62	1022.68	0	7.07	1.8	-609.46	1.8	-561.39	2.12	-659.85
39	40	48.60	-1974.23	204.42	734.78	0	-233.57	1.8	-576.88	1.8	-524.56	2.12	-577.86
40	40	48.60	-1974.41	204.00	734.89	0	-233.53	1.8	-576.94	1.8	-524.61	2.12	-577.92
40	41	50.00	-1974.41	218.72	433.84	0	-479.73	1.8	-545.66	1.8	-487.08	2.12	-494.05
41	1041	50.00	-1974.19	-218.81	433.84	0	-479.67	1.8	-545.61	1.8	-487.04	2.12	-494.00
41	42	51.40	-1974.19	-204.08	735.00	0	-233.38	1.8	-576.90	1.8	-524.58	2.12	-577.91
42	42	51.40	-1973.59	-204.49	734.91	0	-233.29	1.8	-576.74	1.8	-524.43	2.12	-577.75
42	43	52.80	-1973.59	-205.20	1022.83	0	5.54	1.8	-610.93	1.8	-562.71	2.12	-661.16
43	43	52.80	-2200.88	-205.05	917.41	0	-325.57	1.8	-626.15	1.8	-576.13	2.12	-623.08
43	44	54.20	-2196.07	-219.53	1212.08	0	-74.03	1.8	-667.20	1.8	-618.92	2.12	-713.59
44	44	54.20	-1424.17	-219.83	841.61	0	-160.60	1.8	-431.27	1.8	-407.44	2.12	-450.52
44	45	55.60	-1424.17	-207.44	1140.00	0	98.05	1.8	-480.77	1.8	-456.21	2.12	-548.98
45	45	55.60	-1717.69	-207.38	1013.46	0	-321.01	1.8	-501.08	1.8	-474.96	2.12	-502.88
45	46	57.00	-1717.69	-212.27	1316.55	0	-57.42	1.8	-552.82	1.8	-524.39	2.12	-602.81
46	46	57.00	-942.63	-211.31	945.47	0	-168.33	1.8	-275.42	1.8	-270.78	2.12	-285.17
46	47	58.40	-945.05	-172.28	1211.26	0	46.27	1.8	-316.48	1.8	-312.27	2.12	-367.68
47	47	58.40	-1208.44	-171.88	1103.64	0	-205.55	1.8	-296.17	1.8	-316.76	2.12	-348.92
47	48	59.80	-1208.44	-129.46	1310.30	0	-54.48	1.8	-330.78	1.8	-350.48	2.12	-412.03
48	48	59.80	-1208.43	-129.27	1310.42	0	-54.37	1.8	-330.80	1.8	-350.50	2.12	-412.07
48	49	61.20	-1208.43	-83.03	1458.48	0	54.09	1.8	-355.71	1.8	-374.62	2.12	-457.30
49	49	61.20	-1208.44	-82.81	1458.57	0	54.16	1.8	-355.73	1.8	-374.64	2.12	-457.33
49	50	62.60	-1208.44	-46.39	1549.80	0	121.42	1.8	-371.29	1.8	-389.46	2.12	-485.26
50	50	62.60	-1208.44	-46.15	1549.84	0	121.46	1.8	-371.30	1.8	-389.47	2.12	-485.27
50	51	64.00	-1206.69	0.41	1580.20	0	145.66	1.8	-376.56	1.8	-394.07	2.12	-494.50
51	51	64.00	-1206.69	0.60	1580.21	0	145.67	1.8	-376.56	1.8	-394.07	2.12	-494.50
51	52	65.40	-1206.69	42.51	1554.88	0	128.17	1.8	-372.86	1.8	-389.80	2.12	-486.86
52	52	65.40	-1206.69	42.75	1554.82	0	128.11	1.8	-372.84	1.8	-389.79	2.12	-486.84
52	53	66.80	-1206.69	79.19	1468.76	0	66.23	1.8	-359.03	1.8	-375.57	2.12	-460.62
53	53	66.80	-1206.69	79.39	1468.65	0	66.13	1.8	-359.00	1.8	-375.55	2.12	-460.58
53	54	68.20	-1206.69	125.60	1325.59	0	-37.08	1.8	-335.80	1.8	-351.99	2.12	-417.00
54	54	68.20	-1206.69	125.79	1325.48	0	-37.18	1.8	-335.78	1.8	-351.97	2.12	-416.97
54	55	69.60	-1206.69	168.21	1123.99	0	-182.89	1.8	-302.92	1.8	-318.85	2.12	-355.56
55	55	69.60	-941.94	167.37	1231.64	0	83.23	1.8	-323.17	1.8	-314.42	2.12	-376.38
55	56	71.00	-941.07	206.92	971.31	0	-124.32	1.8	-283.84	1.8	-273.72	2.12	-296.01
56	56	71.00	-1717.69	208.28	1342.39	0	-33.76	1.8	-556.08	1.8	-527.96	2.12	-610.84
56	57	72.40	-1717.69	197.10	1042.41	0	-293.46	1.8	-505.76	1.8	-479.88	2.12	-513.10
57	57	72.40	-1424.17	197.07	1168.86	0	125.52	1.8	-485.43	1.8	-461.11	2.12	-559.15
57	58	73.80	-1424.17	206.60	889.30	0	-114.99	1.8	-440.78	1.8	-416.69	2.12	-468.66
58	58	73.80	-2196.08	205.86	1259.85	0	-28.34	1.8	-676.74	1.8	-628.20	2.12	-731.77
58	59	75.20	-2196.08	184.92	990.28	0	-254.31	1.8	-641.16	1.8	-590.27	2.12	-650.97
59	59	75.20	-1967.78	184.41	1096.00	0	77.40	1.8	-625.81	1.8	-576.72	2.12	-688.99
59	60	76.60	-1971.61	189.37	833.20	0	-138.29	1.8	-599.26	1.8	-545.26	2.12	-617.20
60	60	76.60	-1971.55	188.93	833.33	0	-138.15	1.8	-599.27	1.8	-545.26	2.12	-617.23
60	61	78.00	-1971.55	204.51	553.56	0	-363.84	1.8	-573.56	1.8	-512.71	2.12	-542.41
61	1061	78.00	-1938.62	-184.23	570.01	0	-315.31	1.8	-571.35	1.8	-510.89	2.12	-548.16
61	62	79.10	-1938.62	-178.96	770.21	0	-153.96	1.8	-590.29	1.8	-534.12	2.12	-601.57
62	62	79.10	-1938.24	-179.34	770.19	0	-153.86	1.8	-590.19	1.8	-534.04	2.12	-601.48
62	63	80.20	-1938.24	-177.31	966.60	0	7.13	1.8	-612.19	1.8	-558.84	2.12	-656.55
63	63	80.20	-2165.99	-177.35	859.14	0	-325.68	1.8	-627.47	1.8	-572.09	2.12	-618.00
63	64	81.30	-2165.99	-175.35	1054.40	0	-162.77	1.8	-652.96	1.8	-599.06	2.12	-675.79
64	64	81.30	-2165.29	-175.36	1054.80	0	-162.17	1.8	-652.92	1.8	-599.01	2.12	-675.84
64	65	82.40	-2165.29	-177.73	1256.20	0	9.69	1.8	-684.01	1.8	-629.97	2.12	-739.60
65	65	82.40	-1555.58	-177.77	811.21	0	-312.92	1.8	-458.72	1.8	-428.03	2.12	-449.37
65	66	83.50	-1555.58	-162.09	1001.19	0	-149.10	1.8	-490.28	1.8	-458.53	2.12	-511.24
66	66	83.50	-1554.62	-162.31	1001.27	0	-207.19	1.8	-433.05	1.8	-408.82	2.12	-443.72
66	67	84.60	-1554.62	-162.02	1189.18	0	-51.71	1.8	-457.89	1.8	-432.72	2.12	-496.53
67	67	84.60	-775.78	-159.77	817.97	0	-81.84	1.8	-245.18	1.8	-231.59	2.12	-253.76
67	68	85.70	-776.65	-127.08	974.24	0	37.34	1.8	-267.63	1.8	-255.91	2.12	-300.99
68	68	85.70	-945.78	-128.92	902.02	0	-118.87	1.8	-244.62	1.8	-253.88	2.12	-287.18
68	69	86.80	-945.78	-96.14	1021.78	0	-36.39	1.8	-262.91	1.8	-273.46	2.12	-322.84
69	69	86.80	-945.79	-96.06	1021.84	0	-36.34	1.8	-262.93	1.8	-273.47	2.12	-322.86
69	70	87.90	-945.79	-63.56	1108.15	0	22.05	1.8	-275.76	1.8	-287.58	2.12	-348.37
70	70	87.90	-945.79	-63.45	1108.18	0	22.08	1.8	-275.77	1.8	-287.59	2.12	-348.38
70	71	89.00	-945.79	-30.75	1156.89	0	53.00	1.8	-282.34	1.8	-295.54	2.12	-362.39
71	71	89.00	-945.79	-30.68	1156.91	0	53.01	1.8	-282.35	1.8	-295.54	2.12	-362.40
71	72	90.10	-945.79	2.12	1168.54	0	56.87	1.8	-282.76	1.8	-297.41	2.12	-365.07
72	72	90.10	-945.79	2.20	1168.50	0	56.84	1.8	-282.75	1.8	-297.40	2.12	-365.06
72	73	91.20	-945.79	34.81	1143.25	0	33.80	1.8	-277.05	1.8	-293.23	2.12	-356.47
73	73	91.20	-945.79	34.86	1143.21	0	33.77	1.8	-277.04	1.8	-293.22	2.12	-356.46
73	74	92.30	-945.79	67.31	1086.15	0	-12.01	1.8	-266.20	1.8	-283.86	2.12	-338.25
74	74	92.30	-945.79	67.32	1086.09	0	-12.07	1.8	-266.19	1.8	-283.85	2.12	-338.23
74	75	93.40	-945.79	100.02	990.94	0	-85.73	1.8	-248.99	1.8	-268.24	2.12	-308.35
75	75	93.40	-945.79	99.95	990.86	0	-170.45	1.8	-278.39	1.8	-277.54	2.12	-292.60
75	76	94.50	-945.79	132.72	858.50	0	-283.11	1.8	-256.50	1.8	-256.71	2.12	-250.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-782.72	132.64	930.68	0	-49.48	1.8	-245.03	1.8	-246.10	2.12	-276.10
76	77	95.60	-782.72	166.98	761.20	0	-193.15	1.8	-217.70	1.8	-219.64	2.12	-222.38
77	77	95.60	-782.72	166.86	761.09	0	-193.24	1.8	-217.67	1.8	-219.62	2.12	-222.34
77	78	96.70	-782.72	204.44	560.05	0	-363.12	1.8	-185.97	1.8	-188.47	2.12	-158.92
78	78	96.70	-619.65	204.28	633.84	0	-128.24	1.8	-174.57	1.8	-178.07	2.12	-185.05
78	79	97.80	-619.65	236.93	395.36	0	-329.39	1.8	-137.37	1.8	-141.24	2.12	-109.97
79	79	97.80	-619.65	236.69	395.25	0	-329.48	1.8	-137.34	1.8	-141.22	2.12	-109.94
79	80	98.90	-619.65	269.41	119.53	0	-561.75	1.8	-94.68	1.8	-98.76	2.12	-23.28
80	80	98.90	-391.36	269.09	227.41	0	-229.36	1.8	-78.90	1.8	-84.78	2.12	-61.14
80	81	100.00	-391.36	164.05	-85.30	0	-492.43	1.8	-30.95	1.8	-36.74	2.12	36.97
101	101	0.00	-391.36	-178.20	-85.37	0	-492.49	1.8	-30.93	1.8	-36.73	2.12	36.99
101	102	1.10	-395.79	-284.19	244.21	0	-218.85	1.8	-82.96	1.8	-88.48	2.12	-67.05
102	102	1.10	-624.09	-283.31	135.90	0	-551.62	1.8	-98.66	1.8	-102.39	2.12	-29.05
102	103	2.20	-624.09	-249.42	425.60	0	-307.04	1.8	-144.32	1.8	-147.40	2.12	-120.57
103	103	2.20	-624.08	-248.67	425.32	0	-307.28	1.8	-144.26	1.8	-147.35	2.12	-120.47
103	104	3.30	-624.08	-214.88	675.00	0	-96.27	1.8	-183.86	1.8	-186.23	2.12	-199.44
104	104	3.30	-787.15	-214.21	600.85	0	-331.46	1.8	-195.19	1.8	-196.57	2.12	-173.19
104	105	4.40	-787.15	-180.33	811.15	0	-153.44	1.8	-228.86	1.8	-229.40	2.12	-239.83
105	105	4.40	-787.15	-179.82	810.88	0	-153.67	1.8	-228.80	1.8	-229.35	2.12	-239.74
105	106	5.50	-787.15	-138.13	988.08	0	-3.23	1.8	-257.76	1.8	-257.20	2.12	-296.13
106	106	5.50	-950.22	-137.75	915.61	0	-237.12	1.8	-269.16	1.8	-267.76	2.12	-270.35
106	107	6.60	-950.22	-103.85	1053.64	0	-119.49	1.8	-292.23	1.8	-289.61	2.12	-314.48
107	107	6.60	-950.22	-103.52	1053.49	0	-32.70	1.8	-262.65	1.8	-280.20	2.12	-330.44
107	108	7.70	-950.22	-69.69	1152.33	0	44.16	1.8	-280.59	1.8	-296.45	2.12	-361.57
108	108	7.70	-950.22	-69.42	1152.25	0	44.09	1.8	-280.58	1.8	-296.44	2.12	-361.54
108	109	8.80	-950.22	-35.61	1211.97	0	92.02	1.8	-291.93	1.8	-306.25	2.12	-380.61
109	109	8.80	-950.22	-35.41	1211.92	0	91.98	1.8	-291.92	1.8	-306.24	2.12	-380.59
109	110	9.90	-950.22	-1.58	1237.71	0	115.23	1.8	-297.68	1.8	-310.48	2.12	-389.30
110	110	9.90	-950.22	-1.40	1237.68	0	115.20	1.8	-297.68	1.8	-310.47	2.12	-389.29
110	111	11.00	-950.22	32.52	1225.36	0	110.36	1.8	-297.04	1.8	-308.44	2.12	-386.28
111	111	11.00	-950.22	32.68	1225.37	0	110.37	1.8	-297.05	1.8	-308.44	2.12	-386.28
111	112	12.10	-950.22	66.52	1174.41	0	76.99	1.8	-289.91	1.8	-300.03	2.12	-371.37
112	112	12.10	-950.22	66.68	1174.46	0	77.04	1.8	-289.92	1.8	-300.04	2.12	-371.39
112	113	13.20	-950.22	100.44	1084.86	0	15.13	1.8	-276.28	1.8	-285.26	2.12	-344.58
113	113	13.20	-950.22	100.56	1084.93	0	15.19	1.8	-276.29	1.8	-285.28	2.12	-344.60
113	114	14.30	-950.22	134.43	960.21	0	-72.38	1.8	-256.83	1.8	-264.73	2.12	-307.04
114	114	14.30	-780.33	135.23	1032.61	0	85.00	1.8	-279.81	1.8	-266.68	2.12	-320.95
114	115	15.40	-775.77	166.49	868.87	0	-37.57	1.8	-255.39	1.8	-240.39	2.12	-270.91
115	115	15.40	-1554.62	168.80	1240.31	0	-7.24	1.8	-468.27	1.8	-441.70	2.12	-513.91
115	116	16.50	-1554.62	175.42	1045.08	0	-169.44	1.8	-441.29	1.8	-415.98	2.12	-457.98
116	116	16.50	-1554.62	175.84	1045.29	0	-106.07	1.8	-502.99	1.8	-469.56	2.12	-530.87
116	117	17.60	-1554.62	192.32	839.67	0	-286.01	1.8	-465.70	1.8	-434.08	2.12	-460.67
117	117	17.60	-2163.46	192.70	1285.30	0	37.42	1.8	-690.90	1.8	-635.97	2.12	-750.98
117	118	18.70	-2163.46	180.30	1072.92	0	-146.28	1.8	-655.18	1.8	-601.02	2.12	-680.72
118	118	18.70	-2163.46	180.54	1072.70	0	-146.49	1.8	-655.12	1.8	-600.97	2.12	-680.63
118	119	19.80	-2163.46	173.43	876.81	0	-311.36	1.8	-627.83	1.8	-572.48	2.12	-620.77
119	119	19.80	-1935.17	173.28	984.60	0	21.92	1.8	-612.53	1.8	-559.20	2.12	-659.37
119	120	20.90	-1935.17	167.42	797.00	0	-132.08	1.8	-591.28	1.8	-535.09	2.12	-606.24
120	120	20.90	-1935.17	166.97	797.00	0	-132.08	1.8	-591.28	1.8	-535.09	2.12	-606.24
120	121	22.00	-1935.17	176.90	604.97	0	-287.23	1.8	-572.71	1.8	-512.22	2.12	-554.26
121	1121	22.00	-1967.78	-198.05	588.57	0	-335.63	1.8	-574.85	1.8	-513.98	2.12	-548.45
121	122	23.40	-1967.78	-185.61	860.19	0	-115.79	1.8	-600.60	1.8	-546.51	2.12	-622.29
122	122	23.40	-1967.78	-186.17	860.22	0	-115.76	1.8	-600.60	1.8	-546.51	2.12	-622.30
122	123	24.80	-1967.78	-182.26	1120.25	0	97.94	1.8	-629.41	1.8	-579.93	2.12	-696.02
123	123	24.80	-2196.07	-183.05	1014.39	0	-233.92	1.8	-644.70	1.8	-593.42	2.12	-657.92
123	124	26.20	-2196.07	-213.33	1284.46	0	-5.87	1.8	-682.31	1.8	-633.08	2.12	-741.03
124	124	26.20	-1424.17	-213.05	913.49	0	-92.94	1.8	-446.21	1.8	-421.45	2.12	-477.71
124	125	27.60	-1424.17	-205.80	1204.27	0	159.77	1.8	-495.73	1.8	-470.05	2.12	-574.98
125	125	27.60	-1717.69	-205.28	1077.31	0	-259.71	1.8	-515.89	1.8	-488.68	2.12	-528.67
125	126	29.00	-1717.69	-215.55	1382.83	0	7.38	1.8	-570.23	1.8	-540.19	2.12	-631.55
126	126	29.00	-941.08	-214.24	1011.37	0	-89.42	1.8	-291.98	1.8	-280.73	2.12	-309.59
126	127	30.40	-945.21	-174.77	1279.96	0	122.83	1.8	-333.53	1.8	-323.50	2.12	-393.09
127	127	30.40	-1210.45	-173.95	1171.98	0	-143.68	1.8	-313.21	1.8	-327.92	2.12	-372.19
127	128	31.80	-1210.45	-129.94	1379.48	0	8.00	1.8	-347.45	1.8	-362.20	2.12	-435.85
128	128	31.80	-1210.45	-129.98	1379.34	0	7.88	1.8	-347.42	1.8	-362.17	2.12	-435.80
128	129	33.20	-1210.45	-81.35	1526.80	0	115.42	1.8	-371.61	1.8	-386.57	2.12	-481.02
129	129	33.20	-1210.45	-81.46	1526.70	0	115.32	1.8	-371.59	1.8	-386.55	2.12	-480.98
129	130	34.60	-1210.45	-44.64	1615.85	0	180.17	1.8	-386.09	1.8	-401.35	2.12	-508.33
130	130	34.60	-1210.45	-44.76	1615.80	0	180.12	1.8	-386.08	1.8	-401.35	2.12	-508.31
130	131	36.00	-1210.45	-1.18	1642.00	0	198.45	1.8	-389.97	1.8	-405.77	2.12	-516.27
131	131	36.00	-1210.45	-1.32	1641.98	0	198.44	1.8	-389.97	1.8	-405.77	2.12	-516.26
131	132	37.40	-1210.45	47.91	1611.43	0	175.34	1.8	-384.47	1.8	-400.88	2.12	-506.85
132	132	37.40	-1210.45	47.77	1611.47	0	175.37	1.8	-384.48	1.8	-400.88	2.12	-506.87
132	133	38.80	-1210.45	84.57	1517.87	0	105.70	1.8	-368.36	1.8	-385.60	2.12	-478.04
133	133	38.80	-1210.45	84.46	1517.98	0	105.80	1.8	-368.39	1.8	-385.62	2.12	-478.08

Combi_ti.xls

Programa DINTEL PACADAR S.A.
INFRECUENTESG.Tinf.MZ+

11/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1210.45	133.10	1366.28	0	-6.42	1.8	-342.61	1.8	-360.78	2.12	-431.45
134	134	40.20	-1210.45	133.04	1366.42	0	-6.30	1.8	-342.64	1.8	-360.80	2.12	-431.50
134	135	41.60	-1210.45	177.00	1154.52	0	-162.78	1.8	-306.79	1.8	-326.05	2.12	-366.37
135	135	41.60	-946.85	178.25	1262.50	0	89.41	1.8	-327.18	1.8	-321.62	2.12	-385.25
135	136	43.00	-942.63	217.97	988.45	0	-130.93	1.8	-284.10	1.8	-278.25	2.12	-299.70
136	136	43.00	-1717.69	218.82	1359.92	0	-13.61	1.8	-567.62	1.8	-537.20	2.12	-624.61
136	137	44.40	-1717.69	216.70	1050.20	0	-285.60	1.8	-511.61	1.8	-484.11	2.12	-519.13
137	137	44.40	-1424.16	217.14	1177.24	0	133.97	1.8	-491.47	1.8	-465.51	2.12	-565.47
137	138	45.80	-1424.16	227.04	867.40	0	-137.14	1.8	-437.00	1.8	-412.46	2.12	-460.10
138	138	45.80	-2196.07	227.55	1238.30	0	-50.14	1.8	-673.08	1.8	-624.07	2.12	-723.39
138	139	47.20	-2196.07	203.06	942.04	0	-303.48	1.8	-628.44	1.8	-578.16	2.12	-628.99
139	139	47.20	-1967.78	203.20	1047.63	0	28.12	1.8	-613.07	1.8	-564.60	2.12	-666.97
139	140	48.60	-1974.23	200.25	765.69	0	-208.66	1.8	-579.98	1.8	-527.38	2.12	-585.17
140	140	48.60	-1974.41	199.66	765.76	0	-208.65	1.8	-580.04	1.8	-527.43	2.12	-585.23
140	141	50.00	-1974.41	211.15	474.21	0	-447.82	1.8	-548.96	1.8	-490.13	2.12	-502.77
141	1141	50.00	-1974.19	-211.22	474.22	0	-447.75	1.8	-548.90	1.8	-490.08	2.12	-502.72
141	142	51.40	-1974.19	-199.74	765.87	0	-208.49	1.8	-579.99	1.8	-527.39	2.12	-585.21
142	142	51.40	-1973.59	-200.33	765.83	0	-208.36	1.8	-579.84	1.8	-527.25	2.12	-585.06
142	143	52.80	-1973.59	-202.78	1047.77	0	26.58	1.8	-614.54	1.8	-565.92	2.12	-668.28
143	143	52.80	-2200.88	-202.71	942.08	0	-304.81	1.8	-629.65	1.8	-579.25	2.12	-630.05
143	144	54.20	-2196.07	-227.55	1238.28	0	-50.15	1.8	-673.08	1.8	-624.07	2.12	-723.39
144	144	54.20	-1424.17	-227.05	867.39	0	-137.15	1.8	-437.00	1.8	-412.46	2.12	-460.10
144	145	55.60	-1424.17	-217.15	1177.25	0	133.98	1.8	-491.48	1.8	-465.51	2.12	-565.48
145	145	55.60	-1717.69	-216.72	1050.21	0	-285.59	1.8	-511.61	1.8	-484.11	2.12	-519.14
145	146	57.00	-1717.69	-218.82	1359.96	0	-13.57	1.8	-567.64	1.8	-537.21	2.12	-624.63
146	146	57.00	-942.63	-217.99	988.48	0	-130.91	1.8	-284.11	1.8	-278.26	2.12	-299.71
146	147	58.40	-945.05	-177.36	1261.65	0	90.33	1.8	-326.92	1.8	-321.22	2.12	-384.93
147	147	58.40	-1208.44	-177.08	1153.66	0	-161.68	1.8	-306.51	1.8	-325.62	2.12	-366.04
147	148	59.80	-1208.44	-133.11	1365.64	0	-5.15	1.8	-342.36	1.8	-360.39	2.12	-431.18
148	148	59.80	-1208.45	-133.17	1365.51	0	-5.27	1.8	-342.34	1.8	-360.36	2.12	-431.14
148	149	61.20	-1208.45	-84.53	1517.25	0	106.97	1.8	-368.12	1.8	-385.21	2.12	-477.79
149	149	61.20	-1208.44	-84.64	1517.16	0	106.89	1.8	-368.09	1.8	-385.19	2.12	-477.75
149	150	62.60	-1208.44	-47.83	1610.88	0	176.65	1.8	-384.23	1.8	-400.50	2.12	-506.61
150	150	62.60	-1208.44	-47.97	1610.84	0	176.62	1.8	-384.22	1.8	-400.49	2.12	-506.60
150	151	64.00	-1206.69	1.24	1641.46	0	201.20	1.8	-389.57	1.8	-405.15	2.12	-515.96
151	151	64.00	-1206.69	1.10	1641.47	0	201.20	1.8	-389.57	1.8	-405.15	2.12	-515.96
151	152	65.40	-1206.69	44.68	1615.38	0	182.94	1.8	-385.68	1.8	-400.74	2.12	-508.03
152	152	65.40	-1206.69	44.55	1615.42	0	182.98	1.8	-385.69	1.8	-400.75	2.12	-508.05
152	153	66.80	-1206.69	81.36	1526.41	0	118.23	1.8	-371.21	1.8	-385.97	2.12	-480.74
153	153	66.80	-1206.69	81.28	1526.51	0	118.33	1.8	-371.24	1.8	-385.98	2.12	-480.78
153	154	68.20	-1206.69	129.90	1379.15	0	10.84	1.8	-347.05	1.8	-361.61	2.12	-435.59
154	154	68.20	-1206.69	129.85	1379.27	0	10.96	1.8	-347.08	1.8	-361.63	2.12	-435.64
154	155	69.60	-1206.69	173.85	1171.90	0	-140.63	1.8	-312.86	1.8	-327.37	2.12	-372.02
155	155	69.60	-941.94	172.89	1279.88	0	125.47	1.8	-333.22	1.8	-323.03	2.12	-392.93
155	156	71.00	-941.07	214.23	1011.40	0	-89.39	1.8	-291.99	1.8	-280.73	2.12	-309.60
156	156	71.00	-1717.69	215.56	1382.87	0	7.42	1.8	-570.24	1.8	-540.20	2.12	-631.56
156	157	72.40	-1717.69	205.28	1077.33	0	-259.70	1.8	-515.89	1.8	-488.68	2.12	-528.68
157	157	72.40	-1424.17	205.81	1204.27	0	159.77	1.8	-495.73	1.8	-470.05	2.12	-574.98
157	158	73.80	-1424.17	213.05	913.48	0	-92.95	1.8	-446.21	1.8	-421.44	2.12	-477.70
158	158	73.80	-2196.07	213.34	1284.44	0	-5.88	1.8	-682.31	1.8	-633.08	2.12	-741.02
158	159	75.20	-2196.07	183.05	1014.37	0	-233.94	1.8	-644.70	1.8	-593.42	2.12	-657.91
159	159	75.20	-1967.78	182.25	1120.25	0	97.94	1.8	-629.41	1.8	-579.93	2.12	-696.02
159	160	76.60	-1971.61	185.70	860.75	0	-116.41	1.8	-601.63	1.8	-547.43	2.12	-623.28
160	160	76.60	-1971.55	185.12	860.79	0	-116.36	1.8	-601.62	1.8	-547.42	2.12	-623.28
160	161	78.00	-1971.55	197.56	589.87	0	-335.62	1.8	-575.96	1.8	-514.97	2.12	-549.63
161	1161	78.00	-1938.62	-176.75	606.30	0	-287.10	1.8	-573.74	1.8	-513.14	2.12	-555.37
161	162	79.10	-1938.62	-166.83	798.14	0	-132.12	1.8	-592.28	1.8	-535.99	2.12	-607.30
162	162	79.10	-1938.23	-167.26	798.11	0	-132.03	1.8	-592.18	1.8	-535.90	2.12	-607.20
162	163	80.20	-1938.23	-173.13	985.58	0	21.87	1.8	-613.42	1.8	-560.00	2.12	-660.30
163	163	80.20	-2165.99	-173.27	877.75	0	-311.30	1.8	-628.58	1.8	-573.15	2.12	-621.58
163	164	81.30	-2165.99	-180.38	1073.49	0	-146.54	1.8	-655.86	1.8	-601.63	2.12	-681.40
164	164	81.30	-2165.29	-180.15	1073.65	0	-146.19	1.8	-655.73	1.8	-601.52	2.12	-681.32
164	165	82.40	-2165.29	-192.55	1285.87	0	37.37	1.8	-691.43	1.8	-636.45	2.12	-751.53
165	165	82.40	-1555.58	-192.22	840.49	0	-285.62	1.8	-466.01	1.8	-434.39	2.12	-461.11
165	166	83.50	-1555.58	-175.74	1045.65	0	-106.04	1.8	-503.28	1.8	-469.82	2.12	-531.18
166	166	83.50	-1554.62	-175.41	1045.35	0	-169.21	1.8	-441.33	1.8	-416.01	2.12	-458.05
166	167	84.60	-1554.62	-168.81	1240.59	0	-7.01	1.8	-468.31	1.8	-441.73	2.12	-513.98
167	167	84.60	-775.78	-166.47	869.14	0	-37.39	1.8	-255.42	1.8	-240.43	2.12	-270.99
167	168	85.70	-776.65	-132.75	1031.50	0	87.30	1.8	-279.34	1.8	-265.97	2.12	-320.47
168	168	85.70	-945.79	-134.51	959.11	0	-69.46	1.8	-256.29	1.8	-263.91	2.12	-306.53
168	169	86.80	-945.79	-100.64	1083.94	0	18.19	1.8	-275.77	1.8	-284.48	2.12	-344.13
169	169	86.80	-945.79	-100.52	1083.83	0	18.09	1.8	-275.75	1.8	-284.46	2.12	-344.09
169	170	87.90	-945.79	-66.78	1173.55	0	80.09	1.8	-289.40	1.8	-299.26	2.12	-370.94
170	170	87.90	-945.79	-66.61	1173.49	0	80.03	1.8	-289.39	1.8	-299.24	2.12	-370.92
170	171	89.00	-945.79	-32.77	1224.54	0	113.47	1.8	-296.54	1.8	-307.67	2.12	-385.86

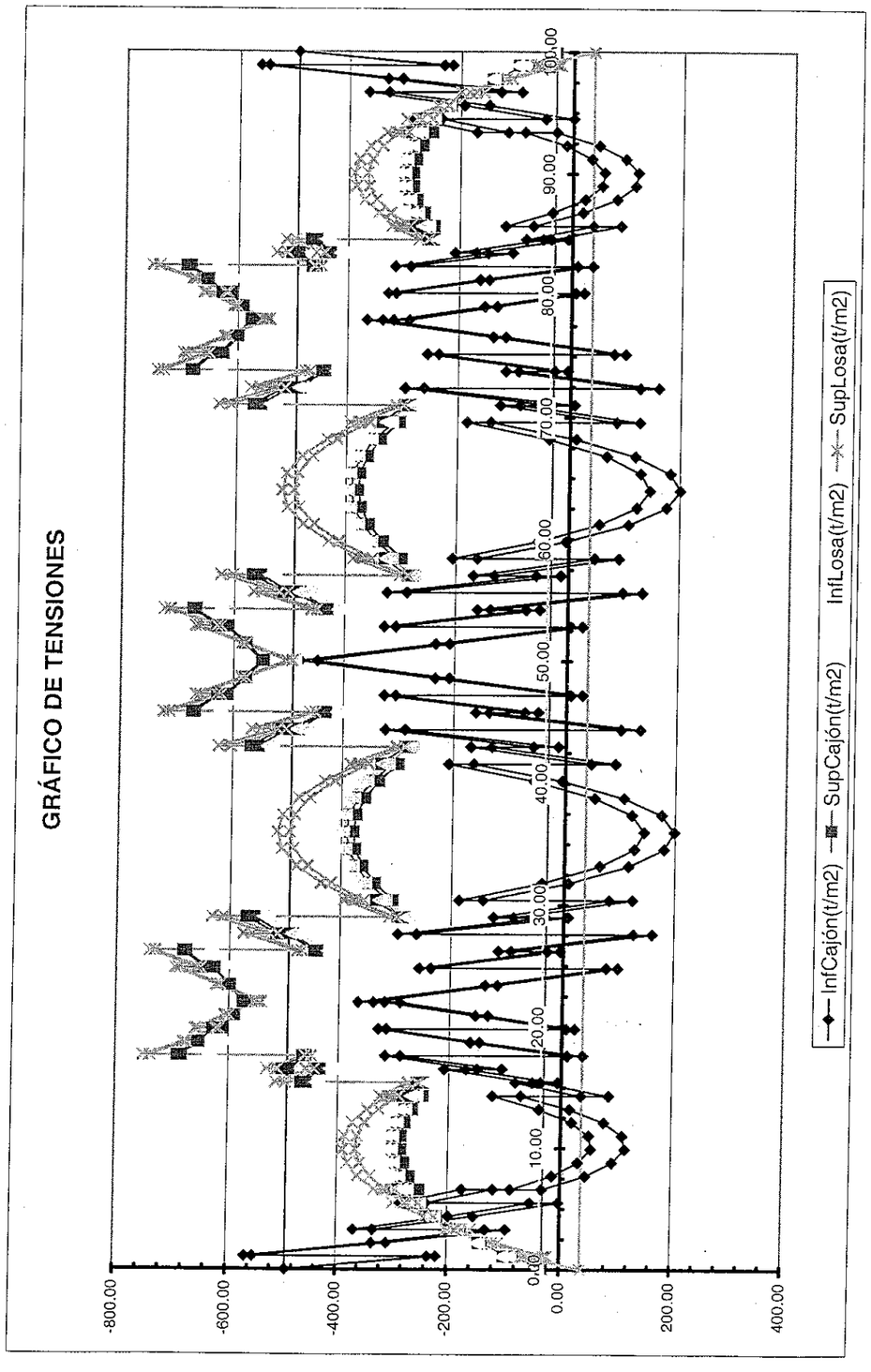
CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-945.79	-32.64	1224.52	0	113.45	1.8	-296.54	1.8	-307.66	2.12	-385.85
171	172	90.10	-945.79	1.31	1236.91	0	118.35	1.8	-297.18	1.8	-309.72	2.12	-388.89
172	172	90.10	-945.79	1.47	1236.94	0	118.37	1.8	-297.18	1.8	-309.72	2.12	-388.89
172	173	91.20	-945.79	35.32	1211.23	0	95.17	1.8	-291.43	1.8	-305.49	2.12	-380.21
173	173	91.20	-945.79	35.50	1211.29	0	95.22	1.8	-291.44	1.8	-305.50	2.12	-380.23
173	174	92.30	-945.79	69.32	1151.67	0	47.35	1.8	-280.10	1.8	-295.71	2.12	-361.19
174	174	92.30	-945.79	69.61	1151.75	0	47.42	1.8	-280.12	1.8	-295.73	2.12	-361.22
174	175	93.40	-945.79	103.44	1053.00	0	-29.38	1.8	-262.18	1.8	-279.48	2.12	-330.12
175	175	93.40	-945.79	103.76	1053.14	0	-115.61	1.8	-291.74	1.8	-288.91	2.12	-314.28
175	176	94.50	-945.79	137.67	915.20	0	-233.17	1.8	-268.67	1.8	-267.07	2.12	-270.18
176	176	94.50	-782.72	138.03	987.67	0	0.73	1.8	-257.27	1.8	-256.52	2.12	-295.96
176	177	95.60	-782.72	179.71	810.56	0	-149.65	1.8	-228.31	1.8	-228.68	2.12	-239.59
177	177	95.60	-782.72	180.22	810.81	0	-149.43	1.8	-228.37	1.8	-228.72	2.12	-239.68
177	178	96.70	-782.72	214.11	600.60	0	-327.38	1.8	-194.70	1.8	-195.90	2.12	-173.06
178	178	96.70	-619.65	214.76	674.76	0	-92.17	1.8	-183.37	1.8	-185.56	2.12	-199.32
178	179	97.80	-619.65	248.56	425.13	0	-303.16	1.8	-143.77	1.8	-146.69	2.12	-120.36
179	179	97.80	-619.66	249.32	425.42	0	-302.91	1.8	-143.84	1.8	-146.75	2.12	-120.46
179	180	98.90	-619.66	283.22	135.81	0	-547.41	1.8	-98.19	1.8	-101.74	2.12	-28.96
180	180	98.90	-391.36	284.09	244.13	0	-214.63	1.8	-82.49	1.8	-87.83	2.12	-66.97
180	181	100.00	-391.36	178.19	-85.37	0	-492.49	1.8	-30.93	1.8	-36.73	2.12	36.99



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
1	1	0.00	-441.09	-254.60	-105.50	0	-556.59	1.8	-34.81	1.8	-41.12	2.12	42.18
1	2	1.10	-436.66	-114.78	31.54	0	-440.02	1.8	-49.34	1.8	-59.65	2.12	1.54
2	2	1.10	-693.96	-115.00	-94.84	0	-815.12	1.8	-67.05	1.8	-75.31	2.12	44.34
2	3	2.20	-693.96	-96.99	21.77	0	-719.47	1.8	-79.84	1.8	-91.60	2.12	9.73
3	3	2.20	-693.96	-97.22	21.73	0	-719.49	1.8	-79.83	1.8	-91.60	2.12	9.74
3	4	3.30	-693.96	-79.22	118.76	0	-639.81	1.8	-90.44	1.8	-105.12	2.12	-19.04
4	4	3.30	-877.74	-79.46	32.16	0	-904.88	1.8	-103.24	1.8	-116.78	2.12	10.51
4	5	4.40	-877.74	-61.48	109.68	0	-841.11	1.8	-111.70	1.8	-127.55	2.12	-12.46
5	5	4.40	-877.74	-61.74	109.66	0	-841.13	1.8	-111.70	1.8	-127.55	2.12	-12.45
5	6	5.50	-877.74	-43.74	167.65	0	-793.28	1.8	-117.99	1.8	-135.57	2.12	-29.60
6	6	5.50	-1061.53	-44.01	82.89	0	-1056.92	1.8	-130.87	1.8	-147.47	2.12	-0.58
6	7	6.60	-1061.53	-26.01	121.43	0	-1024.94	1.8	-135.01	1.8	-152.74	2.12	-11.93
7	7	6.60	-1061.53	-26.33	121.38	0	-865.86	1.8	-97.96	1.8	-139.23	2.12	-35.91
7	8	7.70	-1061.53	-8.34	140.44	0	-853.73	1.8	-100.50	1.8	-142.01	2.12	-41.16
8	8	7.70	-1061.53	-8.65	140.41	0	-853.75	1.8	-100.49	1.8	-142.01	2.12	-41.15
8	9	8.80	-1061.53	9.58	140.03	0	-854.80	1.8	-100.20	1.8	-141.62	2.12	-40.66
9	9	8.80	-1061.54	9.14	139.98	0	-854.84	1.8	-100.19	1.8	-141.62	2.12	-40.65
9	10	9.90	-1061.54	27.24	120.00	0	-869.21	1.8	-97.05	1.8	-138.05	2.12	-34.37
10	10	9.90	-1061.53	26.85	119.99	0	-869.21	1.8	-97.04	1.8	-138.04	2.12	-34.36
10	11	11.00	-1061.53	44.84	80.55	0	-896.78	1.8	-91.07	1.8	-131.31	2.12	-22.34
11	11	11.00	-1061.53	44.40	80.53	0	-896.80	1.8	-91.06	1.8	-131.31	2.12	-22.33
11	12	12.10	-1061.53	62.42	21.77	0	-937.45	1.8	-82.28	1.8	-121.44	2.12	-4.61
12	12	12.10	-1061.53	61.98	21.74	0	-937.48	1.8	-82.28	1.8	-121.43	2.12	-4.61
12	13	13.20	-1061.53	80.04	-56.41	0	-991.27	1.8	-70.69	1.8	-108.41	2.12	18.83
13	13	13.20	-1061.53	79.59	-56.42	0	-991.29	1.8	-70.68	1.8	-108.40	2.12	18.84
13	14	14.30	-1061.53	97.61	-153.90	0	-1058.17	1.8	-56.29	1.8	-92.24	2.12	47.98
14	14	14.30	-871.84	92.50	-69.18	0	-947.74	1.8	-85.11	1.8	-96.92	2.12	39.52
14	15	15.40	-874.66	112.99	-184.67	0	-1035.47	1.8	-70.09	1.8	-79.44	2.12	73.73
15	15	15.40	-1567.05	114.87	144.76	0	-1016.57	1.8	-262.34	1.8	-263.06	2.12	-146.45
15	16	16.50	-1567.05	165.29	3.21	0	-1132.84	1.8	-244.85	1.8	-245.62	2.12	-107.40
16	16	16.50	-1567.05	165.00	3.30	0	-1168.43	1.8	-210.06	1.8	-215.40	2.12	-66.31
16	17	17.60	-1567.05	193.96	-192.23	0	-1332.10	1.8	-183.41	1.8	-188.99	2.12	-9.13
17	17	17.60	-2068.15	193.43	224.33	0	-988.54	1.8	-380.17	1.8	-365.40	2.12	-272.68
17	18	18.70	-2068.15	235.79	-11.29	0	-1187.40	1.8	-346.35	1.8	-331.91	2.12	-201.59
18	18	18.70	-2068.15	235.31	-10.88	0	-1187.01	1.8	-346.46	1.8	-332.00	2.12	-201.76
18	19	19.80	-2068.15	282.49	-294.36	0	-1428.51	1.8	-303.29	1.8	-289.52	2.12	-113.35
19	19	19.80	-1810.85	282.09	-167.48	0	-1051.94	1.8	-286.24	1.8	-274.70	2.12	-157.16
19	20	20.90	-1810.85	341.16	-515.62	0	-1352.32	1.8	-228.85	1.8	-218.98	2.12	-43.92
20	20	20.90	-1810.85	340.96	-515.60	0	-1352.31	1.8	-228.85	1.8	-218.98	2.12	-43.93
20	21	22.00	-1810.85	390.92	-917.10	0	-1700.36	1.8	-160.87	1.8	-152.94	2.12	88.96
21	1021	22.00	-1847.60	-429.47	-936.16	0	-1754.85	1.8	-163.30	1.8	-154.95	2.12	95.46
21	22	23.40	-1847.60	-376.82	-376.63	0	-1268.61	1.8	-258.47	1.8	-248.09	2.12	-91.25
22	22	23.40	-1847.60	-377.06	-376.49	0	-1268.46	1.8	-258.53	1.8	-248.13	2.12	-91.32
22	23	24.80	-1847.60	-314.77	107.59	0	-848.79	1.8	-339.76	1.8	-327.35	2.12	-251.11
23	23	24.80	-2104.90	-313.47	-16.18	0	-1222.83	1.8	-357.09	1.8	-342.65	2.12	-208.30
23	24	26.20	-2104.90	-240.01	362.17	0	-899.52	1.8	-414.97	1.8	-400.16	2.12	-327.42
24	24	26.20	-1420.02	-239.91	32.15	0	-977.41	1.8	-205.67	1.8	-212.55	2.12	-93.87
24	25	27.60	-1420.02	-184.07	328.27	0	-727.74	1.8	-247.03	1.8	-254.28	2.12	-182.82
25	25	27.60	-1750.84	-184.58	178.48	0	-1201.47	1.8	-269.61	1.8	-275.14	2.12	-130.36
25	26	29.00	-1750.84	-108.82	364.06	0	-1047.38	1.8	-292.63	1.8	-299.37	2.12	-183.56
26	26	29.00	-1061.02	-108.24	34.55	0	-1039.67	1.8	-125.83	1.8	-136.28	2.12	8.50
26	27	30.40	-1058.63	-82.08	170.20	0	-936.39	1.8	-141.60	1.8	-156.19	2.12	-31.15
27	27	30.40	-1356.26	-85.51	43.39	0	-1164.91	1.8	-114.76	1.8	-158.09	2.12	-14.90
27	28	31.80	-1356.26	-62.54	147.03	0	-1096.27	1.8	-129.08	1.8	-175.02	2.12	-45.24
28	28	31.80	-1356.26	-63.13	146.97	0	-1096.30	1.8	-129.07	1.8	-175.01	2.12	-45.22
28	29	33.20	-1356.26	-40.22	219.31	0	-1048.87	1.8	-138.85	1.8	-186.85	2.12	-66.33
29	29	33.20	-1356.26	-40.79	219.29	0	-1048.88	1.8	-138.84	1.8	-186.85	2.12	-66.32
29	30	34.60	-1356.26	-16.63	259.25	0	-1023.53	1.8	-143.87	1.8	-193.42	2.12	-77.85
30	30	34.60	-1356.26	-17.15	259.17	0	-1023.58	1.8	-143.85	1.8	-193.41	2.12	-77.82
30	31	36.00	-1356.26	9.43	263.96	0	-1022.61	1.8	-143.58	1.8	-194.24	2.12	-78.85
31	31	36.00	-1356.26	8.90	263.94	0	-1022.63	1.8	-143.58	1.8	-194.23	2.12	-78.84
31	32	37.40	-1356.26	31.91	235.40	0	-1044.52	1.8	-138.37	1.8	-189.63	2.12	-69.98
32	32	37.40	-1356.26	31.33	235.40	0	-1044.52	1.8	-138.37	1.8	-189.63	2.12	-69.97
32	33	38.80	-1356.26	54.23	175.51	0	-1087.66	1.8	-128.61	1.8	-179.94	2.12	-51.86
33	33	38.80	-1356.26	53.65	175.52	0	-1087.66	1.8	-128.61	1.8	-179.94	2.12	-51.86
33	34	40.20	-1356.26	76.57	84.35	0	-1151.99	1.8	-114.31	1.8	-165.16	2.12	-24.52
34	34	40.20	-1356.26	75.95	84.39	0	-1151.97	1.8	-114.32	1.8	-165.16	2.12	-24.53
34	35	41.60	-1356.26	98.94	-38.01	0	-1237.44	1.8	-95.50	1.8	-145.31	2.12	12.02
35	35	41.60	-1060.58	96.00	88.77	0	-1026.12	1.8	-122.52	1.8	-143.51	2.12	-1.91
35	36	43.00	-1063.03	121.75	-64.36	0	-1148.66	1.8	-102.64	1.8	-120.99	2.12	43.92
36	36	43.00	-1750.84	121.81	265.16	0	-1143.64	1.8	-265.84	1.8	-275.42	2.12	-140.37
36	37	44.40	-1750.84	191.32	58.88	0	-1316.70	1.8	-238.57	1.8	-247.33	2.12	-79.65
37	37	44.40	-1420.02	190.73	208.56	0	-843.08	1.8	-215.96	1.8	-226.44	2.12	-132.06
37	38	45.80	-1420.02	243.67	-92.48	0	-1097.43	1.8	-173.81	1.8	-183.88	2.12	-41.38
38	38	45.80	-2104.90	243.21	237.64	0	-1019.43	1.8	-383.14	1.8	-371.52	2.12	-274.97

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-
C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
38	39	47.20	-2104.90	302.11	-140.25	0	-1342.20	1.8	-326.05	1.8	-314.55	2.12	-156.54
39	39	47.20	-1847.60	301.33	-16.10	0	-967.79	1.8	-308.82	1.8	-299.35	2.12	-199.53
39	40	48.60	-1841.15	377.71	-493.75	0	-1379.24	1.8	-228.60	1.8	-220.81	2.12	-41.79
40	40	48.60	-1840.98	377.42	-493.82	0	-1379.26	1.8	-228.53	1.8	-220.75	2.12	-41.72
40	41	50.00	-1840.98	432.74	-1057.53	0	-1869.34	1.8	-132.92	1.8	-127.08	2.12	146.24
41	1041	50.00	-1841.19	-432.66	-1057.54	0	-1869.41	1.8	-132.97	1.8	-127.13	2.12	146.19
41	42	51.40	-1841.19	-377.34	-493.95	0	-1379.43	1.8	-228.57	1.8	-220.79	2.12	-41.73
42	42	51.40	-1841.79	-377.62	-493.89	0	-1379.54	1.8	-228.74	1.8	-220.94	2.12	-41.89
42	43	52.80	-1841.79	-301.74	-16.24	0	-966.27	1.8	-307.35	1.8	-298.03	2.12	-198.22
43	43	52.80	-2100.09	-302.48	-140.29	0	-1340.87	1.8	-324.84	1.8	-313.47	2.12	-155.48
43	44	54.20	-2104.90	-243.21	237.66	0	-1019.42	1.8	-383.15	1.8	-371.53	2.12	-274.98
44	44	54.20	-1420.02	-243.67	-92.49	0	-1097.43	1.8	-173.81	1.8	-183.88	2.12	-41.38
44	45	55.60	-1420.02	-190.72	208.59	0	-843.05	1.8	-215.97	1.8	-226.45	2.12	-132.07
45	45	55.60	-1750.84	-191.31	58.91	0	-1316.67	1.8	-238.58	1.8	-247.34	2.12	-79.66
45	46	57.00	-1750.84	-121.79	265.18	0	-1143.62	1.8	-265.85	1.8	-275.42	2.12	-140.38
46	46	57.00	-1063.03	-121.76	-64.36	0	-1148.66	1.8	-102.64	1.8	-120.99	2.12	43.92
46	47	58.40	-1062.37	-96.92	89.67	0	-1027.00	1.8	-122.79	1.8	-143.92	2.12	-2.24
47	47	58.40	-1358.27	-98.88	-37.12	0	-1238.51	1.8	-95.79	1.8	-145.75	2.12	11.68
47	48	59.80	-1358.27	-75.90	85.23	0	-1153.07	1.8	-114.61	1.8	-165.59	2.12	-24.86
48	48	59.80	-1358.27	-76.49	85.20	0	-1153.08	1.8	-114.60	1.8	-165.59	2.12	-24.85
48	49	61.20	-1358.27	-53.58	176.24	0	-1088.84	1.8	-128.88	1.8	-180.34	2.12	-52.16
49	49	61.20	-1358.27	-54.17	176.25	0	-1088.83	1.8	-128.88	1.8	-180.35	2.12	-52.16
49	50	62.60	-1358.27	-31.27	236.05	0	-1045.75	1.8	-138.63	1.8	-190.03	2.12	-70.25
50	50	62.60	-1358.27	-31.85	236.04	0	-1045.75	1.8	-138.63	1.8	-190.03	2.12	-70.25
50	51	64.00	-1360.02	-8.82	264.50	0	-1025.35	1.8	-143.99	1.8	-194.86	2.12	-79.16
51	51	64.00	-1360.02	-9.35	264.50	0	-1025.35	1.8	-143.99	1.8	-194.86	2.12	-79.16
51	52	65.40	-1360.02	17.25	259.61	0	-1026.39	1.8	-144.25	1.8	-194.02	2.12	-78.11
52	52	65.40	-1360.02	16.71	259.66	0	-1026.35	1.8	-144.26	1.8	-194.02	2.12	-78.12
52	53	66.80	-1360.02	40.87	219.63	0	-1051.75	1.8	-139.23	1.8	-187.44	2.12	-66.58
53	53	66.80	-1360.02	40.31	219.65	0	-1051.73	1.8	-139.23	1.8	-187.44	2.12	-66.58
53	54	68.20	-1360.02	63.21	147.21	0	-1099.24	1.8	-129.45	1.8	-175.58	2.12	-45.45
54	54	68.20	-1360.02	62.62	147.24	0	-1099.22	1.8	-129.45	1.8	-175.59	2.12	-45.46
54	55	69.60	-1360.02	85.59	43.49	0	-1167.94	1.8	-115.12	1.8	-158.64	2.12	-15.08
55	55	69.60	-1061.89	83.96	170.28	0	-939.03	1.8	-141.91	1.8	-156.67	2.12	-31.31
55	56	71.00	-1061.02	108.24	34.55	0	-1039.67	1.8	-125.83	1.8	-136.28	2.12	8.50
56	56	71.00	-1750.84	108.83	364.06	0	-1047.38	1.8	-292.63	1.8	-299.37	2.12	-183.56
56	57	72.40	-1750.84	184.58	178.48	0	-1201.47	1.8	-269.61	1.8	-275.14	2.12	-130.36
57	57	72.40	-1420.02	184.08	328.24	0	-727.77	1.8	-247.02	1.8	-254.27	2.12	-182.81
57	58	73.80	-1420.02	239.92	32.13	0	-977.43	1.8	-205.67	1.8	-212.55	2.12	-93.87
58	58	73.80	-2104.91	240.02	362.15	0	-899.53	1.8	-414.97	1.8	-400.16	2.12	-327.41
58	59	75.20	-2104.91	313.48	-16.20	0	-1222.84	1.8	-357.09	1.8	-342.65	2.12	-208.29
59	59	75.20	-1847.60	314.76	107.60	0	-848.78	1.8	-339.76	1.8	-327.35	2.12	-251.12
59	60	76.60	-1843.78	377.52	-377.01	0	-1267.81	1.8	-257.50	1.8	-247.21	2.12	-90.35
60	60	76.60	-1843.83	377.31	-377.24	0	-1268.04	1.8	-257.45	1.8	-247.17	2.12	-90.26
60	61	78.00	-1843.83	429.98	-937.46	0	-1754.86	1.8	-162.19	1.8	-153.95	2.12	96.63
61	1061	78.00	-1807.39	-391.07	-918.45	0	-1700.50	1.8	-159.83	1.8	-152.01	2.12	90.08
61	62	79.10	-1807.39	-341.12	-516.78	0	-1352.31	1.8	-227.83	1.8	-218.07	2.12	-42.85
62	62	79.10	-1807.77	-341.34	-516.82	0	-1352.45	1.8	-227.92	1.8	-218.15	2.12	-42.93
62	63	80.20	-1807.77	-282.26	-168.50	0	-1051.92	1.8	-285.34	1.8	-273.90	2.12	-156.21
63	63	80.20	-2065.61	-282.66	-295.35	0	-1428.61	1.8	-302.53	1.8	-288.83	2.12	-112.53
63	64	81.30	-2065.61	-235.48	-11.68	0	-1186.96	1.8	-345.72	1.8	-331.34	2.12	-200.99
64	64	81.30	-2066.31	-235.93	-12.03	0	-1187.49	1.8	-345.80	1.8	-331.41	2.12	-200.99
64	65	82.40	-2066.31	-193.57	223.77	0	-988.49	1.8	-379.64	1.8	-364.92	2.12	-272.13
65	65	82.40	-1566.09	-194.06	-192.35	0	-1331.94	1.8	-183.13	1.8	-188.77	2.12	-8.90
65	66	83.50	-1566.09	-165.10	2.92	0	-1168.49	1.8	-209.76	1.8	-215.13	2.12	-65.99
66	66	83.50	-1567.05	-165.32	2.94	0	-1133.06	1.8	-244.82	1.8	-245.59	2.12	-107.33
66	67	84.60	-1567.05	-114.90	144.51	0	-1016.78	1.8	-262.31	1.8	-263.03	2.12	-146.38
67	67	84.60	-874.65	-113.00	-184.94	0	-1035.64	1.8	-70.05	1.8	-79.39	2.12	73.81
67	68	85.70	-875.52	-94.97	-68.08	0	-950.05	1.8	-85.58	1.8	-97.62	2.12	39.05
68	68	85.70	-1065.95	-97.53	-152.81	0	-1061.11	1.8	-56.82	1.8	-93.05	2.12	47.48
68	69	86.80	-1065.95	-79.51	-55.41	0	-994.27	1.8	-71.21	1.8	-109.20	2.12	18.36
69	69	86.80	-1065.96	-79.96	-55.40	0	-994.26	1.8	-71.21	1.8	-109.21	2.12	18.35
69	70	87.90	-1065.96	-61.90	22.66	0	-940.52	1.8	-82.79	1.8	-122.21	2.12	-5.06
70	70	87.90	-1065.96	-62.34	22.68	0	-940.50	1.8	-82.80	1.8	-122.22	2.12	-5.07
70	71	89.00	-1065.96	-44.33	81.35	0	-899.90	1.8	-91.57	1.8	-132.08	2.12	-22.76
71	71	89.00	-1065.96	-44.78	81.39	0	-899.88	1.8	-91.57	1.8	-132.08	2.12	-22.77
71	72	90.10	-1065.96	-26.78	120.74	0	-872.36	1.8	-97.54	1.8	-138.80	2.12	-34.77
72	72	90.10	-1065.96	-27.17	120.75	0	-872.36	1.8	-97.54	1.8	-138.80	2.12	-34.77
72	73	91.20	-1065.96	-9.08	140.63	0	-858.06	1.8	-100.67	1.8	-142.35	2.12	-41.02
73	73	91.20	-1065.96	-9.52	140.69	0	-858.01	1.8	-100.69	1.8	-142.36	2.12	-41.03
73	74	92.30	-1065.96	8.71	140.99	0	-857.02	1.8	-100.96	1.8	-142.73	2.12	-41.50
74	74	92.30	-1065.96	8.41	141.01	0	-857.00	1.8	-100.97	1.8	-142.74	2.12	-41.50
74	75	93.40	-1065.96	26.40	121.88	0	-869.19	1.8	-98.43	1.8	-139.95	2.12	-36.23
75	75	93.40	-1065.96	26.08	121.92	0	-1028.84	1.8	-135.50	1.8	-153.44	2.12	-12.12
75	76	94.50	-1065.96	44.07	83.30	0	-1060.88	1.8	-131.36	1.8	-148.15	2.12	-0.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
76	76	94.50	-882.17	43.82	168.08	0	-797.23	1.8	-118.49	1.8	-136.26	2.12	-29.78
76	77	95.60	-882.17	61.82	109.98	0	-845.15	1.8	-112.18	1.8	-128.23	2.12	-12.60
77	77	95.60	-882.17	61.55	110.02	0	-845.12	1.8	-112.19	1.8	-128.23	2.12	-12.61
77	78	96.70	-882.17	79.53	32.40	0	-908.97	1.8	-103.73	1.8	-117.45	2.12	10.38
78	78	96.70	-698.39	79.29	119.01	0	-643.89	1.8	-90.93	1.8	-105.79	2.12	-19.16
78	79	97.80	-698.39	97.29	21.90	0	-723.64	1.8	-80.31	1.8	-92.25	2.12	9.64
79	79	97.80	-698.38	97.06	21.93	0	-723.61	1.8	-80.31	1.8	-92.25	2.12	9.63
79	80	98.90	-698.38	115.06	-94.76	0	-819.33	1.8	-67.52	1.8	-75.96	2.12	44.26
80	80	98.90	-441.09	114.84	31.63	0	-444.24	1.8	-49.81	1.8	-60.30	2.12	1.46
80	81	100.00	-441.09	254.58	-105.50	0	-556.59	1.8	-34.81	1.8	-41.12	2.12	42.18
101	101	0.00	-441.09	-251.59	-105.57	0	-556.64	1.8	-34.79	1.8	-41.11	2.12	42.20
101	102	1.10	-436.66	-110.95	27.18	0	-443.62	1.8	-48.68	1.8	-59.05	2.12	2.83
102	102	1.10	-693.96	-111.27	-98.96	0	-818.52	1.8	-66.44	1.8	-74.75	2.12	45.56
102	103	2.20	-693.96	-93.69	13.74	0	-726.10	1.8	-78.63	1.8	-90.49	2.12	12.11
103	103	2.20	-693.96	-93.93	13.93	0	-725.94	1.8	-78.66	1.8	-90.52	2.12	12.05
103	104	3.30	-693.96	-76.39	107.56	0	-649.08	1.8	-88.75	1.8	-103.57	2.12	-15.71
104	104	3.30	-877.74	-76.52	21.16	0	-913.98	1.8	-101.59	1.8	-115.26	2.12	13.77
104	105	4.40	-877.74	-58.99	95.70	0	-852.69	1.8	-109.57	1.8	-125.60	2.12	-8.29
105	105	4.40	-877.74	-59.07	95.82	0	-852.59	1.8	-109.59	1.8	-125.62	2.12	-8.33
105	106	5.50	-877.74	-41.52	151.13	0	-807.00	1.8	-115.44	1.8	-133.24	2.12	-24.65
106	106	5.50	-1061.53	-41.49	66.52	0	-1070.51	1.8	-128.34	1.8	-145.16	2.12	4.33
106	107	6.60	-1061.53	-23.93	102.50	0	-1040.70	1.8	-132.04	1.8	-150.04	2.12	-6.21
107	107	6.60	-1061.53	-23.85	102.60	0	-878.22	1.8	-94.87	1.8	-136.44	2.12	-30.61
107	108	7.70	-1061.53	-6.32	119.17	0	-868.01	1.8	-96.94	1.8	-138.81	2.12	-35.08
108	108	7.70	-1061.53	-6.20	119.27	0	-867.94	1.8	-96.96	1.8	-138.82	2.12	-35.11
108	109	8.80	-1061.53	11.34	116.45	0	-870.99	1.8	-96.20	1.8	-138.03	2.12	-33.82
109	109	8.80	-1061.53	11.47	116.50	0	-870.95	1.8	-96.21	1.8	-138.04	2.12	-33.84
109	110	9.90	-1061.53	29.01	94.22	0	-887.30	1.8	-92.59	1.8	-134.06	2.12	-26.78
110	110	9.90	-1061.53	29.19	94.26	0	-887.27	1.8	-92.60	1.8	-134.07	2.12	-26.80
110	111	11.00	-1061.53	46.74	52.51	0	-916.94	1.8	-86.13	1.8	-126.92	2.12	-13.96
111	111	11.00	-1061.53	46.98	52.52	0	-916.93	1.8	-86.13	1.8	-126.92	2.12	-13.97
111	112	12.10	-1061.53	64.50	-8.80	0	-960.01	1.8	-76.79	1.8	-116.57	2.12	4.68
112	112	12.10	-1061.53	64.75	-8.81	0	-960.02	1.8	-76.79	1.8	-116.57	2.12	4.68
112	113	13.20	-1061.53	82.29	-89.69	0	-1016.48	1.8	-64.58	1.8	-103.03	2.12	29.13
113	113	13.20	-1061.53	82.55	-89.72	0	-1016.51	1.8	-64.57	1.8	-103.02	2.12	29.14
113	114	14.30	-1061.53	100.12	-190.21	0	-1086.41	1.8	-49.48	1.8	-86.28	2.12	59.41
114	114	14.30	-871.84	95.78	-105.53	0	-978.83	1.8	-78.41	1.8	-91.04	2.12	51.29
114	115	15.40	-874.66	116.00	-224.38	0	-1069.59	1.8	-62.59	1.8	-72.89	2.12	86.74
115	115	15.40	-1567.05	118.69	104.95	0	-1050.64	1.8	-255.29	1.8	-256.91	2.12	-133.92
115	116	16.50	-1567.05	163.32	-40.74	0	-1170.68	1.8	-236.63	1.8	-238.47	2.12	-93.14
116	116	16.50	-1567.05	163.57	-40.85	0	-1211.10	1.8	-197.26	1.8	-204.28	2.12	-46.63
116	117	17.60	-1567.05	191.15	-234.34	0	-1374.78	1.8	-168.85	1.8	-176.40	2.12	12.24
117	117	17.60	-2068.15	191.26	181.99	0	-1031.44	1.8	-365.57	1.8	-352.76	2.12	-251.23
117	118	18.70	-2068.15	241.25	-57.05	0	-1235.88	1.8	-328.05	1.8	-316.12	2.12	-175.63
118	118	18.70	-2068.15	241.51	-56.79	0	-1235.62	1.8	-328.14	1.8	-316.20	2.12	-175.76
118	119	19.80	-2068.15	298.21	-352.38	0	-1491.43	1.8	-278.38	1.8	-268.06	2.12	-78.56
119	119	19.80	-1810.85	298.88	-225.83	0	-1115.16	1.8	-261.25	1.8	-253.17	2.12	-122.24
119	120	20.90	-1810.85	369.51	-600.76	0	-1444.37	1.8	-192.63	1.8	-187.76	2.12	6.77
120	120	20.90	-1810.85	370.47	-600.71	0	-1444.32	1.8	-192.64	1.8	-187.78	2.12	6.74
120	121	22.00	-1810.85	416.91	-1030.36	0	-1822.82	1.8	-112.67	1.8	-111.40	2.12	156.42
121	1121	22.00	-1847.60	-453.81	-1049.50	0	-1877.39	1.8	-115.08	1.8	-113.39	2.12	162.95
121	122	23.40	-1847.60	-397.38	-457.27	0	-1355.53	1.8	-224.47	1.8	-218.78	2.12	-43.57
122	122	23.40	-1847.60	-396.13	-457.36	0	-1355.62	1.8	-224.44	1.8	-218.75	2.12	-43.52
122	123	24.80	-1847.60	-331.30	50.88	0	-909.11	1.8	-316.80	1.8	-307.55	2.12	-218.64
123	123	24.80	-2104.90	-329.84	-72.89	0	-1283.18	1.8	-334.10	1.8	-322.82	2.12	-175.78
123	124	26.20	-2104.90	-246.67	320.63	0	-942.22	1.8	-399.91	1.8	-387.15	2.12	-305.57
124	124	26.20	-1420.02	-246.33	-9.22	0	-1019.98	1.8	-190.62	1.8	-199.54	2.12	-72.06
124	125	27.60	-1420.02	-187.05	292.24	0	-762.64	1.8	-236.50	1.8	-245.13	2.12	-166.66
125	125	27.60	-1750.84	-187.00	142.68	0	-1236.18	1.8	-259.10	1.8	-266.01	2.12	-114.26
125	126	29.00	-1750.84	-111.23	336.08	0	-1073.38	1.8	-285.75	1.8	-293.37	2.12	-172.45
126	126	29.00	-1061.03	-109.56	6.75	0	-1063.48	1.8	-120.66	1.8	-131.75	2.12	17.54
126	127	30.40	-1058.64	-84.50	145.13	0	-957.71	1.8	-137.13	1.8	-152.24	2.12	-23.16
127	127	30.40	-1356.26	-86.89	18.44	0	-1183.67	1.8	-110.21	1.8	-154.07	2.12	-7.22
127	128	31.80	-1356.26	-64.43	124.31	0	-1112.62	1.8	-125.08	1.8	-171.45	2.12	-38.44
128	128	31.80	-1356.26	-63.94	124.37	0	-1112.57	1.8	-125.09	1.8	-171.46	2.12	-38.46
128	129	33.20	-1356.26	-41.62	198.28	0	-1063.45	1.8	-135.25	1.8	-183.62	2.12	-60.19
129	129	33.20	-1356.26	-41.18	198.32	0	-1063.42	1.8	-135.25	1.8	-183.63	2.12	-60.21
129	130	34.60	-1356.26	-17.69	239.50	0	-1036.83	1.8	-140.56	1.8	-190.44	2.12	-72.19
130	130	34.60	-1356.26	-17.23	239.47	0	-1036.86	1.8	-140.56	1.8	-190.44	2.12	-72.18
130	131	36.00	-1356.26	9.54	244.31	0	-1035.76	1.8	-140.31	1.8	-191.29	2.12	-73.25
131	131	36.00	-1356.26	9.99	244.33	0	-1035.75	1.8	-140.31	1.8	-191.29	2.12	-73.25
131	132	37.40	-1356.26	32.37	214.66	0	-1058.65	1.8	-134.87	1.8	-186.48	2.12	-64.00
132	132	37.40	-1356.26	32.83	214.67	0	-1058.64	1.8	-134.87	1.8	-186.49	2.12	-64.00
132	133	38.80	-1356.26	55.16	153.08	0	-1103.42	1.8	-124.73	1.8	-176.47	2.12	-45.26
133	133	38.80	-1356.26	55.64	153.06	0	-1103.44	1.8	-124.73	1.8	-176.47	2.12	-45.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
133	134	40.20	-1356.26	78.00	59.52	0	-1170.13	1.8	-109.89	1.8	-161.23	2.12	-17.02
134	134	40.20	-1356.26	78.47	59.47	0	-1170.16	1.8	-109.88	1.8	-161.22	2.12	-17.01
134	135	41.60	-1356.26	100.94	-66.10	0	-1258.83	1.8	-90.32	1.8	-140.75	2.12	20.74
135	135	41.60	-1060.58	99.06	60.60	0	-1050.12	1.8	-117.44	1.8	-139.03	2.12	7.13
135	136	43.00	-1063.03	123.89	-96.33	0	-1176.09	1.8	-96.64	1.8	-115.75	2.12	54.36
136	136	43.00	-1750.84	125.14	233.02	0	-1173.76	1.8	-257.64	1.8	-268.27	2.12	-127.28
136	137	44.40	-1750.84	192.84	19.64	0	-1354.95	1.8	-226.81	1.8	-237.12	2.12	-61.73
137	137	44.40	-1420.02	193.00	169.08	0	-881.53	1.8	-204.17	1.8	-216.21	2.12	-114.07
137	138	45.80	-1420.02	249.46	-137.35	0	-1143.64	1.8	-157.43	1.8	-169.73	2.12	-17.66
138	138	45.80	-2104.90	249.60	192.60	0	-1065.79	1.8	-366.75	1.8	-357.36	2.12	-251.21
138	139	47.20	-2104.90	315.16	-199.20	0	-1405.04	1.8	-302.02	1.8	-293.84	2.12	-122.61
139	139	47.20	-1847.60	315.70	-75.25	0	-1030.80	1.8	-284.78	1.8	-278.61	2.12	-165.54
139	140	48.60	-1841.15	397.62	-579.51	0	-1471.52	1.8	-192.63	1.8	-189.81	2.12	8.70
140	140	48.60	-1840.98	398.90	-579.48	0	-1471.42	1.8	-192.62	1.8	-189.80	2.12	8.70
140	141	50.00	-1840.98	458.17	-1177.44	0	-1998.69	1.8	-82.24	1.8	-83.41	2.12	217.26
141	1141	50.00	-1841.18	-458.09	-1177.45	0	-1998.76	1.8	-82.29	1.8	-83.46	2.12	217.22
141	142	51.40	-1841.18	-398.81	-579.58	0	-1471.56	1.8	-192.66	1.8	-189.83	2.12	8.68
142	142	51.40	-1841.79	-397.53	-579.62	0	-1471.79	1.8	-192.78	1.8	-189.94	2.12	8.59
142	143	52.80	-1841.79	-316.12	-75.38	0	-1029.26	1.8	-283.31	1.8	-277.30	2.12	-164.24
143	143	52.80	-2100.09	-315.53	-199.23	0	-1403.70	1.8	-300.82	1.8	-292.76	2.12	-121.55
143	144	54.20	-2104.90	-249.59	192.58	0	-1065.79	1.8	-366.76	1.8	-357.36	2.12	-251.21
144	144	54.20	-1420.02	-249.47	-137.34	0	-1143.64	1.8	-157.44	1.8	-169.73	2.12	-17.66
144	145	55.60	-1420.02	-193.01	169.11	0	-881.50	1.8	-204.18	1.8	-216.22	2.12	-114.09
145	145	55.60	-1750.84	-192.84	19.67	0	-1354.92	1.8	-226.82	1.8	-237.13	2.12	-61.74
145	146	57.00	-1750.84	-125.14	233.02	0	-1173.76	1.8	-257.64	1.8	-268.28	2.12	-127.28
146	146	57.00	-1063.03	-123.90	-96.34	0	-1176.10	1.8	-96.64	1.8	-115.75	2.12	54.36
146	147	58.40	-1062.37	-99.98	61.50	0	-1051.01	1.8	-117.71	1.8	-139.44	2.12	6.79
147	147	58.40	-1358.27	-100.88	-65.18	0	-1259.88	1.8	-90.62	1.8	-141.19	2.12	20.39
147	148	59.80	-1358.27	-78.41	60.27	0	-1171.30	1.8	-110.16	1.8	-161.64	2.12	-17.32
148	148	59.80	-1358.28	-77.94	60.33	0	-1171.25	1.8	-110.17	1.8	-161.65	2.12	-17.35
148	149	61.20	-1358.28	-55.58	153.78	0	-1104.62	1.8	-125.00	1.8	-176.88	2.12	-45.55
149	149	61.20	-1358.27	-55.10	153.79	0	-1104.62	1.8	-125.00	1.8	-176.87	2.12	-45.55
149	150	62.60	-1358.27	-32.77	215.32	0	-1059.88	1.8	-135.13	1.8	-186.88	2.12	-64.27
150	150	62.60	-1358.27	-32.31	215.33	0	-1059.87	1.8	-135.13	1.8	-186.88	2.12	-64.27
150	151	64.00	-1360.02	-9.91	244.86	0	-1038.49	1.8	-140.72	1.8	-191.91	2.12	-73.56
151	151	64.00	-1360.02	-9.46	244.85	0	-1038.50	1.8	-140.72	1.8	-191.91	2.12	-73.56
151	152	65.40	-1360.02	17.31	239.89	0	-1039.68	1.8	-140.95	1.8	-191.04	2.12	-72.46
152	152	65.40	-1360.02	17.77	239.92	0	-1039.65	1.8	-140.96	1.8	-191.05	2.12	-72.47
152	153	66.80	-1360.02	41.25	198.64	0	-1066.31	1.8	-135.64	1.8	-184.22	2.12	-60.45
153	153	66.80	-1360.02	41.70	198.60	0	-1066.33	1.8	-135.63	1.8	-184.21	2.12	-60.44
153	154	68.20	-1360.02	64.02	124.56	0	-1115.55	1.8	-125.45	1.8	-172.03	2.12	-38.67
154	154	68.20	-1360.02	64.50	124.51	0	-1115.59	1.8	-125.44	1.8	-172.02	2.12	-38.66
154	155	69.60	-1360.02	86.96	18.54	0	-1186.70	1.8	-110.57	1.8	-154.62	2.12	-7.40
155	155	69.60	-1061.89	86.36	145.22	0	-960.34	1.8	-137.44	1.8	-152.72	2.12	-23.31
155	156	71.00	-1061.02	109.55	6.74	0	-1063.49	1.8	-120.65	1.8	-131.75	2.12	17.55
156	156	71.00	-1750.84	111.22	336.07	0	-1073.40	1.8	-285.74	1.8	-293.36	2.12	-172.44
156	157	72.40	-1750.84	187.01	142.67	0	-1236.19	1.8	-259.09	1.8	-266.01	2.12	-114.25
157	157	72.40	-1420.02	187.05	292.22	0	-762.66	1.8	-236.49	1.8	-245.13	2.12	-166.65
157	158	73.80	-1420.02	246.33	-9.23	0	-1020.00	1.8	-190.62	1.8	-199.54	2.12	-72.05
158	158	73.80	-2104.90	246.68	320.61	0	-942.23	1.8	-399.91	1.8	-387.15	2.12	-305.56
158	159	75.20	-2104.90	329.86	-72.90	0	-1283.19	1.8	-334.10	1.8	-322.82	2.12	-175.78
159	159	75.20	-1847.60	331.28	50.87	0	-909.12	1.8	-316.80	1.8	-307.55	2.12	-218.63
159	160	76.60	-1843.78	396.60	-457.87	0	-1354.96	1.8	-223.42	1.8	-217.84	2.12	-42.54
160	160	76.60	-1843.83	397.87	-457.89	0	-1354.98	1.8	-223.45	1.8	-217.86	2.12	-42.57
160	161	78.00	-1843.83	454.31	-1050.82	0	-1877.42	1.8	-113.96	1.8	-112.39	2.12	164.14
161	1161	78.00	-1807.39	-417.07	-1031.70	0	-1822.95	1.8	-111.63	1.8	-110.47	2.12	157.53
161	162	79.10	-1807.39	-370.64	-601.91	0	-1444.34	1.8	-191.63	1.8	-186.87	2.12	7.82
162	162	79.10	-1807.77	-369.67	-601.98	0	-1444.51	1.8	-191.69	1.8	-186.93	2.12	7.78
162	163	80.20	-1807.77	-299.05	-226.84	0	-1115.13	1.8	-260.35	1.8	-252.37	2.12	-121.29
163	163	80.20	-2065.60	-298.37	-353.36	0	-1491.52	1.8	-277.62	1.8	-267.37	2.12	-77.74
163	164	81.30	-2065.60	-241.67	-57.59	0	-1235.57	1.8	-327.40	1.8	-315.54	2.12	-174.99
164	164	81.30	-2066.31	-241.40	-57.78	0	-1235.97	1.8	-327.50	1.8	-315.63	2.12	-175.03
164	165	82.40	-2066.31	-191.41	181.41	0	-1031.40	1.8	-365.03	1.8	-352.28	2.12	-250.67
165	165	82.40	-1566.09	-191.25	-234.45	0	-1374.63	1.8	-168.57	1.8	-176.17	2.12	12.47
165	166	83.50	-1566.09	-163.67	-41.26	0	-1211.17	1.8	-196.97	1.8	-204.02	2.12	-46.31
166	166	83.50	-1567.05	-163.35	-41.03	0	-1170.93	1.8	-236.59	1.8	-238.44	2.12	-93.06
166	167	84.60	-1567.05	-118.72	104.70	0	-1050.84	1.8	-255.26	1.8	-256.88	2.12	-133.85
167	167	84.60	-874.65	-116.01	-224.65	0	-1069.77	1.8	-62.55	1.8	-72.84	2.12	86.82
167	168	85.70	-875.52	-98.24	-104.44	0	-981.15	1.8	-78.88	1.8	-91.75	2.12	50.82
168	168	85.70	-1065.96	-100.06	-189.12	0	-1089.34	1.8	-50.02	1.8	-87.09	2.12	58.91
168	169	86.80	-1065.96	-82.49	-88.71	0	-1019.49	1.8	-65.10	1.8	-103.82	2.12	28.66
169	169	86.80	-1065.96	-82.22	-88.68	0	-1019.47	1.8	-65.11	1.8	-103.83	2.12	28.65
169	170	87.90	-1065.96	-64.68	-7.88	0	-963.05	1.8	-77.31	1.8	-117.36	2.12	4.22
170	170	87.90	-1065.96	-64.43	-7.87	0	-963.05	1.8	-77.31	1.8	-117.36	2.12	4.22
170	171	89.00	-1065.96	-46.91	53.37	0	-920.03	1.8	-86.64	1.8	-127.69	2.12	-14.40

CÁLCULO TENSIONAL

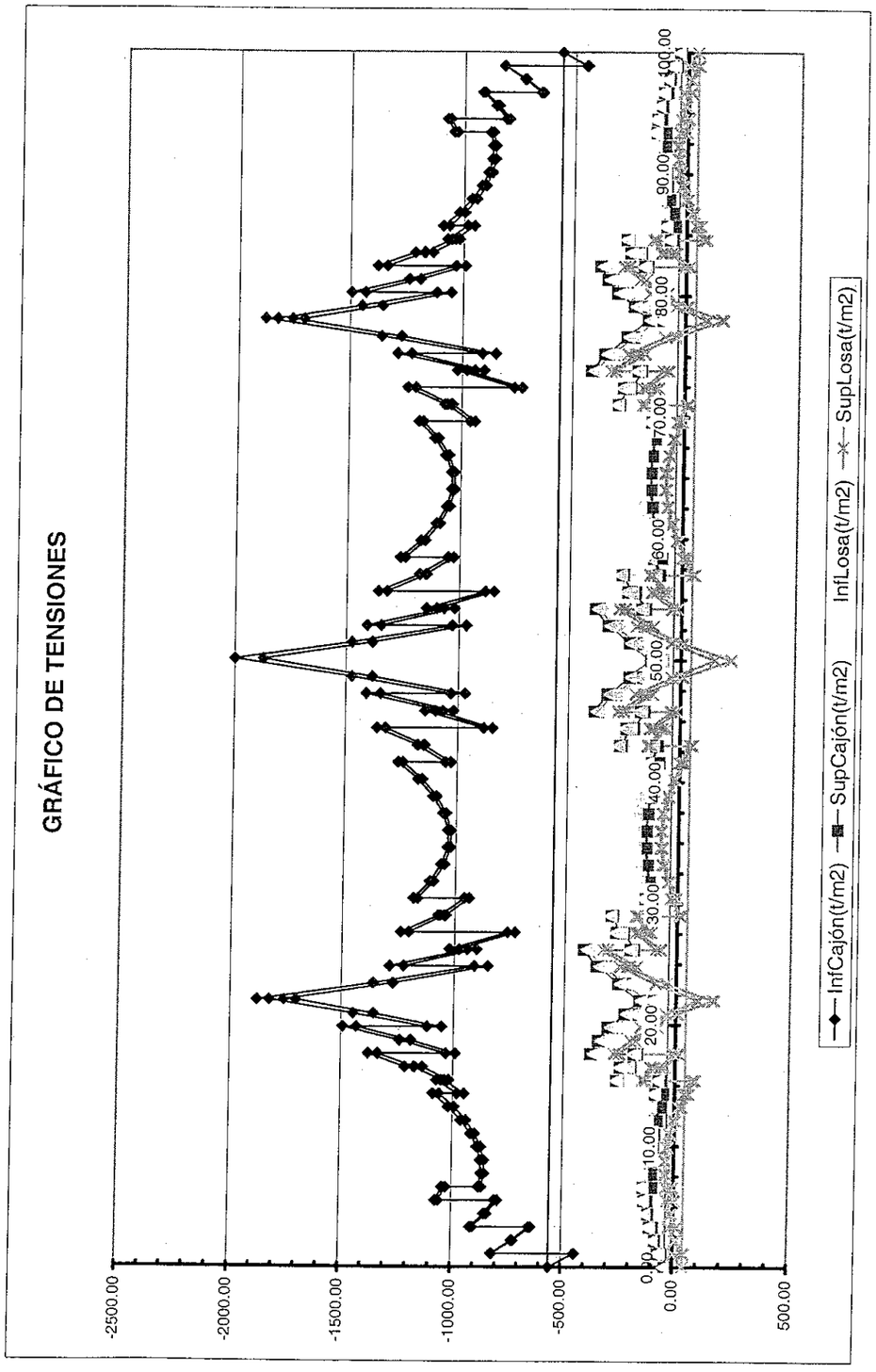
Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD

[1; 1]PPVF1 + [.95; 1.05]eje1f1.ISO.To + [.95; 1.05]eje2f1.ISO.To + [1; 1]PPLACAS + [1; 1]HLP + [.95; 1.05]eje1f3.ISO.To + [.95; 1.05]eje1f3.HIP.To + [.95; 1.05]eje2f3.ISO.To + [.95; 1.05]eje2f3.HIP.To + [1; 1]HLCV + [.7; 1.3]CME

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)	Fibra y fibra	InfCajón sig (t/m2)	Fibra y fibra	SupCajón sig (t/m2)	Fibra y fibra	InfLosa sig (t/m2)	Fibra y fibra	SupLosa sig (t/m2)
171	171	89.00	-1065.96	-46.69	53.37	0	-920.03	1.8	-86.64	1.8	-127.69	2.12	-14.40
171	172	90.10	-1065.96	-29.12	95.03	0	-890.41	1.8	-93.10	1.8	-134.83	2.12	-27.21
172	172	90.10	-1065.96	-28.93	94.98	0	-890.45	1.8	-93.09	1.8	-134.82	2.12	-27.19
172	173	91.20	-1065.96	-11.39	117.16	0	-874.16	1.8	-96.69	1.8	-138.78	2.12	-34.22
173	173	91.20	-1065.96	-11.28	117.10	0	-874.20	1.8	-96.68	1.8	-138.77	2.12	-34.20
173	174	92.30	-1065.96	6.27	119.85	0	-871.20	1.8	-97.44	1.8	-139.55	2.12	-35.46
174	174	92.30	-1065.96	6.39	119.76	0	-871.27	1.8	-97.42	1.8	-139.54	2.12	-35.43
174	175	93.40	-1065.96	23.92	103.10	0	-881.54	1.8	-95.34	1.8	-137.15	2.12	-30.94
175	175	93.40	-1065.96	23.99	103.00	0	-1044.59	1.8	-132.54	1.8	-150.74	2.12	-6.42
175	176	94.50	-1065.96	41.55	66.93	0	-1074.47	1.8	-128.84	1.8	-145.85	2.12	4.15
176	176	94.50	-882.17	41.58	151.55	0	-810.95	1.8	-115.93	1.8	-133.93	2.12	-24.83
176	177	95.60	-882.17	59.13	96.15	0	-856.61	1.8	-110.08	1.8	-126.30	2.12	-8.49
177	177	95.60	-882.17	59.06	96.02	0	-856.72	1.8	-110.06	1.8	-126.28	2.12	-8.44
177	178	96.70	-882.17	76.59	21.39	0	-918.08	1.8	-102.07	1.8	-115.92	2.12	13.65
178	178	96.70	-698.39	76.44	107.83	0	-653.14	1.8	-89.24	1.8	-104.24	2.12	-15.85
178	179	97.80	-698.39	93.98	14.09	0	-730.09	1.8	-79.14	1.8	-91.18	2.12	11.95
179	179	97.80	-698.40	93.77	13.91	0	-730.25	1.8	-79.11	1.8	-91.15	2.12	12.00
179	180	98.90	-698.40	111.35	-98.89	0	-822.75	1.8	-66.91	1.8	-75.39	2.12	45.48
180	180	98.90	-441.09	111.02	27.27	0	-447.83	1.8	-49.16	1.8	-59.70	2.12	2.75
180	181	100.00	-441.09	251.57	-105.57	0	-556.64	1.8	-34.79	1.8	-41.11	2.12	42.20



ESFUERZOS COMBINADOS

ROTURA A FLEXIÓN

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-47.66	0.00
1	2	1.10	0.00	-55.69	66.02
2	2	1.10	0.00	-55.69	66.02
2	3	2.20	0.00	-49.64	123.94
3	3	2.20	0.00	-49.64	123.94
3	4	3.30	0.00	-43.56	175.20
4	4	3.30	0.00	-43.56	175.20
4	5	4.40	0.00	-37.52	219.79
5	5	4.40	0.00	-37.52	219.79
5	6	5.50	0.00	-31.46	257.73
6	6	5.50	0.00	-31.46	257.73
6	7	6.60	0.00	-25.39	289.01
7	7	6.60	0.00	-25.39	289.01
7	8	7.70	0.00	-19.35	313.61
8	8	7.70	0.00	-19.35	313.61
8	9	8.80	0.00	-13.27	331.53
9	9	8.80	0.00	-13.27	331.53
9	10	9.90	0.00	-7.22	342.81
10	10	9.90	0.00	-7.22	342.81
10	11	11.00	0.00	-1.16	347.41
11	11	11.00	0.00	-1.16	347.41
11	12	12.10	0.00	4.90	345.36
12	12	12.10	0.00	4.90	345.36
12	13	13.20	0.00	10.95	336.62
13	13	13.20	0.00	10.95	336.62
13	14	14.30	0.00	17.02	321.26
14	14	14.30	0.00	17.02	321.26
14	15	15.40	0.00	23.07	299.21
15	15	15.40	0.00	23.07	299.21
15	16	16.50	0.00	35.90	266.76
16	16	16.50	0.00	35.90	266.76
16	17	17.60	0.00	48.71	220.24
17	17	17.60	0.00	48.71	220.24
17	18	18.70	0.00	56.53	163.25
18	18	18.70	0.00	56.53	163.25
18	19	19.80	0.00	67.61	94.99
19	19	19.80	0.00	67.61	94.99
19	20	20.90	0.00	78.67	14.52
20	20	20.90	0.00	78.67	14.52
20	21	22.00	0.00	79.55	-82.18
21	1021	22.00	0.00	-95.38	-82.18
21	22	23.40	0.00	-94.29	66.30
22	22	23.40	0.00	-94.29	66.30
22	23	24.80	0.00	-80.20	188.48
23	23	24.80	0.00	-80.20	188.48
23	24	26.20	0.00	-70.39	294.06
24	24	26.20	0.00	-70.39	294.06
24	25	27.60	0.00	-54.07	381.19
25	25	27.60	0.00	-54.07	381.19
25	26	29.00	0.00	-37.76	445.47
26	26	29.00	0.00	-37.76	445.47

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-30.05	492.95
27	27	30.40	0.00	-30.05	492.95
27	28	31.80	0.00	-22.33	529.61
28	28	31.80	0.00	-22.33	529.61
28	29	33.20	0.00	-14.63	555.50
29	29	33.20	0.00	-14.63	555.50
29	30	34.60	0.00	-6.91	570.58
30	30	34.60	0.00	-6.91	570.58
30	31	36.00	0.00	0.80	574.87
31	31	36.00	0.00	0.80	574.87
31	32	37.40	0.00	8.51	568.36
32	32	37.40	0.00	8.51	568.36
32	33	38.80	0.00	16.23	551.07
33	33	38.80	0.00	16.23	551.07
33	34	40.20	0.00	23.92	522.96
34	34	40.20	0.00	23.92	522.96
34	35	41.60	0.00	31.64	484.08
35	35	41.60	0.00	31.64	484.08
35	36	43.00	0.00	39.35	434.39
36	36	43.00	0.00	39.35	434.39
36	37	44.40	0.00	55.66	367.89
37	37	44.40	0.00	55.66	367.89
37	38	45.80	0.00	67.32	279.42
38	38	45.80	0.00	67.32	279.42
38	39	47.20	0.00	81.38	175.35
39	39	47.20	0.00	81.38	175.35
39	40	48.60	0.00	95.47	51.53
40	40	48.60	0.00	95.47	51.53
40	41	50.00	0.00	96.56	-98.59
41	1041	50.00	0.00	-96.56	-98.59
41	42	51.40	0.00	-95.47	51.53
42	42	51.40	0.00	-95.47	51.53
42	43	52.80	0.00	-81.38	175.35
43	43	52.80	0.00	-81.38	175.35
43	44	54.20	0.00	-67.32	279.42
44	44	54.20	0.00	-67.32	279.42
44	45	55.60	0.00	-55.66	367.89
45	45	55.60	0.00	-55.66	367.89
45	46	57.00	0.00	-39.35	434.39
46	46	57.00	0.00	-39.35	434.39
46	47	58.40	0.00	-31.64	484.08
47	47	58.40	0.00	-31.64	484.08
47	48	59.80	0.00	-23.92	522.96
48	48	59.80	0.00	-23.92	522.96
48	49	61.20	0.00	-16.23	551.07
49	49	61.20	0.00	-16.23	551.07
49	50	62.60	0.00	-8.51	568.36
50	50	62.60	0.00	-8.51	568.36
50	51	64.00	0.00	-0.80	574.87
51	51	64.00	0.00	-0.80	574.87
51	52	65.40	0.00	6.91	570.58

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FASE1.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	6.91	570.58
52	53	66.80	0.00	14.63	555.50
53	53	66.80	0.00	14.63	555.50
53	54	68.20	0.00	22.33	529.61
54	54	68.20	0.00	22.33	529.61
54	55	69.60	0.00	30.05	492.95
55	55	69.60	0.00	30.05	492.95
55	56	71.00	0.00	37.76	445.47
56	56	71.00	0.00	37.76	445.47
56	57	72.40	0.00	54.07	381.19
57	57	72.40	0.00	54.07	381.19
57	58	73.80	0.00	70.39	294.06
58	58	73.80	0.00	70.39	294.06
58	59	75.20	0.00	80.20	188.48
59	59	75.20	0.00	80.20	188.48
59	60	76.60	0.00	94.29	66.30
60	60	76.60	0.00	94.29	66.30
60	61	78.00	0.00	95.38	-82.18
61	1061	78.00	0.00	-79.55	-82.18
61	62	79.10	0.00	-78.67	14.52
62	62	79.10	0.00	-78.67	14.52
62	63	80.20	0.00	-67.61	94.99
63	63	80.20	0.00	-67.61	94.99
63	64	81.30	0.00	-56.53	163.25
64	64	81.30	0.00	-56.53	163.25
64	65	82.40	0.00	-48.71	220.24
65	65	82.40	0.00	-48.71	220.24
65	66	83.50	0.00	-35.90	266.76
66	66	83.50	0.00	-35.90	266.76
66	67	84.60	0.00	-23.07	299.21
67	67	84.60	0.00	-23.07	299.21
67	68	85.70	0.00	-17.02	321.26
68	68	85.70	0.00	-17.02	321.26
68	69	86.80	0.00	-10.95	336.62
69	69	86.80	0.00	-10.95	336.62
69	70	87.90	0.00	-4.90	345.36
70	70	87.90	0.00	-4.90	345.36
70	71	89.00	0.00	1.16	347.41
71	71	89.00	0.00	1.16	347.41
71	72	90.10	0.00	7.22	342.81
72	72	90.10	0.00	7.22	342.81
72	73	91.20	0.00	13.27	331.53
73	73	91.20	0.00	13.27	331.53
73	74	92.30	0.00	19.35	313.61
74	74	92.30	0.00	19.35	313.61
74	75	93.40	0.00	25.39	289.01
75	75	93.40	0.00	25.39	289.01
75	76	94.50	0.00	31.46	257.73
76	76	94.50	0.00	31.46	257.73
76	77	95.60	0.00	37.52	219.79
77	77	95.60	0.00	37.52	219.79

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	43.56	175.20
78	78	96.70	0.00	43.56	175.20
78	79	97.80	0.00	49.64	123.94
79	79	97.80	0.00	49.64	123.94
79	80	98.90	0.00	55.69	66.02
80	80	98.90	0.00	55.69	66.02
80	81	100.00	0.00	47.66	0.00
101	101	0.00	0.00	-47.66	0.00
101	102	1.10	0.00	-55.69	66.02
102	102	1.10	0.00	-55.69	66.02
102	103	2.20	0.00	-49.64	123.94
103	103	2.20	0.00	-49.64	123.94
103	104	3.30	0.00	-43.56	175.20
104	104	3.30	0.00	-43.56	175.20
104	105	4.40	0.00	-37.52	219.79
105	105	4.40	0.00	-37.52	219.79
105	106	5.50	0.00	-31.46	257.73
106	106	5.50	0.00	-31.46	257.73
106	107	6.60	0.00	-25.39	289.01
107	107	6.60	0.00	-25.39	289.01
107	108	7.70	0.00	-19.35	313.61
108	108	7.70	0.00	-19.35	313.61
108	109	8.80	0.00	-13.27	331.53
109	109	8.80	0.00	-13.27	331.53
109	110	9.90	0.00	-7.22	342.81
110	110	9.90	0.00	-7.22	342.81
110	111	11.00	0.00	-1.16	347.41
111	111	11.00	0.00	-1.16	347.41
111	112	12.10	0.00	4.90	345.36
112	112	12.10	0.00	4.90	345.36
112	113	13.20	0.00	10.95	336.62
113	113	13.20	0.00	10.95	336.62
113	114	14.30	0.00	17.02	321.26
114	114	14.30	0.00	17.02	321.26
114	115	15.40	0.00	23.07	299.21
115	115	15.40	0.00	23.07	299.21
115	116	16.50	0.00	35.90	266.76
116	116	16.50	0.00	35.90	266.76
116	117	17.60	0.00	48.71	220.24
117	117	17.60	0.00	48.71	220.24
117	118	18.70	0.00	56.53	163.25
118	118	18.70	0.00	56.53	163.25
118	119	19.80	0.00	67.61	94.99
119	119	19.80	0.00	67.61	94.99
119	120	20.90	0.00	78.67	14.52
120	120	20.90	0.00	78.67	14.52
120	121	22.00	0.00	79.55	-82.18
121	1121	22.00	0.00	-95.38	-82.18
121	122	23.40	0.00	-94.29	66.30
122	122	23.40	0.00	-94.29	66.30
122	123	24.80	0.00	-80.20	188.48

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-80.20	188.48
123	124	26.20	0.00	-70.39	294.06
124	124	26.20	0.00	-70.39	294.06
124	125	27.60	0.00	-54.07	381.19
125	125	27.60	0.00	-54.07	381.19
125	126	29.00	0.00	-37.76	445.47
126	126	29.00	0.00	-37.76	445.47
126	127	30.40	0.00	-30.05	492.95
127	127	30.40	0.00	-30.05	492.95
127	128	31.80	0.00	-22.33	529.61
128	128	31.80	0.00	-22.33	529.61
128	129	33.20	0.00	-14.63	555.50
129	129	33.20	0.00	-14.63	555.50
129	130	34.60	0.00	-6.91	570.58
130	130	34.60	0.00	-6.91	570.58
130	131	36.00	0.00	0.80	574.87
131	131	36.00	0.00	0.80	574.87
131	132	37.40	0.00	8.51	568.36
132	132	37.40	0.00	8.51	568.36
132	133	38.80	0.00	16.23	551.07
133	133	38.80	0.00	16.23	551.07
133	134	40.20	0.00	23.92	522.96
134	134	40.20	0.00	23.92	522.96
134	135	41.60	0.00	31.64	484.08
135	135	41.60	0.00	31.64	484.08
135	136	43.00	0.00	39.35	434.39
136	136	43.00	0.00	39.35	434.39
136	137	44.40	0.00	55.66	367.89
137	137	44.40	0.00	55.66	367.89
137	138	45.80	0.00	67.32	279.42
138	138	45.80	0.00	67.32	279.42
138	139	47.20	0.00	81.38	175.35
139	139	47.20	0.00	81.38	175.35
139	140	48.60	0.00	95.47	51.53
140	140	48.60	0.00	95.47	51.53
140	141	50.00	0.00	96.56	-98.59
141	1141	50.00	0.00	-96.56	-98.59
141	142	51.40	0.00	-95.47	51.53
142	142	51.40	0.00	-95.47	51.53
142	143	52.80	0.00	-81.38	175.35
143	143	52.80	0.00	-81.38	175.35
143	144	54.20	0.00	-67.32	279.42
144	144	54.20	0.00	-67.32	279.42
144	145	55.60	0.00	-55.66	367.89
145	145	55.60	0.00	-55.66	367.89
145	146	57.00	0.00	-39.35	434.39
146	146	57.00	0.00	-39.35	434.39
146	147	58.40	0.00	-31.64	484.08
147	147	58.40	0.00	-31.64	484.08
147	148	59.80	0.00	-23.92	522.96
148	148	59.80	0.00	-23.92	522.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-16.23	551.07
149	149	61.20	0.00	-16.23	551.07
149	150	62.60	0.00	-8.51	568.36
150	150	62.60	0.00	-8.51	568.36
150	151	64.00	0.00	-0.80	574.87
151	151	64.00	0.00	-0.80	574.87
151	152	65.40	0.00	6.91	570.58
152	152	65.40	0.00	6.91	570.58
152	153	66.80	0.00	14.63	555.50
153	153	66.80	0.00	14.63	555.50
153	154	68.20	0.00	22.33	529.61
154	154	68.20	0.00	22.33	529.61
154	155	69.60	0.00	30.05	492.95
155	155	69.60	0.00	30.05	492.95
155	156	71.00	0.00	37.76	445.47
156	156	71.00	0.00	37.76	445.47
156	157	72.40	0.00	54.07	381.19
157	157	72.40	0.00	54.07	381.19
157	158	73.80	0.00	70.39	294.06
158	158	73.80	0.00	70.39	294.06
158	159	75.20	0.00	80.20	188.48
159	159	75.20	0.00	80.20	188.48
159	160	76.60	0.00	94.29	66.30
160	160	76.60	0.00	94.29	66.30
160	161	78.00	0.00	95.38	-82.18
161	1161	78.00	0.00	-79.55	-82.18
161	162	79.10	0.00	-78.67	14.52
162	162	79.10	0.00	-78.67	14.52
162	163	80.20	0.00	-67.61	94.99
163	163	80.20	0.00	-67.61	94.99
163	164	81.30	0.00	-56.53	163.25
164	164	81.30	0.00	-56.53	163.25
164	165	82.40	0.00	-48.71	220.24
165	165	82.40	0.00	-48.71	220.24
165	166	83.50	0.00	-35.90	266.76
166	166	83.50	0.00	-35.90	266.76
166	167	84.60	0.00	-23.07	299.21
167	167	84.60	0.00	-23.07	299.21
167	168	85.70	0.00	-17.02	321.26
168	168	85.70	0.00	-17.02	321.26
168	169	86.80	0.00	-10.95	336.62
169	169	86.80	0.00	-10.95	336.62
169	170	87.90	0.00	-4.90	345.36
170	170	87.90	0.00	-4.90	345.36
170	171	89.00	0.00	1.16	347.41
171	171	89.00	0.00	1.16	347.41
171	172	90.10	0.00	7.22	342.81
172	172	90.10	0.00	7.22	342.81
172	173	91.20	0.00	13.27	331.53
173	173	91.20	0.00	13.27	331.53
173	174	92.30	0.00	19.35	313.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:

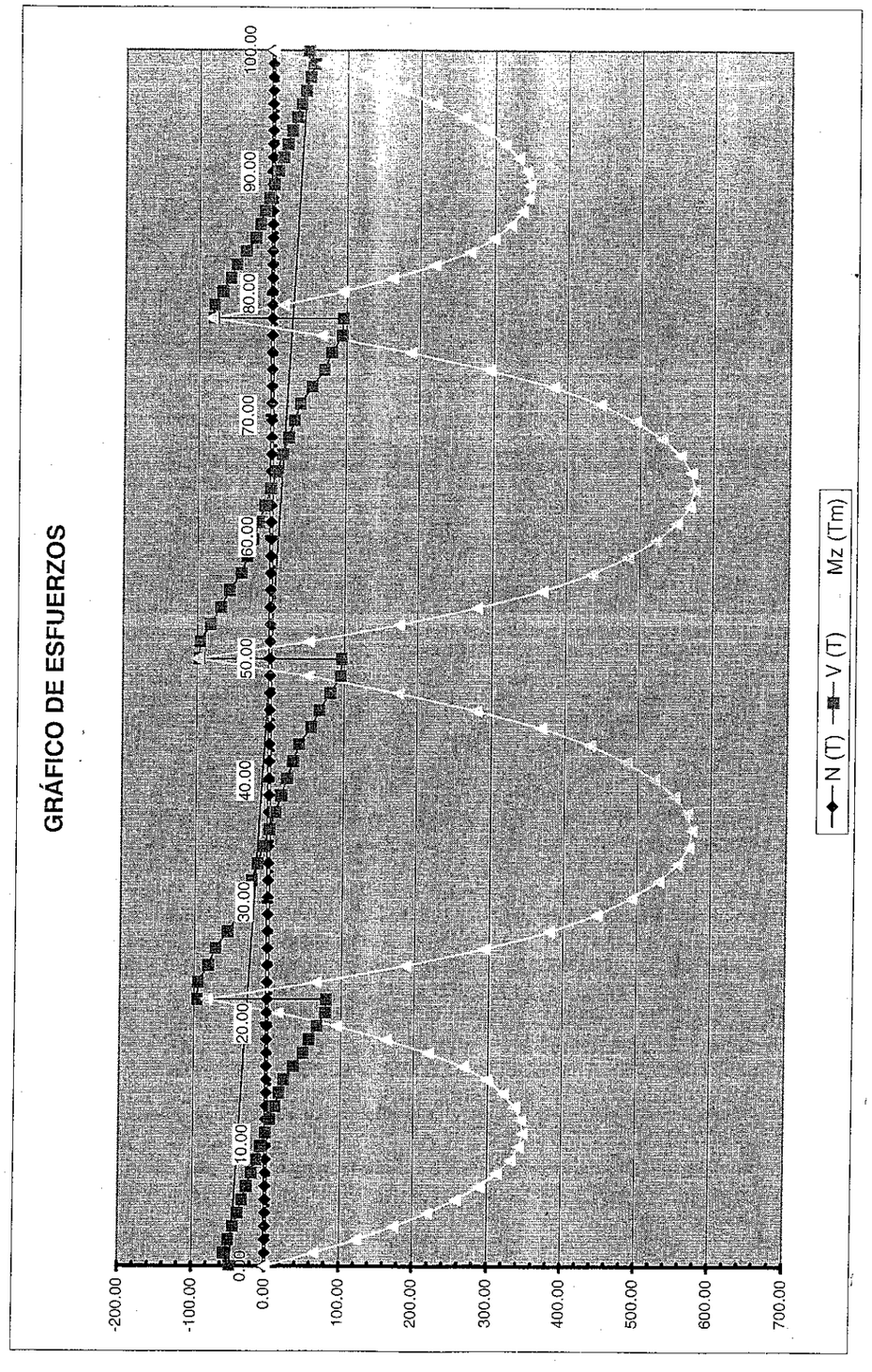
FASE1.T0.MZ+

Construcción fase 1 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	19.35	313.61
174	175	93.40	0.00	25.39	289.01
175	175	93.40	0.00	25.39	289.01
175	176	94.50	0.00	31.46	257.73
176	176	94.50	0.00	31.46	257.73
176	177	95.60	0.00	37.52	219.79
177	177	95.60	0.00	37.52	219.79
177	178	96.70	0.00	43.56	175.20
178	178	96.70	0.00	43.56	175.20
178	179	97.80	0.00	49.64	123.94
179	179	97.80	0.00	49.64	123.94
179	180	98.90	0.00	55.69	66.02
180	180	98.90	0.00	55.69	66.02
180	181	100.00	0.00	47.66	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-

Construcción fase 1 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-47.66	0.00
1	2	1.10	0.00	-41.25	48.90
2	2	1.10	0.00	-41.25	48.90
2	3	2.20	0.00	-36.77	91.81
3	3	2.20	0.00	-36.77	91.81
3	4	3.30	0.00	-32.27	129.78
4	4	3.30	0.00	-32.27	129.78
4	5	4.40	0.00	-27.79	162.81
5	5	4.40	0.00	-27.79	162.81
5	6	5.50	0.00	-23.30	190.91
6	6	5.50	0.00	-23.30	190.91
6	7	6.60	0.00	-18.81	214.08
7	7	6.60	0.00	-18.81	214.08
7	8	7.70	0.00	-14.33	232.30
8	8	7.70	0.00	-14.33	232.30
8	9	8.80	0.00	-9.83	245.58
9	9	8.80	0.00	-9.83	245.58
9	10	9.90	0.00	-5.35	253.93
10	10	9.90	0.00	-5.35	253.93
10	11	11.00	0.00	-0.86	257.34
11	11	11.00	0.00	-0.86	257.34
11	12	12.10	0.00	3.63	255.82
12	12	12.10	0.00	3.63	255.82
12	13	13.20	0.00	8.11	249.35
13	13	13.20	0.00	8.11	249.35
13	14	14.30	0.00	12.61	237.97
14	14	14.30	0.00	12.61	237.97
14	15	15.40	0.00	17.09	221.64
15	15	15.40	0.00	17.09	221.64
15	16	16.50	0.00	26.59	197.60
16	16	16.50	0.00	26.59	197.60
16	17	17.60	0.00	36.08	163.14
17	17	17.60	0.00	36.08	163.14
17	18	18.70	0.00	50.56	114.59
18	18	18.70	0.00	50.56	114.59
18	19	19.80	0.00	61.81	52.81
19	19	19.80	0.00	61.81	52.81
19	20	20.90	0.00	73.05	-21.38
20	20	20.90	0.00	73.05	-21.38
20	21	22.00	0.00	89.79	-110.94
21	1021	22.00	0.00	-106.32	-110.94
21	22	23.40	0.00	-85.01	23.00
22	22	23.40	0.00	-85.01	23.00
22	23	24.80	0.00	-70.69	132.02
23	23	24.80	0.00	-70.69	132.02
23	24	26.20	0.00	-52.14	217.82
24	24	26.20	0.00	-52.14	217.82
24	25	27.60	0.00	-40.05	282.36
25	25	27.60	0.00	-40.05	282.36
25	26	29.00	0.00	-27.97	329.98
26	26	29.00	0.00	-27.97	329.98

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-

Construcción fase 1 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-22.26	365.15
27	27	30.40	0.00	-22.26	365.15
27	28	31.80	0.00	-16.54	392.30
28	28	31.80	0.00	-16.54	392.30
28	29	33.20	0.00	-10.84	411.48
29	29	33.20	0.00	-10.84	411.48
29	30	34.60	0.00	-5.12	422.65
30	30	34.60	0.00	-5.12	422.65
30	31	36.00	0.00	0.59	425.83
31	31	36.00	0.00	0.59	425.83
31	32	37.40	0.00	6.30	421.01
32	32	37.40	0.00	6.30	421.01
32	33	38.80	0.00	12.02	408.20
33	33	38.80	0.00	12.02	408.20
33	34	40.20	0.00	17.72	387.38
34	34	40.20	0.00	17.72	387.38
34	35	41.60	0.00	23.44	358.58
35	35	41.60	0.00	23.44	358.58
35	36	43.00	0.00	29.15	321.77
36	36	43.00	0.00	29.15	321.77
36	37	44.40	0.00	41.23	272.51
37	37	44.40	0.00	41.23	272.51
37	38	45.80	0.00	57.99	205.46
38	38	45.80	0.00	57.99	205.46
38	39	47.20	0.00	72.29	114.29
39	39	47.20	0.00	72.29	114.29
39	40	48.60	0.00	86.60	3.06
40	40	48.60	0.00	86.60	3.06
40	41	50.00	0.00	107.91	-133.10
41	1041	50.00	0.00	-107.91	-133.10
41	42	51.40	0.00	-86.60	3.06
42	42	51.40	0.00	-86.60	3.06
42	43	52.80	0.00	-72.29	114.29
43	43	52.80	0.00	-72.29	114.29
43	44	54.20	0.00	-57.99	205.46
44	44	54.20	0.00	-57.99	205.46
44	45	55.60	0.00	-41.23	272.51
45	45	55.60	0.00	-41.23	272.51
45	46	57.00	0.00	-29.15	321.77
46	46	57.00	0.00	-29.15	321.77
46	47	58.40	0.00	-23.44	358.58
47	47	58.40	0.00	-23.44	358.58
47	48	59.80	0.00	-17.72	387.38
48	48	59.80	0.00	-17.72	387.38
48	49	61.20	0.00	-12.02	408.20
49	49	61.20	0.00	-12.02	408.20
49	50	62.60	0.00	-6.30	421.01
50	50	62.60	0.00	-6.30	421.01
50	51	64.00	0.00	-0.59	425.83
51	51	64.00	0.00	-0.59	425.83
51	52	65.40	0.00	5.12	422.65

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-

Construcción fase 1 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	5.12	422.65
52	53	66.80	0.00	10.84	411.48
53	53	66.80	0.00	10.84	411.48
53	54	68.20	0.00	16.54	392.30
54	54	68.20	0.00	16.54	392.30
54	55	69.60	0.00	22.26	365.15
55	55	69.60	0.00	22.26	365.15
55	56	71.00	0.00	27.97	329.98
56	56	71.00	0.00	27.97	329.98
56	57	72.40	0.00	40.05	282.36
57	57	72.40	0.00	40.05	282.36
57	58	73.80	0.00	52.14	217.82
58	58	73.80	0.00	52.14	217.82
58	59	75.20	0.00	70.69	132.02
59	59	75.20	0.00	70.69	132.02
59	60	76.60	0.00	85.01	23.00
60	60	76.60	0.00	85.01	23.00
60	61	78.00	0.00	106.32	-110.94
61	1061	78.00	0.00	-89.79	-110.94
61	62	79.10	0.00	-73.05	-21.38
62	62	79.10	0.00	-73.05	-21.38
62	63	80.20	0.00	-61.81	52.81
63	63	80.20	0.00	-61.81	52.81
63	64	81.30	0.00	-50.56	114.59
64	64	81.30	0.00	-50.56	114.59
64	65	82.40	0.00	-36.08	163.14
65	65	82.40	0.00	-36.08	163.14
65	66	83.50	0.00	-26.59	197.60
66	66	83.50	0.00	-26.59	197.60
66	67	84.60	0.00	-17.09	221.64
67	67	84.60	0.00	-17.09	221.64
67	68	85.70	0.00	-12.61	237.97
68	68	85.70	0.00	-12.61	237.97
68	69	86.80	0.00	-8.11	249.35
69	69	86.80	0.00	-8.11	249.35
69	70	87.90	0.00	-3.63	255.82
70	70	87.90	0.00	-3.63	255.82
70	71	89.00	0.00	0.86	257.34
71	71	89.00	0.00	0.86	257.34
71	72	90.10	0.00	5.35	253.93
72	72	90.10	0.00	5.35	253.93
72	73	91.20	0.00	9.83	245.58
73	73	91.20	0.00	9.83	245.58
73	74	92.30	0.00	14.33	232.30
74	74	92.30	0.00	14.33	232.30
74	75	93.40	0.00	18.81	214.08
75	75	93.40	0.00	18.81	214.08
75	76	94.50	0.00	23.30	190.91
76	76	94.50	0.00	23.30	190.91
76	77	95.60	0.00	27.79	162.81
77	77	95.60	0.00	27.79	162.81

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-
Construcción fase 1 Mz-
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	32.27	129.78
78	78	96.70	0.00	32.27	129.78
78	79	97.80	0.00	36.77	91.81
79	79	97.80	0.00	36.77	91.81
79	80	98.90	0.00	41.25	48.90
80	80	98.90	0.00	41.25	48.90
80	81	100.00	0.00	47.66	0.00
101	101	0.00	0.00	-47.66	0.00
101	102	1.10	0.00	-41.25	48.90
102	102	1.10	0.00	-41.25	48.90
102	103	2.20	0.00	-36.77	91.81
103	103	2.20	0.00	-36.77	91.81
103	104	3.30	0.00	-32.27	129.78
104	104	3.30	0.00	-32.27	129.78
104	105	4.40	0.00	-27.79	162.81
105	105	4.40	0.00	-27.79	162.81
105	106	5.50	0.00	-23.30	190.91
106	106	5.50	0.00	-23.30	190.91
106	107	6.60	0.00	-18.81	214.08
107	107	6.60	0.00	-18.81	214.08
107	108	7.70	0.00	-14.33	232.30
108	108	7.70	0.00	-14.33	232.30
108	109	8.80	0.00	-9.83	245.58
109	109	8.80	0.00	-9.83	245.58
109	110	9.90	0.00	-5.35	253.93
110	110	9.90	0.00	-5.35	253.93
110	111	11.00	0.00	-0.86	257.34
111	111	11.00	0.00	-0.86	257.34
111	112	12.10	0.00	3.63	255.82
112	112	12.10	0.00	3.63	255.82
112	113	13.20	0.00	8.11	249.35
113	113	13.20	0.00	8.11	249.35
113	114	14.30	0.00	12.61	237.97
114	114	14.30	0.00	12.61	237.97
114	115	15.40	0.00	17.09	221.64
115	115	15.40	0.00	17.09	221.64
115	116	16.50	0.00	26.59	197.60
116	116	16.50	0.00	26.59	197.60
116	117	17.60	0.00	36.08	163.14
117	117	17.60	0.00	36.08	163.14
117	118	18.70	0.00	50.56	114.59
118	118	18.70	0.00	50.56	114.59
118	119	19.80	0.00	61.81	52.81
119	119	19.80	0.00	61.81	52.81
119	120	20.90	0.00	73.05	-21.38
120	120	20.90	0.00	73.05	-21.38
120	121	22.00	0.00	89.79	-110.94
121	1121	22.00	0.00	-106.32	-110.94
121	122	23.40	0.00	-85.01	23.00
122	122	23.40	0.00	-85.01	23.00
122	123	24.80	0.00	-70.69	132.02

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-
Construcción fase 1 Mz-
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-70.69	132.02
123	124	26.20	0.00	-52.14	217.82
124	124	26.20	0.00	-52.14	217.82
124	125	27.60	0.00	-40.05	282.36
125	125	27.60	0.00	-40.05	282.36
125	126	29.00	0.00	-27.97	329.98
126	126	29.00	0.00	-27.97	329.98
126	127	30.40	0.00	-22.26	365.15
127	127	30.40	0.00	-22.26	365.15
127	128	31.80	0.00	-16.54	392.30
128	128	31.80	0.00	-16.54	392.30
128	129	33.20	0.00	-10.84	411.48
129	129	33.20	0.00	-10.84	411.48
129	130	34.60	0.00	-5.12	422.65
130	130	34.60	0.00	-5.12	422.65
130	131	36.00	0.00	0.59	425.83
131	131	36.00	0.00	0.59	425.83
131	132	37.40	0.00	6.30	421.01
132	132	37.40	0.00	6.30	421.01
132	133	38.80	0.00	12.02	408.20
133	133	38.80	0.00	12.02	408.20
133	134	40.20	0.00	17.72	387.38
134	134	40.20	0.00	17.72	387.38
134	135	41.60	0.00	23.44	358.58
135	135	41.60	0.00	23.44	358.58
135	136	43.00	0.00	29.15	321.77
136	136	43.00	0.00	29.15	321.77
136	137	44.40	0.00	41.23	272.51
137	137	44.40	0.00	41.23	272.51
137	138	45.80	0.00	57.99	205.46
138	138	45.80	0.00	57.99	205.46
138	139	47.20	0.00	72.29	114.29
139	139	47.20	0.00	72.29	114.29
139	140	48.60	0.00	86.60	3.06
140	140	48.60	0.00	86.60	3.06
140	141	50.00	0.00	107.91	-133.10
141	1141	50.00	0.00	-107.91	-133.10
141	142	51.40	0.00	-86.60	3.06
142	142	51.40	0.00	-86.60	3.06
142	143	52.80	0.00	-72.29	114.29
143	143	52.80	0.00	-72.29	114.29
143	144	54.20	0.00	-57.99	205.46
144	144	54.20	0.00	-57.99	205.46
144	145	55.60	0.00	-41.23	272.51
145	145	55.60	0.00	-41.23	272.51
145	146	57.00	0.00	-29.15	321.77
146	146	57.00	0.00	-29.15	321.77
146	147	58.40	0.00	-23.44	358.58
147	147	58.40	0.00	-23.44	358.58
147	148	59.80	0.00	-17.72	387.38
148	148	59.80	0.00	-17.72	387.38

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE1.T0.MZ-

Construcción fase 1 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-12.02	408.20
149	149	61.20	0.00	-12.02	408.20
149	150	62.60	0.00	-6.30	421.01
150	150	62.60	0.00	-6.30	421.01
150	151	64.00	0.00	-0.59	425.83
151	151	64.00	0.00	-0.59	425.83
151	152	65.40	0.00	5.12	422.65
152	152	65.40	0.00	5.12	422.65
152	153	66.80	0.00	10.84	411.48
153	153	66.80	0.00	10.84	411.48
153	154	68.20	0.00	16.54	392.30
154	154	68.20	0.00	16.54	392.30
154	155	69.60	0.00	22.26	365.15
155	155	69.60	0.00	22.26	365.15
155	156	71.00	0.00	27.97	329.98
156	156	71.00	0.00	27.97	329.98
156	157	72.40	0.00	40.05	282.36
157	157	72.40	0.00	40.05	282.36
157	158	73.80	0.00	52.14	217.82
158	158	73.80	0.00	52.14	217.82
158	159	75.20	0.00	70.69	132.02
159	159	75.20	0.00	70.69	132.02
159	160	76.60	0.00	85.01	23.00
160	160	76.60	0.00	85.01	23.00
160	161	78.00	0.00	106.32	-110.94
161	1161	78.00	0.00	-89.79	-110.94
161	162	79.10	0.00	-73.05	-21.38
162	162	79.10	0.00	-73.05	-21.38
162	163	80.20	0.00	-61.81	52.81
163	163	80.20	0.00	-61.81	52.81
163	164	81.30	0.00	-50.56	114.59
164	164	81.30	0.00	-50.56	114.59
164	165	82.40	0.00	-36.08	163.14
165	165	82.40	0.00	-36.08	163.14
165	166	83.50	0.00	-26.59	197.60
166	166	83.50	0.00	-26.59	197.60
166	167	84.60	0.00	-17.09	221.64
167	167	84.60	0.00	-17.09	221.64
167	168	85.70	0.00	-12.61	237.97
168	168	85.70	0.00	-12.61	237.97
168	169	86.80	0.00	-8.11	249.35
169	169	86.80	0.00	-8.11	249.35
169	170	87.90	0.00	-3.63	255.82
170	170	87.90	0.00	-3.63	255.82
170	171	89.00	0.00	0.86	257.34
171	171	89.00	0.00	0.86	257.34
171	172	90.10	0.00	5.35	253.93
172	172	90.10	0.00	5.35	253.93
172	173	91.20	0.00	9.83	245.58
173	173	91.20	0.00	9.83	245.58
173	174	92.30	0.00	14.33	232.30

CÁLCULO TENSIONAL

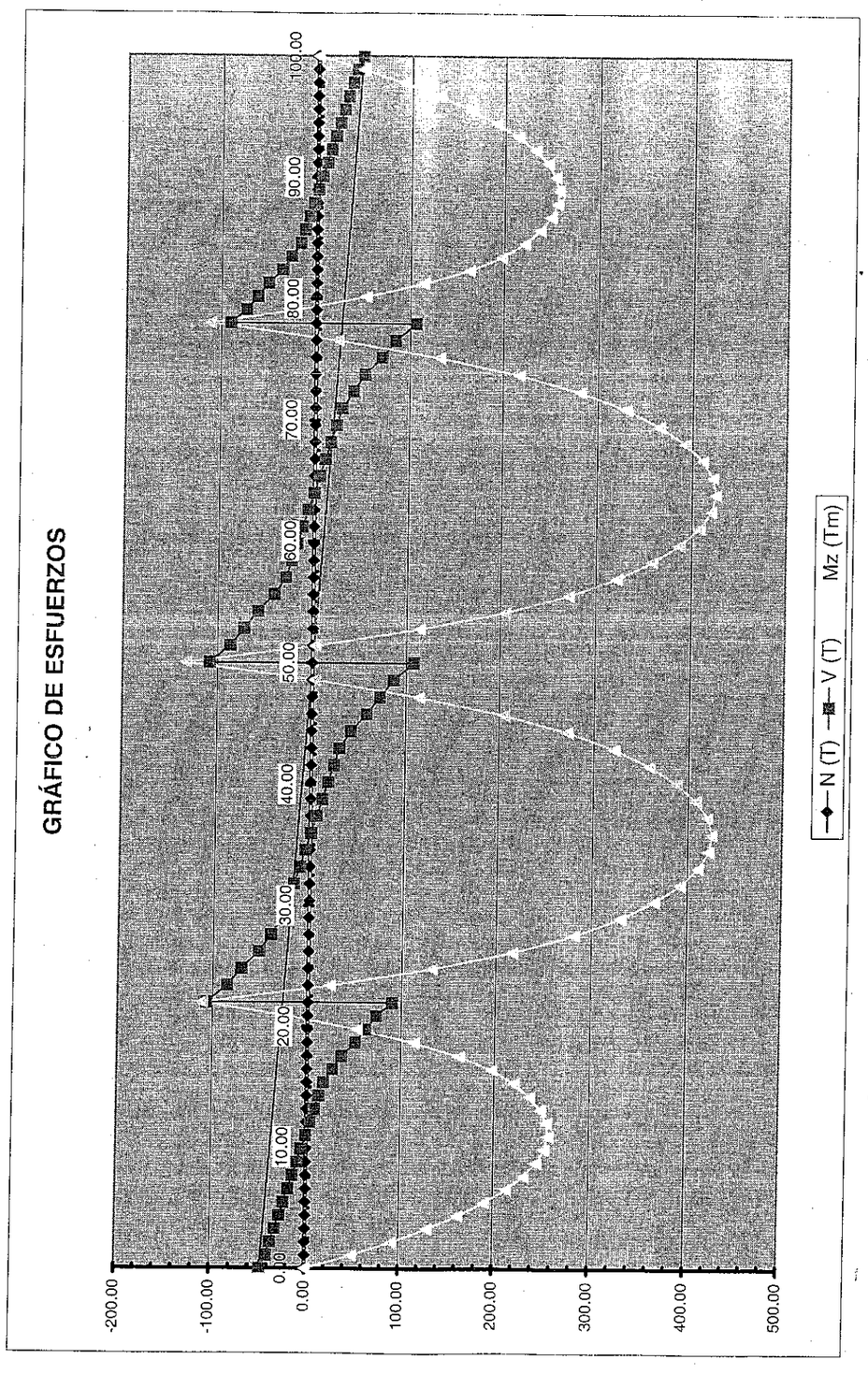
Hipótesis de cálculo:
FASE1.T0.MZ-

Construcción fase 1 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	14.33	232.30
174	175	93.40	0.00	18.81	214.08
175	175	93.40	0.00	18.81	214.08
175	176	94.50	0.00	23.30	190.91
176	176	94.50	0.00	23.30	190.91
176	177	95.60	0.00	27.79	162.81
177	177	95.60	0.00	27.79	162.81
177	178	96.70	0.00	32.27	129.78
178	178	96.70	0.00	32.27	129.78
178	179	97.80	0.00	36.77	91.81
179	179	97.80	0.00	36.77	91.81
179	180	98.90	0.00	41.25	48.90
180	180	98.90	0.00	41.25	48.90
180	181	100.00	0.00	47.66	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-37.71	0.00
1	2	1.10	0.00	-45.74	55.07
2	2	1.10	0.00	-45.74	55.07
2	3	2.20	0.00	-39.69	102.05
3	3	2.20	0.00	-39.69	102.05
3	4	3.30	0.00	-33.61	142.36
4	4	3.30	0.00	-33.61	142.36
4	5	4.40	0.00	-27.57	175.99
5	5	4.40	0.00	-27.57	175.99
5	6	5.50	0.00	-21.51	202.98
6	6	5.50	0.00	-21.51	202.98
6	7	6.60	0.00	-15.44	223.32
7	7	6.60	0.00	-15.44	223.32
7	8	7.70	0.00	-9.40	236.97
8	8	7.70	0.00	-9.40	236.97
8	9	8.80	0.00	-3.32	243.94
9	9	8.80	0.00	-3.32	243.94
9	10	9.90	0.00	2.73	244.27
10	10	9.90	0.00	2.73	244.27
10	11	11.00	0.00	8.79	237.93
11	11	11.00	0.00	8.79	237.93
11	12	12.10	0.00	14.85	224.93
12	12	12.10	0.00	14.85	224.93
12	13	13.20	0.00	20.90	205.23
13	13	13.20	0.00	20.90	205.23
13	14	14.30	0.00	26.97	178.93
14	14	14.30	5.75	25.19	178.93
14	15	15.40	5.75	31.24	145.93
15	15	15.40	0.00	33.02	145.93
15	16	16.50	0.00	45.85	102.54
16	16	16.50	0.00	45.85	102.53
16	17	17.60	0.00	58.66	45.07
17	17	17.60	0.00	58.66	45.06
17	18	18.70	0.00	66.48	-22.87
18	18	18.70	-0.01	66.48	-22.87
18	19	19.80	-0.01	77.56	-102.10
19	19	19.80	0.00	77.56	-102.10
19	20	20.90	0.00	88.62	-193.50
20	20	20.90	0.00	88.62	-193.50
20	21	22.00	0.00	89.50	-301.15
21	1021	22.00	0.00	-100.11	-301.15
21	22	23.40	0.00	-99.02	-146.05
22	22	23.40	0.00	-99.02	-146.05
22	23	24.80	0.00	-84.93	-17.25
23	23	24.80	0.00	-84.92	-17.25
23	24	26.20	0.00	-75.11	94.94
24	24	26.20	0.00	-75.11	94.94
24	25	27.60	0.00	-58.79	188.69
25	25	27.60	-0.01	-58.80	188.69
25	26	29.00	-0.01	-42.49	259.59
26	26	29.00	1.54	-41.90	259.59

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	1.54	-34.19	313.67
27	27	30.40	-0.01	-34.78	313.67
27	28	31.80	-0.01	-27.06	356.94
28	28	31.80	-0.01	-27.06	356.94
28	29	33.20	-0.01	-19.36	389.45
29	29	33.20	-0.01	-19.36	389.45
29	30	34.60	-0.01	-11.64	411.14
30	30	34.60	-0.01	-11.64	411.14
30	31	36.00	-0.01	-3.93	422.04
31	31	36.00	-0.01	-3.93	422.04
31	32	37.40	-0.01	3.78	422.15
32	32	37.40	-0.01	3.78	422.15
32	33	38.80	-0.01	11.50	411.47
33	33	38.80	-0.01	11.50	411.47
33	34	40.20	-0.01	19.19	389.97
34	34	40.20	-0.01	19.19	389.97
34	35	41.60	-0.01	26.91	357.70
35	35	41.60	-1.55	27.49	357.70
35	36	43.00	-1.55	35.20	314.62
36	36	43.00	-0.01	34.62	314.62
36	37	44.40	-0.01	50.93	254.74
37	37	44.40	0.00	50.94	254.73
37	38	45.80	0.00	62.60	172.88
38	38	45.80	0.00	62.60	172.88
38	39	47.20	0.00	76.66	75.41
39	39	47.20	0.00	76.66	75.42
39	40	48.60	0.00	90.75	-41.79
40	40	48.60	0.00	90.75	-41.80
40	41	50.00	0.00	91.84	-185.31
41	1041	50.00	0.00	-91.84	-185.31
41	42	51.40	0.00	-90.75	-41.79
42	42	51.40	0.00	-90.75	-41.79
42	43	52.80	0.00	-76.66	75.42
43	43	52.80	0.00	-76.66	75.41
43	44	54.20	0.00	-62.60	172.87
44	44	54.20	0.00	-62.60	172.87
44	45	55.60	0.00	-50.94	254.74
45	45	55.60	0.00	-50.93	254.73
45	46	57.00	0.00	-34.62	314.63
46	46	57.00	-1.54	-35.21	314.63
46	47	58.40	-1.54	-27.50	357.70
47	47	58.40	0.00	-26.91	357.70
47	48	59.80	0.00	-19.19	389.97
48	48	59.80	0.00	-19.19	389.97
48	49	61.20	0.00	-11.50	411.46
49	49	61.20	0.00	-11.50	411.46
49	50	62.60	0.00	-3.78	422.15
50	50	62.60	0.00	-3.78	422.15
50	51	64.00	0.00	3.93	422.04
51	51	64.00	0.00	3.93	422.04
51	52	65.40	0.00	11.64	411.14

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	11.64	411.14
52	53	66.80	0.00	19.36	389.45
53	53	66.80	0.00	19.36	389.45
53	54	68.20	0.00	27.06	356.95
54	54	68.20	0.00	27.06	356.95
54	55	69.60	0.00	34.78	313.68
55	55	69.60	1.55	34.19	313.68
55	56	71.00	1.55	41.90	259.58
56	56	71.00	0.00	42.49	259.58
56	57	72.40	0.00	58.80	188.70
57	57	72.40	0.00	58.80	188.70
57	58	73.80	0.00	75.12	94.95
58	58	73.80	0.00	75.11	94.95
58	59	75.20	0.00	84.92	-17.26
59	59	75.20	0.00	84.92	-17.25
59	60	76.60	0.00	99.01	-146.05
60	60	76.60	0.00	99.02	-146.05
60	61	78.00	0.00	100.11	-301.15
61	1061	78.00	0.00	-89.50	-301.15
61	62	79.10	0.00	-88.62	-193.51
62	62	79.10	0.00	-88.62	-193.51
62	63	80.20	0.00	-77.56	-102.10
63	63	80.20	0.00	-77.56	-102.09
63	64	81.30	0.00	-66.48	-22.87
64	64	81.30	0.00	-66.48	-22.88
64	65	82.40	0.00	-58.66	45.06
65	65	82.40	0.00	-58.66	45.06
65	66	83.50	0.00	-45.85	102.53
66	66	83.50	0.00	-45.86	102.53
66	67	84.60	0.00	-33.03	145.93
67	67	84.60	5.75	-31.23	145.93
67	68	85.70	5.75	-25.18	178.93
68	68	85.70	0.00	-26.98	178.93
68	69	86.80	0.00	-20.91	205.24
69	69	86.80	0.00	-20.91	205.24
69	70	87.90	0.00	-14.86	224.92
70	70	87.90	0.00	-14.86	224.92
70	71	89.00	0.00	-8.80	237.92
71	71	89.00	0.00	-8.80	237.92
71	72	90.10	0.00	-2.74	244.27
72	72	90.10	0.00	-2.74	244.27
72	73	91.20	0.00	3.31	243.94
73	73	91.20	0.00	3.31	243.94
73	74	92.30	0.00	9.39	236.97
74	74	92.30	0.00	9.39	236.97
74	75	93.40	0.00	15.43	223.32
75	75	93.40	0.00	15.43	223.32
75	76	94.50	0.00	21.50	202.99
76	76	94.50	0.00	21.50	202.99
76	77	95.60	0.00	27.56	176.00
77	77	95.60	0.00	27.56	176.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	33.60	142.35
78	78	96.70	0.00	33.60	142.35
78	79	97.80	0.00	39.68	102.04
79	79	97.80	0.00	39.68	102.04
79	80	98.90	0.00	45.73	55.07
80	80	98.90	0.00	45.73	55.07
80	81	100.00	0.00	37.70	0.00
101	101	0.00	0.00	-37.71	0.00
101	102	1.10	0.00	-45.74	55.07
102	102	1.10	0.00	-45.74	55.07
102	103	2.20	0.00	-39.69	102.05
103	103	2.20	0.00	-39.69	102.05
103	104	3.30	0.00	-33.61	142.36
104	104	3.30	0.00	-33.61	142.36
104	105	4.40	0.00	-27.57	176.00
105	105	4.40	0.00	-27.57	176.00
105	106	5.50	0.00	-21.51	202.99
106	106	5.50	0.00	-21.51	202.99
106	107	6.60	0.00	-15.44	223.32
107	107	6.60	0.00	-15.44	223.32
107	108	7.70	0.00	-9.40	236.97
108	108	7.70	0.00	-9.40	236.97
108	109	8.80	0.00	-3.32	243.94
109	109	8.80	0.00	-3.32	243.94
109	110	9.90	0.00	2.73	244.27
110	110	9.90	0.00	2.73	244.27
110	111	11.00	0.00	8.79	237.93
111	111	11.00	0.00	8.79	237.93
111	112	12.10	0.00	14.85	224.93
112	112	12.10	0.00	14.85	224.93
112	113	13.20	0.00	20.90	205.24
113	113	13.20	0.00	20.90	205.24
113	114	14.30	0.00	26.97	178.93
114	114	14.30	5.75	25.19	178.93
114	115	15.40	5.75	31.24	145.93
115	115	15.40	0.00	33.02	145.93
115	116	16.50	0.00	45.85	102.53
116	116	16.50	0.00	45.85	102.53
116	117	17.60	0.00	58.66	45.06
117	117	17.60	0.00	58.66	45.07
117	118	18.70	0.00	66.48	-22.87
118	118	18.70	0.00	66.48	-22.87
118	119	19.80	0.00	77.56	-102.09
119	119	19.80	0.00	77.56	-102.09
119	120	20.90	0.00	88.62	-193.50
120	120	20.90	0.00	88.62	-193.50
120	121	22.00	0.00	89.50	-301.15
121	1121	22.00	0.00	-100.11	-301.15
121	122	23.40	0.00	-99.02	-146.05
122	122	23.40	0.00	-99.02	-146.05
122	123	24.80	0.00	-84.93	-17.26

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-84.92	-17.25
123	124	26.20	0.00	-75.11	94.94
124	124	26.20	0.00	-75.11	94.94
124	125	27.60	0.00	-58.79	188.68
125	125	27.60	-0.01	-58.80	188.68
125	126	29.00	-0.01	-42.49	259.58
126	126	29.00	1.54	-41.90	259.58
126	127	30.40	1.54	-34.19	313.67
127	127	30.40	-0.01	-34.78	313.67
127	128	31.80	-0.01	-27.06	356.94
128	128	31.80	-0.01	-27.06	356.94
128	129	33.20	-0.01	-19.36	389.45
129	129	33.20	-0.01	-19.36	389.45
129	130	34.60	-0.01	-11.64	411.14
130	130	34.60	-0.01	-11.64	411.14
130	131	36.00	-0.01	-3.93	422.05
131	131	36.00	-0.01	-3.93	422.05
131	132	37.40	-0.01	3.78	422.14
132	132	37.40	-0.01	3.78	422.14
132	133	38.80	-0.01	11.50	411.46
133	133	38.80	-0.01	11.50	411.46
133	134	40.20	-0.01	19.19	389.97
134	134	40.20	-0.01	19.19	389.97
134	135	41.60	-0.01	26.91	357.70
135	135	41.60	-1.55	27.49	357.70
135	136	43.00	-1.55	35.20	314.62
136	136	43.00	-0.01	34.62	314.62
136	137	44.40	-0.01	50.93	254.74
137	137	44.40	0.00	50.93	254.73
137	138	45.80	0.00	62.59	172.88
138	138	45.80	0.00	62.60	172.88
138	139	47.20	0.00	76.66	75.42
139	139	47.20	0.00	76.66	75.42
139	140	48.60	0.00	90.75	-41.78
140	140	48.60	0.00	90.75	-41.79
140	141	50.00	0.00	91.84	-185.29
141	1141	50.00	0.00	-91.84	-185.29
141	142	51.40	0.00	-90.75	-41.79
142	142	51.40	0.00	-90.74	-41.79
142	143	52.80	0.00	-76.65	75.43
143	143	52.80	0.00	-76.66	75.43
143	144	54.20	0.00	-62.60	172.88
144	144	54.20	0.00	-62.60	172.88
144	145	55.60	0.00	-50.94	254.74
145	145	55.60	0.00	-50.93	254.74
145	146	57.00	0.00	-34.62	314.62
146	146	57.00	-1.55	-35.21	314.62
146	147	58.40	-1.55	-27.50	357.71
147	147	58.40	0.00	-26.91	357.71
147	148	59.80	0.00	-19.19	389.97
148	148	59.80	0.00	-19.19	389.97

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-11.50	411.46
149	149	61.20	0.00	-11.50	411.46
149	150	62.60	0.00	-3.78	422.15
150	150	62.60	0.00	-3.78	422.15
150	151	64.00	0.00	3.93	422.04
151	151	64.00	0.00	3.93	422.04
151	152	65.40	0.00	11.64	411.14
152	152	65.40	0.00	11.64	411.14
152	153	66.80	0.00	19.36	389.45
153	153	66.80	0.00	19.36	389.45
153	154	68.20	0.00	27.06	356.94
154	154	68.20	0.00	27.06	356.94
154	155	69.60	0.00	34.78	313.67
155	155	69.60	1.55	34.19	313.67
155	156	71.00	1.55	41.90	259.57
156	156	71.00	0.00	42.49	259.57
156	157	72.40	0.00	58.80	188.69
157	157	72.40	0.00	58.80	188.69
157	158	73.80	0.00	75.12	94.94
158	158	73.80	0.00	75.11	94.94
158	159	75.20	0.00	84.92	-17.26
159	159	75.20	0.00	84.92	-17.26
159	160	76.60	0.00	99.01	-146.05
160	160	76.60	0.00	99.02	-146.05
160	161	78.00	0.00	100.11	-301.14
161	1161	78.00	0.00	-89.50	-301.15
161	162	79.10	0.00	-88.62	-193.50
162	162	79.10	0.00	-88.62	-193.50
162	163	80.20	0.00	-77.56	-102.09
163	163	80.20	0.00	-77.56	-102.09
163	164	81.30	0.00	-66.48	-22.87
164	164	81.30	0.00	-66.48	-22.88
164	165	82.40	0.00	-58.66	45.07
165	165	82.40	0.00	-58.66	45.07
165	166	83.50	0.00	-45.85	102.54
166	166	83.50	0.00	-45.86	102.53
166	167	84.60	0.00	-33.03	145.93
167	167	84.60	5.75	-31.23	145.93
167	168	85.70	5.75	-25.18	178.93
168	168	85.70	0.00	-26.98	178.93
168	169	86.80	0.00	-20.91	205.24
169	169	86.80	0.00	-20.91	205.24
169	170	87.90	0.00	-14.86	224.93
170	170	87.90	0.00	-14.86	224.93
170	171	89.00	0.00	-8.80	237.93
171	171	89.00	0.00	-8.80	237.93
171	172	90.10	0.00	-2.74	244.27
172	172	90.10	0.00	-2.74	244.27
172	173	91.20	0.00	3.31	243.94
173	173	91.20	0.00	3.31	243.94
173	174	92.30	0.00	9.39	236.97

CÁLCULO TENSIONAL

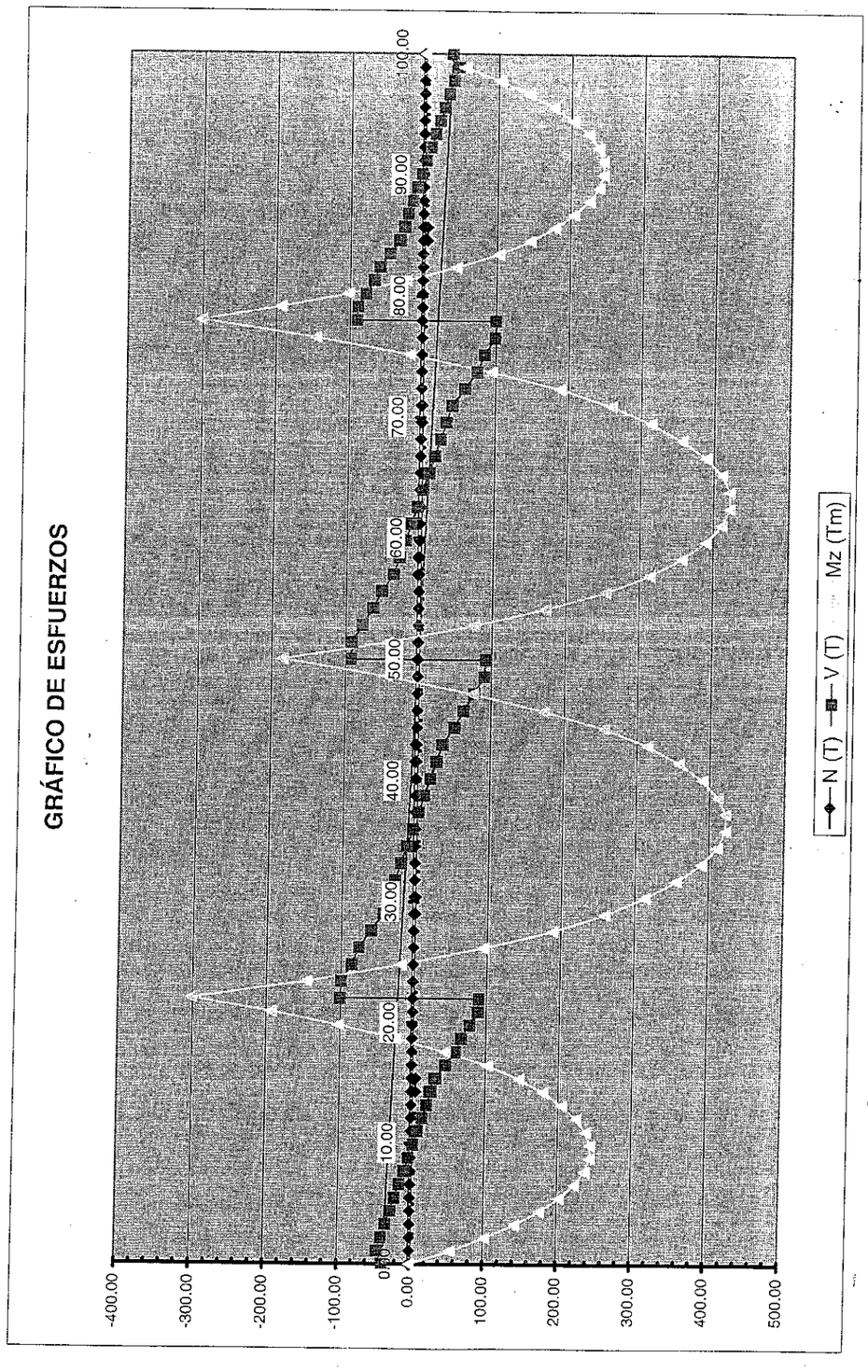
Hipótesis de cálculo:
FASE2.T0.MZ+

Construcción fase 2 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	9.39	236.97
174	175	93.40	0.00	15.43	223.32
175	175	93.40	0.00	15.43	223.32
175	176	94.50	0.00	21.50	202.99
176	176	94.50	0.00	21.50	202.99
176	177	95.60	0.00	27.56	176.00
177	177	95.60	0.00	27.56	176.00
177	178	96.70	0.00	33.60	142.35
178	178	96.70	0.00	33.60	142.35
178	179	97.80	0.00	39.68	102.04
179	179	97.80	0.00	39.68	102.04
179	180	98.90	0.00	45.73	55.07
180	180	98.90	0.00	45.73	55.07
180	181	100.00	0.00	37.70	0.00



CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-37.71	0.00
1	2	1.10	0.00	-31.30	37.95
2	2	1.10	0.00	-31.30	37.95
2	3	2.20	0.00	-26.82	69.92
3	3	2.20	0.00	-26.82	69.92
3	4	3.30	0.00	-22.32	96.94
4	4	3.30	0.00	-22.32	96.94
4	5	4.40	0.00	-17.84	119.01
5	5	4.40	0.00	-17.84	119.01
5	6	5.50	0.00	-13.35	136.16
6	6	5.50	0.00	-13.35	136.16
6	7	6.60	0.00	-8.86	148.39
7	7	6.60	0.00	-8.86	148.39
7	8	7.70	0.00	-4.38	155.66
8	8	7.70	0.00	-4.38	155.66
8	9	8.80	0.00	0.12	157.99
9	9	8.80	0.00	0.12	157.99
9	10	9.90	0.00	4.60	155.39
10	10	9.90	0.00	4.60	155.39
10	11	11.00	0.00	9.09	147.86
11	11	11.00	0.00	9.09	147.86
11	12	12.10	0.00	13.58	135.39
12	12	12.10	0.00	13.58	135.39
12	13	13.20	0.00	18.06	117.96
13	13	13.20	0.00	18.06	117.96
13	14	14.30	0.00	22.56	95.64
14	14	14.30	5.75	20.78	95.64
14	15	15.40	5.75	25.26	68.36
15	15	15.40	0.00	27.04	68.36
15	16	16.50	0.00	36.54	33.38
16	16	16.50	0.00	36.54	33.37
16	17	17.60	0.00	46.03	-12.03
17	17	17.60	0.00	46.03	-12.04
17	18	18.70	0.00	60.51	-71.53
18	18	18.70	-0.01	60.51	-71.53
18	19	19.80	-0.01	71.76	-144.27
19	19	19.80	0.00	71.76	-144.27
19	20	20.90	0.00	83.00	-229.40
20	20	20.90	0.00	83.00	-229.40
20	21	22.00	0.00	99.74	-329.91
21	1021	22.00	0.00	-111.05	-329.91
21	22	23.40	0.00	-89.74	-189.35
22	22	23.40	0.00	-89.74	-189.35
22	23	24.80	0.00	-75.42	-73.71
23	23	24.80	0.00	-75.41	-73.71
23	24	26.20	0.00	-56.86	18.70
24	24	26.20	0.00	-56.86	18.70
24	25	27.60	0.00	-44.77	89.86
25	25	27.60	-0.01	-44.78	89.86
25	26	29.00	-0.01	-32.70	144.10
26	26	29.00	1.54	-32.11	144.10

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	1.54	-26.40	185.87
27	27	30.40	-0.01	-26.99	185.87
27	28	31.80	-0.01	-21.27	219.63
28	28	31.80	-0.01	-21.27	219.63
28	29	33.20	-0.01	-15.57	245.43
29	29	33.20	-0.01	-15.57	245.43
29	30	34.60	-0.01	-9.85	263.21
30	30	34.60	-0.01	-9.85	263.21
30	31	36.00	-0.01	-4.14	273.00
31	31	36.00	-0.01	-4.14	273.00
31	32	37.40	-0.01	1.57	274.80
32	32	37.40	-0.01	1.57	274.80
32	33	38.80	-0.01	7.29	268.60
33	33	38.80	-0.01	7.29	268.60
33	34	40.20	-0.01	12.99	254.39
34	34	40.20	-0.01	12.99	254.39
34	35	41.60	-0.01	18.71	232.20
35	35	41.60	-1.55	19.29	232.20
35	36	43.00	-1.55	25.00	202.00
36	36	43.00	-0.01	24.42	202.00
36	37	44.40	-0.01	36.50	159.36
37	37	44.40	0.00	36.51	159.35
37	38	45.80	0.00	53.27	98.92
38	38	45.80	0.00	53.27	98.92
38	39	47.20	0.00	67.57	14.35
39	39	47.20	0.00	67.57	14.36
39	40	48.60	0.00	81.88	-90.26
40	40	48.60	0.00	81.88	-90.27
40	41	50.00	0.00	103.19	-219.82
41	1041	50.00	0.00	-103.19	-219.82
41	42	51.40	0.00	-81.88	-90.26
42	42	51.40	0.00	-81.88	-90.26
42	43	52.80	0.00	-67.57	14.36
43	43	52.80	0.00	-67.57	14.35
43	44	54.20	0.00	-53.27	98.91
44	44	54.20	0.00	-53.27	98.91
44	45	55.60	0.00	-36.51	159.36
45	45	55.60	0.00	-36.50	159.35
45	46	57.00	0.00	-24.42	202.01
46	46	57.00	-1.54	-25.01	202.01
46	47	58.40	-1.54	-19.30	232.20
47	47	58.40	0.00	-18.71	232.20
47	48	59.80	0.00	-12.99	254.39
48	48	59.80	0.00	-12.99	254.39
48	49	61.20	0.00	-7.29	268.59
49	49	61.20	0.00	-7.29	268.59
49	50	62.60	0.00	-1.57	274.80
50	50	62.60	0.00	-1.57	274.80
50	51	64.00	0.00	4.14	273.00
51	51	64.00	0.00	4.14	273.00
51	52	65.40	0.00	9.85	263.21

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	9.85	263.21
52	53	66.80	0.00	15.57	245.43
53	53	66.80	0.00	15.57	245.43
53	54	68.20	0.00	21.27	219.64
54	54	68.20	0.00	21.27	219.64
54	55	69.60	0.00	26.99	185.88
55	55	69.60	1.55	26.40	185.88
55	56	71.00	1.55	32.11	144.09
56	56	71.00	0.00	32.70	144.09
56	57	72.40	0.00	44.78	89.87
57	57	72.40	0.00	44.78	89.87
57	58	73.80	0.00	56.87	18.71
58	58	73.80	0.00	56.86	18.71
58	59	75.20	0.00	75.41	-73.72
59	59	75.20	0.00	75.41	-73.71
59	60	76.60	0.00	89.73	-189.35
60	60	76.60	0.00	89.74	-189.35
60	61	78.00	0.00	111.05	-329.91
61	1061	78.00	0.00	-99.74	-329.91
61	62	79.10	0.00	-83.00	-229.41
62	62	79.10	0.00	-83.00	-229.41
62	63	80.20	0.00	-71.76	-144.27
63	63	80.20	0.00	-71.76	-144.26
63	64	81.30	0.00	-60.51	-71.53
64	64	81.30	0.00	-60.51	-71.54
64	65	82.40	0.00	-46.03	-12.04
65	65	82.40	0.00	-46.03	-12.04
65	66	83.50	0.00	-36.54	33.37
66	66	83.50	0.00	-36.55	33.37
66	67	84.60	0.00	-27.05	68.36
67	67	84.60	5.75	-25.25	68.36
67	68	85.70	5.75	-20.77	95.64
68	68	85.70	0.00	-22.57	95.64
68	69	86.80	0.00	-18.07	117.97
69	69	86.80	0.00	-18.07	117.97
69	70	87.90	0.00	-13.59	135.38
70	70	87.90	0.00	-13.59	135.38
70	71	89.00	0.00	-9.10	147.85
71	71	89.00	0.00	-9.10	147.85
71	72	90.10	0.00	-4.61	155.39
72	72	90.10	0.00	-4.61	155.39
72	73	91.20	0.00	-0.13	157.99
73	73	91.20	0.00	-0.13	157.99
73	74	92.30	0.00	4.37	155.66
74	74	92.30	0.00	4.37	155.66
74	75	93.40	0.00	8.85	148.39
75	75	93.40	0.00	8.85	148.39
75	76	94.50	0.00	13.34	136.17
76	76	94.50	0.00	13.34	136.17
76	77	95.60	0.00	17.83	119.02
77	77	95.60	0.00	17.83	119.02

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	22.31	96.93
78	78	96.70	0.00	22.31	96.93
78	79	97.80	0.00	26.81	69.91
79	79	97.80	0.00	26.81	69.91
79	80	98.90	0.00	31.29	37.95
80	80	98.90	0.00	31.29	37.95
80	81	100.00	0.00	37.70	0.00
101	101	0.00	0.00	-37.71	0.00
101	102	1.10	0.00	-31.30	37.95
102	102	1.10	0.00	-31.30	37.95
102	103	2.20	0.00	-26.82	69.92
103	103	2.20	0.00	-26.82	69.92
103	104	3.30	0.00	-22.32	96.94
104	104	3.30	0.00	-22.32	96.94
104	105	4.40	0.00	-17.84	119.02
105	105	4.40	0.00	-17.84	119.02
105	106	5.50	0.00	-13.35	136.17
106	106	5.50	0.00	-13.35	136.17
106	107	6.60	0.00	-8.86	148.39
107	107	6.60	0.00	-8.86	148.39
107	108	7.70	0.00	-4.38	155.66
108	108	7.70	0.00	-4.38	155.66
108	109	8.80	0.00	0.12	157.99
109	109	8.80	0.00	0.12	157.99
109	110	9.90	0.00	4.60	155.39
110	110	9.90	0.00	4.60	155.39
110	111	11.00	0.00	9.09	147.86
111	111	11.00	0.00	9.09	147.86
111	112	12.10	0.00	13.58	135.39
112	112	12.10	0.00	13.58	135.39
112	113	13.20	0.00	18.06	117.97
113	113	13.20	0.00	18.06	117.97
113	114	14.30	0.00	22.56	95.64
114	114	14.30	5.75	20.78	95.64
114	115	15.40	5.75	25.26	68.36
115	115	15.40	0.00	27.04	68.36
115	116	16.50	0.00	36.54	33.37
116	116	16.50	0.00	36.54	33.37
116	117	17.60	0.00	46.03	-12.04
117	117	17.60	0.00	46.03	-12.03
117	118	18.70	0.00	60.51	-71.53
118	118	18.70	0.00	60.51	-71.53
118	119	19.80	0.00	71.76	-144.26
119	119	19.80	0.00	71.76	-144.26
119	120	20.90	0.00	83.00	-229.40
120	120	20.90	0.00	83.00	-229.40
120	121	22.00	0.00	99.74	-329.91
121	1121	22.00	0.00	-111.05	-329.91
121	122	23.40	0.00	-89.74	-189.35
122	122	23.40	0.00	-89.74	-189.35
122	123	24.80	0.00	-75.42	-73.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-75.41	-73.71
123	124	26.20	0.00	-56.86	18.70
124	124	26.20	0.00	-56.86	18.70
124	125	27.60	0.00	-44.77	89.85
125	125	27.60	-0.01	-44.78	89.85
125	126	29.00	-0.01	-32.70	144.09
126	126	29.00	1.54	-32.11	144.09
126	127	30.40	1.54	-26.40	185.87
127	127	30.40	-0.01	-26.99	185.87
127	128	31.80	-0.01	-21.27	219.63
128	128	31.80	-0.01	-21.27	219.63
128	129	33.20	-0.01	-15.57	245.43
129	129	33.20	-0.01	-15.57	245.43
129	130	34.60	-0.01	-9.85	263.21
130	130	34.60	-0.01	-9.85	263.21
130	131	36.00	-0.01	-4.14	273.01
131	131	36.00	-0.01	-4.14	273.01
131	132	37.40	-0.01	1.57	274.79
132	132	37.40	-0.01	1.57	274.79
132	133	38.80	-0.01	7.29	268.59
133	133	38.80	-0.01	7.29	268.59
133	134	40.20	-0.01	12.99	254.39
134	134	40.20	-0.01	12.99	254.39
134	135	41.60	-0.01	18.71	232.20
135	135	41.60	-1.55	19.29	232.20
135	136	43.00	-1.55	25.00	202.00
136	136	43.00	-0.01	24.42	202.00
136	137	44.40	-0.01	36.50	159.36
137	137	44.40	0.00	36.50	159.35
137	138	45.80	0.00	53.26	98.92
138	138	45.80	0.00	53.27	98.92
138	139	47.20	0.00	67.57	14.36
139	139	47.20	0.00	67.57	14.36
139	140	48.60	0.00	81.88	-90.25
140	140	48.60	0.00	81.88	-90.26
140	141	50.00	0.00	103.19	-219.80
141	1141	50.00	0.00	-103.19	-219.80
141	142	51.40	0.00	-81.88	-90.26
142	142	51.40	0.00	-81.87	-90.26
142	143	52.80	0.00	-67.56	14.37
143	143	52.80	0.00	-67.57	14.37
143	144	54.20	0.00	-53.27	98.92
144	144	54.20	0.00	-53.27	98.92
144	145	55.60	0.00	-36.51	159.36
145	145	55.60	0.00	-36.50	159.36
145	146	57.00	0.00	-24.42	202.00
146	146	57.00	-1.55	-25.01	202.00
146	147	58.40	-1.55	-19.30	232.21
147	147	58.40	0.00	-18.71	232.21
147	148	59.80	0.00	-12.99	254.39
148	148	59.80	0.00	-12.99	254.39

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-7.29	268.59
149	149	61.20	0.00	-7.29	268.59
149	150	62.60	0.00	-1.57	274.80
150	150	62.60	0.00	-1.57	274.80
150	151	64.00	0.00	4.14	273.00
151	151	64.00	0.00	4.14	273.00
151	152	65.40	0.00	9.85	263.21
152	152	65.40	0.00	9.85	263.21
152	153	66.80	0.00	15.57	245.43
153	153	66.80	0.00	15.57	245.43
153	154	68.20	0.00	21.27	219.63
154	154	68.20	0.00	21.27	219.63
154	155	69.60	0.00	26.99	185.87
155	155	69.60	1.55	26.40	185.87
155	156	71.00	1.55	32.11	144.08
156	156	71.00	0.00	32.70	144.08
156	157	72.40	0.00	44.78	89.86
157	157	72.40	0.00	44.78	89.86
157	158	73.80	0.00	56.87	18.70
158	158	73.80	0.00	56.86	18.70
158	159	75.20	0.00	75.41	-73.72
159	159	75.20	0.00	75.41	-73.72
159	160	76.60	0.00	89.73	-189.35
160	160	76.60	0.00	89.74	-189.35
160	161	78.00	0.00	111.05	-329.90
161	1161	78.00	0.00	-99.74	-329.91
161	162	79.10	0.00	-83.00	-229.40
162	162	79.10	0.00	-83.00	-229.40
162	163	80.20	0.00	-71.76	-144.26
163	163	80.20	0.00	-71.76	-144.26
163	164	81.30	0.00	-60.51	-71.53
164	164	81.30	0.00	-60.51	-71.54
164	165	82.40	0.00	-46.03	-12.03
165	165	82.40	0.00	-46.03	-12.03
165	166	83.50	0.00	-36.54	33.38
166	166	83.50	0.00	-36.55	33.37
166	167	84.60	0.00	-27.05	68.36
167	167	84.60	5.75	-25.25	68.36
167	168	85.70	5.75	-20.77	95.64
168	168	85.70	0.00	-22.57	95.64
168	169	86.80	0.00	-18.07	117.97
169	169	86.80	0.00	-18.07	117.97
169	170	87.90	0.00	-13.59	135.39
170	170	87.90	0.00	-13.59	135.39
170	171	89.00	0.00	-9.10	147.86
171	171	89.00	0.00	-9.10	147.86
171	172	90.10	0.00	-4.61	155.39
172	172	90.10	0.00	-4.61	155.39
172	173	91.20	0.00	-0.13	157.99
173	173	91.20	0.00	-0.13	157.99
173	174	92.30	0.00	4.37	155.66

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE2.T0.MZ-

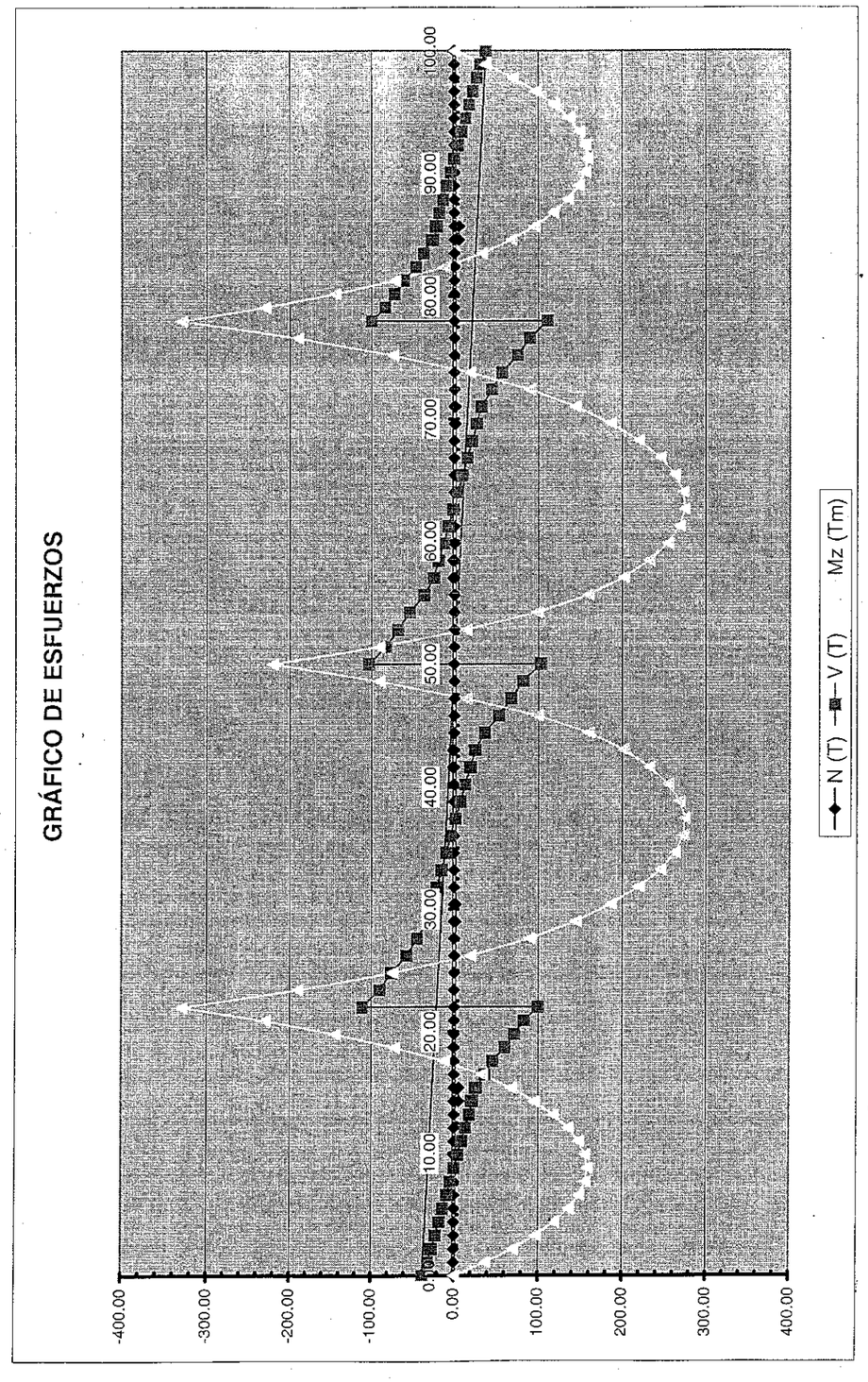
Construcción fase 2 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	4.37	155.66
174	175	93.40	0.00	8.85	148.39
175	175	93.40	0.00	8.85	148.39
175	176	94.50	0.00	13.34	136.17
176	176	94.50	0.00	13.34	136.17
176	177	95.60	0.00	17.83	119.02
177	177	95.60	0.00	17.83	119.02
177	178	96.70	0.00	22.31	96.93
178	178	96.70	0.00	22.31	96.93
178	179	97.80	0.00	26.81	69.91
179	179	97.80	0.00	26.81	69.91
179	180	98.90	0.00	31.29	37.95
180	180	98.90	0.00	31.29	37.95
180	181	100.00	0.00	37.70	0.00

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	14.61	-58.04	306.19
27	27	30.40	-0.01	-61.97	306.19
27	28	31.80	-0.01	-55.17	392.21
28	28	31.80	-0.01	-55.17	392.21
28	29	33.20	-0.01	-38.87	458.06
29	29	33.20	-0.01	-38.87	458.06
29	30	34.60	-0.01	-22.55	501.05
30	30	34.60	-0.01	-22.55	501.05
30	31	36.00	-0.01	-6.24	521.21
31	31	36.00	-0.01	-6.24	521.21
31	32	37.40	-0.01	10.07	518.54
32	32	37.40	-0.01	10.07	518.54
32	33	38.80	-0.01	26.39	493.04
33	33	38.80	-0.01	26.39	493.04
33	34	40.20	-0.01	42.68	444.69
34	34	40.20	-0.01	42.68	444.69
34	35	41.60	-0.01	59.00	373.51
35	35	41.60	13.87	55.63	373.51
35	36	43.00	13.36	62.41	287.97
36	36	43.00	-0.01	65.65	287.97
36	37	44.40	-0.01	81.96	184.65
37	37	44.40	0.00	81.97	184.64
37	38	45.80	0.00	93.63	59.35
38	38	45.80	0.00	93.63	59.35
38	39	47.20	0.00	107.69	-81.56
39	39	47.20	0.00	107.69	-81.55
39	40	48.60	0.00	121.78	-242.20
40	40	48.60	0.00	121.78	-242.21
40	41	50.00	0.00	122.87	-429.16
41	1041	50.00	0.00	-122.87	-429.16
41	42	51.40	0.00	-121.78	-242.20
42	42	51.40	0.00	-121.78	-242.20
42	43	52.80	0.00	-107.69	-81.55
43	43	52.80	0.00	-107.69	-81.56
43	44	54.20	0.00	-93.63	59.34
44	44	54.20	0.00	-93.63	59.34
44	45	55.60	0.00	-81.97	184.65
45	45	55.60	0.00	-81.96	184.64
45	46	57.00	0.00	-65.65	287.98
46	46	57.00	13.37	-62.42	287.98
46	47	58.40	13.88	-55.64	373.51
47	47	58.40	0.00	-59.00	373.51
47	48	59.80	0.00	-42.68	444.69
48	48	59.80	0.00	-42.68	444.69
48	49	61.20	0.00	-26.39	493.03
49	49	61.20	0.00	-26.39	493.03
49	50	62.60	0.00	-10.07	518.54
50	50	62.60	0.00	-10.07	518.54
50	51	64.00	0.00	6.24	521.21
51	51	64.00	0.00	6.24	521.21
51	52	65.40	0.00	22.55	501.05

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	22.55	501.05
52	53	66.80	0.00	38.87	458.06
53	53	66.80	0.00	38.87	458.06
53	54	68.20	0.00	55.17	392.22
54	54	68.20	0.00	55.17	392.22
54	55	69.60	0.00	61.97	306.20
55	55	69.60	14.62	58.04	306.20
55	56	71.00	18.11	72.12	208.94
56	56	71.00	0.00	76.95	208.94
56	57	72.40	0.00	93.26	89.82
57	57	72.40	0.00	93.26	89.82
57	58	73.80	0.00	109.58	-52.17
58	58	73.80	0.00	109.57	-52.17
58	59	75.20	0.00	119.38	-212.62
59	59	75.20	0.00	119.38	-212.61
59	60	76.60	0.00	133.47	-389.65
60	60	76.60	0.00	133.48	-389.65
60	61	78.00	0.00	134.57	-592.99
61	1061	78.00	0.00	-128.03	-592.99
61	62	79.10	0.00	-127.15	-442.97
62	62	79.10	0.00	-127.15	-442.97
62	63	80.20	0.00	-116.09	-309.17
63	63	80.20	0.00	-116.09	-309.16
63	64	81.30	0.00	-105.01	-187.56
64	64	81.30	0.00	-105.01	-187.57
64	65	82.40	0.00	-97.19	-77.24
65	65	82.40	0.00	-97.19	-77.24
65	66	83.50	0.00	-84.38	22.61
66	66	83.50	0.00	-84.39	22.61
66	67	84.60	0.00	-71.56	108.39
67	67	84.60	27.79	-62.83	108.39
67	68	85.70	30.79	-61.09	180.94
68	68	85.70	0.00	-70.76	180.94
68	69	86.80	0.00	-57.93	251.70
69	69	86.80	0.00	-57.93	251.70
69	70	87.90	0.00	-45.13	308.37
70	70	87.90	0.00	-45.13	308.37
70	71	89.00	0.00	-32.30	350.95
71	71	89.00	0.00	-32.30	350.95
71	72	90.10	0.00	-19.49	379.44
72	72	90.10	0.00	-19.49	379.44
72	73	91.20	0.00	-6.68	393.83
73	73	91.20	0.00	-6.68	393.83
73	74	92.30	0.00	6.15	394.13
74	74	92.30	0.00	6.15	394.13
74	75	93.40	0.00	18.96	380.32
75	75	93.40	0.00	18.96	380.32
75	76	94.50	0.00	31.77	352.41
76	76	94.50	0.00	31.77	352.41
76	77	95.60	0.00	44.59	310.41
77	77	95.60	0.00	44.59	310.41

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
FASE3.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	57.39	254.31
78	78	96.70	0.00	57.39	254.31
78	79	97.80	0.00	70.23	184.11
79	79	97.80	0.00	70.23	184.11
79	80	98.90	0.00	83.03	99.82
80	80	98.90	0.00	83.03	99.82
80	81	100.00	0.00	70.34	0.00
101	101	0.00	0.00	-70.35	0.00
101	102	1.10	0.00	-83.04	99.82
102	102	1.10	0.00	-83.04	99.82
102	103	2.20	0.00	-70.24	184.12
103	103	2.20	0.00	-70.24	184.12
103	104	3.30	0.00	-57.40	254.32
104	104	3.30	0.00	-57.40	254.32
104	105	4.40	0.00	-44.60	310.41
105	105	4.40	0.00	-44.60	310.41
105	106	5.50	0.00	-31.78	352.41
106	106	5.50	0.00	-31.78	352.41
106	107	6.60	0.00	-18.97	380.32
107	107	6.60	0.00	-18.97	380.32
107	108	7.70	0.00	-6.16	394.13
108	108	7.70	0.00	-6.16	394.13
108	109	8.80	0.00	6.67	393.83
109	109	8.80	0.00	6.67	393.83
109	110	9.90	0.00	19.48	379.44
110	110	9.90	0.00	19.48	379.44
110	111	11.00	0.00	32.29	350.96
111	111	11.00	0.00	32.29	350.96
111	112	12.10	0.00	45.12	308.38
112	112	12.10	0.00	45.12	308.38
112	113	13.20	0.00	57.92	251.70
113	113	13.20	0.00	57.92	251.70
113	114	14.30	0.00	70.75	180.94
114	114	14.30	30.79	61.10	180.94
114	115	15.40	27.79	62.84	108.39
115	115	15.40	0.00	71.55	108.39
115	116	16.50	0.00	84.38	22.61
116	116	16.50	0.00	84.38	22.61
116	117	17.60	0.00	97.19	-77.25
117	117	17.60	0.00	97.19	-77.24
117	118	18.70	0.00	105.01	-187.56
118	118	18.70	0.00	105.01	-187.56
118	119	19.80	0.00	116.09	-309.16
119	119	19.80	0.00	116.09	-309.16
119	120	20.90	0.00	127.15	-442.96
120	120	20.90	0.00	127.15	-442.96
120	121	22.00	0.00	128.03	-592.99
121	1121	22.00	0.00	-134.57	-592.99
121	122	23.40	0.00	-133.48	-389.65
122	122	23.40	0.00	-133.48	-389.65
122	123	24.80	0.00	-119.39	-212.62

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-119.38	-212.61
123	124	26.20	0.00	-109.57	-52.18
124	124	26.20	0.00	-109.57	-52.18
124	125	27.60	0.00	-93.25	89.80
125	125	27.60	-0.01	-93.26	89.80
125	126	29.00	-0.01	-76.95	208.94
126	126	29.00	18.10	-72.12	208.94
126	127	30.40	14.61	-58.04	306.19
127	127	30.40	-0.01	-61.97	306.19
127	128	31.80	-0.01	-55.17	392.21
128	128	31.80	-0.01	-55.17	392.21
128	129	33.20	-0.01	-38.87	458.07
129	129	33.20	-0.01	-38.87	458.07
129	130	34.60	-0.01	-22.55	501.05
130	130	34.60	-0.01	-22.55	501.05
130	131	36.00	-0.01	-6.24	521.22
131	131	36.00	-0.01	-6.24	521.22
131	132	37.40	-0.01	10.07	518.53
132	132	37.40	-0.01	10.07	518.53
132	133	38.80	-0.01	26.39	493.03
133	133	38.80	-0.01	26.39	493.03
133	134	40.20	-0.01	42.68	444.69
134	134	40.20	-0.01	42.68	444.69
134	135	41.60	-0.01	59.00	373.51
135	135	41.60	13.87	55.63	373.51
135	136	43.00	13.36	62.41	287.97
136	136	43.00	-0.01	65.65	287.97
136	137	44.40	-0.01	81.96	184.65
137	137	44.40	0.00	81.96	184.64
137	138	45.80	0.00	93.62	59.35
138	138	45.80	0.00	93.63	59.35
138	139	47.20	0.00	107.69	-81.55
139	139	47.20	0.00	107.69	-81.55
139	140	48.60	0.00	121.78	-242.20
140	140	48.60	0.00	121.78	-242.21
140	141	50.00	0.00	122.87	-429.15
141	1141	50.00	0.00	-122.87	-429.15
141	142	51.40	0.00	-121.78	-242.21
142	142	51.40	0.00	-121.77	-242.21
142	143	52.80	0.00	-107.68	-81.54
143	143	52.80	0.00	-107.69	-81.54
143	144	54.20	0.00	-93.63	59.35
144	144	54.20	0.00	-93.63	59.35
144	145	55.60	0.00	-81.97	184.65
145	145	55.60	0.00	-81.96	184.65
145	146	57.00	0.00	-65.65	287.97
146	146	57.00	13.36	-62.42	287.97
146	147	58.40	13.87	-55.64	373.52
147	147	58.40	0.00	-59.00	373.52
147	148	59.80	0.00	-42.68	444.69
148	148	59.80	0.00	-42.68	444.69

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FASE3.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-26.39	493.03
149	149	61.20	0.00	-26.39	493.03
149	150	62.60	0.00	-10.07	518.54
150	150	62.60	0.00	-10.07	518.54
150	151	64.00	0.00	6.24	521.21
151	151	64.00	0.00	6.24	521.21
151	152	65.40	0.00	22.55	501.05
152	152	65.40	0.00	22.55	501.05
152	153	66.80	0.00	38.87	458.07
153	153	66.80	0.00	38.87	458.07
153	154	68.20	0.00	55.17	392.21
154	154	68.20	0.00	55.17	392.21
154	155	69.60	0.00	61.97	306.19
155	155	69.60	14.62	58.04	306.19
155	156	71.00	18.11	72.12	208.93
156	156	71.00	0.00	76.95	208.93
156	157	72.40	0.00	93.26	89.81
157	157	72.40	0.00	93.26	89.81
157	158	73.80	0.00	109.58	-52.18
158	158	73.80	0.00	109.57	-52.18
158	159	75.20	0.00	119.38	-212.62
159	159	75.20	0.00	119.38	-212.62
159	160	76.60	0.00	133.47	-389.65
160	160	76.60	0.00	133.48	-389.65
160	161	78.00	0.00	134.57	-592.98
161	1161	78.00	0.00	-128.03	-592.99
161	162	79.10	0.00	-127.15	-442.96
162	162	79.10	0.00	-127.15	-442.96
162	163	80.20	0.00	-116.09	-309.16
163	163	80.20	0.00	-116.09	-309.16
163	164	81.30	0.00	-105.01	-187.56
164	164	81.30	0.00	-105.01	-187.57
164	165	82.40	0.00	-97.19	-77.24
165	165	82.40	0.00	-97.19	-77.24
165	166	83.50	0.00	-84.38	22.62
166	166	83.50	0.00	-84.39	22.61
166	167	84.60	0.00	-71.56	108.39
167	167	84.60	27.79	-62.83	108.39
167	168	85.70	30.79	-61.09	180.94
168	168	85.70	0.00	-70.76	180.94
168	169	86.80	0.00	-57.93	251.70
169	169	86.80	0.00	-57.93	251.70
169	170	87.90	0.00	-45.13	308.38
170	170	87.90	0.00	-45.13	308.38
170	171	89.00	0.00	-32.30	350.96
171	171	89.00	0.00	-32.30	350.96
171	172	90.10	0.00	-19.49	379.44
172	172	90.10	0.00	-19.49	379.44
172	173	91.20	0.00	-6.68	393.83
173	173	91.20	0.00	-6.68	393.83
173	174	92.30	0.00	6.15	394.13

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ+

Construcción fase 3 Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

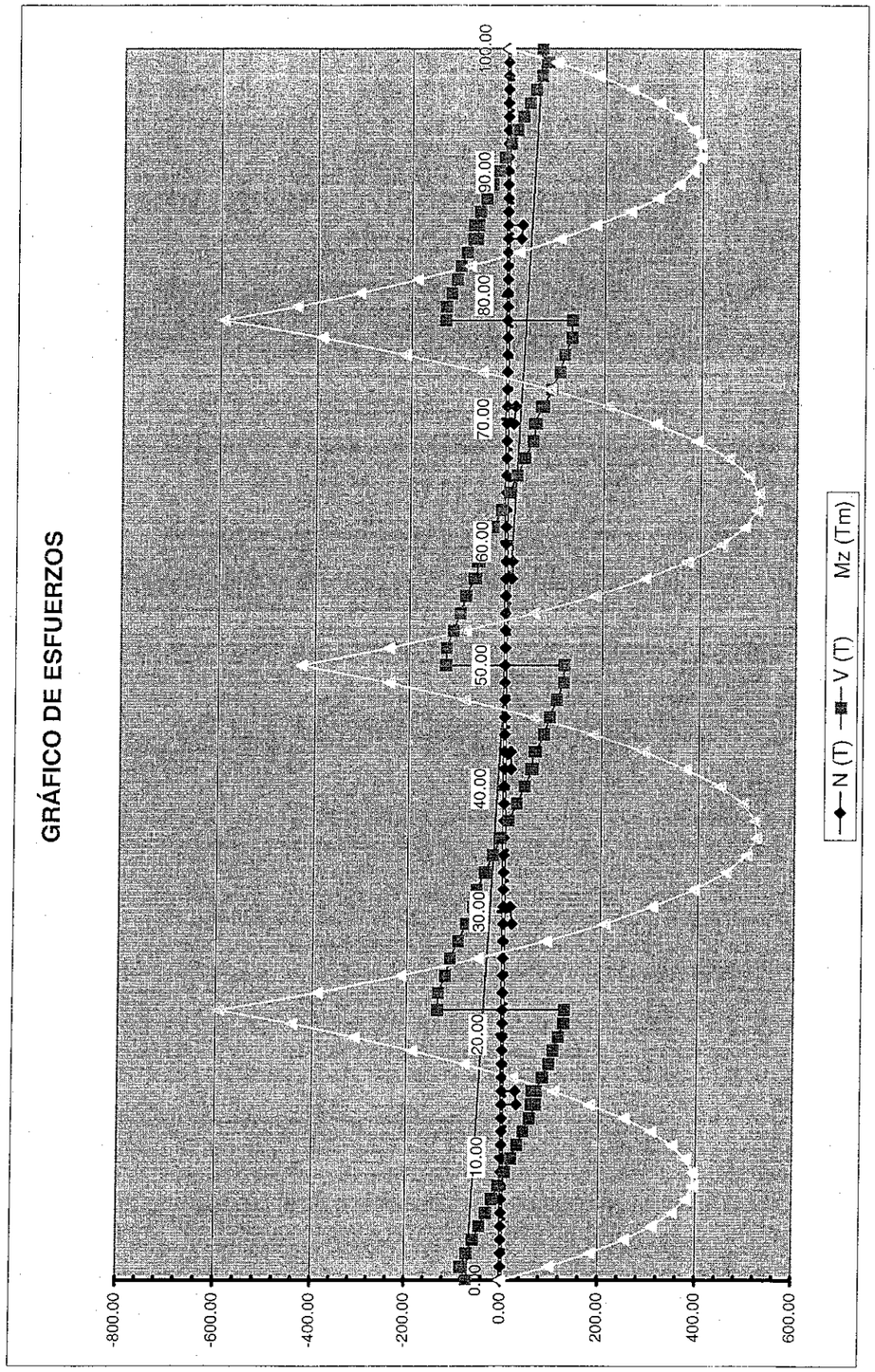
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	6.15	394.13
174	175	93.40	0.00	18.96	380.32
175	175	93.40	0.00	18.96	380.32
175	176	94.50	0.00	31.77	352.41
176	176	94.50	0.00	31.77	352.41
176	177	95.60	0.00	44.59	310.41
177	177	95.60	0.00	44.59	310.41
177	178	96.70	0.00	57.39	254.31
178	178	96.70	0.00	57.39	254.31
178	179	97.80	0.00	70.23	184.11
179	179	97.80	0.00	70.23	184.11
179	180	98.90	0.00	83.03	99.82
180	180	98.90	0.00	83.03	99.82
180	181	100.00	0.00	70.34	0.00

05/09/03

Programa DINTEL PACADAR S.A.
FASE3.T0.MZ+

rotura.esf.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-70.35	0.00
1	2	1.10	0.00	-58.93	71.10
2	2	1.10	0.00	-58.93	71.10
2	3	2.20	0.00	-49.45	130.71
3	3	2.20	0.00	-49.45	130.71
3	4	3.30	0.00	-39.94	179.87
4	4	3.30	0.00	-39.94	179.87
4	5	4.40	0.00	-30.46	218.57
5	5	4.40	0.00	-30.46	218.57
5	6	5.50	0.00	-20.96	246.84
6	6	5.50	0.00	-20.96	246.84
6	7	6.60	0.00	-11.47	264.69
7	7	6.60	0.00	-11.47	264.69
7	8	7.70	0.00	-1.98	272.08
8	8	7.70	0.00	-1.98	272.08
8	9	8.80	0.00	7.52	269.02
9	9	8.80	0.00	7.52	269.02
9	10	9.90	0.00	17.01	255.52
10	10	9.90	0.00	17.01	255.52
10	11	11.00	0.00	26.50	231.59
11	11	11.00	0.00	26.50	231.59
11	12	12.10	0.00	36.00	197.21
12	12	12.10	0.00	36.00	197.21
12	13	13.20	0.00	45.48	152.37
13	13	13.20	0.00	45.48	152.37
13	14	14.30	0.00	54.99	97.13
14	14	14.30	24.30	47.38	97.13
14	15	15.40	35.50	67.92	17.68
15	15	15.40	0.00	79.06	17.68
15	16	16.50	0.00	88.56	-74.51
16	16	16.50	0.00	88.56	-74.52
16	17	17.60	0.00	98.05	-177.14
17	17	17.60	0.00	98.05	-177.15
17	18	18.70	0.00	112.52	-293.86
18	18	18.70	-0.01	112.52	-293.86
18	19	19.80	-0.01	123.77	-423.82
19	19	19.80	0.00	123.77	-423.82
19	20	20.90	0.00	135.02	-566.17
20	20	20.90	0.00	135.02	-566.17
20	21	22.00	0.00	151.76	-723.90
21	1021	22.00	0.00	-157.57	-723.90
21	22	23.40	0.00	-136.26	-518.21
22	22	23.40	0.00	-136.26	-518.21
22	23	24.80	0.00	-121.94	-337.45
23	23	24.80	0.00	-121.93	-337.45
23	24	26.20	0.00	-103.38	-179.91
24	24	26.20	0.00	-103.38	-179.91
24	25	27.60	0.00	-91.29	-43.63
25	25	27.60	-0.01	-91.30	-43.63
25	26	29.00	-0.01	-79.22	75.74
26	26	29.00	23.90	-72.91	75.74

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
FASE3.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.18	-58.60	175.77
27	27	30.40	-0.01	-63.70	175.77
27	28	31.80	-0.01	-42.09	245.76
28	28	31.80	-0.01	-42.09	245.76
28	29	33.20	-0.01	-30.02	296.25
29	29	33.20	-0.01	-30.02	296.25
29	30	34.60	-0.01	-17.93	329.81
30	30	34.60	-0.01	-17.93	329.81
30	31	36.00	-0.01	-5.85	346.46
31	31	36.00	-0.01	-5.85	346.46
31	32	37.40	-0.01	6.23	346.20
32	32	37.40	-0.01	6.23	346.20
32	33	38.80	-0.01	18.32	329.02
33	33	38.80	-0.01	18.32	329.02
33	34	40.20	-0.01	30.39	294.92
34	34	40.20	-0.01	30.39	294.92
34	35	41.60	-0.01	42.48	243.91
35	35	41.60	9.87	40.13	243.91
35	36	43.00	18.58	61.73	166.02
36	36	43.00	-0.01	66.31	166.02
36	37	44.40	-0.01	78.39	64.74
37	37	44.40	0.00	78.40	64.73
37	38	45.80	0.00	95.16	-54.35
38	38	45.80	0.00	95.16	-54.35
38	39	47.20	0.00	109.46	-197.56
39	39	47.20	0.00	109.46	-197.55
39	40	48.60	0.00	123.78	-360.82
40	40	48.60	0.00	123.78	-360.83
40	41	50.00	0.00	145.08	-549.01
41	1041	50.00	0.00	-145.08	-549.01
41	42	51.40	0.00	-123.78	-360.82
42	42	51.40	0.00	-123.78	-360.82
42	43	52.80	0.00	-109.46	-197.55
43	43	52.80	0.00	-109.46	-197.56
43	44	54.20	0.00	-95.16	-54.36
44	44	54.20	0.00	-95.16	-54.36
44	45	55.60	0.00	-78.40	64.74
45	45	55.60	0.00	-78.39	64.73
45	46	57.00	0.00	-66.31	166.03
46	46	57.00	18.59	-61.74	166.03
46	47	58.40	9.88	-40.14	243.91
47	47	58.40	0.00	-42.48	243.91
47	48	59.80	0.00	-30.39	294.92
48	48	59.80	0.00	-30.39	294.92
48	49	61.20	0.00	-18.32	329.01
49	49	61.20	0.00	-18.32	329.01
49	50	62.60	0.00	-6.23	346.20
50	50	62.60	0.00	-6.23	346.20
50	51	64.00	0.00	5.85	346.46
51	51	64.00	0.00	5.85	346.46
51	52	65.40	0.00	17.93	329.81

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 +[1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	17.93	329.81
52	53	66.80	0.00	30.02	296.25
53	53	66.80	0.00	30.02	296.25
53	54	68.20	0.00	42.09	245.77
54	54	68.20	0.00	42.09	245.77
54	55	69.60	0.00	63.70	175.78
55	55	69.60	19.19	58.60	175.78
55	56	71.00	23.91	72.91	75.73
56	56	71.00	0.00	79.22	75.73
56	57	72.40	0.00	91.30	-43.62
57	57	72.40	0.00	91.30	-43.62
57	58	73.80	0.00	103.39	-179.90
58	58	73.80	0.00	103.38	-179.90
58	59	75.20	0.00	121.93	-337.46
59	59	75.20	0.00	121.93	-337.45
59	60	76.60	0.00	136.25	-518.21
60	60	76.60	0.00	136.26	-518.21
60	61	78.00	0.00	157.57	-723.90
61	1061	78.00	0.00	-151.76	-723.90
61	62	79.10	0.00	-135.02	-566.18
62	62	79.10	0.00	-135.02	-566.18
62	63	80.20	0.00	-123.77	-423.82
63	63	80.20	0.00	-123.77	-423.81
63	64	81.30	0.00	-112.52	-293.86
64	64	81.30	0.00	-112.52	-293.87
64	65	82.40	0.00	-98.05	-177.15
65	65	82.40	0.00	-98.05	-177.15
65	66	83.50	0.00	-88.56	-74.52
66	66	83.50	0.00	-88.57	-74.52
66	67	84.60	0.00	-79.07	17.68
67	67	84.60	35.50	-67.91	17.68
67	68	85.70	24.30	-47.37	97.13
68	68	85.70	0.00	-55.00	97.13
68	69	86.80	0.00	-45.49	152.38
69	69	86.80	0.00	-45.49	152.38
69	70	87.90	0.00	-36.01	197.20
70	70	87.90	0.00	-36.01	197.20
70	71	89.00	0.00	-26.51	231.58
71	71	89.00	0.00	-26.51	231.58
71	72	90.10	0.00	-17.02	255.52
72	72	90.10	0.00	-17.02	255.52
72	73	91.20	0.00	-7.53	269.02
73	73	91.20	0.00	-7.53	269.02
73	74	92.30	0.00	1.97	272.08
74	74	92.30	0.00	1.97	272.08
74	75	93.40	0.00	11.46	264.69
75	75	93.40	0.00	11.46	264.69
75	76	94.50	0.00	20.95	246.85
76	76	94.50	0.00	20.95	246.85
76	77	95.60	0.00	30.45	218.58
77	77	95.60	0.00	30.45	218.58

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FASE3.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	39.93	179.86
78	78	96.70	0.00	39.93	179.86
78	79	97.80	0.00	49.44	130.70
79	79	97.80	0.00	49.44	130.70
79	80	98.90	0.00	58.92	71.10
80	80	98.90	0.00	58.92	71.10
80	81	100.00	0.00	70.34	0.00
101	101	0.00	0.00	-70.35	0.00
101	102	1.10	0.00	-58.93	71.10
102	102	1.10	0.00	-58.93	71.10
102	103	2.20	0.00	-49.45	130.71
103	103	2.20	0.00	-49.45	130.71
103	104	3.30	0.00	-39.94	179.87
104	104	3.30	0.00	-39.94	179.87
104	105	4.40	0.00	-30.46	218.58
105	105	4.40	0.00	-30.46	218.58
105	106	5.50	0.00	-20.96	246.85
106	106	5.50	0.00	-20.96	246.85
106	107	6.60	0.00	-11.47	264.69
107	107	6.60	0.00	-11.47	264.69
107	108	7.70	0.00	-1.98	272.08
108	108	7.70	0.00	-1.98	272.08
108	109	8.80	0.00	7.52	269.02
109	109	8.80	0.00	7.52	269.02
109	110	9.90	0.00	17.01	255.52
110	110	9.90	0.00	17.01	255.52
110	111	11.00	0.00	26.50	231.59
111	111	11.00	0.00	26.50	231.59
111	112	12.10	0.00	36.00	197.21
112	112	12.10	0.00	36.00	197.21
112	113	13.20	0.00	45.48	152.38
113	113	13.20	0.00	45.48	152.38
113	114	14.30	0.00	54.99	97.13
114	114	14.30	24.30	47.38	97.13
114	115	15.40	35.50	67.92	17.68
115	115	15.40	0.00	79.06	17.68
115	116	16.50	0.00	88.56	-74.52
116	116	16.50	0.00	88.56	-74.52
116	117	17.60	0.00	98.05	-177.16
117	117	17.60	0.00	98.05	-177.15
117	118	18.70	0.00	112.52	-293.86
118	118	18.70	0.00	112.52	-293.86
118	119	19.80	0.00	123.77	-423.81
119	119	19.80	0.00	123.77	-423.81
119	120	20.90	0.00	135.02	-566.17
120	120	20.90	0.00	135.02	-566.17
120	121	22.00	0.00	151.76	-723.90
121	1121	22.00	0.00	-157.57	-723.90
121	122	23.40	0.00	-136.26	-518.21
122	122	23.40	0.00	-136.26	-518.21
122	123	24.80	0.00	-121.94	-337.46

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-121.93	-337.45
123	124	26.20	0.00	-103.38	-179.91
124	124	26.20	0.00	-103.38	-179.91
124	125	27.60	0.00	-91.29	-43.64
125	125	27.60	-0.01	-91.30	-43.64
125	126	29.00	-0.01	-79.22	75.73
126	126	29.00	23.90	-72.91	75.73
126	127	30.40	19.18	-58.60	175.77
127	127	30.40	-0.01	-63.70	175.77
127	128	31.80	-0.01	-42.09	245.76
128	128	31.80	-0.01	-42.09	245.76
128	129	33.20	-0.01	-30.02	296.26
129	129	33.20	-0.01	-30.02	296.26
129	130	34.60	-0.01	-17.93	329.81
130	130	34.60	-0.01	-17.93	329.81
130	131	36.00	-0.01	-5.85	346.47
131	131	36.00	-0.01	-5.85	346.47
131	132	37.40	-0.01	6.23	346.19
132	132	37.40	-0.01	6.23	346.19
132	133	38.80	-0.01	18.32	329.01
133	133	38.80	-0.01	18.32	329.01
133	134	40.20	-0.01	30.39	294.92
134	134	40.20	-0.01	30.39	294.92
134	135	41.60	-0.01	42.48	243.91
135	135	41.60	9.87	40.13	243.91
135	136	43.00	18.58	61.73	166.02
136	136	43.00	-0.01	66.31	166.02
136	137	44.40	-0.01	78.39	64.74
137	137	44.40	0.00	78.39	64.73
137	138	45.80	0.00	95.15	-54.35
138	138	45.80	0.00	95.16	-54.35
138	139	47.20	0.00	109.46	-197.55
139	139	47.20	0.00	109.46	-197.55
139	140	48.60	0.00	123.78	-360.82
140	140	48.60	0.00	123.78	-360.83
140	141	50.00	0.00	145.08	-549.01
141	1141	50.00	0.00	-145.08	-549.01
141	142	51.40	0.00	-123.78	-360.83
142	142	51.40	0.00	-123.77	-360.83
142	143	52.80	0.00	-109.45	-197.54
143	143	52.80	0.00	-109.46	-197.54
143	144	54.20	0.00	-95.16	-54.35
144	144	54.20	0.00	-95.16	-54.35
144	145	55.60	0.00	-78.40	64.74
145	145	55.60	0.00	-78.39	64.74
145	146	57.00	0.00	-66.31	166.02
146	146	57.00	18.58	-61.74	166.02
146	147	58.40	9.87	-40.14	243.92
147	147	58.40	0.00	-42.48	243.92
147	148	59.80	0.00	-30.39	294.92
148	148	59.80	0.00	-30.39	294.92

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FASE3.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

FASE3.T0.MZ-

Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-18.32	329.01
149	149	61.20	0.00	-18.32	329.01
149	150	62.60	0.00	-6.23	346.20
150	150	62.60	0.00	-6.23	346.20
150	151	64.00	0.00	5.85	346.46
151	151	64.00	0.00	5.85	346.46
151	152	65.40	0.00	17.93	329.81
152	152	65.40	0.00	17.93	329.81
152	153	66.80	0.00	30.02	296.26
153	153	66.80	0.00	30.02	296.26
153	154	68.20	0.00	42.09	245.76
154	154	68.20	0.00	42.09	245.76
154	155	69.60	0.00	63.70	175.77
155	155	69.60	19.19	58.60	175.77
155	156	71.00	23.91	72.91	75.72
156	156	71.00	0.00	79.22	75.72
156	157	72.40	0.00	91.30	-43.63
157	157	72.40	0.00	91.30	-43.63
157	158	73.80	0.00	103.39	-179.91
158	158	73.80	0.00	103.38	-179.91
158	159	75.20	0.00	121.93	-337.46
159	159	75.20	0.00	121.93	-337.46
159	160	76.60	0.00	136.25	-518.21
160	160	76.60	0.00	136.26	-518.21
160	161	78.00	0.00	157.57	-723.89
161	1161	78.00	0.00	-151.76	-723.90
161	162	79.10	0.00	-135.02	-566.17
162	162	79.10	0.00	-135.02	-566.17
162	163	80.20	0.00	-123.77	-423.81
163	163	80.20	0.00	-123.77	-423.81
163	164	81.30	0.00	-112.52	-293.86
164	164	81.30	0.00	-112.52	-293.87
164	165	82.40	0.00	-98.05	-177.15
165	165	82.40	0.00	-98.05	-177.15
165	166	83.50	0.00	-88.56	-74.51
166	166	83.50	0.00	-88.57	-74.52
166	167	84.60	0.00	-79.07	17.68
167	167	84.60	35.50	-67.91	17.68
167	168	85.70	24.30	-47.37	97.13
168	168	85.70	0.00	-55.00	97.13
168	169	86.80	0.00	-45.49	152.38
169	169	86.80	0.00	-45.49	152.38
169	170	87.90	0.00	-36.01	197.21
170	170	87.90	0.00	-36.01	197.21
170	171	89.00	0.00	-26.51	231.59
171	171	89.00	0.00	-26.51	231.59
171	172	90.10	0.00	-17.02	255.52
172	172	90.10	0.00	-17.02	255.52
172	173	91.20	0.00	-7.53	269.02
173	173	91.20	0.00	-7.53	269.02
173	174	92.30	0.00	1.97	272.08

CÁLCULO TENSIONAL

Hipótesis de cálculo:
FASE3.T0.MZ-

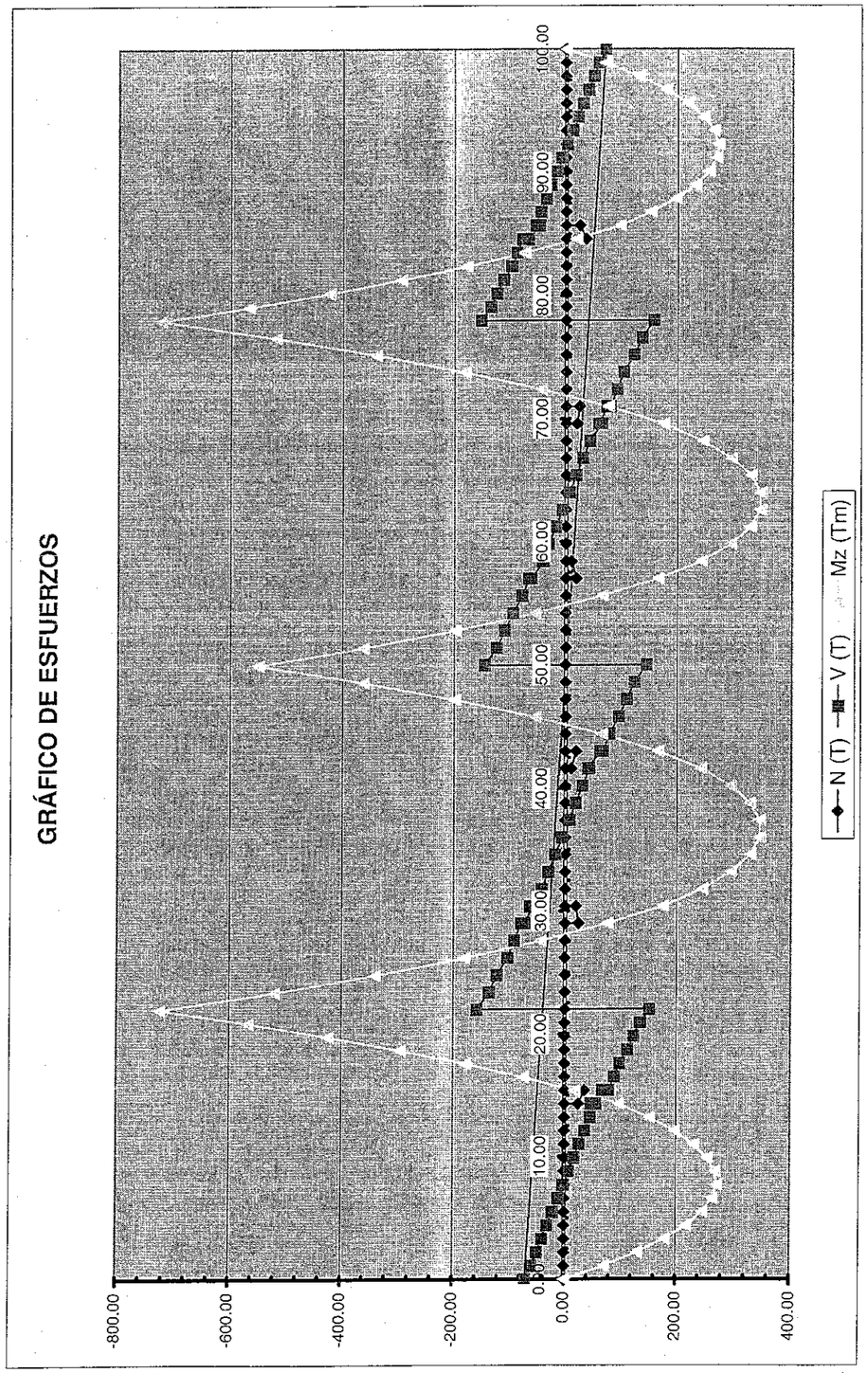
Construcción fase 3 Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1)eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	1.97	272.08
174	175	93.40	0.00	11.46	264.69
175	175	93.40	0.00	11.46	264.69
175	176	94.50	0.00	20.95	246.85
176	176	94.50	0.00	20.95	246.85
176	177	95.60	0.00	30.45	218.58
177	177	95.60	0.00	30.45	218.58
177	178	96.70	0.00	39.93	179.86
178	178	96.70	0.00	39.93	179.86
178	179	97.80	0.00	49.44	130.70
179	179	97.80	0.00	49.44	130.70
179	180	98.90	0.00	58.92	71.10
180	180	98.90	0.00	58.92	71.10
180	181	100.00	0.00	70.34	0.00

05/09/03
Programa DINTEL PACADAR S.A.
FASE3.T0.MZ-
rotura.esf.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1)eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-126.97	-0.04
1	2	1.10	0.00	-186.48	222.16
2	2	1.10	0.00	-185.96	221.99
2	3	2.20	0.00	-157.42	410.85
3	3	2.20	0.00	-156.98	410.67
3	4	3.30	0.00	-128.40	567.60
4	4	3.30	0.00	-128.01	567.46
4	5	4.40	0.00	-99.46	692.56
5	5	4.40	0.00	-99.15	692.43
5	6	5.50	0.00	-70.58	785.77
6	6	5.50	0.00	-70.30	785.67
6	7	6.60	0.00	-41.75	847.32
7	7	6.60	0.00	-41.52	847.25
7	8	7.70	0.00	-12.97	877.23
8	8	7.70	0.00	-12.74	877.18
8	9	8.80	0.00	15.82	875.47
9	9	8.80	0.00	16.01	875.47
9	10	9.90	0.00	44.57	842.13
10	10	9.90	0.00	44.78	842.15
10	11	11.00	0.00	73.33	777.19
11	11	11.00	0.00	73.54	777.24
11	12	12.10	0.00	102.10	680.63
12	12	12.10	0.00	102.35	680.70
12	13	13.20	0.00	130.89	552.39
13	13	13.20	0.00	131.17	552.48
13	14	14.30	0.00	159.76	392.49
14	14	14.30	30.79	150.41	392.59
14	15	15.40	27.79	167.88	213.17
15	15	15.40	0.00	176.96	213.29
15	16	16.50	0.00	141.98	13.13
16	16	16.50	0.00	142.14	13.17
16	17	17.60	0.00	162.45	-154.33
17	17	17.60	0.00	162.63	-154.29
17	18	18.70	0.00	177.96	-340.72
18	18	18.70	-0.01	178.15	-340.68
18	19	19.80	-0.01	196.73	-546.86
19	19	19.80	0.00	196.95	-546.83
19	20	20.90	0.00	215.50	-773.70
20	20	20.90	0.00	215.74	-773.68
20	21	22.00	0.00	224.12	-1025.28
21	1021	22.00	0.00	-230.72	-1025.29
21	22	23.40	0.00	-220.09	-694.01
22	22	23.40	0.00	-219.81	-694.05
22	23	24.80	0.00	-196.16	-402.86
23	23	24.80	0.00	-195.88	-402.92
23	24	26.20	0.00	-176.53	-142.06
24	24	26.20	0.00	-176.30	-142.13
24	25	27.60	0.00	-150.42	86.59
25	25	27.60	-0.01	-150.24	86.52
25	26	29.00	-0.01	-176.72	355.75
26	26	29.00	18.10	-171.49	355.58

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
PERM1.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1)eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	14.61	-137.37	577.91
27	27	30.40	-0.01	-140.98	577.75
27	28	31.80	-0.01	-114.15	760.37
28	28	31.80	-0.01	-113.89	760.24
28	29	33.20	-0.01	-77.55	894.27
29	29	33.20	-0.01	-77.34	894.18
29	30	34.60	-0.01	-40.99	977.01
30	30	34.60	-0.01	-40.80	976.96
30	31	36.00	-0.01	-4.46	1008.65
31	31	36.00	-0.01	-4.28	1008.67
31	32	37.40	-0.01	32.07	989.22
32	32	37.40	-0.01	32.24	989.28
32	33	38.80	-0.01	68.59	918.72
33	33	38.80	-0.01	68.82	918.80
33	34	40.20	-0.01	105.16	797.01
34	34	40.20	-0.01	105.42	797.13
34	35	41.60	-0.01	141.77	624.13
35	35	41.60	13.87	138.75	624.27
35	36	43.00	13.36	165.56	408.35
36	36	43.00	-0.01	169.22	408.54
36	37	44.40	-0.01	140.76	166.26
37	37	44.40	0.00	140.97	166.33
37	38	45.80	0.00	162.17	-48.24
38	38	45.80	0.00	162.41	-48.17
38	39	47.20	0.00	186.03	-292.07
39	39	47.20	0.00	186.29	-292.00
39	40	48.60	0.00	209.93	-569.36
40	40	48.60	0.00	210.22	-569.34
40	41	50.00	0.00	220.86	-886.81
41	1041	50.00	0.00	-220.86	-886.81
41	42	51.40	0.00	-210.22	-569.33
42	42	51.40	0.00	-209.93	-569.36
42	43	52.80	0.00	-186.29	-292.00
43	43	52.80	0.00	-186.03	-292.07
43	44	54.20	0.00	-162.41	-48.18
44	44	54.20	0.00	-162.17	-48.25
44	45	55.60	0.00	-140.97	166.35
45	45	55.60	0.00	-140.76	166.26
45	46	57.00	0.00	-169.22	408.55
46	46	57.00	13.37	-165.57	408.38
46	47	58.40	13.88	-138.76	624.29
47	47	58.40	0.00	-141.77	624.13
47	48	59.80	0.00	-105.42	797.16
48	48	59.80	0.00	-105.16	797.04
48	49	61.20	0.00	-68.82	918.79
49	49	61.20	0.00	-68.59	918.71
49	50	62.60	0.00	-32.24	989.29
50	50	62.60	0.00	-32.05	989.24
50	51	64.00	0.00	4.30	1008.67
51	51	64.00	0.00	4.46	1008.67
51	52	65.40	0.00	40.80	976.98

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	40.99	977.01
52	53	66.80	0.00	77.34	894.20
53	53	66.80	0.00	77.56	894.28
53	54	68.20	0.00	113.89	760.27
54	54	68.20	0.00	114.15	760.39
54	55	69.60	0.00	140.98	577.78
55	55	69.60	14.62	137.39	577.94
55	56	71.00	18.11	171.51	355.58
56	56	71.00	0.00	176.72	355.76
56	57	72.40	0.00	150.24	86.53
57	57	72.40	0.00	150.44	86.60
57	58	73.80	0.00	176.31	-142.13
58	58	73.80	0.00	176.53	-142.06
58	59	75.20	0.00	195.88	-402.93
59	59	75.20	0.00	196.15	-402.86
59	60	76.60	0.00	219.80	-694.05
60	60	76.60	0.00	220.09	-694.02
60	61	78.00	0.00	230.72	-1025.30
61	1061	78.00	0.00	-224.12	-1025.29
61	62	79.10	0.00	-215.74	-773.70
62	62	79.10	0.00	-215.51	-773.72
62	63	80.20	0.00	-196.95	-546.83
63	63	80.20	0.00	-196.74	-546.86
63	64	81.30	0.00	-178.16	-340.68
64	64	81.30	0.00	-177.96	-340.73
64	65	82.40	0.00	-162.63	-154.29
65	65	82.40	0.00	-162.45	-154.34
65	66	83.50	0.00	-142.14	13.17
66	66	83.50	0.00	-141.99	13.12
66	67	84.60	0.00	-176.97	213.29
67	67	84.60	27.79	-167.87	213.17
67	68	85.70	30.79	-150.38	392.61
68	68	85.70	0.00	-159.77	392.49
68	69	86.80	0.00	-131.18	552.49
69	69	86.80	0.00	-130.90	552.40
69	70	87.90	0.00	-102.36	680.69
70	70	87.90	0.00	-102.11	680.62
70	71	89.00	0.00	-73.55	777.23
71	71	89.00	0.00	-73.34	777.19
71	72	90.10	0.00	-44.79	842.17
72	72	90.10	0.00	-44.58	842.15
72	73	91.20	0.00	-16.02	875.47
73	73	91.20	0.00	-15.83	875.48
73	74	92.30	0.00	12.73	877.19
74	74	92.30	0.00	12.96	877.23
74	75	93.40	0.00	41.51	847.27
75	75	93.40	0.00	41.74	847.34
75	76	94.50	0.00	70.29	785.68
76	76	94.50	0.00	70.57	785.78
76	77	95.60	0.00	99.14	692.44
77	77	95.60	0.00	99.45	692.58

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PERM1.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	128.00	567.45
78	78	96.70	0.00	128.39	567.61
78	79	97.80	0.00	156.97	410.66
79	79	97.80	0.00	157.41	410.84
79	80	98.90	0.00	185.95	221.99
80	80	98.90	0.00	186.47	222.16
80	81	100.00	0.00	126.96	-0.04
101	101	0.00	0.00	-165.84	0.09
101	102	1.10	0.00	-171.28	204.74
102	102	1.10	0.00	-171.81	204.93
102	103	2.20	0.00	-144.89	379.10
103	103	2.20	0.00	-145.33	379.28
103	104	3.30	0.00	-118.38	524.29
104	104	3.30	0.00	-118.73	524.45
104	105	4.40	0.00	-91.83	640.25
105	105	4.40	0.00	-92.15	640.37
105	106	5.50	0.00	-65.21	726.90
106	106	5.50	0.00	-65.48	727.01
106	107	6.60	0.00	-38.56	784.25
107	107	6.60	0.00	-38.79	784.32
107	108	7.70	0.00	-11.87	812.17
108	108	7.70	0.00	-12.08	812.21
108	109	8.80	0.00	14.86	810.67
109	109	8.80	0.00	14.66	810.68
109	110	9.90	0.00	41.58	779.72
110	110	9.90	0.00	41.39	779.71
110	111	11.00	0.00	68.31	719.39
111	111	11.00	0.00	68.10	719.34
111	112	12.10	0.00	95.05	629.59
112	112	12.10	0.00	94.80	629.52
112	113	13.20	0.00	121.71	510.42
113	113	13.20	0.00	121.44	510.33
113	114	14.30	0.00	148.39	361.93
114	114	14.30	30.79	138.45	361.82
114	115	15.40	27.79	154.30	196.43
115	115	15.40	0.00	162.66	196.30
115	116	16.50	0.00	135.62	12.98
116	116	16.50	0.00	135.46	12.93
116	117	17.60	0.00	155.13	-146.89
117	117	17.60	0.00	154.95	-146.93
117	118	18.70	0.00	169.62	-324.55
118	118	18.70	0.00	169.42	-324.59
118	119	19.80	0.00	187.35	-520.80
119	119	19.80	0.00	187.13	-520.84
119	120	20.90	0.00	205.05	-736.56
120	120	20.90	0.00	204.82	-736.58
120	121	22.00	0.00	212.56	-975.82
121	1121	22.00	0.00	-219.40	-975.82
121	122	23.40	0.00	-209.59	-659.83
122	122	23.40	0.00	-209.86	-659.80
122	123	24.80	0.00	-187.05	-381.94

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-187.30	-381.87
123	124	26.20	0.00	-168.77	-132.46
124	124	26.20	0.00	-169.00	-132.39
124	125	27.60	0.00	-143.95	86.68
125	125	27.60	-0.01	-144.15	86.75
125	126	29.00	-0.01	-163.54	336.46
126	126	29.00	18.10	-159.12	336.65
126	127	30.40	14.61	-127.07	543.11
127	127	30.40	-0.01	-131.33	543.27
127	128	31.80	-0.01	-106.55	713.81
128	128	31.80	-0.01	-106.81	713.93
128	129	33.20	-0.01	-72.56	839.52
129	129	33.20	-0.01	-72.77	839.61
129	130	34.60	-0.01	-38.48	917.46
130	130	34.60	-0.01	-38.67	917.52
130	131	36.00	-0.01	-4.39	947.66
131	131	36.00	-0.01	-4.56	947.66
131	132	37.40	-0.01	29.72	930.05
132	132	37.40	-0.01	29.52	930.00
132	133	38.80	-0.01	63.82	864.67
133	133	38.80	-0.01	63.59	864.58
133	134	40.20	-0.01	97.86	751.59
134	134	40.20	-0.01	97.59	751.46
134	135	41.60	-0.01	131.87	590.84
135	135	41.60	13.87	128.16	590.68
135	136	43.00	13.36	152.91	391.03
136	136	43.00	-0.01	155.72	390.83
136	137	44.40	-0.01	134.55	167.33
137	137	44.40	0.00	134.35	167.24
137	138	45.80	0.00	154.72	-37.50
138	138	45.80	0.00	154.49	-37.56
138	139	47.20	0.00	177.28	-269.79
139	139	47.20	0.00	177.02	-269.84
139	140	48.60	0.00	199.83	-533.65
140	140	48.60	0.00	199.53	-533.69
140	141	50.00	0.00	209.36	-835.60
141	1141	50.00	0.00	-209.36	-835.60
141	142	51.40	0.00	-199.53	-533.69
142	142	51.40	0.00	-199.82	-533.65
142	143	52.80	0.00	-177.01	-269.84
143	143	52.80	0.00	-177.29	-269.78
143	144	54.20	0.00	-154.49	-37.57
144	144	54.20	0.00	-154.73	-37.50
144	145	55.60	0.00	-134.36	167.25
145	145	55.60	0.00	-134.55	167.32
145	146	57.00	0.00	-155.72	390.85
146	146	57.00	13.36	-152.92	391.04
146	147	58.40	13.87	-128.17	590.71
147	147	58.40	0.00	-131.87	590.86
147	148	59.80	0.00	-97.59	751.47
148	148	59.80	0.00	-97.86	751.59

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PERM1.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-63.59	864.60
149	149	61.20	0.00	-63.82	864.69
149	150	62.60	0.00	-29.52	930.02
150	150	62.60	0.00	-29.72	930.08
150	151	64.00	0.00	4.56	947.66
151	151	64.00	0.00	4.39	947.66
151	152	65.40	0.00	38.67	917.52
152	152	65.40	0.00	38.48	917.48
152	153	66.80	0.00	72.76	839.63
153	153	66.80	0.00	72.56	839.54
153	154	68.20	0.00	106.81	713.95
154	154	68.20	0.00	106.55	713.82
154	155	69.60	0.00	131.33	543.29
155	155	69.60	14.62	127.07	543.13
155	156	71.00	18.11	159.12	336.66
156	156	71.00	0.00	163.54	336.48
156	157	72.40	0.00	144.16	86.77
157	157	72.40	0.00	143.96	86.70
157	158	73.80	0.00	169.01	-132.39
158	158	73.80	0.00	168.77	-132.46
158	159	75.20	0.00	187.30	-381.88
159	159	75.20	0.00	187.04	-381.93
159	160	76.60	0.00	209.86	-659.80
160	160	76.60	0.00	209.59	-659.84
160	161	78.00	0.00	219.40	-975.82
161	1161	78.00	0.00	-212.56	-975.83
161	162	79.10	0.00	-204.82	-736.59
162	162	79.10	0.00	-205.05	-736.57
162	163	80.20	0.00	-187.14	-520.84
163	163	80.20	0.00	-187.35	-520.81
163	164	81.30	0.00	-169.42	-324.60
164	164	81.30	0.00	-169.62	-324.56
164	165	82.40	0.00	-154.95	-146.93
165	165	82.40	0.00	-155.13	-146.88
165	166	83.50	0.00	-135.46	12.93
166	166	83.50	0.00	-135.63	12.97
166	167	84.60	0.00	-162.67	196.30
167	167	84.60	27.79	-154.29	196.43
167	168	85.70	30.79	-138.44	361.81
168	168	85.70	0.00	-148.40	361.92
168	169	86.80	0.00	-121.45	510.33
169	169	86.80	0.00	-121.72	510.42
169	170	87.90	0.00	-94.81	629.52
170	170	87.90	0.00	-95.04	629.59
170	171	89.00	0.00	-68.11	719.34
171	171	89.00	0.00	-68.32	719.39
171	172	90.10	0.00	-41.40	779.71
172	172	90.10	0.00	-41.59	779.72
172	173	91.20	0.00	-14.67	810.67
173	173	91.20	0.00	-14.88	810.67
173	174	92.30	0.00	12.07	812.22

CÁLCULO TENSIONAL

Hipótesis de cálculo:

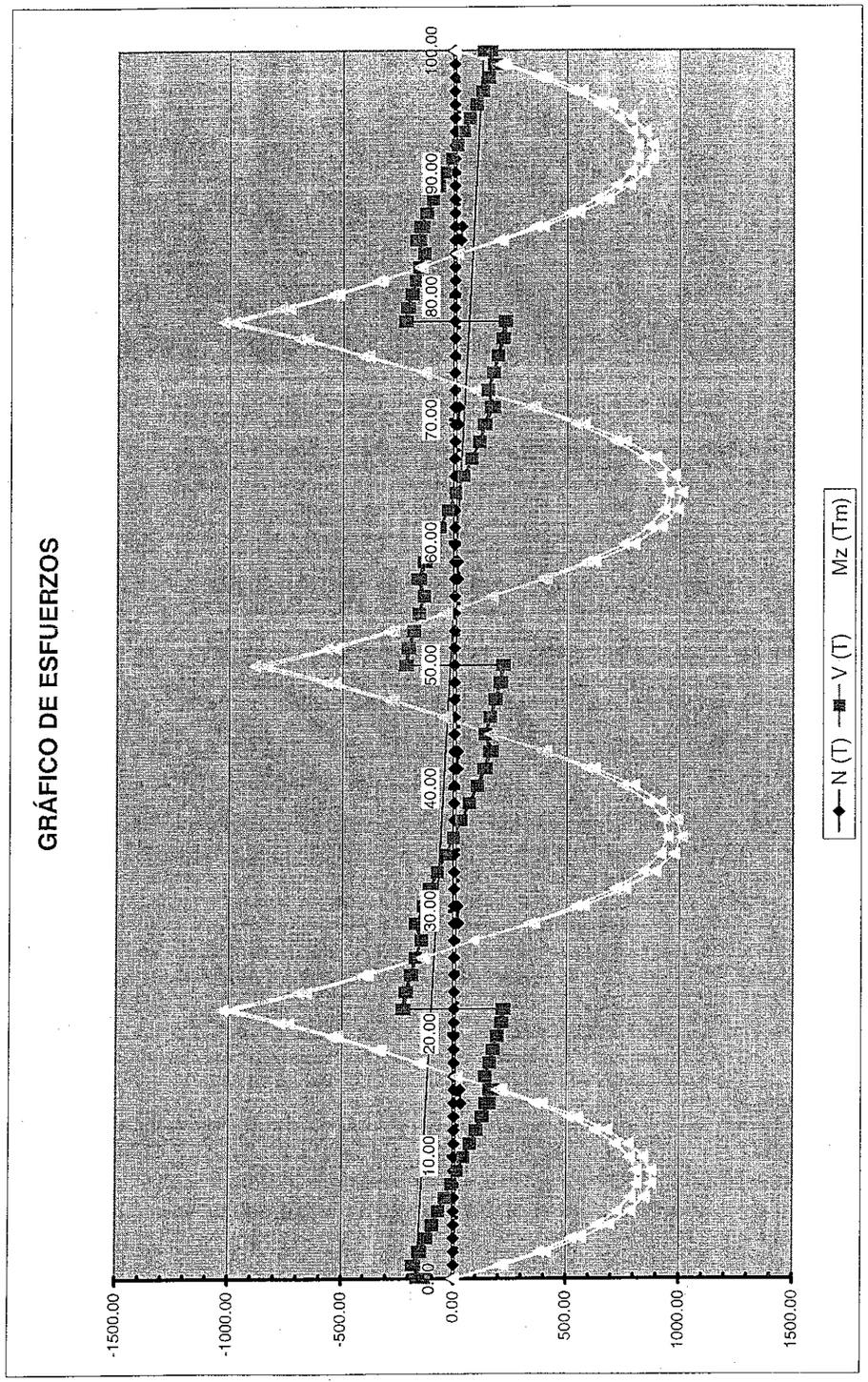
PERM1.T0.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	11.86	812.17
174	175	93.40	0.00	38.78	784.32
175	175	93.40	0.00	38.55	784.25
175	176	94.50	0.00	65.47	727.01
176	176	94.50	0.00	65.20	726.92
176	177	95.60	0.00	92.14	640.39
177	177	95.60	0.00	91.82	640.25
177	178	96.70	0.00	118.74	524.44
178	178	96.70	0.00	118.37	524.28
178	179	97.80	0.00	145.32	379.27
179	179	97.80	0.00	144.88	379.09
179	180	98.90	0.00	171.80	204.93
180	180	98.90	0.00	171.27	204.75
180	181	100.00	0.00	165.83	0.09



CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-182.65	-0.09
1	2	1.10	0.00	-108.05	129.21
2	2	1.10	0.00	-107.84	129.14
2	3	2.20	0.00	-90.85	238.42
3	3	2.20	0.00	-90.68	238.35
3	4	3.30	0.00	-73.67	328.73
4	4	3.30	0.00	-73.51	328.67
4	5	4.40	0.00	-56.52	400.17
5	5	4.40	0.00	-56.40	400.12
5	6	5.50	0.00	-39.40	452.80
6	6	5.50	0.00	-39.28	452.76
6	7	6.60	0.00	-22.29	486.64
7	7	6.60	0.00	-22.20	486.62
7	8	7.70	0.00	-5.21	501.69
8	8	7.70	0.00	-5.12	501.67
8	9	8.80	0.00	11.88	497.94
9	9	8.80	0.00	11.96	497.94
9	10	9.90	0.00	28.95	475.43
10	10	9.90	0.00	29.03	475.43
10	11	11.00	0.00	46.02	434.15
11	11	11.00	0.00	46.11	434.17
11	12	12.10	0.00	63.11	374.10
12	12	12.10	0.00	63.21	374.12
12	13	13.20	0.00	80.19	295.23
13	13	13.20	0.00	80.30	295.26
13	14	14.30	0.00	97.32	197.59
14	14	14.30	24.30	89.83	197.63
14	15	15.40	35.50	117.87	67.37
15	15	15.40	0.00	129.15	67.42
15	16	16.50	0.00	209.71	-94.21
16	16	16.50	0.00	210.11	-94.10
16	17	17.60	0.00	235.34	-339.06
17	17	17.60	0.00	235.80	-338.95
17	18	18.70	0.00	266.01	-615.84
18	18	18.70	-0.01	266.50	-615.73
18	19	19.80	-0.01	293.49	-923.73
19	19	19.80	0.00	294.04	-923.66
19	20	20.90	0.00	321.02	-1261.97
20	20	20.90	0.00	321.60	-1261.91
20	21	22.00	0.00	354.08	-1633.54
21	1021	22.00	0.00	-359.95	-1633.56
21	22	23.40	0.00	-318.62	-1158.54
22	22	23.40	0.00	-317.91	-1158.65
22	23	24.80	0.00	-283.55	-737.61
23	23	24.80	0.00	-282.88	-737.75
23	24	26.20	0.00	-244.30	-368.91
24	24	26.20	0.00	-243.72	-369.09
24	25	27.60	0.00	-211.58	-50.35
25	25	27.60	-0.01	-211.10	-50.53
25	26	29.00	-0.01	-126.66	145.54
26	26	29.00	23.90	-120.18	145.47

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
PERM1.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.18	-96.32	305.00
27	27	30.40	-0.01	-101.29	304.94
27	28	31.80	-0.01	-70.14	420.87
28	28	31.80	-0.01	-70.03	420.82
28	29	33.20	-0.01	-48.41	503.75
29	29	33.20	-0.01	-48.33	503.72
29	30	34.60	-0.01	-26.69	556.23
30	30	34.60	-0.01	-26.62	556.20
30	31	36.00	-0.01	-4.99	578.33
31	31	36.00	-0.01	-4.92	578.34
31	32	37.40	-0.01	16.71	570.09
32	32	37.40	-0.01	16.78	570.11
32	33	38.80	-0.01	38.42	531.48
33	33	38.80	-0.01	38.51	531.52
33	34	40.20	-0.01	60.13	462.46
34	34	40.20	-0.01	60.24	462.51
34	35	41.60	-0.01	81.87	363.05
35	35	41.60	9.87	79.66	363.10
35	36	43.00	18.58	110.81	223.19
36	36	43.00	-0.01	115.55	223.27
36	37	44.40	-0.01	202.00	26.27
37	37	44.40	0.00	202.52	26.46
37	38	45.80	0.00	239.30	-280.39
38	38	45.80	0.00	239.90	-280.21
38	39	47.20	0.00	274.24	-640.11
39	39	47.20	0.00	274.91	-639.96
39	40	48.60	0.00	309.26	-1048.88
40	40	48.60	0.00	309.99	-1048.80
40	41	50.00	0.00	351.35	-1511.74
41	1041	50.00	0.00	-351.35	-1511.74
41	42	51.40	0.00	-309.99	-1048.79
42	42	51.40	0.00	-309.26	-1048.88
42	43	52.80	0.00	-274.91	-639.96
43	43	52.80	0.00	-274.24	-640.11
43	44	54.20	0.00	-239.90	-280.22
44	44	54.20	0.00	-239.30	-280.40
44	45	55.60	0.00	-202.52	26.48
45	45	55.60	0.00	-202.00	26.28
45	46	57.00	0.00	-115.55	223.28
46	46	57.00	18.59	-110.82	223.21
46	47	58.40	9.88	-79.67	363.11
47	47	58.40	0.00	-81.87	363.05
47	48	59.80	0.00	-60.24	462.53
48	48	59.80	0.00	-60.13	462.48
48	49	61.20	0.00	-38.51	531.51
49	49	61.20	0.00	-38.42	531.47
49	50	62.60	0.00	-16.78	570.12
50	50	62.60	0.00	-16.71	570.10
50	51	64.00	0.00	4.93	578.34
51	51	64.00	0.00	4.99	578.34
51	52	65.40	0.00	26.62	556.21

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	26.69	556.23
52	53	66.80	0.00	48.33	503.72
53	53	66.80	0.00	48.42	503.76
53	54	68.20	0.00	70.03	420.84
54	54	68.20	0.00	70.14	420.89
54	55	69.60	0.00	101.29	304.95
55	55	69.60	19.19	96.32	305.02
55	56	71.00	23.91	120.19	145.46
56	56	71.00	0.00	126.66	145.53
56	57	72.40	0.00	211.10	-50.52
57	57	72.40	0.00	211.61	-50.34
57	58	73.80	0.00	243.74	-369.09
58	58	73.80	0.00	244.30	-368.91
58	59	75.20	0.00	282.88	-737.77
59	59	75.20	0.00	283.54	-737.61
59	60	76.60	0.00	317.90	-1158.65
60	60	76.60	0.00	318.62	-1158.56
60	61	78.00	0.00	359.95	-1633.57
61	1061	78.00	0.00	-354.08	-1633.56
61	62	79.10	0.00	-321.60	-1261.94
62	62	79.10	0.00	-321.04	-1261.99
62	63	80.20	0.00	-294.06	-923.66
63	63	80.20	0.00	-293.51	-923.74
63	64	81.30	0.00	-266.52	-615.73
64	64	81.30	0.00	-266.01	-615.85
64	65	82.40	0.00	-235.80	-338.95
65	65	82.40	0.00	-235.34	-339.07
65	66	83.50	0.00	-210.11	-94.10
66	66	83.50	0.00	-209.72	-94.22
66	67	84.60	0.00	-129.16	67.42
67	67	84.60	35.50	-117.86	67.37
67	68	85.70	24.30	-89.81	197.64
68	68	85.70	0.00	-97.33	197.59
68	69	86.80	0.00	-80.31	295.27
69	69	86.80	0.00	-80.20	295.24
69	70	87.90	0.00	-63.22	374.11
70	70	87.90	0.00	-63.12	374.09
70	71	89.00	0.00	-46.12	434.16
71	71	89.00	0.00	-46.03	434.15
71	72	90.10	0.00	-29.04	475.44
72	72	90.10	0.00	-28.96	475.43
72	73	91.20	0.00	-11.97	497.94
73	73	91.20	0.00	-11.89	497.94
73	74	92.30	0.00	5.11	501.68
74	74	92.30	0.00	5.20	501.69
74	75	93.40	0.00	22.19	486.62
75	75	93.40	0.00	22.28	486.65
75	76	94.50	0.00	39.27	452.77
76	76	94.50	0.00	39.39	452.81
76	77	95.60	0.00	56.39	400.13
77	77	95.60	0.00	56.51	400.19

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PERM1.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	73.50	328.66
78	78	96.70	0.00	73.66	328.72
78	79	97.80	0.00	90.67	238.34
79	79	97.80	0.00	90.84	238.41
79	80	98.90	0.00	107.83	129.14
80	80	98.90	0.00	108.04	129.21
80	81	100.00	0.00	182.64	-0.09
101	101	0.00	0.00	-120.26	0.04
101	102	1.10	0.00	-101.98	122.26
102	102	1.10	0.00	-102.19	122.34
102	103	2.20	0.00	-85.86	225.76
103	103	2.20	0.00	-86.03	225.83
103	104	3.30	0.00	-69.67	311.45
104	104	3.30	0.00	-69.81	311.51
104	105	4.40	0.00	-53.48	379.31
105	105	4.40	0.00	-53.60	379.36
105	106	5.50	0.00	-37.25	429.32
106	106	5.50	0.00	-37.36	429.37
106	107	6.60	0.00	-21.02	461.49
107	107	6.60	0.00	-21.11	461.51
107	108	7.70	0.00	-4.77	475.74
108	108	7.70	0.00	-4.85	475.76
108	109	8.80	0.00	11.50	472.10
109	109	8.80	0.00	11.42	472.10
109	110	9.90	0.00	27.76	450.54
110	110	9.90	0.00	27.68	450.53
110	111	11.00	0.00	44.02	411.10
111	111	11.00	0.00	43.94	411.08
111	112	12.10	0.00	60.30	353.74
112	112	12.10	0.00	60.20	353.71
112	113	13.20	0.00	76.53	278.49
113	113	13.20	0.00	76.42	278.46
113	114	14.30	0.00	92.78	185.40
114	114	14.30	24.30	85.06	185.36
114	115	15.40	35.50	112.45	60.69
115	115	15.40	0.00	123.45	60.64
115	116	16.50	0.00	193.77	-94.57
116	116	16.50	0.00	193.37	-94.70
116	117	17.60	0.00	216.98	-320.39
117	117	17.60	0.00	216.53	-320.51
117	118	18.70	0.00	245.11	-575.30
118	118	18.70	0.00	244.62	-575.40
118	119	19.80	0.00	269.98	-858.42
119	119	19.80	0.00	269.43	-858.51
119	120	20.90	0.00	294.80	-1168.86
120	120	20.90	0.00	294.22	-1168.90
120	121	22.00	0.00	325.09	-1509.53
121	1121	22.00	0.00	-331.58	-1509.53
121	122	23.40	0.00	-292.29	-1072.84
122	122	23.40	0.00	-293.00	-1072.75
122	123	24.80	0.00	-260.72	-685.14

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-261.36	-684.97
123	124	26.20	0.00	-224.85	-344.81
124	124	26.20	0.00	-225.43	-344.65
124	125	27.60	0.00	-195.35	-50.10
125	125	27.60	-0.01	-195.85	-49.92
125	126	29.00	-0.01	-121.40	137.83
126	126	29.00	23.90	-115.25	137.91
126	127	30.40	19.18	-92.21	291.12
127	127	30.40	-0.01	-97.44	291.18
127	128	31.80	-0.01	-67.11	402.30
128	128	31.80	-0.01	-67.21	402.35
128	129	33.20	-0.01	-46.43	481.92
129	129	33.20	-0.01	-46.51	481.96
129	130	34.60	-0.01	-25.69	532.47
130	130	34.60	-0.01	-25.77	532.50
130	131	36.00	-0.01	-4.96	554.01
131	131	36.00	-0.01	-5.03	554.01
131	132	37.40	-0.01	15.78	546.48
132	132	37.40	-0.01	15.70	546.46
132	133	38.80	-0.01	36.51	509.92
133	133	38.80	-0.01	36.42	509.89
133	134	40.20	-0.01	57.22	444.35
134	134	40.20	-0.01	57.12	444.30
134	135	41.60	-0.01	77.92	349.77
135	135	41.60	9.87	75.44	349.71
135	136	43.00	18.58	105.76	216.28
136	136	43.00	-0.01	110.17	216.21
136	137	44.40	-0.01	186.43	28.94
137	137	44.40	0.00	185.92	28.73
137	138	45.80	0.00	220.64	-253.47
138	138	45.80	0.00	220.05	-253.62
138	139	47.20	0.00	252.32	-584.28
139	139	47.20	0.00	251.66	-584.42
139	140	48.60	0.00	283.93	-959.34
140	140	48.60	0.00	283.20	-959.42
140	141	50.00	0.00	322.49	-1383.38
141	1141	50.00	0.00	-322.49	-1383.38
141	142	51.40	0.00	-283.20	-959.42
142	142	51.40	0.00	-283.92	-959.33
142	143	52.80	0.00	-251.65	-584.40
143	143	52.80	0.00	-252.34	-584.26
143	144	54.20	0.00	-220.05	-253.64
144	144	54.20	0.00	-220.65	-253.46
144	145	55.60	0.00	-185.93	28.75
145	145	55.60	0.00	-186.43	28.94
145	146	57.00	0.00	-110.17	216.21
146	146	57.00	18.58	-105.77	216.29
146	147	58.40	9.87	-75.45	349.72
147	147	58.40	0.00	-77.92	349.79
147	148	59.80	0.00	-57.12	444.30
148	148	59.80	0.00	-57.22	444.35

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PERM1.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.T0.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-36.42	509.89
149	149	61.20	0.00	-36.51	509.93
149	150	62.60	0.00	-15.70	546.48
150	150	62.60	0.00	-15.78	546.50
150	151	64.00	0.00	5.03	554.01
151	151	64.00	0.00	4.96	554.01
151	152	65.40	0.00	25.77	532.50
152	152	65.40	0.00	25.69	532.48
152	153	66.80	0.00	46.50	481.96
153	153	66.80	0.00	46.43	481.93
153	154	68.20	0.00	67.21	402.36
154	154	68.20	0.00	67.11	402.31
154	155	69.60	0.00	97.44	291.19
155	155	69.60	19.19	92.21	291.12
155	156	71.00	23.91	115.25	137.91
156	156	71.00	0.00	121.40	137.84
156	157	72.40	0.00	195.87	-49.90
157	157	72.40	0.00	195.36	-50.07
157	158	73.80	0.00	225.44	-344.65
158	158	73.80	0.00	224.85	-344.83
158	159	75.20	0.00	261.36	-684.98
159	159	75.20	0.00	260.71	-685.12
159	160	76.60	0.00	293.00	-1072.75
160	160	76.60	0.00	292.29	-1072.86
160	161	78.00	0.00	331.58	-1509.54
161	1161	78.00	0.00	-325.09	-1509.55
161	162	79.10	0.00	-294.24	-1168.92
162	162	79.10	0.00	-294.80	-1168.88
162	163	80.20	0.00	-269.45	-858.52
163	163	80.20	0.00	-269.98	-858.44
163	164	81.30	0.00	-244.62	-575.42
164	164	81.30	0.00	-245.11	-575.31
164	165	82.40	0.00	-216.53	-320.51
165	165	82.40	0.00	-216.98	-320.38
165	166	83.50	0.00	-193.37	-94.70
166	166	83.50	0.00	-193.78	-94.59
166	167	84.60	0.00	-123.46	60.64
167	167	84.60	35.50	-112.44	60.69
167	168	85.70	24.30	-85.05	185.35
168	168	85.70	0.00	-92.79	185.39
168	169	86.80	0.00	-76.43	278.46
169	169	86.80	0.00	-76.54	278.49
169	170	87.90	0.00	-60.21	353.71
170	170	87.90	0.00	-60.30	353.74
170	171	89.00	0.00	-43.95	411.08
171	171	89.00	0.00	-44.03	411.10
171	172	90.10	0.00	-27.69	450.53
172	172	90.10	0.00	-27.77	450.54
172	173	91.20	0.00	-11.43	472.09
173	173	91.20	0.00	-11.51	472.09
173	174	92.30	0.00	4.84	475.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.T0.MZ-

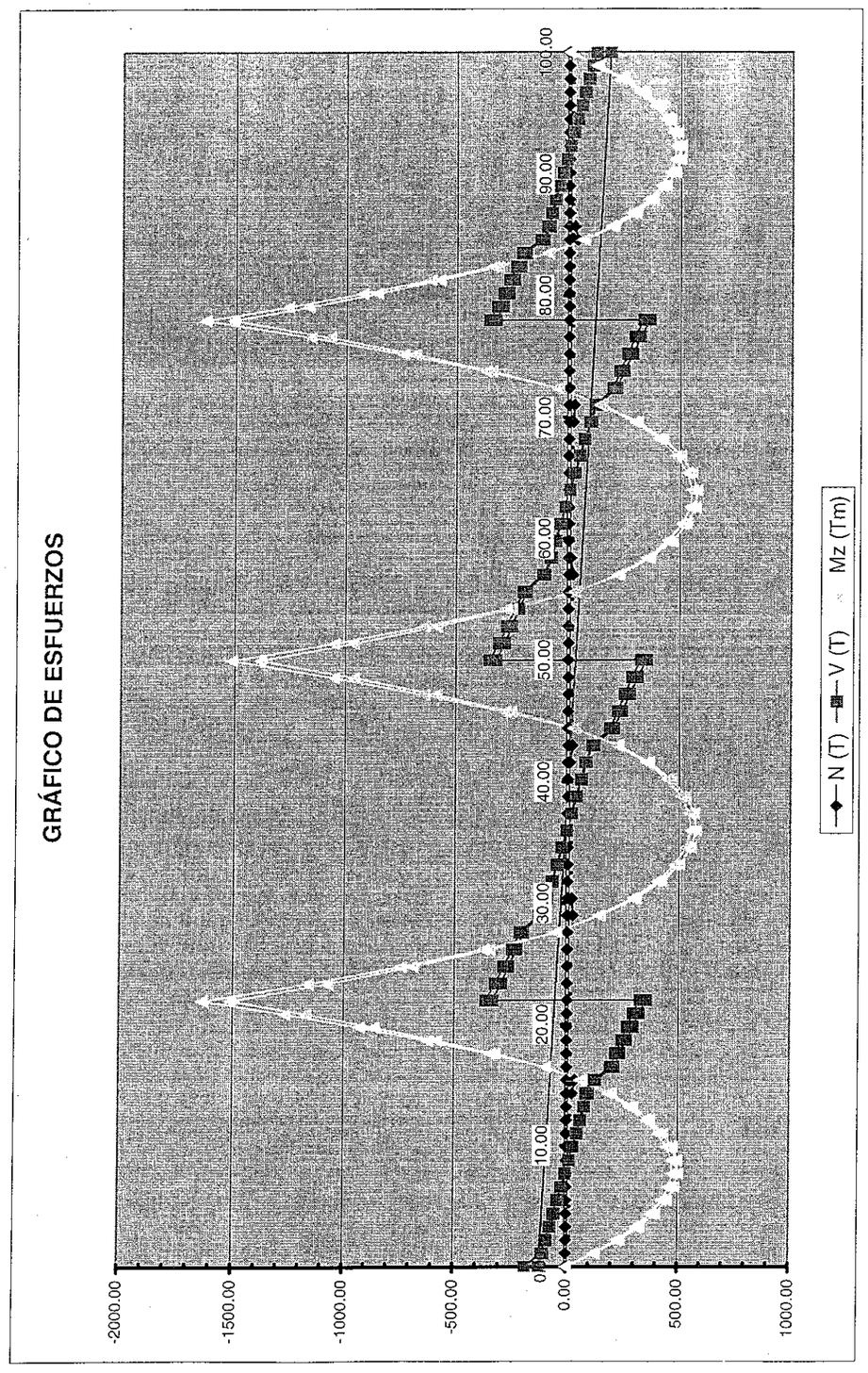
C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	4.76	475.74
174	175	93.40	0.00	21.10	461.51
175	175	93.40	0.00	21.01	461.49
175	176	94.50	0.00	37.35	429.37
176	176	94.50	0.00	37.24	429.33
176	177	95.60	0.00	53.59	379.37
177	177	95.60	0.00	53.47	379.31
177	178	96.70	0.00	69.81	311.50
178	178	96.70	0.00	69.66	311.44
178	179	97.80	0.00	86.02	225.82
179	179	97.80	0.00	85.85	225.75
179	180	98.90	0.00	102.18	122.34
180	180	98.90	0.00	101.97	122.27
180	181	100.00	0.00	120.25	0.04

05/09/03
Programa DINTEL PACADAR S.A.
PERM1.T0.MZ-



rotura.esf.xls

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-152.76	1.38
1	2	1.10	0.00	-376.26	441.37
2	2	1.10	0.00	-377.05	441.69
2	3	2.20	0.00	-326.90	823.92
3	3	2.20	0.00	-327.55	824.20
3	4	3.30	0.00	-277.48	1149.00
4	4	3.30	0.00	-277.94	1149.33
4	5	4.40	0.00	-218.66	1416.36
5	5	4.40	0.00	-218.96	1416.63
5	6	5.50	0.00	-165.75	1637.04
6	6	5.50	0.00	-166.03	1637.23
6	7	6.60	0.00	-115.78	1800.44
7	7	6.60	0.00	-116.01	1800.61
7	8	7.70	0.00	-65.89	1906.47
8	8	7.70	0.00	-65.95	1906.61
8	9	8.80	0.00	-16.30	1953.40
9	9	8.80	0.00	-16.27	1953.49
9	10	9.90	0.00	33.68	1953.08
10	10	9.90	0.00	33.76	1953.09
10	11	11.00	0.00	84.07	1895.92
11	11	11.00	0.00	84.09	1895.93
11	12	12.10	0.00	134.27	1781.59
12	12	12.10	0.00	134.39	1781.52
12	13	13.20	0.00	184.09	1609.03
13	13	13.20	0.00	184.15	1608.93
13	14	14.30	0.00	234.43	1386.26
14	14	14.30	30.79	224.81	1386.10
14	15	15.40	27.79	263.86	1120.00
15	15	15.40	0.00	272.54	1119.83
15	16	16.50	0.00	258.62	808.63
16	16	16.50	0.00	258.23	808.24
16	17	17.60	0.00	275.99	508.73
17	17	17.60	0.00	275.85	508.17
17	18	18.70	0.00	254.80	203.67
18	18	18.70	-0.01	254.65	202.77
18	19	19.80	-0.01	245.02	-74.42
19	19	19.80	0.00	244.74	-75.53
19	20	20.90	0.00	235.18	-339.97
20	20	20.90	0.00	234.26	-339.95
20	21	22.00	0.00	218.02	-599.23
21	1021	22.00	0.00	-208.44	-599.24
21	22	23.40	0.00	-212.54	-280.63
22	22	23.40	0.00	-213.56	-280.71
22	23	24.80	0.00	-220.38	25.60
23	23	24.80	0.00	-221.54	25.65
23	24	26.20	0.00	-282.14	371.03
24	24	26.20	0.00	-283.72	372.45
24	25	27.60	0.00	-280.64	761.84
25	25	27.60	-0.01	-280.88	763.17
25	26	29.00	-0.01	-319.35	1215.83
26	26	29.00	18.10	-314.34	1216.30

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INFRECT.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	14.61	-256.66	1616.14
27	27	30.40	-0.01	-260.48	1616.49
27	28	31.80	-0.01	-204.68	1937.99
28	28	31.80	-0.01	-204.43	1938.24
28	29	33.20	-0.01	-132.05	2173.01
29	29	33.20	-0.01	-131.72	2173.26
29	30	34.60	-0.01	-77.65	2321.20
30	30	34.60	-0.01	-77.28	2321.31
30	31	36.00	-0.01	-12.91	2375.37
31	31	36.00	-0.01	-12.62	2375.39
31	32	37.40	-0.01	60.50	2344.95
32	32	37.40	-0.01	60.84	2344.88
32	33	38.80	-0.01	114.90	2220.41
33	33	38.80	-0.01	115.23	2220.20
33	34	40.20	-0.01	187.70	2009.10
34	34	40.20	-0.01	187.94	2008.84
34	35	41.60	-0.01	253.26	1708.09
35	35	41.60	13.87	250.01	1707.70
35	36	43.00	13.36	300.96	1325.14
36	36	43.00	-0.01	304.35	1324.71
36	37	44.40	-0.01	277.55	898.67
37	37	44.40	0.00	277.45	897.49
37	38	45.80	0.00	281.26	505.32
38	38	45.80	0.00	280.48	503.71
38	39	47.20	0.00	236.98	146.69
39	39	47.20	0.00	237.13	145.86
39	40	48.60	0.00	218.79	-175.44
40	40	48.60	0.00	217.76	-175.39
40	41	50.00	0.00	212.06	-501.64
41	1041	50.00	0.00	-212.06	-501.64
41	42	51.40	0.00	-217.76	-175.40
42	42	51.40	0.00	-218.79	-175.44
42	43	52.80	0.00	-237.13	145.84
43	43	52.80	0.00	-236.98	146.67
43	44	54.20	0.00	-280.48	503.72
44	44	54.20	0.00	-281.26	505.33
44	45	55.60	0.00	-277.46	897.52
45	45	55.60	0.00	-277.55	898.68
45	46	57.00	0.00	-304.35	1324.74
46	46	57.00	13.37	-300.97	1325.19
46	47	58.40	13.88	-250.02	1707.74
47	47	58.40	0.00	-253.26	1708.13
47	48	59.80	0.00	-187.94	2008.91
48	48	59.80	0.00	-187.70	2009.17
48	49	61.20	0.00	-115.23	2220.21
49	49	61.20	0.00	-114.90	2220.38
49	50	62.60	0.00	-60.84	2344.91
50	50	62.60	0.00	-60.49	2345.02
50	51	64.00	0.00	12.62	2375.40
51	51	64.00	0.00	12.91	2375.40
51	52	65.40	0.00	77.26	2321.34

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	77.63	2321.22
52	53	66.80	0.00	131.72	2173.34
53	53	66.80	0.00	132.04	2173.09
53	54	68.20	0.00	204.43	1938.34
54	54	68.20	0.00	204.68	1938.08
54	55	69.60	0.00	260.48	1616.53
55	55	69.60	14.62	256.68	1616.20
55	56	71.00	18.11	314.37	1216.32
56	56	71.00	0.00	319.33	1215.85
56	57	72.40	0.00	280.88	763.20
57	57	72.40	0.00	280.66	761.87
57	58	73.80	0.00	283.71	372.43
58	58	73.80	0.00	282.12	371.02
58	59	75.20	0.00	221.56	25.65
59	59	75.20	0.00	220.37	25.58
59	60	76.60	0.00	213.55	-280.73
60	60	76.60	0.00	212.54	-280.65
60	61	78.00	0.00	208.44	-599.24
61	1061	78.00	0.00	-218.02	-599.25
61	62	79.10	0.00	-234.26	-339.96
62	62	79.10	0.00	-235.19	-339.99
62	63	80.20	0.00	-244.75	-75.53
63	63	80.20	0.00	-245.02	-74.42
63	64	81.30	0.00	-254.65	202.79
64	64	81.30	0.00	-254.80	203.66
64	65	82.40	0.00	-275.85	508.17
65	65	82.40	0.00	-276.01	508.72
65	66	83.50	0.00	-258.23	808.28
66	66	83.50	0.00	-258.63	808.66
66	67	84.60	0.00	-272.55	1119.86
67	67	84.60	27.79	-263.85	1120.07
67	68	85.70	30.79	-224.79	1386.19
68	68	85.70	0.00	-234.44	1386.32
68	69	86.80	0.00	-184.16	1608.99
69	69	86.80	0.00	-184.11	1609.13
69	70	87.90	0.00	-134.40	1781.56
70	70	87.90	0.00	-134.28	1781.65
70	71	89.00	0.00	-84.13	1895.97
71	71	89.00	0.00	-84.08	1895.99
71	72	90.10	0.00	-33.77	1953.17
72	72	90.10	0.00	-33.71	1953.14
72	73	91.20	0.00	16.24	1953.58
73	73	91.20	0.00	16.28	1953.49
73	74	92.30	0.00	65.95	1906.68
74	74	92.30	0.00	65.85	1906.55
74	75	93.40	0.00	115.99	1800.69
75	75	93.40	0.00	115.77	1800.48
75	76	94.50	0.00	166.02	1637.29
76	76	94.50	0.00	165.74	1637.10
76	77	95.60	0.00	218.95	1416.70
77	77	95.60	0.00	218.63	1416.43

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INFRECT.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	277.92	1149.30
78	78	96.70	0.00	277.46	1149.03
78	79	97.80	0.00	327.53	824.16
79	79	97.80	0.00	326.88	823.90
79	80	98.90	0.00	377.03	441.69
80	80	98.90	0.00	376.24	441.37
80	81	100.00	0.00	152.75	1.38
101	101	0.00	0.00	-182.11	1.19
101	102	1.10	0.00	-410.29	479.49
102	102	1.10	0.00	-408.44	478.85
102	103	2.20	0.00	-355.48	892.81
103	103	2.20	0.00	-353.89	892.21
103	104	3.30	0.00	-301.07	1242.60
104	104	3.30	0.00	-299.68	1242.05
104	105	4.40	0.00	-246.69	1529.97
105	105	4.40	0.00	-245.60	1529.43
105	106	5.50	0.00	-177.98	1766.79
106	106	5.50	0.00	-177.20	1766.36
106	107	6.60	0.00	-124.16	1941.75
107	107	6.60	0.00	-123.47	1941.46
107	108	7.70	0.00	-70.59	2054.92
108	108	7.70	0.00	-70.01	2054.74
108	109	8.80	0.00	-17.15	2106.33
109	109	8.80	0.00	-16.71	2106.26
109	110	9.90	0.00	36.19	2105.73
110	110	9.90	0.00	36.60	2105.66
110	111	11.00	0.00	89.65	2045.25
111	111	11.00	0.00	90.01	2045.29
111	112	12.10	0.00	142.96	1923.91
112	112	12.10	0.00	143.33	1924.05
112	113	13.20	0.00	196.04	1741.68
113	113	13.20	0.00	196.38	1741.85
113	114	14.30	0.00	249.36	1505.20
114	114	14.30	30.79	240.11	1505.49
114	115	15.40	27.79	281.74	1222.45
115	115	15.40	0.00	290.82	1222.79
115	116	16.50	0.00	288.77	891.38
116	116	16.50	0.00	289.68	891.82
116	117	17.60	0.00	309.49	557.03
117	117	17.60	0.00	310.38	557.32
117	118	18.70	0.00	271.09	224.83
118	118	18.70	0.00	271.71	224.46
118	119	19.80	0.00	245.57	-62.30
119	119	19.80	0.00	245.49	-62.69
119	120	20.90	0.00	221.70	-320.09
120	120	20.90	0.00	221.06	-320.08
120	121	22.00	0.00	214.09	-574.48
121	1121	22.00	0.00	-205.31	-574.48
121	122	23.40	0.00	-214.58	-259.08
122	122	23.40	0.00	-215.37	-259.05
122	123	24.80	0.00	-224.33	52.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-225.58	52.42
123	124	26.20	0.00	-302.93	408.72
124	124	26.20	0.00	-302.20	409.24
124	125	27.60	0.00	-302.69	828.14
125	125	27.60	-0.01	-301.55	828.43
125	126	29.00	-0.01	-338.08	1299.19
126	126	29.00	18.10	-332.89	1298.79
126	127	30.40	14.61	-271.04	1720.11
127	127	30.40	-0.01	-274.84	1719.70
127	128	31.80	-0.01	-215.26	2057.02
128	128	31.80	-0.01	-215.24	2056.69
128	129	33.20	-0.01	-137.50	2302.79
129	129	33.20	-0.01	-137.63	2302.55
129	130	34.60	-0.01	-82.01	2457.97
130	130	34.60	-0.01	-82.18	2457.87
130	131	36.00	-0.01	-13.89	2513.93
131	131	36.00	-0.01	-14.07	2513.89
131	132	37.40	-0.01	64.79	2482.28
132	132	37.40	-0.01	64.60	2482.36
132	133	38.80	-0.01	120.17	2351.21
133	133	38.80	-0.01	120.06	2351.46
133	134	40.20	-0.01	197.82	2130.06
134	134	40.20	-0.01	197.81	2130.37
134	135	41.60	-0.01	266.80	1814.79
135	135	41.60	13.87	263.60	1815.19
135	136	43.00	13.36	318.38	1412.52
136	136	43.00	-0.01	321.86	1412.94
136	137	44.40	-0.01	300.46	966.66
137	137	44.40	0.00	301.46	966.54
137	138	45.80	0.00	301.28	544.25
138	138	45.80	0.00	302.46	543.59
138	139	47.20	0.00	240.25	173.42
139	139	47.20	0.00	240.73	173.22
139	140	48.60	0.00	219.82	-148.77
140	140	48.60	0.00	218.99	-148.75
140	141	50.00	0.00	207.93	-470.78
141	1141	50.00	0.00	-207.93	-470.78
141	142	51.40	0.00	-218.99	-148.77
142	142	51.40	0.00	-219.81	-148.79
142	143	52.80	0.00	-240.72	173.21
143	143	52.80	0.00	-240.26	173.42
143	144	54.20	0.00	-302.46	543.59
144	144	54.20	0.00	-301.31	544.26
144	145	55.60	0.00	-301.47	966.58
145	145	55.60	0.00	-300.50	966.69
145	146	57.00	0.00	-321.86	1413.03
146	146	57.00	13.36	-318.41	1412.61
146	147	58.40	13.87	-263.64	1815.28
147	147	58.40	0.00	-266.85	1814.85
147	148	59.80	0.00	-197.85	2130.44
148	148	59.80	0.00	-197.84	2130.15

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECT.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-120.07	2351.51
149	149	61.20	0.00	-120.19	2351.30
149	150	62.60	0.00	-64.60	2482.49
150	150	62.60	0.00	-64.79	2482.40
150	151	64.00	0.00	14.07	2513.98
151	151	64.00	0.00	13.89	2514.00
151	152	65.40	0.00	82.18	2457.93
152	152	65.40	0.00	82.00	2458.04
152	153	66.80	0.00	137.60	2302.66
153	153	66.80	0.00	137.52	2302.89
153	154	68.20	0.00	215.24	2056.78
154	154	68.20	0.00	215.26	2057.07
154	155	69.60	0.00	274.82	1719.76
155	155	69.60	14.62	271.05	1720.20
155	156	71.00	18.11	332.89	1298.84
156	156	71.00	0.00	338.12	1299.24
156	157	72.40	0.00	301.55	828.45
157	157	72.40	0.00	302.70	828.16
157	158	73.80	0.00	302.21	409.23
158	158	73.80	0.00	302.93	408.70
158	159	75.20	0.00	225.58	52.41
159	159	75.20	0.00	224.32	52.73
159	160	76.60	0.00	215.37	-259.05
160	160	76.60	0.00	214.58	-259.09
160	161	78.00	0.00	205.31	-574.46
161	1161	78.00	0.00	-214.09	-574.51
161	162	79.10	0.00	-221.06	-320.08
162	162	79.10	0.00	-221.70	-320.14
162	163	80.20	0.00	-245.52	-62.69
163	163	80.20	0.00	-245.59	-62.32
163	164	81.30	0.00	-271.71	224.48
164	164	81.30	0.00	-271.09	224.84
164	165	82.40	0.00	-310.38	557.34
165	165	82.40	0.00	-309.51	557.07
165	166	83.50	0.00	-289.69	891.87
166	166	83.50	0.00	-288.78	891.46
166	167	84.60	0.00	-290.84	1222.85
167	167	84.60	27.79	-281.73	1222.50
167	168	85.70	30.79	-240.10	1505.56
168	168	85.70	0.00	-249.35	1505.25
168	169	86.80	0.00	-196.37	1741.95
169	169	86.80	0.00	-196.05	1741.71
169	170	87.90	0.00	-143.35	1924.10
170	170	87.90	0.00	-142.96	1923.96
170	171	89.00	0.00	-90.03	2045.35
171	171	89.00	0.00	-89.68	2045.28
171	172	90.10	0.00	-36.61	2105.69
172	172	90.10	0.00	-36.24	2105.74
172	173	91.20	0.00	16.68	2106.27
173	173	91.20	0.00	17.11	2106.38
173	174	92.30	0.00	69.96	2054.80

CÁLCULO TENSIONAL

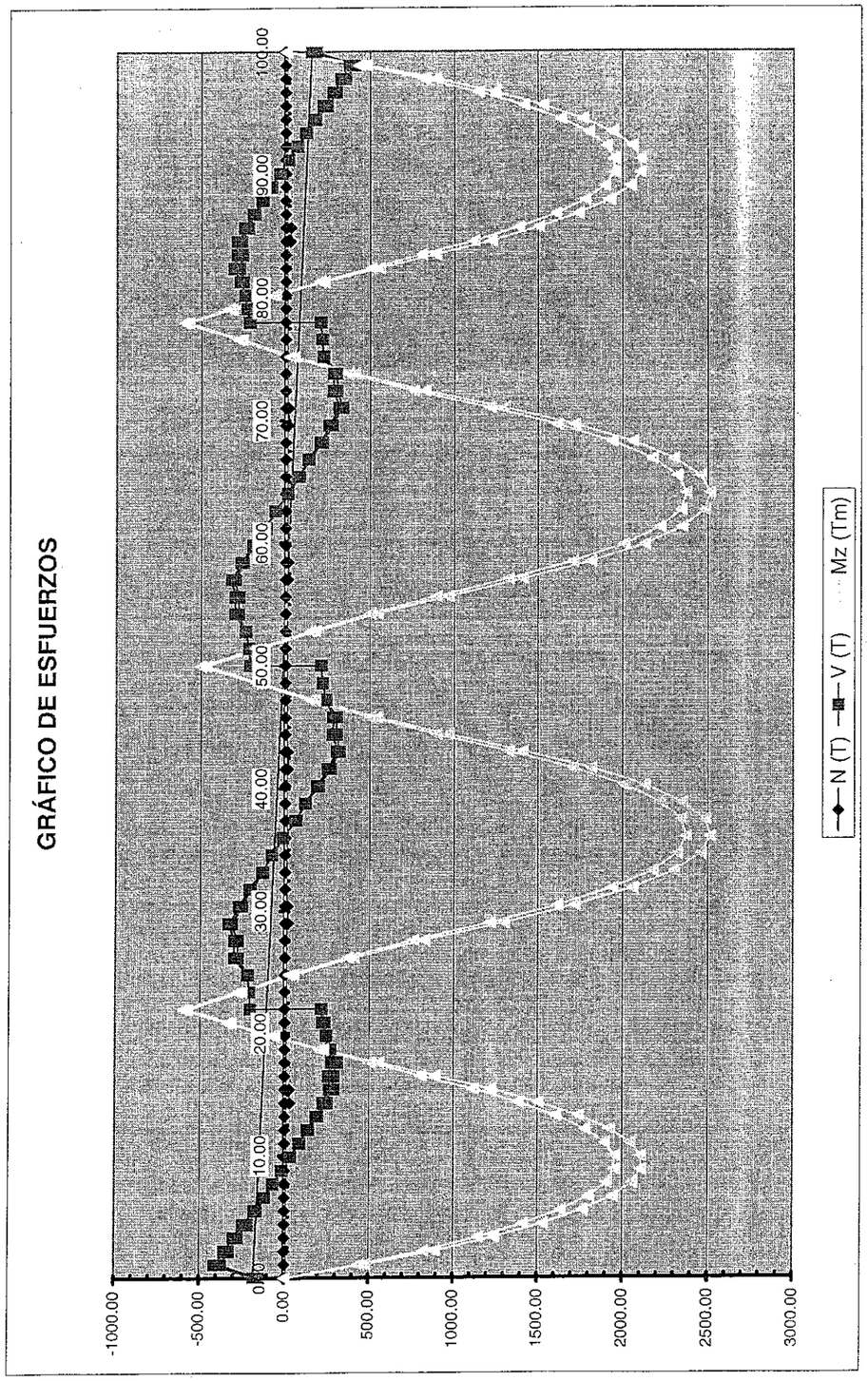
Hipótesis de cálculo:
INFRECT.T0.MZ+

C. Totales dominante Tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	70.58	2054.98
174	175	93.40	0.00	123.46	1941.52
175	175	93.40	0.00	124.17	1941.80
175	176	94.50	0.00	177.21	1766.43
176	176	94.50	0.00	177.97	1766.86
176	177	95.60	0.00	245.58	1529.49
177	177	95.60	0.00	246.67	1529.99
177	178	96.70	0.00	299.67	1242.06
178	178	96.70	0.00	301.03	1242.60
178	179	97.80	0.00	353.87	892.19
179	179	97.80	0.00	355.44	892.81
179	180	98.90	0.00	408.42	478.87
180	180	98.90	0.00	410.27	479.49
180	181	100.00	0.00	182.10	1.19



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-318.83	-1.19
1	2	1.10	0.00	-76.31	95.34
2	2	1.10	0.00	-76.91	95.34
2	3	2.20	0.00	-58.12	169.62
3	3	2.20	0.00	-58.71	169.62
3	4	3.30	0.00	-39.90	223.83
4	4	3.30	0.00	-40.48	223.83
4	5	4.40	0.00	-21.71	258.02
5	5	4.40	0.00	-22.29	258.02
5	6	5.50	0.00	-3.49	272.18
6	6	5.50	0.00	-4.10	272.15
6	7	6.60	0.00	14.71	266.37
7	7	6.60	0.00	14.02	266.31
7	8	7.70	0.00	32.82	240.55
8	8	7.70	0.00	32.15	240.52
8	9	8.80	0.00	51.39	194.80
9	9	8.80	0.00	50.50	194.74
9	10	9.90	0.00	69.49	128.80
10	10	9.90	0.00	68.66	128.78
10	11	11.00	0.00	87.45	42.89
11	11	11.00	0.00	86.56	42.84
11	12	12.10	0.00	105.40	-62.73
12	12	12.10	0.00	104.48	-62.80
12	13	13.20	0.00	123.38	-188.22
13	13	13.20	0.00	122.43	-188.27
13	14	14.30	0.00	141.27	-333.32
14	14	14.30	24.30	132.68	-333.39
14	15	15.40	35.50	162.60	-511.87
15	15	15.40	0.00	172.71	-511.90
15	16	16.50	0.00	255.60	-722.81
16	16	16.50	0.00	254.88	-722.69
16	17	17.60	0.00	294.66	-1020.66
17	17	17.60	0.00	293.49	-1020.33
17	18	18.70	0.00	363.41	-1381.70
18	18	18.70	-0.01	362.32	-1380.98
18	19	19.80	-0.01	438.02	-1818.72
19	19	19.80	0.00	437.07	-1817.76
19	20	20.90	0.00	535.09	-2362.45
20	20	20.90	0.00	534.49	-2362.42
20	21	22.00	0.00	618.33	-2994.52
21	1021	22.00	0.00	-653.51	-2994.35
21	22	23.40	0.00	-567.29	-2148.92
22	22	23.40	0.00	-568.01	-2148.63
22	23	24.80	0.00	-467.44	-1424.16
23	23	24.80	0.00	-465.26	-1424.09
23	24	26.20	0.00	-339.53	-877.92
24	24	26.20	0.00	-339.56	-878.98
24	25	27.60	0.00	-253.31	-465.22
25	25	27.60	-0.01	-254.49	-466.22
25	26	29.00	-0.01	-128.19	-237.56
26	26	29.00	23.90	-123.28	-237.66

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INFRECT.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.18	-94.56	-77.90
27	27	30.40	-0.01	-100.88	-77.94
27	28	31.80	-0.01	-67.30	35.77
28	28	31.80	-0.01	-68.51	35.71
28	29	33.20	-0.01	-44.61	114.89
29	29	33.20	-0.01	-45.72	114.90
29	30	34.60	-0.01	-19.44	160.05
30	30	34.60	-0.01	-20.51	159.94
30	31	36.00	-0.01	10.32	165.92
31	31	36.00	-0.01	9.26	165.89
31	32	37.40	-0.01	33.39	136.14
32	32	37.40	-0.01	32.21	136.10
32	33	38.80	-0.01	56.13	74.27
33	33	38.80	-0.01	54.95	74.25
33	34	40.20	-0.01	78.88	-19.46
34	34	40.20	-0.01	77.66	-19.44
34	35	41.60	-0.01	101.75	-144.96
35	35	41.60	9.87	98.15	-144.96
35	36	43.00	18.58	133.67	-313.11
36	36	43.00	-0.01	136.80	-313.01
36	37	44.40	-0.01	251.46	-559.30
37	37	44.40	0.00	250.15	-558.50
37	38	45.80	0.00	335.64	-960.52
38	38	45.80	0.00	334.54	-959.27
38	39	47.20	0.00	428.76	-1486.38
39	39	47.20	0.00	427.02	-1485.71
39	40	48.60	0.00	553.08	-2175.71
40	40	48.60	0.00	552.22	-2175.77
40	41	50.00	0.00	643.43	-3006.34
41	1041	50.00	0.00	-643.43	-3006.34
41	42	51.40	0.00	-552.24	-2175.76
42	42	51.40	0.00	-553.08	-2175.71
42	43	52.80	0.00	-427.02	-1485.69
43	43	52.80	0.00	-428.76	-1486.36
43	44	54.20	0.00	-334.54	-959.24
44	44	54.20	0.00	-335.64	-960.51
44	45	55.60	0.00	-250.13	-558.46
45	45	55.60	0.00	-251.46	-559.28
45	46	57.00	0.00	-136.78	-312.95
46	46	57.00	18.59	-133.68	-313.09
46	47	58.40	9.88	-98.16	-144.96
47	47	58.40	0.00	-101.74	-144.96
47	48	59.80	0.00	-77.66	-19.43
48	48	59.80	0.00	-78.87	-19.42
48	49	61.20	0.00	-54.93	74.24
49	49	61.20	0.00	-56.13	74.26
49	50	62.60	0.00	-32.21	136.11
50	50	62.60	0.00	-33.38	136.11
50	51	64.00	0.00	-9.26	165.90
51	51	64.00	0.00	-10.32	165.90
51	52	65.40	0.00	20.53	159.93

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	19.44	160.02
52	53	66.80	0.00	45.72	114.88
53	53	66.80	0.00	44.62	114.89
53	54	68.20	0.00	68.51	35.72
54	54	68.20	0.00	67.30	35.73
54	55	69.60	0.00	100.88	-77.95
55	55	69.60	19.19	94.57	-77.94
55	56	71.00	23.91	123.29	-237.66
56	56	71.00	0.00	128.19	-237.56
56	57	72.40	0.00	254.49	-466.22
57	57	72.40	0.00	253.34	-465.24
57	58	73.80	0.00	339.58	-879.00
58	58	73.80	0.00	339.53	-877.93
58	59	75.20	0.00	465.26	-1424.12
59	59	75.20	0.00	467.43	-1424.14
59	60	76.60	0.00	568.00	-2148.65
60	60	76.60	0.00	567.29	-2148.94
60	61	78.00	0.00	653.55	-2994.38
61	1061	78.00	0.00	-618.33	-2994.61
61	62	79.10	0.00	-534.49	-2362.48
62	62	79.10	0.00	-535.11	-2362.53
62	63	80.20	0.00	-437.08	-1817.79
63	63	80.20	0.00	-438.04	-1818.77
63	64	81.30	0.00	-362.34	-1381.01
64	64	81.30	0.00	-363.41	-1381.75
64	65	82.40	0.00	-293.49	-1020.35
65	65	82.40	0.00	-294.66	-1020.69
65	66	83.50	0.00	-254.88	-722.72
66	66	83.50	0.00	-255.61	-722.82
66	67	84.60	0.00	-172.72	-511.92
67	67	84.60	35.50	-162.59	-511.90
67	68	85.70	24.30	-132.66	-333.42
68	68	85.70	0.00	-141.27	-333.36
68	69	86.80	0.00	-122.43	-188.30
69	69	86.80	0.00	-123.39	-188.24
69	70	87.90	0.00	-104.49	-62.85
70	70	87.90	0.00	-105.41	-62.78
70	71	89.00	0.00	-86.57	42.80
71	71	89.00	0.00	-87.46	42.85
71	72	90.10	0.00	-68.67	128.73
72	72	90.10	0.00	-69.50	128.77
72	73	91.20	0.00	-50.51	194.68
73	73	91.20	0.00	-51.40	194.78
73	74	92.30	0.00	-32.16	240.49
74	74	92.30	0.00	-32.83	240.52
74	75	93.40	0.00	-14.03	266.30
75	75	93.40	0.00	-14.72	266.33
75	76	94.50	0.00	4.09	272.14
76	76	94.50	0.00	3.48	272.19
76	77	95.60	0.00	22.28	257.99
77	77	95.60	0.00	21.70	258.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	40.47	223.80
78	78	96.70	0.00	39.89	223.79
78	79	97.80	0.00	58.70	169.61
79	79	97.80	0.00	58.09	169.61
79	80	98.90	0.00	76.87	95.34
80	80	98.90	0.00	76.30	95.34
80	81	100.00	0.00	318.80	-1.19
101	101	0.00	0.00	-322.74	-1.38
101	102	1.10	0.00	-74.44	93.25
102	102	1.10	0.00	-74.86	93.55
102	103	2.20	0.00	-56.30	165.65
103	103	2.20	0.00	-56.60	165.93
103	104	3.30	0.00	-38.08	217.95
104	104	3.30	0.00	-38.20	218.21
104	105	4.40	0.00	-19.71	250.05
105	105	4.40	0.00	-19.73	250.24
105	106	5.50	0.00	-1.20	261.74
106	106	5.50	0.00	-1.05	261.93
106	107	6.60	0.00	17.50	252.90
107	107	6.60	0.00	17.71	253.07
107	108	7.70	0.00	36.21	223.41
108	108	7.70	0.00	36.50	223.57
108	109	8.80	0.00	55.01	173.25
109	109	8.80	0.00	55.32	173.36
109	110	9.90	0.00	73.84	102.27
110	110	9.90	0.00	74.24	102.34
110	111	11.00	0.00	92.77	10.54
111	111	11.00	0.00	93.26	10.59
111	112	12.10	0.00	111.78	-102.22
112	112	12.10	0.00	112.31	-102.19
112	113	13.20	0.00	130.80	-235.95
113	113	13.20	0.00	131.38	-235.98
113	114	14.30	0.00	149.97	-390.73
114	114	14.30	24.30	143.00	-390.80
114	115	15.40	35.50	173.01	-580.48
115	115	15.40	0.00	184.88	-580.62
115	116	16.50	0.00	258.12	-805.08
116	116	16.50	0.00	258.71	-805.24
116	117	17.60	0.00	296.54	-1106.92
117	117	17.60	0.00	296.94	-1106.94
117	118	18.70	0.00	381.78	-1483.29
118	118	18.70	0.00	382.46	-1482.76
118	119	19.80	0.00	476.64	-1952.90
119	119	19.80	0.00	478.13	-1952.49
119	120	20.90	0.00	598.44	-2558.34
120	120	20.90	0.00	600.46	-2558.23
120	121	22.00	0.00	678.33	-3255.14
121	1121	22.00	0.00	-710.18	-3255.11
121	122	23.40	0.00	-616.09	-2333.46
122	122	23.40	0.00	-613.46	-2333.65
122	123	24.80	0.00	-507.32	-1550.90

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-504.33	-1550.96
123	124	26.20	0.00	-359.58	-965.20
124	124	26.20	0.00	-358.71	-966.06
124	125	27.60	0.00	-265.23	-532.87
125	125	27.60	-0.01	-264.96	-533.57
125	126	29.00	-0.01	-137.27	-283.28
126	126	29.00	23.90	-130.07	-283.16
126	127	30.40	19.18	-102.69	-112.74
127	127	30.40	-0.01	-106.84	-112.66
127	128	31.80	-0.01	-73.50	9.42
128	128	31.80	-0.01	-72.51	9.49
128	129	33.20	-0.01	-48.96	94.59
129	129	33.20	-0.01	-48.06	94.63
129	130	34.60	-0.01	-22.33	143.84
130	130	34.60	-0.01	-21.41	143.78
130	131	36.00	-0.01	10.49	150.41
131	131	36.00	-0.01	11.42	150.43
131	132	37.40	-0.01	35.04	117.92
132	132	37.40	-0.01	35.97	117.92
132	133	38.80	-0.01	59.54	51.06
133	133	38.80	-0.01	60.52	51.05
133	134	40.20	-0.01	84.13	-50.19
134	134	40.20	-0.01	85.10	-50.24
134	135	41.60	-0.01	108.93	-186.00
135	135	41.60	9.87	107.57	-186.06
135	136	43.00	18.58	142.11	-367.00
136	136	43.00	-0.01	147.76	-367.08
136	137	44.40	-0.01	260.38	-633.93
137	137	44.40	0.00	260.88	-633.45
137	138	45.80	0.00	353.75	-1055.14
138	138	45.80	0.00	354.26	-1054.10
138	139	47.20	0.00	461.77	-1618.66
139	139	47.20	0.00	463.04	-1618.25
139	140	48.60	0.00	600.26	-2371.38
140	140	48.60	0.00	602.91	-2371.19
140	141	50.00	0.00	702.34	-3281.15
141	1141	50.00	0.00	-702.36	-3281.15
141	142	51.40	0.00	-602.91	-2371.15
142	142	51.40	0.00	-600.25	-2371.35
142	143	52.80	0.00	-463.03	-1618.20
143	143	52.80	0.00	-461.77	-1618.61
143	144	54.20	0.00	-354.24	-1054.08
144	144	54.20	0.00	-353.76	-1055.10
144	145	55.60	0.00	-260.89	-633.39
145	145	55.60	0.00	-260.38	-633.87
145	146	57.00	0.00	-147.76	-367.06
146	146	57.00	18.58	-142.12	-366.98
146	147	58.40	9.87	-107.58	-186.05
147	147	58.40	0.00	-108.93	-185.97
147	148	59.80	0.00	-85.10	-50.26
148	148	59.80	0.00	-84.13	-50.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-60.52	51.06
149	149	61.20	0.00	-59.54	51.05
149	150	62.60	0.00	-35.97	117.92
150	150	62.60	0.00	-35.04	117.92
150	151	64.00	0.00	-11.42	150.38
151	151	64.00	0.00	-10.49	150.37
151	152	65.40	0.00	21.41	143.74
152	152	65.40	0.00	22.33	143.81
152	153	66.80	0.00	48.05	94.58
153	153	66.80	0.00	48.96	94.55
153	154	68.20	0.00	72.51	9.43
154	154	68.20	0.00	73.50	9.37
154	155	69.60	0.00	106.84	-112.71
155	155	69.60	19.19	102.67	-112.78
155	156	71.00	23.91	130.06	-283.20
156	156	71.00	0.00	137.29	-283.33
156	157	72.40	0.00	264.98	-533.61
157	157	72.40	0.00	265.24	-532.89
157	158	73.80	0.00	358.72	-966.09
158	158	73.80	0.00	359.58	-965.21
158	159	75.20	0.00	504.37	-1550.95
159	159	75.20	0.00	507.30	-1550.92
159	160	76.60	0.00	613.46	-2333.67
160	160	76.60	0.00	616.09	-2333.52
160	161	78.00	0.00	710.20	-3255.18
161	1161	78.00	0.00	-678.33	-3255.21
161	162	79.10	0.00	-600.48	-2558.29
162	162	79.10	0.00	-598.44	-2558.44
162	163	80.20	0.00	-478.14	-1952.55
163	163	80.20	0.00	-476.64	-1952.96
163	164	81.30	0.00	-382.46	-1482.79
164	164	81.30	0.00	-381.78	-1483.32
164	165	82.40	0.00	-296.94	-1106.98
165	165	82.40	0.00	-296.54	-1106.94
165	166	83.50	0.00	-258.71	-805.30
166	166	83.50	0.00	-258.13	-805.11
166	167	84.60	0.00	-184.89	-580.64
167	167	84.60	35.50	-173.00	-580.54
167	168	85.70	24.30	-142.99	-390.83
168	168	85.70	0.00	-149.99	-390.78
168	169	86.80	0.00	-131.42	-236.01
169	169	86.80	0.00	-130.81	-235.98
169	170	87.90	0.00	-112.32	-102.22
170	170	87.90	0.00	-111.78	-102.25
170	171	89.00	0.00	-93.27	10.55
171	171	89.00	0.00	-92.79	10.52
171	172	90.10	0.00	-74.25	102.34
172	172	90.10	0.00	-73.83	102.25
172	173	91.20	0.00	-55.32	173.31
173	173	91.20	0.00	-55.03	173.21
173	174	92.30	0.00	-36.51	223.54

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.MZ-

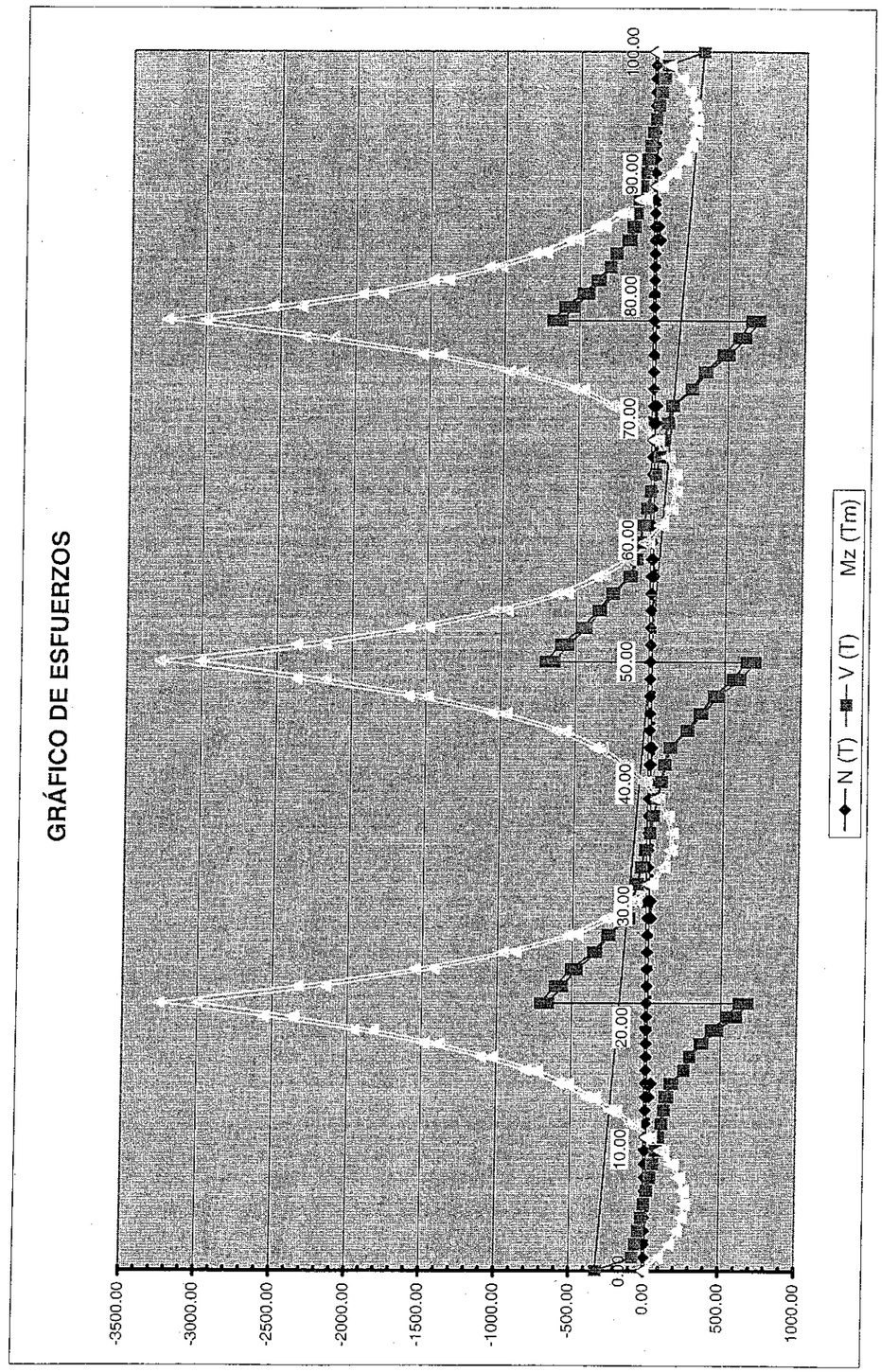
C. Totales dominante Tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-36.22	223.39
174	175	93.40	0.00	-17.72	253.05
175	175	93.40	0.00	-17.51	252.88
175	176	94.50	0.00	1.04	261.93
176	176	94.50	0.00	1.18	261.75
176	177	95.60	0.00	19.70	250.24
177	177	95.60	0.00	19.70	250.01
177	178	96.70	0.00	38.20	218.16
178	178	96.70	0.00	38.04	217.96
178	179	97.80	0.00	56.57	165.92
179	179	97.80	0.00	56.29	165.64
179	180	98.90	0.00	74.85	93.55
180	180	98.90	0.00	74.43	93.25
180	181	100.00	0.00	322.72	-1.38

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-147.60	1.09
1	2	1.10	0.00	-349.68	410.03
2	2	1.10	0.00	-350.20	410.26
2	3	2.20	0.00	-304.37	766.32
3	3	2.20	0.00	-304.80	766.51
3	4	3.30	0.00	-259.04	1070.24
4	4	3.30	0.00	-259.33	1070.47
4	5	4.40	0.00	-206.20	1321.62
5	5	4.40	0.00	-206.37	1321.81
5	6	5.50	0.00	-158.09	1529.32
6	6	5.50	0.00	-158.26	1529.45
6	7	6.60	0.00	-112.34	1684.85
7	7	6.60	0.00	-112.49	1684.98
7	8	7.70	0.00	-66.68	1788.16
8	8	7.70	0.00	-66.68	1788.26
8	9	8.80	0.00	-21.25	1837.86
9	9	8.80	0.00	-21.18	1837.92
9	10	9.90	0.00	24.50	1843.44
10	10	9.90	0.00	24.60	1843.46
10	11	11.00	0.00	70.56	1797.23
11	11	11.00	0.00	70.61	1797.25
11	12	12.10	0.00	116.47	1698.96
12	12	12.10	0.00	116.61	1698.92
12	13	13.20	0.00	162.08	1547.77
13	13	13.20	0.00	162.18	1547.70
13	14	14.30	0.00	208.13	1350.08
14	14	14.30	30.79	198.57	1349.97
14	15	15.40	27.79	233.30	1113.70
15	15	15.40	0.00	242.06	1113.59
15	16	16.50	0.00	223.93	837.11
16	16	16.50	0.00	223.65	836.80
16	17	17.60	0.00	241.91	576.20
17	17	17.60	0.00	241.84	575.75
17	18	18.70	0.00	228.07	307.38
18	18	18.70	-0.01	227.98	306.66
18	19	19.80	-0.01	224.00	56.17
19	19	19.80	0.00	223.81	55.29
19	20	20.90	0.00	219.88	-189.13
20	20	20.90	0.00	219.19	-189.10
20	21	22.00	0.00	207.88	-434.35
21	1021	22.00	0.00	-210.22	-434.36
21	22	23.40	0.00	-211.36	-116.96
22	22	23.40	0.00	-212.13	-117.04
22	23	24.80	0.00	-212.85	182.49
23	23	24.80	0.00	-213.73	182.52
23	24	26.20	0.00	-258.34	507.23
24	24	26.20	0.00	-259.55	508.35
24	25	27.60	0.00	-251.91	861.85
25	25	27.60	-0.01	-252.07	862.90
25	26	29.00	-0.01	-288.14	1275.11
26	26	29.00	18.10	-283.08	1275.46

rotura.esf.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECG.T0.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	14.61	-230.12	1636.03
27	27	30.40	-0.01	-233.90	1636.28
27	28	31.80	-0.01	-183.89	1926.24
28	28	31.80	-0.01	-183.64	1926.43
28	29	33.20	-0.01	-118.46	2137.29
29	29	33.20	-0.01	-118.16	2137.48
29	30	34.60	-0.01	-67.63	2268.63
30	30	34.60	-0.01	-67.30	2268.71
30	31	36.00	-0.01	-8.54	2314.54
31	31	36.00	-0.01	-8.27	2314.55
31	32	37.40	-0.01	57.50	2282.57
32	32	37.40	-0.01	57.81	2282.52
32	33	38.80	-0.01	108.32	2165.07
33	33	38.80	-0.01	108.63	2164.92
33	34	40.20	-0.01	173.87	1967.93
34	34	40.20	-0.01	174.12	1967.74
34	35	41.60	-0.01	233.65	1688.79
35	35	41.60	13.87	230.44	1688.50
35	36	43.00	13.36	276.56	1335.51
36	36	43.00	-0.01	280.00	1335.21
36	37	44.40	-0.01	252.87	942.15
37	37	44.40	0.00	252.83	941.22
37	38	45.80	0.00	260.13	580.83
38	38	45.80	0.00	259.55	579.56
38	39	47.20	0.00	229.47	241.40
39	39	47.20	0.00	229.65	240.74
39	40	48.60	0.00	219.70	-75.52
40	40	48.60	0.00	218.94	-75.48
40	41	50.00	0.00	216.51	-403.73
41	1041	50.00	0.00	-216.51	-403.73
41	42	51.40	0.00	-218.94	-75.48
42	42	51.40	0.00	-219.70	-75.52
42	43	52.80	0.00	-229.65	240.73
43	43	52.80	0.00	-229.47	241.38
43	44	54.20	0.00	-259.55	579.56
44	44	54.20	0.00	-260.13	580.83
44	45	55.60	0.00	-252.85	941.26
45	45	55.60	0.00	-252.87	942.17
45	46	57.00	0.00	-280.00	1335.23
46	46	57.00	13.37	-276.57	1335.56
46	47	58.40	13.88	-230.45	1688.54
47	47	58.40	0.00	-233.65	1688.82
47	48	59.80	0.00	-174.12	1967.80
48	48	59.80	0.00	-173.87	1967.98
48	49	61.20	0.00	-108.63	2164.93
49	49	61.20	0.00	-108.32	2165.05
49	50	62.60	0.00	-57.81	2282.54
50	50	62.60	0.00	-57.48	2282.62
50	51	64.00	0.00	8.27	2314.57
51	51	64.00	0.00	8.54	2314.57
51	52	65.40	0.00	67.29	2268.74

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	67.62	2268.65
52	53	66.80	0.00	118.16	2137.54
53	53	66.80	0.00	118.46	2137.36
53	54	68.20	0.00	183.64	1926.51
54	54	68.20	0.00	183.89	1926.33
54	55	69.60	0.00	233.90	1636.32
55	55	69.60	14.62	230.14	1636.09
55	56	71.00	18.11	283.12	1275.48
56	56	71.00	0.00	288.12	1275.14
56	57	72.40	0.00	252.07	862.92
57	57	72.40	0.00	251.93	861.87
57	58	73.80	0.00	259.55	508.34
58	58	73.80	0.00	258.32	507.22
58	59	75.20	0.00	213.74	182.51
59	59	75.20	0.00	212.84	182.47
59	60	76.60	0.00	212.12	-117.06
60	60	76.60	0.00	211.36	-116.98
60	61	78.00	0.00	210.22	-434.35
61	1061	78.00	0.00	-207.88	-434.36
61	62	79.10	0.00	-219.19	-189.12
62	62	79.10	0.00	-219.89	-189.14
62	63	80.20	0.00	-223.82	55.29
63	63	80.20	0.00	-224.00	56.18
63	64	81.30	0.00	-227.99	306.68
64	64	81.30	0.00	-228.07	307.37
64	65	82.40	0.00	-241.84	575.75
65	65	82.40	0.00	-241.93	576.19
65	66	83.50	0.00	-223.65	836.83
66	66	83.50	0.00	-223.94	837.13
66	67	84.60	0.00	-242.07	1113.62
67	67	84.60	27.79	-233.29	1113.76
67	68	85.70	30.79	-198.54	1350.04
68	68	85.70	0.00	-208.14	1350.12
68	69	86.80	0.00	-162.19	1547.76
69	69	86.80	0.00	-162.11	1547.85
69	70	87.90	0.00	-116.62	1698.94
70	70	87.90	0.00	-116.48	1698.99
70	71	89.00	0.00	-70.65	1797.27
71	71	89.00	0.00	-70.57	1797.28
71	72	90.10	0.00	-24.61	1843.52
72	72	90.10	0.00	-24.52	1843.49
72	73	91.20	0.00	21.15	1838.00
73	73	91.20	0.00	21.23	1837.93
73	74	92.30	0.00	66.67	1788.32
74	74	92.30	0.00	66.64	1788.23
74	75	93.40	0.00	112.46	1685.04
75	75	93.40	0.00	112.33	1684.88
75	76	94.50	0.00	158.25	1529.49
76	76	94.50	0.00	158.08	1529.36
76	77	95.60	0.00	206.36	1321.87
77	77	95.60	0.00	206.16	1321.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	259.30	1070.45
78	78	96.70	0.00	259.01	1070.26
78	79	97.80	0.00	304.78	766.47
79	79	97.80	0.00	304.35	766.29
79	80	98.90	0.00	350.18	410.26
80	80	98.90	0.00	349.65	410.03
80	81	100.00	0.00	147.59	1.09
101	101	0.00	0.00	-178.86	0.97
101	102	1.10	0.00	-373.86	437.04
102	102	1.10	0.00	-372.49	436.57
102	103	2.20	0.00	-324.73	815.08
103	103	2.20	0.00	-323.55	814.64
103	104	3.30	0.00	-275.90	1136.45
104	104	3.30	0.00	-274.86	1136.05
104	105	4.40	0.00	-227.09	1402.05
105	105	4.40	0.00	-226.28	1401.64
105	106	5.50	0.00	-166.80	1621.34
106	106	5.50	0.00	-166.22	1621.01
106	107	6.60	0.00	-118.41	1785.29
107	107	6.60	0.00	-117.90	1785.06
107	108	7.70	0.00	-70.21	1893.91
108	108	7.70	0.00	-69.79	1893.77
108	109	8.80	0.00	-22.11	1947.24
109	109	8.80	0.00	-21.80	1947.19
109	110	9.90	0.00	25.90	1953.07
110	110	9.90	0.00	26.20	1953.01
110	111	11.00	0.00	74.02	1905.13
111	111	11.00	0.00	74.26	1905.15
111	112	12.10	0.00	122.00	1802.60
112	112	12.10	0.00	122.26	1802.69
112	113	13.20	0.00	169.81	1645.49
113	113	13.20	0.00	170.03	1645.61
113	114	14.30	0.00	217.80	1439.11
114	114	14.30	30.79	208.42	1439.33
114	115	15.40	27.79	244.88	1192.32
115	115	15.40	0.00	253.82	1192.57
115	116	16.50	0.00	246.77	903.27
116	116	16.50	0.00	247.47	903.61
116	117	17.60	0.00	267.25	616.32
117	117	17.60	0.00	267.93	616.55
117	118	18.70	0.00	239.43	327.54
118	118	18.70	0.00	239.89	327.23
118	119	19.80	0.00	222.56	71.09
119	119	19.80	0.00	222.45	70.77
119	120	20.90	0.00	207.00	-165.79
120	120	20.90	0.00	206.44	-165.78
120	121	22.00	0.00	202.42	-404.65
121	1121	22.00	0.00	-205.45	-404.65
121	122	23.40	0.00	-210.90	-92.89
122	122	23.40	0.00	-211.59	-92.86
122	123	24.80	0.00	-214.19	208.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-215.24	208.15
123	124	26.20	0.00	-273.42	539.31
124	124	26.20	0.00	-272.88	539.74
124	125	27.60	0.00	-268.26	914.91
125	125	27.60	-0.01	-267.38	915.16
125	126	29.00	-0.01	-300.49	1337.94
126	126	29.00	18.10	-295.45	1337.66
126	127	30.40	14.61	-239.56	1712.25
127	127	30.40	-0.01	-243.45	1711.96
127	128	31.80	-0.01	-190.83	2012.17
128	128	31.80	-0.01	-190.87	2011.93
128	129	33.20	-0.01	-121.83	2230.16
129	129	33.20	-0.01	-121.97	2229.99
129	130	34.60	-0.01	-70.62	2366.14
130	130	34.60	-0.01	-70.79	2366.07
130	131	36.00	-0.01	-9.30	2413.19
131	131	36.00	-0.01	-9.49	2413.16
131	132	37.40	-0.01	60.46	2380.59
132	132	37.40	-0.01	60.27	2380.64
132	133	38.80	-0.01	111.58	2258.90
133	133	38.80	-0.01	111.45	2259.08
133	134	40.20	-0.01	180.51	2055.61
134	134	40.20	-0.01	180.45	2055.83
134	135	41.60	-0.01	242.50	1767.49
135	135	41.60	13.87	239.19	1767.77
135	136	43.00	13.36	287.97	1401.95
136	136	43.00	-0.01	291.32	1402.24
136	137	44.40	-0.01	269.96	996.76
137	137	44.40	0.00	270.72	996.65
137	138	45.80	0.00	274.65	614.12
138	138	45.80	0.00	275.55	613.57
138	139	47.20	0.00	230.34	267.23
139	139	47.20	0.00	230.67	267.06
139	140	48.60	0.00	218.50	-47.04
140	140	48.60	0.00	217.78	-47.04
140	141	50.00	0.00	210.90	-368.80
141	1141	50.00	0.00	-210.90	-368.80
141	142	51.40	0.00	-217.78	-47.05
142	142	51.40	0.00	-218.49	-47.06
142	143	52.80	0.00	-230.66	267.06
143	143	52.80	0.00	-230.35	267.24
143	144	54.20	0.00	-275.55	613.58
144	144	54.20	0.00	-274.68	614.13
144	145	55.60	0.00	-270.73	996.68
145	145	55.60	0.00	-269.99	996.79
145	146	57.00	0.00	-291.32	1402.32
146	146	57.00	13.36	-288.00	1402.02
146	147	58.40	13.87	-239.23	1767.86
147	147	58.40	0.00	-242.54	1767.54
147	148	59.80	0.00	-180.48	2055.89
148	148	59.80	0.00	-180.53	2055.69

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-111.46	2259.13
149	149	61.20	0.00	-111.60	2258.98
149	150	62.60	0.00	-60.27	2380.76
150	150	62.60	0.00	-60.46	2380.69
150	151	64.00	0.00	9.49	2413.24
151	151	64.00	0.00	9.30	2413.25
151	152	65.40	0.00	70.79	2366.12
152	152	65.40	0.00	70.61	2366.20
152	153	66.80	0.00	121.94	2230.08
153	153	66.80	0.00	121.84	2230.25
153	154	68.20	0.00	190.87	2012.01
154	154	68.20	0.00	190.83	2012.21
154	155	69.60	0.00	243.44	1712.02
155	155	69.60	14.62	239.57	1712.33
155	156	71.00	18.11	295.45	1337.71
156	156	71.00	0.00	300.52	1337.99
156	157	72.40	0.00	267.39	915.18
157	157	72.40	0.00	268.27	914.93
157	158	73.80	0.00	272.89	539.72
158	158	73.80	0.00	273.42	539.29
158	159	75.20	0.00	215.24	208.13
159	159	75.20	0.00	214.18	208.38
159	160	76.60	0.00	211.59	-92.86
160	160	76.60	0.00	210.90	-92.90
160	161	78.00	0.00	205.45	-404.63
161	1161	78.00	0.00	-202.42	-404.67
161	162	79.10	0.00	-206.45	-165.79
162	162	79.10	0.00	-207.00	-165.84
162	163	80.20	0.00	-222.48	70.76
163	163	80.20	0.00	-222.58	71.06
163	164	81.30	0.00	-239.89	327.25
164	164	81.30	0.00	-239.43	327.54
164	165	82.40	0.00	-267.93	616.56
165	165	82.40	0.00	-267.27	616.36
165	166	83.50	0.00	-247.48	903.66
166	166	83.50	0.00	-246.78	903.33
166	167	84.60	0.00	-253.84	1192.61
167	167	84.60	27.79	-244.87	1192.36
167	168	85.70	30.79	-208.41	1439.37
168	168	85.70	0.00	-217.80	1439.14
168	169	86.80	0.00	-170.03	1645.68
169	169	86.80	0.00	-169.82	1645.50
169	170	87.90	0.00	-122.28	1802.74
170	170	87.90	0.00	-122.01	1802.64
170	171	89.00	0.00	-74.28	1905.19
171	171	89.00	0.00	-74.04	1905.15
171	172	90.10	0.00	-26.21	1953.04
172	172	90.10	0.00	-25.94	1953.09
172	173	91.20	0.00	21.77	1947.19
173	173	91.20	0.00	22.07	1947.27
173	174	92.30	0.00	69.75	1893.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:

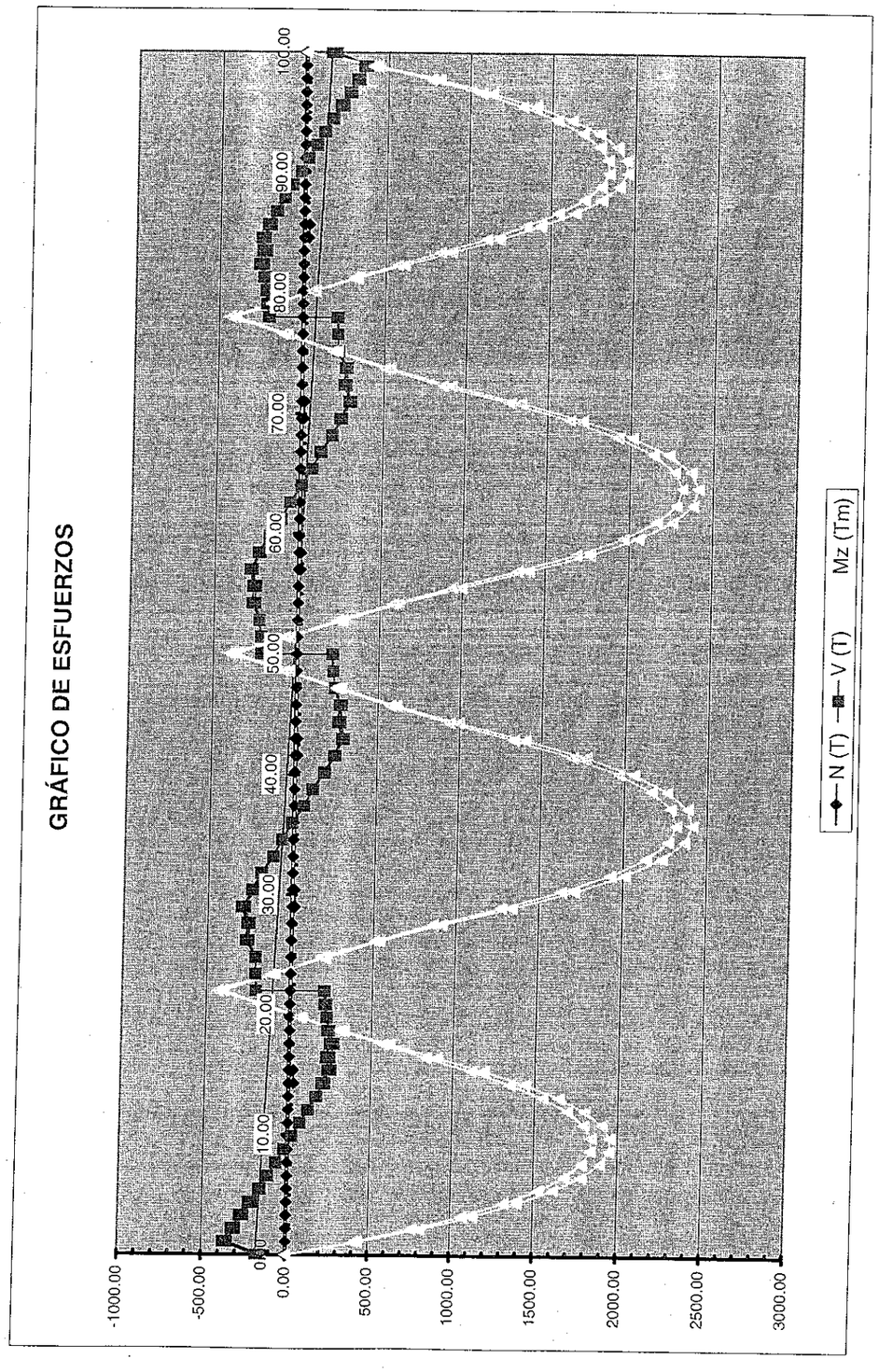
INFRECG.T0.MZ+

C. Totales dominante Gradinete Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	70.20	1893.95
174	175	93.40	0.00	117.89	1785.11
175	175	93.40	0.00	118.41	1785.32
175	176	94.50	0.00	166.22	1621.07
176	176	94.50	0.00	166.78	1621.40
176	177	95.60	0.00	226.26	1401.69
177	177	95.60	0.00	227.06	1402.06
177	178	96.70	0.00	274.85	1136.05
178	178	96.70	0.00	275.86	1136.46
178	179	97.80	0.00	323.52	814.62
179	179	97.80	0.00	324.69	815.07
179	180	98.90	0.00	372.46	436.59
180	180	98.90	0.00	373.84	437.05
180	181	100.00	0.00	178.85	0.97



CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-291.59	-0.97
1	2	1.10	0.00	-82.65	102.12
2	2	1.10	0.00	-83.09	102.10
2	3	2.20	0.00	-64.67	183.38
3	3	2.20	0.00	-65.10	183.37
3	4	3.30	0.00	-46.65	244.81
4	4	3.30	0.00	-47.09	244.80
4	5	4.40	0.00	-28.67	286.45
5	5	4.40	0.00	-29.11	286.44
5	6	5.50	0.00	-10.67	308.31
6	6	5.50	0.00	-11.13	308.27
6	7	6.60	0.00	7.31	310.43
7	7	6.60	0.00	6.78	310.37
7	8	7.70	0.00	25.21	292.78
8	8	7.70	0.00	24.70	292.75
8	9	8.80	0.00	43.48	255.43
9	9	8.80	0.00	42.79	255.38
9	10	9.90	0.00	61.38	198.13
10	10	9.90	0.00	60.73	198.11
10	11	11.00	0.00	79.17	121.14
11	11	11.00	0.00	78.47	121.11
11	12	12.10	0.00	96.94	24.63
12	12	12.10	0.00	96.23	24.58
12	13	13.20	0.00	114.74	-91.53
13	13	13.20	0.00	114.01	-91.57
13	14	14.30	0.00	132.48	-227.14
14	14	14.30	24.30	124.11	-227.18
14	15	15.40	35.50	153.66	-396.02
15	15	15.40	0.00	164.00	-396.04
15	16	16.50	0.00	246.42	-597.09
16	16	16.50	0.00	245.93	-596.97
16	17	17.60	0.00	282.80	-884.34
17	17	17.60	0.00	281.95	-884.06
17	18	18.70	0.00	343.93	-1228.53
18	18	18.70	-0.01	343.16	-1227.93
18	19	19.80	-0.01	409.12	-1639.72
19	19	19.80	0.00	408.46	-1638.94
19	20	20.90	0.00	492.28	-2142.35
20	20	20.90	0.00	491.91	-2142.32
20	21	22.00	0.00	565.48	-2722.32
21	1021	22.00	0.00	-594.80	-2722.19
21	22	23.40	0.00	-517.55	-1950.85
22	22	23.40	0.00	-517.99	-1950.63
22	23	24.80	0.00	-430.67	-1286.85
23	23	24.80	0.00	-428.78	-1286.82
23	24	26.20	0.00	-320.49	-776.12
24	24	26.20	0.00	-320.39	-777.00
24	25	27.60	0.00	-244.96	-382.24
25	25	27.60	-0.01	-245.81	-383.08
25	26	29.00	-0.01	-127.88	-160.94
26	26	29.00	23.90	-122.66	-161.03

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INFRECG.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.18	-94.91	-1.32
27	27	30.40	-0.01	-100.96	-1.37
27	28	31.80	-0.01	-67.87	112.79
28	28	31.80	-0.01	-68.81	112.73
28	29	33.20	-0.01	-45.37	192.66
29	29	33.20	-0.01	-46.24	192.66
29	30	34.60	-0.01	-20.89	239.29
30	30	34.60	-0.01	-21.73	239.19
30	31	36.00	-0.01	7.25	248.40
31	31	36.00	-0.01	6.42	248.38
31	32	37.40	-0.01	30.05	222.93
32	32	37.40	-0.01	29.12	222.90
32	33	38.80	-0.01	52.59	165.71
33	33	38.80	-0.01	51.66	165.70
33	34	40.20	-0.01	75.13	76.92
34	34	40.20	-0.01	74.17	76.95
34	35	41.60	-0.01	97.77	-43.36
35	35	41.60	9.87	94.45	-43.35
35	36	43.00	18.58	129.10	-205.85
36	36	43.00	-0.01	132.55	-205.76
36	37	44.40	-0.01	241.57	-442.19
37	37	44.40	0.00	240.63	-441.51
37	38	45.80	0.00	316.37	-824.50
38	38	45.80	0.00	315.62	-823.46
38	39	47.20	0.00	397.85	-1317.13
39	39	47.20	0.00	396.60	-1316.56
39	40	48.60	0.00	504.31	-1950.34
40	40	48.60	0.00	503.78	-1950.38
40	41	50.00	0.00	585.01	-2707.42
41	1041	50.00	0.00	-585.01	-2707.42
41	42	51.40	0.00	-503.79	-1950.37
42	42	51.40	0.00	-504.31	-1950.34
42	43	52.80	0.00	-396.60	-1316.55
43	43	52.80	0.00	-397.85	-1317.11
43	44	54.20	0.00	-315.62	-823.44
44	44	54.20	0.00	-316.37	-824.49
44	45	55.60	0.00	-240.61	-441.47
45	45	55.60	0.00	-241.57	-442.17
45	46	57.00	0.00	-132.54	-205.70
46	46	57.00	18.59	-129.11	-205.83
46	47	58.40	9.88	-94.46	-43.34
47	47	58.40	0.00	-97.77	-43.36
47	48	59.80	0.00	-74.17	76.96
48	48	59.80	0.00	-75.12	76.96
48	49	61.20	0.00	-51.65	165.69
49	49	61.20	0.00	-52.59	165.70
49	50	62.60	0.00	-29.12	222.91
50	50	62.60	0.00	-30.05	222.91
50	51	64.00	0.00	-6.42	248.39
51	51	64.00	0.00	-7.25	248.39
51	52	65.40	0.00	21.75	239.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	20.89	239.26
52	53	66.80	0.00	46.24	192.65
53	53	66.80	0.00	45.38	192.67
53	54	68.20	0.00	68.81	112.75
54	54	68.20	0.00	67.87	112.76
54	55	69.60	0.00	100.96	-1.37
55	55	69.60	19.19	94.92	-1.35
55	56	71.00	23.91	122.67	-161.04
56	56	71.00	0.00	127.88	-160.94
56	57	72.40	0.00	245.81	-383.08
57	57	72.40	0.00	244.99	-382.26
57	58	73.80	0.00	320.42	-777.02
58	58	73.80	0.00	320.49	-776.13
58	59	75.20	0.00	428.78	-1286.85
59	59	75.20	0.00	430.66	-1286.83
59	60	76.60	0.00	517.98	-1950.65
60	60	76.60	0.00	517.55	-1950.86
60	61	78.00	0.00	594.83	-2722.22
61	1061	78.00	0.00	-565.48	-2722.40
61	62	79.10	0.00	-491.91	-2142.37
62	62	79.10	0.00	-492.29	-2142.43
62	63	80.20	0.00	-408.48	-1638.97
63	63	80.20	0.00	-409.14	-1639.76
63	64	81.30	0.00	-343.17	-1227.96
64	64	81.30	0.00	-343.93	-1228.57
64	65	82.40	0.00	-281.95	-884.07
65	65	82.40	0.00	-282.80	-884.37
65	66	83.50	0.00	-245.93	-597.00
66	66	83.50	0.00	-246.43	-597.10
66	67	84.60	0.00	-164.01	-396.05
67	67	84.60	35.50	-153.65	-396.05
67	68	85.70	24.30	-124.09	-227.21
68	68	85.70	0.00	-132.48	-227.17
68	69	86.80	0.00	-114.00	-91.59
69	69	86.80	0.00	-114.75	-91.55
69	70	87.90	0.00	-96.24	24.54
70	70	87.90	0.00	-96.95	24.60
70	71	89.00	0.00	-78.48	121.07
71	71	89.00	0.00	-79.18	121.11
71	72	90.10	0.00	-60.74	198.07
72	72	90.10	0.00	-61.39	198.10
72	73	91.20	0.00	-42.80	255.33
73	73	91.20	0.00	-43.49	255.41
73	74	92.30	0.00	-24.71	292.72
74	74	92.30	0.00	-25.22	292.75
74	75	93.40	0.00	-6.79	310.36
75	75	93.40	0.00	-7.32	310.39
75	76	94.50	0.00	11.12	308.26
76	76	94.50	0.00	10.66	308.32
76	77	95.60	0.00	29.10	286.42
77	77	95.60	0.00	28.66	286.44

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INFRECG.T0.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	47.08	244.77
78	78	96.70	0.00	46.64	244.78
78	79	97.80	0.00	65.09	183.36
79	79	97.80	0.00	64.64	183.37
79	80	98.90	0.00	83.06	102.10
80	80	98.90	0.00	82.64	102.12
80	81	100.00	0.00	291.57	-0.97
101	101	0.00	0.00	-282.25	-1.09
101	102	1.10	0.00	-79.95	99.06
102	102	1.10	0.00	-80.32	99.31
102	103	2.20	0.00	-62.21	177.67
103	103	2.20	0.00	-62.48	177.91
103	104	3.30	0.00	-44.40	236.65
104	104	3.30	0.00	-44.52	236.87
104	105	4.40	0.00	-26.46	275.90
105	105	4.40	0.00	-26.51	276.06
105	106	5.50	0.00	-8.41	295.26
106	106	5.50	0.00	-8.32	295.42
106	107	6.60	0.00	9.79	294.61
107	107	6.60	0.00	9.94	294.76
107	108	7.70	0.00	28.01	273.87
108	108	7.70	0.00	28.23	274.00
108	109	8.80	0.00	46.31	233.02
109	109	8.80	0.00	46.54	233.11
109	110	9.90	0.00	64.63	171.92
110	110	9.90	0.00	64.93	171.98
110	111	11.00	0.00	83.02	90.65
111	111	11.00	0.00	83.40	90.69
111	112	12.10	0.00	101.48	-11.03
112	112	12.10	0.00	101.89	-11.01
112	113	13.20	0.00	119.95	-133.06
113	113	13.20	0.00	120.39	-133.10
113	114	14.30	0.00	138.53	-275.50
114	114	14.30	24.30	131.41	-275.57
114	115	15.40	35.50	160.89	-452.25
115	115	15.40	0.00	172.59	-452.36
115	116	16.50	0.00	245.25	-662.98
116	116	16.50	0.00	245.64	-663.13
116	117	17.60	0.00	280.63	-949.61
117	117	17.60	0.00	280.86	-949.65
117	118	18.70	0.00	354.45	-1301.69
118	118	18.70	0.00	354.89	-1301.29
118	119	19.80	0.00	435.31	-1734.01
119	119	19.80	0.00	436.39	-1733.70
119	120	20.90	0.00	537.71	-2280.44
120	120	20.90	0.00	539.21	-2280.37
120	121	22.00	0.00	607.68	-2906.01
121	1121	22.00	0.00	-634.46	-2906.00
121	122	23.40	0.00	-551.33	-2081.33
122	122	23.40	0.00	-549.37	-2081.47
122	123	24.80	0.00	-458.00	-1377.74

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-455.74	-1377.76
123	124	26.20	0.00	-332.64	-841.12
124	124	26.20	0.00	-332.05	-841.78
124	125	27.60	0.00	-251.25	-436.32
125	125	27.60	-0.01	-251.14	-436.84
125	126	29.00	-0.01	-134.10	-199.06
126	126	29.00	23.90	-127.10	-198.95
126	127	30.40	19.18	-100.59	-31.97
127	127	30.40	-0.01	-104.96	-31.89
127	128	31.80	-0.01	-72.22	88.00
128	128	31.80	-0.01	-71.45	88.07
128	129	33.20	-0.01	-48.45	172.05
129	129	33.20	-0.01	-47.75	172.09
129	130	34.60	-0.01	-23.00	221.57
130	130	34.60	-0.01	-22.28	221.52
130	131	36.00	-0.01	7.40	231.13
131	131	36.00	-0.01	8.13	231.15
131	132	37.40	-0.01	31.19	203.63
132	132	37.40	-0.01	31.91	203.63
132	133	38.80	-0.01	54.93	142.84
133	133	38.80	-0.01	55.70	142.81
133	134	40.20	-0.01	78.74	48.72
134	134	40.20	-0.01	79.50	48.67
134	135	41.60	-0.01	102.73	-78.85
135	135	41.60	9.87	101.15	-78.91
135	136	43.00	18.58	134.84	-250.35
136	136	43.00	-0.01	140.24	-250.42
136	137	44.40	-0.01	245.59	-501.36
137	137	44.40	0.00	245.89	-501.02
137	138	45.80	0.00	327.13	-894.80
138	138	45.80	0.00	327.42	-894.01
138	139	47.20	0.00	419.88	-1411.78
139	139	47.20	0.00	420.76	-1411.48
139	140	48.60	0.00	536.99	-2088.97
140	140	48.60	0.00	538.97	-2088.84
140	141	50.00	0.00	626.37	-2901.59
141	1141	50.00	0.00	-626.39	-2901.59
141	142	51.40	0.00	-538.97	-2088.81
142	142	51.40	0.00	-536.98	-2088.95
142	143	52.80	0.00	-420.75	-1411.44
143	143	52.80	0.00	-419.89	-1411.74
143	144	54.20	0.00	-327.40	-893.99
144	144	54.20	0.00	-327.14	-894.77
144	145	55.60	0.00	-245.90	-500.96
145	145	55.60	0.00	-245.59	-501.31
145	146	57.00	0.00	-140.24	-250.40
146	146	57.00	18.58	-134.85	-250.33
146	147	58.40	9.87	-101.16	-78.89
147	147	58.40	0.00	-102.73	-78.82
147	148	59.80	0.00	-79.50	48.65
148	148	59.80	0.00	-78.74	48.73

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-55.70	142.83
149	149	61.20	0.00	-54.93	142.83
149	150	62.60	0.00	-31.91	203.63
150	150	62.60	0.00	-31.19	203.63
150	151	64.00	0.00	-8.13	231.11
151	151	64.00	0.00	-7.40	231.10
151	152	65.40	0.00	22.28	221.49
152	152	65.40	0.00	23.00	221.55
152	153	66.80	0.00	47.74	172.06
153	153	66.80	0.00	48.45	172.03
153	154	68.20	0.00	71.45	88.01
154	154	68.20	0.00	72.22	87.96
154	155	69.60	0.00	104.96	-31.93
155	155	69.60	19.19	100.58	-32.00
155	156	71.00	23.91	127.10	-198.98
156	156	71.00	0.00	134.11	-199.10
156	157	72.40	0.00	251.15	-436.86
157	157	72.40	0.00	251.26	-436.32
157	158	73.80	0.00	332.06	-841.80
158	158	73.80	0.00	332.64	-841.14
158	159	75.20	0.00	455.77	-1377.76
159	159	75.20	0.00	457.98	-1377.76
159	160	76.60	0.00	549.37	-2081.49
160	160	76.60	0.00	551.33	-2081.39
160	161	78.00	0.00	634.48	-2906.05
161	1161	78.00	0.00	-607.68	-2906.08
161	162	79.10	0.00	-539.23	-2280.41
162	162	79.10	0.00	-537.71	-2280.52
162	163	80.20	0.00	-436.40	-1733.74
163	163	80.20	0.00	-435.31	-1734.05
163	164	81.30	0.00	-354.89	-1301.32
164	164	81.30	0.00	-354.45	-1301.72
164	165	82.40	0.00	-280.86	-949.68
165	165	82.40	0.00	-280.63	-949.63
165	166	83.50	0.00	-245.64	-663.18
166	166	83.50	0.00	-245.26	-663.00
166	167	84.60	0.00	-172.60	-452.38
167	167	84.60	35.50	-160.88	-452.29
167	168	85.70	24.30	-131.40	-275.59
168	168	85.70	0.00	-138.55	-275.54
168	169	86.80	0.00	-120.42	-133.12
169	169	86.80	0.00	-119.96	-133.09
169	170	87.90	0.00	-101.90	-11.04
170	170	87.90	0.00	-101.49	-11.05
170	171	89.00	0.00	-83.41	90.66
171	171	89.00	0.00	-83.03	90.63
171	172	90.10	0.00	-64.94	171.97
172	172	90.10	0.00	-64.62	171.91
172	173	91.20	0.00	-46.54	233.07
173	173	91.20	0.00	-46.33	232.98
173	174	92.30	0.00	-28.24	273.98

CÁLCULO TENSIONAL

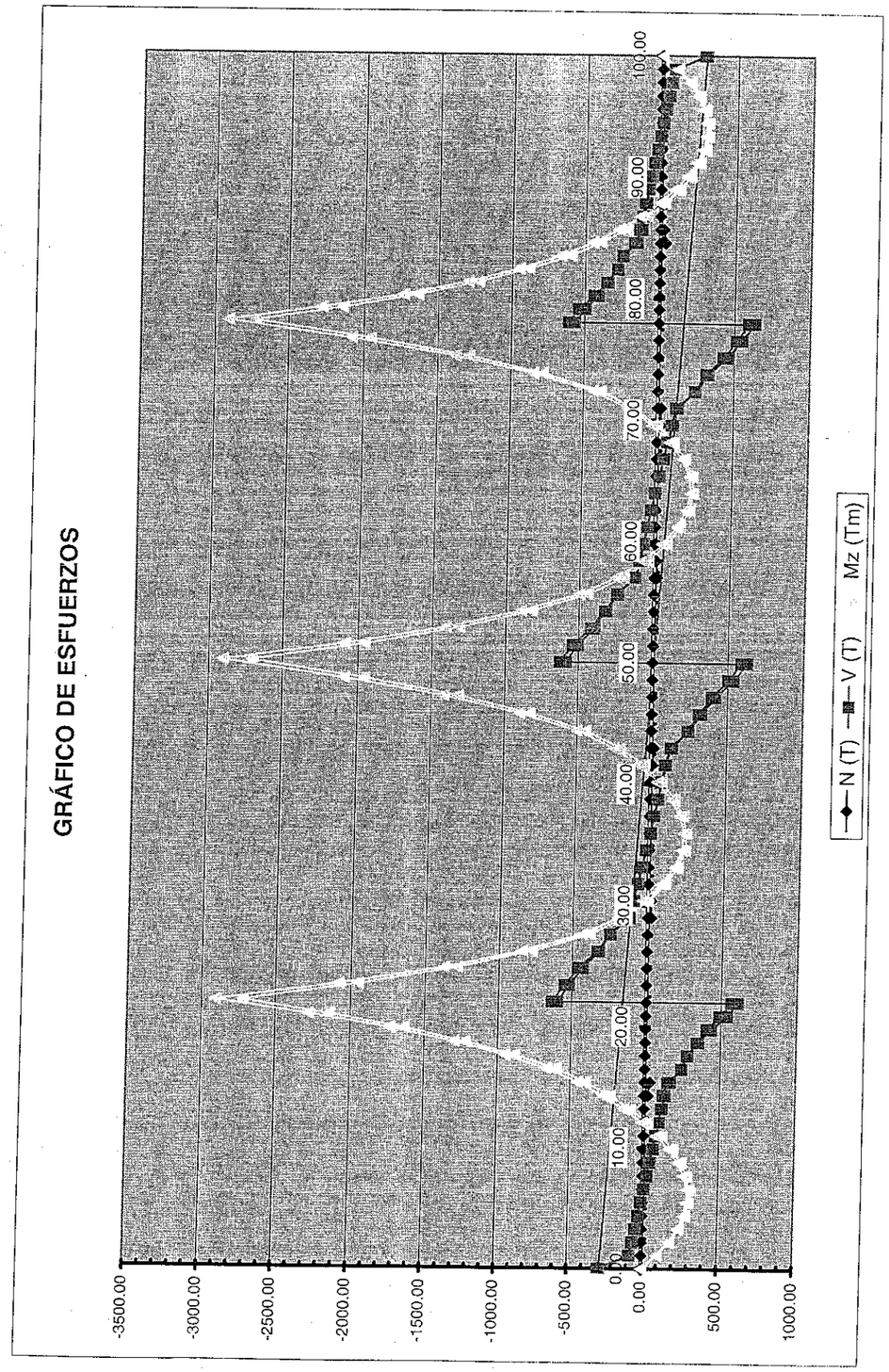
Hipótesis de cálculo:
INFRECG.T0.MZ-

C. Totales dominante Gradinete Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-28.02	273.86
174	175	93.40	0.00	-9.95	294.74
175	175	93.40	0.00	-9.80	294.60
175	176	94.50	0.00	8.31	295.42
176	176	94.50	0.00	8.39	295.26
176	177	95.60	0.00	26.48	276.06
177	177	95.60	0.00	26.45	275.87
177	178	96.70	0.00	44.52	236.83
178	178	96.70	0.00	44.37	236.65
178	179	97.80	0.00	62.46	177.90
179	179	97.80	0.00	62.20	177.66
179	180	98.90	0.00	80.31	99.31
180	180	98.90	0.00	79.94	99.06
180	181	100.00	0.00	282.23	-1.09



CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-151.68	-0.03
1	2	1.10	0.00	-230.88	270.22
2	2	1.10	0.00	-230.34	270.04
2	3	2.20	0.00	-201.74	507.70
3	3	2.20	0.00	-201.31	507.53
3	4	3.30	0.00	-172.71	713.21
4	4	3.30	0.00	-172.31	713.07
4	5	4.40	0.00	-143.72	886.88
5	5	4.40	0.00	-143.41	886.76
5	6	5.50	0.00	-114.81	1028.77
6	6	5.50	0.00	-114.53	1028.67
6	7	6.60	0.00	-85.94	1138.95
7	7	6.60	0.00	-85.70	1138.88
7	8	7.70	0.00	-57.11	1217.42
8	8	7.70	-0.01	-56.89	1217.36
8	9	8.80	-0.01	-28.29	1264.20
9	9	8.80	0.00	-28.08	1264.18
9	10	9.90	0.00	0.51	1279.33
10	10	9.90	0.00	0.72	1279.36
10	11	11.00	0.00	29.31	1262.82
11	11	11.00	0.00	29.52	1262.89
11	12	12.10	0.00	58.13	1214.66
12	12	12.10	0.00	58.38	1214.72
12	13	13.20	0.00	86.98	1134.77
13	13	13.20	0.00	87.26	1134.86
13	14	14.30	0.00	115.88	1023.14
14	14	14.30	12.56	112.23	1023.26
14	15	15.40	6.94	129.76	892.54
15	15	15.40	0.00	132.31	892.66
15	16	16.50	0.00	97.35	741.61
16	16	16.50	0.00	97.51	741.66
16	17	17.60	0.00	117.87	623.19
17	17	17.60	-0.01	118.06	623.24
17	18	18.70	-0.01	133.42	485.84
18	18	18.70	-0.01	133.61	485.88
18	19	19.80	-0.01	152.22	328.68
19	19	19.80	0.00	152.45	328.71
19	20	20.90	0.00	171.05	150.76
20	20	20.90	0.00	171.28	150.79
20	21	22.00	0.00	175.58	-49.67
21	1021	22.00	0.00	-216.89	-49.67
21	22	23.40	0.00	-211.46	265.87
22	22	23.40	0.00	-211.18	265.83
22	23	24.80	0.00	-187.49	544.90
23	23	24.80	0.00	-187.21	544.83
23	24	26.20	0.00	-167.79	793.49
24	24	26.20	0.00	-167.55	793.43
24	25	27.60	0.00	-141.63	1009.88
25	25	27.60	0.00	-141.43	1009.80
25	26	29.00	0.00	-167.86	1266.68
26	26	29.00	4.53	-166.27	1266.50

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PERM1.Tinf.MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.66	-132.09	1476.91
27	27	30.40	0.00	-132.74	1476.75
27	28	31.80	0.00	-105.87	1647.81
28	28	31.80	0.00	-105.61	1647.70
28	29	33.20	0.00	-69.20	1770.07
29	29	33.20	0.00	-69.00	1769.97
29	30	34.60	0.00	-32.60	1841.11
30	30	34.60	0.00	-32.40	1841.05
30	31	36.00	0.00	3.99	1860.96
31	31	36.00	0.00	4.15	1860.98
31	32	37.40	0.00	40.55	1829.66
32	32	37.40	0.00	40.74	1829.71
32	33	38.80	0.00	77.14	1747.20
33	33	38.80	0.00	77.39	1747.29
33	34	40.20	0.00	113.78	1613.50
34	34	40.20	0.00	114.02	1613.61
34	35	41.60	0.00	150.41	1428.51
35	35	41.60	6.46	149.15	1428.65
35	36	43.00	3.34	176.02	1201.06
36	36	43.00	0.00	177.27	1201.26
36	37	44.40	0.00	148.87	947.62
37	37	44.40	0.00	149.07	947.70
37	38	45.80	0.00	170.31	721.77
38	38	45.80	0.00	170.55	721.84
38	39	47.20	0.00	194.23	466.48
39	39	47.20	0.00	194.50	466.54
39	40	48.60	0.00	218.18	177.66
40	40	48.60	0.00	218.48	177.70
40	41	50.00	0.00	223.93	-147.70
41	1041	50.00	0.00	-223.93	-147.70
41	42	51.40	0.00	-218.48	177.70
42	42	51.40	0.00	-218.18	177.66
42	43	52.80	0.00	-194.50	466.53
43	43	52.80	0.00	-194.23	466.48
43	44	54.20	0.00	-170.55	721.82
44	44	54.20	0.00	-170.31	721.76
44	45	55.60	0.00	-149.07	947.72
45	45	55.60	0.00	-148.86	947.64
45	46	57.00	0.00	-177.26	1201.24
46	46	57.00	3.34	-176.03	1201.06
46	47	58.40	6.46	-149.16	1428.67
47	47	58.40	0.00	-150.42	1428.51
47	48	59.80	0.00	-114.03	1613.63
48	48	59.80	0.00	-113.77	1613.51
48	49	61.20	0.00	-77.38	1747.28
49	49	61.20	0.01	-77.14	1747.21
49	50	62.60	0.01	-40.74	1829.72
50	50	62.60	0.00	-40.54	1829.67
50	51	64.00	0.00	-4.14	1860.95
51	51	64.00	0.00	-3.98	1860.96
51	52	65.40	0.00	32.41	1841.05

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	32.60	1841.09
52	53	66.80	0.00	69.00	1769.97
53	53	66.80	0.00	69.21	1770.06
53	54	68.20	0.00	105.61	1647.70
54	54	68.20	0.00	105.87	1647.82
54	55	69.60	0.00	132.74	1476.74
55	55	69.60	3.66	132.10	1476.91
55	56	71.00	4.53	166.28	1266.52
56	56	71.00	0.00	167.87	1266.69
56	57	72.40	0.00	141.43	1009.81
57	57	72.40	0.00	141.63	1009.87
57	58	73.80	0.00	167.55	793.42
58	58	73.80	0.00	167.79	793.48
58	59	75.20	0.00	187.21	544.83
59	59	75.20	0.00	187.48	544.90
59	60	76.60	0.00	211.17	265.84
60	60	76.60	0.00	211.45	265.87
60	61	78.00	0.00	216.88	-49.65
61	1061	78.00	0.00	-175.58	-49.67
61	62	79.10	0.00	-171.28	150.78
62	62	79.10	0.00	-171.04	150.77
62	63	80.20	0.00	-152.45	328.69
63	63	80.20	0.00	-152.23	328.67
63	64	81.30	0.00	-133.61	485.88
64	64	81.30	0.00	-133.43	485.83
64	65	82.40	0.00	-118.07	623.24
65	65	82.40	0.00	-117.87	623.20
65	66	83.50	0.00	-97.51	741.65
66	66	83.50	0.01	-97.35	741.61
66	67	84.60	0.01	-132.31	892.66
67	67	84.60	6.95	-129.76	892.54
67	68	85.70	12.57	-112.23	1023.25
68	68	85.70	0.01	-115.88	1023.14
68	69	86.80	0.01	-87.26	1134.86
69	69	86.80	0.01	-86.98	1134.76
69	70	87.90	0.01	-58.38	1214.72
70	70	87.90	0.00	-58.14	1214.65
70	71	89.00	0.00	-29.54	1262.87
71	71	89.00	0.00	-29.33	1262.82
71	72	90.10	0.00	-0.73	1279.37
72	72	90.10	0.02	-0.52	1279.33
72	73	91.20	0.02	28.07	1264.17
73	73	91.20	0.00	28.27	1264.19
73	74	92.30	0.00	56.87	1217.36
74	74	92.30	0.00	57.10	1217.40
74	75	93.40	0.00	85.69	1138.87
75	75	93.40	0.00	85.93	1138.95
75	76	94.50	0.00	114.52	1028.66
76	76	94.50	0.01	114.81	1028.77
76	77	95.60	0.01	143.41	886.76
77	77	95.60	0.00	143.71	886.90

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	172.30	713.07
78	78	96.70	0.00	172.70	713.23
78	79	97.80	0.00	201.31	507.52
79	79	97.80	0.00	201.74	507.69
79	80	98.90	0.00	230.34	270.03
80	80	98.90	0.00	230.87	270.22
80	81	100.00	0.00	151.67	-0.03
101	101	0.00	0.00	-190.55	0.09
101	102	1.10	0.00	-215.68	252.79
102	102	1.10	0.00	-216.19	252.98
102	103	2.20	0.00	-189.21	475.96
103	103	2.20	0.00	-189.66	476.13
103	104	3.30	0.00	-162.69	669.90
104	104	3.30	0.00	-163.03	670.06
104	105	4.40	0.00	-136.09	834.59
105	105	4.40	0.00	-136.41	834.70
105	106	5.50	0.00	-109.44	969.89
106	106	5.50	0.00	-109.70	970.00
106	107	6.60	0.00	-82.74	1075.86
107	107	6.60	0.00	-82.96	1075.92
107	108	7.70	0.00	-56.00	1152.33
108	108	7.70	-0.01	-56.21	1152.38
108	109	8.80	-0.01	-29.24	1199.36
109	109	8.80	0.00	-29.42	1199.37
109	110	9.90	0.00	-2.46	1216.91
110	110	9.90	0.00	-2.67	1216.90
110	111	11.00	0.00	24.29	1205.01
111	111	11.00	0.00	24.09	1204.95
111	112	12.10	0.00	51.06	1163.60
112	112	12.10	0.00	50.82	1163.52
112	113	13.20	0.00	77.79	1092.78
113	113	13.20	0.00	77.53	1092.70
113	114	14.30	0.00	104.50	992.59
114	114	14.30	12.57	100.27	992.49
114	115	15.40	6.95	116.16	875.79
115	115	15.40	0.00	117.99	875.66
115	116	16.50	0.00	90.98	741.48
116	116	16.50	0.00	90.83	741.42
116	117	17.60	0.00	110.55	630.67
117	117	17.60	-0.01	110.37	630.61
117	118	18.70	-0.01	125.08	502.02
118	118	18.70	-0.01	124.88	501.97
118	119	19.80	-0.01	142.84	354.73
119	119	19.80	0.00	142.64	354.70
119	120	20.90	0.00	160.59	187.92
120	120	20.90	0.00	160.35	187.91
120	121	22.00	0.00	164.01	-0.18
121	1121	22.00	0.00	-205.56	-0.18
121	122	23.40	0.00	-200.94	300.06
122	122	23.40	0.00	-201.22	300.10
122	123	24.80	0.00	-178.37	565.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-178.63	565.90
123	124	26.20	0.00	-160.03	803.11
124	124	26.20	0.00	-160.25	803.18
124	125	27.60	0.00	-135.15	1009.97
125	125	27.60	0.00	-135.34	1010.03
125	126	29.00	0.00	-154.69	1247.39
126	126	29.00	4.53	-153.89	1247.58
126	127	30.40	3.66	-121.78	1442.09
127	127	30.40	0.00	-123.09	1442.25
127	128	31.80	0.00	-98.27	1601.25
128	128	31.80	0.00	-98.53	1601.37
128	129	33.20	0.00	-64.22	1715.30
129	129	33.20	0.00	-64.43	1715.39
129	130	34.60	0.00	-30.09	1781.53
130	130	34.60	0.00	-30.27	1781.59
130	131	36.00	0.00	4.06	1799.94
131	131	36.00	0.00	3.87	1799.95
131	132	37.40	0.00	38.21	1770.48
132	132	37.40	0.00	38.02	1770.44
132	133	38.80	0.00	72.36	1693.17
133	133	38.80	0.00	72.15	1693.09
133	134	40.20	0.00	106.47	1568.05
134	134	40.20	0.00	106.20	1567.94
134	135	41.60	0.00	140.53	1395.22
135	135	41.60	6.46	138.58	1395.06
135	136	43.00	3.34	163.37	1183.72
136	136	43.00	0.00	163.76	1183.53
136	137	44.40	0.00	142.64	948.71
137	137	44.40	0.00	142.44	948.63
137	138	45.80	0.00	162.86	732.53
138	138	45.80	0.00	162.64	732.47
138	139	47.20	0.00	185.48	488.76
139	139	47.20	0.00	185.21	488.71
139	140	48.60	0.00	208.08	213.41
140	140	48.60	0.00	207.79	213.38
140	141	50.00	0.00	212.41	-96.47
141	1141	50.00	0.00	-212.40	-96.47
141	142	51.40	0.00	-207.78	213.37
142	142	51.40	0.00	-208.08	213.42
142	143	52.80	0.00	-185.21	488.71
143	143	52.80	0.00	-185.48	488.75
143	144	54.20	0.00	-162.63	732.42
144	144	54.20	0.00	-162.87	732.50
144	145	55.60	0.00	-142.45	948.62
145	145	55.60	0.00	-142.64	948.70
145	146	57.00	0.00	-163.76	1183.53
146	146	57.00	3.34	-163.38	1183.72
146	147	58.40	6.46	-138.59	1395.05
147	147	58.40	0.00	-140.53	1395.22
147	148	59.80	0.00	-106.20	1567.93
148	148	59.80	0.00	-106.47	1568.06

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Programa DINTEL PACADAR S.A.
PERM1.Tinf.MZ+
05/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:

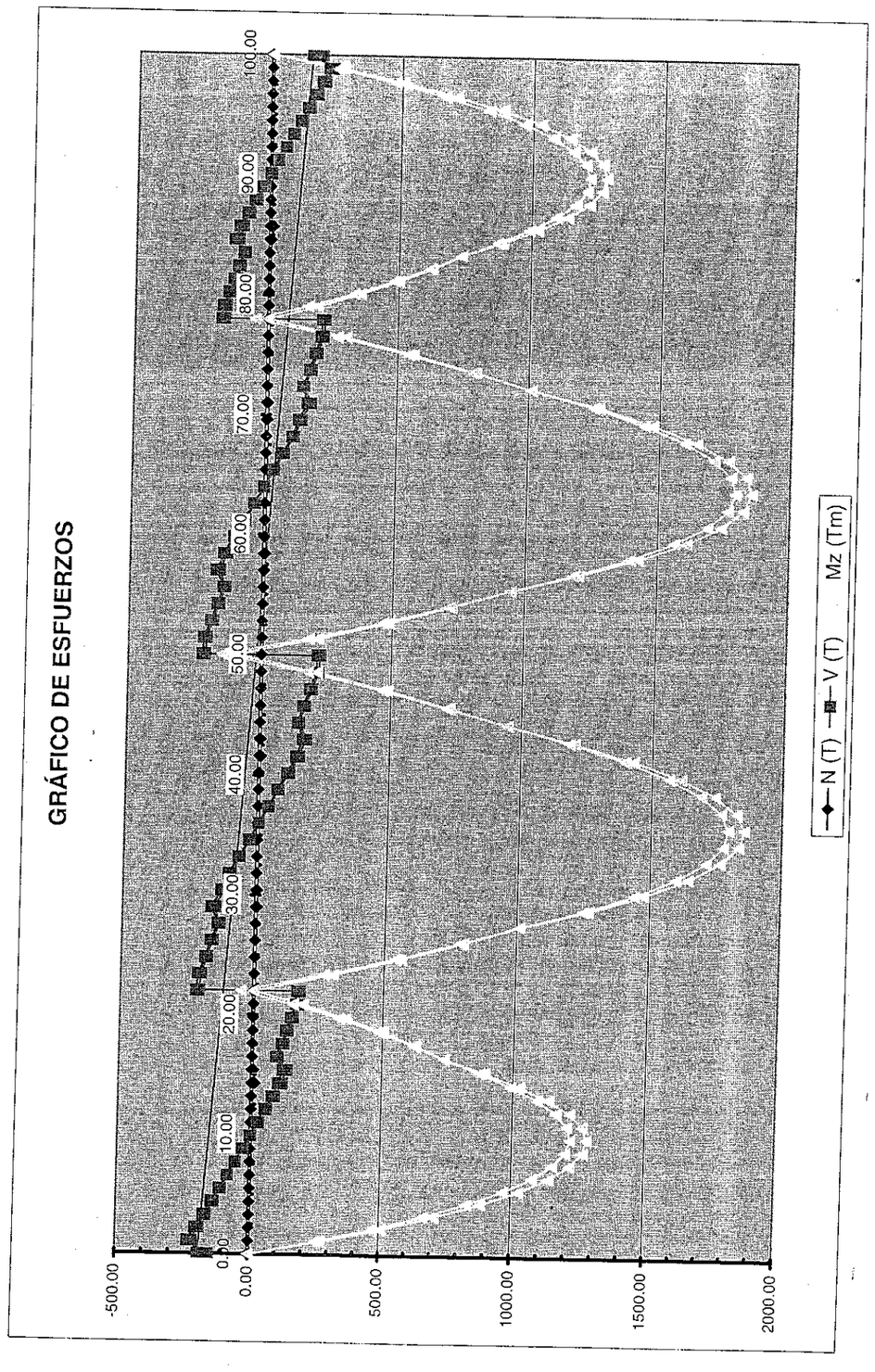
PERM1.Tinf.MZ+

C. Permanentes sin gradiente Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-72.15	1693.07
149	149	61.20	0.00	-72.36	1693.15
149	150	62.60	0.00	-38.02	1770.43
150	150	62.60	0.00	-38.21	1770.49
150	151	64.00	0.00	-3.87	1799.95
151	151	64.00	0.00	-4.06	1799.94
151	152	65.40	0.00	30.27	1781.59
152	152	65.40	0.00	30.09	1781.54
152	153	66.80	0.00	64.42	1715.39
153	153	66.80	0.00	64.22	1715.31
153	154	68.20	0.00	98.53	1601.37
154	154	68.20	0.00	98.27	1601.26
154	155	69.60	0.00	123.09	1442.25
155	155	69.60	3.66	121.78	1442.09
155	156	71.00	4.53	153.89	1247.60
156	156	71.00	0.00	154.69	1247.42
156	157	72.40	0.00	135.35	1010.05
157	157	72.40	0.00	135.16	1009.98
157	158	73.80	0.00	160.26	803.18
158	158	73.80	0.01	160.03	803.10
158	159	75.20	0.01	178.63	565.89
159	159	75.20	0.00	178.36	565.84
159	160	76.60	0.00	201.22	300.13
160	160	76.60	0.00	200.94	300.07
160	161	78.00	0.00	205.56	-0.17
161	1161	78.00	0.00	-164.02	-0.17
161	162	79.10	0.00	-160.37	187.91
162	162	79.10	0.00	-160.57	187.92
162	163	80.20	0.00	-142.62	354.70
163	163	80.20	0.00	-142.83	354.74
163	164	81.30	0.00	-124.87	501.97
164	164	81.30	0.00	-125.08	502.01
164	165	82.40	0.00	-110.37	630.62
165	165	82.40	0.00	-110.54	630.67
165	166	83.50	0.00	-90.82	741.41
166	166	83.50	0.01	-90.99	741.45
166	167	84.60	0.01	-118.00	875.68
167	167	84.60	6.95	-116.14	875.80
167	168	85.70	12.57	-100.26	992.45
168	168	85.70	0.00	-104.51	992.56
168	169	86.80	0.00	-77.54	1092.69
169	169	86.80	0.00	-77.80	1092.78
169	170	87.90	0.00	-50.83	1163.53
170	170	87.90	0.00	-51.06	1163.60
170	171	89.00	0.00	-24.11	1204.96
171	171	89.00	0.00	-24.32	1205.01
171	172	90.10	0.00	2.66	1216.90
172	172	90.10	0.00	2.47	1216.90
172	173	91.20	0.00	29.42	1199.37
173	173	91.20	0.00	29.21	1199.36
173	174	92.30	0.00	56.20	1152.38



CÁLCULO TENSIONAL

Hipótesis de cálculo:

PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-207.36	-0.09
1	2	1.10	0.00	-129.45	151.71
2	2	1.10	0.00	-129.23	151.64
2	3	2.20	0.00	-112.17	284.43
3	3	2.20	0.00	-112.01	284.36
3	4	3.30	0.00	-94.95	398.17
4	4	3.30	0.00	-94.79	398.11
4	5	4.40	0.00	-77.75	493.01
5	5	4.40	0.00	-77.63	492.96
5	6	5.50	0.00	-60.57	568.97
6	6	5.50	0.00	-60.46	568.93
6	7	6.60	0.00	-43.42	626.08
7	7	6.60	0.00	-43.32	626.05
7	8	7.70	0.00	-26.28	664.32
8	8	7.70	-0.01	-26.19	664.29
8	9	8.80	-0.01	-9.14	683.72
9	9	8.80	0.00	-9.05	683.70
9	10	9.90	0.00	7.99	684.27
10	10	9.90	0.00	8.08	684.30
10	11	11.00	0.00	25.12	666.02
11	11	11.00	0.00	25.21	666.04
11	12	12.10	0.00	42.26	628.91
12	12	12.10	0.00	42.37	628.93
12	13	13.20	0.00	59.43	572.95
13	13	13.20	0.00	59.54	572.99
13	14	14.30	0.00	76.60	498.11
14	14	14.30	-0.30	76.81	498.17
14	15	15.40	7.36	104.91	391.29
15	15	15.40	0.00	107.38	391.33
15	16	16.50	0.00	187.97	253.64
16	16	16.50	0.00	188.38	253.77
16	17	17.60	0.00	213.68	32.62
17	17	17.60	-0.01	214.13	32.75
17	18	18.70	-0.01	244.40	-220.32
18	18	18.70	0.00	244.89	-220.22
18	19	19.80	0.00	271.93	-504.46
19	19	19.80	0.00	272.48	-504.39
19	20	20.90	0.00	299.52	-819.01
20	20	20.90	0.00	300.10	-818.97
20	21	22.00	0.00	327.06	-1163.90
21	1021	22.00	0.00	-346.00	-1163.92
21	22	23.40	0.00	-311.68	-703.54
22	22	23.40	0.00	-310.98	-703.63
22	23	24.80	0.00	-276.56	-292.36
23	23	24.80	0.00	-275.88	-292.52
23	24	26.20	0.00	-237.21	66.46
24	24	26.20	0.00	-236.64	66.29
24	25	27.60	0.00	-204.44	375.06
25	25	27.60	0.00	-203.93	374.87
25	26	29.00	0.00	-119.42	560.86
26	26	29.00	5.58	-117.85	560.79

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	4.40	-93.91	710.82
27	27	30.40	0.00	-94.89	710.76
27	28	31.80	0.00	-63.68	817.71
28	28	31.80	0.00	-63.58	817.67
28	29	33.20	0.00	-41.86	891.47
29	29	33.20	0.00	-41.79	891.42
29	30	34.60	0.00	-20.09	934.75
30	30	34.60	0.00	-20.00	934.73
30	31	36.00	0.00	1.69	947.56
31	31	36.00	0.00	1.75	947.56
31	32	37.40	0.00	23.45	929.89
32	32	37.40	0.00	23.53	929.92
32	33	38.80	0.00	45.23	881.77
33	33	38.80	0.00	45.34	881.82
33	34	40.20	0.00	67.05	803.16
34	34	40.20	0.00	67.13	803.20
34	35	41.60	0.00	88.82	694.03
35	35	41.60	-0.13	88.99	694.09
35	36	43.00	5.05	120.22	545.02
36	36	43.00	0.00	121.70	545.11
36	37	44.40	0.00	208.23	339.42
37	37	44.40	0.00	208.73	339.61
37	38	45.80	0.00	245.57	24.04
38	38	45.80	0.00	246.17	24.21
38	39	47.20	0.00	280.59	-344.54
39	39	47.20	0.00	281.26	-344.40
39	40	48.60	0.00	315.67	-762.24
40	40	48.60	0.00	316.41	-762.15
40	41	50.00	0.00	350.75	-1229.17
41	1041	50.00	0.00	-350.75	-1229.17
41	42	51.40	0.00	-316.41	-762.15
42	42	51.40	0.00	-315.67	-762.24
42	43	52.80	0.00	-281.26	-344.41
43	43	52.80	0.00	-280.59	-344.54
43	44	54.20	0.00	-246.17	24.20
44	44	54.20	0.00	-245.57	24.02
44	45	55.60	0.00	-208.73	339.64
45	45	55.60	0.00	-208.21	339.45
45	46	57.00	0.00	-121.69	545.09
46	46	57.00	5.05	-120.23	545.02
46	47	58.40	-0.14	-89.00	694.09
47	47	58.40	0.00	-88.82	694.03
47	48	59.80	0.00	-67.13	803.21
48	48	59.80	0.00	-67.04	803.17
48	49	61.20	0.00	-45.33	881.81
49	49	61.20	0.01	-45.23	881.79
49	50	62.60	0.01	-23.53	929.93
50	50	62.60	0.00	-23.45	929.90
50	51	64.00	0.00	-1.75	947.54
51	51	64.00	0.00	-1.68	947.55
51	52	65.40	0.00	20.01	934.72

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	20.09	934.74
52	53	66.80	0.00	41.79	891.42
53	53	66.80	0.00	41.87	891.46
53	54	68.20	0.00	63.58	817.66
54	54	68.20	0.00	63.68	817.71
54	55	69.60	0.00	94.89	710.73
55	55	69.60	4.40	93.90	710.80
55	56	71.00	5.57	117.85	560.79
56	56	71.00	0.00	119.43	560.86
56	57	72.40	0.00	203.93	374.88
57	57	72.40	0.00	204.44	375.05
57	58	73.80	0.00	236.64	66.28
58	58	73.80	0.00	237.22	66.44
58	59	75.20	0.00	275.89	-292.53
59	59	75.20	0.00	276.55	-292.36
59	60	76.60	0.00	310.97	-703.62
60	60	76.60	0.00	311.67	-703.54
60	61	78.00	0.00	345.99	-1163.91
61	1061	78.00	0.00	-327.06	-1163.91
61	62	79.10	0.00	-300.10	-818.97
62	62	79.10	0.00	-299.53	-819.02
62	63	80.20	0.00	-272.49	-504.41
63	63	80.20	0.00	-271.95	-504.48
63	64	81.30	0.00	-244.90	-220.22
64	64	81.30	0.00	-244.42	-220.32
64	65	82.40	0.00	-214.14	32.75
65	65	82.40	0.00	-213.68	32.63
65	66	83.50	0.00	-188.38	253.76
66	66	83.50	0.01	-187.98	253.65
66	67	84.60	0.01	-107.38	391.34
67	67	84.60	7.37	-104.92	391.29
67	68	85.70	-0.30	-76.81	498.16
68	68	85.70	0.01	-76.60	498.11
68	69	86.80	0.01	-59.54	572.99
69	69	86.80	0.01	-59.43	572.95
69	70	87.90	0.01	-42.37	628.94
70	70	87.90	0.00	-42.27	628.92
70	71	89.00	0.00	-25.23	666.03
71	71	89.00	0.00	-25.14	666.01
71	72	90.10	0.00	-8.09	684.30
72	72	90.10	0.02	-8.00	684.28
72	73	91.20	0.02	9.04	683.69
73	73	91.20	0.00	9.12	683.70
73	74	92.30	0.00	26.17	664.28
74	74	92.30	0.00	26.27	664.30
74	75	93.40	0.00	43.31	626.04
75	75	93.40	0.00	43.41	626.08
75	76	94.50	0.00	60.45	568.92
76	76	94.50	0.01	60.58	568.96
76	77	95.60	0.01	77.63	492.97
77	77	95.60	0.00	77.74	493.02

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	94.78	398.12
78	78	96.70	0.00	94.95	398.18
78	79	97.80	0.00	112.00	284.35
79	79	97.80	0.00	112.18	284.42
79	80	98.90	0.00	129.24	151.63
80	80	98.90	0.00	129.44	151.71
80	81	100.00	0.00	207.35	-0.09
101	101	0.00	0.00	-144.97	0.03
101	102	1.10	0.00	-123.39	144.75
102	102	1.10	0.00	-123.59	144.83
102	103	2.20	0.00	-107.17	271.76
103	103	2.20	0.00	-107.36	271.83
103	104	3.30	0.00	-90.96	380.89
104	104	3.30	0.00	-91.09	380.95
104	105	4.40	0.00	-74.70	472.17
105	105	4.40	0.00	-74.84	472.20
105	106	5.50	0.00	-58.43	545.49
106	106	5.50	0.00	-58.54	545.53
106	107	6.60	0.00	-42.15	600.91
107	107	6.60	0.00	-42.23	600.93
107	108	7.70	0.00	-25.83	638.35
108	108	7.70	-0.01	-25.92	638.37
108	109	8.80	-0.01	-9.51	657.84
109	109	8.80	0.00	-9.58	657.84
109	110	9.90	0.00	6.81	659.38
110	110	9.90	0.00	6.73	659.38
110	111	11.00	0.00	23.12	642.96
111	111	11.00	0.00	23.05	642.92
111	112	12.10	0.00	39.44	608.55
112	112	12.10	0.00	39.35	608.51
112	113	13.20	0.00	55.76	556.21
113	113	13.20	0.00	55.65	556.18
113	114	14.30	0.00	72.05	485.94
114	114	14.30	-0.30	72.03	485.91
114	115	15.40	7.37	99.48	384.61
115	115	15.40	0.00	101.67	384.55
115	116	16.50	0.00	172.03	253.30
116	116	16.50	0.00	171.64	253.17
116	117	17.60	0.00	195.32	51.34
117	117	17.60	-0.01	194.86	51.21
117	118	18.70	-0.01	223.50	-179.78
118	118	18.70	-0.01	223.00	-179.88
118	119	19.80	-0.01	248.41	-439.16
119	119	19.80	0.00	247.88	-439.24
119	120	20.90	0.00	273.30	-725.89
120	120	20.90	0.00	272.71	-725.92
120	121	22.00	0.00	298.07	-1039.87
121	1121	22.00	0.00	-317.61	-1039.87
121	122	23.40	0.00	-285.34	-617.83
122	122	23.40	0.00	-286.05	-617.74
122	123	24.80	0.00	-253.72	-239.89

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-254.37	-239.72
123	124	26.20	0.00	-217.76	90.57
124	124	26.20	0.00	-218.34	90.73
124	125	27.60	0.00	-188.19	375.32
125	125	27.60	0.00	-188.68	375.48
125	126	29.00	0.00	-114.17	553.16
126	126	29.00	5.58	-112.92	553.23
126	127	30.40	4.40	-89.80	696.92
127	127	30.40	0.00	-91.04	696.98
127	128	31.80	0.00	-60.65	799.13
128	128	31.80	0.00	-60.76	799.18
128	129	33.20	0.00	-39.89	869.62
129	129	33.20	0.00	-39.97	869.65
129	130	34.60	0.00	-19.09	910.97
130	130	34.60	0.00	-19.15	910.99
130	131	36.00	0.00	1.72	923.21
131	131	36.00	0.00	1.64	923.22
131	132	37.40	0.00	22.53	906.29
132	132	37.40	0.00	22.45	906.28
132	133	38.80	0.00	43.33	860.24
133	133	38.80	0.00	43.25	860.20
133	134	40.20	0.00	64.13	785.04
134	134	40.20	0.00	64.01	784.99
134	135	41.60	0.00	84.89	680.75
135	135	41.60	-0.13	84.78	680.69
135	136	43.00	5.05	115.17	538.11
136	136	43.00	0.00	116.30	538.03
136	137	44.40	0.00	192.64	342.10
137	137	44.40	0.00	192.13	341.91
137	138	45.80	0.00	226.91	50.98
138	138	45.80	0.00	226.32	50.82
138	139	47.20	0.00	258.66	-288.71
139	139	47.20	0.00	257.99	-288.85
139	140	48.60	0.00	290.35	-672.67
140	140	48.60	0.00	289.61	-672.74
140	141	50.00	0.00	321.89	-1100.79
141	1141	50.00	0.00	-321.88	-1100.79
141	142	51.40	0.00	-289.61	-672.75
142	142	51.40	0.00	-290.35	-672.65
142	143	52.80	0.00	-258.00	-288.84
143	143	52.80	0.00	-258.67	-288.71
143	144	54.20	0.00	-226.31	50.77
144	144	54.20	0.00	-226.92	50.95
144	145	55.60	0.00	-192.14	341.91
145	145	55.60	0.00	-192.64	342.10
145	146	57.00	0.00	-116.30	538.03
146	146	57.00	5.05	-115.18	538.10
146	147	58.40	-0.13	-84.79	680.67
147	147	58.40	0.00	-84.89	680.74
147	148	59.80	0.00	-64.01	784.98
148	148	59.80	0.00	-64.13	785.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-43.25	860.18
149	149	61.20	0.00	-43.33	860.21
149	150	62.60	0.00	-22.45	906.26
150	150	62.60	0.00	-22.53	906.30
150	151	64.00	0.00	-1.64	923.21
151	151	64.00	0.00	-1.72	923.20
151	152	65.40	0.00	19.15	911.00
152	152	65.40	0.00	19.09	910.98
152	153	66.80	0.00	39.96	869.65
153	153	66.80	0.00	39.89	869.61
153	154	68.20	0.00	60.76	799.17
154	154	68.20	0.00	60.65	799.13
154	155	69.60	0.00	91.04	696.97
155	155	69.60	4.40	89.79	696.91
155	156	71.00	5.57	112.91	553.25
156	156	71.00	0.00	114.16	553.18
156	157	72.40	0.00	188.70	375.51
157	157	72.40	0.00	188.20	375.32
157	158	73.80	0.00	218.35	90.73
158	158	73.80	0.01	217.78	90.55
158	159	75.20	0.01	254.37	-239.75
159	159	75.20	0.00	253.71	-239.88
159	160	76.60	0.00	286.06	-617.71
160	160	76.60	0.00	285.34	-617.83
160	161	78.00	0.00	317.61	-1039.88
161	1161	78.00	0.00	-298.08	-1039.88
161	162	79.10	0.00	-272.74	-725.94
162	162	79.10	0.00	-273.29	-725.90
162	163	80.20	0.00	-247.88	-439.25
163	163	80.20	0.00	-248.40	-439.16
163	164	81.30	0.00	-222.99	-179.89
164	164	81.30	0.00	-223.51	-179.78
164	165	82.40	0.00	-194.87	51.21
165	165	82.40	0.00	-195.32	51.34
165	166	83.50	0.00	-171.63	253.15
166	166	83.50	0.01	-172.04	253.26
166	167	84.60	0.01	-101.68	384.57
167	167	84.60	7.37	-99.47	384.62
167	168	85.70	-0.30	-72.03	485.87
168	168	85.70	0.00	-72.06	485.92
168	169	86.80	0.00	-55.66	556.17
169	169	86.80	0.00	-55.77	556.21
169	170	87.90	0.00	-39.36	608.52
170	170	87.90	0.00	-39.45	608.55
170	171	89.00	0.00	-23.07	642.94
171	171	89.00	0.00	-23.16	642.96
171	172	90.10	0.00	-6.74	659.39
172	172	90.10	0.00	-6.81	659.37
172	173	91.20	0.00	9.58	657.84
173	173	91.20	0.00	9.50	657.84
173	174	92.30	0.00	25.91	638.36

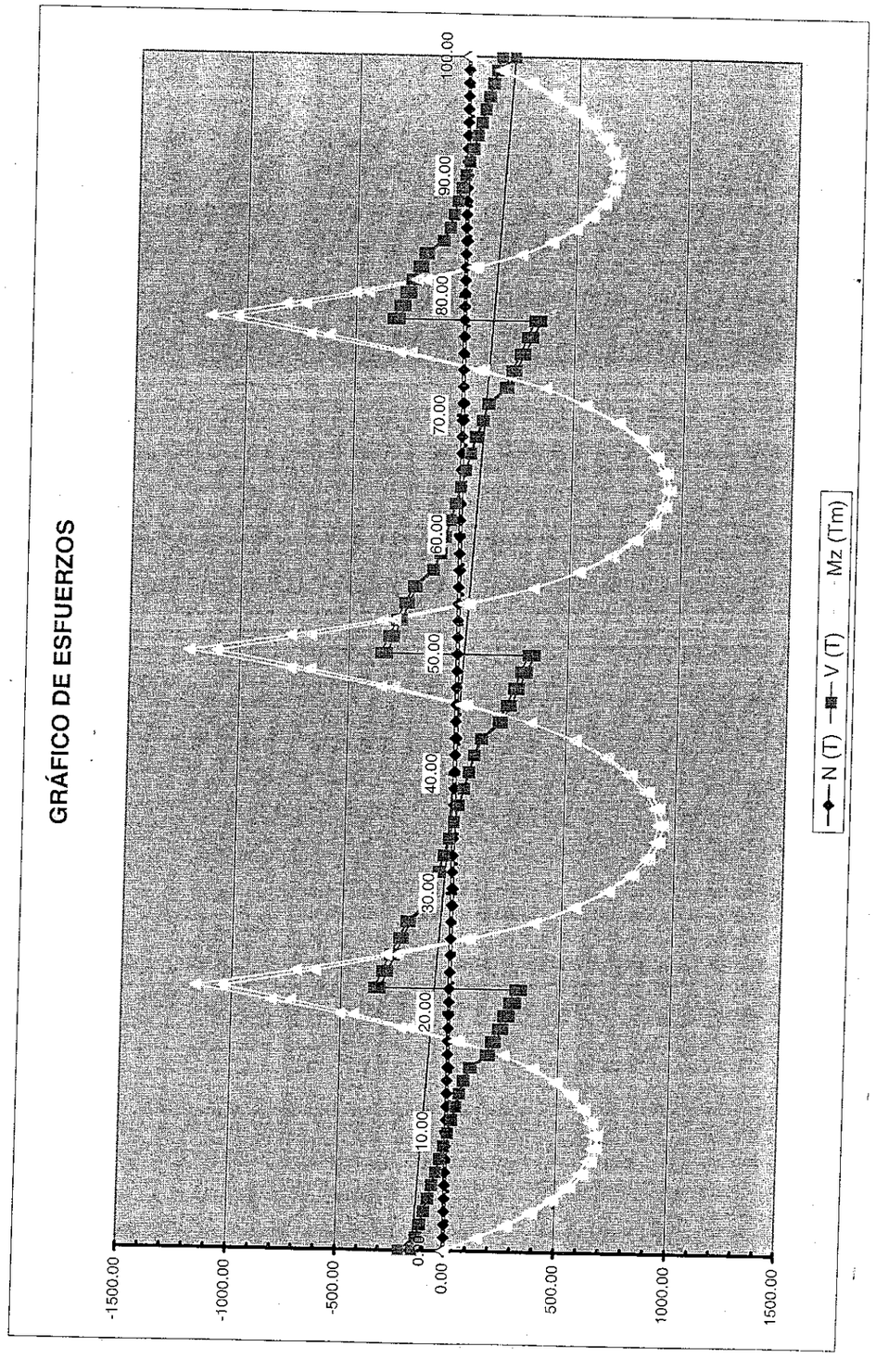
CÁLCULO TENSIONAL

Hipótesis de cálculo:
PERM1.Tinf.MZ-

C. Permanentes sin gradiente Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	25.82	638.35
174	175	93.40	0.00	42.22	600.93
175	175	93.40	0.00	42.13	600.91
175	176	94.50	0.00	58.52	545.52
176	176	94.50	0.00	58.43	545.47
176	177	95.60	0.00	74.83	472.21
177	177	95.60	0.00	74.69	472.16
177	178	96.70	0.00	91.09	380.96
178	178	96.70	0.00	90.95	380.90
178	179	97.80	0.00	107.35	271.82
179	179	97.80	0.00	107.18	271.75
179	180	98.90	0.00	123.60	144.82
180	180	98.90	0.00	123.38	144.76
180	181	100.00	0.00	144.96	0.03



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-177.48	1.38
1	2	1.10	0.00	-420.66	489.42
2	2	1.10	0.00	-421.43	489.75
2	3	2.20	0.00	-371.22	920.77
3	3	2.20	0.00	-371.88	921.05
3	4	3.30	0.00	-321.79	1294.61
4	4	3.30	0.00	-322.24	1294.94
4	5	4.40	0.00	-262.92	1610.69
5	5	4.40	0.00	-263.23	1610.96
5	6	5.50	0.00	-209.98	1880.04
6	6	5.50	0.00	-210.26	1880.23
6	7	6.60	0.00	-159.96	2092.06
7	7	6.60	0.00	-160.19	2092.23
7	8	7.70	0.00	-110.02	2246.66
8	8	7.70	-0.01	-110.10	2246.79
8	9	8.80	-0.01	-60.41	2342.13
9	9	8.80	0.00	-60.37	2342.20
9	10	9.90	0.00	-10.37	2390.27
10	10	9.90	0.00	-10.29	2390.30
10	11	11.00	0.00	40.05	2381.55
11	11	11.00	0.00	40.07	2381.58
11	12	12.10	0.00	90.29	2315.62
12	12	12.10	0.00	90.42	2315.54
12	13	13.20	0.00	140.18	2191.41
13	13	13.20	0.00	140.24	2191.31
13	14	14.30	0.00	190.55	2016.92
14	14	14.30	12.56	186.63	2016.76
14	15	15.40	6.94	225.73	1799.37
15	15	15.40	0.00	227.88	1799.20
15	16	16.50	0.00	213.99	1537.11
16	16	16.50	0.00	213.60	1536.73
16	17	17.60	0.00	231.41	1286.25
17	17	17.60	-0.01	231.28	1285.69
17	18	18.70	-0.01	210.27	1030.23
18	18	18.70	-0.01	210.10	1029.33
18	19	19.80	-0.01	200.51	801.12
19	19	19.80	0.00	200.24	800.01
19	20	20.90	0.00	190.73	584.49
20	20	20.90	0.00	189.81	584.52
20	21	22.00	0.00	169.48	376.38
21	1021	22.00	0.00	-194.61	376.37
21	22	23.40	0.00	-203.90	679.25
22	22	23.40	0.00	-204.93	679.17
22	23	24.80	0.00	-211.71	973.36
23	23	24.80	0.00	-212.87	973.40
23	24	26.20	0.00	-273.40	1306.59
24	24	26.20	0.00	-274.97	1308.01
24	25	27.60	0.00	-271.85	1685.13
25	25	27.60	0.00	-272.07	1686.45
25	26	29.00	0.00	-310.49	2126.75
26	26	29.00	4.53	-309.11	2127.22

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.66	-251.38	2515.13
27	27	30.40	0.00	-252.24	2515.48
27	28	31.80	0.00	-196.40	2825.43
28	28	31.80	0.00	-196.15	2825.70
28	29	33.20	0.00	-123.70	3048.81
29	29	33.20	0.00	-123.38	3049.05
29	30	34.60	0.00	-69.26	3185.29
30	30	34.60	0.00	-68.89	3185.40
30	31	36.00	0.00	-4.47	3227.68
31	31	36.00	0.00	-4.18	3227.69
31	32	37.40	0.00	68.99	3185.38
32	32	37.40	0.00	69.34	3185.31
32	33	38.80	0.00	123.45	3048.90
33	33	38.80	0.00	123.79	3048.69
33	34	40.20	0.00	196.32	2825.59
34	34	40.20	0.00	196.55	2825.31
34	35	41.60	0.00	261.90	2512.48
35	35	41.60	6.46	260.41	2512.09
35	36	43.00	3.34	311.42	2117.85
36	36	43.00	0.00	312.40	2117.43
36	37	44.40	0.00	285.66	1680.03
37	37	44.40	0.00	285.55	1678.86
37	38	45.80	0.00	289.41	1275.33
38	38	45.80	0.00	288.62	1273.72
38	39	47.20	0.00	245.18	905.24
39	39	47.20	0.00	245.34	904.40
39	40	48.60	0.00	227.05	571.58
40	40	48.60	0.00	226.01	571.64
40	41	50.00	0.00	215.13	237.47
41	1041	50.00	0.00	-215.13	237.47
41	42	51.40	0.00	-226.01	571.62
42	42	51.40	0.00	-227.05	571.58
42	43	52.80	0.00	-245.34	904.37
43	43	52.80	0.00	-245.18	905.22
43	44	54.20	0.00	-288.62	1273.72
44	44	54.20	0.00	-289.41	1275.33
44	45	55.60	0.00	-285.57	1678.90
45	45	55.60	0.00	-285.65	1680.07
45	46	57.00	0.00	-312.39	2117.43
46	46	57.00	3.34	-311.43	2117.88
46	47	58.40	6.46	-260.42	2512.12
47	47	58.40	0.00	-261.91	2512.51
47	48	59.80	0.00	-196.55	2825.37
48	48	59.80	0.00	-196.31	2825.64
48	49	61.20	0.00	-123.78	3048.70
49	49	61.20	0.01	-123.45	3048.89
49	50	62.60	0.01	-69.34	3185.34
50	50	62.60	0.00	-68.98	3185.45
50	51	64.00	0.00	4.17	3227.68
51	51	64.00	0.00	4.47	3227.69
51	52	65.40	0.00	68.87	3185.42

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	69.24	3185.29
52	53	66.80	0.00	123.38	3049.11
53	53	66.80	0.00	123.69	3048.87
53	54	68.20	0.00	196.15	2825.76
54	54	68.20	0.00	196.40	2825.50
54	55	69.60	0.00	252.24	2515.49
55	55	69.60	3.66	251.39	2515.17
55	56	71.00	4.53	309.14	2127.26
56	56	71.00	0.00	310.48	2126.78
56	57	72.40	0.00	272.07	1686.47
57	57	72.40	0.00	271.85	1685.14
57	58	73.80	0.00	274.95	1307.98
58	58	73.80	0.00	273.38	1306.56
58	59	75.20	0.00	212.89	973.41
59	59	75.20	0.00	211.70	973.34
59	60	76.60	0.00	204.92	679.17
60	60	76.60	0.00	203.90	679.24
60	61	78.00	0.00	194.60	376.40
61	1061	78.00	0.00	-169.48	376.37
61	62	79.10	0.00	-189.81	584.52
62	62	79.10	0.00	-190.72	584.49
62	63	80.20	0.00	-200.24	799.99
63	63	80.20	0.00	-200.52	801.10
63	64	81.30	0.00	-210.11	1029.34
64	64	81.30	0.00	-210.28	1030.23
64	65	82.40	0.00	-231.29	1285.70
65	65	82.40	0.00	-231.43	1286.25
65	66	83.50	0.00	-213.60	1536.76
66	66	83.50	0.01	-213.99	1537.15
66	67	84.60	0.01	-227.88	1799.23
67	67	84.60	6.95	-225.73	1799.43
67	68	85.70	12.57	-186.63	2016.83
68	68	85.70	0.01	-190.55	2016.96
68	69	86.80	0.01	-140.24	2191.36
69	69	86.80	0.01	-140.20	2191.49
69	70	87.90	0.01	-90.42	2315.59
70	70	87.90	0.00	-90.30	2315.68
70	71	89.00	0.00	-40.12	2381.60
71	71	89.00	0.00	-40.07	2381.62
71	72	90.10	0.00	10.28	2390.38
72	72	90.10	0.02	10.34	2390.33
72	73	91.20	0.02	60.34	2342.28
73	73	91.20	0.00	60.38	2342.19
73	74	92.30	0.00	110.08	2246.84
74	74	92.30	0.00	109.99	2246.73
74	75	93.40	0.00	160.17	2092.29
75	75	93.40	0.00	159.95	2092.09
75	76	94.50	0.00	210.25	1880.27
76	76	94.50	0.01	209.98	1880.08
76	77	95.60	0.01	263.23	1611.01
77	77	95.60	0.00	262.88	1610.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	322.22	1294.92
78	78	96.70	0.00	321.77	1294.64
78	79	97.80	0.00	371.86	921.01
79	79	97.80	0.00	371.21	920.75
79	80	98.90	0.00	421.42	489.74
80	80	98.90	0.00	420.64	489.42
80	81	100.00	0.00	177.47	1.38
101	101	0.00	0.00	-206.83	1.19
101	102	1.10	0.00	-454.69	527.54
102	102	1.10	0.00	-452.83	526.91
102	103	2.20	0.00	-399.80	989.66
103	103	2.20	0.00	-398.23	989.07
103	104	3.30	0.00	-345.38	1388.20
104	104	3.30	0.00	-343.97	1387.66
104	105	4.40	0.00	-290.94	1724.31
105	105	4.40	0.00	-289.86	1723.76
105	106	5.50	0.00	-222.21	2009.78
106	106	5.50	0.00	-221.43	2009.35
106	107	6.60	0.00	-168.35	2233.36
107	107	6.60	0.00	-167.65	2233.06
107	108	7.70	0.00	-114.73	2395.08
108	108	7.70	-0.01	-114.14	2394.91
108	109	8.80	-0.01	-61.25	2495.02
109	109	8.80	0.00	-60.79	2494.95
109	110	9.90	0.00	-7.86	2542.92
110	110	9.90	0.00	-7.45	2542.85
110	111	11.00	0.00	45.63	2530.87
111	111	11.00	0.00	46.00	2530.90
111	112	12.10	0.00	98.97	2457.91
112	112	12.10	0.00	99.35	2458.05
112	113	13.20	0.00	152.12	2324.04
113	113	13.20	0.00	152.47	2324.22
113	114	14.30	0.00	205.47	2135.85
114	114	14.30	12.57	201.93	2136.16
114	115	15.40	6.95	243.59	1901.82
115	115	15.40	0.00	246.15	1902.15
115	116	16.50	0.00	244.13	1619.88
116	116	16.50	0.00	245.05	1620.30
116	117	17.60	0.00	264.91	1334.59
117	117	17.60	-0.01	265.80	1334.86
117	118	18.70	-0.01	226.55	1051.39
118	118	18.70	-0.01	227.16	1051.02
118	119	19.80	-0.01	201.07	813.24
119	119	19.80	0.00	201.00	812.85
119	120	20.90	0.00	177.25	604.40
120	120	20.90	0.00	176.59	604.41
120	121	22.00	0.00	165.54	401.15
121	1121	22.00	0.00	-191.47	401.16
121	122	23.40	0.00	-205.93	700.81
122	122	23.40	0.00	-206.73	700.85
122	123	24.80	0.00	-215.64	1000.49

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-216.91	1000.20
123	124	26.20	0.00	-294.19	1344.29
124	124	26.20	0.00	-293.45	1344.82
124	125	27.60	0.00	-293.89	1751.42
125	125	27.60	0.00	-292.74	1751.71
125	126	29.00	0.00	-329.23	2210.12
126	126	29.00	4.53	-327.67	2209.71
126	127	30.40	3.66	-265.76	2619.09
127	127	30.40	0.00	-266.60	2618.68
127	128	31.80	0.00	-206.98	2944.46
128	128	31.80	0.00	-206.96	2944.13
128	129	33.20	0.00	-129.16	3178.56
129	129	33.20	0.00	-129.29	3178.33
129	130	34.60	0.00	-73.63	3322.04
130	130	34.60	0.00	-73.78	3321.94
130	131	36.00	0.00	-5.44	3366.21
131	131	36.00	0.00	-5.63	3366.18
131	132	37.40	0.00	73.29	3322.72
132	132	37.40	0.00	73.10	3322.80
132	133	38.80	0.00	128.72	3179.71
133	133	38.80	0.00	128.62	3179.96
133	134	40.20	0.00	206.44	2946.53
134	134	40.20	0.00	206.41	2946.85
134	135	41.60	0.00	275.45	2619.17
135	135	41.60	6.46	274.01	2619.57
135	136	43.00	3.34	328.85	2205.21
136	136	43.00	0.00	329.90	2205.63
136	137	44.40	0.00	308.56	1748.04
137	137	44.40	0.00	309.55	1747.93
137	138	45.80	0.00	309.42	1314.27
138	138	45.80	0.00	310.60	1313.61
138	139	47.20	0.00	248.44	931.97
139	139	47.20	0.00	248.93	931.77
139	140	48.60	0.00	228.07	598.29
140	140	48.60	0.00	227.24	598.31
140	141	50.00	0.00	210.99	268.35
141	1141	50.00	0.00	-210.98	268.35
141	142	51.40	0.00	-227.23	598.29
142	142	51.40	0.00	-228.07	598.28
142	143	52.80	0.00	-248.93	931.75
143	143	52.80	0.00	-248.44	931.96
143	144	54.20	0.00	-310.59	1313.58
144	144	54.20	0.00	-309.45	1314.26
144	145	55.60	0.00	-309.56	1747.95
145	145	55.60	0.00	-308.59	1748.06
145	146	57.00	0.00	-329.90	2205.71
146	146	57.00	3.34	-328.88	2205.29
146	147	58.40	6.46	-274.06	2619.63
147	147	58.40	0.00	-275.51	2619.21
147	148	59.80	0.00	-206.45	2946.90
148	148	59.80	0.00	-206.46	2946.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-128.63	3179.99
149	149	61.20	0.00	-128.73	3179.77
149	150	62.60	0.00	-73.10	3322.90
150	150	62.60	0.00	-73.29	3322.82
150	151	64.00	0.00	5.63	3366.27
151	151	64.00	0.00	5.44	3366.28
151	152	65.40	0.00	73.78	3322.01
152	152	65.40	0.00	73.61	3322.10
152	153	66.80	0.00	129.26	3178.42
153	153	66.80	0.00	129.18	3178.66
153	154	68.20	0.00	206.96	2944.21
154	154	68.20	0.00	206.98	2944.50
154	155	69.60	0.00	266.58	2618.72
155	155	69.60	3.66	265.76	2619.16
155	156	71.00	4.53	327.66	2209.78
156	156	71.00	0.00	329.26	2210.18
156	157	72.40	0.00	292.75	1751.74
157	157	72.40	0.00	293.90	1751.43
157	158	73.80	0.00	293.46	1344.80
158	158	73.80	0.01	294.20	1344.26
158	159	75.20	0.01	216.90	1000.17
159	159	75.20	0.00	215.64	1000.50
159	160	76.60	0.00	206.73	700.87
160	160	76.60	0.00	205.93	700.82
160	161	78.00	0.00	191.47	401.19
161	1161	78.00	0.00	-165.55	401.14
161	162	79.10	0.00	-176.61	604.41
162	162	79.10	0.00	-177.22	604.35
162	163	80.20	0.00	-201.00	812.85
163	163	80.20	0.00	-201.07	813.23
163	164	81.30	0.00	-227.15	1051.05
164	164	81.30	0.00	-226.55	1051.41
164	165	82.40	0.00	-265.80	1334.88
165	165	82.40	0.00	-264.92	1334.62
165	166	83.50	0.00	-245.06	1620.35
166	166	83.50	0.01	-244.14	1619.93
166	167	84.60	0.01	-246.18	1902.22
167	167	84.60	6.95	-243.58	1901.88
167	168	85.70	12.57	-201.92	2136.20
168	168	85.70	0.00	-205.46	2135.89
168	169	86.80	0.00	-152.46	2324.31
169	169	86.80	0.00	-152.13	2324.07
169	170	87.90	0.00	-99.38	2458.11
170	170	87.90	0.00	-98.98	2457.97
170	171	89.00	0.00	-46.03	2530.97
171	171	89.00	0.00	-45.68	2530.90
171	172	90.10	0.00	7.44	2542.89
172	172	90.10	0.00	7.82	2542.92
172	173	91.20	0.00	60.77	2494.97
173	173	91.20	0.00	61.20	2495.06
173	174	92.30	0.00	114.10	2394.95

CÁLCULO TENSIONAL

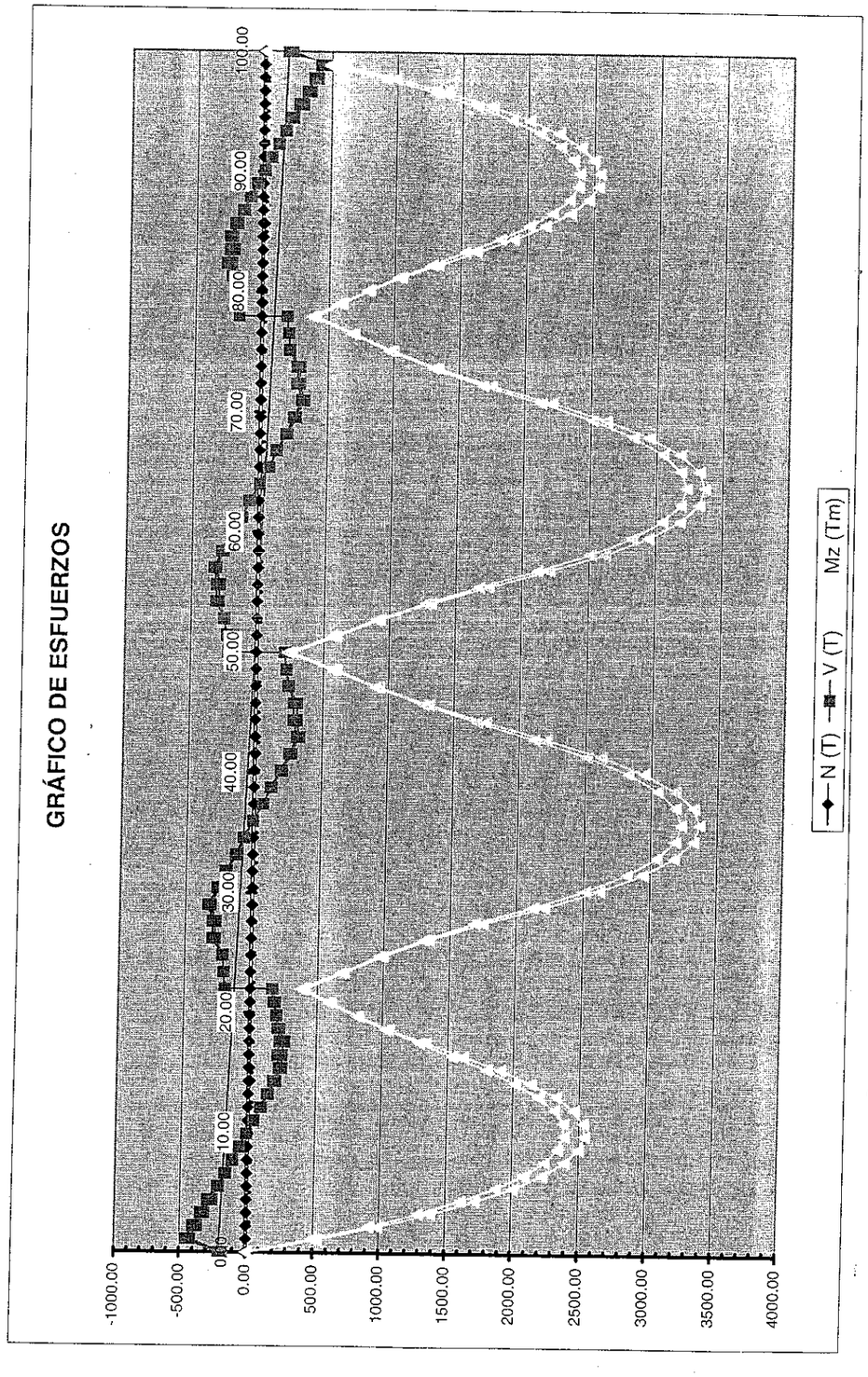
Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ+

C. Infrecuentes dominante tren Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	114.72	2395.15
174	175	93.40	0.00	167.64	2233.11
175	175	93.40	0.00	168.35	2233.40
175	176	94.50	0.00	221.42	2009.41
176	176	94.50	0.00	222.19	2009.83
176	177	95.60	0.00	289.84	1723.81
177	177	95.60	0.00	290.92	1724.31
177	178	96.70	0.00	343.97	1387.67
178	178	96.70	0.00	345.34	1388.22
178	179	97.80	0.00	398.21	989.05
179	179	97.80	0.00	399.78	989.66
179	180	98.90	0.00	452.82	526.91
180	180	98.90	0.00	454.67	527.54
180	181	100.00	0.00	206.82	1.19



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-343.54	-1.19
1	2	1.10	0.00	-97.71	117.84
2	2	1.10	0.00	-98.30	117.83
2	3	2.20	0.00	-79.44	215.62
3	3	2.20	0.00	-80.03	215.62
3	4	3.30	0.00	-61.18	293.27
4	4	3.30	0.00	-61.76	293.27
4	5	4.40	0.00	-42.93	350.86
5	5	4.40	0.00	-43.52	350.86
5	6	5.50	0.00	-24.67	388.35
6	6	5.50	0.00	-25.28	388.32
6	7	6.60	0.00	-6.42	405.80
7	7	6.60	0.00	-7.09	405.74
7	8	7.70	0.00	11.75	403.18
8	8	7.70	-0.01	11.08	403.13
8	9	8.80	-0.01	30.37	380.58
9	9	8.80	0.00	29.49	380.50
9	10	9.90	0.00	48.53	337.64
10	10	9.90	0.00	47.70	337.64
10	11	11.00	0.00	66.55	274.76
11	11	11.00	0.00	65.66	274.72
11	12	12.10	0.00	84.55	192.09
12	12	12.10	0.00	83.64	192.00
12	13	13.20	0.00	102.62	89.51
13	13	13.20	0.00	101.67	89.45
13	14	14.30	0.00	120.55	-32.80
14	14	14.30	-0.30	119.66	-32.85
14	15	15.40	7.36	149.64	-187.95
15	15	15.40	0.00	150.94	-187.99
15	16	16.50	0.00	233.87	-374.96
16	16	16.50	0.00	233.15	-374.82
16	17	17.60	0.00	273.01	-648.98
17	17	17.60	-0.01	271.83	-648.64
17	18	18.70	-0.01	341.80	-986.19
18	18	18.70	0.00	340.70	-985.46
18	19	19.80	0.00	416.46	-1399.45
19	19	19.80	0.00	415.51	-1398.49
19	20	20.90	0.00	513.59	-1919.50
20	20	20.90	0.00	512.99	-1919.47
20	21	22.00	0.00	591.31	-2524.88
21	1021	22.00	0.00	-639.55	-2524.71
21	22	23.40	0.00	-560.35	-1693.92
22	22	23.40	0.00	-561.08	-1693.62
22	23	24.80	0.00	-460.45	-978.91
23	23	24.80	0.00	-458.27	-978.87
23	24	26.20	0.00	-332.45	-442.56
24	24	26.20	0.00	-332.48	-443.60
24	25	27.60	0.00	-246.16	-39.80
25	25	27.60	0.00	-247.32	-40.82
25	26	29.00	0.00	-120.95	177.77
26	26	29.00	5.58	-120.95	177.67

INFRECUENTEST.Tinf.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	4.40	-92.15	327.92
27	27	30.40	0.00	-94.48	327.88
27	28	31.80	0.00	-60.84	432.60
28	28	31.80	0.00	-62.05	432.55
28	29	33.20	0.00	-38.06	502.61
29	29	33.20	0.00	-39.19	502.60
29	30	34.60	0.00	-12.84	538.58
30	30	34.60	0.00	-13.90	538.47
30	31	36.00	0.00	17.00	535.14
31	31	36.00	0.00	15.93	535.11
31	32	37.40	0.00	40.13	495.94
32	32	37.40	0.00	38.96	495.91
32	33	38.80	0.00	62.94	424.56
33	33	38.80	0.00	61.79	424.55
33	34	40.20	0.00	85.80	321.24
34	34	40.20	0.00	84.55	321.25
34	35	41.60	0.00	108.70	186.02
35	35	41.60	-0.13	107.48	186.02
35	36	43.00	5.05	143.08	8.72
36	36	43.00	0.00	142.95	8.83
36	37	44.40	0.00	257.69	-246.16
37	37	44.40	0.00	256.37	-245.35
37	38	45.80	0.00	341.91	-656.10
38	38	45.80	0.00	340.81	-654.85
38	39	47.20	0.00	435.11	-1190.81
39	39	47.20	0.00	433.37	-1190.15
39	40	48.60	0.00	559.49	-1889.07
40	40	48.60	0.00	558.64	-1889.12
40	41	50.00	0.00	642.83	-2723.77
41	1041	50.00	0.00	-642.83	-2723.77
41	42	51.40	0.00	-558.66	-1889.12
42	42	51.40	0.00	-559.49	-1889.07
42	43	52.80	0.00	-433.37	-1190.14
43	43	52.80	0.00	-435.11	-1190.79
43	44	54.20	0.00	-340.81	-654.82
44	44	54.20	0.00	-341.91	-656.10
44	45	55.60	0.00	-256.35	-245.31
45	45	55.60	0.00	-257.68	-246.11
45	46	57.00	0.00	-142.92	8.86
46	46	57.00	5.05	-143.09	8.72
46	47	58.40	-0.14	-107.49	186.03
47	47	58.40	0.00	-108.69	186.02
47	48	59.80	0.00	-84.55	321.26
48	48	59.80	0.00	-85.77	321.26
48	49	61.20	0.00	-61.76	424.54
49	49	61.20	0.01	-62.94	424.58
49	50	62.60	0.01	-38.96	495.92
50	50	62.60	0.00	-40.13	495.92
50	51	64.00	0.00	-15.94	535.10
51	51	64.00	0.00	-16.99	535.11
51	52	65.40	0.00	13.93	538.44

INFRECUENTEST.Tinf.MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	12.84	538.53
52	53	66.80	0.00	39.19	502.58
53	53	66.80	0.00	38.07	502.59
53	54	68.20	0.00	62.05	432.54
54	54	68.20	0.00	60.84	432.55
54	55	69.60	0.00	94.48	327.84
55	55	69.60	4.40	92.15	327.85
55	56	71.00	5.57	120.95	177.67
56	56	71.00	0.00	120.96	177.77
56	57	72.40	0.00	247.32	-40.82
57	57	72.40	0.00	246.17	-39.85
57	58	73.80	0.00	332.48	-443.64
58	58	73.80	0.00	332.46	-442.58
58	59	75.20	0.00	458.28	-978.87
59	59	75.20	0.00	460.44	-978.89
59	60	76.60	0.00	561.07	-1693.63
60	60	76.60	0.00	560.34	-1693.93
60	61	78.00	0.00	639.58	-2524.72
61	1061	78.00	0.00	-591.31	-2524.96
61	62	79.10	0.00	-512.99	-1919.51
62	62	79.10	0.00	-513.60	-1919.56
62	63	80.20	0.00	-415.52	-1398.54
63	63	80.20	0.00	-416.48	-1399.51
63	64	81.30	0.00	-340.72	-985.50
64	64	81.30	0.00	-341.81	-986.22
64	65	82.40	0.00	-271.84	-648.65
65	65	82.40	0.00	-273.01	-648.98
65	66	83.50	0.00	-233.15	-374.86
66	66	83.50	0.01	-233.87	-374.96
66	67	84.60	0.01	-150.94	-188.00
67	67	84.60	7.37	-149.65	-187.98
67	68	85.70	-0.30	-119.66	-32.89
68	68	85.70	0.01	-120.54	-32.84
68	69	86.80	0.01	-101.66	89.42
69	69	86.80	0.01	-102.62	89.47
69	70	87.90	0.01	-83.64	191.98
70	70	87.90	0.00	-84.56	192.06
70	71	89.00	0.00	-65.68	274.67
71	71	89.00	0.00	-66.57	274.72
71	72	90.10	0.00	-47.71	337.60
72	72	90.10	0.02	-48.54	337.61
72	73	91.20	0.02	-29.50	380.44
73	73	91.20	0.00	-30.38	380.53
73	74	92.30	0.00	-11.10	403.09
74	74	92.30	0.00	-11.76	403.13
74	75	93.40	0.00	7.08	405.71
75	75	93.40	0.00	6.41	405.75
75	76	94.50	0.00	25.27	388.29
76	76	94.50	0.01	24.67	388.34
76	77	95.60	0.01	43.53	350.83
77	77	95.60	0.00	42.92	350.84

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	61.75	293.26
78	78	96.70	0.00	61.17	293.25
78	79	97.80	0.00	80.03	215.61
79	79	97.80	0.00	79.42	215.61
79	80	98.90	0.00	98.28	117.82
80	80	98.90	0.00	97.70	117.84
80	81	100.00	0.00	343.52	-1.19
101	101	0.00	0.00	-347.46	-1.38
101	102	1.10	0.00	-95.85	115.75
102	102	1.10	0.00	-96.26	116.05
102	103	2.20	0.00	-77.62	211.65
103	103	2.20	0.00	-77.93	211.94
103	104	3.30	0.00	-59.36	287.39
104	104	3.30	0.00	-59.48	287.65
104	105	4.40	0.00	-40.93	342.90
105	105	4.40	0.00	-40.96	343.08
105	106	5.50	0.00	-22.38	377.90
106	106	5.50	0.00	-22.23	378.09
106	107	6.60	0.00	-3.63	392.32
107	107	6.60	0.00	-3.41	392.48
107	108	7.70	0.00	15.14	386.01
108	108	7.70	-0.01	15.44	386.18
108	109	8.80	-0.01	34.00	359.00
109	109	8.80	0.00	34.32	359.10
109	110	9.90	0.00	52.89	311.12
110	110	9.90	0.00	53.28	311.20
110	111	11.00	0.00	71.87	242.39
111	111	11.00	0.00	72.38	242.43
111	112	12.10	0.00	90.92	152.59
112	112	12.10	0.00	91.46	152.61
112	113	13.20	0.00	110.04	41.77
113	113	13.20	0.00	110.61	41.74
113	114	14.30	0.00	129.24	-90.20
114	114	14.30	-0.30	129.97	-90.26
114	115	15.40	7.37	160.03	-256.56
115	115	15.40	0.00	163.10	-256.71
115	116	16.50	0.00	236.38	-457.20
116	116	16.50	0.00	236.98	-457.38
116	117	17.60	0.00	274.88	-735.18
117	117	17.60	-0.01	275.27	-735.23
117	118	18.70	-0.01	360.17	-1087.77
118	118	18.70	-0.01	360.84	-1087.24
118	119	19.80	-0.01	455.08	-1533.64
119	119	19.80	0.00	456.57	-1533.23
119	120	20.90	0.00	576.94	-2115.36
120	120	20.90	0.00	578.95	-2115.26
120	121	22.00	0.00	651.31	-2785.48
121	1121	22.00	0.00	-696.22	-2785.46
121	122	23.40	0.00	-609.14	-1878.44
122	122	23.40	0.00	-606.51	-1878.64
122	123	24.80	0.00	-500.32	-1105.65

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-497.34	-1105.70
123	124	26.20	0.00	-352.50	-529.82
124	124	26.20	0.00	-351.62	-530.67
124	125	27.60	0.00	-258.07	-107.46
125	125	27.60	0.00	-257.79	-108.17
125	126	29.00	0.00	-130.05	132.05
126	126	29.00	5.58	-127.74	132.17
126	127	30.40	4.40	-100.28	293.07
127	127	30.40	0.00	-100.44	293.14
127	128	31.80	0.00	-67.05	406.25
128	128	31.80	0.00	-66.05	406.32
128	129	33.20	0.00	-42.42	482.28
129	129	33.20	0.00	-41.53	482.33
129	130	34.60	0.00	-15.72	522.34
130	130	34.60	0.00	-14.80	522.28
130	131	36.00	0.00	17.17	519.61
131	131	36.00	0.00	18.09	519.63
131	132	37.40	0.00	41.79	477.72
132	132	37.40	0.00	42.71	477.74
132	133	38.80	0.00	66.35	401.38
133	133	38.80	0.00	67.34	401.36
133	134	40.20	0.00	91.03	290.50
134	134	40.20	0.00	92.00	290.46
134	135	41.60	0.00	115.90	144.98
135	135	41.60	-0.13	116.91	144.92
135	136	43.00	5.05	151.51	-45.18
136	136	43.00	0.00	153.89	-45.26
136	137	44.40	0.00	266.58	-320.77
137	137	44.40	0.00	267.09	-320.28
137	138	45.80	0.00	360.02	-750.69
138	138	45.80	0.00	360.53	-749.66
138	139	47.20	0.00	468.11	-1323.08
139	139	47.20	0.00	469.38	-1322.68
139	140	48.60	0.00	606.67	-2084.71
140	140	48.60	0.00	609.33	-2084.51
140	141	50.00	0.00	701.74	-2998.56
141	1141	50.00	0.00	-701.75	-2998.56
141	142	51.40	0.00	-609.32	-2084.48
142	142	51.40	0.00	-606.68	-2084.67
142	143	52.80	0.00	-469.38	-1322.64
143	143	52.80	0.00	-468.10	-1323.05
143	144	54.20	0.00	-360.50	-749.67
144	144	54.20	0.00	-360.03	-750.68
144	145	55.60	0.00	-267.10	-320.23
145	145	55.60	0.00	-266.58	-320.72
145	146	57.00	0.00	-153.89	-45.25
146	146	57.00	5.05	-151.52	-45.17
146	147	58.40	-0.13	-116.92	144.90
147	147	58.40	0.00	-115.90	144.99
147	148	59.80	0.00	-92.00	290.43
148	148	59.80	0.00	-91.03	290.51

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-67.34	401.35
149	149	61.20	0.00	-66.35	401.33
149	150	62.60	0.00	-42.71	477.71
150	150	62.60	0.00	-41.79	477.71
150	151	64.00	0.00	-18.09	519.59
151	151	64.00	0.00	-17.17	519.57
151	152	65.40	0.00	14.80	522.25
152	152	65.40	0.00	15.72	522.31
152	153	66.80	0.00	41.52	482.27
153	153	66.80	0.00	42.42	482.24
153	154	68.20	0.00	66.05	406.25
154	154	68.20	0.00	67.05	406.20
154	155	69.60	0.00	100.44	293.08
155	155	69.60	4.40	100.25	293.00
155	156	71.00	5.57	127.72	132.15
156	156	71.00	0.00	130.06	132.02
156	157	72.40	0.00	257.81	-108.20
157	157	72.40	0.00	258.08	-107.49
157	158	73.80	0.00	351.63	-530.71
158	158	73.80	0.01	352.51	-529.84
158	159	75.20	0.01	497.37	-1105.71
159	159	75.20	0.00	500.30	-1105.67
159	160	76.60	0.00	606.52	-1878.63
160	160	76.60	0.00	609.14	-1878.49
160	161	78.00	0.00	696.24	-2785.52
161	1161	78.00	0.00	-651.33	-2785.53
161	162	79.10	0.00	-578.98	-2115.31
162	162	79.10	0.00	-576.92	-2115.46
162	163	80.20	0.00	-456.57	-1533.28
163	163	80.20	0.00	-455.07	-1533.68
163	164	81.30	0.00	-360.84	-1087.26
164	164	81.30	0.00	-360.18	-1087.79
164	165	82.40	0.00	-275.28	-735.25
165	165	82.40	0.00	-274.87	-735.22
165	166	83.50	0.00	-236.98	-457.45
166	166	83.50	0.01	-236.39	-457.26
166	167	84.60	0.01	-163.11	-256.71
167	167	84.60	7.37	-160.03	-256.60
167	168	85.70	-0.30	-129.96	-90.31
168	168	85.70	0.00	-129.27	-90.25
168	169	86.80	0.00	-110.65	41.70
169	169	86.80	0.00	-110.05	41.73
169	170	87.90	0.00	-91.47	152.59
170	170	87.90	0.00	-90.93	152.57
170	171	89.00	0.00	-72.40	242.41
171	171	89.00	0.00	-71.91	242.37
171	172	90.10	0.00	-53.29	311.19
172	172	90.10	0.00	-52.88	311.09
172	173	91.20	0.00	-34.31	359.07
173	173	91.20	0.00	-34.02	358.95
173	174	92.30	0.00	-15.45	386.14

CÁLCULO TENSIONAL

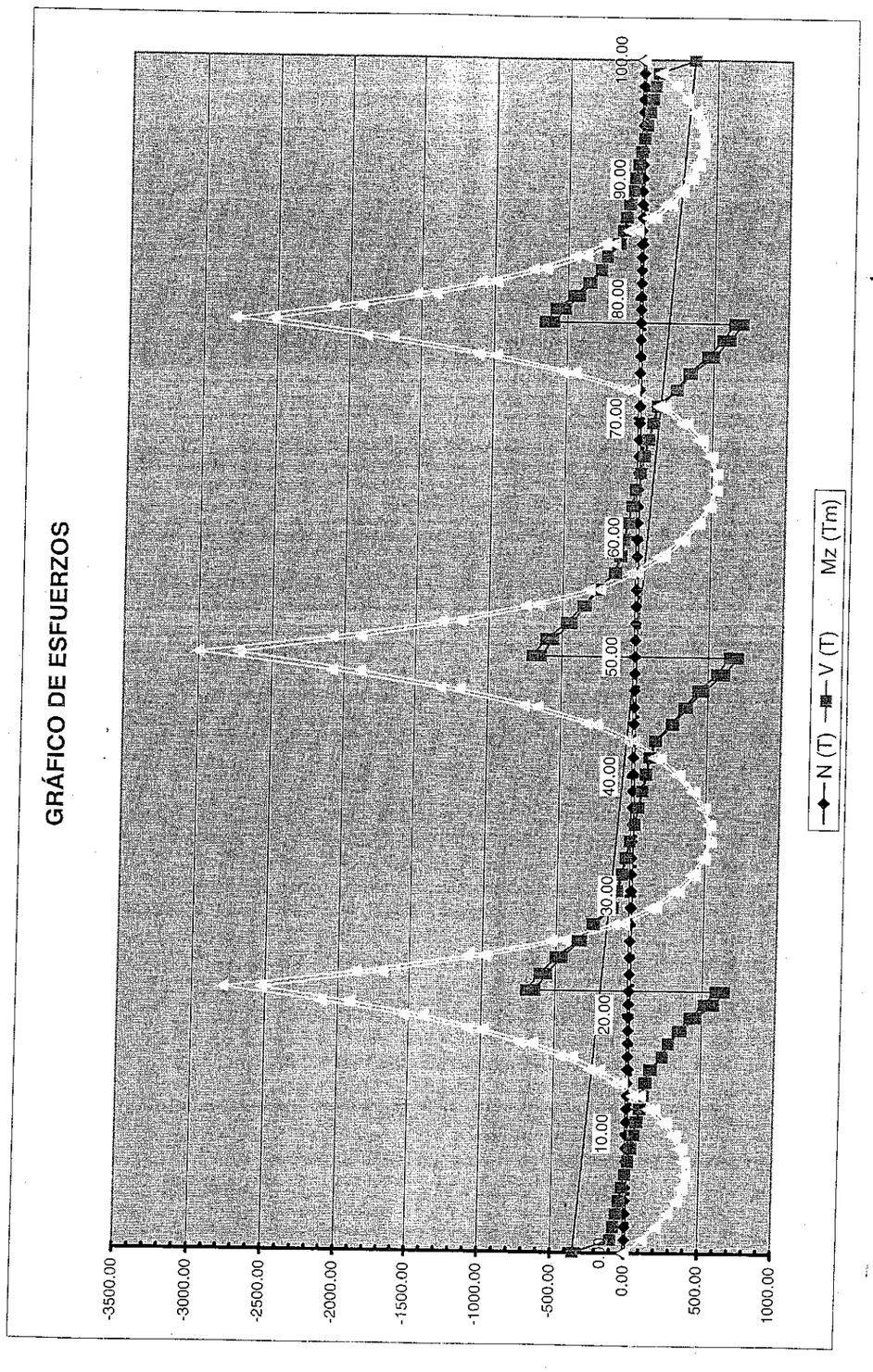
Hipótesis de cálculo:
INFRECUENTEST.Tinf.MZ-

C. Infrecuentes dominante tren Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-15.15	385.99
174	175	93.40	0.00	3.40	392.46
175	175	93.40	0.00	3.61	392.30
175	176	94.50	0.00	22.22	378.08
176	176	94.50	0.00	22.36	377.89
176	177	95.60	0.00	40.94	343.07
177	177	95.60	0.00	40.92	342.86
177	178	96.70	0.00	59.48	287.62
178	178	96.70	0.00	59.33	287.42
178	179	97.80	0.00	77.90	211.92
179	179	97.80	0.00	77.63	211.64
179	180	98.90	0.00	96.26	116.04
180	180	98.90	0.00	95.84	115.75
180	181	100.00	0.00	347.44	-1.38



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.66	-224.84	2535.03
27	27	30.40	0.00	-225.66	2535.28
27	28	31.80	0.00	-175.61	2813.69
28	28	31.80	0.00	-175.36	2813.88
28	29	33.20	0.00	-110.11	3013.10
29	29	33.20	0.00	-109.82	3013.26
29	30	34.60	0.00	-59.24	3132.73
30	30	34.60	0.00	-58.90	3132.80
30	31	36.00	0.00	-0.09	3166.84
31	31	36.00	0.00	0.17	3166.86
31	32	37.40	0.00	65.99	3123.00
32	32	37.40	0.00	66.30	3122.95
32	33	38.80	0.00	116.87	2993.56
33	33	38.80	0.00	117.20	2993.41
33	34	40.20	0.00	182.50	2784.41
34	34	40.20	0.00	182.72	2784.21
34	35	41.60	0.00	242.29	2493.17
35	35	41.60	6.46	240.84	2492.89
35	36	43.00	3.34	287.03	2128.22
36	36	43.00	0.00	288.06	2127.92
36	37	44.40	0.00	260.98	1723.52
37	37	44.40	0.00	260.94	1722.59
37	38	45.80	0.00	268.27	1350.83
38	38	45.80	0.00	267.69	1349.56
38	39	47.20	0.00	237.67	999.94
39	39	47.20	0.00	237.85	999.28
39	40	48.60	0.00	227.96	671.50
40	40	48.60	0.00	227.19	671.56
40	41	50.00	0.00	219.57	335.38
41	1041	50.00	0.00	-219.57	335.38
41	42	51.40	0.00	-227.19	671.54
42	42	51.40	0.00	-227.96	671.50
42	43	52.80	0.00	-237.85	999.26
43	43	52.80	0.00	-237.67	999.93
43	44	54.20	0.00	-267.69	1349.56
44	44	54.20	0.00	-268.27	1350.83
44	45	55.60	0.00	-260.95	1722.63
45	45	55.60	0.00	-260.97	1723.55
45	46	57.00	0.00	-288.05	2127.92
46	46	57.00	3.34	-287.04	2128.24
46	47	58.40	6.46	-240.85	2492.92
47	47	58.40	0.00	-242.29	2493.20
47	48	59.80	0.00	-182.73	2784.26
48	48	59.80	0.00	-182.49	2784.45
48	49	61.20	0.00	-117.19	2993.41
49	49	61.20	0.01	-116.87	2993.55
49	50	62.60	0.01	-66.30	3122.98
50	50	62.60	0.00	-65.98	3123.05
50	51	64.00	0.00	-0.17	3166.85
51	51	64.00	0.00	0.10	3166.86
51	52	65.40	0.00	58.90	3132.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	59.23	3132.72
52	53	66.80	0.00	109.82	3013.31
53	53	66.80	0.00	110.11	3013.14
53	54	68.20	0.00	175.36	2813.94
54	54	68.20	0.00	175.61	2813.76
54	55	69.60	0.00	225.66	2535.28
55	55	69.60	3.66	224.85	2535.06
55	56	71.00	4.53	277.89	2186.41
56	56	71.00	0.00	279.27	2186.07
56	57	72.40	0.00	243.26	1786.20
57	57	72.40	0.00	243.12	1785.15
57	58	73.80	0.00	250.79	1443.89
58	58	73.80	0.00	249.58	1442.76
58	59	75.20	0.00	205.07	1130.28
59	59	75.20	0.00	204.17	1130.24
59	60	76.60	0.00	203.49	842.84
60	60	76.60	0.00	202.72	842.90
60	61	78.00	0.00	196.38	541.29
61	1061	78.00	0.00	-159.33	541.27
61	62	79.10	0.00	-174.74	735.36
62	62	79.10	0.00	-175.42	735.34
62	63	80.20	0.00	-179.31	930.82
63	63	80.20	0.00	-179.50	931.70
63	64	81.30	0.00	-183.44	1133.23
64	64	81.30	0.00	-183.54	1133.93
64	65	82.40	0.00	-197.28	1353.28
65	65	82.40	0.00	-197.35	1353.72
65	66	83.50	0.00	-179.02	1565.31
66	66	83.50	0.01	-179.30	1565.62
66	67	84.60	0.01	-197.40	1792.99
67	67	84.60	6.95	-195.17	1793.13
67	68	85.70	12.57	-160.39	1980.68
68	68	85.70	0.01	-164.25	1980.77
68	69	86.80	0.01	-118.28	2130.13
69	69	86.80	0.01	-118.19	2130.21
69	70	87.90	0.01	-72.65	2232.97
70	70	87.90	0.00	-72.51	2233.02
70	71	89.00	0.00	-26.64	2282.91
71	71	89.00	0.00	-26.56	2282.91
71	72	90.10	0.00	19.45	2280.72
72	72	90.10	0.02	19.54	2280.67
72	73	91.20	0.02	65.25	2226.70
73	73	91.20	0.00	65.32	2226.64
73	74	92.30	0.00	110.81	2128.48
74	74	92.30	0.00	110.77	2128.40
74	75	93.40	0.00	156.64	1976.64
75	75	93.40	0.00	156.52	1976.49
75	76	94.50	0.00	202.48	1772.47
76	76	94.50	0.01	202.31	1772.34
76	77	95.60	0.01	250.64	1516.19
77	77	95.60	0.00	250.41	1516.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	303.60	1216.07
78	78	96.70	0.00	303.32	1215.88
78	79	97.80	0.00	349.12	863.32
79	79	97.80	0.00	348.68	863.15
79	80	98.90	0.00	394.57	458.30
80	80	98.90	0.00	394.05	458.09
80	81	100.00	0.00	172.31	1.09
101	101	0.00	0.00	-203.57	0.97
101	102	1.10	0.00	-418.26	485.10
102	102	1.10	0.00	-416.87	484.62
102	103	2.20	0.00	-369.06	911.94
103	103	2.20	0.00	-367.89	911.49
103	104	3.30	0.00	-320.21	1282.06
104	104	3.30	0.00	-319.16	1281.66
104	105	4.40	0.00	-271.34	1596.38
105	105	4.40	0.00	-270.55	1595.97
105	106	5.50	0.00	-211.03	1864.32
106	106	5.50	0.00	-210.45	1864.00
106	107	6.60	0.00	-162.60	2076.90
107	107	6.60	0.00	-162.08	2076.66
107	108	7.70	0.00	-114.35	2234.07
108	108	7.70	-0.01	-113.92	2233.94
108	109	8.80	-0.01	-66.21	2335.93
109	109	8.80	0.00	-65.88	2335.87
109	110	9.90	0.00	-18.14	2390.26
110	110	9.90	0.00	-17.86	2390.21
110	111	11.00	0.00	30.00	2390.75
111	111	11.00	0.00	30.25	2390.76
111	112	12.10	0.00	78.02	2336.60
112	112	12.10	0.00	78.28	2336.70
112	113	13.20	0.00	125.89	2227.85
113	113	13.20	0.00	126.11	2227.98
113	114	14.30	0.00	173.91	2069.77
114	114	14.30	12.57	170.23	2069.99
114	115	15.40	6.95	206.74	1871.68
115	115	15.40	0.00	209.15	1871.92
115	116	16.50	0.00	202.14	1631.77
116	116	16.50	0.00	202.84	1632.10
116	117	17.60	0.00	222.68	1393.88
117	117	17.60	-0.01	223.35	1394.09
117	118	18.70	-0.01	194.89	1154.10
118	118	18.70	-0.01	195.34	1153.79
118	119	19.80	-0.01	178.06	946.62
119	119	19.80	0.00	177.96	946.30
119	120	20.90	0.00	162.55	758.70
120	120	20.90	0.00	161.98	758.70
120	121	22.00	0.00	153.87	570.99
121	1121	22.00	0.00	-191.61	570.99
121	122	23.40	0.00	-202.25	867.00
122	122	23.40	0.00	-202.95	867.04
122	123	24.80	0.00	-205.51	1156.13

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-206.57	1155.92
123	124	26.20	0.00	-264.68	1474.87
124	124	26.20	0.00	-264.13	1475.31
124	125	27.60	0.00	-259.46	1838.19
125	125	27.60	0.00	-258.57	1838.44
125	126	29.00	0.00	-291.64	2248.87
126	126	29.00	4.53	-290.23	2248.59
126	127	30.40	3.66	-234.28	2611.23
127	127	30.40	0.00	-235.21	2610.93
127	128	31.80	0.00	-182.55	2899.60
128	128	31.80	0.00	-182.59	2899.37
128	129	33.20	0.00	-113.49	3105.94
129	129	33.20	0.00	-113.64	3105.77
129	130	34.60	0.00	-62.24	3230.21
130	130	34.60	0.00	-62.40	3230.14
130	131	36.00	0.00	-0.86	3265.47
131	131	36.00	0.00	-1.05	3265.45
131	132	37.40	0.00	68.96	3221.03
132	132	37.40	0.00	68.76	3221.08
132	133	38.80	0.00	120.13	3087.41
133	133	38.80	0.00	120.01	3087.59
133	134	40.20	0.00	189.13	2872.08
134	134	40.20	0.00	189.05	2872.31
134	135	41.60	0.00	251.15	2571.87
135	135	41.60	6.46	249.61	2572.16
135	136	43.00	3.34	298.44	2194.64
136	136	43.00	0.00	299.35	2194.94
136	137	44.40	0.00	278.06	1778.14
137	137	44.40	0.00	278.81	1778.04
137	138	45.80	0.00	282.79	1384.14
138	138	45.80	0.00	283.69	1383.60
138	139	47.20	0.00	238.53	1025.78
139	139	47.20	0.00	238.87	1025.61
139	140	48.60	0.00	226.76	700.01
140	140	48.60	0.00	226.04	700.03
140	141	50.00	0.00	213.96	370.33
141	1141	50.00	0.00	-213.95	370.33
141	142	51.40	0.00	-226.03	700.00
142	142	51.40	0.00	-226.76	700.00
142	143	52.80	0.00	-238.87	1025.60
143	143	52.80	0.00	-238.53	1025.77
143	144	54.20	0.00	-283.68	1383.57
144	144	54.20	0.00	-282.82	1384.13
144	145	55.60	0.00	-278.82	1778.06
145	145	55.60	0.00	-278.08	1778.16
145	146	57.00	0.00	-299.35	2195.00
146	146	57.00	3.34	-298.46	2194.70
146	147	58.40	6.46	-249.65	2572.20
147	147	58.40	0.00	-251.19	2571.90
147	148	59.80	0.00	-189.08	2872.35
148	148	59.80	0.00	-189.15	2872.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-120.01	3087.60
149	149	61.20	0.00	-120.14	3087.44
149	150	62.60	0.00	-68.76	3221.16
150	150	62.60	0.00	-68.96	3221.11
150	151	64.00	0.00	1.05	3265.52
151	151	64.00	0.00	0.86	3265.53
151	152	65.40	0.00	62.40	3230.20
152	152	65.40	0.00	62.22	3230.26
152	153	66.80	0.00	113.61	3105.85
153	153	66.80	0.00	113.50	3106.02
153	154	68.20	0.00	182.59	2899.43
154	154	68.20	0.00	182.55	2899.65
154	155	69.60	0.00	235.20	2610.98
155	155	69.60	3.66	234.28	2611.29
155	156	71.00	4.53	290.22	2248.65
156	156	71.00	0.00	291.66	2248.94
156	157	72.40	0.00	258.58	1838.46
157	157	72.40	0.00	259.47	1838.20
157	158	73.80	0.00	264.14	1475.29
158	158	73.80	0.01	264.68	1474.85
158	159	75.20	0.01	206.56	1155.90
159	159	75.20	0.00	205.50	1156.15
159	160	76.60	0.00	202.95	867.06
160	160	76.60	0.00	202.25	867.01
160	161	78.00	0.00	191.61	571.02
161	1161	78.00	0.00	-153.88	570.98
161	162	79.10	0.00	-161.99	758.70
162	162	79.10	0.00	-162.53	758.66
162	163	80.20	0.00	-177.96	946.30
163	163	80.20	0.00	-178.06	946.62
163	164	81.30	0.00	-195.33	1153.82
164	164	81.30	0.00	-194.89	1154.11
164	165	82.40	0.00	-223.35	1394.11
165	165	82.40	0.00	-222.68	1393.91
165	166	83.50	0.00	-202.84	1632.13
166	166	83.50	0.01	-202.15	1631.81
166	167	84.60	0.01	-209.18	1871.98
167	167	84.60	6.95	-206.73	1871.73
167	168	85.70	12.57	-170.22	2070.01
168	168	85.70	0.00	-173.91	2069.78
168	169	86.80	0.00	-126.11	2228.04
169	169	86.80	0.00	-125.90	2227.87
169	170	87.90	0.00	-78.30	2336.75
170	170	87.90	0.00	-78.03	2336.65
170	171	89.00	0.00	-30.28	2390.81
171	171	89.00	0.00	-30.05	2390.77
171	172	90.10	0.00	17.85	2390.24
172	172	90.10	0.00	18.11	2390.26
172	173	91.20	0.00	65.87	2335.88
173	173	91.20	0.00	66.17	2335.96
173	174	92.30	0.00	113.88	2233.97

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTESG.Tinf.MZ+

C. Infrecuentes dominante GRAD Mz+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	114.34	2234.12
174	175	93.40	0.00	162.07	2076.70
175	175	93.40	0.00	162.59	2076.92
175	176	94.50	0.00	210.44	1864.05
176	176	94.50	0.00	211.00	1864.37
176	177	95.60	0.00	270.52	1596.01
177	177	95.60	0.00	271.32	1596.39
177	178	96.70	0.00	319.15	1281.67
178	178	96.70	0.00	320.17	1282.07
178	179	97.80	0.00	367.86	911.47
179	179	97.80	0.00	369.03	911.93
179	180	98.90	0.00	416.86	484.63
180	180	98.90	0.00	418.23	485.10
180	181	100.00	0.00	203.56	0.97

05/09/03

Programa DINTEL PACADAR S.A.
INFRECUENTESG.Tinf.MZ+

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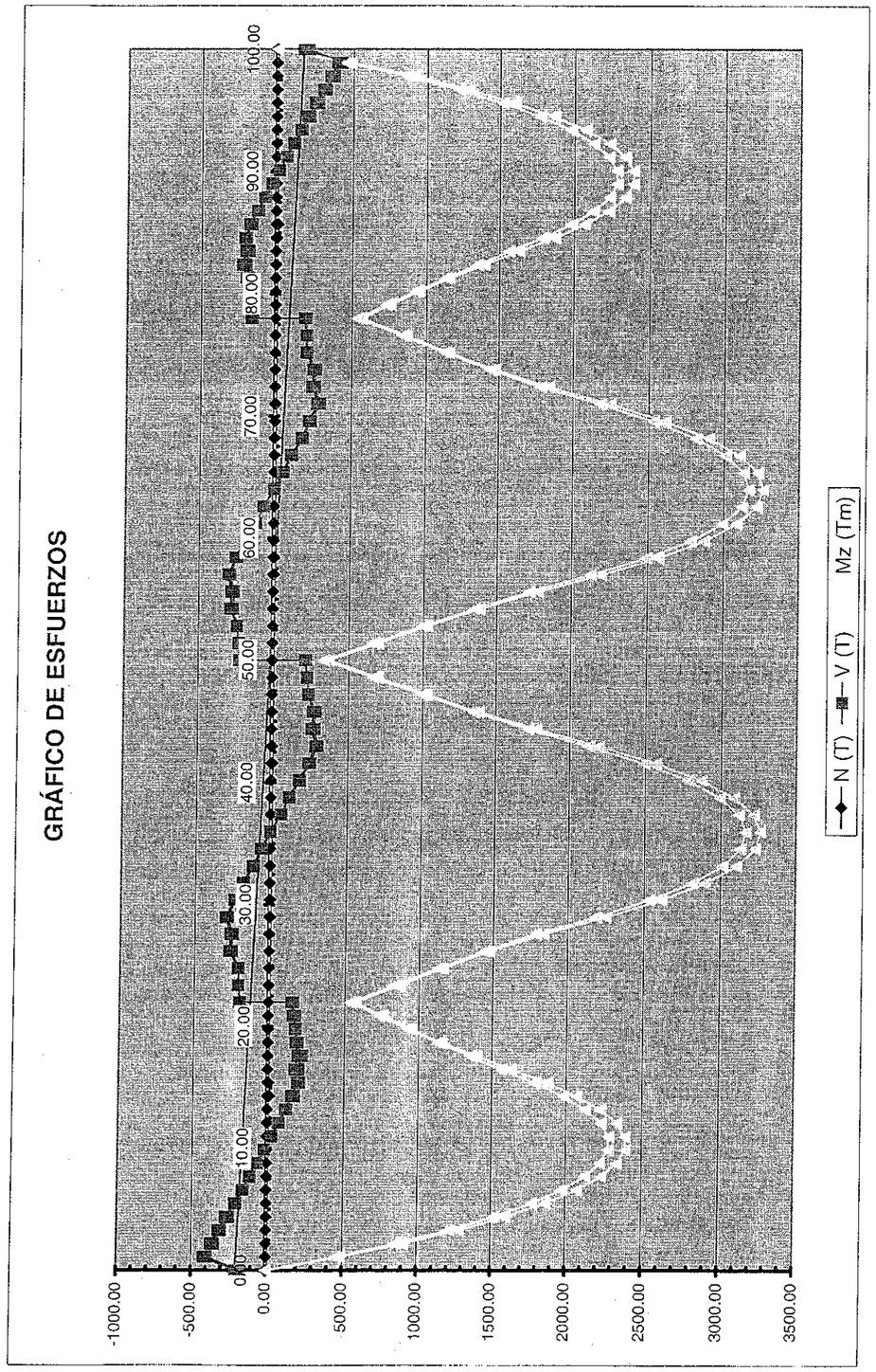


CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-316.31	-0.97
1	2	1.10	0.00	-104.06	124.61
2	2	1.10	0.00	-104.49	124.59
2	3	2.20	0.00	-85.99	229.38
3	3	2.20	0.00	-86.43	229.37
3	4	3.30	0.00	-67.94	314.25
4	4	3.30	0.00	-68.37	314.24
4	5	4.40	0.00	-49.90	379.29
5	5	4.40	0.00	-50.34	379.28
5	6	5.50	0.00	-31.85	424.48
6	6	5.50	0.00	-32.31	424.44
6	7	6.60	0.00	-13.82	449.86
7	7	6.60	0.00	-14.34	449.80
7	8	7.70	0.00	4.15	455.41
8	8	7.70	-0.01	3.63	455.36
8	9	8.80	-0.01	22.47	441.21
9	9	8.80	0.00	21.78	441.14
9	10	9.90	0.00	40.42	406.97
10	10	9.90	0.00	39.78	406.97
10	11	11.00	0.00	58.26	353.01
11	11	11.00	0.00	57.57	352.98
11	12	12.10	0.00	76.09	279.45
12	12	12.10	0.00	75.38	279.39
12	13	13.20	0.00	93.98	186.20
13	13	13.20	0.00	93.25	186.16
13	14	14.30	0.00	111.76	73.38
14	14	14.30	-0.30	111.09	73.35
14	15	15.40	7.36	140.70	-72.10
15	15	15.40	0.00	142.23	-72.12
15	16	16.50	0.00	224.69	-249.24
16	16	16.50	0.00	224.20	-249.10
16	17	17.60	0.00	261.14	-512.66
17	17	17.60	-0.01	260.29	-512.36
17	18	18.70	-0.01	322.32	-833.02
18	18	18.70	0.00	321.54	-832.41
18	19	19.80	0.00	387.55	-1220.45
19	19	19.80	0.00	386.90	-1219.67
19	20	20.90	0.00	470.77	-1699.40
20	20	20.90	0.00	470.41	-1699.37
20	21	22.00	0.00	538.46	-2252.69
21	1021	22.00	0.00	-580.84	-2252.55
21	22	23.40	0.00	-510.62	-1495.84
22	22	23.40	0.00	-511.06	-1495.62
22	23	24.80	0.00	-423.67	-841.60
23	23	24.80	0.00	-421.79	-841.60
23	24	26.20	0.00	-313.40	-340.75
24	24	26.20	0.00	-313.31	-341.62
24	25	27.60	0.00	-237.82	43.17
25	25	27.60	0.00	-238.64	42.32
25	26	29.00	0.00	-120.64	254.39
26	26	29.00	5.58	-120.33	254.29

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	4.40	-92.50	404.50
27	27	30.40	0.00	-94.56	404.45
27	28	31.80	0.00	-61.41	509.62
28	28	31.80	0.00	-62.36	509.57
28	29	33.20	0.00	-38.82	580.38
29	29	33.20	0.00	-39.71	580.36
29	30	34.60	0.00	-14.29	617.82
30	30	34.60	0.00	-15.12	617.72
30	31	36.00	0.00	13.94	617.62
31	31	36.00	0.00	13.09	617.60
31	32	37.40	0.00	36.79	582.73
32	32	37.40	0.00	35.87	582.71
32	33	38.80	0.00	59.40	516.01
33	33	38.80	0.00	58.50	516.00
33	34	40.20	0.00	82.05	417.63
34	34	40.20	0.00	81.07	417.64
34	35	41.60	0.00	104.72	287.62
35	35	41.60	-0.13	103.78	287.63
35	36	43.00	5.05	138.51	115.98
36	36	43.00	0.00	138.70	116.09
36	37	44.40	0.00	247.80	-129.05
37	37	44.40	0.00	246.84	-128.36
37	38	45.80	0.00	322.64	-520.07
38	38	45.80	0.00	321.88	-519.03
38	39	47.20	0.00	404.20	-1021.55
39	39	47.20	0.00	402.95	-1021.00
39	40	48.60	0.00	510.73	-1663.70
40	40	48.60	0.00	510.19	-1663.73
40	41	50.00	0.00	584.42	-2424.85
41	1041	50.00	0.00	-584.42	-2424.85
41	42	51.40	0.00	-510.21	-1663.73
42	42	51.40	0.00	-510.73	-1663.70
42	43	52.80	0.00	-402.95	-1020.99
43	43	52.80	0.00	-404.20	-1021.54
43	44	54.20	0.00	-321.88	-519.01
44	44	54.20	0.00	-322.64	-520.07
44	45	55.60	0.00	-246.82	-128.32
45	45	55.60	0.00	-247.78	-129.00
45	46	57.00	0.00	-138.67	116.11
46	46	57.00	5.05	-138.52	115.98
46	47	58.40	-0.14	-103.79	287.64
47	47	58.40	0.00	-104.72	287.62
47	48	59.80	0.00	-81.07	417.65
48	48	59.80	0.00	-82.02	417.64
48	49	61.20	0.00	-58.47	515.99
49	49	61.20	0.01	-59.40	516.02
49	50	62.60	0.01	-35.87	582.72
50	50	62.60	0.00	-36.80	582.71
50	51	64.00	0.00	-13.10	617.59
51	51	64.00	0.00	-13.93	617.60
51	52	65.40	0.00	15.14	617.70

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	14.29	617.77
52	53	66.80	0.00	39.71	580.35
53	53	66.80	0.00	38.83	580.37
53	54	68.20	0.00	62.36	509.57
54	54	68.20	0.00	61.41	509.58
54	55	69.60	0.00	94.56	404.42
55	55	69.60	4.40	92.50	404.44
55	56	71.00	5.57	120.33	254.29
56	56	71.00	0.00	120.65	254.39
56	57	72.40	0.00	238.64	42.32
57	57	72.40	0.00	237.82	43.13
57	58	73.80	0.00	313.31	-341.65
58	58	73.80	0.00	313.41	-340.78
58	59	75.20	0.00	421.80	-841.60
59	59	75.20	0.00	423.66	-841.59
59	60	76.60	0.00	511.05	-1495.63
60	60	76.60	0.00	510.61	-1495.85
60	61	78.00	0.00	580.86	-2252.55
61	1061	78.00	0.00	-538.46	-2252.75
61	62	79.10	0.00	-470.41	-1699.41
62	62	79.10	0.00	-470.78	-1699.45
62	63	80.20	0.00	-386.91	-1219.71
63	63	80.20	0.00	-387.57	-1220.51
63	64	81.30	0.00	-321.55	-832.44
64	64	81.30	0.00	-322.33	-833.04
64	65	82.40	0.00	-260.30	-512.37
65	65	82.40	0.00	-261.14	-512.66
65	66	83.50	0.00	-224.20	-249.14
66	66	83.50	0.01	-224.69	-249.24
66	67	84.60	0.01	-142.23	-72.13
67	67	84.60	7.37	-140.70	-72.13
67	68	85.70	-0.30	-111.09	73.32
68	68	85.70	0.01	-111.75	73.35
68	69	86.80	0.01	-93.23	186.14
69	69	86.80	0.01	-93.98	186.17
69	70	87.90	0.01	-75.39	279.37
70	70	87.90	0.00	-76.10	279.43
70	71	89.00	0.00	-57.59	352.94
71	71	89.00	0.00	-58.29	352.98
71	72	90.10	0.00	-39.79	406.94
72	72	90.10	0.02	-40.43	406.95
72	73	91.20	0.02	-21.79	441.09
73	73	91.20	0.00	-22.48	441.17
73	74	92.30	0.00	-3.64	455.33
74	74	92.30	0.00	-4.16	455.36
74	75	93.40	0.00	14.33	449.78
75	75	93.40	0.00	13.81	449.82
75	76	94.50	0.00	32.30	424.42
76	76	94.50	0.01	31.85	424.47
76	77	95.60	0.01	50.35	379.25
77	77	95.60	0.00	49.89	379.27

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	68.36	314.23
78	78	96.70	0.00	67.93	314.24
78	79	97.80	0.00	86.42	229.36
79	79	97.80	0.00	85.97	229.37
79	80	98.90	0.00	104.47	124.58
80	80	98.90	0.00	104.05	124.61
80	81	100.00	0.00	316.28	-0.97
101	101	0.00	0.00	-306.96	-1.09
101	102	1.10	0.00	-101.36	121.55
102	102	1.10	0.00	-101.72	121.80
102	103	2.20	0.00	-83.53	223.68
103	103	2.20	0.00	-83.81	223.92
103	104	3.30	0.00	-65.68	306.09
104	104	3.30	0.00	-65.80	306.31
104	105	4.40	0.00	-47.69	368.76
105	105	4.40	0.00	-47.74	368.90
105	106	5.50	0.00	-29.59	411.42
106	106	5.50	0.00	-29.50	411.58
106	107	6.60	0.00	-11.33	434.04
107	107	6.60	0.00	-11.17	434.17
107	108	7.70	0.00	6.95	436.48
108	108	7.70	-0.01	7.17	436.61
108	109	8.80	-0.01	25.30	418.77
109	109	8.80	0.00	25.54	418.85
109	110	9.90	0.00	43.68	380.77
110	110	9.90	0.00	43.97	380.84
110	111	11.00	0.00	62.12	322.51
111	111	11.00	0.00	62.51	322.53
111	112	12.10	0.00	80.63	243.78
112	112	12.10	0.00	81.04	243.79
112	113	13.20	0.00	99.18	144.65
113	113	13.20	0.00	99.62	144.63
113	114	14.30	0.00	117.80	25.03
114	114	14.30	-0.30	118.38	24.98
114	115	15.40	7.37	147.92	-128.33
115	115	15.40	0.00	150.81	-128.46
115	116	16.50	0.00	223.51	-315.10
116	116	16.50	0.00	223.92	-315.27
116	117	17.60	0.00	258.97	-577.88
117	117	17.60	-0.01	259.19	-577.94
117	118	18.70	-0.01	332.84	-906.17
118	118	18.70	-0.01	333.28	-905.77
118	119	19.80	-0.01	413.75	-1314.75
119	119	19.80	0.00	414.83	-1314.43
119	120	20.90	0.00	516.21	-1837.47
120	120	20.90	0.00	517.70	-1837.39
120	121	22.00	0.00	580.67	-2436.36
121	1121	22.00	0.00	-620.50	-2436.34
121	122	23.40	0.00	-544.38	-1626.32
122	122	23.40	0.00	-542.42	-1626.46
122	123	24.80	0.00	-451.00	-932.50

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-448.75	-932.51
123	124	26.20	0.00	-325.55	-405.74
124	124	26.20	0.00	-324.96	-406.39
124	125	27.60	0.00	-244.09	-10.91
125	125	27.60	0.00	-243.97	-11.44
125	126	29.00	0.00	-126.87	216.27
126	126	29.00	5.58	-124.78	216.38
126	127	30.40	4.40	-98.19	373.84
127	127	30.40	0.00	-98.56	373.91
127	128	31.80	0.00	-65.77	484.82
128	128	31.80	0.00	-64.99	484.90
128	129	33.20	0.00	-41.91	559.75
129	129	33.20	0.00	-41.22	559.79
129	130	34.60	0.00	-16.40	600.07
130	130	34.60	0.00	-15.67	600.02
130	131	36.00	0.00	14.08	600.33
131	131	36.00	0.00	14.80	600.35
131	132	37.40	0.00	37.94	563.44
132	132	37.40	0.00	38.66	563.45
132	133	38.80	0.00	61.75	493.15
133	133	38.80	0.00	62.52	493.13
133	134	40.20	0.00	85.65	389.41
134	134	40.20	0.00	86.40	389.37
134	135	41.60	0.00	109.70	252.13
135	135	41.60	-0.13	110.49	252.07
135	136	43.00	5.05	144.24	71.48
136	136	43.00	0.00	146.37	71.40
136	137	44.40	0.00	251.80	-188.20
137	137	44.40	0.00	252.10	-187.84
137	138	45.80	0.00	333.40	-590.36
138	138	45.80	0.00	333.69	-589.56
138	139	47.20	0.00	426.22	-1116.21
139	139	47.20	0.00	427.10	-1115.91
139	140	48.60	0.00	543.41	-1802.30
140	140	48.60	0.00	545.39	-1802.15
140	141	50.00	0.00	625.77	-2619.00
141	1141	50.00	0.00	-625.78	-2619.00
141	142	51.40	0.00	-545.38	-1802.13
142	142	51.40	0.00	-543.41	-1802.27
142	143	52.80	0.00	-427.10	-1115.88
143	143	52.80	0.00	-426.22	-1116.18
143	144	54.20	0.00	-333.67	-589.58
144	144	54.20	0.00	-333.41	-590.35
144	145	55.60	0.00	-252.11	-187.80
145	145	55.60	0.00	-251.80	-188.15
145	146	57.00	0.00	-146.37	71.41
146	146	57.00	5.05	-144.25	71.48
146	147	58.40	-0.13	-110.50	252.05
147	147	58.40	0.00	-109.70	252.14
147	148	59.80	0.00	-86.40	389.34
148	148	59.80	0.00	-85.65	389.42

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-62.52	493.12
149	149	61.20	0.00	-61.75	493.11
149	150	62.60	0.00	-38.66	563.42
150	150	62.60	0.00	-37.94	563.43
150	151	64.00	0.00	-14.80	600.31
151	151	64.00	0.00	-14.08	600.29
151	152	65.40	0.00	15.67	600.00
152	152	65.40	0.00	16.40	600.05
152	153	66.80	0.00	41.21	559.74
153	153	66.80	0.00	41.91	559.71
153	154	68.20	0.00	64.99	484.83
154	154	68.20	0.00	65.77	484.78
154	155	69.60	0.00	98.56	373.86
155	155	69.60	4.40	98.16	373.78
155	156	71.00	5.57	124.76	216.37
156	156	71.00	0.00	126.88	216.25
156	157	72.40	0.00	243.99	-11.46
157	157	72.40	0.00	244.10	-10.93
157	158	73.80	0.00	324.97	-406.42
158	158	73.80	0.01	325.56	-405.76
158	159	75.20	0.01	448.77	-932.52
159	159	75.20	0.00	450.98	-932.51
159	160	76.60	0.00	542.43	-1626.45
160	160	76.60	0.00	544.38	-1626.35
160	161	78.00	0.00	620.51	-2436.39
161	1161	78.00	0.00	-580.68	-2436.40
161	162	79.10	0.00	-517.73	-1837.44
162	162	79.10	0.00	-516.19	-1837.55
162	163	80.20	0.00	-414.84	-1314.47
163	163	80.20	0.00	-413.74	-1314.78
163	164	81.30	0.00	-333.27	-905.79
164	164	81.30	0.00	-332.84	-906.19
164	165	82.40	0.00	-259.20	-577.96
165	165	82.40	0.00	-258.96	-577.91
165	166	83.50	0.00	-223.91	-315.33
166	166	83.50	0.01	-223.52	-315.16
166	167	84.60	0.01	-150.82	-128.45
167	167	84.60	7.37	-147.91	-128.36
167	168	85.70	-0.30	-118.38	24.93
168	168	85.70	0.00	-117.83	24.98
168	169	86.80	0.00	-99.65	144.60
169	169	86.80	0.00	-99.19	144.63
169	170	87.90	0.00	-81.05	243.78
170	170	87.90	0.00	-80.64	243.76
170	171	89.00	0.00	-62.53	322.52
171	171	89.00	0.00	-62.16	322.49
171	172	90.10	0.00	-43.98	380.83
172	172	90.10	0.00	-43.66	380.75
172	173	91.20	0.00	-25.53	418.82
173	173	91.20	0.00	-25.32	418.73
173	174	92.30	0.00	-7.18	436.58

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTESG.Tinf.MZ-

C. Infrecuentes dominante GRAD Mz-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

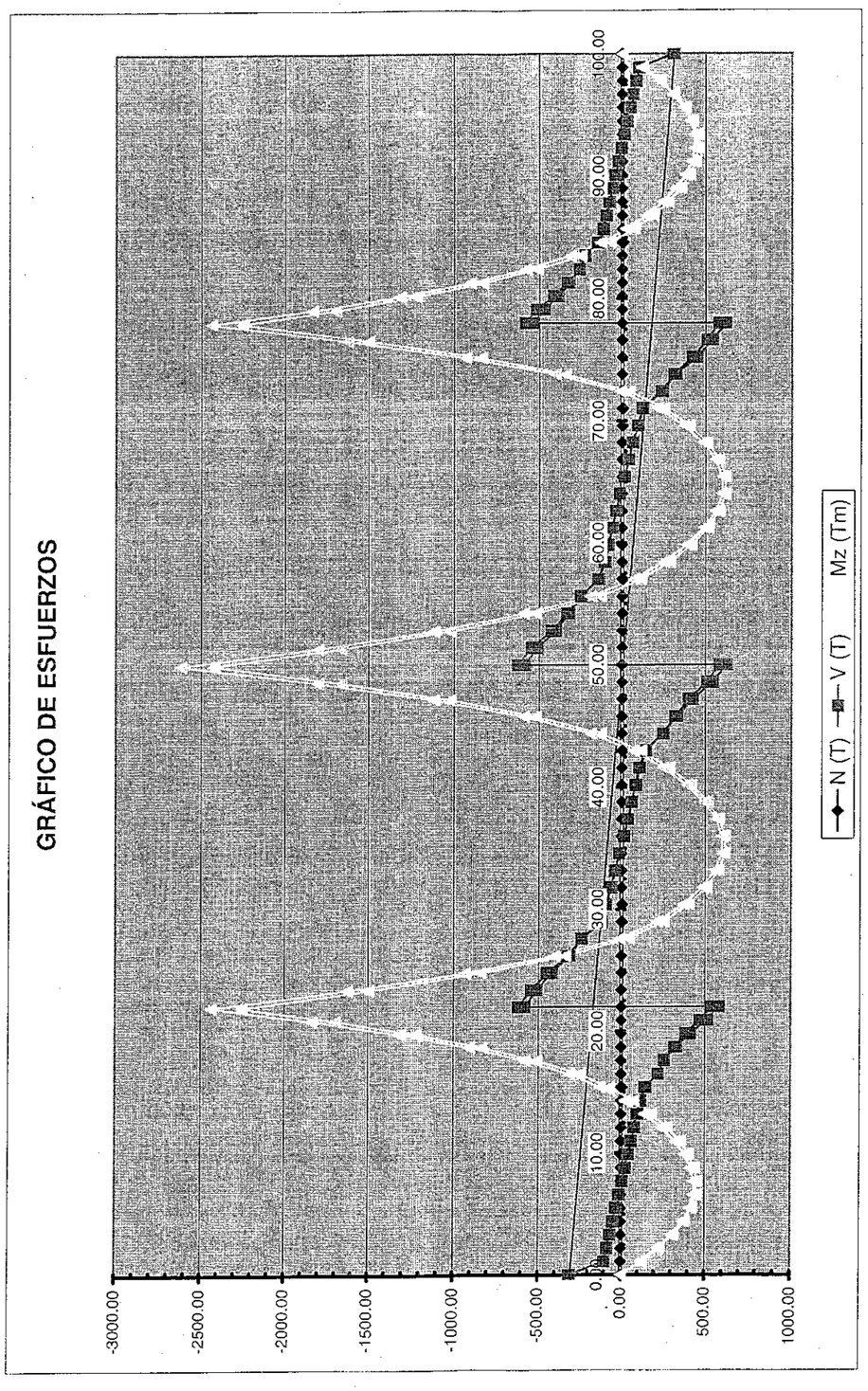
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-6.96	436.46
174	175	93.40	0.00	11.16	434.15
175	175	93.40	0.00	11.32	434.02
175	176	94.50	0.00	29.48	411.57
176	176	94.50	0.00	29.57	411.41
176	177	95.60	0.00	47.72	368.90
177	177	95.60	0.00	47.68	368.72
177	178	96.70	0.00	65.80	306.29
178	178	96.70	0.00	65.65	306.11
178	179	97.80	0.00	83.79	223.90
179	179	97.80	0.00	83.54	223.67
179	180	98.90	0.00	101.73	121.80
180	180	98.90	0.00	101.35	121.55
180	181	100.00	0.00	306.94	-1.09

05/09/03

Programa DINTEL PACADAR S.A.
INFRECUENTESG.Tinf.MZ-

rotura.esf.xls



MOMENTOS ÚLTIMOS DE LAS SECCIONES

SIN REFUERZOS

SECCIONES EN ROTURA

SECCION	PRET INF	PRET SUP	ANCHO LOSA	POST LOSA	ARM LOSA
A	20	4	14 m	---	Φ12 a 20 cm
B	34	4	14 m	---	Φ12 a 20 cm
C	44	4	14 m	---	Φ12 a 20 cm
D	54	4	14 m	---	Φ12 a 20 cm
E	54	4	14 m	---	Φ12 a 20 cm
F	70	4	14 m	---	Φ12 a 20 cm
G	44	4	14 m	42	Φ20 a 20 cm
H	34	4	14 m	84	Φ20 a 20 cm
I	20	4	14 m	84	Φ20 a 20 cm
J	22	4	14 m	84	Φ20 a 20 cm
K	36	4	14 m	84	Φ20 a 20 cm
L	36	4	14 m	42	Φ20 a 20 cm
M	54	4	14 m	42	Φ20 a 20 cm

MOMENTOS ÚLTIMOS DE LAS SECCIONES

SECCION	CAJON		SECCION TOTAL	
	Mu+	Mu-	Mu+	Mu-
A	763.7	-147.5	962.2	-794.1
B	1198.9	-140.3	1586.5	-776.8
C	1412.6	-133.6	2025.1	-765.4
D	1586.0	-128.6	2453.1	-757.3
E	1586.0	-128.6	2453.1	-757.3
F	1731.2	-122.8	3123.6	-746.1
G	1412.6	-133.6	2051.0	-2725.4
H	1198.9	-140.3	1620.1	-3086.0
I	763.8	-147.5	1015.6	-3316.3
J	836.7	-145.8	1104.1	-3283.2
K	1243.7	-139.2	1705.4	-3053.2
L	1243.8	-139.2	1705.4	-2850.7
M	1586.0	-128.6	2472.9	-2562.8

NOTAS: Los momentos últimos de las secciones se expresan en m·ton

Proyecto:
VTO TORRENTE DEL BO

Seccion:A

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	20.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1143.4	10.88	1093131.8
	(1)	609.7	18.98	1028315.1
	(2)	735.2	16.15	1050423.5
F.pura -	(0)	867.1	181.28	2519684.9
	(1)	359.7	154.23	2076724.5
	(2)	456.1	164.07	2232914.9
C.Simple	(0)	4921.7	61.07	24808539.2
	(1)	1444.9	61.19	7438473.1

	(2)	2072.6	61.14	10574363.2
T.Simple	(0)	107.6	63.24	757201.7
	(1)	107.6	63.24	757201.7
	(2)	107.6	63.24	757201.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: A

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 463.02Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 763.7 Xu(cm.): 60.8

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00195 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -147.5 Xu(cm.): 197.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00110 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 503.3 aplicado en Yo(cm)= 179.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: A

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 463.02Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 962.2 Xu(cm.): 14.2

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00071 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -794.1 Xu(cm.): 188.5

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00145 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 854.4 aplicado en Yo(cm)= 111.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:B

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	10.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1429.3	13.68	1784712.0
	(1)	761.1	23.99	1654824.5
	(2)	918.5	20.37	1699349.5
F.pura -	(0)	883.3	181.77	2529364.8
	(1)	374.8	156.72	2121259.5
	(2)	471.3	165.66	2261947.5
C.Simple	(0)	4940.5	61.62	25191828.5
	(1)	1463.7	63.02	7817667.0
	(2)	2091.4	62.42	10955303.7
T.Simple	(0)	126.4	84.18	1074917.0
	(1)	126.4	84.18	1074917.0
	(2)	126.4	84.18	1074917.0

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T┌tulo Secci├n: B

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 733.11Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1198.9 Xu(cm.): 84.6

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00809
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -140.3 Xu(cm.): 194.3

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00143 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 796.9 aplicado en Yo(cm)= 188.5

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: B

* PRESOLICITACIONES ELASTICAS
Análisis SIN FISURACION
Pretensado: 733.11Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1586.5 Xu(cm.): 17.9

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00091 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -776.8 Xu(cm.): 186.1

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00172 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1148.0 aplicado en Yo(cm)= 135.0

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:C

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_\Pi 1$	$J_\Pi 2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) Π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	20.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1601.6	15.35	2260124.5
	(1)	852.5	26.94	2076462.2
	(2)	1029.0	22.87	2139483.6
F.pura -	(0)	895.0	182.08	2535147.4
	(1)	385.8	158.31	2148640.4
	(2)	482.5	166.69	2279836.1
C.Simple	(0)	4954.0	62.00	25458331.6
	(1)	1477.1	64.29	8077204.9

	(2)	2104.8	63.32	11217794.7
T.Simple	(0)	139.9	95.56	1245367.7
	(1)	139.9	95.56	1245367.7
	(2)	139.9	95.56	1245367.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: C

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 926.03Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ψ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1412.6 Xu(cm.): 104.5

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00474
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -133.6 Xu(cm.): 192.6

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00164 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1006.6 aplicado en Yo(cm)= 191.4

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: C

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 926.03Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ψ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2025.1 Xu(cm.): 20.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00104 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -765.4 Xu(cm.): 184.1

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00194 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1357.7 aplicado en Yo(cm)= 145.4

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:D

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	J╓1	J╓2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) ╓(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	6.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1755.0	16.82	2712834.8
	(1)	934.2	29.51	2471234.9
	(2)	1127.5	25.06	2554135.2
F.pura -	(0)	907.0	182.34	2539324.0
	(1)	397.1	159.71	2170922.5
	(2)	493.9	167.58	2294133.0
T.Simple	(0)	4967.4	62.37	25712289.2
	(1)	1490.5	65.51	8321215.2
	(2)	2118.2	64.18	11465999.1
T.Simple	(0)	153.3	104.68	1378266.7
	(1)	153.3	104.68	1378266.7
	(2)	153.3	104.68	1378266.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T╒tulo Secci╞n: D

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╓*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1586.0 Xu(cm.): 123.0

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00289
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -128.6 Xu(cm.): 190.9

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00184 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1216.3 aplicado en Yo(cm)= 192.8

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: D

* PRESOLICITACIONES ELASTICAS
Análisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2453.1 Xu(cm.): 22.2

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00117 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -757.3 Xu(cm.): 181.6

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00218 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1567.4 aplicado en Yo(cm)= 152.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:E

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	6.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1755.0	16.82	2712834.8
	(1)	934.2	29.51	2471234.9
	(2)	1127.5	25.06	2554135.2
F.pura -	(0)	907.0	182.34	2539324.0
	(1)	397.1	159.71	2170922.5
	(2)	493.9	167.58	2294133.0
C.Simple	(0)	4967.4	62.37	25712289.2
	(1)	1490.5	65.51	8321215.2

	(2)	2118.2	64.18	11465999.1
T Simple	(0)	153.3	104.68	1378266.7
	(1)	153.3	104.68	1378266.7
	(2)	153.3	104.68	1378266.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: E

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Análisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1586.0 Xu(cm.): 123.0

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00289
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -128.6 Xu(cm.): 190.9

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00184 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1216.3 aplicado en Yo(cm)= 192.8

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)*

Título Sección: E

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2453.1 Xu(cm.): 22.2

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00117 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -757.3 Xu(cm.): 181.6

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00218 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1567.4 aplicado en Yo(cm)= 152.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
V) TORRENTE DEL BO

Seccion:F

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	J╥1	J╥2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) ╥(mm)	Yo(cm)	Mc	Nsr
	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	22.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1974.0	18.89	3407523.3
	(1)	1027.2	33.13	3065667.0
	(2)	1268.3	28.13	3182850.8
F.pura -	(0)	926.6	182.70	2544260.2
	(1)	415.6	161.66	2200302.5
	(2)	512.6	168.84	2312776.7
T.Simple	(0)	4988.9	62.95	26103983.4
	(1)	1512.0	67.39	8691205.7
	(2)	2139.7	65.52	11845073.9
T.Simple	(0)	174.8	116.12	1541234.2
	(1)	174.8	116.12	1541234.2
	(2)	174.8	116.12	1541234.2

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T╒tulo Secci╞n: F

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1427.64Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1731.2 Xu(cm.): 141.3

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00160
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -122.8 Xu(cm.): 187.8

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00220 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1551.8 aplicado en Yo(cm)= 193.9

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Seccion: F

PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1427.64Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 3123.6 Xu(cm.): 25.1

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00135 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -746.1 Xu(cm.): 176.9

Nu(Tn.): -.4 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00261 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7449.9 aplicado en Yo(cm)= 70.1

TRACCION SIMPLE(Rigido/Plastico):

N Tn.): 1902.9 aplicado en Yo(cm)= 160.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:G

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	20.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	42.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1782.1	15.24	2273754.1
	(1)	980.3	24.57	2114444.3
	(2)	1166.6	21.51	2164560.1
F.pura -	(0)	1236.1	154.56	7008183.3
	(1)	644.5	113.39	4854378.9
	(2)	763.2	126.28	5515966.6
C.Simple	(0)	5144.4	60.24	25888072.0
	(1)	1667.6	58.59	8511363.0

	(2)	2295.3	59.26	11649940.4
T imple	(0)	330.3	48.74	1790622.0
	(1)	330.3	48.74	1790622.0
	(2)	330.3	48.74	1790622.0

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Tftulo Secci├n: G

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1736.31Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

A lisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1412.6 Xu(cm.): 103.5

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00474
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -133.6 Xu(cm.): 192.3

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00164 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1006.6 aplicado en Yo(cm)= 191.4

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S. rciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Tftulo Secci├n: G

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1736.31Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2051.0 Xu(cm.): 22.8

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00132 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -2725.4 Xu(cm.): 90.7

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00226
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 2862.6 aplicado en Yo(cm)= 76.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VT TORRENTE DEL BO

Seccion:H

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	10.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1686.7	13.79	1798304.7
	(1)	944.0	21.57	1685206.9
	(2)	1115.3	19.09	1719672.0
F.pura -	(0)	1315.1	147.98	8024578.5
	(1)	702.3	103.65	5230978.5
	(2)	826.2	117.31	6074404.5
C.Simple	(0)	5187.4	59.37	25728836.8
	(1)	1710.5	56.01	8329991.8
	(2)	2338.2	57.36	11477407.5
T.Simple	(0)	373.3	38.05	1495246.3
	(1)	373.3	38.05	1495246.3
	(2)	373.3	38.05	1495246.3

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Tπtulo Secciπn: H

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2353.67Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1198.9 Xu(cm.): 82.9

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00809
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -140.3 Xu(cm.): 193.8

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00143 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 796.9 aplicado en Yo(cm)= 188.5

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: H

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2353.67Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1620.1 Xu(cm.): 24.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00151 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3086.0 Xu(cm.): 66.7

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00129
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3533.6 aplicado en Yo(cm)= 53.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:I

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	20.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1449.3	11.49	1109174.5
	(1)	821.2	17.64	1045403.2
	(2)	965.3	15.71	1064443.2
F.pura -	(0)	1300.7	147.17	7964402.4
	(1)	687.7	100.90	5035960.4
	(2)	811.9	115.30	5929393.3
C.Simple	(0)	5168.6	58.84	25333445.4
	(1)	1691.7	54.37	7912951.9

	(2)	2319.4	56.17	11069128.1
T Simple	(0)	354.5	29.25	949227.5
	(1)	354.5	29.25	949227.5
	(2)	354.5	29.25	949227.5

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: I

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2083.58Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 763.8 Xu(cm.): 58.6

Nu(Tn.): -.6 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00196 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -147.5 Xu(cm.): 196.6

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00110 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 503.3 aplicado en Yo(cm)= 179.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: I

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2083.58Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1015.6 Xu(cm.): 21.9

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00138 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3316.3 Xu(cm.): 70.4

Nu(Tn.): -.3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00146
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3240.0 aplicado en Yo(cm)= 40.0

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:J

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	J╥1	J╥2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) ╥(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	22.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1486.0	11.85	1212363.2
	(1)	840.1	18.25	1142094.7
	(2)	988.5	16.24	1163152.9
F.pura -	(0)	1302.7	147.29	7974215.8
	(1)	689.7	101.31	5066464.5
	(2)	813.9	115.60	5952238.3
C.Simple	(0)	5171.3	58.92	25392912.0
	(1)	1694.4	54.61	7975984.5
	(2)	2322.1	56.34	11130714.1
T.Simple	(0)	357.2	30.59	1034099.3
	(1)	357.2	30.59	1034099.3
	(2)	357.2	30.59	1034099.3

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T╒tulo Secci├n: J

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2122.16Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 836.7 Xu(cm.): 61.1

Nu(Tn.): -.4 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00216 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -145.8 Xu(cm.): 196.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00115 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 545.2 aplicado en Yo(cm)= 181.5

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: J

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2122.16Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1104.1 Xu(cm.): 22.2

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00139 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3283.2 Xu(cm.): 69.9

Nu(Tn.): -.3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00143
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3282.0 aplicado en Yo(cm)= 42.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:K

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	12.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1717.8	14.09	1893985.5
	(1)	960.2	22.08	1773060.5
	(2)	1135.0	19.52	1809990.0
F.pura -	(0)	1317.2	148.09	8032597.2
	(1)	704.4	104.03	5257214.6
	(2)	828.3	117.59	6093912.4
C.Simple	(0)	5190.1	59.45	25783969.0
	(1)	1713.2	56.24	8387678.8

	(2)	2340.9	57.52	11534064.6
T Simple	(0)	376.0	39.23	1567517.9
	(1)	376.0	39.23	1567517.9
	(2)	376.0	39.23	1567517.9

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: K

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2392.25Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Análisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1243.7 Xu(cm.): 86.8

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00723
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -139.2 Xu(cm.): 193.5

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00147 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 838.8 aplicado en Yo(cm)= 189.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: K

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2392.25Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1705.4 Xu(cm.): 24.4

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00153 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3053.2 Xu(cm.): 66.1

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00126
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3575.5 aplicado en Yo(cm)= 55.4

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:L

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	12.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	42.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

3.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
T:pura +	(0)	1659.5	14.07	1893957.3
	(1)	915.9	22.54	1769763.6
	(2)	1088.4	19.78	1808583.6
T.pura -	(0)	1227.6	154.14	6983095.4
	(1)	636.1	111.88	4767287.8
	(2)	754.9	125.20	5452377.9
T.Simple	(0)	5133.7	59.94	25669626.1
	(1)	1656.8	57.66	8286865.0
	(2)	2284.5	58.58	11427904.6
T.Simple	(0)	319.6	43.57	1527473.6
	(1)	319.6	43.57	1527473.6
	(2)	319.6	43.57	1527473.6

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: L

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1581.97Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1243.8 Xu(cm.): 87.7

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00723
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -139.2 Xu(cm.): 193.7

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00147 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 838.8 aplicado en Yo(cm)= 189.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: L

* RESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1581.97Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1705.8 Xu(cm.): 21.4

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00124 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -2850.7 Xu(cm.): 92.9

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00240
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 2694.8 aplicado en Yo(cm)= 68.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:M

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	6.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	0.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	42.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1922.5	16.57	2727336.6
	(1)	1054.6	26.86	2520880.9
	(2)	1256.4	23.47	2586206.0
F.pura -	(0)	1246.9	155.05	7035301.4
	(1)	655.3	115.16	4952393.3
	(2)	773.8	127.56	5587128.0
C.Simple	(0)	5157.9	60.60	26148602.3
	(1)	1681.0	59.72	8776632.2

	(2)	2308.7	60.07	11913289.5
Simple	(0)	343.8	54.64	2084700.6
	(1)	343.8	54.64	2084700.6
	(2)	343.8	54.64	2084700.6

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: M

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1929.24Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1586.0 Xu(cm.): 122.1

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00289
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -128.6 Xu(cm.): 190.7

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00184 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3290.8 aplicado en Yo(cm)= 138.7

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1216.3 aplicado en Yo(cm)= 192.8

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
Sparciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: M

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1929.24Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2472.9 Xu(cm.): 24.3

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00142 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -2562.8 Xu(cm.): 88.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00210
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8074.1 aplicado en Yo(cm)= 65.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3072.3 aplicado en Yo(cm)= 85.0

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
Sparciales resistentes: Rcu(Kg/cm):

ENVOLVENTE DE ROTURA A FLEXIÓN

SIN REFUERZOS

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 1.MZ

Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
1	2	1.10	A	C	763.70	66.02	-0.70	-147.50	48.90	2.90
2	2	1.10	A	C	763.70	66.02	-0.70	-147.50	48.90	2.90
2	3	2.20	A	C	763.70	123.94	0.40	-147.50	91.81	4.00
3	3	2.20	B	C	1198.90	123.94	0.40	-140.30	91.81	4.00
3	4	3.30	B	C	1198.90	175.20	1.50	-140.30	129.78	5.10
4	4	3.30	B	C	1198.90	175.20	1.50	-140.30	129.78	5.10
4	5	4.40	B	C	1198.90	219.79	2.60	-140.30	162.81	6.20
5	5	4.40	C	C	1412.60	219.79	2.60	-133.60	162.81	6.20
5	6	5.50	C	C	1412.60	257.73	3.70	-133.60	190.91	7.30
6	6	5.50	C	C	1412.60	257.73	3.70	-133.60	190.91	7.30
6	7	6.60	C	C	1412.60	289.01	4.80	-133.60	214.08	8.40
7	7	6.60	D	C	1524.20	289.01	4.80	-129.70	214.08	8.40
7	8	7.70	D	C	1524.20	313.61	5.90	-129.70	232.30	9.50
8	8	7.70	D	C	1524.20	313.61	5.90	-129.70	232.30	9.50
8	9	8.80	D	C	1524.20	331.53	7.00	-129.70	245.58	10.60
9	9	8.80	D	C	1524.20	331.53	7.00	-129.70	245.58	10.60
9	10	9.90	D	C	1524.20	342.81	8.10	-129.70	253.93	11.70
10	10	9.90	D	C	1524.20	342.81	8.10	-129.70	253.93	11.70
10	11	11.00	D	C	1524.20	347.41	9.20	-129.70	257.34	12.80
11	11	11.00	D	C	1524.20	347.41	12.80	-129.70	257.34	9.20
11	12	12.10	D	C	1524.20	345.36	13.90	-129.70	255.82	10.30
12	12	12.10	D	C	1524.20	345.36	13.90	-129.70	255.82	10.30
12	13	13.20	D	C	1524.20	336.62	15.00	-129.70	249.35	11.40
13	13	13.20	D	C	1524.20	336.62	15.00	-129.70	249.35	11.40
13	14	14.30	D	C	1524.20	321.26	16.10	-129.70	237.97	12.50
14	14	14.30	C	C	1412.60	321.26	16.10	-133.60	237.97	12.50
14	15	15.40	C	C	1412.60	299.21	17.20	-133.60	221.64	13.60
15	15	15.40	G	C	1412.60	299.21	17.20	-133.60	221.64	13.60
15	16	16.50	G	C	1412.60	266.76	18.30	-133.60	197.60	14.70
16	16	16.50	H	C	1412.60	266.76	18.30	-133.60	197.60	14.70
16	17	17.60	H	C	1412.60	220.24	19.40	-133.60	163.14	15.80
17	17	17.60	I	C	1198.90	220.24	19.40	-140.30	163.14	15.80
17	18	18.70	I	C	1198.90	163.25	20.50	-140.30	114.59	16.90
18	18	18.70	I	C	1198.90	163.25	20.50	-140.30	114.59	16.90
18	19	19.80	I	C	1198.90	94.99	21.60	-140.30	52.81	18.00
19	19	19.80	J	C	763.80	94.99	21.60	-147.50	52.81	18.00
19	20	20.90	J	C	763.80	14.52	22.70	-147.50	-21.38	19.10
20	20	20.90	J	C	763.80	14.52	22.70	-147.50	-21.38	19.10
20	21	22.00	J	C	763.80	-82.18	23.80	-147.50	-110.94	20.20
21	1021	22.00	N	C	836.70	-82.18	20.20	-145.80	-110.94	23.80
21	22	23.40	N	C	836.70	66.30	21.60	-145.80	23.00	25.20
22	22	23.40	N	C	836.70	66.30	21.60	-145.80	23.00	25.20
22	23	24.80	N	C	836.70	188.48	23.00	-145.80	132.02	26.60
23	23	24.80	O	C	1243.70	188.48	23.00	-139.20	132.02	26.60
23	24	26.20	O	C	1243.70	294.06	24.40	-139.20	217.82	28.00
24	24	26.20	O	C	1243.70	294.06	24.40	-139.20	217.82	28.00
24	25	27.60	O	C	1243.70	381.19	25.80	-139.20	282.36	29.40
25	25	27.60	K	C	1586.00	381.19	25.80	-128.60	282.36	29.40
25	26	29.00	K	C	1586.00	445.47	27.20	-128.60	329.98	30.80
26	26	29.00	E	C	1586.00	445.47	27.20	-128.60	329.98	30.80
26	27	30.40	E	C	1586.00	492.95	28.60	-128.60	365.15	32.20
27	27	30.40	F	C	1699.40	492.95	28.60	-124.50	365.15	32.20
27	28	31.80	F	C	1699.40	529.61	30.00	-124.50	392.30	33.60
28	28	31.80	F	C	1699.40	529.61	30.00	-124.50	392.30	33.60
28	29	33.20	F	C	1699.40	555.50	31.40	-124.50	411.48	35.00
29	29	33.20	F	C	1699.40	555.50	31.40	-124.50	411.48	35.00
29	30	34.60	F	C	1699.40	570.58	32.80	-124.50	422.65	36.40
30	30	34.60	F	C	1699.40	570.58	32.80	-124.50	422.65	36.40
30	31	36.00	F	C	1699.40	574.87	34.20	-124.50	425.83	37.80
31	31	36.00	F	C	1699.40	574.87	37.80	-124.50	425.83	34.20
31	32	37.40	F	C	1699.40	568.36	39.20	-124.50	421.01	35.60

CÁLCULO EN ROTURA

Hipótesis de cálculo:

NVOLOVENTE FASE 1.MZ

Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	C	1699.40	568.36	39.20	-124.50	421.01	35.60
32	33	38.80	F	C	1699.40	551.07	40.60	-124.50	408.20	37.00
33	33	38.80	F	C	1699.40	551.07	40.60	-124.50	408.20	37.00
33	34	40.20	F	C	1699.40	522.96	42.00	-124.50	387.38	38.40
34	34	40.20	F	C	1699.40	522.96	42.00	-124.50	387.38	38.40
34	35	41.60	F	C	1699.40	484.08	43.40	-124.50	358.58	39.80
35	35	41.60	E	C	1586.00	484.08	43.40	-128.60	358.58	39.80
35	36	43.00	E	C	1586.00	434.39	44.80	-128.60	321.77	41.20
36	36	43.00	K	C	1586.00	434.39	44.80	-128.60	321.77	41.20
36	37	44.40	K	C	1586.00	367.89	46.20	-128.60	272.51	42.60
37	37	44.40	L	C	1243.70	367.89	46.20	-139.20	272.51	42.60
37	38	45.80	L	C	1243.70	279.42	47.60	-139.20	205.46	44.00
38	38	45.80	L	C	1243.70	279.42	47.60	-139.20	205.46	44.00
38	39	47.20	L	C	1243.70	175.35	49.00	-139.20	114.29	45.40
39	39	47.20	M	C	836.70	175.35	49.00	-145.80	114.29	45.40
39	40	48.60	M	C	836.70	51.53	50.40	-145.80	3.06	46.80
40	40	48.60	M	C	836.70	51.53	50.40	-145.80	3.06	46.80
40	41	50.00	M	C	836.70	-98.59	51.80	-145.80	-133.10	48.20
41	1041	50.00	M	C	836.70	-98.59	48.20	-145.80	-133.10	51.80
41	42	51.40	M	C	836.70	51.53	49.60	-145.80	3.06	53.20
42	42	51.40	M	C	836.70	51.53	49.60	-145.80	3.06	53.20
42	43	52.80	M	C	836.70	175.35	51.00	-145.80	114.29	54.60
43	43	52.80	L	C	1243.70	175.35	51.00	-139.20	114.29	54.60
43	44	54.20	L	C	1243.70	279.42	52.40	-139.20	205.46	56.00
44	44	54.20	L	C	1243.70	279.42	52.40	-139.20	205.46	56.00
44	45	55.60	L	C	1243.70	367.89	53.80	-139.20	272.51	57.40
45	45	55.60	K	C	1586.00	367.89	53.80	-128.60	272.51	57.40
45	46	57.00	K	C	1586.00	434.39	55.20	-128.60	321.77	58.80
46	46	57.00	E	C	1586.00	434.39	55.20	-128.60	321.77	58.80
46	47	58.40	E	C	1586.00	484.08	56.60	-128.60	358.58	60.20
47	47	58.40	F	C	1699.40	484.08	56.60	-124.50	358.58	60.20
47	48	59.80	F	C	1699.40	522.96	58.00	-124.50	387.38	61.60
48	48	59.80	F	C	1699.40	522.96	58.00	-124.50	387.38	61.60
48	49	61.20	F	C	1699.40	551.07	59.40	-124.50	408.20	63.00
49	49	61.20	F	C	1699.40	551.07	59.40	-124.50	408.20	63.00
49	50	62.60	F	C	1699.40	568.36	60.80	-124.50	421.01	64.40
50	50	62.60	F	C	1699.40	568.36	60.80	-124.50	421.01	64.40
50	51	64.00	F	C	1699.40	574.87	62.20	-124.50	425.83	65.80
51	51	64.00	F	C	1699.40	574.87	65.80	-124.50	425.83	62.20
51	52	65.40	F	C	1699.40	570.58	67.20	-124.50	422.65	63.60
52	52	65.40	F	C	1699.40	570.58	67.20	-124.50	422.65	63.60
52	53	66.80	F	C	1699.40	555.50	68.60	-124.50	411.48	65.00
53	53	66.80	F	C	1699.40	555.50	68.60	-124.50	411.48	65.00
53	54	68.20	F	C	1699.40	529.61	70.00	-124.50	392.30	66.40
54	54	68.20	F	C	1699.40	529.61	70.00	-124.50	392.30	66.40
54	55	69.60	F	C	1699.40	492.95	71.40	-124.50	365.15	67.80
55	55	69.60	E	C	1586.00	492.95	71.40	-128.60	365.15	67.80
55	56	71.00	E	C	1586.00	445.47	72.80	-128.60	329.98	69.20
56	56	71.00	K	C	1586.00	445.47	72.80	-128.60	329.98	69.20
56	57	72.40	K	C	1586.00	381.19	74.20	-128.60	282.36	70.60
57	57	72.40	O	C	1243.70	381.19	74.20	-139.20	282.36	70.60
57	58	73.80	O	C	1243.70	294.06	75.60	-139.20	217.82	72.00
58	58	73.80	O	C	1243.70	294.06	75.60	-139.20	217.82	72.00
58	59	75.20	O	C	1243.70	188.48	77.00	-139.20	132.02	73.40
59	59	75.20	N	C	836.70	188.48	77.00	-145.80	132.02	73.40
59	60	76.60	N	C	836.70	66.30	78.40	-145.80	23.00	74.80
60	60	76.60	N	C	836.70	66.30	78.40	-145.80	23.00	74.80
60	61	78.00	N	C	836.70	-82.18	79.80	-145.80	-110.94	76.20
61	1061	78.00	J	C	763.80	-82.18	76.20	-147.50	-110.94	79.80
61	62	79.10	J	C	763.80	14.52	77.30	-147.50	-21.38	80.90
62	62	79.10	J	C	763.80	14.52	77.30	-147.50	-21.38	80.90
62	63	80.20	J	C	763.80	94.99	78.40	-147.50	52.81	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 1.MZ

Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	I	C	1198.90	94.99	78.40	-140.30	52.81	82.00
63	64	81.30	I	C	1198.90	163.25	79.50	-140.30	114.59	83.10
64	64	81.30	I	C	1198.90	163.25	79.50	-140.30	114.59	83.10
64	65	82.40	I	C	1198.90	220.24	80.60	-140.30	163.14	84.20
65	65	82.40	H	C	1412.60	220.24	80.60	-133.60	163.14	84.20
65	66	83.50	H	C	1412.60	266.76	81.70	-133.60	197.60	85.30
66	66	83.50	G	C	1412.60	266.76	81.70	-133.60	197.60	85.30
66	67	84.60	G	C	1412.60	299.21	82.80	-133.60	221.64	86.40
67	67	84.60	C	C	1412.60	299.21	82.80	-133.60	221.64	86.40
67	68	85.70	C	C	1412.60	321.26	83.90	-133.60	237.97	87.50
68	68	85.70	D	C	1524.20	321.26	83.90	-129.70	237.97	87.50
68	69	86.80	D	C	1524.20	336.62	85.00	-129.70	249.35	88.60
69	69	86.80	D	C	1524.20	336.62	85.00	-129.70	249.35	88.60
69	70	87.90	D	C	1524.20	345.36	86.10	-129.70	255.82	89.70
70	70	87.90	D	C	1524.20	345.36	86.10	-129.70	255.82	89.70
70	71	89.00	D	C	1524.20	347.41	87.20	-129.70	257.34	90.80
71	71	89.00	D	C	1524.20	347.41	90.80	-129.70	257.34	87.20
71	72	90.10	D	C	1524.20	342.81	91.90	-129.70	253.93	88.30
72	72	90.10	D	C	1524.20	342.81	91.90	-129.70	253.93	88.30
72	73	91.20	D	C	1524.20	331.53	93.00	-129.70	245.58	89.40
73	73	91.20	D	C	1524.20	331.53	93.00	-129.70	245.58	89.40
73	74	92.30	D	C	1524.20	313.61	94.10	-129.70	232.30	90.50
74	74	92.30	D	C	1524.20	313.61	94.10	-129.70	232.30	90.50
74	75	93.40	D	C	1524.20	289.01	95.20	-129.70	214.08	91.60
75	75	93.40	C	C	1412.60	289.01	95.20	-133.60	214.08	91.60
75	76	94.50	C	C	1412.60	257.73	96.30	-133.60	190.91	92.70
76	76	94.50	C	C	1412.60	257.73	96.30	-133.60	190.91	92.70
76	77	95.60	C	C	1412.60	219.79	97.40	-133.60	162.81	93.80
77	77	95.60	B	C	1198.90	219.79	97.40	-140.30	162.81	93.80
77	78	96.70	B	C	1198.90	175.20	98.50	-140.30	129.78	94.90
78	78	96.70	B	C	1198.90	175.20	98.50	-140.30	129.78	94.90
78	79	97.80	B	C	1198.90	123.94	99.60	-140.30	91.81	96.00
79	79	97.80	A	C	763.70	123.94	99.60	-147.50	91.81	96.00
79	80	98.90	A	C	763.70	66.02	100.70	-147.50	48.90	97.10
80	80	98.90	A	C	763.70	66.02	100.70	-147.50	48.90	97.10
80	81	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20
101	101	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
101	102	1.10	A	C	763.70	66.02	-0.70	-147.50	48.90	2.90
102	102	1.10	A	C	763.70	66.02	-0.70	-147.50	48.90	2.90
102	103	2.20	A	C	763.70	123.94	0.40	-147.50	91.81	4.00
103	103	2.20	B	C	1198.90	123.94	0.40	-140.30	91.81	4.00
103	104	3.30	B	C	1198.90	175.20	1.50	-140.30	129.78	5.10
104	104	3.30	B	C	1198.90	175.20	1.50	-140.30	129.78	5.10
104	105	4.40	B	C	1198.90	219.79	2.60	-140.30	162.81	6.20
105	105	4.40	C	C	1412.60	219.79	2.60	-133.60	162.81	6.20
105	106	5.50	C	C	1412.60	257.73	3.70	-133.60	190.91	7.30
106	106	5.50	C	C	1412.60	257.73	3.70	-133.60	190.91	7.30
106	107	6.60	C	C	1412.60	289.01	4.80	-133.60	214.08	8.40
107	107	6.60	D	C	1524.20	289.01	4.80	-129.70	214.08	8.40
107	108	7.70	D	C	1524.20	313.61	5.90	-129.70	232.30	9.50
108	108	7.70	D	C	1524.20	313.61	5.90	-129.70	232.30	9.50
108	109	8.80	D	C	1524.20	331.53	7.00	-129.70	245.58	10.60
109	109	8.80	D	C	1524.20	331.53	7.00	-129.70	245.58	10.60
109	110	9.90	D	C	1524.20	342.81	8.10	-129.70	253.93	11.70
110	110	9.90	D	C	1524.20	342.81	8.10	-129.70	253.93	11.70
110	111	11.00	D	C	1524.20	347.41	9.20	-129.70	257.34	12.80
111	111	11.00	D	C	1524.20	347.41	12.80	-129.70	257.34	9.20
111	112	12.10	D	C	1524.20	345.36	13.90	-129.70	255.82	10.30
112	112	12.10	D	C	1524.20	345.36	13.90	-129.70	255.82	10.30
112	113	13.20	D	C	1524.20	336.62	15.00	-129.70	249.35	11.40
113	113	13.20	D	C	1524.20	336.62	15.00	-129.70	249.35	11.40
113	114	14.30	D	C	1524.20	321.26	16.10	-129.70	237.97	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 1.MZ

Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	C	1412.60	321.26	16.10	-133.60	237.97	12.50
114	115	15.40	C	C	1412.60	299.21	17.20	-133.60	221.64	13.60
115	115	15.40	G	C	1412.60	299.21	17.20	-133.60	221.64	13.60
115	116	16.50	G	C	1412.60	266.76	18.30	-133.60	197.60	14.70
116	116	16.50	H	C	1412.60	266.76	18.30	-133.60	197.60	14.70
116	117	17.60	H	C	1412.60	220.24	19.40	-133.60	163.14	15.80
117	117	17.60	I	C	1198.90	220.24	19.40	-140.30	163.14	15.80
117	118	18.70	I	C	1198.90	163.25	20.50	-140.30	114.59	16.90
118	118	18.70	I	C	1198.90	163.25	20.50	-140.30	114.59	16.90
118	119	19.80	I	C	1198.90	94.99	21.60	-140.30	52.81	18.00
119	119	19.80	J	C	763.80	94.99	21.60	-147.50	52.81	18.00
119	120	20.90	J	C	763.80	14.52	22.70	-147.50	-21.38	19.10
120	120	20.90	J	C	763.80	14.52	22.70	-147.50	-21.38	19.10
120	121	22.00	J	C	763.80	-82.18	23.80	-147.50	-110.94	20.20
121	1121	22.00	N	C	836.70	-82.18	20.20	-145.80	-110.94	23.80
121	122	23.40	N	C	836.70	66.30	21.60	-145.80	23.00	25.20
122	122	23.40	N	C	836.70	66.30	21.60	-145.80	23.00	25.20
122	123	24.80	N	C	836.70	188.48	23.00	-145.80	132.02	26.60
123	123	24.80	O	C	1243.70	188.48	23.00	-139.20	132.02	26.60
123	124	26.20	O	C	1243.70	294.06	24.40	-139.20	217.82	28.00
124	124	26.20	O	C	1243.70	294.06	24.40	-139.20	217.82	28.00
124	125	27.60	O	C	1243.70	381.19	25.80	-139.20	282.36	29.40
125	125	27.60	K	C	1586.00	381.19	25.80	-128.60	282.36	29.40
125	126	29.00	K	C	1586.00	445.47	27.20	-128.60	329.98	30.80
126	126	29.00	E	C	1586.00	445.47	27.20	-128.60	329.98	30.80
126	127	30.40	E	C	1586.00	492.95	28.60	-128.60	365.15	32.20
127	127	30.40	F	C	1699.40	492.95	28.60	-124.50	365.15	32.20
127	128	31.80	F	C	1699.40	529.61	30.00	-124.50	392.30	33.60
128	128	31.80	F	C	1699.40	529.61	30.00	-124.50	392.30	33.60
128	129	33.20	F	C	1699.40	555.50	31.40	-124.50	411.48	35.00
129	129	33.20	F	C	1699.40	555.50	31.40	-124.50	411.48	35.00
129	130	34.60	F	C	1699.40	570.58	32.80	-124.50	422.65	36.40
130	130	34.60	F	C	1699.40	570.58	32.80	-124.50	422.65	36.40
130	131	36.00	F	C	1699.40	574.87	34.20	-124.50	425.83	37.80
131	131	36.00	F	C	1699.40	574.87	37.80	-124.50	425.83	34.20
131	132	37.40	F	C	1699.40	568.36	39.20	-124.50	421.01	35.60
132	132	37.40	F	C	1699.40	568.36	39.20	-124.50	421.01	35.60
132	133	38.80	F	C	1699.40	551.07	40.60	-124.50	408.20	37.00
133	133	38.80	F	C	1699.40	551.07	40.60	-124.50	408.20	37.00
133	134	40.20	F	C	1699.40	522.96	42.00	-124.50	387.38	38.40
134	134	40.20	F	C	1699.40	522.96	42.00	-124.50	387.38	38.40
134	135	41.60	F	C	1699.40	484.08	43.40	-124.50	358.58	39.80
135	135	41.60	E	C	1586.00	484.08	43.40	-128.60	358.58	39.80
135	136	43.00	E	C	1586.00	434.39	44.80	-128.60	321.77	41.20
136	136	43.00	K	C	1586.00	434.39	44.80	-128.60	321.77	41.20
136	137	44.40	K	C	1586.00	367.89	46.20	-128.60	272.51	42.60
137	137	44.40	L	C	1243.70	367.89	46.20	-139.20	272.51	42.60
137	138	45.80	L	C	1243.70	279.42	47.60	-139.20	205.46	44.00
138	138	45.80	L	C	1243.70	279.42	47.60	-139.20	205.46	44.00
138	139	47.20	L	C	1243.70	175.35	49.00	-139.20	114.29	45.40
139	139	47.20	M	C	836.70	175.35	49.00	-145.80	114.29	45.40
139	140	48.60	M	C	836.70	51.53	50.40	-145.80	3.06	46.80
140	140	48.60	M	C	836.70	51.53	50.40	-145.80	3.06	46.80
140	141	50.00	M	C	836.70	-98.59	51.80	-145.80	-133.10	48.20
141	1141	50.00	M	C	836.70	-98.59	48.20	-145.80	-133.10	51.80
141	142	51.40	M	C	836.70	51.53	49.60	-145.80	3.06	53.20
142	142	51.40	M	C	836.70	51.53	49.60	-145.80	3.06	53.20
142	143	52.80	M	C	836.70	175.35	51.00	-145.80	114.29	54.60
143	143	52.80	L	C	1243.70	175.35	51.00	-139.20	114.29	54.60
143	144	54.20	L	C	1243.70	279.42	52.40	-139.20	205.46	56.00
144	144	54.20	L	C	1243.70	279.42	52.40	-139.20	205.46	56.00
144	145	55.60	L	C	1243.70	367.89	53.80	-139.20	272.51	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 1.MZ

Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	K	C	1586.00	367.89	53.80	-128.60	272.51	57.40
145	146	57.00	K	C	1586.00	434.39	55.20	-128.60	321.77	58.80
146	146	57.00	E	C	1586.00	434.39	55.20	-128.60	321.77	58.80
146	147	58.40	E	C	1586.00	484.08	56.60	-128.60	358.58	60.20
147	147	58.40	F	C	1699.40	484.08	56.60	-124.50	358.58	60.20
147	148	59.80	F	C	1699.40	522.96	58.00	-124.50	387.38	61.60
148	148	59.80	F	C	1699.40	522.96	58.00	-124.50	387.38	61.60
148	149	61.20	F	C	1699.40	551.07	59.40	-124.50	408.20	63.00
149	149	61.20	F	C	1699.40	551.07	59.40	-124.50	408.20	63.00
149	150	62.60	F	C	1699.40	568.36	60.80	-124.50	421.01	64.40
150	150	62.60	F	C	1699.40	568.36	60.80	-124.50	421.01	64.40
150	151	64.00	F	C	1699.40	574.87	62.20	-124.50	425.83	65.80
151	151	64.00	F	C	1699.40	574.87	65.80	-124.50	425.83	62.20
151	152	65.40	F	C	1699.40	570.58	67.20	-124.50	422.65	63.60
152	152	65.40	F	C	1699.40	570.58	67.20	-124.50	422.65	63.60
152	153	66.80	F	C	1699.40	555.50	68.60	-124.50	411.48	65.00
153	153	66.80	F	C	1699.40	555.50	68.60	-124.50	411.48	65.00
153	154	68.20	F	C	1699.40	529.61	70.00	-124.50	392.30	66.40
154	154	68.20	F	C	1699.40	529.61	70.00	-124.50	392.30	66.40
154	155	69.60	F	C	1699.40	492.95	71.40	-124.50	365.15	67.80
155	155	69.60	E	C	1586.00	492.95	71.40	-128.60	365.15	67.80
155	156	71.00	E	C	1586.00	445.47	72.80	-128.60	329.98	69.20
156	156	71.00	K	C	1586.00	445.47	72.80	-128.60	329.98	69.20
156	157	72.40	K	C	1586.00	381.19	74.20	-128.60	282.36	70.60
157	157	72.40	O	C	1243.70	381.19	74.20	-139.20	282.36	70.60
157	158	73.80	O	C	1243.70	294.06	75.60	-139.20	217.82	72.00
158	158	73.80	O	C	1243.70	294.06	75.60	-139.20	217.82	72.00
158	159	75.20	O	C	1243.70	188.48	77.00	-139.20	132.02	73.40
159	159	75.20	N	C	836.70	188.48	77.00	-145.80	132.02	73.40
159	160	76.60	N	C	836.70	66.30	78.40	-145.80	23.00	74.80
160	160	76.60	N	C	836.70	66.30	78.40	-145.80	23.00	74.80
160	161	78.00	N	C	836.70	-82.18	79.80	-145.80	-110.94	76.20
161	1161	78.00	J	C	763.80	-82.18	76.20	-147.50	-110.94	79.80
161	162	79.10	J	C	763.80	14.52	77.30	-147.50	-21.38	80.90
162	162	79.10	J	C	763.80	14.52	77.30	-147.50	-21.38	80.90
162	163	80.20	J	C	763.80	94.99	78.40	-147.50	52.81	82.00
163	163	80.20	I	C	1198.90	94.99	78.40	-140.30	52.81	82.00
163	164	81.30	I	C	1198.90	163.25	79.50	-140.30	114.59	83.10
164	164	81.30	I	C	1198.90	163.25	79.50	-140.30	114.59	83.10
164	165	82.40	I	C	1198.90	220.24	80.60	-140.30	163.14	84.20
165	165	82.40	H	C	1412.60	220.24	80.60	-133.60	163.14	84.20
165	166	83.50	H	C	1412.60	266.76	81.70	-133.60	197.60	85.30
166	166	83.50	G	C	1412.60	266.76	81.70	-133.60	197.60	85.30
166	167	84.60	G	C	1412.60	299.21	82.80	-133.60	221.64	86.40
167	167	84.60	C	C	1412.60	299.21	82.80	-133.60	221.64	86.40
167	168	85.70	C	C	1412.60	321.26	83.90	-133.60	237.97	87.50
168	168	85.70	D	C	1524.20	321.26	83.90	-129.70	237.97	87.50
168	169	86.80	D	C	1524.20	336.62	85.00	-129.70	249.35	88.60
169	169	86.80	D	C	1524.20	336.62	85.00	-129.70	249.35	88.60
169	170	87.90	D	C	1524.20	345.36	86.10	-129.70	255.82	89.70
170	170	87.90	D	C	1524.20	345.36	86.10	-129.70	255.82	89.70
170	171	89.00	D	C	1524.20	347.41	87.20	-129.70	257.34	90.80
171	171	89.00	D	C	1524.20	347.41	90.80	-129.70	257.34	87.20
171	172	90.10	D	C	1524.20	342.81	91.90	-129.70	253.93	88.30
172	172	90.10	D	C	1524.20	342.81	91.90	-129.70	253.93	88.30
172	173	91.20	D	C	1524.20	331.53	93.00	-129.70	245.58	89.40
173	173	91.20	D	C	1524.20	331.53	93.00	-129.70	245.58	89.40
173	174	92.30	D	C	1524.20	313.61	94.10	-129.70	232.30	90.50
174	174	92.30	D	C	1524.20	313.61	94.10	-129.70	232.30	90.50
174	175	93.40	D	C	1524.20	289.01	95.20	-129.70	214.08	91.60
175	175	93.40	C	C	1412.60	289.01	95.20	-133.60	214.08	91.60
175	176	94.50	C	C	1412.60	257.73	96.30	-133.60	190.91	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 1.MZ

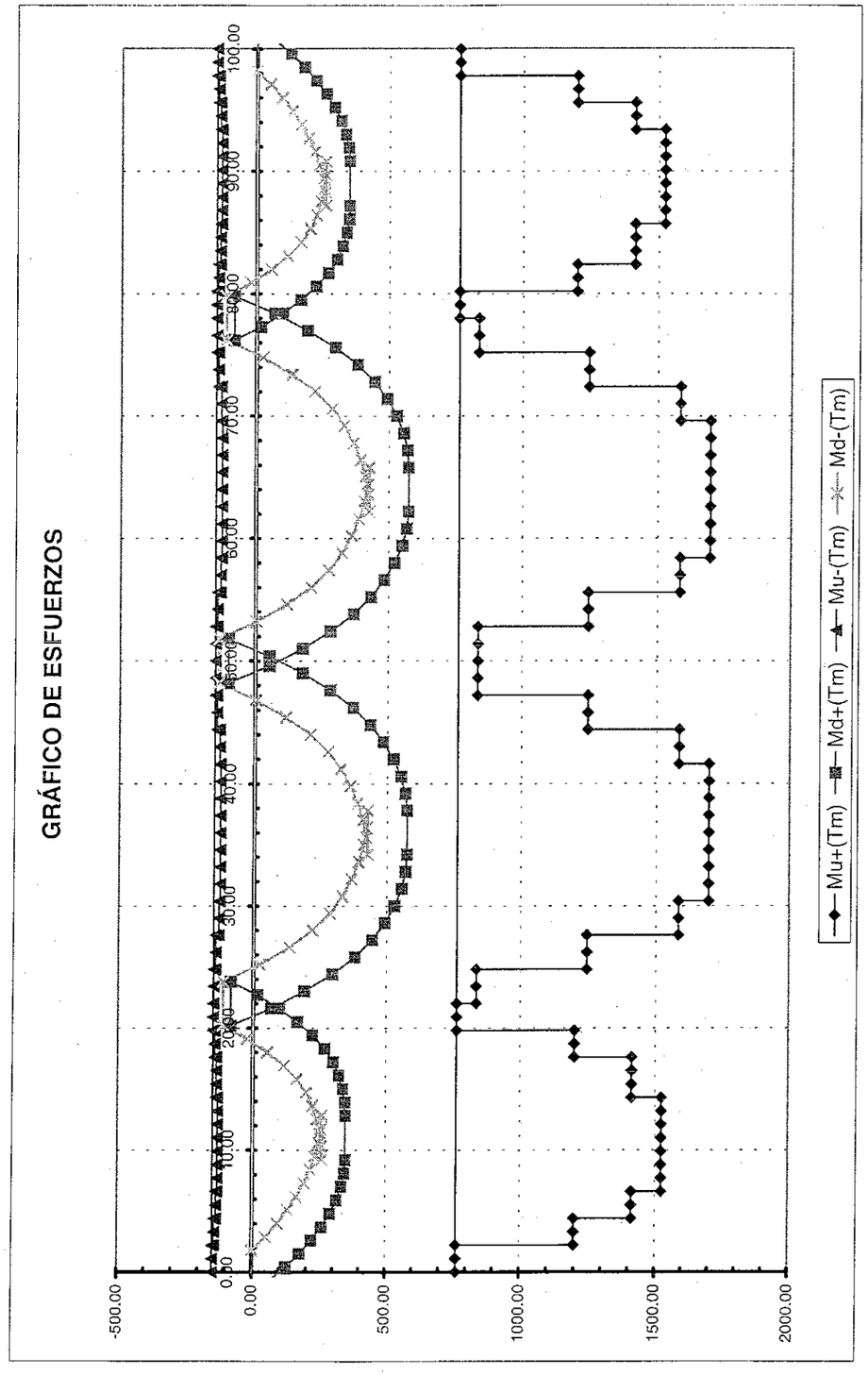
Construcción fase 1 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	C	1412.60	257.73	96.30	-133.60	190.91	92.70
176	177	95.60	C	C	1412.60	219.79	97.40	-133.60	162.81	93.80
177	177	95.60	B	C	1198.90	219.79	97.40	-140.30	162.81	93.80
177	178	96.70	B	C	1198.90	175.20	98.50	-140.30	129.78	94.90
178	178	96.70	B	C	1198.90	175.20	98.50	-140.30	129.78	94.90
178	179	97.80	B	C	1198.90	123.94	99.60	-140.30	91.81	96.00
179	179	97.80	A	C	763.70	123.94	99.60	-147.50	91.81	96.00
179	180	98.90	A	C	763.70	66.02	100.70	-147.50	48.90	97.10
180	180	98.90	A	C	763.70	66.02	100.70	-147.50	48.90	97.10
180	181	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20



CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
1	2	1.10	A	C	763.70	55.07	-0.70	-147.50	37.95	2.90
2	2	1.10	A	C	763.70	55.07	-0.70	-147.50	37.95	2.90
2	3	2.20	A	C	763.70	102.05	0.40	-147.50	69.92	4.00
3	3	2.20	B	C	1198.90	102.05	0.40	-140.30	69.92	4.00
3	4	3.30	B	C	1198.90	142.36	1.50	-140.30	96.94	5.10
4	4	3.30	B	C	1198.90	142.36	1.50	-140.30	96.94	5.10
4	5	4.40	B	C	1198.90	175.99	2.60	-140.30	119.01	6.20
5	5	4.40	C	C	1412.60	175.99	2.60	-133.60	119.01	6.20
5	6	5.50	C	C	1412.60	202.98	3.70	-133.60	136.16	7.30
6	6	5.50	C	C	1412.60	202.98	3.70	-133.60	136.16	7.30
6	7	6.60	C	C	1412.60	223.32	4.80	-133.60	148.39	8.40
7	7	6.60	D	C	1524.20	223.32	4.80	-129.70	148.39	8.40
7	8	7.70	D	C	1524.20	236.97	5.90	-129.70	155.66	9.50
8	8	7.70	D	C	1524.20	236.97	5.90	-129.70	155.66	9.50
8	9	8.80	D	C	1524.20	243.94	7.00	-129.70	157.99	10.60
9	9	8.80	D	C	1524.20	243.94	7.00	-129.70	157.99	10.60
9	10	9.90	D	C	1524.20	244.27	8.10	-129.70	155.39	11.70
10	10	9.90	D	C	1524.20	244.27	8.10	-129.70	155.39	11.70
10	11	11.00	D	C	1524.20	237.93	9.20	-129.70	147.86	12.80
11	11	11.00	D	C	1524.20	237.93	12.80	-129.70	147.86	9.20
11	12	12.10	D	C	1524.20	224.93	13.90	-129.70	135.39	10.30
12	12	12.10	D	C	1524.20	224.93	13.90	-129.70	135.39	10.30
12	13	13.20	D	C	1524.20	205.23	15.00	-129.70	117.96	11.40
13	13	13.20	D	C	1524.20	205.23	15.00	-129.70	117.96	11.40
13	14	14.30	D	C	1524.20	178.93	16.10	-129.70	95.64	12.50
14	14	14.30	C	C	1412.60	178.93	16.10	-133.60	95.64	12.50
14	15	15.40	C	C	1412.60	145.93	17.20	-133.60	68.36	13.60
15	15	15.40	G	C	1412.60	145.93	17.20	-133.60	68.36	13.60
15	16	16.50	G	C	1412.60	102.54	18.30	-133.60	33.38	14.70
16	16	16.50	H	C	1412.60	102.53	18.30	-133.60	33.37	14.70
16	17	17.60	H	C	1412.60	45.07	19.40	-133.60	-12.03	15.80
17	17	17.60	I	C	1198.90	45.06	19.40	-140.30	-12.04	15.80
17	18	18.70	I	C	1198.90	-22.87	20.50	-140.30	-71.53	16.90
18	18	18.70	I	C	1198.90	-22.87	20.50	-140.30	-71.53	16.90
18	19	19.80	I	C	1198.90	-102.10	21.60	-140.30	-144.27	18.00
19	19	19.80	J	C	763.80	-102.10	21.60	-147.50	-144.27	18.00
19	20	20.90	J	C	763.80	-193.50	22.70	-147.50	-229.40	19.10
20	20	20.90	J	C	763.80	-193.50	22.70	-147.50	-229.40	19.10
20	21	22.00	J	C	763.80	-301.15	23.80	-147.50	-329.91	20.20
21	1021	22.00	N	C	836.70	-301.15	20.20	-145.80	-329.91	23.80
21	22	23.40	N	C	836.70	-146.05	21.60	-145.80	-189.35	25.20
22	22	23.40	N	C	836.70	-146.05	21.60	-145.80	-189.35	25.20
22	23	24.80	N	C	836.70	-17.25	23.00	-145.80	-73.71	26.60
23	23	24.80	O	C	1243.70	-17.25	23.00	-139.20	-73.71	26.60
23	24	26.20	O	C	1243.70	94.94	24.40	-139.20	18.70	28.00
24	24	26.20	O	C	1243.70	94.94	24.40	-139.20	18.70	28.00
24	25	27.60	O	C	1243.70	188.69	25.80	-139.20	89.86	29.40
25	25	27.60	K	C	1586.00	188.69	25.80	-128.60	89.86	29.40
25	26	29.00	K	C	1586.00	259.59	27.20	-128.60	144.10	30.80
26	26	29.00	E	C	1586.00	259.59	27.20	-128.60	144.10	30.80
26	27	30.40	E	C	1586.00	313.67	28.60	-128.60	185.87	32.20
27	27	30.40	F	C	1699.40	313.67	28.60	-124.50	185.87	32.20
27	28	31.80	F	C	1699.40	356.94	30.00	-124.50	219.63	33.60
28	28	31.80	F	C	1699.40	356.94	30.00	-124.50	219.63	33.60
28	29	33.20	F	C	1699.40	389.45	31.40	-124.50	245.43	35.00
29	29	33.20	F	C	1699.40	389.45	31.40	-124.50	245.43	35.00
29	30	34.60	F	C	1699.40	411.14	32.80	-124.50	263.21	36.40
30	30	34.60	F	C	1699.40	411.14	32.80	-124.50	263.21	36.40
30	31	36.00	F	C	1699.40	422.04	34.20	-124.50	273.00	37.80
31	31	36.00	F	C	1699.40	422.04	37.80	-124.50	273.00	34.20
31	32	37.40	F	C	1699.40	422.15	39.20	-124.50	274.80	35.60

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CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	C	1699.40	422.15	39.20	-124.50	274.80	35.60
32	33	38.80	F	C	1699.40	411.47	40.60	-124.50	268.60	37.00
33	33	38.80	F	C	1699.40	411.47	40.60	-124.50	268.60	37.00
33	34	40.20	F	C	1699.40	389.97	42.00	-124.50	254.39	38.40
34	34	40.20	F	C	1699.40	389.97	42.00	-124.50	254.39	38.40
34	35	41.60	F	C	1699.40	357.70	43.40	-124.50	232.20	39.80
35	35	41.60	E	C	1586.00	357.70	43.40	-128.60	232.20	39.80
35	36	43.00	E	C	1586.00	314.62	44.80	-128.60	202.00	41.20
36	36	43.00	K	C	1586.00	314.62	44.80	-128.60	202.00	41.20
36	37	44.40	K	C	1586.00	254.74	46.20	-128.60	159.36	42.60
37	37	44.40	L	C	1243.70	254.73	46.20	-139.20	159.35	42.60
37	38	45.80	L	C	1243.70	172.88	47.60	-139.20	98.92	44.00
38	38	45.80	L	C	1243.70	172.88	47.60	-139.20	98.92	44.00
38	39	47.20	L	C	1243.70	75.41	49.00	-139.20	14.35	45.40
39	39	47.20	M	C	836.70	75.42	49.00	-145.80	14.36	45.40
39	40	48.60	M	C	836.70	-41.79	50.40	-145.80	-90.26	46.80
40	40	48.60	M	C	836.70	-41.80	50.40	-145.80	-90.27	46.80
40	41	50.00	M	C	836.70	-185.31	51.80	-145.80	-219.82	48.20
41	1041	50.00	M	C	836.70	-185.31	48.20	-145.80	-219.82	51.80
41	42	51.40	M	C	836.70	-41.79	49.60	-145.80	-90.26	53.20
42	42	51.40	M	C	836.70	-41.79	49.60	-145.80	-90.26	53.20
42	43	52.80	M	C	836.70	75.42	51.00	-145.80	14.36	54.60
43	43	52.80	L	C	1243.70	75.41	51.00	-139.20	14.35	54.60
43	44	54.20	L	C	1243.70	172.87	52.40	-139.20	98.91	56.00
44	44	54.20	L	C	1243.70	172.87	52.40	-139.20	98.91	56.00
44	45	55.60	L	C	1243.70	254.74	53.80	-139.20	159.36	57.40
45	45	55.60	K	C	1586.00	254.73	53.80	-128.60	159.35	57.40
45	46	57.00	K	C	1586.00	314.63	55.20	-128.60	202.01	58.80
46	46	57.00	E	C	1586.00	314.63	55.20	-128.60	202.01	58.80
46	47	58.40	E	C	1586.00	357.70	56.60	-128.60	232.20	60.20
47	47	58.40	F	C	1699.40	357.70	56.60	-124.50	232.20	60.20
47	48	59.80	F	C	1699.40	389.97	58.00	-124.50	254.39	61.60
48	48	59.80	F	C	1699.40	389.97	58.00	-124.50	254.39	61.60
48	49	61.20	F	C	1699.40	411.46	59.40	-124.50	268.59	63.00
49	49	61.20	F	C	1699.40	411.46	59.40	-124.50	268.59	63.00
49	50	62.60	F	C	1699.40	422.15	60.80	-124.50	274.80	64.40
50	50	62.60	F	C	1699.40	422.15	60.80	-124.50	274.80	64.40
50	51	64.00	F	C	1699.40	422.04	62.20	-124.50	273.00	65.80
51	51	64.00	F	C	1699.40	422.04	65.80	-124.50	273.00	62.20
51	52	65.40	F	C	1699.40	411.14	67.20	-124.50	263.21	63.60
52	52	65.40	F	C	1699.40	411.14	67.20	-124.50	263.21	63.60
52	53	66.80	F	C	1699.40	389.45	68.60	-124.50	245.43	65.00
53	53	66.80	F	C	1699.40	389.45	68.60	-124.50	245.43	65.00
53	54	68.20	F	C	1699.40	356.95	70.00	-124.50	219.64	66.40
54	54	68.20	F	C	1699.40	356.95	70.00	-124.50	219.64	66.40
54	55	69.60	F	C	1699.40	313.68	71.40	-124.50	185.88	67.80
55	55	69.60	E	C	1586.00	313.68	71.40	-128.60	185.88	67.80
55	56	71.00	E	C	1586.00	259.58	72.80	-128.60	144.09	69.20
56	56	71.00	K	C	1586.00	259.58	72.80	-128.60	144.09	69.20
56	57	72.40	K	C	1586.00	188.70	74.20	-128.60	89.87	70.60
57	57	72.40	O	C	1243.70	188.70	74.20	-139.20	89.87	70.60
57	58	73.80	O	C	1243.70	94.95	75.60	-139.20	18.71	72.00
58	58	73.80	O	C	1243.70	94.95	75.60	-139.20	18.71	72.00
58	59	75.20	O	C	1243.70	-17.26	77.00	-139.20	-73.72	73.40
59	59	75.20	N	C	836.70	-17.25	77.00	-145.80	-73.71	73.40
59	60	76.60	N	C	836.70	-146.05	78.40	-145.80	-189.35	74.80
60	60	76.60	N	C	836.70	-146.05	78.40	-145.80	-189.35	74.80
60	61	78.00	N	C	836.70	-301.15	79.80	-145.80	-329.91	76.20
61	1061	78.00	J	C	763.80	-301.15	76.20	-147.50	-329.91	79.80
61	62	79.10	J	C	763.80	-193.51	77.30	-147.50	-229.41	80.90
62	62	79.10	J	C	763.80	-193.51	77.30	-147.50	-229.41	80.90
62	63	80.20	J	C	763.80	-102.10	78.40	-147.50	-144.27	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	I	C	1198.90	-102.09	78.40	-140.30	-144.26	82.00
63	64	81.30	I	C	1198.90	-22.87	79.50	-140.30	-71.53	83.10
64	64	81.30	I	C	1198.90	-22.88	79.50	-140.30	-71.54	83.10
64	65	82.40	I	C	1198.90	45.06	80.60	-140.30	-12.04	84.20
65	65	82.40	H	C	1412.60	45.06	80.60	-133.60	-12.04	84.20
65	66	83.50	H	C	1412.60	102.53	81.70	-133.60	33.37	85.30
66	66	83.50	G	C	1412.60	102.53	81.70	-133.60	33.37	85.30
66	67	84.60	G	C	1412.60	145.93	82.80	-133.60	68.36	86.40
67	67	84.60	C	C	1412.60	145.93	82.80	-133.60	68.36	86.40
67	68	85.70	C	C	1412.60	178.93	83.90	-133.60	95.64	87.50
68	68	85.70	D	C	1524.20	178.93	83.90	-129.70	95.64	87.50
68	69	86.80	D	C	1524.20	205.24	85.00	-129.70	117.97	88.60
69	69	86.80	D	C	1524.20	205.24	85.00	-129.70	117.97	88.60
69	70	87.90	D	C	1524.20	224.92	86.10	-129.70	135.38	89.70
70	70	87.90	D	C	1524.20	224.92	86.10	-129.70	135.38	89.70
70	71	89.00	D	C	1524.20	237.92	87.20	-129.70	147.85	90.80
71	71	89.00	D	C	1524.20	237.92	90.80	-129.70	147.85	87.20
71	72	90.10	D	C	1524.20	244.27	91.90	-129.70	155.39	88.30
72	72	90.10	D	C	1524.20	244.27	91.90	-129.70	155.39	88.30
72	73	91.20	D	C	1524.20	243.94	93.00	-129.70	157.99	89.40
73	73	91.20	D	C	1524.20	243.94	93.00	-129.70	157.99	89.40
73	74	92.30	D	C	1524.20	236.97	94.10	-129.70	155.66	90.50
74	74	92.30	D	C	1524.20	236.97	94.10	-129.70	155.66	90.50
74	75	93.40	D	C	1524.20	223.32	95.20	-129.70	148.39	91.60
75	75	93.40	C	C	1412.60	223.32	95.20	-133.60	148.39	91.60
75	76	94.50	C	C	1412.60	202.99	96.30	-133.60	136.17	92.70
76	76	94.50	C	C	1412.60	202.99	96.30	-133.60	136.17	92.70
76	77	95.60	C	C	1412.60	176.00	97.40	-133.60	119.02	93.80
77	77	95.60	B	C	1198.90	176.00	97.40	-140.30	119.02	93.80
77	78	96.70	B	C	1198.90	142.35	98.50	-140.30	96.93	94.90
78	78	96.70	B	C	1198.90	142.35	98.50	-140.30	96.93	94.90
78	79	97.80	B	C	1198.90	102.04	99.60	-140.30	69.91	96.00
79	79	97.80	A	C	763.70	102.04	99.60	-147.50	69.91	96.00
79	80	98.90	A	C	763.70	55.07	100.70	-147.50	37.95	97.10
80	80	98.90	A	C	763.70	55.07	100.70	-147.50	37.95	97.10
80	81	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20
101	101	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
101	102	1.10	A	C	763.70	55.07	-0.70	-147.50	37.95	2.90
102	102	1.10	A	C	763.70	55.07	-0.70	-147.50	37.95	2.90
102	103	2.20	A	C	763.70	102.05	0.40	-147.50	69.92	4.00
103	103	2.20	B	C	1198.90	102.05	0.40	-140.30	69.92	4.00
103	104	3.30	B	C	1198.90	142.36	1.50	-140.30	96.94	5.10
104	104	3.30	B	C	1198.90	142.36	1.50	-140.30	96.94	5.10
104	105	4.40	B	C	1198.90	176.00	2.60	-140.30	119.02	6.20
105	105	4.40	C	C	1412.60	176.00	2.60	-133.60	119.02	6.20
105	106	5.50	C	C	1412.60	202.99	3.70	-133.60	136.17	7.30
106	106	5.50	C	C	1412.60	202.99	3.70	-133.60	136.17	7.30
106	107	6.60	C	C	1412.60	223.32	4.80	-133.60	148.39	8.40
107	107	6.60	D	C	1524.20	223.32	4.80	-129.70	148.39	8.40
107	108	7.70	D	C	1524.20	236.97	5.90	-129.70	155.66	9.50
108	108	7.70	D	C	1524.20	236.97	5.90	-129.70	155.66	9.50
108	109	8.80	D	C	1524.20	243.94	7.00	-129.70	157.99	10.60
109	109	8.80	D	C	1524.20	243.94	7.00	-129.70	157.99	10.60
109	110	9.90	D	C	1524.20	244.27	8.10	-129.70	155.39	11.70
110	110	9.90	D	C	1524.20	244.27	8.10	-129.70	155.39	11.70
110	111	11.00	D	C	1524.20	237.93	9.20	-129.70	147.86	12.80
111	111	11.00	D	C	1524.20	237.93	12.80	-129.70	147.86	9.20
111	112	12.10	D	C	1524.20	224.93	13.90	-129.70	135.39	10.30
112	112	12.10	D	C	1524.20	224.93	13.90	-129.70	135.39	10.30
112	113	13.20	D	C	1524.20	205.24	15.00	-129.70	117.97	11.40
113	113	13.20	D	C	1524.20	205.24	15.00	-129.70	117.97	11.40
113	114	14.30	D	C	1524.20	178.93	16.10	-129.70	95.64	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	C	1412.60	178.93	16.10	-133.60	95.64	12.50
114	115	15.40	C	C	1412.60	145.93	17.20	-133.60	68.36	13.60
115	115	15.40	G	C	1412.60	145.93	17.20	-133.60	68.36	13.60
115	116	16.50	G	C	1412.60	102.53	18.30	-133.60	33.37	14.70
116	116	16.50	H	C	1412.60	102.53	18.30	-133.60	33.37	14.70
116	117	17.60	H	C	1412.60	45.06	19.40	-133.60	-12.04	15.80
117	117	17.60	I	C	1198.90	45.07	19.40	-140.30	-12.03	15.80
117	118	18.70	I	C	1198.90	-22.87	20.50	-140.30	-71.53	16.90
118	118	18.70	I	C	1198.90	-22.87	20.50	-140.30	-71.53	16.90
118	119	19.80	I	C	1198.90	-102.09	21.60	-140.30	-144.26	18.00
119	119	19.80	J	C	763.80	-102.09	21.60	-147.50	-144.26	18.00
119	120	20.90	J	C	763.80	-193.50	22.70	-147.50	-229.40	19.10
120	120	20.90	J	C	763.80	-193.50	22.70	-147.50	-229.40	19.10
120	121	22.00	J	C	763.80	-301.15	23.80	-147.50	-329.91	20.20
121	1121	22.00	N	C	836.70	-301.15	20.20	-145.80	-329.91	23.80
121	122	23.40	N	C	836.70	-146.05	21.60	-145.80	-189.35	25.20
122	122	23.40	N	C	836.70	-146.05	21.60	-145.80	-189.35	25.20
122	123	24.80	N	C	836.70	-17.26	23.00	-145.80	-73.72	26.60
123	123	24.80	O	C	1243.70	-17.25	23.00	-139.20	-73.71	26.60
123	124	26.20	O	C	1243.70	94.94	24.40	-139.20	18.70	28.00
124	124	26.20	O	C	1243.70	94.94	24.40	-139.20	18.70	28.00
124	125	27.60	O	C	1243.70	188.68	25.80	-139.20	89.85	29.40
125	125	27.60	K	C	1586.00	188.68	25.80	-128.60	89.85	29.40
125	126	29.00	K	C	1586.00	259.58	27.20	-128.60	144.09	30.80
126	126	29.00	E	C	1586.00	259.58	27.20	-128.60	144.09	30.80
126	127	30.40	E	C	1586.00	313.67	28.60	-128.60	185.87	32.20
127	127	30.40	F	C	1699.40	313.67	28.60	-124.50	185.87	32.20
127	128	31.80	F	C	1699.40	356.94	30.00	-124.50	219.63	33.60
128	128	31.80	F	C	1699.40	356.94	30.00	-124.50	219.63	33.60
128	129	33.20	F	C	1699.40	389.45	31.40	-124.50	245.43	35.00
129	129	33.20	F	C	1699.40	389.45	31.40	-124.50	245.43	35.00
129	130	34.60	F	C	1699.40	411.14	32.80	-124.50	263.21	36.40
130	130	34.60	F	C	1699.40	411.14	32.80	-124.50	263.21	36.40
130	131	36.00	F	C	1699.40	422.05	34.20	-124.50	273.01	37.80
131	131	36.00	F	C	1699.40	422.05	37.80	-124.50	273.01	34.20
131	132	37.40	F	C	1699.40	422.14	39.20	-124.50	274.79	35.60
132	132	37.40	F	C	1699.40	422.14	39.20	-124.50	274.79	35.60
132	133	38.80	F	C	1699.40	411.46	40.60	-124.50	268.59	37.00
133	133	38.80	F	C	1699.40	411.46	40.60	-124.50	268.59	37.00
133	134	40.20	F	C	1699.40	389.97	42.00	-124.50	254.39	38.40
134	134	40.20	F	C	1699.40	389.97	42.00	-124.50	254.39	38.40
134	135	41.60	F	C	1699.40	357.70	43.40	-124.50	232.20	39.80
135	135	41.60	E	C	1586.00	357.70	43.40	-128.60	232.20	39.80
135	136	43.00	E	C	1586.00	314.62	44.80	-128.60	202.00	41.20
136	136	43.00	K	C	1586.00	314.62	44.80	-128.60	202.00	41.20
136	137	44.40	K	C	1586.00	254.74	46.20	-128.60	159.36	42.60
137	137	44.40	L	C	1243.70	254.73	46.20	-139.20	159.35	42.60
137	138	45.80	L	C	1243.70	172.88	47.60	-139.20	98.92	44.00
138	138	45.80	L	C	1243.70	172.88	47.60	-139.20	98.92	44.00
138	139	47.20	L	C	1243.70	75.42	49.00	-139.20	14.36	45.40
139	139	47.20	M	C	836.70	75.42	49.00	-145.80	14.36	45.40
139	140	48.60	M	C	836.70	-41.78	50.40	-145.80	-90.25	46.80
140	140	48.60	M	C	836.70	-41.79	50.40	-145.80	-90.26	46.80
140	141	50.00	M	C	836.70	-185.29	51.80	-145.80	-219.80	48.20
141	1141	50.00	M	C	836.70	-185.29	48.20	-145.80	-219.80	51.80
141	142	51.40	M	C	836.70	-41.79	49.60	-145.80	-90.26	53.20
142	142	51.40	M	C	836.70	-41.79	49.60	-145.80	-90.26	53.20
142	143	52.80	M	C	836.70	75.43	51.00	-145.80	14.37	54.60
143	143	52.80	L	C	1243.70	75.43	51.00	-139.20	14.37	54.60
143	144	54.20	L	C	1243.70	172.88	52.40	-139.20	98.92	56.00
144	144	54.20	L	C	1243.70	172.88	52.40	-139.20	98.92	56.00
144	145	55.60	L	C	1243.70	254.74	53.80	-139.20	159.36	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:

VVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1)eje1f3.HIP.To + [1; 1)eje2f3.HIP.To

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	K	C	1586.00	254.74	53.80	-128.60	159.36	57.40
145	146	57.00	K	C	1586.00	314.62	55.20	-128.60	202.00	58.80
146	146	57.00	E	C	1586.00	314.62	55.20	-128.60	202.00	58.80
146	147	58.40	E	C	1586.00	357.71	56.60	-128.60	232.21	60.20
147	147	58.40	F	C	1699.40	357.71	56.60	-124.50	232.21	60.20
147	148	59.80	F	C	1699.40	389.97	58.00	-124.50	254.39	61.60
148	148	59.80	F	C	1699.40	389.97	58.00	-124.50	254.39	61.60
148	149	61.20	F	C	1699.40	411.46	59.40	-124.50	268.59	63.00
149	149	61.20	F	C	1699.40	411.46	59.40	-124.50	268.59	63.00
149	150	62.60	F	C	1699.40	422.15	60.80	-124.50	274.80	64.40
150	150	62.60	F	C	1699.40	422.15	60.80	-124.50	274.80	64.40
150	151	64.00	F	C	1699.40	422.04	62.20	-124.50	273.00	65.80
151	151	64.00	F	C	1699.40	422.04	65.80	-124.50	273.00	62.20
151	152	65.40	F	C	1699.40	411.14	67.20	-124.50	263.21	63.60
152	152	65.40	F	C	1699.40	411.14	67.20	-124.50	263.21	63.60
152	153	66.80	F	C	1699.40	389.45	68.60	-124.50	245.43	65.00
153	153	66.80	F	C	1699.40	389.45	68.60	-124.50	245.43	65.00
153	154	68.20	F	C	1699.40	356.94	70.00	-124.50	219.63	66.40
154	154	68.20	F	C	1699.40	356.94	70.00	-124.50	219.63	66.40
154	155	69.60	F	C	1699.40	313.67	71.40	-124.50	185.87	67.80
155	155	69.60	E	C	1586.00	313.67	71.40	-128.60	185.87	67.80
155	156	71.00	E	C	1586.00	259.57	72.80	-128.60	144.08	69.20
156	156	71.00	K	C	1586.00	259.57	72.80	-128.60	144.08	69.20
156	157	72.40	K	C	1586.00	188.69	74.20	-128.60	89.86	70.60
157	157	72.40	O	C	1243.70	188.69	74.20	-139.20	89.86	70.60
157	158	73.80	O	C	1243.70	94.94	75.60	-139.20	18.70	72.00
158	158	73.80	O	C	1243.70	94.94	75.60	-139.20	18.70	72.00
158	159	75.20	O	C	1243.70	-17.26	77.00	-139.20	-73.72	73.40
159	159	75.20	N	C	836.70	-17.26	77.00	-145.80	-73.72	73.40
159	160	76.60	N	C	836.70	-146.05	78.40	-145.80	-189.35	74.80
160	160	76.60	N	C	836.70	-146.05	78.40	-145.80	-189.35	74.80
160	161	78.00	N	C	836.70	-301.14	79.80	-145.80	-329.90	76.20
161	1161	78.00	J	C	763.80	-301.15	76.20	-147.50	-329.91	79.80
161	162	79.10	J	C	763.80	-193.50	77.30	-147.50	-229.40	80.90
162	162	79.10	J	C	763.80	-193.50	77.30	-147.50	-229.40	80.90
162	163	80.20	J	C	763.80	-102.09	78.40	-147.50	-144.26	82.00
163	163	80.20	I	C	1198.90	-102.09	78.40	-140.30	-144.26	82.00
163	164	81.30	I	C	1198.90	-22.87	79.50	-140.30	-71.53	83.10
164	164	81.30	I	C	1198.90	-22.88	79.50	-140.30	-71.54	83.10
164	165	82.40	I	C	1198.90	45.07	80.60	-140.30	-12.03	84.20
165	165	82.40	H	C	1412.60	45.07	80.60	-133.60	-12.03	84.20
165	166	83.50	H	C	1412.60	102.54	81.70	-133.60	33.38	85.30
166	166	83.50	G	C	1412.60	102.53	81.70	-133.60	33.37	85.30
166	167	84.60	G	C	1412.60	145.93	82.80	-133.60	68.36	86.40
167	167	84.60	C	C	1412.60	145.93	82.80	-133.60	68.36	86.40
167	168	85.70	C	C	1412.60	178.93	83.90	-133.60	95.64	87.50
168	168	85.70	D	C	1524.20	178.93	83.90	-129.70	95.64	87.50
168	169	86.80	D	C	1524.20	205.24	85.00	-129.70	117.97	88.60
169	169	86.80	D	C	1524.20	205.24	85.00	-129.70	117.97	88.60
169	170	87.90	D	C	1524.20	224.93	86.10	-129.70	135.39	89.70
170	170	87.90	D	C	1524.20	224.93	86.10	-129.70	135.39	89.70
170	171	89.00	D	C	1524.20	237.93	87.20	-129.70	147.86	90.80
171	171	89.00	D	C	1524.20	237.93	90.80	-129.70	147.86	87.20
171	172	90.10	D	C	1524.20	244.27	91.90	-129.70	155.39	88.30
172	172	90.10	D	C	1524.20	244.27	91.90	-129.70	155.39	88.30
172	173	91.20	D	C	1524.20	243.94	93.00	-129.70	157.99	89.40
173	173	91.20	D	C	1524.20	243.94	93.00	-129.70	157.99	89.40
173	174	92.30	D	C	1524.20	236.97	94.10	-129.70	155.66	90.50
174	174	92.30	D	C	1524.20	236.97	94.10	-129.70	155.66	90.50
174	175	93.40	D	C	1524.20	223.32	95.20	-129.70	148.39	91.60
175	175	93.40	C	C	1412.60	223.32	95.20	-133.60	148.39	91.60
175	176	94.50	C	C	1412.60	202.99	96.30	-133.60	136.17	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 2.MZ

Construcción fase 2 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1)eje1f3.HIP.To + [1; 1)eje2f3.HIP.To

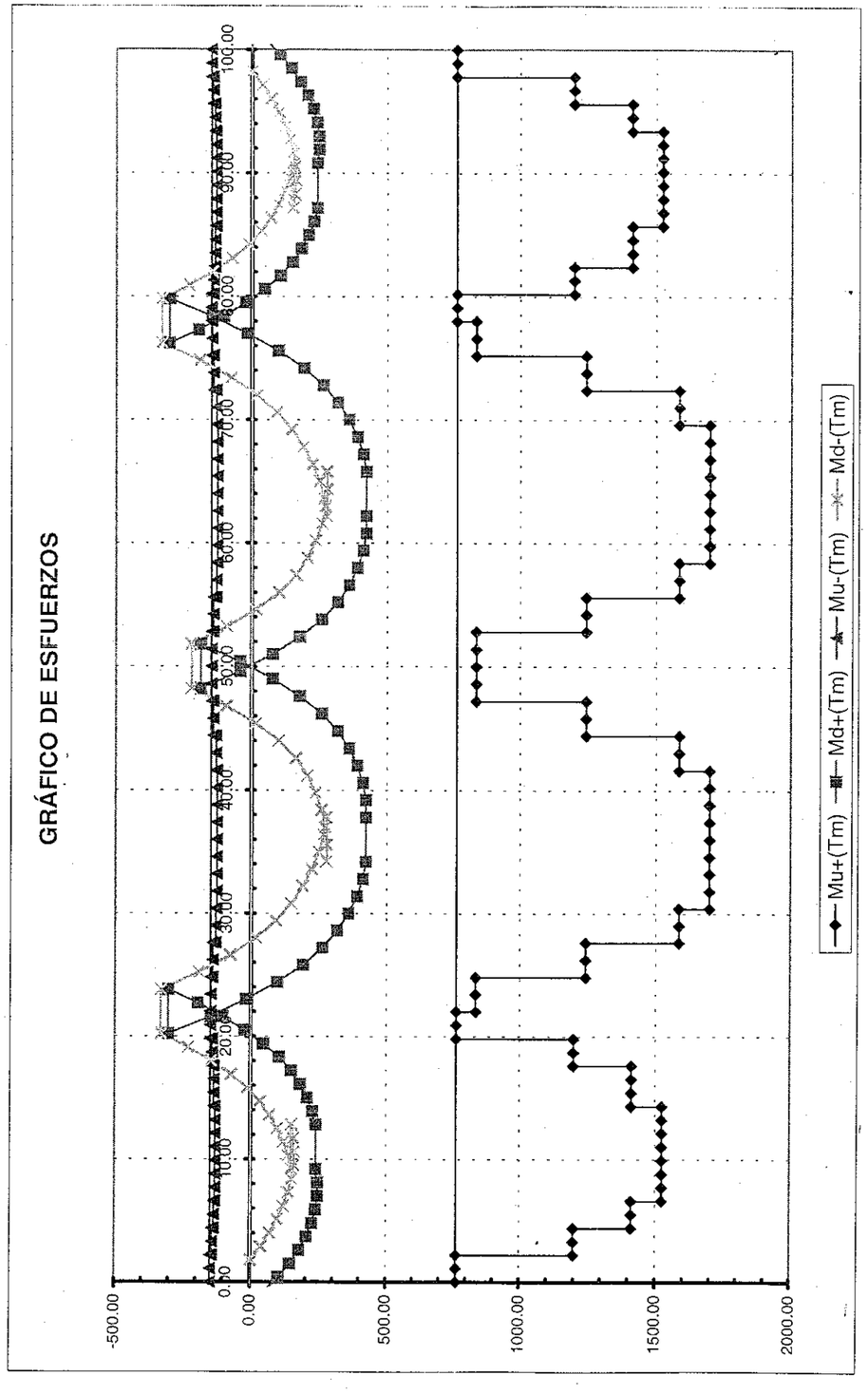
Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	C	1412.60	202.99	96.30	-133.60	136.17	92.70
176	177	95.60	C	C	1412.60	176.00	97.40	-133.60	119.02	93.80
177	177	95.60	B	C	1198.90	176.00	97.40	-140.30	119.02	93.80
177	178	96.70	B	C	1198.90	142.35	98.50	-140.30	96.93	94.90
178	178	96.70	B	C	1198.90	142.35	98.50	-140.30	96.93	94.90
178	179	97.80	B	C	1198.90	102.04	99.60	-140.30	69.91	96.00
179	179	97.80	A	C	763.70	102.04	99.60	-147.50	69.91	96.00
179	180	98.90	A	C	763.70	55.07	100.70	-147.50	37.95	97.10
180	180	98.90	A	C	763.70	55.07	100.70	-147.50	37.95	97.10
180	181	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20

Programa DINTEL PACADAR S.A.
ENVOLOVENTE FASE 2.MZ

GRÁFICO DE ESFUERZOS



CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
1	2	1.10	A	C	763.70	99.82	-0.70	-147.50	71.10	2.90
2	2	1.10	A	C	763.70	99.82	-0.70	-147.50	71.10	2.90
2	3	2.20	A	C	763.70	184.12	0.40	-147.50	130.71	4.00
3	3	2.20	B	C	1198.90	184.12	0.40	-140.30	130.71	4.00
3	4	3.30	B	C	1198.90	254.32	1.50	-140.30	179.87	5.10
4	4	3.30	B	C	1198.90	254.32	1.50	-140.30	179.87	5.10
4	5	4.40	B	C	1198.90	310.40	2.60	-140.30	218.57	6.20
5	5	4.40	C	C	1412.60	310.40	2.60	-133.60	218.57	6.20
5	6	5.50	C	C	1412.60	352.40	3.70	-133.60	246.84	7.30
6	6	5.50	C	C	1412.60	352.40	3.70	-133.60	246.84	7.30
6	7	6.60	C	C	1412.60	380.32	4.80	-133.60	264.69	8.40
7	7	6.60	D	C	1524.20	380.32	4.80	-129.70	264.69	8.40
7	8	7.70	D	C	1524.20	394.13	5.90	-129.70	272.08	9.50
8	8	7.70	D	C	1524.20	394.13	9.50	-129.70	272.08	5.90
8	9	8.80	D	C	1524.20	393.83	10.60	-129.70	269.02	7.00
9	9	8.80	D	C	1524.20	393.83	10.60	-129.70	269.02	7.00
9	10	9.90	D	C	1524.20	379.44	11.70	-129.70	255.52	8.10
10	10	9.90	D	C	1524.20	379.44	11.70	-129.70	255.52	8.10
10	11	11.00	D	C	1524.20	350.96	12.80	-129.70	231.59	9.20
11	11	11.00	D	C	1524.20	350.96	12.80	-129.70	231.59	9.20
11	12	12.10	D	C	1524.20	308.38	13.90	-129.70	197.21	10.30
12	12	12.10	D	C	1524.20	308.38	13.90	-129.70	197.21	10.30
12	13	13.20	D	C	1524.20	251.69	15.00	-129.70	152.37	11.40
13	13	13.20	D	C	1524.20	251.69	15.00	-129.70	152.37	11.40
13	14	14.30	D	C	1524.20	180.94	16.10	-129.70	97.13	12.50
14	14	14.30	C	C	1412.60	180.94	16.10	-133.60	97.13	12.50
14	15	15.40	C	C	1412.60	108.39	17.20	-133.60	17.68	13.60
15	15	15.40	G	T	2051.00	108.39	17.20	-2725.40	17.68	13.60
15	16	16.50	G	T	2051.00	22.62	18.30	-2725.40	-74.51	14.70
16	16	16.50	H	T	2045.70	22.61	18.30	-2922.00	-74.52	14.70
16	17	17.60	H	T	2045.70	-77.23	19.40	-2922.00	-177.14	15.80
17	17	17.60	I	T	1620.10	-77.24	19.40	-3086.10	-177.15	15.80
17	18	18.70	I	T	1620.10	-187.56	20.50	-3086.10	-293.86	16.90
18	18	18.70	I	T	1620.10	-187.56	20.50	-3086.10	-293.86	16.90
18	19	19.80	I	T	1620.10	-309.17	21.60	-3086.10	-423.82	18.00
19	19	19.80	J	T	1015.60	-309.17	21.60	-3316.30	-423.82	18.00
19	20	20.90	J	T	1015.60	-442.96	22.70	-3316.30	-566.17	19.10
20	20	20.90	J	T	1015.60	-442.96	22.70	-3316.30	-566.17	19.10
20	21	22.00	J	T	1015.60	-592.99	23.80	-3316.30	-723.90	20.20
21	1021	22.00	N	T	1104.10	-592.99	20.20	-3283.20	-723.90	23.80
21	22	23.40	N	T	1104.10	-389.65	21.60	-3283.20	-518.21	25.20
22	22	23.40	N	T	1104.10	-389.65	21.60	-3283.20	-518.21	25.20
22	23	24.80	N	T	1104.10	-212.61	23.00	-3283.20	-337.45	26.60
23	23	24.80	O	T	1705.40	-212.61	23.00	-3053.20	-337.45	26.60
23	24	26.20	O	T	1705.40	-52.18	24.40	-3053.20	-179.91	28.00
24	24	26.20	O	T	1705.40	-52.18	24.40	-3053.20	-179.91	28.00
24	25	27.60	O	T	1705.40	89.81	25.80	-3053.20	-43.63	29.40
25	25	27.60	K	C	1586.00	89.81	25.80	-128.60	-43.63	29.40
25	26	29.00	K	C	1586.00	208.95	27.20	-128.60	75.74	30.80
26	26	29.00	E	C	1586.00	208.95	27.20	-128.60	75.74	30.80
26	27	30.40	E	C	1586.00	306.19	28.60	-128.60	175.77	32.20
27	27	30.40	F	C	1699.40	306.19	28.60	-124.50	175.77	32.20
27	28	31.80	F	C	1699.40	392.21	30.00	-124.50	245.76	33.60
28	28	31.80	F	C	1699.40	392.21	30.00	-124.50	245.76	33.60
28	29	33.20	F	C	1699.40	458.06	31.40	-124.50	296.25	35.00
29	29	33.20	F	C	1699.40	458.06	31.40	-124.50	296.25	35.00
29	30	34.60	F	C	1699.40	501.05	32.80	-124.50	329.81	36.40
30	30	34.60	F	C	1699.40	501.05	32.80	-124.50	329.81	36.40
30	31	36.00	F	C	1699.40	521.21	34.20	-124.50	346.46	37.80
31	31	36.00	F	C	1699.40	521.21	37.80	-124.50	346.46	34.20
31	32	37.40	F	C	1699.40	518.54	39.20	-124.50	346.20	35.60

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	C	1699.40	518.54	39.20	-124.50	346.20	35.60
32	33	38.80	F	C	1699.40	493.04	40.60	-124.50	329.02	37.00
33	33	38.80	F	C	1699.40	493.04	40.60	-124.50	329.02	37.00
33	34	40.20	F	C	1699.40	444.69	42.00	-124.50	294.92	38.40
34	34	40.20	F	C	1699.40	444.69	42.00	-124.50	294.92	38.40
34	35	41.60	F	C	1699.40	373.51	43.40	-124.50	243.91	39.80
35	35	41.60	E	C	1586.00	373.51	43.40	-128.60	243.91	39.80
35	36	43.00	E	C	1586.00	287.97	44.80	-128.60	166.02	41.20
36	36	43.00	K	T	2472.90	287.97	44.80	-2562.80	166.02	41.20
36	37	44.40	K	T	2472.90	184.65	46.20	-2562.80	64.74	42.60
37	37	44.40	L	T	1705.40	184.64	46.20	-3053.20	64.73	42.60
37	38	45.80	L	T	1705.40	59.35	47.60	-3053.20	-54.35	44.00
38	38	45.80	L	T	1705.40	59.35	47.60	-3053.20	-54.35	44.00
38	39	47.20	L	T	1705.40	-81.56	49.00	-3053.20	-197.56	45.40
39	39	47.20	M	T	1104.10	-81.55	49.00	-3283.20	-197.55	45.40
39	40	48.60	M	T	1104.10	-242.20	50.40	-3283.20	-360.82	46.80
40	40	48.60	M	T	1104.10	-242.21	50.40	-3283.20	-360.83	46.80
40	41	50.00	M	T	1104.10	-429.16	51.80	-3283.20	-549.01	48.20
41	1041	50.00	M	T	1104.10	-429.16	48.20	-3283.20	-549.01	51.80
41	42	51.40	M	T	1104.10	-242.20	49.60	-3283.20	-360.82	53.20
42	42	51.40	M	T	1104.10	-242.20	49.60	-3283.20	-360.82	53.20
42	43	52.80	M	T	1104.10	-81.55	51.00	-3283.20	-197.55	54.60
43	43	52.80	L	T	1705.40	-81.56	51.00	-3053.20	-197.56	54.60
43	44	54.20	L	T	1705.40	59.34	52.40	-3053.20	-54.36	56.00
44	44	54.20	L	T	1705.40	59.34	52.40	-3053.20	-54.36	56.00
44	45	55.60	L	T	1705.40	184.65	53.80	-3053.20	64.74	57.40
45	45	55.60	K	T	2472.90	184.64	53.80	-2562.80	64.73	57.40
45	46	57.00	K	T	2472.90	287.98	55.20	-2562.80	166.03	58.80
46	46	57.00	E	C	1586.00	287.98	55.20	-128.60	166.03	58.80
46	47	58.40	E	C	1586.00	373.51	56.60	-128.60	243.91	60.20
47	47	58.40	F	C	1699.40	373.51	56.60	-124.50	243.91	60.20
47	48	59.80	F	C	1699.40	444.69	58.00	-124.50	294.92	61.60
48	48	59.80	F	C	1699.40	444.69	58.00	-124.50	294.92	61.60
48	49	61.20	F	C	1699.40	493.03	59.40	-124.50	329.01	63.00
49	49	61.20	F	C	1699.40	493.03	59.40	-124.50	329.01	63.00
49	50	62.60	F	C	1699.40	518.54	60.80	-124.50	346.20	64.40
50	50	62.60	F	C	1699.40	518.54	60.80	-124.50	346.20	64.40
50	51	64.00	F	C	1699.40	521.21	62.20	-124.50	346.46	65.80
51	51	64.00	F	C	1699.40	521.21	65.80	-124.50	346.46	62.20
51	52	65.40	F	C	1699.40	501.05	67.20	-124.50	329.81	63.60
52	52	65.40	F	C	1699.40	501.05	67.20	-124.50	329.81	63.60
52	53	66.80	F	C	1699.40	458.06	68.60	-124.50	296.25	65.00
53	53	66.80	F	C	1699.40	458.06	68.60	-124.50	296.25	65.00
53	54	68.20	F	C	1699.40	392.22	70.00	-124.50	245.77	66.40
54	54	68.20	F	C	1699.40	392.22	70.00	-124.50	245.77	66.40
54	55	69.60	F	C	1699.40	306.20	71.40	-124.50	175.78	67.80
55	55	69.60	E	C	1586.00	306.20	71.40	-128.60	175.78	67.80
55	56	71.00	E	C	1586.00	208.94	72.80	-128.60	75.73	69.20
56	56	71.00	K	C	1586.00	208.94	72.80	-128.60	75.73	69.20
56	57	72.40	K	C	1586.00	89.82	74.20	-128.60	-43.62	70.60
57	57	72.40	O	T	1705.40	89.82	74.20	-3053.20	-43.62	70.60
57	58	73.80	O	T	1705.40	-52.17	75.60	-3053.20	-179.90	72.00
58	58	73.80	O	T	1705.40	-52.17	75.60	-3053.20	-179.90	72.00
58	59	75.20	O	T	1705.40	-212.62	77.00	-3053.20	-337.46	73.40
59	59	75.20	N	T	1104.10	-212.61	77.00	-3283.20	-337.45	73.40
59	60	76.60	N	T	1104.10	-389.65	78.40	-3283.20	-518.21	74.80
60	60	76.60	N	T	1104.10	-389.65	78.40	-3283.20	-518.21	74.80
60	61	78.00	N	T	1104.10	-592.99	79.80	-3283.20	-723.90	76.20
61	1061	78.00	J	T	1015.60	-592.99	76.20	-3316.30	-723.90	79.80
61	62	79.10	J	T	1015.60	-442.97	77.30	-3316.30	-566.18	80.90
62	62	79.10	J	T	1015.60	-442.97	77.30	-3316.30	-566.18	80.90
62	63	80.20	J	T	1015.60	-309.17	78.40	-3316.30	-423.82	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	I	T	1620.10	-309.16	78.40	-3086.10	-423.81	82.00
63	64	81.30	I	T	1620.10	-187.56	79.50	-3086.10	-293.86	83.10
64	64	81.30	I	T	1620.10	-187.57	79.50	-3086.10	-293.87	83.10
64	65	82.40	I	T	1620.10	-77.24	80.60	-3086.10	-177.15	84.20
65	65	82.40	H	T	2045.70	-77.24	80.60	-2922.00	-177.15	84.20
65	66	83.50	H	T	2045.70	22.61	81.70	-2922.00	-74.52	85.30
66	66	83.50	G	T	2051.00	22.61	81.70	-2725.40	-74.52	85.30
66	67	84.60	G	T	2051.00	108.39	82.80	-2725.40	17.68	86.40
67	67	84.60	C	C	1412.60	108.39	82.80	-133.60	17.68	86.40
67	68	85.70	C	C	1412.60	180.94	83.90	-133.60	97.13	87.50
68	68	85.70	D	C	1524.20	180.94	83.90	-129.70	97.13	87.50
68	69	86.80	D	C	1524.20	251.70	85.00	-129.70	152.38	88.60
69	69	86.80	D	C	1524.20	251.70	85.00	-129.70	152.38	88.60
69	70	87.90	D	C	1524.20	308.37	86.10	-129.70	197.20	89.70
70	70	87.90	D	C	1524.20	308.37	86.10	-129.70	197.20	89.70
70	71	89.00	D	C	1524.20	350.95	87.20	-129.70	231.58	90.80
71	71	89.00	D	C	1524.20	350.95	87.20	-129.70	231.58	90.80
71	72	90.10	D	C	1524.20	379.44	88.30	-129.70	255.52	91.90
72	72	90.10	D	C	1524.20	379.44	88.30	-129.70	255.52	91.90
72	73	91.20	D	C	1524.20	393.83	89.40	-129.70	269.02	93.00
73	73	91.20	D	C	1524.20	393.83	89.40	-129.70	269.02	93.00
73	74	92.30	D	C	1524.20	394.13	90.50	-129.70	272.08	94.10
74	74	92.30	D	C	1524.20	394.13	94.10	-129.70	272.08	90.50
74	75	93.40	D	C	1524.20	380.32	95.20	-129.70	264.69	91.60
75	75	93.40	C	C	1412.60	380.32	95.20	-133.60	264.69	91.60
75	76	94.50	C	C	1412.60	352.41	96.30	-133.60	246.85	92.70
76	76	94.50	C	C	1412.60	352.41	96.30	-133.60	246.85	92.70
76	77	95.60	C	C	1412.60	310.41	97.40	-133.60	218.58	93.80
77	77	95.60	B	C	1198.90	310.41	97.40	-140.30	218.58	93.80
77	78	96.70	B	C	1198.90	254.31	98.50	-140.30	179.86	94.90
78	78	96.70	B	C	1198.90	254.31	98.50	-140.30	179.86	94.90
78	79	97.80	B	C	1198.90	184.11	99.60	-140.30	130.70	96.00
79	79	97.80	A	C	763.70	184.11	99.60	-147.50	130.70	96.00
79	80	98.90	A	C	763.70	99.82	100.70	-147.50	71.10	97.10
80	80	98.90	A	C	763.70	99.82	100.70	-147.50	71.10	97.10
80	81	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20
101	101	0.00	A	C	763.70	0.00	-1.80	-147.50	0.00	1.80
101	102	1.10	A	C	763.70	99.82	-0.70	-147.50	71.10	2.90
102	102	1.10	A	C	763.70	99.82	-0.70	-147.50	71.10	2.90
102	103	2.20	A	C	763.70	184.12	0.40	-147.50	130.71	4.00
103	103	2.20	B	C	1198.90	184.12	0.40	-140.30	130.71	4.00
103	104	3.30	B	C	1198.90	254.32	1.50	-140.30	179.87	5.10
104	104	3.30	B	C	1198.90	254.32	1.50	-140.30	179.87	5.10
104	105	4.40	B	C	1198.90	310.41	2.60	-140.30	218.58	6.20
105	105	4.40	C	C	1412.60	310.41	2.60	-133.60	218.58	6.20
105	106	5.50	C	C	1412.60	352.41	3.70	-133.60	246.85	7.30
106	106	5.50	C	C	1412.60	352.41	3.70	-133.60	246.85	7.30
106	107	6.60	C	C	1412.60	380.32	4.80	-133.60	264.69	8.40
107	107	6.60	D	C	1524.20	380.32	4.80	-129.70	264.69	8.40
107	108	7.70	D	C	1524.20	394.13	5.90	-129.70	272.08	9.50
108	108	7.70	D	C	1524.20	394.13	9.50	-129.70	272.08	5.90
108	109	8.80	D	C	1524.20	393.83	10.60	-129.70	269.02	7.00
109	109	8.80	D	C	1524.20	393.83	10.60	-129.70	269.02	7.00
109	110	9.90	D	C	1524.20	379.44	11.70	-129.70	255.52	8.10
110	110	9.90	D	C	1524.20	379.44	11.70	-129.70	255.52	8.10
110	111	11.00	D	C	1524.20	350.96	12.80	-129.70	231.59	9.20
111	111	11.00	D	C	1524.20	350.96	12.80	-129.70	231.59	9.20
111	112	12.10	D	C	1524.20	308.38	13.90	-129.70	197.21	10.30
112	112	12.10	D	C	1524.20	308.38	13.90	-129.70	197.21	10.30
112	113	13.20	D	C	1524.20	251.70	15.00	-129.70	152.38	11.40
113	113	13.20	D	C	1524.20	251.70	15.00	-129.70	152.38	11.40
113	114	14.30	D	C	1524.20	180.94	16.10	-129.70	97.13	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	C	1412.60	180.94	16.10	-133.60	97.13	12.50
114	115	15.40	C	C	1412.60	108.39	17.20	-133.60	17.68	13.60
115	115	15.40	G	T	2051.00	108.39	17.20	-2725.40	17.68	13.60
115	116	16.50	G	T	2051.00	22.61	18.30	-2725.40	-74.52	14.70
116	116	16.50	H	T	2045.70	22.61	18.30	-2922.00	-74.52	14.70
116	117	17.60	H	T	2045.70	-77.25	19.40	-2922.00	-177.16	15.80
117	117	17.60	I	T	1620.10	-77.24	19.40	-3086.10	-177.15	15.80
117	118	18.70	I	T	1620.10	-187.56	20.50	-3086.10	-293.86	16.90
118	118	18.70	I	T	1620.10	-187.56	20.50	-3086.10	-293.86	16.90
118	119	19.80	I	T	1620.10	-309.16	21.60	-3086.10	-423.81	18.00
119	119	19.80	J	T	1015.60	-309.16	21.60	-3316.30	-423.81	18.00
119	120	20.90	J	T	1015.60	-442.96	22.70	-3316.30	-566.17	19.10
120	120	20.90	J	T	1015.60	-442.96	22.70	-3316.30	-566.17	19.10
120	121	22.00	J	T	1015.60	-592.99	23.80	-3316.30	-723.90	20.20
121	1121	22.00	N	T	1104.10	-592.99	20.20	-3283.20	-723.90	23.80
121	122	23.40	N	T	1104.10	-389.65	21.60	-3283.20	-518.21	25.20
122	122	23.40	N	T	1104.10	-389.65	21.60	-3283.20	-518.21	25.20
122	123	24.80	N	T	1104.10	-212.62	23.00	-3283.20	-337.46	26.60
123	123	24.80	O	T	1705.40	-212.61	23.00	-3053.20	-337.45	26.60
123	124	26.20	O	T	1705.40	-52.18	24.40	-3053.20	-179.91	28.00
124	124	26.20	O	T	1705.40	-52.18	24.40	-3053.20	-179.91	28.00
124	125	27.60	O	T	1705.40	89.80	25.80	-3053.20	-43.64	29.40
125	125	27.60	K	C	1586.00	89.80	25.80	-128.60	-43.64	29.40
125	126	29.00	K	C	1586.00	208.94	27.20	-128.60	75.73	30.80
126	126	29.00	E	C	1586.00	208.94	27.20	-128.60	75.73	30.80
126	127	30.40	E	C	1586.00	306.19	28.60	-128.60	175.77	32.20
127	127	30.40	F	C	1699.40	306.19	28.60	-124.50	175.77	32.20
127	128	31.80	F	C	1699.40	392.21	30.00	-124.50	245.76	33.60
128	128	31.80	F	C	1699.40	392.21	30.00	-124.50	245.76	33.60
128	129	33.20	F	C	1699.40	458.07	31.40	-124.50	296.26	35.00
129	129	33.20	F	C	1699.40	458.07	31.40	-124.50	296.26	35.00
129	130	34.60	F	C	1699.40	501.05	32.80	-124.50	329.81	36.40
130	130	34.60	F	C	1699.40	501.05	32.80	-124.50	329.81	36.40
130	131	36.00	F	C	1699.40	521.22	34.20	-124.50	346.47	37.80
131	131	36.00	F	C	1699.40	521.22	37.80	-124.50	346.47	34.20
131	132	37.40	F	C	1699.40	518.53	39.20	-124.50	346.19	35.60
132	132	37.40	F	C	1699.40	518.53	39.20	-124.50	346.19	35.60
132	133	38.80	F	C	1699.40	493.03	40.60	-124.50	329.01	37.00
133	133	38.80	F	C	1699.40	493.03	40.60	-124.50	329.01	37.00
133	134	40.20	F	C	1699.40	444.69	42.00	-124.50	294.92	38.40
134	134	40.20	F	C	1699.40	444.69	42.00	-124.50	294.92	38.40
134	135	41.60	F	C	1699.40	373.51	43.40	-124.50	243.91	39.80
135	135	41.60	E	C	1586.00	373.51	43.40	-128.60	243.91	39.80
135	136	43.00	E	C	1586.00	287.97	44.80	-128.60	166.02	41.20
136	136	43.00	K	T	2472.90	287.97	44.80	-2562.80	166.02	41.20
136	137	44.40	K	T	2472.90	184.65	46.20	-2562.80	64.74	42.60
137	137	44.40	L	T	1705.40	184.64	46.20	-3053.20	64.73	42.60
137	138	45.80	L	T	1705.40	59.35	47.60	-3053.20	-54.35	44.00
138	138	45.80	L	T	1705.40	59.35	47.60	-3053.20	-54.35	44.00
138	139	47.20	L	T	1705.40	-81.55	49.00	-3053.20	-197.55	45.40
139	139	47.20	M	T	1104.10	-81.55	49.00	-3283.20	-197.55	45.40
139	140	48.60	M	T	1104.10	-242.20	50.40	-3283.20	-360.82	46.80
140	140	48.60	M	T	1104.10	-242.21	50.40	-3283.20	-360.83	46.80
140	141	50.00	M	T	1104.10	-429.15	51.80	-3283.20	-549.01	48.20
141	1141	50.00	M	T	1104.10	-429.15	48.20	-3283.20	-549.01	51.80
141	142	51.40	M	T	1104.10	-242.21	49.60	-3283.20	-360.83	53.20
142	142	51.40	M	T	1104.10	-242.21	49.60	-3283.20	-360.83	53.20
142	143	52.80	M	T	1104.10	-81.54	51.00	-3283.20	-197.54	54.60
143	143	52.80	L	T	1705.40	-81.54	51.00	-3053.20	-197.54	54.60
143	144	54.20	L	T	1705.40	59.35	52.40	-3053.20	-54.35	56.00
144	144	54.20	L	T	1705.40	59.35	52.40	-3053.20	-54.35	56.00
144	145	55.60	L	T	1705.40	184.65	53.80	-3053.20	64.74	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	K	T	2472.90	184.65	53.80	-2562.80	64.74	57.40
145	146	57.00	K	T	2472.90	287.97	55.20	-2562.80	166.02	58.80
146	146	57.00	E	C	1586.00	287.97	55.20	-128.60	166.02	58.80
146	147	58.40	E	C	1586.00	373.52	56.60	-128.60	243.92	60.20
147	147	58.40	F	C	1699.40	373.52	56.60	-124.50	243.92	60.20
147	148	59.80	F	C	1699.40	444.69	58.00	-124.50	294.92	61.60
148	148	59.80	F	C	1699.40	444.69	58.00	-124.50	294.92	61.60
148	149	61.20	F	C	1699.40	493.03	59.40	-124.50	329.01	63.00
149	149	61.20	F	C	1699.40	493.03	59.40	-124.50	329.01	63.00
149	150	62.60	F	C	1699.40	518.54	60.80	-124.50	346.20	64.40
150	150	62.60	F	C	1699.40	518.54	60.80	-124.50	346.20	64.40
150	151	64.00	F	C	1699.40	521.21	62.20	-124.50	346.46	65.80
151	151	64.00	F	C	1699.40	521.21	65.80	-124.50	346.46	62.20
151	152	65.40	F	C	1699.40	501.05	67.20	-124.50	329.81	63.60
152	152	65.40	F	C	1699.40	501.05	67.20	-124.50	329.81	63.60
152	153	66.80	F	C	1699.40	458.07	68.60	-124.50	296.26	65.00
153	153	66.80	F	C	1699.40	458.07	68.60	-124.50	296.26	65.00
153	154	68.20	F	C	1699.40	392.21	70.00	-124.50	245.76	66.40
154	154	68.20	F	C	1699.40	392.21	70.00	-124.50	245.76	66.40
154	155	69.60	F	C	1699.40	306.19	71.40	-124.50	175.77	67.80
155	155	69.60	E	C	1586.00	306.19	71.40	-128.60	175.77	67.80
155	156	71.00	E	C	1586.00	208.93	72.80	-128.60	75.72	69.20
156	156	71.00	K	C	1586.00	208.93	72.80	-128.60	75.72	69.20
156	157	72.40	K	C	1586.00	89.81	74.20	-128.60	-43.63	70.60
157	157	72.40	O	T	1705.40	89.81	74.20	-3053.20	-43.63	70.60
157	158	73.80	O	T	1705.40	-52.18	75.60	-3053.20	-179.91	72.00
158	158	73.80	O	T	1705.40	-52.18	75.60	-3053.20	-179.91	72.00
158	159	75.20	O	T	1705.40	-212.62	77.00	-3053.20	-337.46	73.40
159	159	75.20	N	T	1104.10	-212.62	77.00	-3283.20	-337.46	73.40
159	160	76.60	N	T	1104.10	-389.65	78.40	-3283.20	-518.21	74.80
160	160	76.60	N	T	1104.10	-389.65	78.40	-3283.20	-518.21	74.80
160	161	78.00	N	T	1104.10	-592.98	79.80	-3283.20	-723.89	76.20
161	1161	78.00	J	T	1015.60	-592.99	76.20	-3316.30	-723.90	79.80
161	162	79.10	J	T	1015.60	-442.96	77.30	-3316.30	-566.17	80.90
162	162	79.10	J	T	1015.60	-442.96	77.30	-3316.30	-566.17	80.90
162	163	80.20	J	T	1015.60	-309.16	78.40	-3316.30	-423.81	82.00
163	163	80.20	I	T	1620.10	-309.16	78.40	-3086.10	-423.81	82.00
163	164	81.30	I	T	1620.10	-187.56	79.50	-3086.10	-293.86	83.10
164	164	81.30	I	T	1620.10	-187.57	79.50	-3086.10	-293.87	83.10
164	165	82.40	I	T	1620.10	-77.24	80.60	-3086.10	-177.15	84.20
165	165	82.40	H	T	2045.70	-77.24	80.60	-2922.00	-177.15	84.20
165	166	83.50	H	T	2045.70	22.62	81.70	-2922.00	-74.51	85.30
166	166	83.50	G	T	2051.00	22.61	81.70	-2725.40	-74.52	85.30
166	167	84.60	G	T	2051.00	108.39	82.80	-2725.40	17.68	86.40
167	167	84.60	C	C	1412.60	108.39	82.80	-133.60	17.68	86.40
167	168	85.70	C	C	1412.60	180.94	83.90	-133.60	97.13	87.50
168	168	85.70	D	C	1524.20	180.94	83.90	-129.70	97.13	87.50
168	169	86.80	D	C	1524.20	251.70	85.00	-129.70	152.38	88.60
169	169	86.80	D	C	1524.20	251.70	85.00	-129.70	152.38	88.60
169	170	87.90	D	C	1524.20	308.38	86.10	-129.70	197.21	89.70
170	170	87.90	D	C	1524.20	308.38	86.10	-129.70	197.21	89.70
170	171	89.00	D	C	1524.20	350.96	87.20	-129.70	231.59	90.80
171	171	89.00	D	C	1524.20	350.96	87.20	-129.70	231.59	90.80
171	172	90.10	D	C	1524.20	379.44	88.30	-129.70	255.52	91.90
172	172	90.10	D	C	1524.20	379.44	88.30	-129.70	255.52	91.90
172	173	91.20	D	C	1524.20	393.83	89.40	-129.70	269.02	93.00
173	173	91.20	D	C	1524.20	393.83	89.40	-129.70	269.02	93.00
173	174	92.30	D	C	1524.20	394.13	90.50	-129.70	272.08	94.10
174	174	92.30	D	C	1524.20	394.13	94.10	-129.70	272.08	90.50
174	175	93.40	D	C	1524.20	380.32	95.20	-129.70	264.69	91.60
175	175	93.40	C	C	1412.60	380.32	95.20	-133.60	264.69	91.60
175	176	94.50	C	C	1412.60	352.41	96.30	-133.60	246.85	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE FASE 3.MZ

Construcción fase 3 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV

Coef. exc:

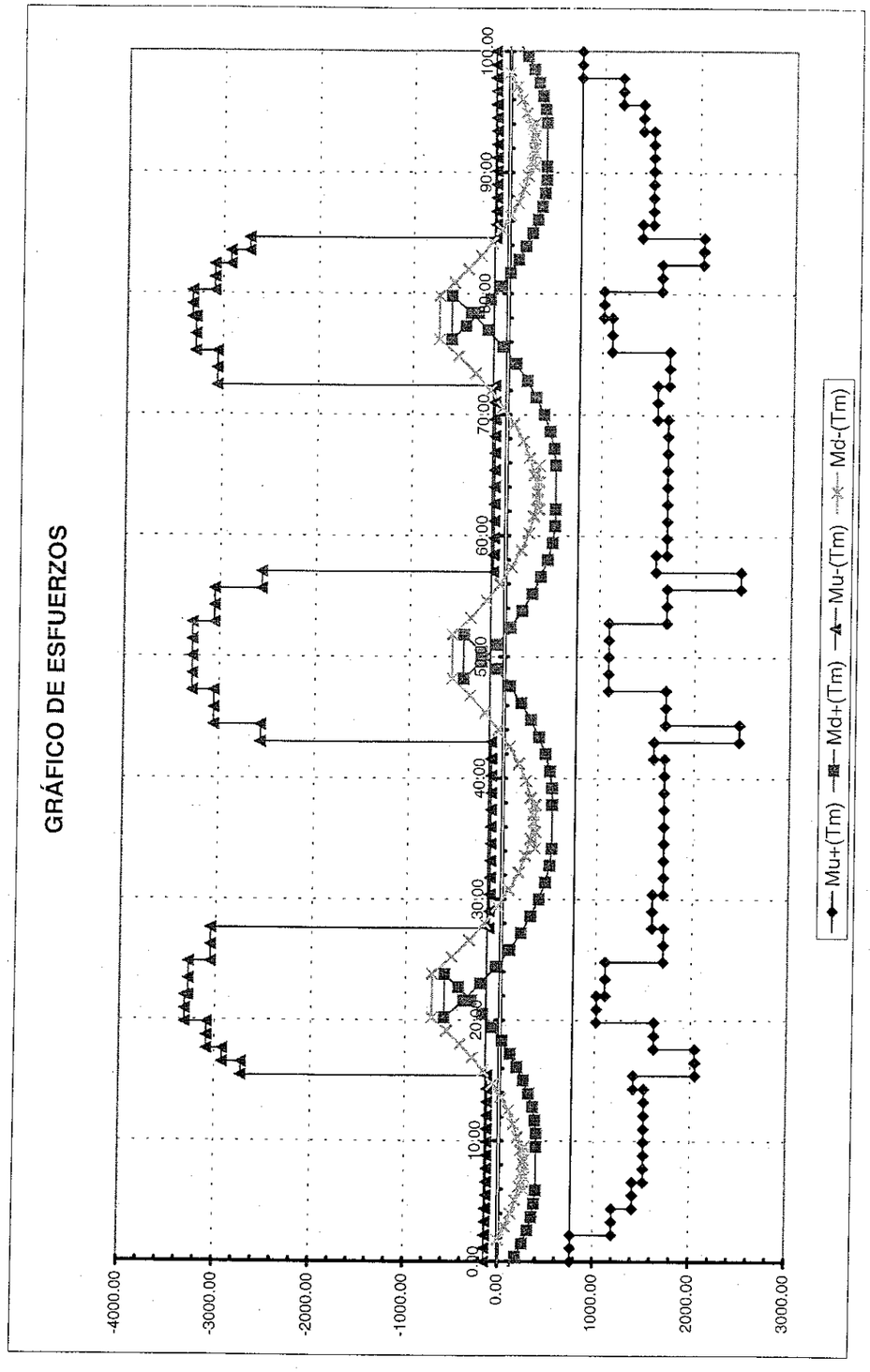
Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	C	1412.60	352.41	96.30	-133.60	246.85	92.70
176	177	95.60	C	C	1412.60	310.41	97.40	-133.60	218.58	93.80
177	177	95.60	B	C	1198.90	310.41	97.40	-140.30	218.58	93.80
177	178	96.70	B	C	1198.90	254.31	98.50	-140.30	179.86	94.90
178	178	96.70	B	C	1198.90	254.31	98.50	-140.30	179.86	94.90
178	179	97.80	B	C	1198.90	184.11	99.60	-140.30	130.70	96.00
179	179	97.80	A	C	763.70	184.11	99.60	-147.50	130.70	96.00
179	180	98.90	A	C	763.70	99.82	100.70	-147.50	71.10	97.10
180	180	98.90	A	C	763.70	99.82	100.70	-147.50	71.10	97.10
180	181	100.00	A	C	763.70	0.00	101.80	-147.50	0.00	98.20

05/09/03

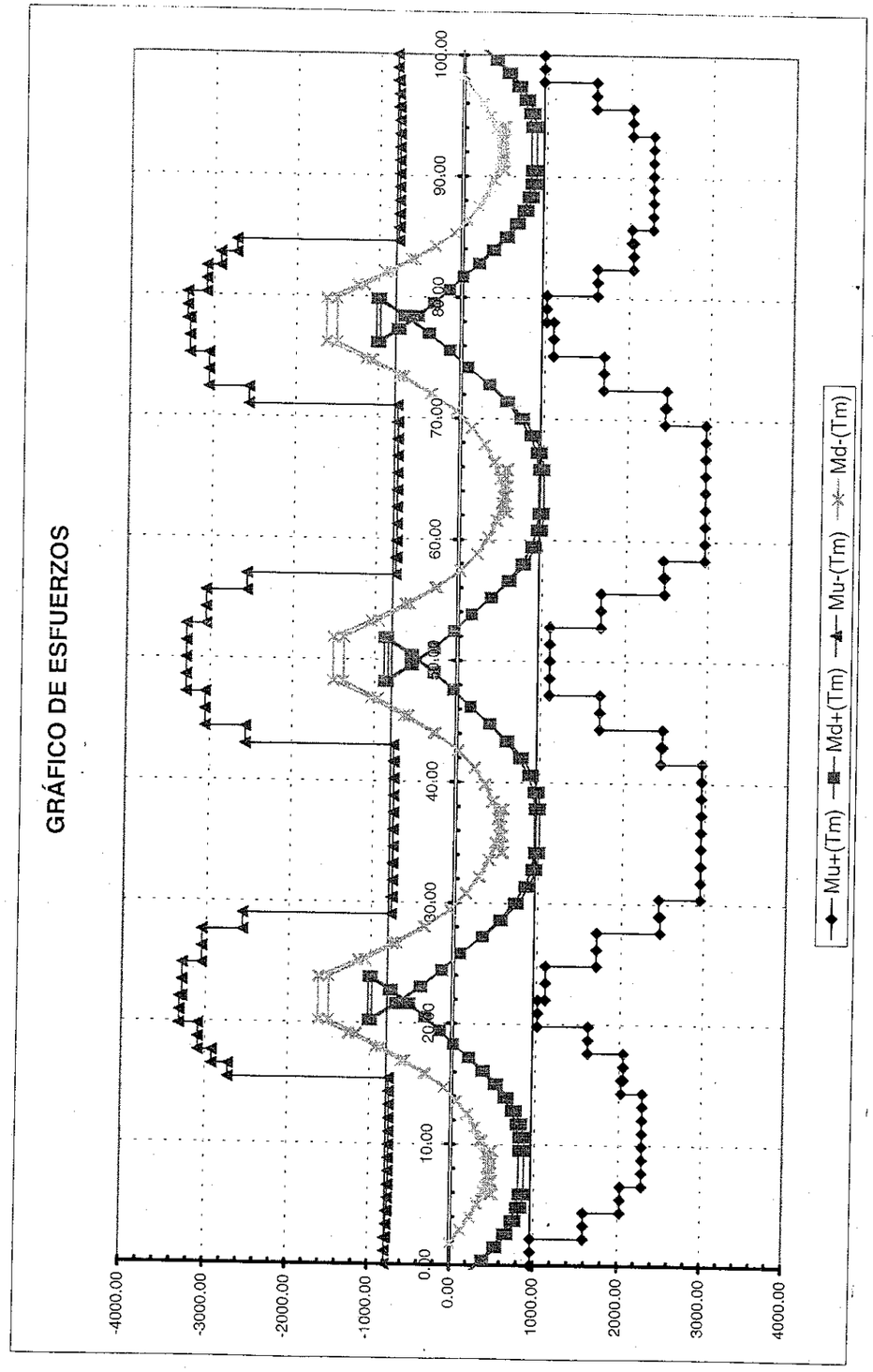
Programa DINTEL PACADAR S.A.
ENVOLOVENTE FASE 3.MZ

rotura.esf.xls



Programa DINTEL PACADAR S.A.
ENVOLOVENTE PERM.MZ

GRÁFICO DE ESFUERZOS



CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1, 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	T	962.20	1.38	-1.80	-794.10	-0.97	1.80
1	2	1.10	A	T	962.20	441.37	-0.70	-794.10	102.12	2.90
2	2	1.10	A	T	962.20	441.69	-0.70	-794.10	102.10	2.90
2	3	2.20	A	T	962.20	823.92	0.40	-794.10	183.38	4.00
3	3	2.20	B	T	1586.50	824.20	0.40	-776.80	183.37	4.00
3	4	3.30	B	T	1586.50	1149.00	1.50	-776.80	244.81	5.10
4	4	3.30	B	T	1586.50	1149.33	1.50	-776.80	244.80	5.10
4	5	4.40	B	T	1586.50	1416.36	2.60	-776.80	286.45	6.20
5	5	4.40	C	T	2025.10	1416.63	2.60	-765.40	286.44	6.20
5	6	5.50	C	T	2025.10	1637.04	3.70	-765.40	308.31	7.30
6	6	5.50	C	T	2025.10	1637.23	3.70	-765.40	308.27	7.30
6	7	6.60	C	T	2025.10	1800.44	4.80	-765.40	310.43	8.40
7	7	6.60	D	T	2284.30	1800.61	4.80	-759.60	310.37	8.40
7	8	7.70	D	T	2284.30	1906.47	5.90	-759.60	292.78	9.50
8	8	7.70	D	T	2284.30	1906.61	9.50	-759.60	292.75	5.90
8	9	8.80	D	T	2284.30	1953.40	10.60	-759.60	255.43	7.00
9	9	8.80	D	T	2284.30	1953.49	10.60	-759.60	255.38	7.00
9	10	9.90	D	T	2284.30	1953.08	11.70	-759.60	198.13	8.10
10	10	9.90	D	T	2284.30	1953.09	11.70	-759.60	198.11	8.10
10	11	11.00	D	T	2284.30	1895.92	12.80	-759.60	121.14	9.20
11	11	11.00	D	T	2284.30	1895.93	12.80	-759.60	121.11	9.20
11	12	12.10	D	T	2284.30	1781.59	13.90	-759.60	24.63	10.30
12	12	12.10	D	T	2284.30	1781.52	13.90	-759.60	24.58	10.30
12	13	13.20	D	T	2284.30	1609.03	15.00	-759.60	-91.53	11.40
13	13	13.20	D	T	2284.30	1608.93	15.00	-759.60	-91.57	11.40
13	14	14.30	D	T	2284.30	1386.26	16.10	-759.60	-227.14	12.50
14	14	14.30	C	T	2025.10	1386.10	16.10	-765.40	-227.18	12.50
14	15	15.40	C	T	2025.10	1120.00	17.20	-765.40	-396.02	13.60
15	15	15.40	G	T	2051.00	1119.83	17.20	-2725.40	-396.04	13.60
15	16	16.50	G	T	2051.00	837.11	18.30	-2725.40	-597.09	14.70
16	16	16.50	H	T	2045.70	836.80	18.30	-2922.00	-596.97	14.70
16	17	17.60	H	T	2045.70	576.20	19.40	-2922.00	-884.34	15.80
17	17	17.60	I	T	1620.10	575.75	19.40	-3086.10	-884.06	15.80
17	18	18.70	I	T	1620.10	307.38	20.50	-3086.10	-1228.53	16.90
18	18	18.70	I	T	1620.10	306.66	20.50	-3086.10	-1227.93	16.90
18	19	19.80	I	T	1620.10	56.17	21.60	-3086.10	-1639.72	18.00
19	19	19.80	J	T	1015.60	55.29	21.60	-3316.30	-1638.94	18.00
19	20	20.90	J	T	1015.60	-189.13	22.70	-3316.30	-2142.35	19.10
20	20	20.90	J	T	1015.60	-189.10	22.70	-3316.30	-2142.32	19.10
20	21	22.00	J	T	1015.60	-434.35	23.80	-3316.30	-2722.32	20.20
21	1021	22.00	N	T	1104.10	-434.36	20.20	-3283.20	-2722.19	23.80
21	22	23.40	N	T	1104.10	-116.96	21.60	-3283.20	-1950.85	25.20
22	22	23.40	N	T	1104.10	-117.04	21.60	-3283.20	-1950.63	25.20
22	23	24.80	N	T	1104.10	182.49	23.00	-3283.20	-1286.85	26.60
23	23	24.80	O	T	1705.40	182.52	23.00	-3053.20	-1286.82	26.60
23	24	26.20	O	T	1705.40	507.23	24.40	-3053.20	-776.12	28.00
24	24	26.20	O	T	1705.40	508.35	24.40	-3053.20	-777.00	28.00
24	25	27.60	O	T	1705.40	861.85	25.80	-3053.20	-382.24	29.40
25	25	27.60	K	T	2472.90	862.90	25.80	-2562.80	-383.08	29.40
25	26	29.00	K	T	2472.90	1275.11	27.20	-2562.80	-160.94	30.80
26	26	29.00	E	T	2453.10	1275.46	27.20	-757.30	-161.03	30.80
26	27	30.40	E	T	2453.10	1636.03	28.60	-757.30	-1.32	32.20
27	27	30.40	F	T	2956.70	1636.28	28.60	-749.20	-1.37	32.20
27	28	31.80	F	T	2956.70	1937.99	30.00	-749.20	112.79	33.60
28	28	31.80	F	T	2956.70	1938.24	30.00	-749.20	112.73	33.60
28	29	33.20	F	T	2956.70	2173.01	31.40	-749.20	192.66	35.00
29	29	33.20	F	T	2956.70	2173.26	31.40	-749.20	192.66	35.00
29	30	34.60	F	T	2956.70	2321.20	32.80	-749.20	239.29	36.40
30	30	34.60	F	T	2956.70	2321.31	32.80	-749.20	239.19	36.40
30	31	36.00	F	T	2956.70	2375.37	34.20	-749.20	248.40	37.80
31	31	36.00	F	T	2956.70	2375.39	37.80	-749.20	248.38	34.20
31	32	37.40	F	T	2956.70	2344.95	39.20	-749.20	222.93	35.60

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ
Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	T	2956.70	2344.88	39.20	-749.20	222.90	35.60
32	33	38.80	F	T	2956.70	2220.41	40.60	-749.20	165.71	37.00
33	33	38.80	F	T	2956.70	2220.20	40.60	-749.20	165.70	37.00
33	34	40.20	F	T	2956.70	2009.10	42.00	-749.20	76.92	38.40
34	34	40.20	F	T	2956.70	2008.84	42.00	-749.20	76.95	38.40
34	35	41.60	F	T	2956.70	1708.09	43.40	-749.20	-43.36	39.80
35	35	41.60	E	T	2453.10	1707.70	43.40	-757.30	-43.35	39.80
35	36	43.00	E	T	2453.10	1335.51	44.80	-757.30	-205.85	41.20
36	36	43.00	K	T	2472.90	1335.21	44.80	-2562.80	-205.76	41.20
36	37	44.40	K	T	2472.90	942.15	46.20	-2562.80	-442.19	42.60
37	37	44.40	L	T	1705.40	941.22	46.20	-3053.20	-441.51	42.60
37	38	45.80	L	T	1705.40	580.83	47.60	-3053.20	-824.50	44.00
38	38	45.80	L	T	1705.40	579.56	47.60	-3053.20	-823.46	44.00
38	39	47.20	L	T	1705.40	241.40	49.00	-3053.20	-1317.13	45.40
39	39	47.20	M	T	1104.10	240.74	49.00	-3283.20	-1316.56	45.40
39	40	48.60	M	T	1104.10	-75.52	50.40	-3283.20	-1950.34	46.80
40	40	48.60	M	T	1104.10	-75.48	50.40	-3283.20	-1950.38	46.80
40	41	50.00	M	T	1104.10	-403.73	51.80	-3283.20	-2707.42	48.20
41	1041	50.00	M	T	1104.10	-403.73	48.20	-3283.20	-2707.42	51.80
41	42	51.40	M	T	1104.10	-75.48	49.60	-3283.20	-1950.37	53.20
42	42	51.40	M	T	1104.10	-75.52	49.60	-3283.20	-1950.34	53.20
42	43	52.80	M	T	1104.10	240.73	51.00	-3283.20	-1316.55	54.60
43	43	52.80	L	T	1705.40	241.38	51.00	-3053.20	-1317.11	54.60
43	44	54.20	L	T	1705.40	579.56	52.40	-3053.20	-823.44	56.00
44	44	54.20	L	T	1705.40	580.83	52.40	-3053.20	-824.49	56.00
44	45	55.60	L	T	1705.40	941.26	53.80	-3053.20	-441.47	57.40
45	45	55.60	K	T	2472.90	942.17	53.80	-2562.80	-442.17	57.40
45	46	57.00	K	T	2472.90	1335.23	55.20	-2562.80	-205.70	58.80
46	46	57.00	E	T	2453.10	1335.56	55.20	-757.30	-205.83	58.80
46	47	58.40	E	T	2453.10	1707.74	56.60	-757.30	-43.34	60.20
47	47	58.40	F	T	2956.70	1708.13	56.60	-749.20	-43.36	60.20
47	48	59.80	F	T	2956.70	2008.91	58.00	-749.20	76.96	61.60
48	48	59.80	F	T	2956.70	2009.17	58.00	-749.20	76.96	61.60
48	49	61.20	F	T	2956.70	2220.21	59.40	-749.20	165.69	63.00
49	49	61.20	F	T	2956.70	2220.38	59.40	-749.20	165.70	63.00
49	50	62.60	F	T	2956.70	2344.91	60.80	-749.20	222.91	64.40
50	50	62.60	F	T	2956.70	2345.02	60.80	-749.20	222.91	64.40
50	51	64.00	F	T	2956.70	2375.40	62.20	-749.20	248.39	65.80
51	51	64.00	F	T	2956.70	2375.40	65.80	-749.20	248.39	62.20
51	52	65.40	F	T	2956.70	2321.34	67.20	-749.20	239.18	63.60
52	52	65.40	F	T	2956.70	2321.22	67.20	-749.20	239.26	63.60
52	53	66.80	F	T	2956.70	2173.34	68.60	-749.20	192.65	65.00
53	53	66.80	F	T	2956.70	2173.09	68.60	-749.20	192.67	65.00
53	54	68.20	F	T	2956.70	1938.34	70.00	-749.20	112.75	66.40
54	54	68.20	F	T	2956.70	1938.08	70.00	-749.20	112.76	66.40
54	55	69.60	F	T	2956.70	1636.32	71.40	-749.20	-1.37	67.80
55	55	69.60	E	T	2453.10	1636.09	71.40	-757.30	-1.35	67.80
55	56	71.00	E	T	2453.10	1275.48	72.80	-757.30	-161.04	69.20
56	56	71.00	K	T	2472.90	1275.14	72.80	-2562.80	-160.94	69.20
56	57	72.40	K	T	2472.90	862.92	74.20	-2562.80	-383.08	70.60
57	57	72.40	O	T	1705.40	861.87	74.20	-3053.20	-382.26	70.60
57	58	73.80	O	T	1705.40	508.34	75.60	-3053.20	-777.02	72.00
58	58	73.80	O	T	1705.40	507.22	75.60	-3053.20	-776.13	72.00
58	59	75.20	O	T	1705.40	182.51	77.00	-3053.20	-1286.85	73.40
59	59	75.20	N	T	1104.10	182.47	77.00	-3283.20	-1286.83	73.40
59	60	76.60	N	T	1104.10	-117.06	78.40	-3283.20	-1950.65	74.80
60	60	76.60	N	T	1104.10	-116.98	78.40	-3283.20	-1950.86	74.80
60	61	78.00	N	T	1104.10	-434.35	79.80	-3283.20	-2722.22	76.20
61	1061	78.00	J	T	1015.60	-434.36	79.80	-3316.30	-2722.40	79.80
61	62	79.10	J	T	1015.60	-189.12	77.30	-3316.30	-2142.37	80.90
62	62	79.10	J	T	1015.60	-189.14	77.30	-3316.30	-2142.43	80.90
62	63	80.20	J	T	1015.60	55.29	78.40	-3316.30	-1638.97	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ
Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	I	T	1620.10	56.18	78.40	-3086.10	-1639.76	82.00
63	64	81.30	I	T	1620.10	306.68	79.50	-3086.10	-1227.96	83.10
64	64	81.30	I	T	1620.10	307.37	79.50	-3086.10	-1228.57	83.10
64	65	82.40	I	T	1620.10	575.75	80.60	-3086.10	-884.07	84.20
65	65	82.40	H	T	2045.70	576.19	80.60	-2922.00	-884.37	84.20
65	66	83.50	H	T	2045.70	836.83	81.70	-2922.00	-597.00	85.30
66	66	83.50	G	T	2051.00	837.13	81.70	-2725.40	-597.10	85.30
66	67	84.60	G	T	2051.00	1119.86	82.80	-2725.40	-396.05	86.40
67	67	84.60	C	T	2025.10	1120.07	82.80	-765.40	-396.05	86.40
67	68	85.70	C	T	2025.10	1386.19	83.90	-765.40	-227.21	87.50
68	68	85.70	D	T	2284.30	1386.32	83.90	-759.60	-227.17	87.50
68	69	86.80	D	T	2284.30	1608.99	85.00	-759.60	-91.59	88.60
69	69	86.80	D	T	2284.30	1609.13	85.00	-759.60	-91.55	88.60
69	70	87.90	D	T	2284.30	1781.56	86.10	-759.60	24.54	89.70
70	70	87.90	D	T	2284.30	1781.65	86.10	-759.60	24.60	89.70
70	71	89.00	D	T	2284.30	1895.97	87.20	-759.60	121.07	90.80
71	71	89.00	D	T	2284.30	1895.99	87.20	-759.60	121.11	90.80
71	72	90.10	D	T	2284.30	1953.17	88.30	-759.60	198.07	91.90
72	72	90.10	D	T	2284.30	1953.14	88.30	-759.60	198.10	91.90
72	73	91.20	D	T	2284.30	1953.58	89.40	-759.60	255.33	93.00
73	73	91.20	D	T	2284.30	1953.49	89.40	-759.60	255.41	93.00
73	74	92.30	D	T	2284.30	1906.68	90.50	-759.60	292.72	94.10
74	74	92.30	D	T	2284.30	1906.55	94.10	-759.60	292.75	90.50
74	75	93.40	D	T	2284.30	1800.69	95.20	-759.60	310.36	91.60
75	75	93.40	C	T	2025.10	1800.48	95.20	-765.40	310.39	91.60
75	76	94.50	C	T	2025.10	1637.29	96.30	-765.40	308.26	92.70
76	76	94.50	C	T	2025.10	1637.10	96.30	-765.40	308.32	92.70
76	77	95.60	C	T	2025.10	1416.70	97.40	-765.40	286.42	93.80
77	77	95.60	B	T	1586.50	1416.43	97.40	-776.80	286.44	93.80
77	78	96.70	B	T	1586.50	1149.30	98.50	-776.80	244.77	94.90
78	78	96.70	B	T	1586.50	1149.03	98.50	-776.80	244.78	94.90
78	79	97.80	B	T	1586.50	824.16	99.60	-776.80	183.36	96.00
79	79	97.80	A	T	962.20	823.90	99.60	-794.10	183.37	96.00
79	80	98.90	A	T	962.20	441.69	100.70	-794.10	102.10	97.10
80	80	98.90	A	T	962.20	441.37	100.70	-794.10	102.12	97.10
80	81	100.00	A	T	962.20	1.38	101.80	-794.10	-0.97	98.20
101	101	0.00	A	T	962.20	1.19	-1.80	-794.10	-1.09	1.80
101	102	1.10	A	T	962.20	479.49	-0.70	-794.10	99.06	2.90
102	102	1.10	A	T	962.20	478.85	-0.70	-794.10	99.31	2.90
102	103	2.20	A	T	962.20	892.81	0.40	-794.10	177.67	4.00
103	103	2.20	B	T	1586.50	892.21	0.40	-776.80	177.91	4.00
103	104	3.30	B	T	1586.50	1242.60	1.50	-776.80	236.65	5.10
104	104	3.30	B	T	1586.50	1242.05	1.50	-776.80	236.87	5.10
104	105	4.40	B	T	1586.50	1529.97	2.60	-776.80	275.90	6.20
105	105	4.40	C	T	2025.10	1529.43	2.60	-765.40	276.06	6.20
105	106	5.50	C	T	2025.10	1766.79	3.70	-765.40	295.26	7.30
106	106	5.50	C	T	2025.10	1766.36	3.70	-765.40	295.42	7.30
106	107	6.60	C	T	2025.10	1941.75	4.80	-765.40	294.61	8.40
107	107	6.60	D	T	2284.30	1941.46	4.80	-759.60	294.76	8.40
107	108	7.70	D	T	2284.30	2054.92	5.90	-759.60	273.87	9.50
108	108	7.70	D	T	2284.30	2054.74	9.50	-759.60	274.00	5.90
108	109	8.80	D	T	2284.30	2106.33	10.60	-759.60	233.02	7.00
109	109	8.80	D	T	2284.30	2106.26	10.60	-759.60	233.11	7.00
109	110	9.90	D	T	2284.30	2105.73	11.70	-759.60	171.92	8.10
110	110	9.90	D	T	2284.30	2105.66	11.70	-759.60	171.98	8.10
110	111	11.00	D	T	2284.30	2045.25	12.80	-759.60	90.65	9.20
111	111	11.00	D	T	2284.30	2045.29	12.80	-759.60	90.69	9.20
111	112	12.10	D	T	2284.30	1923.91	13.90	-759.60	-11.03	10.30
112	112	12.10	D	T	2284.30	1924.05	13.90	-759.60	-11.01	10.30
112	113	13.20	D	T	2284.30	1741.68	15.00	-759.60	-133.06	11.40
113	113	13.20	D	T	2284.30	1741.85	15.00	-759.60	-133.10	11.40
113	114	14.30	D	T	2284.30	1505.20	16.10	-759.60	-275.50	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ

Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	T	2025.10	1505.49	16.10	-765.40	-275.57	12.50
114	115	15.40	C	T	2025.10	1222.45	17.20	-765.40	-452.25	13.60
115	115	15.40	G	T	2051.00	1222.79	17.20	-2725.40	-452.36	13.60
115	116	16.50	G	T	2051.00	903.27	18.30	-2725.40	-662.98	14.70
116	116	16.50	H	T	2045.70	903.61	18.30	-2922.00	-663.13	14.70
116	117	17.60	H	T	2045.70	616.32	19.40	-2922.00	-949.61	15.80
117	117	17.60	I	T	1620.10	616.55	19.40	-3086.10	-949.55	15.80
117	118	18.70	I	T	1620.10	327.54	20.50	-3086.10	-1301.69	16.90
118	118	18.70	I	T	1620.10	327.23	20.50	-3086.10	-1301.29	16.90
118	119	19.80	I	T	1620.10	71.09	21.60	-3086.10	-1734.01	18.00
119	119	19.80	J	T	1015.60	70.77	21.60	-3316.30	-1733.70	18.00
119	120	20.90	J	T	1015.60	-165.79	22.70	-3316.30	-2280.44	19.10
120	120	20.90	J	T	1015.60	-165.78	22.70	-3316.30	-2280.37	19.10
120	121	22.00	J	T	1015.60	-404.65	23.80	-3316.30	-2906.01	20.20
121	1121	22.00	N	T	1104.10	-404.65	20.20	-3283.20	-2906.00	23.80
121	122	23.40	N	T	1104.10	-92.89	21.60	-3283.20	-2081.33	25.20
122	122	23.40	N	T	1104.10	-92.86	21.60	-3283.20	-2081.47	25.20
122	123	24.80	N	T	1104.10	208.37	23.00	-3283.20	-1377.74	26.60
123	123	24.80	O	T	1705.40	208.15	23.00	-3053.20	-1377.76	26.60
123	124	26.20	O	T	1705.40	539.31	24.40	-3053.20	-841.12	28.00
124	124	26.20	O	T	1705.40	539.74	24.40	-3053.20	-841.78	28.00
124	125	27.60	O	T	1705.40	914.91	25.80	-3053.20	-436.32	29.40
125	125	27.60	K	T	2472.90	915.16	25.80	-2562.80	-436.84	29.40
125	126	29.00	K	T	2472.90	1337.94	27.20	-2562.80	-199.06	30.80
126	126	29.00	E	T	2453.10	1337.66	27.20	-757.30	-198.95	30.80
126	127	30.40	E	T	2453.10	1720.11	28.60	-757.30	-31.97	32.20
127	127	30.40	F	T	2956.70	1719.70	28.60	-749.20	-31.89	32.20
127	128	31.80	F	T	2956.70	2057.02	30.00	-749.20	88.00	33.60
128	128	31.80	F	T	2956.70	2056.69	30.00	-749.20	88.07	33.60
128	129	33.20	F	T	2956.70	2302.79	31.40	-749.20	172.05	35.00
129	129	33.20	F	T	2956.70	2302.55	31.40	-749.20	172.09	35.00
129	130	34.60	F	T	2956.70	2457.97	32.80	-749.20	221.57	36.40
130	130	34.60	F	T	2956.70	2457.87	32.80	-749.20	221.52	36.40
130	131	36.00	F	T	2956.70	2513.93	34.20	-749.20	231.13	37.80
131	131	36.00	F	T	2956.70	2513.89	37.80	-749.20	231.15	34.20
131	132	37.40	F	T	2956.70	2482.28	39.20	-749.20	203.63	35.60
132	132	37.40	F	T	2956.70	2482.36	39.20	-749.20	203.63	35.60
132	133	38.80	F	T	2956.70	2351.21	40.60	-749.20	142.84	37.00
133	133	38.80	F	T	2956.70	2351.46	40.60	-749.20	142.81	37.00
133	134	40.20	F	T	2956.70	2130.06	42.00	-749.20	48.72	38.40
134	134	40.20	F	T	2956.70	2130.37	42.00	-749.20	48.67	38.40
134	135	41.60	F	T	2956.70	1814.79	43.40	-749.20	-78.85	39.80
135	135	41.60	E	T	2453.10	1815.19	43.40	-757.30	-78.91	39.80
135	136	43.00	E	T	2453.10	1412.52	44.80	-757.30	-250.35	41.20
136	136	43.00	K	T	2472.90	1412.94	44.80	-2562.80	-250.42	41.20
136	137	44.40	K	T	2472.90	996.76	46.20	-2562.80	-501.36	42.60
137	137	44.40	L	T	1705.40	996.65	46.20	-3053.20	-501.02	42.60
137	138	45.80	L	T	1705.40	614.12	47.60	-3053.20	-894.80	44.00
138	138	45.80	L	T	1705.40	613.57	47.60	-3053.20	-894.01	44.00
138	139	47.20	L	T	1705.40	267.23	49.00	-3053.20	-1411.78	45.40
139	139	47.20	M	T	1104.10	267.06	49.00	-3283.20	-1411.48	45.40
139	140	48.60	M	T	1104.10	-47.04	50.40	-3283.20	-2088.97	46.80
140	140	48.60	M	T	1104.10	-47.04	50.40	-3283.20	-2088.84	46.80
140	141	50.00	M	T	1104.10	-368.80	51.80	-3283.20	-2901.59	48.20
141	1141	50.00	M	T	1104.10	-368.80	48.20	-3283.20	-2901.59	51.80
141	142	51.40	M	T	1104.10	-47.05	49.60	-3283.20	-2088.81	53.20
142	142	51.40	M	T	1104.10	-47.06	49.60	-3283.20	-2088.95	53.20
142	143	52.80	M	T	1104.10	267.06	51.00	-3283.20	-1411.44	54.60
143	143	52.80	L	T	1705.40	267.24	51.00	-3053.20	-1411.74	54.60
143	144	54.20	L	T	1705.40	613.58	52.40	-3053.20	-893.99	56.00
144	144	54.20	L	T	1705.40	614.13	52.40	-3053.20	-894.77	56.00
144	145	55.60	L	T	1705.40	996.68	53.80	-3053.20	-500.96	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ

Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	K	T	2472.90	996.79	53.80	-2562.80	-501.31	57.40
145	146	57.00	K	T	2472.90	1413.03	55.20	-2562.80	-250.40	58.80
146	146	57.00	E	T	2453.10	1412.61	55.20	-757.30	-250.33	58.80
146	147	58.40	E	T	2453.10	1815.28	56.60	-757.30	-78.89	60.20
147	147	58.40	F	T	2956.70	1814.85	56.60	-749.20	-78.82	60.20
147	148	59.80	F	T	2956.70	2130.44	58.00	-749.20	48.65	61.60
148	148	59.80	F	T	2956.70	2130.15	58.00	-749.20	48.73	61.60
148	149	61.20	F	T	2956.70	2351.51	59.40	-749.20	142.83	63.00
149	149	61.20	F	T	2956.70	2351.30	59.40	-749.20	142.83	63.00
149	150	62.60	F	T	2956.70	2482.49	60.80	-749.20	203.63	64.40
150	150	62.60	F	T	2956.70	2482.40	60.80	-749.20	203.63	64.40
150	151	64.00	F	T	2956.70	2513.98	62.20	-749.20	231.11	65.80
151	151	64.00	F	T	2956.70	2514.00	65.80	-749.20	231.10	62.20
151	152	65.40	F	T	2956.70	2457.93	67.20	-749.20	221.49	63.60
152	152	65.40	F	T	2956.70	2458.04	67.20	-749.20	221.55	63.60
152	153	66.80	F	T	2956.70	2302.66	68.60	-749.20	172.06	65.00
153	153	66.80	F	T	2956.70	2302.89	68.60	-749.20	172.03	65.00
153	154	68.20	F	T	2956.70	2056.78	70.00	-749.20	88.01	66.40
154	154	68.20	F	T	2956.70	2057.07	70.00	-749.20	87.96	66.40
154	155	69.60	F	T	2956.70	1719.76	71.40	-749.20	-31.93	67.80
155	155	69.60	E	T	2453.10	1720.20	71.40	-757.30	-32.00	67.80
155	156	71.00	E	T	2453.10	1337.71	72.80	-757.30	-198.98	69.20
156	156	71.00	K	T	2472.90	1337.99	72.80	-2562.80	-199.10	69.20
156	157	72.40	K	T	2472.90	915.18	74.20	-2562.80	-436.86	70.60
157	157	72.40	O	T	1705.40	914.93	74.20	-3053.20	-436.32	70.60
157	158	73.80	O	T	1705.40	539.72	75.60	-3053.20	-841.80	72.00
158	158	73.80	O	T	1705.40	539.29	75.60	-3053.20	-841.14	72.00
158	159	75.20	O	T	1705.40	208.13	77.00	-3053.20	-1377.76	73.40
159	159	75.20	N	T	1104.10	208.38	77.00	-3283.20	-1377.76	73.40
159	160	76.60	N	T	1104.10	-92.86	78.40	-3283.20	-2081.49	74.80
160	160	76.60	N	T	1104.10	-92.90	78.40	-3283.20	-2081.39	74.80
160	161	78.00	N	T	1104.10	-404.63	79.80	-3283.20	-2906.05	76.20
161	1161	78.00	J	T	1015.60	-404.67	76.20	-3316.30	-2906.08	79.80
161	162	79.10	J	T	1015.60	-165.79	77.30	-3316.30	-2280.41	80.90
162	162	79.10	J	T	1015.60	-165.84	77.30	-3316.30	-2280.52	80.90
162	163	80.20	J	T	1015.60	70.76	78.40	-3316.30	-1733.74	82.00
163	163	80.20	I	T	1620.10	71.06	78.40	-3086.10	-1734.05	82.00
163	164	81.30	I	T	1620.10	327.25	79.50	-3086.10	-1301.32	83.10
164	164	81.30	I	T	1620.10	327.54	79.50	-3086.10	-1301.72	83.10
164	165	82.40	I	T	1620.10	616.56	80.60	-3086.10	-949.68	84.20
165	165	82.40	H	T	2045.70	616.36	80.60	-2922.00	-949.63	84.20
165	166	83.50	H	T	2045.70	903.66	81.70	-2922.00	-663.18	85.30
166	166	83.50	G	T	2051.00	903.33	81.70	-2725.40	-663.00	85.30
166	167	84.60	G	T	2051.00	1222.85	82.80	-2725.40	-452.38	86.40
167	167	84.60	C	T	2025.10	1222.50	82.80	-765.40	-452.29	86.40
167	168	85.70	C	T	2025.10	1505.56	83.90	-765.40	-275.59	87.50
168	168	85.70	D	T	2284.30	1505.25	83.90	-759.60	-275.54	87.50
168	169	86.80	D	T	2284.30	1741.95	85.00	-759.60	-133.12	88.60
169	169	86.80	D	T	2284.30	1741.71	85.00	-759.60	-133.09	88.60
169	170	87.90	D	T	2284.30	1924.10	86.10	-759.60	-11.04	89.70
170	170	87.90	D	T	2284.30	1923.96	86.10	-759.60	-11.05	89.70
170	171	89.00	D	T	2284.30	2045.35	87.20	-759.60	90.66	90.80
171	171	89.00	D	T	2284.30	2045.28	87.20	-759.60	90.63	90.80
171	172	90.10	D	T	2284.30	2105.69	88.30	-759.60	171.97	91.90
172	172	90.10	D	T	2284.30	2105.74	88.30	-759.60	171.91	91.90
172	173	91.20	D	T	2284.30	2106.27	89.40	-759.60	233.07	93.00
173	173	91.20	D	T	2284.30	2106.38	89.40	-759.60	232.98	93.00
173	174	92.30	D	T	2284.30	2054.80	90.50	-759.60	273.98	94.10
174	174	92.30	D	T	2284.30	2054.98	94.10	-759.60	273.86	90.50
174	175	93.40	D	T	2284.30	1941.52	95.20	-759.60	294.74	91.60
175	175	93.40	C	T	2025.10	1941.80	95.20	-765.40	294.60	91.60
175	176	94.50	C	T	2025.10	1766.43	96.30	-765.40	295.42	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales t0 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1t3.HIP.To + [1; 1]eje2t3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [0; 1.8]TRENM.MZ + [0; .75]SCPASI

Coef. exc:

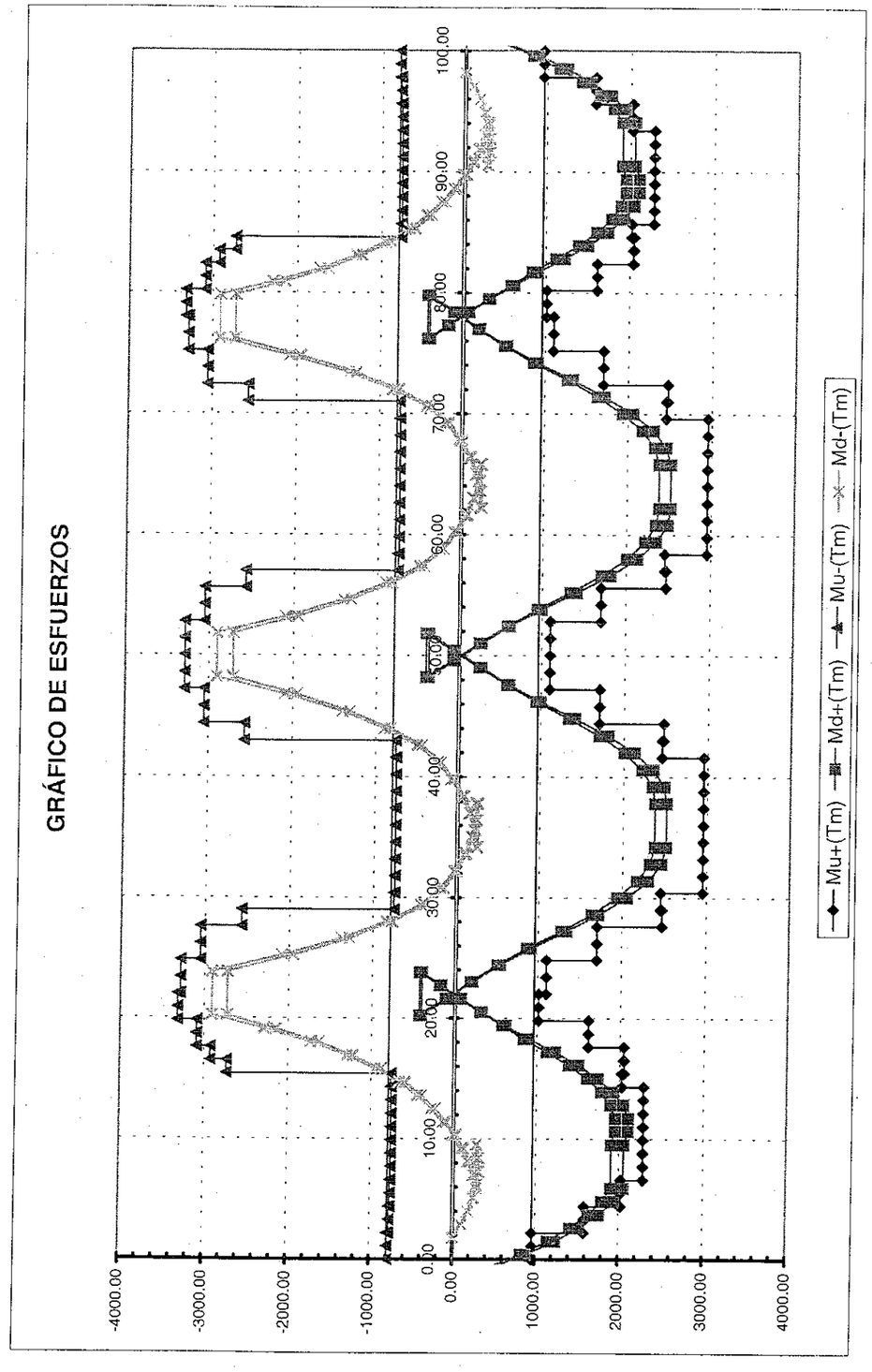
Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	T	2025.10	1766.86	96.30	-765.40	295.26	92.70
176	177	95.60	C	T	2025.10	1529.49	97.40	-765.40	276.06	93.80
177	177	95.60	B	T	1586.50	1529.99	97.40	-776.80	275.87	93.80
177	178	96.70	B	T	1586.50	1242.06	98.50	-776.80	236.83	94.90
178	178	96.70	B	T	1586.50	1242.60	98.50	-776.80	236.65	94.90
178	179	97.80	B	T	1586.50	892.19	99.60	-776.80	177.90	96.00
179	179	97.80	A	T	962.20	892.81	99.60	-794.10	177.66	96.00
179	180	98.90	A	T	962.20	478.87	100.70	-794.10	99.31	97.10
180	180	98.90	A	T	962.20	479.49	100.70	-794.10	99.06	97.10
180	181	100.00	A	T	962.20	1.19	101.80	-794.10	-1.09	98.20

05/09/03

GRÁFICO DE ESFUERZOS

Programa DINTEL PACADAR S.A.
ENVOLOVENTE INFREC.MZ



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CÁLCULO EN ROTURA

Hipótesis de cálculo:
VVOLOVENTE PERM.MZ

Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	T	962.20	-0.03	-1.80	-794.10	-0.09	1.80
1	2	1.10	A	T	962.20	272.55	-0.70	-794.10	153.23	2.90
2	2	1.10	B	T	1586.50	272.38	-0.70	-776.80	153.16	2.90
2	3	2.20	B	T	1586.50	512.37	0.40	-776.80	287.47	4.00
3	3	2.20	B	T	1586.50	512.20	0.40	-776.80	287.40	4.00
3	4	3.30	B	T	1586.50	720.21	1.50	-776.80	402.74	5.10
4	4	3.30	C	T	2025.10	720.07	1.50	-765.40	402.68	5.10
4	5	4.40	C	T	2025.10	896.22	2.60	-765.40	499.11	6.20
5	5	4.40	C	T	2025.10	896.10	2.60	-765.40	499.06	6.20
5	6	5.50	C	T	2025.10	1040.44	3.70	-765.40	576.59	7.30
6	6	5.50	D	T	2453.10	1040.35	3.70	-757.30	576.55	7.30
6	7	6.60	D	T	2453.10	1152.96	4.80	-757.30	635.22	8.40
7	7	6.60	D	T	2453.10	1152.89	4.80	-757.30	635.20	8.40
7	8	7.70	D	T	2453.10	1233.76	5.90	-757.30	674.99	9.50
8	8	7.70	D	T	2453.10	1233.70	5.90	-757.30	674.96	9.50
8	9	8.80	D	T	2453.10	1282.88	7.00	-757.30	695.92	10.60
9	9	8.80	D	T	2453.10	1282.86	7.00	-757.30	695.90	7.00
9	10	9.90	D	T	2453.10	1300.36	8.10	-757.30	698.00	8.10
10	10	9.90	D	T	2453.10	1300.38	11.70	-757.30	698.02	8.10
10	11	11.00	D	T	2453.10	1286.19	12.80	-757.30	681.27	9.20
11	11	11.00	D	T	2453.10	1286.23	12.80	-757.30	681.29	9.20
11	12	12.10	D	T	2453.10	1240.34	13.90	-757.30	645.68	10.30
12	12	12.10	D	T	2453.10	1240.41	13.90	-757.30	645.71	10.30
12	13	13.20	D	T	2453.10	1162.79	15.00	-757.30	591.25	11.40
13	13	13.20	D	T	2453.10	1162.88	15.00	-757.30	591.29	11.40
13	14	14.30	D	T	2453.10	1053.50	16.10	-757.30	517.93	12.50
14	14	14.30	C	T	2025.10	1053.61	16.10	-765.40	517.99	12.50
14	15	15.40	C	T	2025.10	925.22	17.20	-765.40	412.63	13.60
15	15	15.40	G	T	2051.00	925.34	17.20	-2725.40	412.67	13.60
15	16	16.50	G	T	2051.00	776.63	18.30	-2725.40	276.51	14.70
16	16	16.50	G	T	2051.00	776.68	18.30	-2725.40	276.64	14.70
16	17	17.60	G	T	2051.00	660.54	19.40	-2725.40	57.01	15.80
17	17	17.60	H	T	1620.10	660.59	19.40	-3086.00	57.14	15.80
17	18	18.70	H	T	1620.10	525.51	20.50	-3086.00	-194.42	16.90
18	18	18.70	H	T	1620.10	525.56	20.50	-3086.00	-194.31	16.90
18	19	19.80	H	T	1620.10	370.68	21.60	-3086.00	-477.03	18.00
19	19	19.80	I	T	1015.60	370.72	21.60	-3316.30	-476.96	18.00
19	20	20.90	I	T	1015.60	195.11	22.70	-3316.30	-790.05	19.10
20	20	20.90	I	T	1015.60	195.13	22.70	-3316.30	-790.01	19.10
20	21	22.00	I	T	1015.60	-3.00	23.80	-3316.30	-1133.43	20.20
21	1021	22.00	J	T	1104.10	-2.99	20.20	-3283.20	-1133.44	23.80
21	22	23.40	J	T	1104.10	311.52	21.60	-3283.20	-673.72	25.20
22	22	23.40	J	T	1104.10	311.49	21.60	-3283.20	-673.82	25.20
22	23	24.80	J	T	1104.10	589.52	23.00	-3283.20	-263.23	26.60
23	23	24.80	K	T	1705.40	589.45	23.00	-3053.20	-263.38	26.60
23	24	26.20	K	T	1705.40	837.07	24.40	-3053.20	94.92	28.00
24	24	26.20	L	T	1705.40	837.01	24.40	-2850.70	94.75	28.00
24	25	27.60	L	T	1705.40	1052.43	25.80	-2850.70	402.85	29.40
25	25	27.60	M	T	2472.90	1052.34	25.80	-2562.80	402.65	29.40
25	26	29.00	M	T	2472.90	1308.19	27.20	-2562.80	587.97	30.80
26	26	29.00	E	T	2453.10	1308.02	27.20	-757.30	587.90	30.80
26	27	30.40	E	T	2453.10	1517.39	28.60	-757.30	737.25	32.20
27	27	30.40	F	T	3123.60	1517.23	28.60	-746.10	737.19	32.20
27	28	31.80	F	T	3123.60	1687.26	30.00	-746.10	843.47	33.60
28	28	31.80	F	T	3123.60	1687.14	30.00	-746.10	843.42	33.60
28	29	33.20	F	T	3123.60	1808.48	31.40	-746.10	916.55	35.00
29	29	33.20	F	T	3123.60	1808.38	31.40	-746.10	916.51	35.00
29	30	34.60	F	T	3123.60	1878.50	32.80	-746.10	959.17	36.40
30	30	34.60	F	T	3123.60	1878.45	32.80	-746.10	959.15	36.40
30	31	36.00	F	T	3123.60	1897.31	34.20	-746.10	971.30	37.80
31	31	36.00	F	T	3123.60	1897.33	37.80	-746.10	971.30	34.20
31	32	37.40	F	T	3123.60	1864.97	39.20	-746.10	952.95	35.60

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE PERM.MZ

Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	T	3123.60	1865.03	39.20	-746.10	952.98	35.60
32	33	38.80	F	T	3123.60	1781.49	40.60	-746.10	904.16	37.00
33	33	38.80	F	T	3123.60	1781.58	40.60	-746.10	904.21	37.00
33	34	40.20	F	T	3123.60	1646.73	42.00	-746.10	824.86	38.40
34	34	40.20	F	T	3123.60	1646.85	42.00	-746.10	824.91	38.40
34	35	41.60	F	T	3123.60	1460.72	43.40	-746.10	715.06	39.80
35	35	41.60	E	T	2453.10	1460.86	43.40	-757.30	715.11	39.80
35	36	43.00	E	T	2453.10	1232.22	44.80	-757.30	565.38	41.20
36	36	43.00	M	T	2472.90	1232.42	44.80	-2562.80	565.46	41.20
36	37	44.40	M	T	2472.90	977.76	46.20	-2562.80	359.10	42.60
37	37	44.40	L	T	1705.40	977.84	46.20	-2850.70	359.29	42.60
37	38	45.80	L	T	1705.40	750.87	47.60	-2850.70	43.04	44.00
38	38	45.80	K	T	1705.40	750.94	47.60	-3053.20	43.22	44.00
38	39	47.20	K	T	1705.40	494.55	49.00	-3053.20	-326.21	45.40
39	39	47.20	J	T	1104.10	494.60	49.00	-3283.20	-326.08	45.40
39	40	48.60	J	T	1104.10	204.69	50.40	-3283.20	-744.59	46.80
40	40	48.60	J	T	1104.10	204.73	50.40	-3283.20	-744.50	46.80
40	41	50.00	J	T	1104.10	-121.71	51.80	-3283.20	-1212.20	48.20
41	1041	50.00	J	T	1104.10	-121.71	48.20	-3283.20	-1212.20	51.80
41	42	51.40	J	T	1104.10	204.72	49.60	-3283.20	-744.51	53.20
42	42	51.40	J	T	1104.10	204.68	49.60	-3283.20	-744.60	53.20
42	43	52.80	J	T	1104.10	494.60	51.00	-3283.20	-326.08	54.60
43	43	52.80	K	T	1705.40	494.54	51.00	-3053.20	-326.22	54.60
43	44	54.20	K	T	1705.40	750.93	52.40	-3053.20	43.21	56.00
44	44	54.20	L	T	1705.40	750.86	52.40	-2850.70	43.02	56.00
44	45	55.60	L	T	1705.40	977.86	53.80	-2850.70	359.32	57.40
45	45	55.60	M	T	2472.90	977.78	53.80	-2562.80	359.13	57.40
45	46	57.00	M	T	2472.90	1232.41	55.20	-2562.80	565.45	58.80
46	46	57.00	E	T	2453.10	1232.24	55.20	-757.30	565.38	58.80
46	47	58.40	E	T	2453.10	1460.86	56.60	-757.30	715.11	60.20
47	47	58.40	F	T	3123.60	1460.71	56.60	-746.10	715.05	60.20
47	48	59.80	F	T	3123.60	1646.89	58.00	-746.10	824.93	61.60
48	48	59.80	F	T	3123.60	1646.77	58.00	-746.10	824.88	61.60
48	49	61.20	F	T	3123.60	1781.56	59.40	-746.10	904.20	63.00
49	49	61.20	F	T	3123.60	1781.48	59.40	-746.10	904.17	63.00
49	50	62.60	F	T	3123.60	1865.03	60.80	-746.10	952.98	64.40
50	50	62.60	F	T	3123.60	1864.97	60.80	-746.10	952.95	64.40
50	51	64.00	F	T	3123.60	1897.30	62.20	-746.10	971.28	65.80
51	51	64.00	F	T	3123.60	1897.31	65.80	-746.10	971.29	62.20
51	52	65.40	F	T	3123.60	1878.44	67.20	-746.10	959.14	63.60
52	52	65.40	F	T	3123.60	1878.47	67.20	-746.10	959.15	63.60
52	53	66.80	F	T	3123.60	1808.39	68.60	-746.10	916.51	65.00
53	53	66.80	F	T	3123.60	1808.48	68.60	-746.10	916.55	65.00
53	54	68.20	F	T	3123.60	1687.15	70.00	-746.10	843.42	66.40
54	54	68.20	F	T	3123.60	1687.28	70.00	-746.10	843.48	66.40
54	55	69.60	F	T	3123.60	1517.23	71.40	-746.10	737.17	67.80
55	55	69.60	E	T	2453.10	1517.38	71.40	-757.30	737.24	67.80
55	56	71.00	E	T	2453.10	1308.03	72.80	-757.30	587.90	69.20
56	56	71.00	M	T	2472.90	1308.21	72.80	-2562.80	587.97	69.20
56	57	72.40	M	T	2472.90	1052.35	74.20	-2562.80	402.66	70.60
57	57	72.40	L	T	1705.40	1052.41	74.20	-2850.70	402.83	70.60
57	58	73.80	L	T	1705.40	837.00	75.60	-2850.70	94.74	72.00
58	58	73.80	K	T	1705.40	837.06	75.60	-3053.20	94.90	72.00
58	59	75.20	K	T	1705.40	589.45	77.00	-3053.20	-263.39	73.40
59	59	75.20	J	T	1104.10	589.52	77.00	-3283.20	-263.23	73.40
59	60	76.60	J	T	1104.10	311.50	78.40	-3283.20	-673.81	74.80
60	60	76.60	J	T	1104.10	311.52	78.40	-3283.20	-673.73	74.80
60	61	78.00	J	T	1104.10	-2.99	79.80	-3283.20	-1133.43	76.20
61	1061	78.00	I	T	1015.60	-2.97	76.20	-3316.30	-1133.42	79.80
61	62	79.10	I	T	1015.60	195.12	77.30	-3316.30	-790.02	80.90
62	62	79.10	I	T	1015.60	195.10	77.30	-3316.30	-790.07	80.90
62	63	80.20	I	T	1015.60	370.71	78.40	-3316.30	-476.97	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE PERM.MZ
Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	H	T	1620.10	370.68	78.40	-3086.00	-477.05	82.00
63	64	81.30	H	T	1620.10	525.56	79.50	-3086.00	-194.31	83.10
64	64	81.30	H	T	1620.10	525.52	79.50	-3086.00	-194.41	83.10
64	65	82.40	H	T	1620.10	660.59	80.60	-3086.00	57.15	84.20
65	65	82.40	G	T	2051.00	660.54	80.60	-2725.40	57.02	84.20
65	66	83.50	G	T	2051.00	776.66	81.70	-2725.40	276.62	85.30
66	66	83.50	G	T	2051.00	776.62	81.70	-2725.40	276.51	85.30
66	67	84.60	G	T	2051.00	925.33	82.80	-2725.40	412.67	86.40
67	67	84.60	C	T	2025.10	925.21	82.80	-765.40	412.62	86.40
67	68	85.70	C	T	2025.10	1053.61	83.90	-765.40	517.98	87.50
68	68	85.70	D	T	2453.10	1053.48	83.90	-757.30	517.92	87.50
68	69	86.80	D	T	2453.10	1162.87	85.00	-757.30	591.29	88.60
69	69	86.80	D	T	2453.10	1162.78	85.00	-757.30	591.25	88.60
69	70	87.90	D	T	2453.10	1240.39	86.10	-757.30	645.71	89.70
70	70	87.90	D	T	2453.10	1240.32	86.10	-757.30	645.68	89.70
70	71	89.00	D	T	2453.10	1286.21	87.20	-757.30	681.28	90.80
71	71	89.00	D	T	2453.10	1286.19	87.20	-757.30	681.27	90.80
71	72	90.10	D	T	2453.10	1300.38	88.30	-757.30	698.02	91.90
72	72	90.10	D	T	2453.10	1300.35	91.90	-757.30	698.00	88.30
72	73	91.20	D	T	2453.10	1282.84	93.00	-757.30	695.89	89.40
73	73	91.20	D	T	2453.10	1282.87	93.00	-757.30	695.90	89.40
73	74	92.30	D	T	2453.10	1233.70	94.10	-757.30	674.95	90.50
74	74	92.30	D	T	2453.10	1233.73	94.10	-757.30	674.96	90.50
74	75	93.40	D	T	2453.10	1152.87	95.20	-757.30	635.18	91.60
75	75	93.40	D	T	2453.10	1152.96	95.20	-757.30	635.23	91.60
75	76	94.50	D	T	2453.10	1040.33	96.30	-757.30	576.54	92.70
76	76	94.50	C	T	2025.10	1040.44	96.30	-765.40	576.58	92.70
76	77	95.60	C	T	2025.10	896.09	97.40	-765.40	499.06	93.80
77	77	95.60	C	T	2025.10	896.24	97.40	-765.40	499.12	93.80
77	78	96.70	C	T	2025.10	720.06	98.50	-765.40	402.68	94.90
78	78	96.70	B	T	1586.50	720.23	98.50	-776.80	402.75	94.90
78	79	97.80	B	T	1586.50	512.19	99.60	-776.80	287.40	96.00
79	79	97.80	B	T	1586.50	512.36	99.60	-776.80	287.47	96.00
79	80	98.90	B	T	1586.50	272.37	100.70	-776.80	153.16	97.10
80	80	98.90	A	T	962.20	272.55	100.70	-794.10	153.23	97.10
80	81	100.00	A	T	962.20	-0.03	101.80	-794.10	-0.09	98.20
101	101	0.00	A	T	962.20	0.09	-1.80	-794.10	0.03	1.80
101	102	1.10	A	T	962.20	255.12	-0.70	-794.10	146.28	2.90
102	102	1.10	B	T	1586.50	255.32	-0.70	-776.80	146.36	2.90
102	103	2.20	B	T	1586.50	480.62	0.40	-776.80	274.81	4.00
103	103	2.20	B	T	1586.50	480.80	0.40	-776.80	274.88	4.00
103	104	3.30	B	T	1586.50	676.89	1.50	-776.80	385.45	5.10
104	104	3.30	C	T	2025.10	677.06	1.50	-765.40	385.52	5.10
104	105	4.40	C	T	2025.10	843.93	2.60	-765.40	478.27	6.20
105	105	4.40	C	T	2025.10	844.04	2.60	-765.40	478.30	6.20
105	106	5.50	C	T	2025.10	981.58	3.70	-765.40	553.12	7.30
106	106	5.50	D	T	2453.10	981.68	3.70	-757.30	553.16	7.30
106	107	6.60	D	T	2453.10	1089.87	4.80	-757.30	610.06	8.40
107	107	6.60	D	T	2453.10	1089.93	4.80	-757.30	610.08	8.40
107	108	7.70	D	T	2453.10	1168.67	5.90	-757.30	649.02	9.50
108	108	7.70	D	T	2453.10	1168.72	5.90	-757.30	649.04	5.90
108	109	8.80	D	T	2453.10	1218.04	7.00	-757.30	670.04	7.00
109	109	8.80	D	T	2453.10	1218.04	7.00	-757.30	670.03	7.00
109	110	9.90	D	T	2453.10	1237.92	8.10	-757.30	673.10	8.10
110	110	9.90	D	T	2453.10	1237.91	11.70	-757.30	673.10	8.10
110	111	11.00	D	T	2453.10	1228.35	12.80	-757.30	658.20	9.20
111	111	11.00	D	T	2453.10	1228.29	12.80	-757.30	658.17	9.20
111	112	12.10	D	T	2453.10	1189.28	13.90	-757.30	625.32	10.30
112	112	12.10	D	T	2453.10	1189.20	13.90	-757.30	625.28	10.30
112	113	13.20	D	T	2453.10	1120.80	15.00	-757.30	574.51	11.40
113	113	13.20	D	T	2453.10	1120.72	15.00	-757.30	574.47	11.40
113	114	14.30	D	T	2453.10	1022.93	16.10	-757.30	505.75	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE PERM.MZ
Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	T	2025.10	1022.83	16.10	-765.40	505.72	12.50
114	115	15.40	C	T	2025.10	908.47	17.20	-765.40	405.95	13.60
115	115	15.40	G	T	2051.00	908.34	17.20	-2725.40	405.89	13.60
115	116	16.50	G	T	2051.00	776.49	18.30	-2725.40	276.16	14.70
116	116	16.50	G	T	2051.00	776.44	18.30	-2725.40	276.04	14.70
116	117	17.60	G	T	2051.00	668.01	19.40	-2725.40	75.72	15.80
117	117	17.60	H	T	1620.10	667.96	19.40	-3086.00	75.60	15.80
117	118	18.70	H	T	1620.10	541.71	20.50	-3086.00	-153.86	16.90
118	118	18.70	H	T	1620.10	541.66	20.50	-3086.00	-153.97	16.90
118	119	19.80	H	T	1620.10	396.74	21.60	-3086.00	-411.72	18.00
119	119	19.80	I	T	1015.60	396.71	21.60	-3316.30	-411.81	18.00
119	120	20.90	I	T	1015.60	232.28	22.70	-3316.30	-696.92	19.10
120	120	20.90	I	T	1015.60	232.26	22.70	-3316.30	-696.96	19.10
120	121	22.00	I	T	1015.60	46.49	23.80	-3316.30	-1009.40	20.20
121	1121	22.00	J	T	1104.10	46.50	20.20	-3283.20	-1009.39	23.80
121	122	23.40	J	T	1104.10	345.71	21.60	-3283.20	-588.02	25.20
122	122	23.40	J	T	1104.10	345.75	21.60	-3283.20	-587.93	25.20
122	123	24.80	J	T	1104.10	610.44	23.00	-3283.20	-210.76	26.60
123	123	24.80	K	T	1705.40	610.52	23.00	-3053.20	-210.59	26.60
123	124	26.20	K	T	1705.40	846.69	24.40	-3053.20	119.03	28.00
124	124	26.20	L	T	1705.40	846.76	24.40	-2850.70	119.19	28.00
124	125	27.60	L	T	1705.40	1052.53	25.80	-2850.70	403.11	29.40
125	125	27.60	M	T	2472.90	1052.58	25.80	-2562.80	403.26	29.40
125	126	29.00	M	T	2472.90	1288.91	27.20	-2562.80	580.27	30.80
126	126	29.00	E	T	2453.10	1289.10	27.20	-757.30	580.35	30.80
126	127	30.40	E	T	2453.10	1482.56	28.60	-757.30	723.35	32.20
127	127	30.40	F	T	3123.60	1482.72	28.60	-746.10	723.41	32.20
127	128	31.80	F	T	3123.60	1640.70	30.00	-746.10	824.89	33.60
128	128	31.80	F	T	3123.60	1640.82	30.00	-746.10	824.95	33.60
128	129	33.20	F	T	3123.60	1753.72	31.40	-746.10	894.70	35.00
129	129	33.20	F	T	3123.60	1753.81	31.40	-746.10	894.74	35.00
129	130	34.60	F	T	3123.60	1818.93	32.80	-746.10	935.39	36.40
130	130	34.60	F	T	3123.60	1818.97	32.80	-746.10	935.41	36.40
130	131	36.00	F	T	3123.60	1836.29	34.20	-746.10	946.94	37.80
131	131	36.00	F	T	3123.60	1836.30	37.80	-746.10	946.96	34.20
131	132	37.40	F	T	3123.60	1805.78	39.20	-746.10	929.34	35.60
132	132	37.40	F	T	3123.60	1805.74	39.20	-746.10	929.33	35.60
132	133	38.80	F	T	3123.60	1727.45	40.60	-746.10	882.62	37.00
133	133	38.80	F	T	3123.60	1727.36	40.60	-746.10	882.58	37.00
133	134	40.20	F	T	3123.60	1601.31	42.00	-746.10	806.75	38.40
134	134	40.20	F	T	3123.60	1601.19	42.00	-746.10	806.71	38.40
134	135	41.60	F	T	3123.60	1427.41	43.40	-746.10	701.77	39.80
135	135	41.60	E	T	2453.10	1427.27	43.40	-757.30	701.72	39.80
135	136	43.00	E	T	2453.10	1214.90	44.80	-757.30	558.47	41.20
136	136	43.00	M	T	2472.90	1214.71	44.80	-2562.80	558.39	41.20
136	137	44.40	M	T	2472.90	978.85	46.20	-2562.80	361.78	42.60
137	137	44.40	L	T	1705.40	978.77	46.20	-2850.70	361.59	42.60
137	138	45.80	L	T	1705.40	761.63	47.60	-2850.70	69.98	44.00
138	138	45.80	K	T	1705.40	761.56	47.60	-3053.20	69.82	44.00
138	139	47.20	K	T	1705.40	516.85	49.00	-3053.20	-270.37	45.40
139	139	47.20	J	T	1104.10	516.78	49.00	-3283.20	-270.51	45.40
139	140	48.60	J	T	1104.10	240.44	50.40	-3283.20	-655.02	46.80
140	140	48.60	J	T	1104.10	240.41	50.40	-3283.20	-655.09	46.80
140	141	50.00	J	T	1104.10	-70.46	51.80	-3283.20	-1083.81	48.20
141	1141	50.00	J	T	1104.10	-70.46	48.20	-3283.20	-1083.81	51.80
141	142	51.40	J	T	1104.10	240.41	49.60	-3283.20	-655.09	53.20
142	142	51.40	J	T	1104.10	240.45	49.60	-3283.20	-655.00	53.20
142	143	52.80	J	T	1104.10	516.77	51.00	-3283.20	-270.52	54.60
143	143	52.80	K	T	1705.40	516.84	51.00	-3053.20	-270.37	54.60
143	144	54.20	K	T	1705.40	761.53	52.40	-3053.20	69.78	56.00
144	144	54.20	L	T	1705.40	761.60	52.40	-2850.70	69.95	56.00
144	145	55.60	L	T	1705.40	978.76	53.80	-2850.70	361.59	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:
NVOLOVENTE PERM.MZ

Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	M	T	2472.90	978.84	53.80	-2562.80	361.78	57.40
145	146	57.00	M	T	2472.90	1214.70	55.20	-2562.80	558.38	58.80
146	146	57.00	E	T	2453.10	1214.89	55.20	-757.30	558.45	58.80
146	147	58.40	E	T	2453.10	1427.27	56.60	-757.30	701.71	60.20
147	147	58.40	F	T	3123.60	1427.44	56.60	-746.10	701.78	60.20
147	148	59.80	F	T	3123.60	1601.18	58.00	-746.10	806.69	61.60
148	148	59.80	F	T	3123.60	1601.30	58.00	-746.10	806.74	61.60
148	149	61.20	F	T	3123.60	1727.34	59.40	-746.10	882.56	63.00
149	149	61.20	F	T	3123.60	1727.43	59.40	-746.10	882.59	63.00
149	150	62.60	F	T	3123.60	1805.75	60.80	-746.10	929.32	64.40
150	150	62.60	F	T	3123.60	1805.81	60.80	-746.10	929.36	64.40
150	151	64.00	F	T	3123.60	1836.29	62.20	-746.10	946.94	65.80
151	151	64.00	F	T	3123.60	1836.28	65.80	-746.10	946.93	62.20
151	152	65.40	F	T	3123.60	1818.95	67.20	-746.10	935.40	63.60
152	152	65.40	F	T	3123.60	1818.91	67.20	-746.10	935.38	63.60
152	153	66.80	F	T	3123.60	1753.81	68.60	-746.10	894.74	65.00
153	153	66.80	F	T	3123.60	1753.73	68.60	-746.10	894.70	65.00
153	154	68.20	F	T	3123.60	1640.82	70.00	-746.10	824.93	66.40
154	154	68.20	F	T	3123.60	1640.69	70.00	-746.10	824.88	66.40
154	155	69.60	F	T	3123.60	1482.74	71.40	-746.10	723.41	67.80
155	155	69.60	E	T	2453.10	1482.57	71.40	-757.30	723.34	67.80
155	156	71.00	E	T	2453.10	1289.10	72.80	-757.30	580.36	69.20
156	156	71.00	M	T	2472.90	1288.93	72.80	-2562.80	580.29	69.20
156	157	72.40	M	T	2472.90	1052.60	74.20	-2562.80	403.29	70.60
157	157	72.40	L	T	1705.40	1052.52	74.20	-2850.70	403.10	70.60
157	158	73.80	L	T	1705.40	846.76	75.60	-2850.70	119.20	72.00
158	158	73.80	K	T	1705.40	846.69	75.60	-3053.20	119.01	72.00
158	159	75.20	K	T	1705.40	610.50	77.00	-3053.20	-210.61	73.40
159	159	75.20	J	T	1104.10	610.45	77.00	-3283.20	-210.74	73.40
159	160	76.60	J	T	1104.10	345.77	78.40	-3283.20	-587.91	74.80
160	160	76.60	J	T	1104.10	345.73	78.40	-3283.20	-588.01	74.80
160	161	78.00	J	T	1104.10	46.51	79.80	-3283.20	-1009.40	76.20
161	1161	78.00	I	T	1015.60	46.52	76.20	-3316.30	-1009.39	79.80
161	162	79.10	I	T	1015.60	232.25	77.30	-3316.30	-696.99	80.90
162	162	79.10	I	T	1015.60	232.26	77.30	-3316.30	-696.95	80.90
162	163	80.20	I	T	1015.60	396.71	78.40	-3316.30	-411.82	82.00
163	163	80.20	H	T	1620.10	396.74	78.40	-3086.00	-411.73	82.00
163	164	81.30	H	T	1620.10	541.65	79.50	-3086.00	-153.98	83.10
164	164	81.30	H	T	1620.10	541.71	79.50	-3086.00	-153.86	83.10
164	165	82.40	H	T	1620.10	667.96	80.60	-3086.00	75.60	84.20
165	165	82.40	G	T	2051.00	668.02	80.60	-2725.40	75.73	84.20
165	166	83.50	G	T	2051.00	776.42	81.70	-2725.40	276.01	85.30
166	166	83.50	G	T	2051.00	776.46	81.70	-2725.40	276.12	85.30
166	167	84.60	G	T	2051.00	908.35	82.80	-2725.40	405.91	86.40
167	167	84.60	C	T	2025.10	908.47	82.80	-765.40	405.95	86.40
167	168	85.70	C	T	2025.10	1022.79	83.90	-765.40	505.69	87.50
168	168	85.70	D	T	2453.10	1022.91	83.90	-757.30	505.74	87.50
168	169	86.80	D	T	2453.10	1120.70	85.00	-757.30	574.46	88.60
169	169	86.80	D	T	2453.10	1120.79	85.00	-757.30	574.50	88.60
169	170	87.90	D	T	2453.10	1189.20	86.10	-757.30	625.29	89.70
170	170	87.90	D	T	2453.10	1189.27	86.10	-757.30	625.31	89.70
170	171	89.00	D	T	2453.10	1228.29	87.20	-757.30	658.17	90.80
171	171	89.00	D	T	2453.10	1228.35	87.20	-757.30	658.20	90.80
171	172	90.10	D	T	2453.10	1237.90	88.30	-757.30	673.10	91.90
172	172	90.10	D	T	2453.10	1237.91	91.90	-757.30	673.09	91.90
172	173	91.20	D	T	2453.10	1218.02	93.00	-757.30	670.03	93.00
173	173	91.20	D	T	2453.10	1218.03	93.00	-757.30	670.03	93.00
173	174	92.30	D	T	2453.10	1168.72	94.10	-757.30	649.03	94.10
174	174	92.30	D	T	2453.10	1168.66	94.10	-757.30	649.01	90.50
174	175	93.40	D	T	2453.10	1089.92	95.20	-757.30	610.07	91.60
175	175	93.40	D	T	2453.10	1089.86	95.20	-757.30	610.06	91.60
175	176	94.50	D	T	2453.10	981.65	96.30	-757.30	553.13	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE PERM.MZ

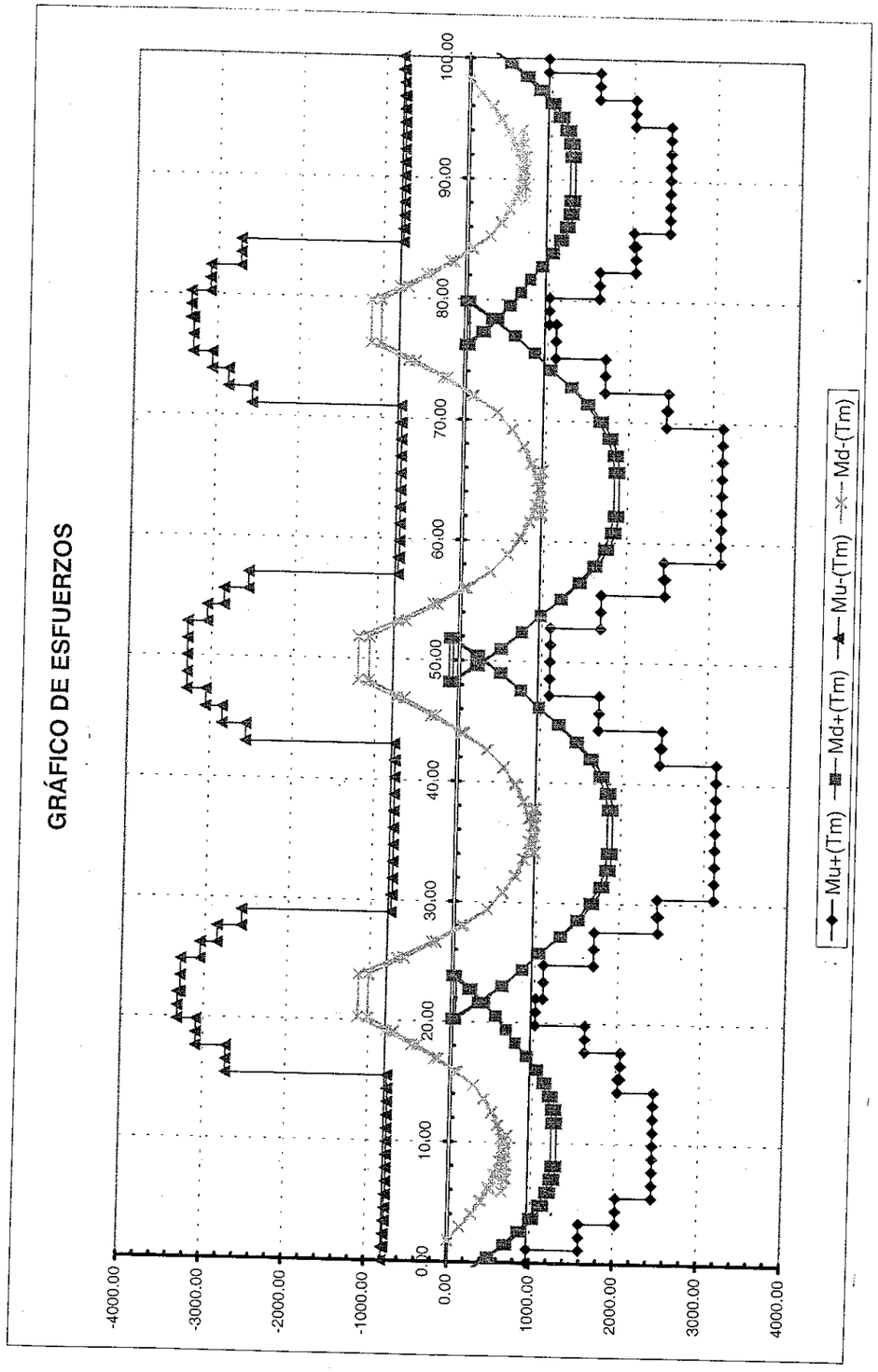
Cargas permanenetes tinf 4 Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	T	2025.10	981.57	96.30	-765.40	553.10	92.70
176	177	95.60	C	T	2025.10	844.04	97.40	-765.40	478.30	93.80
177	177	95.60	C	T	2025.10	843.91	97.40	-765.40	478.26	93.80
177	178	96.70	C	T	2025.10	677.04	98.50	-765.40	385.52	94.90
178	178	96.70	B	T	1586.50	676.90	98.50	-776.80	385.47	94.90
178	179	97.80	B	T	1586.50	480.79	99.60	-776.80	274.87	96.00
179	179	97.80	B	T	1586.50	480.62	99.60	-776.80	274.80	96.00
179	180	98.90	B	T	1586.50	255.30	100.70	-776.80	146.35	97.10
180	180	98.90	A	T	962.20	255.14	100.70	-794.10	146.28	97.10
180	181	100.00	A	T	962.20	0.09	101.80	-794.10	0.03	98.20



CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
1	1	0.00	A	T	962.20	1.38	-1.80	-794.10	-1.19	1.80
1	2	1.10	A	T	962.20	491.75	-0.70	-794.10	119.36	2.90
2	2	1.10	B	T	1586.50	492.09	-0.70	-776.80	119.36	2.90
2	3	2.20	B	T	1586.50	925.44	0.40	-776.80	218.67	4.00
3	3	2.20	B	T	1586.50	925.72	0.40	-776.80	218.67	4.00
3	4	3.30	B	T	1586.50	1301.61	1.50	-776.80	297.84	5.10
4	4	3.30	C	T	2025.10	1301.93	1.50	-765.40	297.84	5.10
4	5	4.40	C	T	2025.10	1620.03	2.60	-765.40	356.96	6.20
5	5	4.40	C	T	2025.10	1620.30	2.60	-765.40	356.96	6.20
5	6	5.50	C	T	2025.10	1891.71	3.70	-765.40	395.97	7.30
6	6	5.50	D	T	2453.10	1891.91	3.70	-757.30	395.94	7.30
6	7	6.60	D	T	2453.10	2106.07	4.80	-757.30	414.95	8.40
7	7	6.60	D	T	2453.10	2106.24	4.80	-757.30	414.89	8.40
7	8	7.70	D	T	2453.10	2263.00	5.90	-757.30	413.85	9.50
8	8	7.70	D	T	2453.10	2263.13	5.90	-757.30	413.80	9.50
8	9	8.80	D	T	2453.10	2360.81	7.00	-757.30	392.78	10.60
9	9	8.80	D	T	2453.10	2360.88	7.00	-757.30	392.70	7.00
9	10	9.90	D	T	2453.10	2411.31	8.10	-757.30	351.38	8.10
10	10	9.90	D	T	2453.10	2411.32	11.70	-757.30	351.36	8.10
10	11	11.00	D	T	2453.10	2404.92	12.80	-757.30	290.01	9.20
11	11	11.00	D	T	2453.10	2404.92	12.80	-757.30	289.96	9.20
11	12	12.10	D	T	2453.10	2341.30	13.90	-757.30	208.86	10.30
12	12	12.10	D	T	2453.10	2341.24	13.90	-757.30	208.78	10.30
12	13	13.20	D	T	2453.10	2219.43	15.00	-757.30	107.81	11.40
13	13	13.20	D	T	2453.10	2219.34	15.00	-757.30	107.76	11.40
13	14	14.30	D	T	2453.10	2047.27	16.10	-757.30	-12.98	12.50
14	14	14.30	C	T	2025.10	2047.11	16.10	-765.40	-13.03	12.50
14	15	15.40	C	T	2025.10	1832.05	17.20	-765.40	-166.61	13.60
15	15	15.40	G	T	2051.00	1831.88	17.20	-2725.40	-166.64	13.60
15	16	16.50	G	T	2051.00	1600.61	18.30	-2725.40	-352.09	14.70
16	16	16.50	G	T	2051.00	1600.32	18.30	-2725.40	-351.95	14.70
16	17	17.60	G	T	2051.00	1391.06	19.40	-2725.40	-624.59	15.80
17	17	17.60	H	T	1620.10	1390.63	19.40	-3086.00	-624.25	15.80
17	18	18.70	H	T	1620.10	1173.60	20.50	-3086.00	-960.28	16.90
18	18	18.70	H	T	1620.10	1172.90	20.50	-3086.00	-959.55	16.90
18	19	19.80	H	T	1620.10	973.71	21.60	-3086.00	-1372.03	18.00
19	19	19.80	I	T	1015.60	972.84	21.60	-3316.30	-1371.05	18.00
19	20	20.90	I	T	1015.60	779.68	22.70	-3316.30	-1890.54	19.10
20	20	20.90	I	T	1015.60	779.70	22.70	-3316.30	-1890.52	19.10
20	21	22.00	I	T	1015.60	587.93	23.80	-3316.30	-2494.41	20.20
21	1021	22.00	J	T	1104.10	587.94	20.20	-3283.20	-2494.23	23.80
21	22	23.40	J	T	1104.10	888.57	21.60	-3283.20	-1664.11	25.20
22	22	23.40	J	T	1104.10	888.50	21.60	-3283.20	-1663.80	25.20
22	23	24.80	J	T	1104.10	1174.86	23.00	-3283.20	-949.78	26.60
23	23	24.80	K	T	1705.40	1174.89	23.00	-3053.20	-949.73	26.60
23	24	26.20	K	T	1705.40	1486.37	24.40	-3053.20	-414.09	28.00
24	24	26.20	L	T	1705.40	1487.50	24.40	-2850.70	-415.14	28.00
24	25	27.60	L	T	1705.40	1827.69	25.80	-2850.70	-12.02	29.40
25	25	27.60	M	T	2472.90	1828.72	25.80	-2562.80	-13.03	29.40
25	26	29.00	M	T	2472.90	2227.56	27.20	-2562.80	204.88	30.80
26	26	29.00	E	T	2453.10	2227.90	27.20	-757.30	204.78	30.80
26	27	30.40	E	T	2453.10	2575.51	28.60	-757.30	354.35	32.20
27	27	30.40	F	T	3123.60	2575.75	28.60	-746.10	354.31	32.20
27	28	31.80	F	T	3123.50	2864.88	30.00	-746.10	458.36	33.60
28	28	31.80	F	T	3123.60	2865.14	30.00	-746.10	458.30	33.60
28	29	33.20	F	T	3123.60	3087.22	31.40	-746.10	527.69	35.00
29	29	33.20	F	T	3123.60	3087.47	31.40	-746.10	527.69	35.00
29	30	34.60	F	T	3123.60	3222.69	32.80	-746.10	563.00	36.40
30	30	34.60	F	T	3123.60	3222.80	32.80	-746.10	562.89	36.40
30	31	36.00	F	T	3123.60	3264.03	34.20	-746.10	558.88	37.80
31	31	36.00	F	T	3123.60	3264.05	37.80	-746.10	558.85	34.20
31	32	37.40	F	T	3123.60	3220.69	39.20	-746.10	519.00	35.60

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
32	32	37.40	F	T	3123.60	3220.63	39.20	-746.10	518.97	35.60
32	33	38.80	F	T	3123.60	3083.18	40.60	-746.10	446.95	37.00
33	33	38.80	F	T	3123.60	3082.98	40.60	-746.10	446.94	37.00
33	34	40.20	F	T	3123.60	2858.82	42.00	-746.10	342.94	38.40
34	34	40.20	F	T	3123.60	2858.56	42.00	-746.10	342.96	38.40
34	35	41.60	F	T	3123.60	2544.68	43.40	-746.10	207.05	39.80
35	35	41.60	E	T	2453.10	2544.29	43.40	-757.30	207.05	39.80
35	36	43.00	E	T	2453.10	2159.39	44.80	-757.30	29.08	41.20
36	36	43.00	M	T	2472.90	2159.09	44.80	-2562.80	29.18	41.20
36	37	44.40	M	T	2472.90	1753.65	46.20	-2562.80	-226.48	42.60
37	37	44.40	L	T	1705.40	1752.73	46.20	-2850.70	-225.67	42.60
37	38	45.80	L	T	1705.40	1379.93	47.60	-2850.70	-637.09	44.00
38	38	45.80	K	T	1705.40	1378.66	47.60	-3053.20	-635.84	44.00
38	39	47.20	K	T	1705.40	1028.01	49.00	-3053.20	-1172.48	45.40
39	39	47.20	J	T	1104.10	1027.34	49.00	-3283.20	-1171.83	45.40
39	40	48.60	J	T	1104.10	698.53	50.40	-3283.20	-1871.42	46.80
40	40	48.60	J	T	1104.10	698.59	50.40	-3283.20	-1871.47	46.80
40	41	50.00	J	T	1104.10	361.37	51.80	-3283.20	-2706.80	48.20
41	1041	50.00	J	T	1104.10	361.37	48.20	-3283.20	-2706.80	51.80
41	42	51.40	J	T	1104.10	698.56	49.60	-3283.20	-1871.48	53.20
42	42	51.40	J	T	1104.10	698.52	49.60	-3283.20	-1871.43	53.20
42	43	52.80	J	T	1104.10	1027.33	51.00	-3283.20	-1171.81	54.60
43	43	52.80	K	T	1705.40	1027.99	51.00	-3053.20	-1172.47	54.60
43	44	54.20	K	T	1705.40	1378.67	52.40	-3053.20	-635.81	56.00
44	44	54.20	L	T	1705.40	1379.93	52.40	-2850.70	-637.10	56.00
44	45	55.60	L	T	1705.40	1752.77	53.80	-2850.70	-225.63	57.40
45	45	55.60	M	T	2472.90	1753.69	53.80	-2562.80	-226.43	57.40
45	46	57.00	M	T	2472.90	2159.09	55.20	-2562.80	29.22	58.80
46	46	57.00	E	T	2453.10	2159.42	55.20	-757.30	29.08	58.80
46	47	58.40	E	T	2453.10	2544.32	56.60	-757.30	207.05	60.20
47	47	58.40	F	T	3123.60	2544.71	56.60	-746.10	207.04	60.20
47	48	59.80	F	T	3123.60	2858.63	58.00	-746.10	342.98	61.60
48	48	59.80	F	T	3123.60	2858.90	58.00	-746.10	342.98	61.60
48	49	61.20	F	T	3123.60	3082.98	59.40	-746.10	446.92	63.00
49	49	61.20	F	T	3123.60	3083.16	59.40	-746.10	446.96	63.00
49	50	62.60	F	T	3123.60	3220.64	60.80	-746.10	518.97	64.40
50	50	62.60	F	T	3123.60	3220.75	60.80	-746.10	518.97	64.40
50	51	64.00	F	T	3123.60	3264.04	62.20	-746.10	558.84	65.80
51	51	64.00	F	T	3123.60	3264.04	65.80	-746.10	558.85	62.20
51	52	65.40	F	T	3123.60	3222.81	67.20	-746.10	562.86	63.60
52	52	65.40	F	T	3123.60	3222.68	67.20	-746.10	562.94	63.60
52	53	66.80	F	T	3123.60	3087.53	68.60	-746.10	527.67	65.00
53	53	66.80	F	T	3123.60	3087.29	68.60	-746.10	527.68	65.00
53	54	68.20	F	T	3123.60	2865.21	70.00	-746.10	458.31	66.40
54	54	68.20	F	T	3123.60	2864.96	70.00	-746.10	458.32	66.40
54	55	69.60	F	T	3123.60	2575.77	71.40	-746.10	354.27	67.80
55	55	69.60	E	T	2453.10	2575.53	71.40	-757.30	354.28	67.80
55	56	71.00	E	T	2453.10	2227.93	72.80	-757.30	204.78	69.20
56	56	71.00	M	T	2472.90	2227.58	72.80	-2562.80	204.88	69.20
56	57	72.40	M	T	2472.90	1828.75	74.20	-2562.80	-13.04	70.60
57	57	72.40	L	T	1705.40	1827.69	74.20	-2850.70	-12.07	70.60
57	58	73.80	L	T	1705.40	1487.47	75.60	-2850.70	-415.17	72.00
58	58	73.80	K	T	1705.40	1486.35	75.60	-3053.20	-414.12	72.00
58	59	75.20	K	T	1705.40	1174.89	77.00	-3053.20	-949.74	73.40
59	59	75.20	J	T	1104.10	1174.85	77.00	-3283.20	-949.76	73.40
59	60	76.60	J	T	1104.10	888.50	78.40	-3283.20	-1663.81	74.80
60	60	76.60	J	T	1104.10	888.56	78.40	-3283.20	-1664.11	74.80
60	61	78.00	J	T	1104.10	587.96	79.80	-3283.20	-2494.24	76.20
61	1061	78.00	I	T	1015.60	587.96	76.20	-3316.30	-2494.47	79.80
61	62	79.10	I	T	1015.60	779.70	77.30	-3316.30	-1890.56	80.90
62	62	79.10	I	T	1015.60	779.68	77.30	-3316.30	-1890.61	80.90
62	63	80.20	I	T	1015.60	972.83	78.40	-3316.30	-1371.11	82.00

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
63	63	80.20	H	T	1620.10	973.71	78.40	-3086.00	-1372.08	82.00
63	64	81.30	H	T	1620.10	1172.91	79.50	-3086.00	-959.59	83.10
64	64	81.30	H	T	1620.10	1173.61	79.50	-3086.00	-960.31	83.10
64	65	82.40	H	T	1620.10	1390.63	80.60	-3086.00	-624.26	84.20
65	65	82.40	G	T	2051.00	1391.06	80.60	-2725.40	-624.60	84.20
65	66	83.50	G	T	2051.00	1600.32	81.70	-2725.40	-352.00	85.30
66	66	83.50	G	T	2051.00	1600.63	81.70	-2725.40	-352.09	85.30
66	67	84.60	G	T	2051.00	1831.90	82.80	-2725.40	-166.67	86.40
67	67	84.60	C	T	2025.10	1832.10	82.80	-765.40	-166.65	86.40
67	68	85.70	C	T	2025.10	2047.18	83.90	-765.40	-13.07	87.50
68	68	85.70	D	T	2453.10	2047.30	83.90	-757.30	-13.03	87.50
68	69	86.80	D	T	2453.10	2219.38	85.00	-757.30	107.71	88.60
69	69	86.80	D	T	2453.10	2219.51	85.00	-757.30	107.77	88.60
69	70	87.90	D	T	2453.10	2341.26	86.10	-757.30	208.74	89.70
70	70	87.90	D	T	2453.10	2341.35	86.10	-757.30	208.82	89.70
70	71	89.00	D	T	2453.10	2404.94	87.20	-757.30	289.91	90.80
71	71	89.00	D	T	2453.10	2404.98	87.20	-757.30	289.98	90.80
71	72	90.10	D	T	2453.10	2411.39	88.30	-757.30	351.32	91.90
72	72	90.10	D	T	2453.10	2411.34	91.90	-757.30	351.33	88.30
72	73	91.20	D	T	2453.10	2360.95	93.00	-757.30	392.63	89.40
73	73	91.20	D	T	2453.10	2360.88	93.00	-757.30	392.73	89.40
73	74	92.30	D	T	2453.10	2263.18	94.10	-757.30	413.76	90.50
74	74	92.30	D	T	2453.10	2263.05	94.10	-757.30	413.79	90.50
74	75	93.40	D	T	2453.10	2106.29	95.20	-757.30	414.85	91.60
75	75	93.40	D	T	2453.10	2106.10	95.20	-757.30	414.90	91.60
75	76	94.50	D	T	2453.10	1891.94	96.30	-757.30	395.91	92.70
76	76	94.50	C	T	2025.10	1891.75	96.30	-765.40	395.96	92.70
76	77	95.60	C	T	2025.10	1620.34	97.40	-765.40	356.92	93.80
77	77	95.60	C	T	2025.10	1620.09	97.40	-765.40	356.93	93.80
77	78	96.70	C	T	2025.10	1301.90	98.50	-765.40	297.82	94.90
78	78	96.70	B	T	1586.50	1301.64	98.50	-776.80	297.82	94.90
78	79	97.80	B	T	1586.50	925.68	99.60	-776.80	218.66	96.00
79	79	97.80	B	T	1586.50	925.42	99.60	-776.80	218.66	96.00
79	80	98.90	B	T	1586.50	492.08	100.70	-776.80	119.35	97.10
80	80	98.90	A	T	962.20	491.75	100.70	-794.10	119.36	97.10
80	81	100.00	A	T	962.20	1.38	101.80	-794.10	-1.19	98.20
101	101	0.00	A	T	962.20	1.19	-1.80	-794.10	-1.38	1.80
101	102	1.10	A	T	962.20	529.87	-0.70	-794.10	117.27	2.90
102	102	1.10	B	T	1586.50	529.25	-0.70	-776.80	117.58	2.90
102	103	2.20	B	T	1586.50	994.33	0.40	-776.80	214.70	4.00
103	103	2.20	B	T	1586.50	993.74	0.40	-776.80	214.99	4.00
103	104	3.30	B	T	1586.50	1395.19	1.50	-776.80	291.95	5.10
104	104	3.30	C	T	2025.10	1394.66	1.50	-765.40	292.22	5.10
104	105	4.40	C	T	2025.10	1733.65	2.60	-765.40	349.00	6.20
105	105	4.40	C	T	2025.10	1733.10	2.60	-765.40	349.18	6.20
105	106	5.50	C	T	2025.10	2021.46	3.70	-765.40	385.53	7.30
106	106	5.50	D	T	2453.10	2021.03	3.70	-757.30	385.72	7.30
106	107	6.60	D	T	2453.10	2247.37	4.80	-757.30	401.47	8.40
107	107	6.60	D	T	2453.10	2247.07	4.80	-757.30	401.63	8.40
107	108	7.70	D	T	2453.10	2411.42	5.90	-757.30	396.68	9.50
108	108	7.70	D	T	2453.10	2411.25	5.90	-757.30	396.85	5.90
108	109	8.80	D	T	2453.10	2513.70	7.00	-757.30	371.20	7.00
109	109	8.80	D	T	2453.10	2513.62	7.00	-757.30	371.29	7.00
109	110	9.90	D	T	2453.10	2563.93	8.10	-757.30	324.84	8.10
110	110	9.90	D	T	2453.10	2563.86	11.70	-757.30	324.92	8.10
110	111	11.00	D	T	2453.10	2554.21	12.80	-757.30	257.63	9.20
111	111	11.00	D	T	2453.10	2554.24	12.80	-757.30	257.67	9.20
111	112	12.10	D	T	2453.10	2483.60	13.90	-757.30	169.36	10.30
112	112	12.10	D	T	2453.10	2483.73	13.90	-757.30	169.38	10.30
112	113	13.20	D	T	2453.10	2352.06	15.00	-757.30	60.07	11.40
113	113	13.20	D	T	2453.10	2352.24	15.00	-757.30	60.03	11.40
113	114	14.30	D	T	2453.10	2166.19	16.10	-757.30	-70.39	12.50

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;
Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
114	114	14.30	C	T	2025.10	2166.50	16.10	-765.40	-70.44	12.50
114	115	15.40	C	T	2025.10	1934.50	17.20	-765.40	-235.22	13.60
115	115	15.40	G	T	2051.00	1934.83	17.20	-2725.40	-235.37	13.60
115	116	16.50	G	T	2051.00	1666.78	18.30	-2725.40	-434.34	14.70
116	116	16.50	G	T	2051.00	1667.12	18.30	-2725.40	-434.51	14.70
116	117	17.60	G	T	2051.00	1431.23	19.40	-2725.40	-710.80	15.80
117	117	17.60	H	T	1620.10	1431.44	19.40	-3086.00	-710.84	15.80
117	118	18.70	H	T	1620.10	1193.79	20.50	-3086.00	-1061.85	16.90
118	118	18.70	H	T	1620.10	1193.47	20.50	-3086.00	-1061.32	16.90
118	119	19.80	H	T	1620.10	988.63	21.60	-3086.00	-1506.21	18.00
119	119	19.80	I	T	1015.60	988.31	21.60	-3316.30	-1505.80	18.00
119	120	20.90	I	T	1015.60	803.05	22.70	-3316.30	-2086.40	19.10
120	120	20.90	I	T	1015.60	803.06	22.70	-3316.30	-2086.29	19.10
120	121	22.00	I	T	1015.60	617.66	23.80	-3316.30	-2755.00	20.20
121	1121	22.00	J	T	1104.10	617.67	20.20	-3283.20	-2754.97	23.80
121	122	23.40	J	T	1104.10	912.65	21.60	-3283.20	-1848.63	25.20
122	122	23.40	J	T	1104.10	912.69	21.60	-3283.20	-1848.83	25.20
122	123	24.80	J	T	1104.10	1200.76	23.00	-3283.20	-1076.51	26.60
123	123	24.80	K	T	1705.40	1200.53	23.00	-3053.20	-1076.57	26.60
123	124	26.20	K	T	1705.40	1518.46	24.40	-3053.20	-501.36	28.00
124	124	26.20	L	T	1705.40	1518.89	24.40	-2850.70	-502.21	28.00
124	125	27.60	L	T	1705.40	1880.75	25.80	-2850.70	-79.67	29.40
125	125	27.60	M	T	2472.90	1880.98	25.80	-2562.80	-80.39	29.40
125	126	29.00	M	T	2472.90	2290.39	27.20	-2562.80	159.16	30.80
126	126	29.00	E	T	2453.10	2290.11	27.20	-757.30	159.28	30.80
126	127	30.40	E	T	2453.10	2659.56	28.60	-757.30	319.50	32.20
127	127	30.40	F	T	3123.60	2659.16	28.60	-746.10	319.57	32.20
127	128	31.80	F	T	3123.60	2983.91	30.00	-746.10	432.01	33.60
128	128	31.80	F	T	3123.60	2983.59	30.00	-746.10	432.09	33.60
128	129	33.20	F	T	3123.60	3216.98	31.40	-746.10	507.37	35.00
129	129	33.20	F	T	3123.60	3216.75	31.40	-746.10	507.42	35.00
129	130	34.60	F	T	3123.60	3359.43	32.80	-746.10	546.76	36.40
130	130	34.60	F	T	3123.60	3359.32	32.80	-746.10	546.69	36.40
130	131	36.00	F	T	3123.60	3402.56	34.20	-746.10	543.35	37.80
131	131	36.00	F	T	3123.60	3402.54	37.80	-746.10	543.37	34.20
131	132	37.40	F	T	3123.60	3358.02	39.20	-746.10	500.77	35.60
132	132	37.40	F	T	3123.60	3358.10	39.20	-746.10	500.79	35.60
132	133	38.80	F	T	3123.60	3213.99	40.60	-746.10	423.76	37.00
133	133	38.80	F	T	3123.60	3214.24	40.60	-746.10	423.75	37.00
133	134	40.20	F	T	3123.60	2979.79	42.00	-746.10	312.22	38.40
134	134	40.20	F	T	3123.60	2980.10	42.00	-746.10	312.17	38.40
134	135	41.60	F	T	3123.60	2651.37	43.40	-746.10	166.00	39.80
135	135	41.60	E	T	2453.10	2651.77	43.40	-757.30	165.95	39.80
135	136	43.00	E	T	2453.10	2236.39	44.80	-757.30	-24.82	41.20
136	136	43.00	M	T	2472.90	2236.81	44.80	-2562.80	-24.90	41.20
136	137	44.40	M	T	2472.90	1808.28	46.20	-2562.80	-301.09	42.60
137	137	44.40	L	T	1705.40	1808.18	46.20	-2850.70	-300.60	42.60
137	138	45.80	L	T	1705.40	1413.24	47.60	-2850.70	-731.69	44.00
138	138	45.80	K	T	1705.40	1412.70	47.60	-3053.20	-730.66	44.00
138	139	47.20	K	T	1705.40	1053.87	49.00	-3053.20	-1304.74	45.40
139	139	47.20	J	T	1104.10	1053.69	49.00	-3283.20	-1304.35	45.40
139	140	48.60	J	T	1104.10	727.04	50.40	-3283.20	-2067.06	46.80
140	140	48.60	J	T	1104.10	727.06	50.40	-3283.20	-2066.85	46.80
140	141	50.00	J	T	1104.10	396.34	51.80	-3283.20	-2981.58	48.20
141	1141	50.00	J	T	1104.10	396.34	48.20	-3283.20	-2981.58	51.80
141	142	51.40	J	T	1104.10	727.04	49.60	-3283.20	-2066.82	53.20
142	142	51.40	J	T	1104.10	727.04	49.60	-3283.20	-2067.02	53.20
142	143	52.80	J	T	1104.10	1053.66	51.00	-3283.20	-1304.31	54.60
143	143	52.80	K	T	1705.40	1053.86	51.00	-3053.20	-1304.71	54.60
143	144	54.20	K	T	1705.40	1412.68	52.40	-3053.20	-730.66	56.00
144	144	54.20	L	T	1705.40	1413.23	52.40	-2850.70	-731.68	56.00
144	145	55.60	L	T	1705.40	1808.20	53.80	-2850.70	-300.55	57.40

CÁLCULO EN ROTURA

Hipótesis de cálculo:
ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1I3.HIP.To + [1; 1]eje2I3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;
Coef. exc:

Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
145	145	55.60	M	T	2472.90	1808.30	53.80	-2562.80	-301.04	57.40
145	146	57.00	M	T	2472.90	2236.87	55.20	-2562.80	-24.90	58.80
146	146	57.00	E	T	2453.10	2236.45	55.20	-757.30	-24.82	58.80
146	147	58.40	E	T	2453.10	2651.85	56.60	-757.30	165.94	60.20
147	147	58.40	F	T	3123.60	2651.43	56.60	-746.10	166.03	60.20
147	148	59.80	F	T	3123.60	2980.15	58.00	-746.10	312.14	61.60
148	148	59.80	F	T	3123.60	2979.86	58.00	-746.10	312.22	61.60
148	149	61.20	F	T	3123.60	3214.26	59.40	-746.10	423.73	63.00
149	149	61.20	F	T	3123.60	3214.04	59.40	-746.10	423.72	63.00
149	150	62.60	F	T	3123.60	3358.21	60.80	-746.10	500.77	64.40
150	150	62.60	F	T	3123.60	3358.13	60.80	-746.10	500.77	64.40
150	151	64.00	F	T	3123.60	3402.61	62.20	-746.10	543.32	65.80
151	151	64.00	F	T	3123.60	3402.62	65.80	-746.10	543.30	62.20
151	152	65.40	F	T	3123.60	3359.37	67.20	-746.10	546.64	63.60
152	152	65.40	F	T	3123.60	3359.47	67.20	-746.10	546.71	63.60
152	153	66.80	F	T	3123.60	3216.84	68.60	-746.10	507.36	65.00
153	153	66.80	F	T	3123.60	3217.08	68.60	-746.10	507.32	65.00
153	154	68.20	F	T	3123.60	2983.65	70.00	-746.10	432.01	66.40
154	154	68.20	F	T	3123.60	2983.94	70.00	-746.10	431.95	66.40
154	155	69.60	F	T	3123.60	2659.22	71.40	-746.10	319.52	67.80
155	155	69.60	E	T	2453.10	2659.64	71.40	-757.30	319.44	67.80
155	156	71.00	E	T	2453.10	2290.16	72.80	-757.30	159.25	69.20
156	156	71.00	M	T	2472.90	2290.44	72.80	-2562.80	159.12	69.20
156	157	72.40	M	T	2472.90	1881.00	74.20	-2562.80	-80.42	70.60
157	157	72.40	L	T	1705.40	1880.74	74.20	-2850.70	-79.71	70.60
157	158	73.80	L	T	1705.40	1518.88	75.60	-2850.70	-502.24	72.00
158	158	73.80	K	T	1705.40	1518.44	75.60	-3053.20	-501.38	72.00
158	159	75.20	K	T	1705.40	1200.51	77.00	-3053.20	-1076.58	73.40
159	159	75.20	J	T	1104.10	1200.76	77.00	-3283.20	-1076.54	73.40
159	160	76.60	J	T	1104.10	912.71	78.40	-3283.20	-1848.83	74.80
160	160	76.60	J	T	1104.10	912.66	78.40	-3283.20	-1848.68	74.80
160	161	78.00	J	T	1104.10	617.70	79.80	-3283.20	-2755.03	76.20
161	1161	78.00	I	T	1015.60	617.67	76.20	-3316.30	-2755.04	79.80
161	162	79.10	I	T	1015.60	803.04	77.30	-3316.30	-2086.36	80.90
162	162	79.10	I	T	1015.60	802.99	77.30	-3316.30	-2086.51	80.90
162	163	80.20	I	T	1015.60	988.31	78.40	-3316.30	-1505.85	82.00
163	163	80.20	H	T	1620.10	988.61	78.40	-3086.00	-1506.26	82.00
163	164	81.30	H	T	1620.10	1193.50	79.50	-3086.00	-1061.35	83.10
164	164	81.30	H	T	1620.10	1193.80	79.50	-3086.00	-1061.87	83.10
164	165	82.40	H	T	1620.10	1431.45	80.60	-3086.00	-710.87	84.20
165	165	82.40	G	T	2051.00	1431.26	80.60	-2725.40	-710.83	84.20
165	166	83.50	G	T	2051.00	1667.14	81.70	-2725.40	-434.59	85.30
166	166	83.50	G	T	2051.00	1666.82	81.70	-2725.40	-434.40	85.30
166	167	84.60	G	T	2051.00	1934.89	82.80	-2725.40	-235.38	86.40
167	167	84.60	C	T	2025.10	1934.55	82.80	-765.40	-235.27	86.40
167	168	85.70	C	T	2025.10	2166.54	83.90	-765.40	-70.49	87.50
168	168	85.70	D	T	2453.10	2166.24	83.90	-757.30	-70.43	87.50
168	169	86.80	D	T	2453.10	2352.32	85.00	-757.30	59.99	88.60
169	169	86.80	D	T	2453.10	2352.08	85.00	-757.30	60.02	88.60
169	170	87.90	D	T	2453.10	2483.78	86.10	-757.30	169.35	89.70
170	170	87.90	D	T	2453.10	2483.64	86.10	-757.30	169.33	89.70
170	171	89.00	D	T	2453.10	2554.29	87.20	-757.30	257.64	90.80
171	171	89.00	D	T	2453.10	2554.24	87.20	-757.30	257.61	90.80
171	172	90.10	D	T	2453.10	2563.89	88.30	-757.30	324.91	91.90
172	172	90.10	D	T	2453.10	2563.93	91.90	-757.30	324.81	91.90
172	173	91.20	D	T	2453.10	2513.63	93.00	-757.30	371.25	93.00
173	173	91.20	D	T	2453.10	2513.73	93.00	-757.30	371.14	93.00
173	174	92.30	D	T	2453.10	2411.29	94.10	-757.30	396.81	94.10
174	174	92.30	D	T	2453.10	2411.48	94.10	-757.30	396.66	90.50
174	175	93.40	D	T	2453.10	2247.12	95.20	-757.30	401.61	91.60
175	175	93.40	D	T	2453.10	2247.41	95.20	-757.30	401.45	91.60
175	176	94.50	D	T	2453.10	2021.07	96.30	-757.30	385.70	92.70

CÁLCULO EN ROTURA

Hipótesis de cálculo:

ENVOLOVENTE INFREC.MZ

Envolvente cargas totales tinf Mz

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.755]CMBALASTO + [1; 1.35]CMRESTO + [1; 1.35]RCEXT + [1; 1.35]RPT + [1;

Coef. exc:

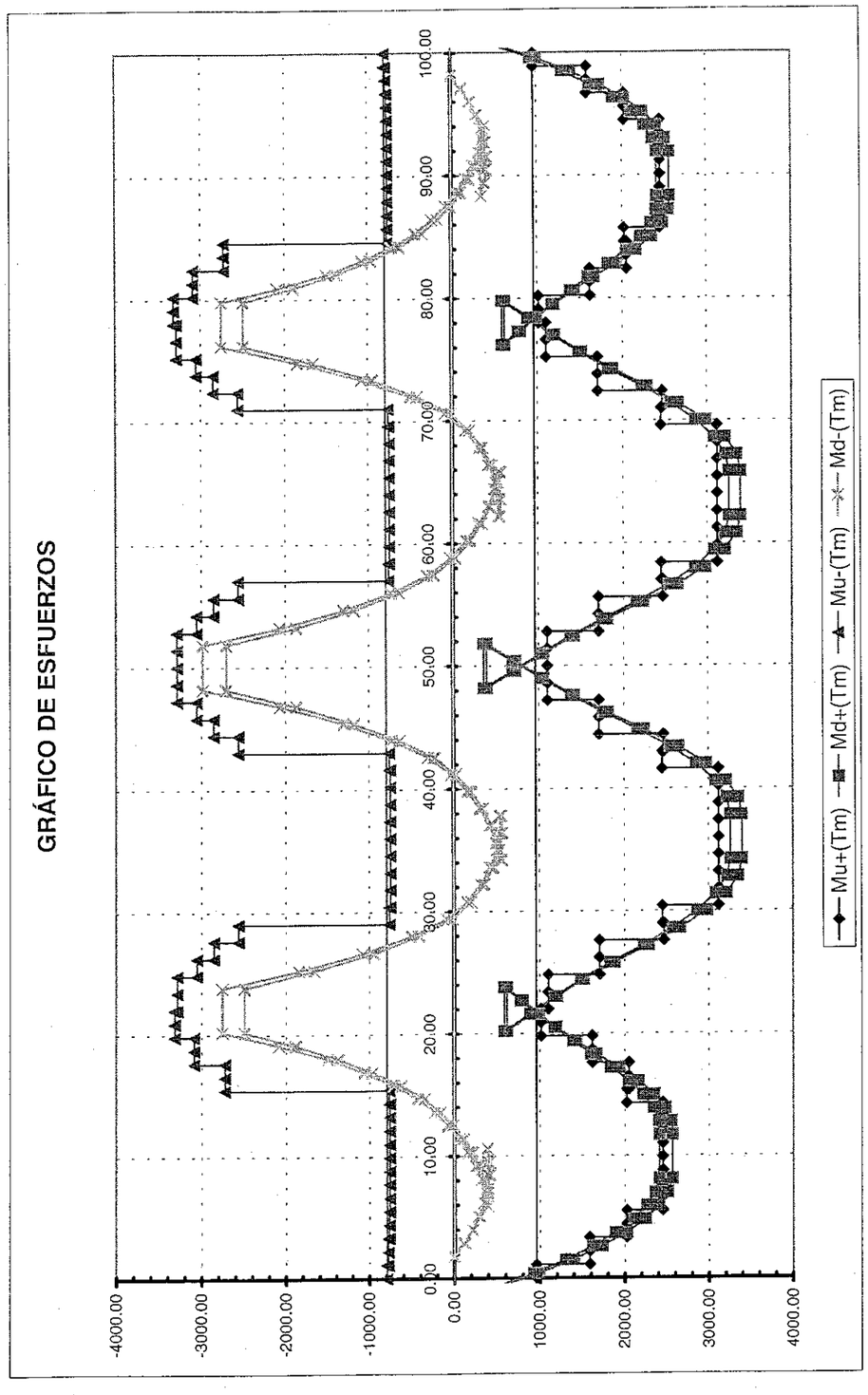
Decalaje 1.8

Barra	Nudo	X	Seccion	Estado	Mu+(Tm)	Md+(Tm)	X+(m)	Mu-(Tm)	Md-(Tm)	X-(m)
176	176	94.50	C	T	2025.10	2021.51	96.30	-765.40	385.52	92.70
176	177	95.60	C	T	2025.10	1733.13	97.40	-765.40	349.16	93.80
177	177	95.60	C	T	2025.10	1733.65	97.40	-765.40	348.96	93.80
177	178	96.70	C	T	2025.10	1394.66	98.50	-765.40	292.18	94.90
178	178	96.70	B	T	1586.50	1395.22	98.50	-776.80	291.99	94.90
178	179	97.80	B	T	1586.50	993.72	99.60	-776.80	214.97	96.00
179	179	97.80	B	T	1586.50	994.33	99.60	-776.80	214.69	96.00
179	180	98.90	B	T	1586.50	529.24	100.70	-776.80	117.56	97.10
180	180	98.90	A	T	962.20	529.87	100.70	-794.10	117.27	97.10
180	181	100.00	A	T	962.20	1.19	101.80	-794.10	-1.38	98.20

05/09/03

Programa DINTEL PACADAR S.A.
ENVOLOVENTE INFREC.MZ

rotura.esf.xls



MOMENTOS ÚLTIMOS DE LAS SECCIONES

CON REFUERZOS

MOMENTOS ÚLTIMOS DE LAS SECCIONES CON REFUERZOS

SECCION	CAJON		SECCION TOTAL	
	Mu+	Mu-	Mu+	Mu-
A	1001.1	-147.5	1266.4	-794.1
B	1360.9	-140.3	1887.9	-776.8
C	1556.9	-133.6	2324.6	-765.4
D	1674.1	-140.8	2750.7	-759.6
E	1699.7	-128.6	2877.8	-757.3
F	1786.8	-144.6	3544.0	-776.7
G	1657.9	-354.1	2353.9	-2980.2
H	1446.3	-360.2	1917.2	-3346.0
I	1019.9	-367.5	1317.0	-3576.3
J	1195.6	-367.5	1530.4	-3654.8
K	1559.6	-362.4	2127.4	-3424.3
L	1559.5	-362.4	2137.2	-3198.2
M	1699.7	-128.6	2892.6	-2562.8

NOTAS: Los momentos últimos de las secciones se expresan en m·ton

Refuerzo inferior de rotura

SECCIONES EN ROTURA

SECCION	PRET INF	PRET SUP	ANCHO LOSA	POST LOSA	ARM LOSA	REF INFERIOR	REF SUPERIOR
A	20	4	14 m	---	Φ12 a 20 cm	7 Φ 25	
B	34	4	14 m	---	Φ12 a 20 cm	7 Φ 25	
C	44	4	14 m	---	Φ12 a 20 cm	7 Φ 25	
D	54	4	14 m	---	Φ12 a 20 cm	7 Φ 25	
E	54	4	14 m	---	Φ12 a 20 cm	10 Φ 25	
F	70	4	14 m	---	Φ12 a 20 cm	10 Φ 25	
G	44	4	14 m	42	Φ20 a 20 cm	7 Φ 25	6 Φ 25
H	34	4	14 m	84	Φ20 a 20 cm	7 Φ 25	6 Φ 25
I	20	4	14 m	84	Φ20 a 20 cm	7 Φ 25	6 Φ 25
J	22	4	14 m	84	Φ20 a 20 cm	10 Φ 25	6 Φ 25
K	36	4	14 m	84	Φ20 a 20 cm	10 Φ 25	6 Φ 25
L	36	4	14 m	42	Φ20 a 20 cm	10 Φ 25	6 Φ 25
M	54	4	14 m	42	Φ20 a 20 cm	10 Φ 25	

Proyecto:
V TORRENTE DEL BO

Seccion:A REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	20.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1616.8	15.50	2336538.9
	(1)	860.5	27.22	2147174.0
	(2)	1038.7	23.11	2212181.5
F:pura -	(0)	894.5	182.27	2542634.8
	(1)	385.6	158.77	2164237.5
	(2)	482.2	167.05	2292513.5
C.Simple	(0)	4954.5	62.04	25512739.3
	(1)	1477.6	64.45	8130559.9
	(2)	2105.3	63.43	11271596.3
T.Simple	(0)	140.4	97.05	1284943.7
	(1)	140.4	97.05	1284943.7
	(2)	140.4	97.05	1284943.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: A REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 463.02Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1001.1 Xu(cm.): 70.8

Nu(Tn.): -.5 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00282 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -150.6 Xu(cm.): 198.3

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00102 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3443.2 aplicado en Yo(cm)= 141.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 655.7 aplicado en Yo(cm)= 186.1

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: A REF M+

* RESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 463.02Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1266.4 Xu(cm.): 16.0

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00081 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -802.8 Xu(cm.): 190.0

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00135 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7602.3 aplicado en Yo(cm)= 72.9

TRACCION SIMPLE(Rigido/Plastico):

N Tn.): 1006.8 aplicado en Yo(cm)= 125.9

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:B REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_\Pi 1$	$J_\Pi 2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) Π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	10.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1830.6	17.55	2998061.8
	(1)	974.3	30.81	2723434.1
	(2)	1176.0	26.15	2817700.2
F.pura -	(0)	910.8	182.72	2551512.1
	(1)	401.1	160.89	2201167.1
	(2)	497.9	168.44	2317454.8
C.Simple	(0)	4973.3	62.58	25890846.8
	(1)	1496.4	66.20	8492774.1

	(2)	2124.1	64.67	11640502.2
T imple	(0)	159.2	109.69	1475074.9
	(1)	159.2	109.69	1475074.9
	(2)	159.2	109.69	1475074.9

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T╒tulo Secci├n: B REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 733.11Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

A lisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1360.9 Xu(cm.): 99.2

Nu(Tn.): .8 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00552
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -146.5 Xu(cm.): 195.7

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00132 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3443.2 aplicado en Yo(cm)= 141.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 949.2 aplicado en Yo(cm)= 191.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S arciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

T╒tulo Secci├n: B REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 733.11Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[╥*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1887.9 Xu(cm.): 19.4

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00100 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -788.7 Xu(cm.): 188.0

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00160 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7602.3 aplicado en Yo(cm)= 72.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1300.3 aplicado en Yo(cm)= 143.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
V TORRENTE DEL BO

Seccion:C REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	20.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1968.2	18.85	3455070.7
	(1)	1024.8	33.09	3114854.8
	(2)	1264.5	28.09	3231563.7
F.pura -	(0)	922.7	183.01	2556784.2
	(1)	412.5	162.24	2223855.4
	(2)	509.3	169.34	2332778.0
C.Simple	(0)	4986.7	62.96	26153721.1
	(1)	1509.8	67.41	8740690.4
	(2)	2137.5	65.54	11894675.7
T.Simple	(0)	172.6	116.93	1582147.6
	(1)	172.6	116.93	1582147.6
	(2)	172.6	116.93	1582147.6

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Tπtulo Secciπn: C REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 926.03Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1556.9 Xu(cm.): 119.2

Nu(Tn.): .5 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00329
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -142.6 Xu(cm.): 194.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00152 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3443.2 aplicado en Yo(cm)= 141.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1158.9 aplicado en Yo(cm)= 193.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: C REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 926.03Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2324.6 Xu(cm.): 21.5

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00113 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -779.6 Xu(cm.): 186.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00178 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7602.3 aplicado en Yo(cm)= 72.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1510.0 aplicado en Yo(cm)= 151.8

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:D REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	6.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	0.0	25.0	35.5	CT	0
12	4	35.0	12.0	23.0	CT	0
13	4	35.0	12.0	3.0	CT	0
14	3	0.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2095.2	20.04	3891362.8
	(1)	1049.0	35.23	3482844.8
	(2)	1346.3	29.84	3622992.6
F.pura -	(0)	934.8	183.25	2560543.0
	(1)	424.1	163.43	2242155.9
	(2)	521.0	170.12	2344895.6
C.Simple	(0)	5000.1	63.33	26404155.7
	(1)	1523.3	68.58	8973631.6

	(2)	2151.0	66.38	12134893.7
Tramo	(0)	186.0	122.90	1667541.1
	(1)	186.0	122.90	1667541.1
	(2)	186.0	122.90	1667541.1

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: D REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1674.1 Xu(cm.): 133.2

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00221
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -140.8 Xu(cm.): 192.5

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00171 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3443.2 aplicado en Yo(cm)= 141.8

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1368.6 aplicado en Yo(cm)= 194.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
Sparciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: D REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2750.7 Xu(cm.): 23.4

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00124 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -774.4 Xu(cm.): 184.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00198 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7602.3 aplicado en Yo(cm)= 72.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1719.7 aplicado en Yo(cm)= 157.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
Sparciales resistentes: Rcu(Kg/cm):

Proyecto:
VT TORRENTE DEL BO

Seccion:F REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

ECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	22.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
0	4	10.0	25.0	207.0	CT	0
1	4	0.0	25.0	35.5	CT	0
2	4	35.0	12.0	23.0	CT	0
3	4	35.0	12.0	3.0	CT	0
4	3	0.0	13.4	14.0	*T	0

ECCIONES INTERMEDIAS

um.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
5	PL	14

* CONSTANTES ESTATICAS *

.COMPLETA

ipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
:pura +	(0)	2402.1	22.89	5047425.6
	(1)	1111.6	40.62	4437723.6
	(2)	1480.9	34.06	4648631.9
pura -	(0)	966.6	183.93	2573343.5
	(1)	455.1	166.41	2291477.1
	(2)	551.9	172.16	2379312.0
Simple	(0)	5035.6	64.30	27081779.5
	(1)	1558.8	71.62	9590970.8
	(2)	2186.5	68.58	12777063.4
T.Simple	(0)	221.5	135.56	1854357.6
	(1)	221.5	135.56	1854357.6
	(2)	221.5	135.56	1854357.6

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

TΓtulo Secci$\vdash$n: F REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1427.64Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1786.8 Xu(cm.): 149.2

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00124
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -144.6 Xu(cm.): 190.8

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00196 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3508.5 aplicado en Yo(cm)= 143.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1769.5 aplicado en Yo(cm)= 195.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: F REF M+

* RESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1427.64Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ψ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 3544.0 Xu(cm.): 26.8

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00146 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -776.7 Xu(cm.): 182.1

Nu(Tn.): -.3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00224 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7667.6 aplicado en Yo(cm)= 74.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 2120.6 aplicado en Yo(cm)= 165.5

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:G REF M+ M-

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jψ1	Jψ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) ψ(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	20.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	6.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	42.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2171.3	18.69	3481324.2
	(1)	1191.7	30.26	3185792.4
	(2)	1419.5	26.45	3279193.1
F.pura -	(0)	1303.4	153.37	7490019.2
	(1)	703.2	114.75	5312340.2
	(2)	823.5	126.49	5960680.2
C.Simple	(0)	5205.2	61.04	26617160.5
	(1)	1728.3	61.07	9247119.6

	(2)	2356.0	61.06	12382998.8
T.Simple	(0)	391.1	61.23	2566322.9
	(1)	391.1	61.23	2566322.9
	(2)	391.1	61.23	2566322.9

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: G REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1736.31Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1657.9 Xu(cm.): 105.7

Nu(Tn.): .5 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00450
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -354.1 Xu(cm.): 191.6

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00168 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3573.8 aplicado en Yo(cm)= 138.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1289.6 aplicado en Yo(cm)= 177.7

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: G REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1736.31Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2353.9 Xu(cm.): 24.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00140 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -2980.2 Xu(cm.): 93.4

Nu(Tn.): 1.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00238
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8357.1 aplicado en Yo(cm)= 67.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3145.6 aplicado en Yo(cm)= 81.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VT. TORRENTE DEL BO

Seccion:H REF M+ M-

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	10.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	6.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7
		8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2095.0	17.44	3024270.9
	(1)	1164.2	27.59	2791826.7
	(2)	1379.5	24.32	2863548.4
F.pura -	(0)	1380.4	147.15	8489561.6
	(1)	760.0	105.68	5711449.8
	(2)	885.2	118.12	6526531.8
C.Simple	(0)	5248.2	60.18	26465148.0
	(1)	1771.3	58.52	9087746.1
	(2)	2399.0	59.17	12226532.5
T.Simple	(0)	434.1	50.80	2372720.0
	(1)	434.1	50.80	2372720.0
	(2)	434.1	50.80	2372720.0

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: H REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2353.67Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1446.3 Xu(cm.): 84.9

Nu(Tn.): .4 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00766
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -360.2 Xu(cm.): 192.8

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00149 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3573.8 aplicado en Yo(cm)= 138.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1079.9 aplicado en Yo(cm)= 172.9

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: H REF M+ M-

* RESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2353.67Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1917.9 Xu(cm.): 25.3

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00158 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3346.0 Xu(cm.): 71.0

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00144
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8357.1 aplicado en Yo(cm)= 67.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3816.6 aplicado en Yo(cm)= 59.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:I REF M+ M-

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	20.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	7.0	25.0	207.0	CT	0
11	4	6.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	1908.4	15.68	2362919.4
	(1)	1066.0	24.59	2196084.3
	(2)	1260.4	21.74	2247091.3
F.pura -	(0)	1365.9	146.36	8427631.6
	(1)	745.0	103.19	5524620.2
	(2)	870.5	116.26	6384426.0
C.Simple	(0)	5229.4	59.66	26074171.5
	(1)	1752.5	56.96	8684860.4

	(2)	2380.2	58.03	11828382.8
T.Simple	(0)	415.3	43.86	1910732.1
	(1)	415.3	43.86	1910732.1
	(2)	415.3	43.86	1910732.1

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: I REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2083.58Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1019.9 Xu(cm.): 61.1

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00216 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -367.5 Xu(cm.): 195.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00120 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3573.8 aplicado en Yo(cm)= 138.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 786.3 aplicado en Yo(cm)= 161.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)*

Título Sección: I REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2083.58Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1317.0 Xu(cm.): 23.2

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00145 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3576.3 Xu(cm.): 74.2

Nu(Tn.): -.9 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00160
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8357.1 aplicado en Yo(cm)= 67.9

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3523.0 aplicado en Yo(cm)= 47.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Pr ecto:
VTO TORRENTE DEL BO

Seccion:F REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

ECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) $_{\pi}$(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	18.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
.0	4	10.0	25.0	207.0	CT	0
.1	4	0.0	25.0	35.5	CT	0
.2	4	35.0	12.0	23.0	CT	0
.3	4	35.0	12.0	3.0	CT	0
.4	3	0.0	13.4	14.0	*T	0

ECCIONES INTERMEDIAS

Num	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

.COMPLETA

ipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
:pura +	(0)	2359.1	22.50	4882942.2
	(1)	1102.4	39.86	4304568.4
	(2)	1471.1	33.46	4504297.2
.: ra -	(0)	961.6	183.85	2572322.4
	(1)	450.3	166.04	2286164.0
	(2)	547.1	171.91	2375779.7
.Simple	(0)	5030.3	64.16	26986118.5
	(1)	1553.4	71.18	9505310.1
	(2)	2181.1	68.26	12687308.9
T.Simple	(0)	216.2	134.02	1833115.9
	(1)	216.2	134.02	1833115.9
	(2)	216.2	134.02	1833115.9

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T $_{\pi}$tulo Secci $_{\pi}$n: F REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1350.47Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[$_{\pi}$*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1766.7 Xu(cm.): 146.1

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00142
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -145.0 Xu(cm.): 191.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00188 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3508.5 aplicado en Yo(cm)= 143.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1685.6 aplicado en Yo(cm)= 195.6

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: F REF M+

* ESOLICITACIONES ELASTICAS
Análisis SIN FISURACION
Pretensado: 1350.47Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ϕ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 3378.2 Xu(cm.): 26.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00141 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -777.8 Xu(cm.): 183.0

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00216 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7667.6 aplicado en Yo(cm)= 74.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 2036.7 aplicado en Yo(cm)= 164.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:E REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\phi}1$	$J_{\phi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat. Num	B(cm)	H(cm)	ϕ(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2		184.8	C*	0
2	1	36.0	137.8		47.0	C*	0
3	1	119.0	15.0		32.0	C*	0
4	2	700.0	32.0		0.0	C*	0
5	3	24.0	13.4		207.0	*T	0
6	3	24.0	13.4		202.0	*T	0
7	3	6.0	13.4		197.0	*T	0
8	3	0.0	13.4		192.0	*T	0
9	3	4.0	13.4		37.0	*T	0
10	4	10.0	25.0		207.0	CT	0
11	4	0.0	25.0		35.5	CT	0
12	4	35.0	12.0		23.0	CT	0
13	4	35.0	12.0		3.0	CT	0
14	3	0.0	13.4		14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2225.2	21.26	4384914.7
	(1)	1074.4	37.50	3897180.7
	(2)	1430.0	31.63	4064884.3
F.pura -	(0)	946.8	183.62	2569189.5
	(1)	436.0	164.87	2269436.7
	(2)	532.7	171.13	2364754.6
C.Simple	(0)	5014.2	63.73	26697905.4
	(1)	1537.3	69.85	9244735.9

	(2)	2165.0	67.29	12415372.8
T Simple	(0)	200.0	128.89	1762545.5
	(1)	200.0	128.89	1762545.5
	(2)	200.0	128.89	1762545.5

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: E REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Análisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ϕ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1699.7 Xu(cm.): 136.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00203
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -145.1 Xu(cm.): 193.2

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00166 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3508.5 aplicado en Yo(cm)= 143.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1433.9 aplicado en Yo(cm)= 195.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)*

Título Sección: E REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1118.96Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[ϕ*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2877.8 Xu(cm.): 23.9

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00128 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -780.4 Xu(cm.): 185.4

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00191 Etmx= .01000
Rompe la fibra superior de la S.parcial 4

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -7667.6 aplicado en Yo(cm)= 74.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1785.0 aplicado en Yo(cm)= 159.5

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VT TORRENTE DEL BO

Seccion:M REF M+

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	24.0	13.4	202.0	*T	0
7	3	6.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
0	4	10.0	25.0	207.0	CT	0
1	4	0.0	25.0	35.5	CT	0
2	4	35.0	20.0	23.0	CT	0
3	4	35.0	20.0	3.0	CT	0
4	3	42.0	13.4	14.0	*T	0

ECCIONES INTERMEDIAS

um.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
5	PL	14

* CONSTANTES ESTATICAS *

COMPLETA

po	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
pura +	(0)	2363.3	20.71	4406735.5
	(1)	1247.2	33.99	3997227.2
	(2)	1539.5	29.55	4128407.7
pura -	(0)	1283.0	156.98	7162860.1
	(1)	692.5	121.40	5330452.1
	(2)	810.2	132.18	5874145.7
Simple	(0)	5204.6	61.92	27158668.2
	(1)	1727.8	63.74	9780132.2
	(2)	2355.4	63.01	12919400.1
T.Simple	(0)	390.5	73.03	3055787.7
	(1)	390.5	73.03	3055787.7
	(2)	390.5	73.03	3055787.7

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Tπtulo Secciπn: M REF M+

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1929.24Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1699.7 Xu(cm.): 135.6

Nu(Tn.): -0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00203
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -145.1 Xu(cm.): 192.9

Nu(Tn.): .3 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00166 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3508.5 aplicado en Yo(cm)= 143.1

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1433.9 aplicado en Yo(cm)= 195.2

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: M REF M+

Proyecto:
VTO TORRENTE DEL BO

Seccion:J REF M+ M-

* RESOLICITACIONES ELASTICAS

Analisis SIN FISURACION
Pretensado: 1929.24Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2892.6 Xu(cm.): 25.8

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00151 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -2915.2 Xu(cm.): 96.6

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00248
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8291.8 aplicado en Yo(cm)= 69.5

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3289.9 aplicado en Yo(cm)= 93.1

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_\Pi 1$	$J_\Pi 2$
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) Π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	22.0	13.4	207.0	*T	0
6	3	0.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	10.0	25.0	207.0	CT	0
11	4	6.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	84.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2078.1	17.28	2976823.0
	(1)	1155.2	27.33	2750690.1
	(2)	1368.7	24.09	2820423.1
F.pura -	(0)	1378.5	147.11	8490682.8
	(1)	758.2	105.50	5704693.3
	(2)	883.4	117.99	6522897.6
C.Simple	(0)	5246.1	60.13	26441505.2
	(1)	1769.2	58.38	9063301.8

	(2)	2396.9	59.08	12202406.3
T mple	(0)	432.0	50.22	2344380.3
	(1)	432.0	50.22	2344380.3
	(2)	432.0	50.22	2344380.3

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T tulo Secci n: J REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2122.16Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

An isis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1195.6 Xu(cm.): 67.3

Nu(Tn.): -.8 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00268 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -367.5 Xu(cm.): 195.2

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00120 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3639.1 aplicado en Yo(cm)= 139.2

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 893.5 aplicado en Yo(cm)= 166.9

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S. rciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)*

T tulo Secci n: J REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2122.16Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1530.4 Xu(cm.): 23.9

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00150 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3654.8 Xu(cm.): 75.9

Nu(Tn.): -.1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00166
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8422.4 aplicado en Yo(cm)= 69.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3630.3 aplicado en Yo(cm)= 52.0

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VT TORRENTE DEL BO

Seccion:K REF M+ M-

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	$J_{\pi}1$	$J_{\pi}2$
1 (HO)	500.0	1.50	319285	2.60	1.45
2 (HO)	300.0	1.50	285770	2.60	1.45
3 (PR)	17100.0	1.15	2000000		
4 (RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	12.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
0	4	10.0	25.0	207.0	CT	0
1	4	6.0	25.0	35.5	CT	0
2	4	35.0	20.0	23.0	CT	0
3	4	35.0	20.0	3.0	CT	0
4	3	84.0	13.4	14.0	*T	0

ECCIONES INTERMEDIAS

um.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
5	PL	14

* CONSTANTES ESTATICAS *

COMPLETA

po	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
pura +	(0)	2250.4	18.89	3622418.3
	(1)	1246.4	30.07	3324395.9
	(2)	1479.0	26.45	3416912.8
pura -	(0)	1393.2	147.87	8549489.4
	(1)	773.4	107.88	5880541.5
	(2)	898.2	119.78	6657198.7
Simple	(0)	5264.9	60.65	26826048.0
	(1)	1788.0	59.91	9454544.3
	(2)	2415.7	60.20	12590999.0
T.Simple	(0)	450.8	56.61	2767178.2
	(1)	450.8	56.61	2767178.2
	(2)	450.8	56.61	2767178.2

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

T┌tulo Secci├n: K REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2392.25Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 1559.6 Xu(cm.): 95.0

Nu(Tn.): .8 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00583
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

Mu(m.T): -362.4 Xu(cm.): 193.1

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00148 Etmx= .01000
Rompe la fibra superior de la S.parcial 3

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -3639.1 aplicado en Yo(cm)= 139.2

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 1187.1 aplicado en Yo(cm)= 175.9

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: K REF M+ M-

* REDISTRIBUCIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 2392.25Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[Π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2127.4 Xu(cm.): 26.0

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00162 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3424.3 Xu(cm.): 72.7

Nu(Tn.): -.4 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00149
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8422.4 aplicado en Yo(cm)= 69.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3923.8 aplicado en Yo(cm)= 63.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
N.parciales resistentes: Rcu(Kg/cm):

Proyecto:
VTO TORRENTE DEL BO

Seccion:L REF M+ M-

MATERIALES

Num.	Fck (Kg/cm2)	Gamma	M.El. (Kg/cm2)	Jπ1	Jπ2
1(HO)	500.0	1.50	319285	2.60	1.45
2(HO)	300.0	1.50	285770	2.60	1.45
3(PR)	17100.0	1.15	2000000		
4(RD)	5100.0	1.15	2000000		

SECCIONES PARCIALES

Num	Mat.	B(cm) Num	H(cm) π(mm)	Yo(cm)	Mc	Nsr
1	1	179.0	27.2	184.8	C*	0
2	1	36.0	137.8	47.0	C*	0
3	1	119.0	15.0	32.0	C*	0
4	2	700.0	32.0	0.0	C*	0
5	3	24.0	13.4	207.0	*T	0
6	3	12.0	13.4	202.0	*T	0
7	3	0.0	13.4	197.0	*T	0
8	3	0.0	13.4	192.0	*T	0
9	3	4.0	13.4	37.0	*T	0
10	4	10.0	25.0	207.0	CT	0
11	4	6.0	25.0	35.5	CT	0
12	4	35.0	20.0	23.0	CT	0
13	4	35.0	20.0	3.0	CT	0
14	3	42.0	13.4	14.0	*T	0

SECCIONES INTERMEDIAS

Num.	Codigo	Componentes
1	HC	1 2 3
2	PS	9
3	PI	5 6 7 8
4	CA	1 2 3 5 6 7 8 9 10 11
5	HL	4
6	PL	14

* CONSTANTES ESTATICAS *

S.COMPLETA

Tipo	Acciones	Area(cm2)	Xcg(cm)	Inercia(cm4)
F:pura +	(0)	2204.3	19.00	3621378.2
	(1)	1209.2	30.79	3310379.9
	(2)	1440.6	26.91	3408773.7
F.pura -	(0)	1305.6	153.55	7506105.7
	(1)	705.7	115.27	5351709.4
	(2)	825.9	126.89	5991950.2
C.Simple	(0)	5208.5	61.14	26705511.1
	(1)	1731.6	61.38	9335323.1

	(2)	2359.3	61.29	12471260.9
T.Simple	(0)	394.4	62.60	2653779.0
	(1)	394.4	62.60	2653779.0
	(2)	394.4	62.60	2653779.0

*** Nota: Homogeneizadas a E=2100000 Kp/cm2 ***

ANALISIS EN ROTURA(ELASTOPLASTICO)

Título Sección: L REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1581.97Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION CA

Analisis con Resistencia de materiales MINORADAS
De) Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

fu(m.T): 1559.5 Xu(cm.): 96.1

Nu(Tn.): .2 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00582
Rompe la fibra superior de la S.parcial 3

FLEXION PURA NEGATIVA:

u(m.T): -362.4 Xu(cm.): 193.3

u( ).): 0.0 Qu(Tn.): 0.0

eformaciones Ultimas: Ecmx= -.00148 Etmx= .01000
ompe la fibra superior de la S.parcial 3

OMPRESION SIMPLE(Rigido/Plastico):

u(Tn.): -3639.1 aplicado en Yo(cm)= 139.2

TRACCION SIMPLE(Rigido/Plastico):

u(Tn.): 1187.1 aplicado en Yo(cm)= 175.9

ORTANTE ULTIMO(Rigido/Plastico):

u(Tn.): 0.0 Ru(Kg/cm): 0.0

1(cm): 0.0 Xv2(cm): 0.0
parciales resistentes: Rcu(Kg/cm):

NALISIS EN ROTURA(ELASTOPLASTICO)*

Título Sección: L REF M+ M-

* PRESOLICITACIONES ELASTICAS
Analisis SIN FISURACION
Pretensado: 1581.97Tn.
(Todas las Armaduras activas a .80*Fyk)

ESTUDIO SECCION COMPLETA

Analisis con Resistencia de materiales MINORADAS
Def. Ultima Acero Estructural(COMPRESION)(%): 2.50
Def. Ultima Acero Estructural(TRACCION)(%): 2.50
Deformacion Ultima Hormigon(COMPRESION) : Pivote en Bloque de Hormigon
Deformacion Ultima Hormigon(TRACCION)(%): 1.00
Coeficiente Ideal Fluencia[π*(Cperm./Ctot.)]: 0.00

FLEXION PURA POSITIVA:

Mu(m.T): 2137.2 Xu(cm.): 23.3

Nu(Tn.): 0.0 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00135 Etmx= .01000
Rompe la fibra inferior de la S.parcial 1

FLEXION PURA NEGATIVA:

Mu(m.T): -3198.2 Xu(cm.): 98.4

Nu(Tn.): .1 Qu(Tn.): 0.0

Deformaciones Ultimas: Ecmx= -.00350 Etmx= .00269
Rompe la fibra inferior de la S.parcial 1

COMPRESION SIMPLE(Rigido/Plastico):

Nu(Tn.): -8422.4 aplicado en Yo(cm)= 69.0

TRACCION SIMPLE(Rigido/Plastico):

Nu(Tn.): 3043.1 aplicado en Yo(cm)= 77.3

CORTANTE ULTIMO(Rigido/Plastico):

Vu(Tn.): 0.0 Ru(Kg/cm): 0.0

Xv1(cm): 0.0 Xv2(cm): 0.0
S.parciales resistentes: Rcu(Kg/cm):

ESFUERZOS COMBINADOS

ROTURA A CORTANTE

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-84.55	-0.04
1	2	1.10	0.00	-63.89	89.55
2	2	1.10	0.00	-64.55	89.49
2	3	2.20	0.00	-44.94	171.69
3	3	2.20	0.00	-45.84	171.63
3	4	3.30	0.00	-25.26	246.20
4	4	3.30	0.00	-26.32	247.24
4	5	4.40	0.00	-4.81	309.95
5	5	4.40	0.00	-6.08	309.85
5	6	5.50	0.00	16.36	357.71
6	6	5.50	0.00	14.92	359.11
6	7	6.60	0.00	38.23	389.38
7	7	6.60	0.00	36.58	392.06
7	8	7.70	0.00	61.55	442.87
8	8	7.70	0.00	59.83	455.33
8	9	8.80	0.00	93.89	858.52
9	9	8.80	0.00	91.40	883.43
9	10	9.90	0.00	131.27	822.44
10	10	9.90	0.00	129.56	874.86
10	11	11.00	0.00	170.91	811.03
11	11	11.00	0.00	170.28	896.52
11	12	12.10	0.00	213.89	840.76
12	12	12.10	0.00	214.81	862.30
12	13	13.20	0.00	258.99	650.60
13	13	13.20	0.00	259.75	655.87
13	14	14.30	0.00	304.94	420.91
14	14	14.30	30.73	295.89	428.32
14	15	15.40	35.44	341.72	121.38
15	15	15.40	0.00	353.28	122.58
15	16	16.50	0.00	399.38	-238.68
16	16	16.50	0.00	400.24	-142.76
16	17	17.60	0.00	446.85	-567.63
17	17	17.60	-0.01	447.95	-536.10
17	18	18.70	-0.01	495.92	-1021.85
18	18	18.70	0.00	496.84	-1016.25
18	19	19.80	0.00	545.24	-1564.91
19	19	19.80	0.00	545.91	-1557.08
19	20	20.90	0.00	594.72	-2167.62
20	20	20.90	0.00	594.97	-2164.50
20	21	22.00	0.00	651.54	-2840.65
21	1021	22.00	0.00	-180.20	-550.07
21	22	23.40	0.00	-149.94	-308.21
22	22	23.40	0.00	-151.37	-300.14
22	23	24.80	0.00	-127.20	-82.08
23	23	24.80	0.00	-129.16	-82.84
23	24	26.20	0.00	-104.11	116.43
24	24	26.20	0.00	-106.46	115.88
24	25	27.60	0.00	-80.38	294.12
25	25	27.60	0.00	-83.18	296.77
25	26	29.00	0.00	-55.90	460.59
26	26	29.00	18.83	-54.12	463.94

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To +[1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	15.34	-26.05	592.40
27	27	30.40	0.00	-33.15	633.58
27	28	31.80	0.00	-3.85	771.50
28	28	31.80	0.00	-6.65	762.13
28	29	33.20	0.00	24.54	881.32
29	29	33.20	0.00	21.18	892.31
29	30	34.60	0.00	53.65	936.77
30	30	34.60	0.00	51.02	1008.22
30	31	36.00	0.00	87.75	1325.32
31	31	36.00	0.00	86.38	1347.06
31	32	37.40	0.00	137.36	1501.16
32	32	37.40	0.00	137.85	1634.56
32	33	38.80	0.00	191.21	1506.33
33	33	38.80	0.00	193.48	1536.26
33	34	40.20	0.00	247.92	1325.06
34	34	40.20	0.00	249.85	1326.82
34	35	41.60	0.00	305.89	1028.07
35	35	41.60	13.15	303.81	1051.71
35	36	43.00	17.86	361.31	648.28
36	36	43.00	0.00	367.60	722.11
36	37	44.40	0.00	426.00	225.66
37	37	44.40	0.00	428.03	251.59
37	38	45.80	0.00	487.59	-325.57
38	38	45.80	0.00	489.29	-311.29
38	39	47.20	0.00	549.93	-1001.50
39	39	47.20	0.00	551.13	-997.37
39	40	48.60	0.00	612.59	-1787.37
40	40	48.60	0.00	613.13	-1779.40
40	41	50.00	0.00	684.92	-2660.33
41	1041	50.00	0.00	-177.93	-719.81
41	42	51.40	0.00	-147.67	-481.09
42	42	51.40	0.00	-149.78	-472.55
42	43	52.80	0.00	-125.64	-256.43
43	43	52.80	0.00	-128.20	-251.99
43	44	54.20	0.00	-103.13	-53.52
44	44	54.20	0.00	-106.07	-38.92
44	45	55.60	0.00	-79.96	139.36
45	45	55.60	0.00	-83.04	165.38
45	46	57.00	0.00	-55.90	320.79
46	46	57.00	12.64	-55.27	393.66
46	47	58.40	9.15	-27.15	522.05
47	47	58.40	0.00	-31.62	546.00
47	48	59.80	0.00	-2.50	643.68
48	48	59.80	0.00	-4.91	643.93
48	49	61.20	0.00	26.73	754.30
49	49	61.20	0.00	23.61	779.41
49	50	62.60	0.00	56.84	826.07
50	50	62.60	0.00	54.76	904.72
50	51	64.00	0.00	89.80	977.23
51	51	64.00	0.00	89.15	1048.21
51	52	65.40	0.00	140.25	1432.99

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	142.02	1508.67
52	53	66.80	0.00	195.54	1374.52
53	53	66.80	0.00	198.04	1386.89
53	54	68.20	0.00	252.63	1168.90
54	54	68.20	0.00	254.69	1197.88
54	55	69.60	0.00	310.98	892.94
55	55	69.60	19.91	308.23	934.89
55	56	71.00	24.63	365.75	522.80
56	56	71.00	0.00	374.22	526.02
56	57	72.40	0.00	432.49	42.38
57	57	72.40	0.00	434.18	44.73
57	58	73.80	0.00	493.89	-556.25
58	58	73.80	0.00	495.04	-557.11
58	59	75.20	0.00	555.59	-1255.00
59	59	75.20	0.00	556.20	-1256.10
59	60	76.60	0.00	617.55	-2052.34
60	60	76.60	0.00	617.51	-2044.55
60	61	78.00	0.00	689.41	-2933.90
61	1061	78.00	0.00	-190.57	-658.16
61	62	79.10	0.00	-166.82	-454.06
62	62	79.10	0.00	-168.48	-450.92
62	63	80.20	0.00	-149.71	-260.35
63	63	80.20	0.00	-151.71	-250.36
63	64	81.30	0.00	-132.36	-70.78
64	64	81.30	0.00	-134.62	-65.06
64	65	82.40	0.00	-114.70	104.02
65	65	82.40	0.00	-116.82	163.10
65	66	83.50	0.00	-96.28	319.64
66	66	83.50	0.00	-98.05	410.48
66	67	84.60	0.00	-76.61	556.88
67	67	84.60	27.73	-69.19	558.48
67	68	85.70	24.24	-47.39	683.59
68	68	85.70	0.00	-56.47	688.94
68	69	86.80	0.00	-33.98	783.77
69	69	86.80	0.00	-35.54	797.15
69	70	87.90	0.00	-10.78	890.86
70	70	87.90	0.00	-12.71	907.60
70	71	89.00	0.00	13.18	1057.65
71	71	89.00	0.00	12.11	1111.57
71	72	90.10	0.00	38.56	1241.73
72	72	90.10	0.00	38.20	1294.10
72	73	91.20	0.00	68.52	1308.47
73	73	91.20	0.00	69.42	1353.77
73	74	92.30	0.00	104.26	1635.03
74	74	92.30	0.00	105.29	1647.50
74	75	93.40	0.00	147.58	1621.71
75	75	93.40	0.00	148.42	1624.29
75	76	94.50	0.00	192.54	1502.45
76	76	94.50	0.00	193.18	1504.35
76	77	95.60	0.00	238.32	1324.10
77	77	95.60	0.00	238.70	1323.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	284.55	1092.93
78	78	96.70	0.00	284.72	1093.76
78	79	97.80	0.00	331.20	798.36
79	79	97.80	0.00	331.02	798.09
79	80	98.90	0.00	378.52	434.75
80	80	98.90	0.00	378.00	434.42
80	81	100.00	0.00	429.07	0.18
101	101	0.00	0.00	-77.97	0.16
101	102	1.10	0.00	-58.29	85.05
102	102	1.10	0.00	-59.00	85.38
102	103	2.20	0.00	-40.03	167.47
103	103	2.20	0.00	-40.74	167.73
103	104	3.30	0.00	-20.49	245.53
104	104	3.30	0.00	-21.09	247.06
104	105	4.40	0.00	0.37	315.12
105	105	4.40	0.00	-0.25	315.24
105	106	5.50	0.00	22.43	369.56
106	106	5.50	0.00	21.73	370.33
106	107	6.60	0.00	45.52	407.18
107	107	6.60	0.00	44.71	409.98
107	108	7.70	0.00	70.42	466.69
108	108	7.70	0.00	69.71	490.64
108	109	8.80	0.00	104.55	907.88
109	109	8.80	0.00	103.49	950.77
109	110	9.90	0.00	144.35	888.79
110	110	9.90	0.00	144.28	935.39
110	111	11.00	0.00	186.97	878.27
111	111	11.00	0.00	188.39	976.51
111	112	12.10	0.00	233.59	915.55
112	112	12.10	0.00	236.03	919.83
112	113	13.20	0.00	282.19	696.40
113	113	13.20	0.00	284.57	697.60
113	114	14.30	0.00	331.63	450.97
114	114	14.30	30.73	324.25	451.64
114	115	15.40	35.44	372.25	124.49
115	115	15.40	0.00	385.56	126.49
115	116	16.50	0.00	433.95	-261.06
116	116	16.50	0.00	436.09	-257.69
116	117	17.60	0.00	485.35	-714.76
117	117	17.60	0.00	487.50	-711.63
117	118	18.70	0.00	538.18	-1235.76
118	118	18.70	0.00	540.38	-1229.65
118	119	19.80	0.00	591.64	-1823.29
119	119	19.80	0.00	594.06	-1770.84
119	120	20.90	0.00	645.83	-2433.67
120	120	20.90	0.00	648.27	-2421.35
120	121	22.00	0.00	707.95	-3157.63
121	1121	22.00	0.00	-174.88	-487.61
121	122	23.40	0.00	-145.78	-252.33
122	122	23.40	0.00	-146.86	-252.55
122	123	24.80	0.00	-123.62	-36.54

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-124.94	-36.79
123	124	26.20	0.00	-100.49	164.00
124	124	26.20	0.00	-102.06	171.20
124	125	27.60	0.00	-76.30	353.36
125	125	27.60	0.00	-78.02	358.40
125	126	29.00	0.00	-50.80	527.55
126	126	29.00	18.83	-47.64	566.76
126	127	30.40	15.34	-19.35	700.69
127	127	30.40	0.00	-24.96	700.88
127	128	31.80	0.00	4.56	804.89
128	128	31.80	0.00	2.64	805.26
128	129	33.20	0.00	34.45	942.04
129	129	33.20	0.00	31.76	948.86
129	130	34.60	0.00	65.54	999.72
130	130	34.60	0.00	63.77	1072.15
130	131	36.00	0.00	102.49	1373.69
131	131	36.00	0.00	101.84	1382.33
131	132	37.40	0.00	153.98	1550.74
132	132	37.40	0.00	155.29	1666.13
132	133	38.80	0.00	210.12	1535.73
133	133	38.80	0.00	213.29	1574.90
133	134	40.20	0.00	269.52	1356.91
134	134	40.20	0.00	272.61	1359.09
134	135	41.60	0.00	330.97	1047.52
135	135	41.60	13.15	330.36	1050.12
135	136	43.00	17.86	390.38	622.66
136	136	43.00	0.00	397.65	625.62
136	137	44.40	0.00	458.78	97.86
137	137	44.40	0.00	461.61	136.98
137	138	45.80	0.00	524.25	-475.62
138	138	45.80	0.00	527.45	-429.50
138	139	47.20	0.00	591.46	-1168.48
139	139	47.20	0.00	594.78	-1150.84
139	140	48.60	0.00	659.86	-2000.73
140	140	48.60	0.00	663.16	-1993.34
140	141	50.00	0.00	738.83	-2942.79
141	1141	50.00	-0.01	-172.05	-641.30
141	142	51.40	-0.01	-142.96	-409.88
142	142	51.40	0.00	-144.64	-402.45
142	143	52.80	0.00	-121.38	-189.12
143	143	52.80	0.00	-123.21	-171.69
143	144	54.20	0.00	-98.70	27.16
144	144	54.20	0.00	-100.50	73.04
144	145	55.60	0.00	-74.70	253.69
145	145	55.60	0.00	-76.15	292.44
145	146	57.00	0.00	-49.04	450.92
146	146	57.00	12.64	-47.36	452.69
146	147	58.40	9.15	-19.00	584.72
147	147	58.40	0.00	-23.08	587.08
147	148	59.80	0.00	6.51	689.10
148	148	59.80	0.00	4.51	689.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY+

C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	36.89	816.17
149	149	61.20	0.00	34.33	850.79
149	150	62.60	0.00	68.99	904.97
150	150	62.60	0.00	67.66	970.26
150	151	64.00	0.00	104.35	1061.45
151	151	64.00	0.00	104.41	1117.56
151	152	65.40	0.00	156.70	1481.35
152	152	65.40	0.00	158.99	1555.67
152	153	66.80	0.00	214.03	1419.97
153	153	66.80	0.00	217.32	1428.32
153	154	68.20	0.00	273.73	1204.15
154	154	68.20	0.00	276.76	1204.66
154	155	69.60	0.00	335.42	888.15
155	155	69.60	19.91	333.00	888.54
155	156	71.00	24.63	393.01	454.83
156	156	71.00	0.00	402.17	495.24
156	157	72.40	0.00	463.23	-13.50
157	157	72.40	0.00	466.13	-8.14
157	158	73.80	0.00	528.97	-646.02
158	158	73.80	0.00	531.88	-638.56
158	159	75.20	0.00	595.85	-1383.35
159	159	75.20	0.00	598.69	-1383.42
159	160	76.60	0.00	663.69	-2237.84
160	160	76.60	0.00	666.35	-2238.02
160	161	78.00	0.00	742.16	-3194.78
161	1161	78.00	0.00	-184.10	-524.17
161	162	79.10	0.00	-161.33	-326.86
162	162	79.10	0.00	-162.51	-313.56
162	163	80.20	0.00	-144.55	-127.01
163	163	80.20	0.00	-145.76	-73.95
163	164	81.30	0.00	-127.05	103.74
164	164	81.30	0.00	-128.06	110.26
164	165	82.40	0.00	-108.62	278.89
165	165	82.40	0.00	-109.75	281.82
165	166	83.50	0.00	-89.50	439.11
166	166	83.50	0.00	-90.69	442.74
166	167	84.60	0.00	-69.36	591.29
167	167	84.60	27.73	-61.96	593.42
167	168	85.70	24.24	-40.11	722.29
168	168	85.70	0.00	-49.23	722.78
168	169	86.80	0.00	-26.56	834.63
169	169	86.80	0.00	-28.19	835.85
169	170	87.90	0.00	-3.26	940.33
170	170	87.90	0.00	-5.19	940.40
170	171	89.00	0.00	21.69	1101.51
171	171	89.00	0.00	20.27	1162.46
171	172	90.10	0.00	47.42	1317.47
172	172	90.10	0.00	46.83	1274.65
172	173	91.20	0.00	78.81	1384.83
173	173	91.20	0.00	79.66	1450.90
173	174	92.30	0.00	116.06	1711.93

Cortante.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECT.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY+

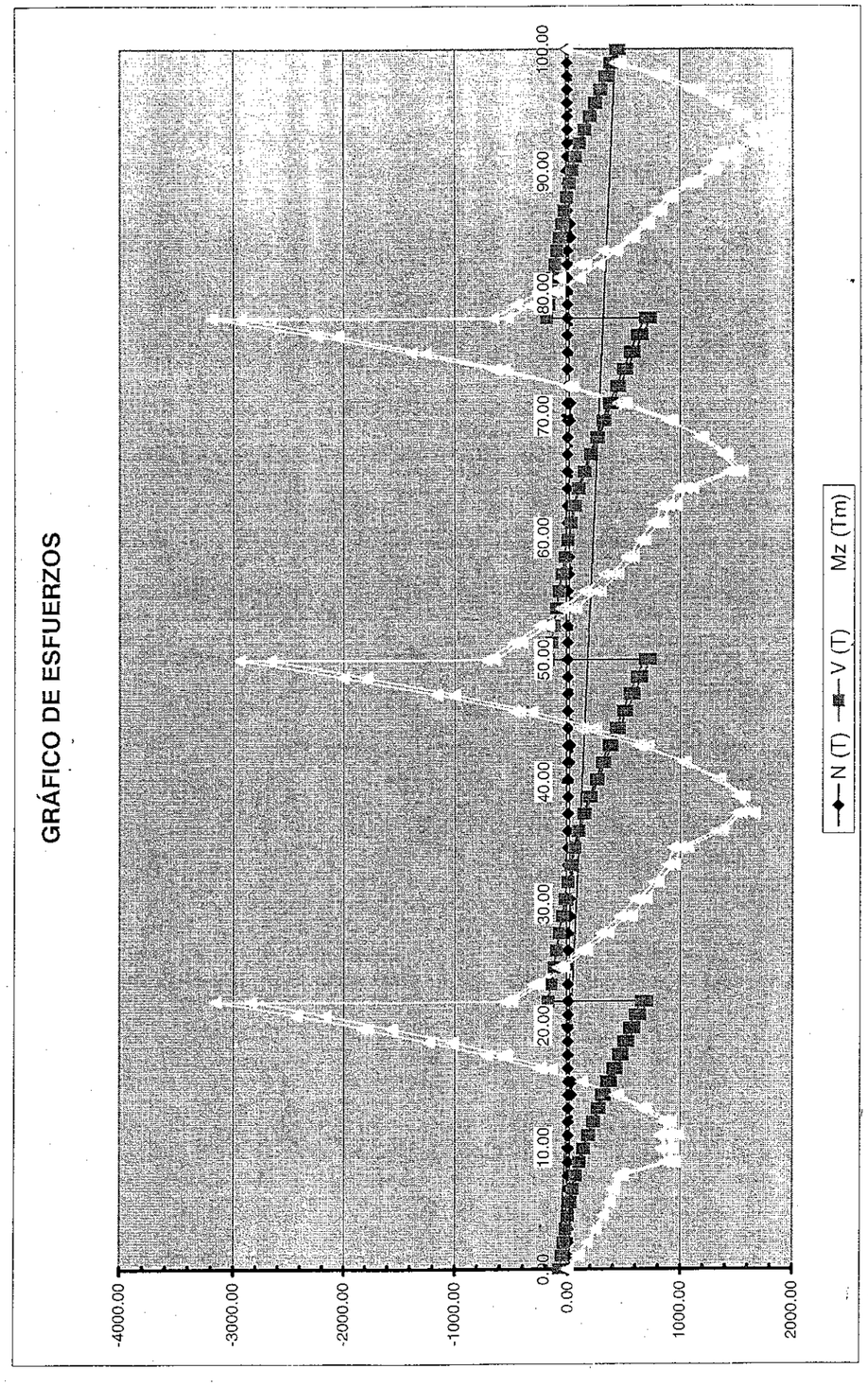
C. Totales dominante Tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	117.52	1735.53
174	175	93.40	0.00	161.23	1712.91
175	175	93.40	0.00	162.84	1718.13
175	176	94.50	0.00	208.64	1595.50
176	176	94.50	0.00	210.21	1596.41
176	177	95.60	0.00	257.36	1410.35
177	177	95.60	0.00	258.95	1410.71
177	178	96.70	0.00	306.82	1168.82
178	178	96.70	0.00	308.52	1170.59
178	179	97.80	0.00	357.47	858.23
179	179	97.80	0.00	359.31	858.81
179	180	98.90	0.00	409.70	469.69
180	180	98.90	0.00	411.68	470.33
180	181	100.00	0.00	466.02	-0.32

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-189.91	-0.14
1	2	1.10	0.00	-108.05	129.21
2	2	1.10	0.00	-107.84	129.14
2	3	2.20	0.00	-90.85	238.42
3	3	2.20	0.00	-90.68	238.35
3	4	3.30	0.00	-73.67	328.73
4	4	3.30	0.00	-73.51	328.67
4	5	4.40	0.00	-56.52	400.17
5	5	4.40	0.00	-56.40	400.12
5	6	5.50	0.00	-39.40	452.80
6	6	5.50	0.00	-39.28	452.76
6	7	6.60	0.00	-22.29	486.64
7	7	6.60	0.00	-22.20	486.62
7	8	7.70	0.00	-5.21	501.69
8	8	7.70	0.00	-5.12	501.67
8	9	8.80	0.00	11.88	497.94
9	9	8.80	0.00	11.96	497.94
9	10	9.90	0.00	28.95	475.43
10	10	9.90	0.00	29.03	475.43
10	11	11.00	0.00	46.02	434.15
11	11	11.00	0.00	46.11	434.17
11	12	12.10	0.00	63.11	374.10
12	12	12.10	0.00	63.21	374.12
12	13	13.20	0.00	80.19	295.23
13	13	13.20	0.00	80.30	295.26
13	14	14.30	0.00	97.32	197.59
14	14	14.30	24.24	89.83	197.63
14	15	15.40	35.44	117.87	67.37
15	15	15.40	0.00	129.15	67.42
15	16	16.50	0.00	209.71	-94.21
16	16	16.50	0.00	210.11	-94.10
16	17	17.60	0.00	235.34	-339.06
17	17	17.60	-0.01	235.80	-338.95
17	18	18.70	-0.01	266.01	-615.84
18	18	18.70	0.00	266.50	-615.73
18	19	19.80	0.00	293.49	-923.73
19	19	19.80	0.00	293.50	-929.19
19	20	20.90	0.00	324.06	-1284.36
20	20	20.90	0.00	322.97	-1287.47
20	21	22.00	0.00	358.51	-1669.85
21	1021	22.00	0.00	-666.97	-2933.87
21	22	23.40	0.00	-599.51	-2072.82
22	22	23.40	0.00	-599.58	-2080.65
22	23	24.80	0.00	-540.20	-1308.18
23	23	24.80	0.00	-539.60	-1307.06
23	24	26.20	0.00	-476.79	-633.36
24	24	26.20	0.00	-475.60	-632.48
24	25	27.60	0.00	-218.90	-54.70
25	25	27.60	0.00	-418.47	-56.47
25	26	29.00	0.00	-126.66	145.54
26	26	29.00	24.63	-120.18	145.47

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.91	-96.32	305.00
27	27	30.40	0.00	-101.29	304.94
27	28	31.80	0.00	-70.14	420.87
28	28	31.80	0.00	-70.03	420.82
28	29	33.20	0.00	-48.41	503.75
29	29	33.20	0.00	-48.33	503.72
29	30	34.60	0.00	-26.69	556.23
30	30	34.60	0.00	-26.62	556.20
30	31	36.00	0.00	-4.99	578.33
31	31	36.00	0.00	-4.92	578.34
31	32	37.40	0.00	16.71	570.09
32	32	37.40	0.00	16.78	570.11
32	33	38.80	0.00	38.42	531.48
33	33	38.80	0.00	38.51	531.52
33	34	40.20	0.00	60.13	462.46
34	34	40.20	0.00	60.24	462.51
34	35	41.60	0.00	81.87	363.05
35	35	41.60	9.15	79.66	363.10
35	36	43.00	17.86	110.81	223.19
36	36	43.00	0.00	115.55	223.27
36	37	44.40	0.00	202.00	26.27
37	37	44.40	0.00	202.52	26.46
37	38	45.80	0.00	239.30	-280.39
38	38	45.80	0.00	239.90	-280.21
38	39	47.20	0.00	274.24	-640.11
39	39	47.20	0.00	274.91	-639.96
39	40	48.60	0.00	309.26	-1048.88
40	40	48.60	0.00	309.99	-1048.80
40	41	50.00	0.00	351.35	-1511.74
41	1041	50.00	0.00	-659.38	-2862.21
41	42	51.40	0.00	-592.04	-2013.91
42	42	51.40	0.00	-591.50	-2021.88
42	43	52.80	0.00	-532.04	-1259.99
43	43	52.80	0.00	-530.84	-1264.11
43	44	54.20	0.00	-472.19	-599.26
44	44	54.20	0.00	-470.51	-613.53
44	45	55.60	0.00	-410.51	-62.96
45	45	55.60	0.00	-408.47	-88.91
45	46	57.00	0.00	-121.88	222.31
46	46	57.00	17.86	-116.86	222.13
46	47	58.40	9.15	-79.67	363.11
47	47	58.40	0.00	-81.87	363.05
47	48	59.80	0.00	-60.24	462.53
48	48	59.80	0.00	-60.13	462.48
48	49	61.20	0.00	-38.51	531.51
49	49	61.20	0.00	-38.42	531.47
49	50	62.60	0.00	-16.78	570.12
50	50	62.60	0.00	-16.71	570.10
50	51	64.00	0.00	4.93	578.34
51	51	64.00	0.00	4.99	578.34
51	52	65.40	0.00	26.62	556.21

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	26.69	556.23
52	53	66.80	0.00	48.33	503.72
53	53	66.80	0.00	48.42	503.76
53	54	68.20	0.00	70.03	420.84
54	54	68.20	0.00	70.14	420.89
54	55	69.60	0.00	101.29	304.95
55	55	69.60	19.91	96.32	305.02
55	56	71.00	24.63	120.19	145.46
56	56	71.00	0.00	126.66	145.53
56	57	72.40	0.00	211.10	-50.52
57	57	72.40	0.00	211.61	-50.34
57	58	73.80	0.00	243.74	-369.09
58	58	73.80	0.00	244.30	-368.91
58	59	75.20	0.00	282.88	-737.77
59	59	75.20	0.00	283.54	-737.61
59	60	76.60	0.00	317.90	-1158.65
60	60	76.60	0.00	318.62	-1158.56
60	61	78.00	0.00	359.95	-1633.57
61	1061	78.00	0.00	-633.98	-2840.70
61	62	79.10	0.00	-580.88	-2181.96
62	62	79.10	0.00	-580.63	-2185.10
62	63	80.20	0.00	-533.39	-1589.20
63	63	80.20	0.00	-532.72	-1597.03
63	64	81.30	0.00	-485.89	-1061.29
64	64	81.30	0.00	-484.95	-1066.84
64	65	82.40	0.00	-435.32	-593.20
65	65	82.40	0.00	-434.22	-624.72
65	66	83.50	0.00	-390.95	-211.90
66	66	83.50	0.00	-390.10	-307.85
66	67	84.60	0.00	-291.74	-6.03
67	67	84.60	35.44	-280.37	-7.14
67	68	85.70	24.24	-89.81	197.64
68	68	85.70	0.00	-97.33	197.59
68	69	86.80	0.00	-80.31	295.27
69	69	86.80	0.00	-80.20	295.24
69	70	87.90	0.00	-63.22	374.11
70	70	87.90	0.00	-63.12	374.09
70	71	89.00	0.00	-46.12	434.16
71	71	89.00	0.00	-46.03	434.15
71	72	90.10	0.00	-29.04	475.44
72	72	90.10	0.00	-28.96	475.43
72	73	91.20	0.00	-11.97	497.94
73	73	91.20	0.00	-11.89	497.94
73	74	92.30	0.00	-56.04	455.36
74	74	92.30	0.00	-57.93	452.12
74	75	93.40	0.00	-32.24	441.07
75	75	93.40	0.00	-35.88	438.70
75	76	94.50	0.00	-10.78	404.86
76	76	94.50	0.00	-12.32	403.46
76	77	95.60	0.00	11.92	350.12
77	77	95.60	0.00	10.53	350.19

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	33.84	280.17
78	78	96.70	0.00	32.63	279.06
78	79	97.80	0.00	55.02	195.40
79	79	97.80	0.00	53.97	195.42
79	80	98.90	0.00	75.38	102.28
80	80	98.90	0.00	74.55	102.29
80	81	100.00	0.00	155.35	-0.12
101	101	0.00	0.00	-372.36	-0.38
101	102	1.10	0.00	-101.98	122.26
102	102	1.10	0.00	-102.19	122.34
102	103	2.20	0.00	-85.86	225.76
103	103	2.20	0.00	-86.03	225.83
103	104	3.30	0.00	-69.67	311.45
104	104	3.30	0.00	-69.81	311.51
104	105	4.40	0.00	-53.48	379.31
105	105	4.40	0.00	-53.60	379.36
105	106	5.50	0.00	-37.25	429.32
106	106	5.50	0.00	-37.36	429.37
106	107	6.60	0.00	-21.02	461.49
107	107	6.60	0.00	-21.11	461.51
107	108	7.70	0.00	-4.77	475.74
108	108	7.70	0.00	-4.85	475.76
108	109	8.80	0.00	11.50	472.10
109	109	8.80	0.00	11.42	472.10
109	110	9.90	0.00	27.76	450.54
110	110	9.90	0.00	27.68	450.53
110	111	11.00	0.00	44.02	411.10
111	111	11.00	0.00	43.94	411.08
111	112	12.10	0.00	60.30	353.74
112	112	12.10	0.00	60.20	353.71
112	113	13.20	0.00	76.53	278.49
113	113	13.20	0.00	76.42	278.46
113	114	14.30	0.00	92.78	185.40
114	114	14.30	24.24	85.06	185.36
114	115	15.40	35.44	112.45	60.69
115	115	15.40	0.00	123.45	60.64
115	116	16.50	0.00	193.77	-94.57
116	116	16.50	0.00	193.37	-94.70
116	117	17.60	0.00	216.98	-320.39
117	117	17.60	0.00	216.53	-320.51
117	118	18.70	0.00	245.11	-575.30
118	118	18.70	0.00	244.62	-575.40
118	119	19.80	0.00	269.98	-858.42
119	119	19.80	0.00	269.43	-858.51
119	120	20.90	0.00	294.80	-1168.86
120	120	20.90	0.00	294.22	-1168.90
120	121	22.00	0.00	325.09	-1509.53
121	1121	22.00	0.00	-719.73	-3194.70
121	122	23.40	0.00	-648.36	-2266.28
122	122	23.40	0.00	-645.69	-2266.09
122	123	24.80	0.00	-582.69	-1435.47

Cortante.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECT.T0.VY-

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-579.84	-1435.41
123	124	26.20	0.00	-513.63	-714.78
124	124	26.20	0.00	-510.73	-722.26
124	125	27.60	0.00	-452.11	-106.99
125	125	27.60	0.00	-449.19	-112.34
125	126	29.00	0.00	-121.40	137.83
126	126	29.00	24.63	-115.25	137.91
126	127	30.40	19.91	-92.21	291.12
127	127	30.40	0.00	-97.44	291.18
127	128	31.80	0.00	-67.11	402.30
128	128	31.80	0.00	-67.21	402.35
128	129	33.20	0.00	-46.43	481.92
129	129	33.20	0.00	-46.51	481.96
129	130	34.60	0.00	-25.69	532.47
130	130	34.60	0.00	-25.77	532.50
130	131	36.00	0.00	-4.96	554,01
131	131	36.00	0.00	-5.03	554.01
131	132	37.40	0.00	15.78	546.48
132	132	37.40	0.00	15.70	546.46
132	133	38.80	0.00	36.51	509.92
133	133	38.80	0.00	36.42	509.89
133	134	40.20	0.00	57.22	444.35
134	134	40.20	0.00	57.12	444.30
134	135	41.60	0.00	77.92	349.77
135	135	41.60	9.15	75.44	349.71
135	136	43.00	17.86	105.76	216.28
136	136	43.00	0.00	110.17	216.21
136	137	44.40	0.00	186.43	28.94
137	137	44.40	0.00	185.92	28.73
137	138	45.80	0.00	220.64	-253.47
138	138	45.80	0.00	220.05	-253.62
138	139	47.20	0.00	252.32	-584.28
139	139	47.20	0.00	251.66	-584.42
139	140	48.60	0.00	283.93	-959.34
140	140	48.60	0.00	283.20	-959.42
140	141	50.00	0.00	322.49	-1383.38
141	1141	50.00	-0.01	-713.29	-3144.67
141	142	51.40	-0.01	-642.09	-2227.84
142	142	51.40	0.00	-638.77	-2235.22
142	143	52.80	0.00	-575.70	-1413.43
143	143	52.80	0.00	-572.41	-1431.07
143	144	54.20	0.00	-510.36	-717.45
144	144	54.20	0.00	-507.17	-763.56
144	145	55.60	0.00	-444.09	-177.54
145	145	55.60	0.00	-441.26	-216.68
145	146	57.00	0.00	-116.50	215.25
146	146	57.00	17.86	-111.82	215.21
146	147	58.40	9.15	-75.45	349.72
147	147	58.40	0.00	-77.92	349.79
147	148	59.80	0.00	-57.12	444.30
148	148	59.80	0.00	-57.22	444.35

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-36.42	509.89
149	149	61.20	0.00	-36.51	509.93
149	150	62.60	0.00	-15.70	546.48
150	150	62.60	0.00	-15.78	546.50
150	151	64.00	0.00	5.03	554.01
151	151	64.00	0.00	4.96	554.01
151	152	65.40	0.00	25.77	532.50
152	152	65.40	0.00	25.69	532.48
152	153	66.80	0.00	46.50	481.96
153	153	66.80	0.00	46.43	481.93
153	154	68.20	0.00	67.21	402.36
154	154	68.20	0.00	67.11	402.31
154	155	69.60	0.00	97.44	291.19
155	155	69.60	19.91	92.21	291.12
155	156	71.00	24.63	115.25	137.91
156	156	71.00	0.00	121.40	137.84
156	157	72.40	0.00	195.87	-49.90
157	157	72.40	0.00	195.36	-50.07
157	158	73.80	0.00	225.44	-344.65
158	158	73.80	0.00	224.85	-344.83
158	159	75.20	0.00	261.36	-684.98
159	159	75.20	0.00	260.71	-685.12
159	160	76.60	0.00	293.00	-1072.75
160	160	76.60	0.00	292.29	-1072.86
160	161	78.00	0.00	331.58	-1509.54
161	1161	78.00	0.00	-690.35	-3157.70
161	162	79.10	0.00	-634.20	-2438.82
162	162	79.10	0.00	-631.76	-2451.15
162	163	80.20	0.00	-581.56	-1802.97
163	163	80.20	0.00	-579.10	-1855.44
163	164	81.30	0.00	-529.42	-1274.70
164	164	81.30	0.00	-527.24	-1280.78
164	165	82.40	0.00	-474.91	-768.73
165	165	82.40	0.00	-472.74	-771.87
165	166	83.50	0.00	-426.79	-326.88
166	166	83.50	0.00	-424.65	-330.25
166	167	84.60	0.00	-332.60	8.11
167	167	84.60	35.44	-319.07	6.06
167	168	85.70	24.24	-85.05	185.35
168	168	85.70	0.00	-92.79	185.39
168	169	86.80	0.00	-76.43	278.46
169	169	86.80	0.00	-76.54	278.49
169	170	87.90	0.00	-60.21	353.71
170	170	87.90	0.00	-60.30	353.74
170	171	89.00	0.00	-43.95	411.08
171	171	89.00	0.00	-44.03	411.10
171	172	90.10	0.00	-27.69	450.53
172	172	90.10	0.00	-27.77	450.54
172	173	91.20	0.00	-11.43	472.09
173	173	91.20	0.00	-11.51	472.09
173	174	92.30	0.00	4.84	475.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECT.T0.VY-

C. Totales dominante Tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	4.76	475.74
174	175	93.40	0.00	21.10	461.51
175	175	93.40	0.00	19.06	459.07
175	176	94.50	0.00	35.59	426.22
176	176	94.50	0.00	35.36	425.51
176	177	95.60	0.00	7.92	369.39
177	177	95.60	0.00	7.41	369.30
177	178	96.70	0.00	31.06	291.44
178	178	96.70	0.00	30.56	289.97
178	179	97.80	0.00	52.96	199.87
179	179	97.80	0.00	52.42	199.62
179	180	98.90	0.00	73.57	102.73
180	180	98.90	0.00	73.02	102.43
180	181	100.00	0.00	120.25	0.04

CÁLCULO TENSIONAL

Hipótesis de cálculo:

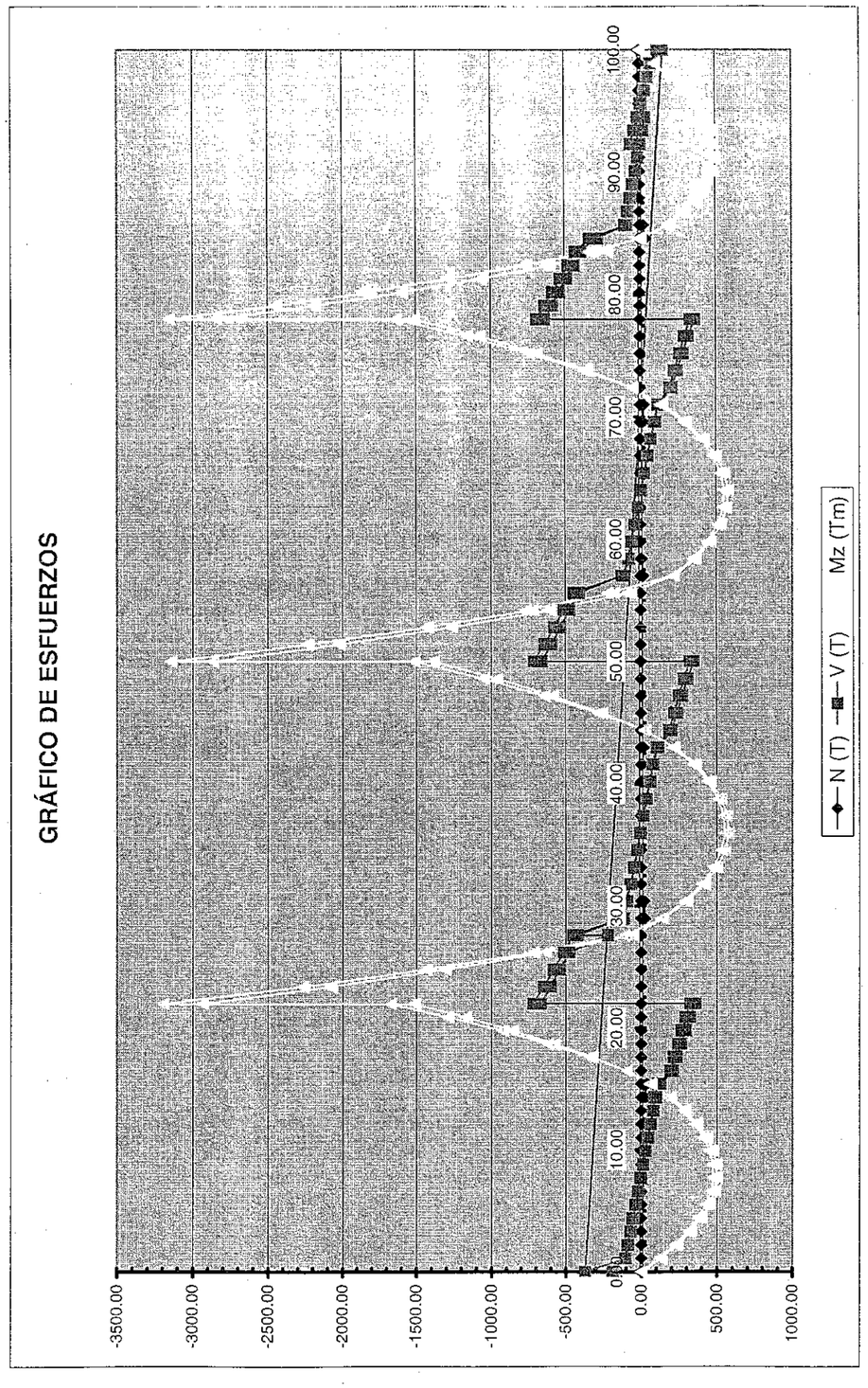
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-93.03	-0.04
1	2	1.10	0.00	-72.72	97.48
2	2	1.10	0.00	-73.21	97.42
2	3	2.20	0.00	-54.12	185.04
3	3	2.20	0.00	-54.81	184.98
3	4	3.30	0.00	-34.94	262.71
4	4	3.30	0.00	-35.76	263.53
4	5	4.40	0.00	-15.15	327.99
5	5	4.40	0.00	-16.15	327.90
5	6	5.50	0.00	5.21	376.73
6	6	5.50	0.00	4.08	377.84
6	7	6.60	0.00	26.12	408.83
7	7	6.60	0.00	24.82	410.97
7	8	7.70	0.00	48.37	462.78
8	8	7.70	0.00	47.01	472.75
8	9	8.80	0.00	78.97	844.72
9	9	8.80	0.00	77.01	864.65
9	10	9.90	0.00	114.31	808.60
10	10	9.90	0.00	112.98	850.54
10	11	11.00	0.00	151.46	786.24
11	11	11.00	0.00	151.00	854.65
11	12	12.10	0.00	191.59	808.09
12	12	12.10	0.00	192.37	825.33
12	13	13.20	0.00	233.42	630.24
13	13	13.20	0.00	234.09	634.48
13	14	14.30	0.00	275.96	414.45
14	14	14.30	30.73	266.84	420.40
14	15	15.40	35.44	309.22	136.28
15	15	15.40	0.00	320.77	137.27
15	16	16.50	0.00	363.30	-195.95
16	16	16.50	0.00	364.08	-119.19
16	17	17.60	0.00	407.07	-510.50
17	17	17.60	-0.01	408.04	-485.25
17	18	18.70	-0.01	452.13	-931.64
18	18	18.70	0.00	452.96	-927.15
18	19	19.80	0.00	497.40	-1430.25
19	19	19.80	0.00	498.04	-1423.98
19	20	20.90	0.00	542.80	-1983.00
20	20	20.90	0.00	543.12	-1980.49
20	21	22.00	0.00	595.57	-2599.22
21	1021	22.00	0.00	-187.62	-395.02
21	22	23.40	0.00	-157.69	-144.69
22	22	23.40	0.00	-158.77	-138.24
22	23	24.80	0.00	-135.11	85.92
23	23	24.80	0.00	-136.63	85.31
23	24	26.20	0.00	-112.26	288.31
24	24	26.20	0.00	-114.09	287.85
24	25	27.60	0.00	-88.90	467.91
25	25	27.60	0.00	-91.10	470.02
25	26	29.00	0.00	-64.91	634.19
26	26	29.00	18.83	-62.49	636.86



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-93.03	-0.04
1	2	1.10	0.00	-72.72	97.48
2	2	1.10	0.00	-73.21	97.42
2	3	2.20	0.00	-54.12	185.04
3	3	2.20	0.00	-54.81	184.98
3	4	3.30	0.00	-34.94	262.71
4	4	3.30	0.00	-35.76	263.53
4	5	4.40	0.00	-15.15	327.99
5	5	4.40	0.00	-16.15	327.90
5	6	5.50	0.00	5.21	376.73
6	6	5.50	0.00	4.08	377.84
6	7	6.60	0.00	26.12	408.83
7	7	6.60	0.00	24.82	410.97
7	8	7.70	0.00	48.37	462.78
8	8	7.70	0.00	47.01	472.75
8	9	8.80	0.00	78.97	844.72
9	9	8.80	0.00	77.01	864.65
9	10	9.90	0.00	114.31	808.60
10	10	9.90	0.00	112.98	850.54
10	11	11.00	0.00	151.46	786.24
11	11	11.00	0.00	151.00	854.65
11	12	12.10	0.00	191.59	808.09
12	12	12.10	0.00	192.37	825.33
12	13	13.20	0.00	233.42	630.24
13	13	13.20	0.00	234.09	634.48
13	14	14.30	0.00	275.96	414.45
14	14	14.30	30.73	266.84	420.40
14	15	15.40	35.44	309.22	136.28
15	15	15.40	0.00	320.77	137.27
15	16	16.50	0.00	363.30	-195.95
16	16	16.50	0.00	364.08	-119.19
16	17	17.60	0.00	407.07	-510.50
17	17	17.60	-0.01	408.04	-485.25
17	18	18.70	-0.01	452.13	-931.64
18	18	18.70	0.00	452.96	-927.15
18	19	19.80	0.00	497.40	-1430.25
19	19	19.80	0.00	498.04	-1423.98
19	20	20.90	0.00	542.80	-1983.00
20	20	20.90	0.00	543.12	-1980.49
20	21	22.00	0.00	595.57	-2599.22
21	1021	22.00	0.00	-187.62	-395.02
21	22	23.40	0.00	-157.69	-144.69
22	22	23.40	0.00	-158.77	-138.24
22	23	24.80	0.00	-135.11	85.92
23	23	24.80	0.00	-136.63	85.31
23	24	26.20	0.00	-112.26	288.31
24	24	26.20	0.00	-114.09	287.85
24	25	27.60	0.00	-88.90	467.91
25	25	27.60	0.00	-91.10	470.02
25	26	29.00	0.00	-64.91	634.19
26	26	29.00	18.83	-62.49	636.86

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	15.34	-35.71	764.69
27	27	30.40	0.00	-42.15	797.62
27	28	31.80	0.00	-14.39	926.81
28	28	31.80	0.00	-16.60	919.30
28	29	33.20	0.00	12.68	1027.43
29	29	33.20	0.00	10.00	1036.21
29	30	34.60	0.00	40.30	1078.46
30	30	34.60	0.00	38.22	1135.62
30	31	36.00	0.00	72.11	1441.02
31	31	36.00	0.00	71.05	1458.42
31	32	37.40	0.00	118.99	1607.53
32	32	37.40	0.00	119.41	1714.26
32	33	38.80	0.00	169.37	1593.81
33	33	38.80	0.00	171.23	1617.77
33	34	40.20	0.00	222.05	1420.69
34	34	40.20	0.00	223.65	1422.12
34	35	41.60	0.00	275.75	1144.77
35	35	41.60	13.15	273.48	1163.71
35	36	43.00	17.86	326.75	792.15
36	36	43.00	0.00	332.78	851.26
36	37	44.40	0.00	386.77	394.83
37	37	44.40	0.00	388.50	415.61
37	38	45.80	0.00	443.41	-115.70
38	38	45.80	0.00	444.89	-104.24
38	39	47.20	0.00	500.67	-736.34
39	39	47.20	0.00	501.77	-733.01
39	40	48.60	0.00	558.20	-1455.31
40	40	48.60	0.00	558.79	-1448.91
40	41	50.00	0.00	625.38	-2255.67
41	1041	50.00	0.00	-186.51	-753.21
41	42	51.40	0.00	-156.58	-504.40
42	42	51.40	0.00	-158.21	-497.57
42	43	52.80	0.00	-134.57	-273.96
43	43	52.80	0.00	-136.57	-270.43
43	44	54.20	0.00	-112.18	-67.07
44	44	54.20	0.00	-114.49	-55.40
44	45	55.60	0.00	-89.28	125.68
45	45	55.60	0.00	-91.70	146.48
45	46	57.00	0.00	-65.66	303.15
46	46	57.00	12.64	-64.48	361.43
46	47	58.40	9.15	-37.65	490.26
47	47	58.40	0.00	-41.67	509.41
47	48	59.80	0.00	-14.05	607.45
48	48	59.80	0.00	-15.96	607.64
48	49	61.20	0.00	13.68	709.75
49	49	61.20	0.00	11.20	729.82
49	50	62.60	0.00	42.11	774.88
50	50	62.60	0.00	40.47	837.79
50	51	64.00	0.00	72.95	902.59
51	51	64.00	0.00	72.44	959.38
51	52	65.40	0.00	120.40	1340.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	121.86	1400.81
52	53	66.80	0.00	171.94	1276.86
53	53	66.80	0.00	173.99	1286.78
53	54	68.20	0.00	224.92	1085.53
54	54	68.20	0.00	226.63	1108.73
54	55	69.60	0.00	278.93	827.68
55	55	69.60	19.91	275.77	861.27
55	56	71.00	24.63	329.05	484.05
56	56	71.00	0.00	337.17	486.66
56	57	72.40	0.00	391.02	43.57
57	57	72.40	0.00	392.47	45.48
57	58	73.80	0.00	447.51	-503.57
58	58	73.80	0.00	448.54	-504.22
58	59	75.20	0.00	504.25	-1141.14
59	59	75.20	0.00	504.87	-1141.98
59	60	76.60	0.00	561.22	-1867.94
60	60	76.60	0.00	561.33	-1861.69
60	61	78.00	0.00	628.01	-2673.84
61	1061	78.00	0.00	-185.92	-481.48
61	62	79.10	0.00	-162.42	-283.89
62	62	79.10	0.00	-163.70	-281.38
62	63	80.20	0.00	-145.28	-98.98
63	63	80.20	0.00	-146.84	-90.99
63	64	81.30	0.00	-127.97	78.82
64	64	81.30	0.00	-129.73	83.39
64	65	82.40	0.00	-110.40	241.02
65	65	82.40	0.00	-112.06	288.27
65	66	83.50	0.00	-92.23	432.09
66	66	83.50	0.00	-93.61	504.75
66	67	84.60	0.00	-73.01	637.52
67	67	84.60	27.73	-65.30	638.78
67	68	85.70	24.24	-44.46	749.74
68	68	85.70	0.00	-53.22	754.01
68	69	86.80	0.00	-31.83	836.85
69	69	86.80	0.00	-33.05	847.55
69	70	87.90	0.00	-9.85	925.72
70	70	87.90	0.00	-11.37	939.10
70	71	89.00	0.00	12.75	1071.69
71	71	89.00	0.00	11.91	1114.83
71	72	90.10	0.00	36.78	1218.79
72	72	90.10	0.00	36.51	1260.69
72	73	91.20	0.00	64.47	1263.59
73	73	91.20	0.00	65.21	1299.84
73	74	92.30	0.00	97.48	1562.85
74	74	92.30	0.00	98.35	1572.84
74	75	93.40	0.00	137.73	1541.85
75	75	93.40	0.00	138.46	1543.93
75	76	94.50	0.00	179.46	1421.62
76	76	94.50	0.00	180.03	1423.17
76	77	95.60	0.00	221.86	1247.79
77	77	95.60	0.00	222.21	1247.53

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	264.61	1025.35
78	78	96.70	0.00	264.82	1026.05
78	79	97.80	0.00	307.72	745.83
79	79	97.80	0.00	307.66	745.64
79	80	98.90	0.00	351.37	404.70
80	80	98.90	0.00	351.06	404.47
80	81	100.00	0.00	398.15	0.13
101	101	0.00	0.00	-86.43	0.13
101	102	1.10	0.00	-67.03	92.49
102	102	1.10	0.00	-67.64	92.77
102	103	2.20	0.00	-49.20	179.13
103	103	2.20	0.00	-49.80	179.35
103	104	3.30	0.00	-30.33	258.72
104	104	3.30	0.00	-30.83	259.95
104	105	4.40	0.00	-10.40	327.96
105	105	4.40	0.00	-10.92	328.07
105	106	5.50	0.00	10.49	381.51
106	106	5.50	0.00	9.91	382.14
106	107	6.60	0.00	32.21	418.04
107	107	6.60	0.00	31.54	420.28
107	108	7.70	0.00	55.55	476.65
108	108	7.70	0.00	54.97	495.81
108	109	8.80	0.00	87.30	871.24
109	109	8.80	0.00	86.41	905.56
109	110	9.90	0.00	124.17	849.20
110	110	9.90	0.00	124.08	886.48
110	111	11.00	0.00	163.30	828.48
111	111	11.00	0.00	164.39	907.06
111	112	12.10	0.00	205.93	857.71
112	112	12.10	0.00	207.84	861.12
112	113	13.20	0.00	250.15	658.49
113	113	13.20	0.00	252.00	659.44
113	114	14.30	0.00	295.03	432.39
114	114	14.30	30.73	287.15	432.91
114	115	15.40	35.44	330.93	135.42
115	115	15.40	0.00	343.73	137.00
115	116	16.50	0.00	387.77	-213.93
116	116	16.50	0.00	389.41	-211.26
116	117	17.60	0.00	434.20	-624.47
117	117	17.60	0.00	435.83	-621.99
117	118	18.70	0.00	481.76	-1094.66
118	118	18.70	0.00	483.42	-1089.80
118	119	19.80	0.00	529.81	-1623.90
119	119	19.80	0.00	531.64	-1581.95
119	120	20.90	0.00	578.45	-2177.22
120	120	20.90	0.00	580.28	-2167.37
120	121	22.00	0.00	634.90	-2828.01
121	1121	22.00	0.00	-181.10	-335.15
121	122	23.40	0.00	-152.26	-93.15
122	122	23.40	0.00	-153.18	-93.32
122	123	24.80	0.00	-130.43	126.54

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-131.53	126.35
123	124	26.20	0.00	-107.81	328.28
124	124	26.20	0.00	-109.12	334.05
124	125	27.60	0.00	-84.34	515.32
125	125	27.60	0.00	-85.76	519.37
125	126	29.00	0.00	-59.78	686.22
126	126	29.00	18.83	-56.32	717.60
126	127	30.40	15.34	-29.53	848.54
127	127	30.40	0.00	-34.83	848.71
127	128	31.80	0.00	-7.05	949.81
128	128	31.80	0.00	-8.61	950.12
128	129	33.20	0.00	21.00	1071.64
129	129	33.20	0.00	18.83	1077.10
129	130	34.60	0.00	50.02	1124.08
130	130	34.60	0.00	48.59	1182.02
130	131	36.00	0.00	83.92	1467.52
131	131	36.00	0.00	83.36	1474.43
131	132	37.40	0.00	131.81	1635.36
132	132	37.40	0.00	132.82	1727.66
132	133	38.80	0.00	183.54	1606.52
133	133	38.80	0.00	186.04	1637.84
133	134	40.20	0.00	237.87	1437.09
134	134	40.20	0.00	240.29	1438.80
134	135	41.60	0.00	293.83	1153.67
135	135	41.60	13.15	292.60	1155.72
135	136	43.00	17.86	347.47	768.19
136	136	43.00	0.00	354.12	770.52
136	137	44.40	0.00	409.88	293.12
137	137	44.40	0.00	412.04	324.38
137	138	45.80	0.00	469.01	-230.36
138	138	45.80	0.00	471.45	-193.49
138	139	47.20	0.00	529.51	-858.76
139	139	47.20	0.00	532.04	-844.68
139	140	48.60	0.00	590.95	-1608.09
140	140	48.60	0.00	593.45	-1602.20
140	141	50.00	0.00	662.74	-2455.96
141	1141	50.00	-0.01	-179.51	-680.16
141	142	51.40	-0.01	-150.68	-440.30
142	142	51.40	0.00	-152.07	-434.35
142	143	52.80	0.00	-129.31	-215.68
143	143	52.80	0.00	-130.83	-201.73
143	144	54.20	0.00	-107.06	-0.40
144	144	54.20	0.00	-108.55	36.31
144	145	55.60	0.00	-83.74	217.33
145	145	55.60	0.00	-84.94	248.34
145	146	57.00	0.00	-59.09	405.84
146	146	57.00	12.64	-57.14	407.28
146	147	58.40	9.15	-30.29	537.72
147	147	58.40	0.00	-34.05	539.62
147	148	59.80	0.00	-6.22	640.14
148	148	59.80	0.00	-7.83	640.51

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	22.23	754.92
149	149	61.20	0.00	20.16	782.61
149	150	62.60	0.00	52.06	833.28
150	150	62.60	0.00	50.97	885.51
150	151	64.00	0.00	84.60	965.11
151	151	64.00	0.00	84.64	1009.99
151	152	65.40	0.00	133.14	1367.05
152	152	65.40	0.00	134.93	1426.50
152	153	66.80	0.00	185.82	1302.31
153	153	66.80	0.00	188.41	1308.97
153	154	68.20	0.00	240.39	1104.46
154	154	68.20	0.00	242.76	1104.85
154	155	69.60	0.00	296.55	816.94
155	155	69.60	19.91	293.52	817.23
155	156	71.00	24.63	348.39	425.88
156	156	71.00	0.00	356.90	458.18
156	157	72.40	0.00	412.56	-1.01
157	157	72.40	0.00	414.78	3.24
157	158	73.80	0.00	471.92	-570.50
158	158	73.80	0.00	474.12	-564.57
158	159	75.20	0.00	532.15	-1233.26
159	159	75.20	0.00	534.29	-1233.34
159	160	76.60	0.00	593.15	-1999.17
160	160	76.60	0.00	595.14	-1999.33
160	161	78.00	0.00	664.53	-2857.73
161	1161	78.00	0.00	-178.43	-364.40
161	162	79.10	0.00	-155.84	-174.70
162	162	79.10	0.00	-156.84	-164.06
162	163	80.20	0.00	-139.20	12.89
163	163	80.20	0.00	-140.20	55.35
163	164	81.30	0.00	-121.97	221.65
164	164	81.30	0.00	-122.82	226.87
164	165	82.40	0.00	-103.99	382.39
165	165	82.40	0.00	-104.93	384.74
165	166	83.50	0.00	-85.46	527.62
166	166	83.50	0.00	-86.45	530.53
166	167	84.60	0.00	-66.06	663.69
167	167	84.60	27.73	-58.42	665.40
167	168	85.70	24.24	-37.68	778.23
168	168	85.70	0.00	-46.52	778.63
168	169	86.80	0.00	-25.12	874.17
169	169	86.80	0.00	-26.44	875.14
169	170	87.90	0.00	-3.23	961.21
170	170	87.90	0.00	-4.79	961.27
170	171	89.00	0.00	19.99	1102.17
171	171	89.00	0.00	18.83	1150.93
171	172	90.10	0.00	44.13	1274.41
172	172	90.10	0.00	43.65	1240.15
172	173	91.20	0.00	72.82	1319.51
173	173	91.20	0.00	73.48	1372.37
173	174	92.30	0.00	106.80	1611.37

CÁLCULO TENSIONAL

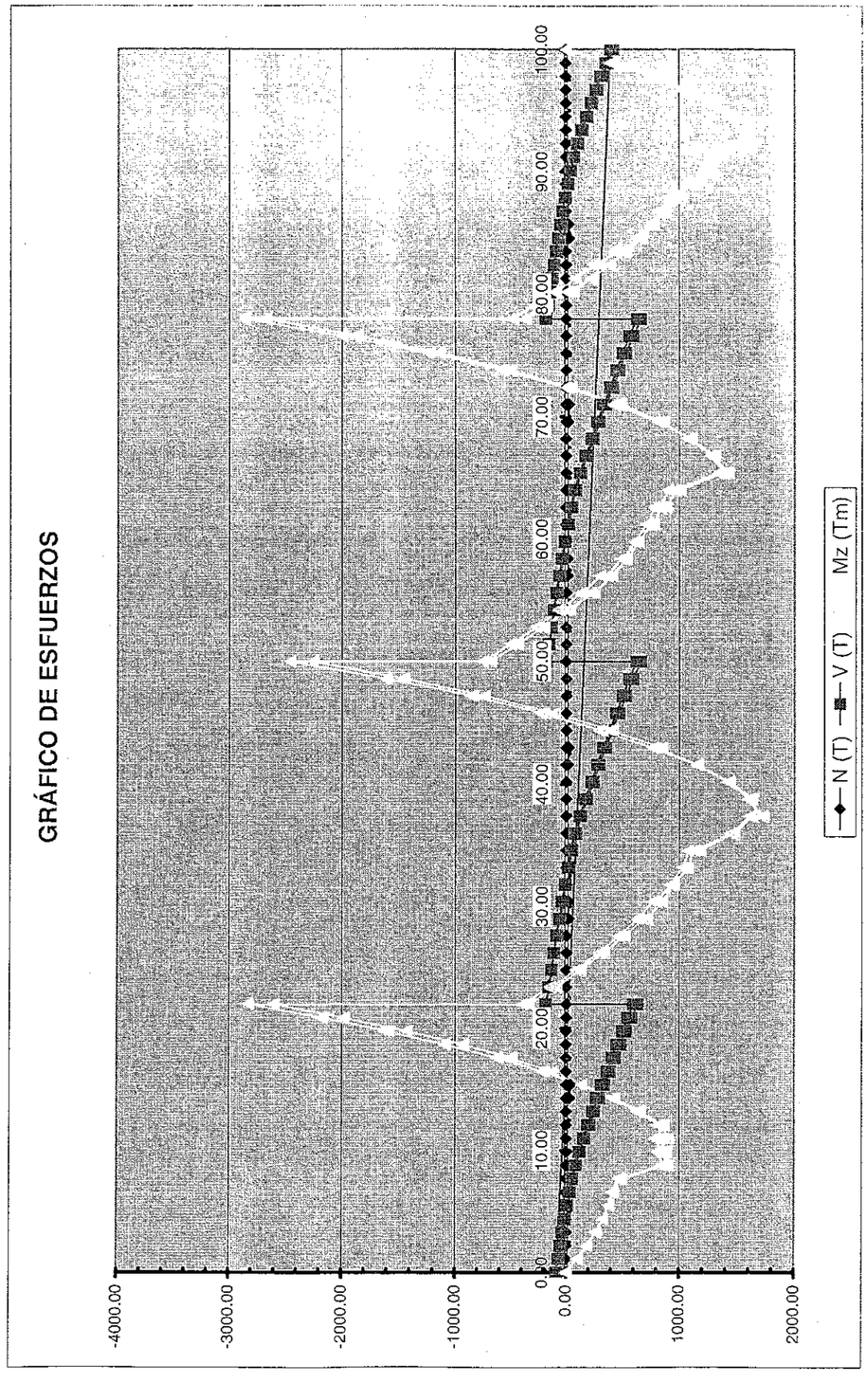
Hipótesis de cálculo:
INFRECG.T0.VY+

C. Totales dominante Gradinete VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	107.92	1630.24
174	175	93.40	0.00	148.10	1602.22
175	175	93.40	0.00	149.34	1606.38
175	176	94.50	0.00	191.37	1484.33
176	176	94.50	0.00	192.57	1485.04
176	177	95.60	0.00	235.68	1306.38
177	177	95.60	0.00	236.89	1306.64
177	178	96.70	0.00	280.57	1077.46
178	178	96.70	0.00	281.85	1078.85
178	179	97.80	0.00	326.40	787.44
179	179	97.80	0.00	327.79	787.87
179	180	98.90	0.00	373.48	429.24
180	180	98.90	0.00	374.96	429.72
180	181	100.00	0.00	424.35	-0.24



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-398.17	0.13
1	2	1.10	0.00	-351.09	404.47
2	2	1.10	0.00	-351.40	404.71
2	3	2.20	0.00	-307.67	745.67
3	3	2.20	0.00	-307.74	745.87
3	4	3.30	0.00	-264.84	1026.02
4	4	3.30	0.00	-264.62	1025.37
4	5	4.40	0.00	-222.24	1247.51
5	5	4.40	0.00	-221.87	1247.76
5	6	5.50	0.00	-180.04	1423.16
6	6	5.50	0.00	-179.47	1421.58
6	7	6.60	0.00	-138.48	1543.86
7	7	6.60	0.00	-137.77	1541.84
7	8	7.70	0.00	-98.39	1572.82
8	8	7.70	0.00	-97.48	1569.07
8	9	8.80	0.00	-64.41	1340.55
9	9	8.80	0.00	-63.71	1304.32
9	10	9.90	0.00	-34.30	1299.82
10	10	9.90	0.00	-34.66	1257.91
10	11	11.00	0.00	-8.34	1150.85
11	11	11.00	0.00	-9.27	1107.71
11	12	12.10	0.00	16.27	970.48
12	12	12.10	0.00	14.68	957.08
12	13	13.20	0.00	39.32	872.74
13	13	13.20	0.00	38.03	862.02
13	14	14.30	0.00	60.84	771.56
14	14	14.30	24.24	52.02	767.26
14	15	15.40	27.73	74.28	647.21
15	15	15.40	0.00	81.88	645.94
15	16	16.50	0.00	103.91	502.62
16	16	16.50	0.00	102.45	429.93
16	17	17.60	0.00	123.70	274.10
17	17	17.60	-0.01	121.92	226.82
17	18	18.70	-0.01	142.67	55.69
18	18	18.70	0.00	140.79	51.10
18	19	19.80	0.00	159.94	-137.20
19	19	19.80	0.00	159.40	-141.64
19	20	20.90	0.00	176.83	-322.39
20	20	20.90	0.00	176.73	-322.39
20	21	22.00	0.00	199.22	-529.16
21	1021	22.00	0.00	-628.01	-2673.81
21	22	23.40	0.00	-561.33	-1861.66
22	22	23.40	0.00	-561.24	-1867.94
22	23	24.80	0.00	-504.86	-1141.96
23	23	24.80	0.00	-504.25	-1141.10
23	24	26.20	0.00	-448.54	-504.23
24	24	26.20	0.00	-447.47	-503.57
24	25	27.60	0.00	-392.41	45.44
25	25	27.60	0.00	-391.02	43.54
25	26	29.00	0.00	-337.17	486.65
26	26	29.00	24.63	-329.04	484.01

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	19.91	-275.76	861.23
27	27	30.40	0.00	-278.93	827.64
27	28	31.80	0.00	-226.63	1108.71
28	28	31.80	0.00	-224.92	1085.48
28	29	33.20	0.00	-173.97	1286.74
29	29	33.20	0.00	-171.94	1276.86
29	30	34.60	0.00	-121.86	1400.82
30	30	34.60	0.00	-120.40	1340.25
30	31	36.00	0.00	-72.12	993.47
31	31	36.00	0.00	-72.70	910.51
31	32	37.40	0.00	-38.49	878.29
32	32	37.40	0.00	-40.21	815.36
32	33	38.80	0.00	-7.47	766.37
33	33	38.80	0.00	-10.04	746.27
33	34	40.20	0.00	21.44	637.73
34	34	40.20	0.00	19.45	637.53
34	35	41.60	0.00	48.89	530.72
35	35	41.60	9.15	44.76	511.50
35	36	43.00	12.64	73.41	371.41
36	36	43.00	0.00	74.47	313.12
36	37	44.40	0.00	102.34	142.82
37	37	44.40	0.00	99.78	121.94
37	38	45.80	0.00	126.82	-75.08
38	38	45.80	0.00	124.35	-86.76
38	39	47.20	0.00	150.57	-308.47
39	39	47.20	0.00	148.40	-312.04
39	40	48.60	0.00	173.86	-556.28
40	40	48.60	0.00	172.05	-563.13
40	41	50.00	0.00	203.81	-834.86
41	1041	50.00	0.00	-625.38	-2255.68
41	42	51.40	0.00	-558.79	-1448.92
42	42	51.40	0.00	-558.20	-1455.31
42	43	52.80	0.00	-501.77	-733.01
43	43	52.80	0.00	-500.67	-736.33
43	44	54.20	0.00	-444.89	-104.25
44	44	54.20	0.00	-443.43	-115.71
44	45	55.60	0.00	-388.50	415.64
45	45	55.60	0.00	-386.77	394.83
45	46	57.00	0.00	-332.78	851.28
46	46	57.00	17.86	-326.76	792.19
46	47	58.40	13.15	-273.49	1163.74
47	47	58.40	0.00	-275.75	1144.78
47	48	59.80	0.00	-223.65	1422.17
48	48	59.80	0.00	-222.06	1420.74
48	49	61.20	0.00	-171.23	1617.80
49	49	61.20	0.00	-169.37	1593.83
49	50	62.60	0.00	-119.41	1714.32
50	50	62.60	0.00	-118.98	1607.57
50	51	64.00	0.00	-70.94	1492.54
51	51	64.00	0.00	-72.01	1448.93
51	52	65.40	0.00	-36.62	1176.64

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	-38.76	1119.46
52	53	66.80	0.00	-6.65	1073.81
53	53	66.80	0.00	-9.37	1064.99
53	54	68.20	0.00	21.71	950.98
54	54	68.20	0.00	19.41	958.46
54	55	69.60	0.00	49.00	820.94
55	55	69.60	15.34	42.47	787.97
55	56	71.00	18.83	71.08	649.37
56	56	71.00	0.00	73.38	646.67
56	57	72.40	0.00	101.38	469.36
57	57	72.40	0.00	99.07	467.22
57	58	73.80	0.00	126.09	271.68
58	58	73.80	0.00	124.08	272.08
58	59	75.20	0.00	150.28	51.25
59	59	75.20	0.00	148.60	51.85
59	60	76.60	0.00	174.07	-192.47
60	60	76.60	0.00	172.82	-198.96
60	61	78.00	0.00	204.57	-471.72
61	1061	78.00	0.00	-595.60	-2599.27
61	62	79.10	0.00	-543.13	-1980.52
62	62	79.10	0.00	-542.82	-1983.05
62	63	80.20	0.00	-498.06	-1424.00
63	63	80.20	0.00	-497.42	-1430.28
63	64	81.30	0.00	-452.98	-927.16
64	64	81.30	0.00	-452.13	-931.62
64	65	82.40	0.00	-408.04	-485.25
65	65	82.40	0.00	-407.07	-510.49
65	66	83.50	0.00	-364.09	-119.18
66	66	83.50	0.00	-363.33	-195.96
66	67	84.60	0.00	-320.79	137.25
67	67	84.60	35.44	-309.21	136.28
67	68	85.70	30.73	-266.83	420.42
68	68	85.70	0.00	-275.99	414.47
68	69	86.80	0.00	-234.11	634.49
69	69	86.80	0.00	-233.43	630.23
69	70	87.90	0.00	-192.38	825.32
70	70	87.90	0.00	-191.61	808.08
70	71	89.00	0.00	-151.01	854.65
71	71	89.00	0.00	-151.47	786.24
71	72	90.10	0.00	-112.99	850.56
72	72	90.10	0.00	-114.32	808.62
72	73	91.20	0.00	-77.02	864.64
73	73	91.20	0.00	-78.98	844.74
73	74	92.30	0.00	-46.39	507.36
74	74	92.30	0.00	-47.84	503.63
74	75	93.40	0.00	-22.86	450.45
75	75	93.40	0.00	-24.25	448.29
75	76	94.50	0.00	-0.77	414.44
76	76	94.50	0.00	-1.98	413.33
76	77	95.60	0.00	20.82	360.13
77	77	95.60	0.00	19.72	360.19

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	41.77	289.87
78	78	96.70	0.00	40.84	288.99
78	79	97.80	0.00	62.15	203.99
79	79	97.80	0.00	61.34	204.02
79	80	98.90	0.00	81.87	107.66
80	80	98.90	0.00	81.25	107.68
80	81	100.00	0.00	102.99	-0.02
101	101	0.00	0.00	-424.37	-0.24
101	102	1.10	0.00	-374.98	429.70
102	102	1.10	0.00	-373.51	429.23
102	103	2.20	0.00	-327.83	787.89
103	103	2.20	0.00	-326.43	787.48
103	104	3.30	0.00	-281.89	1078.85
104	104	3.30	0.00	-280.57	1077.47
104	105	4.40	0.00	-236.91	1306.64
105	105	4.40	0.00	-235.70	1306.35
105	106	5.50	0.00	-192.58	1485.01
106	106	5.50	0.00	-191.39	1484.30
106	107	6.60	0.00	-149.37	1606.37
107	107	6.60	0.00	-148.12	1602.22
107	108	7.70	0.00	-107.94	1630.24
108	108	7.70	0.00	-106.81	1620.01
108	109	8.80	0.00	-72.52	1426.93
109	109	8.80	0.00	-71.78	1374.10
109	110	9.90	0.00	-40.85	1292.60
110	110	9.90	0.00	-41.26	1326.84
110	111	11.00	0.00	-14.25	1199.27
111	111	11.00	0.00	-15.33	1150.54
111	112	12.10	0.00	11.18	1003.49
112	112	12.10	0.00	9.71	1003.48
112	113	13.20	0.00	34.65	909.32
113	113	13.20	0.00	33.40	908.34
113	114	14.30	0.00	56.55	802.70
114	114	14.30	24.24	47.82	802.36
114	115	15.40	27.73	70.30	677.42
115	115	15.40	0.00	78.00	675.73
115	116	16.50	0.00	100.13	528.48
116	116	16.50	0.00	99.26	525.57
116	117	17.60	0.00	118.80	185.76
117	117	17.60	0.00	118.35	185.66
117	118	18.70	0.00	134.70	45.55
118	118	18.70	0.00	134.21	45.47
118	119	19.80	0.00	150.56	-111.13
119	119	19.80	0.00	150.02	-111.22
119	120	20.90	0.00	166.37	-285.23
120	120	20.90	0.00	165.81	-285.27
120	121	22.00	0.00	187.66	-479.68
121	1121	22.00	0.00	-664.54	-2857.67
121	122	23.40	0.00	-595.14	-1999.29
122	122	23.40	0.00	-593.15	-1999.12
122	123	24.80	0.00	-534.29	-1233.31

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-532.14	-1233.23
123	124	26.20	0.00	-474.12	-564.55
124	124	26.20	0.00	-471.92	-570.50
124	125	27.60	0.00	-414.77	3.22
125	125	27.60	0.00	-412.54	-1.03
125	126	29.00	0.00	-356.90	458.13
126	126	29.00	24.63	-348.37	425.86
126	127	30.40	19.91	-293.51	817.17
127	127	30.40	0.00	-296.55	816.90
127	128	31.80	0.00	-242.76	1104.80
128	128	31.80	0.00	-240.39	1104.43
128	129	33.20	0.00	-188.41	1308.93
129	129	33.20	0.00	-185.83	1302.30
129	130	34.60	0.00	-134.93	1426.46
130	130	34.60	0.00	-133.15	1367.07
130	131	36.00	0.00	-84.34	1055.20
131	131	36.00	0.00	-84.33	974.89
131	132	37.40	0.00	-48.52	938.60
132	132	37.40	0.00	-49.54	886.37
132	133	38.80	0.00	-15.44	830.66
133	133	38.80	0.00	-17.44	803.01
133	134	40.20	0.00	14.83	680.36
134	134	40.20	0.00	13.32	679.99
134	135	41.60	0.00	43.35	567.99
135	135	41.60	9.15	39.69	566.15
135	136	43.00	12.64	68.74	420.99
136	136	43.00	0.00	70.83	419.59
136	137	44.40	0.00	98.87	244.13
137	137	44.40	0.00	97.80	213.16
137	138	45.80	0.00	124.81	10.88
138	138	45.80	0.00	123.49	-25.78
138	139	47.20	0.00	149.47	-251.67
139	139	47.20	0.00	148.14	-265.61
139	140	48.60	0.00	173.11	-512.14
140	140	48.60	0.00	171.90	-518.08
140	141	50.00	0.00	202.94	-789.18
141	1141	50.00	-0.01	-662.74	-2455.98
141	142	51.40	-0.01	-593.46	-1602.20
142	142	51.40	0.00	-590.96	-1608.09
142	143	52.80	0.00	-532.04	-844.65
143	143	52.80	0.00	-529.55	-858.73
143	144	54.20	0.00	-471.45	-193.49
144	144	54.20	0.00	-469.02	-230.34
144	145	55.60	0.00	-412.05	324.42
145	145	55.60	0.00	-409.88	293.15
145	146	57.00	0.00	-354.12	770.58
146	146	57.00	17.86	-347.48	768.22
146	147	58.40	13.15	-292.63	1155.79
147	147	58.40	0.00	-293.84	1153.74
147	148	59.80	0.00	-240.29	1438.87
148	148	59.80	0.00	-237.87	1437.17

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-186.04	1637.93
149	149	61.20	0.00	-183.54	1606.60
149	150	62.60	0.00	-132.82	1727.74
150	150	62.60	0.00	-131.81	1635.42
150	151	64.00	0.00	-83.33	1519.70
151	151	64.00	0.00	-83.78	1477.37
151	152	65.40	0.00	-46.56	1235.73
152	152	65.40	0.00	-47.93	1177.78
152	153	66.80	0.00	-14.52	1126.34
153	153	66.80	0.00	-16.62	1120.88
153	154	68.20	0.00	15.19	991.66
154	154	68.20	0.00	13.73	991.36
154	155	69.60	0.00	43.71	879.39
155	155	69.60	15.34	38.51	879.27
155	156	71.00	18.83	67.51	734.19
156	156	71.00	0.00	71.10	702.84
156	157	72.40	0.00	99.29	518.62
157	157	72.40	0.00	98.00	514.62
157	158	73.80	0.00	124.98	312.67
158	158	73.80	0.00	123.81	306.92
158	159	75.20	0.00	149.73	81.06
159	159	75.20	0.00	148.81	81.26
159	160	76.60	0.00	173.77	-165.89
160	160	76.60	0.00	173.02	-165.67
160	161	78.00	0.00	204.07	-438.31
161	1161	78.00	0.00	-634.90	-2828.07
161	162	79.10	0.00	-580.31	-2167.40
162	162	79.10	0.00	-578.48	-2177.26
162	163	80.20	0.00	-531.68	-1581.99
163	163	80.20	0.00	-529.81	-1623.94
163	164	81.30	0.00	-483.42	-1089.83
164	164	81.30	0.00	-481.78	-1094.67
164	165	82.40	0.00	-435.86	-621.99
165	165	82.40	0.00	-434.22	-624.47
165	166	83.50	0.00	-389.41	-211.28
166	166	83.50	0.00	-387.78	-213.96
166	167	84.60	0.00	-343.74	136.99
167	167	84.60	35.44	-330.92	135.43
167	168	85.70	30.73	-287.15	432.89
168	168	85.70	0.00	-295.04	432.36
168	169	86.80	0.00	-252.01	659.45
169	169	86.80	0.00	-250.16	658.47
169	170	87.90	0.00	-207.86	861.12
170	170	87.90	0.00	-205.92	857.71
170	171	89.00	0.00	-164.40	907.05
171	171	89.00	0.00	-163.31	828.47
171	172	90.10	0.00	-124.09	886.45
172	172	90.10	0.00	-124.18	849.18
172	173	91.20	0.00	-86.42	905.54
173	173	91.20	0.00	-87.33	871.22
173	174	92.30	0.00	-54.23	541.88

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECG.T0.VY-

C. Totales dominante Gradinete VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

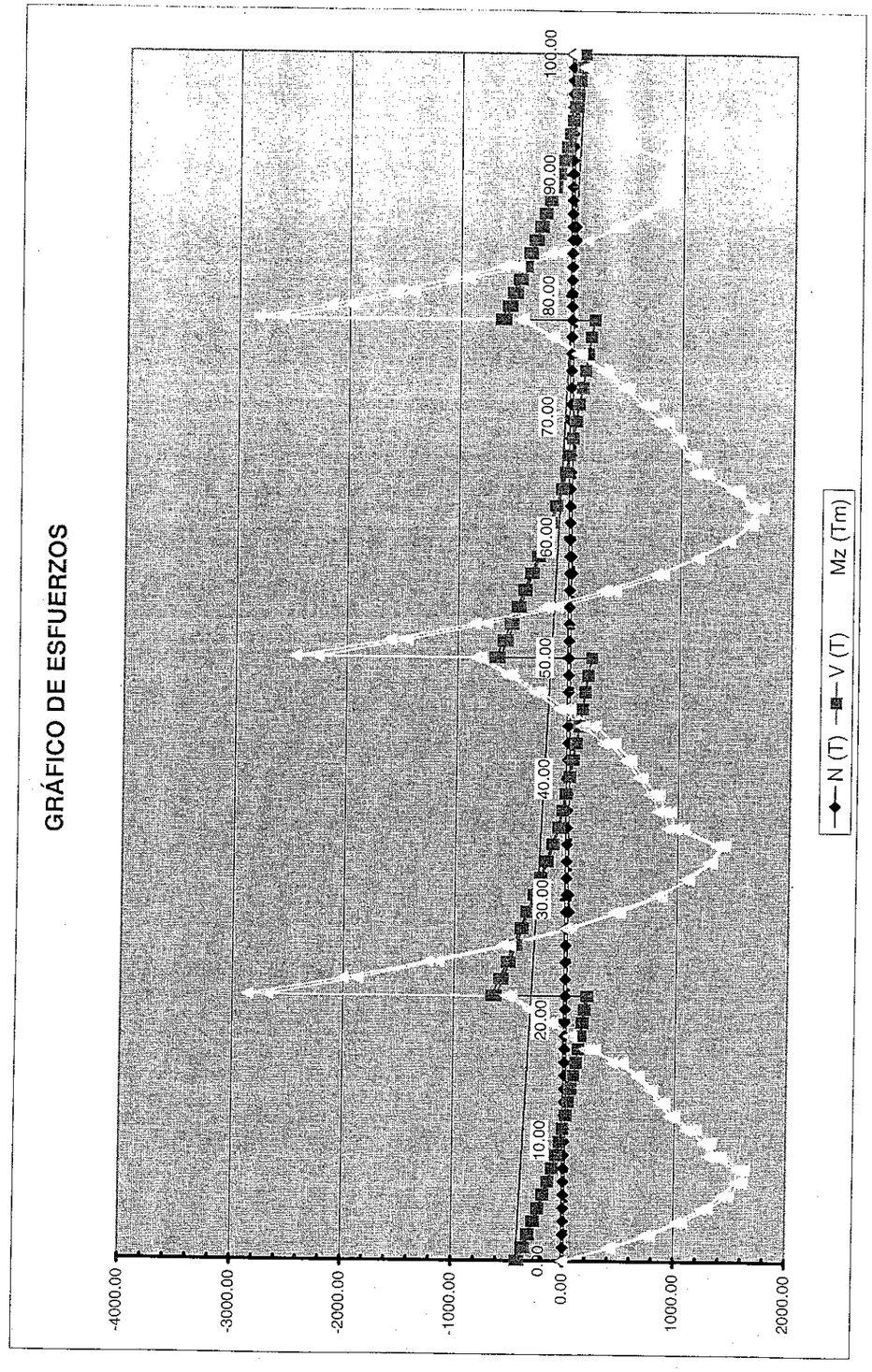
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-54.76	531.35
174	175	93.40	0.00	-29.03	473.17
175	175	93.40	0.00	-29.61	470.96
175	176	94.50	0.00	-5.58	431.24
176	176	94.50	0.00	-6.09	430.63
176	177	95.60	0.00	17.06	371.38
177	177	95.60	0.00	16.62	371.30
177	178	96.70	0.00	38.81	295.45
178	178	96.70	0.00	38.38	294.26
178	179	97.80	0.00	59.57	205.06
179	179	97.80	0.00	59.11	204.85
179	180	98.90	0.00	79.29	106.66
180	180	98.90	0.00	78.81	106.40
180	181	100.00	0.00	99.96	0.12

05/09/03

Programa DINTEL PACADAR S.A.
INFRECG.T0.VY-

GRÁFICO DE ESFUERZOS



Cortante.xls

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-105.44	-0.04
1	2	1.10	0.00	-86.68	113.56
2	2	1.10	-0.01	-87.34	113.51
2	3	2.20	-0.01	-67.65	220.74
3	3	2.20	0.00	-68.55	220.69
3	4	3.30	0.00	-47.93	320.21
4	4	3.30	0.00	-48.99	321.25
4	5	4.40	0.00	-27.43	408.89
5	5	4.40	0.00	-28.70	408.79
5	6	5.50	0.00	-6.21	481.50
6	6	5.50	0.00	-7.64	482.91
6	7	6.60	0.00	15.72	537.96
7	7	6.60	0.00	14.07	540.64
7	8	7.70	0.00	39.10	616.16
8	8	7.70	0.00	37.38	628.62
8	9	8.80	0.00	71.49	1056.50
9	9	8.80	-0.01	69.00	1081.40
9	10	9.90	-0.01	108.93	1045.02
10	10	9.90	0.00	107.22	1097.44
10	11	11.00	0.00	148.63	1058.15
11	11	11.00	0.00	148.00	1143.63
11	12	12.10	0.00	191.66	1112.35
12	12	12.10	0.00	192.58	1133.89
12	13	13.20	0.00	236.84	946.62
13	13	13.20	0.00	237.60	951.90
13	14	14.30	0.00	282.83	741.25
14	14	14.30	6.19	281.47	748.67
14	15	15.40	7.36	327.37	466.63
15	15	15.40	0.00	330.11	467.84
15	16	16.50	0.00	376.25	132.04
16	16	16.50	0.00	377.13	227.98
16	17	17.60	0.00	423.81	-171.56
17	17	17.60	0.00	424.90	-140.02
17	18	18.70	0.00	472.92	-600.43
18	18	18.70	0.00	473.84	-594.82
18	19	19.80	0.00	522.30	-1118.21
19	19	19.80	0.00	522.96	-1110.38
19	20	20.90	0.00	571.82	-1695.71
20	20	20.90	0.00	572.08	-1692.60
20	21	22.00	0.00	623.13	-2340.53
21	1021	22.00	0.00	-163.14	428.11
21	22	23.40	0.00	-139.90	650.99
22	22	23.40	0.00	-141.33	659.07
22	23	24.80	0.00	-117.11	863.01
23	23	24.80	0.00	-119.07	862.25
23	24	26.20	0.00	-93.92	1047.31
24	24	26.20	0.00	-96.28	1046.76
24	25	27.60	0.00	-70.13	1210.69
25	25	27.60	0.00	-72.92	1213.32
25	26	29.00	0.00	-45.57	1362.74
26	26	29.00	4.71	-48.18	1416.39

Cortante.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECUENTEST.Tinf.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.84	-20.04	1531.87
27	27	30.40	0.00	-23.66	1521.86
27	28	31.80	0.00	5.69	1646.45
28	28	31.80	0.00	2.91	1637.08
28	29	33.20	0.00	34.19	1742.81
29	29	33.20	0.00	30.81	1753.79
29	30	34.60	0.00	63.34	1784.73
30	30	34.60	0.00	60.74	1856.18
30	31	36.00	0.00	97.53	2159.63
31	31	36.00	0.00	96.16	2181.36
31	32	37.40	0.00	147.20	2321.69
32	32	37.40	0.00	147.71	2455.10
32	33	38.80	0.00	201.13	2313.01
33	33	38.80	0.00	203.42	2342.95
33	34	40.20	0.00	257.93	2117.79
34	34	40.20	0.00	259.86	2119.54
34	35	41.60	0.00	315.95	1806.73
35	35	41.60	3.28	316.41	1830.37
35	36	43.00	4.47	373.99	1413.44
36	36	43.00	0.00	376.84	1487.28
36	37	44.40	0.00	435.33	977.79
37	37	44.40	0.00	437.36	1003.73
37	38	45.80	0.00	496.97	413.49
38	38	45.80	0.00	498.67	427.77
38	39	47.20	0.00	559.39	-275.63
39	39	47.20	0.00	560.59	-271.52
39	40	48.60	0.00	622.12	-1074.80
40	40	48.60	0.00	622.66	-1066.81
40	41	50.00	0.00	688.73	-1895.23
41	1041	50.00	0.00	-177.82	-420.27
41	42	51.40	0.00	-154.05	-115.33
42	42	51.40	0.00	-156.15	-106.79
42	43	52.80	0.00	-131.96	118.21
43	43	52.80	0.00	-134.53	122.66
43	44	54.20	0.00	-109.39	329.96
44	44	54.20	0.00	-112.34	344.54
44	45	55.60	0.00	-86.19	531.56
45	45	55.60	0.00	-89.26	557.60
45	46	57.00	0.00	-62.06	721.67
46	46	57.00	3.75	-63.71	794.54
46	47	58.40	2.88	-35.53	931.98
47	47	58.40	0.00	-38.39	955.92
47	48	59.80	0.00	-9.23	1063.08
48	48	59.80	0.01	-11.64	1063.33
48	49	61.20	0.01	20.06	1183.08
49	49	61.20	0.00	16.94	1208.19
49	50	62.60	0.00	50.22	1264.13
50	50	62.60	0.00	48.14	1342.78
50	51	64.00	0.00	83.24	1424.52
51	51	64.00	0.00	82.60	1495.52
51	52	65.40	0.00	133.75	1889.45

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	135.52	1965.12
52	53	66.80	0.00	189.09	1840.03
53	53	66.80	0.00	191.58	1852.40
53	54	68.20	0.00	246.24	1643.42
54	54	68.20	0.00	248.31	1672.41
54	55	69.60	0.00	304.64	1376.36
55	55	69.60	4.39	305.34	1367.11
55	56	71.00	5.56	362.94	965.24
56	56	71.00	0.00	367.26	1018.77
56	57	72.40	0.00	425.57	544.84
57	57	72.40	0.00	427.27	547.17
57	58	73.80	0.00	487.03	-44.16
58	58	73.80	-0.01	488.19	-45.03
58	59	75.20	-0.01	548.82	-733.34
59	59	75.20	0.00	549.42	-734.43
59	60	76.60	0.00	610.80	-1521.18
60	60	76.60	0.00	610.75	-1513.40
60	61	78.00	0.00	677.45	-2389.65
61	1061	78.00	0.00	-139.90	364.16
61	62	79.10	0.00	-120.24	514.76
62	62	79.10	0.00	-121.89	517.90
62	63	80.20	0.00	-103.08	657.18
63	63	80.20	0.00	-105.08	667.18
63	64	81.30	0.00	-85.70	795.46
64	64	81.30	0.00	-87.95	801.19
64	65	82.40	0.00	-68.00	918.90
65	65	82.40	0.00	-70.12	977.97
65	66	83.50	0.00	-49.54	1083.13
66	66	83.50	0.00	-51.29	1173.98
66	67	84.60	0.00	-29.83	1268.92
67	67	84.60	6.93	-28.95	1270.51
67	68	85.70	6.06	-7.11	1344.59
68	68	85.70	0.01	-10.46	1349.92
68	69	86.80	0.01	12.05	1394.15
69	69	86.80	0.00	10.51	1407.54
69	70	87.90	0.00	35.32	1450.56
70	70	87.90	0.00	33.40	1467.30
70	71	89.00	0.00	59.32	1566.63
71	71	89.00	0.00	58.24	1620.56
71	72	90.10	0.00	84.73	1699.95
72	72	90.10	0.00	84.39	1752.29
72	73	91.20	0.00	114.74	1715.84
73	73	91.20	0.00	115.63	1761.15
73	74	92.30	0.00	150.51	1991.53
74	74	92.30	0.00	151.55	2004.01
74	75	93.40	0.00	193.89	1927.31
75	75	93.40	0.00	194.72	1929.91
75	76	94.50	0.00	238.88	1757.10
76	76	94.50	0.00	239.54	1759.00
76	77	95.60	0.00	284.72	1527.74
77	77	95.60	0.00	285.08	1527.40

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	330.98	1245.53
78	78	96.70	0.00	331.15	1246.37
78	79	97.80	0.00	377.65	899.89
79	79	97.80	0.01	377.48	899.61
79	80	98.90	0.01	425.04	485.13
80	80	98.90	0.00	424.52	484.81
80	81	100.00	0.00	474.18	0.18
101	101	0.00	0.00	-98.86	0.16
101	102	1.10	0.00	-81.08	109.06
102	102	1.10	-0.01	-81.79	109.40
102	103	2.20	-0.01	-62.74	216.52
103	103	2.20	0.00	-63.45	216.79
103	104	3.30	0.00	-43.16	319.54
104	104	3.30	0.00	-43.76	321.07
104	105	4.40	0.00	-22.24	414.07
105	105	4.40	0.00	-22.87	414.18
105	106	5.50	0.00	-0.14	493.35
106	106	5.50	0.00	-0.84	494.13
106	107	6.60	0.00	23.01	555.75
107	107	6.60	0.00	22.21	558.54
107	108	7.70	0.00	47.97	639.96
108	108	7.70	0.00	47.26	663.92
108	109	8.80	0.00	82.16	1105.83
109	109	8.80	0.00	81.10	1148.70
109	110	9.90	0.00	122.01	1111.35
110	110	9.90	0.00	121.94	1157.97
110	111	11.00	0.00	164.69	1125.37
111	111	11.00	0.00	166.12	1223.60
111	112	12.10	0.00	211.35	1187.13
112	112	12.10	0.00	213.79	1191.40
112	113	13.20	0.00	260.04	992.41
113	113	13.20	0.00	262.41	993.62
113	114	14.30	0.00	309.51	771.32
114	114	14.30	6.19	309.84	771.99
114	115	15.40	7.36	357.90	469.75
115	115	15.40	0.00	362.39	471.74
115	116	16.50	0.00	410.82	109.68
116	116	16.50	0.00	412.98	113.04
116	117	17.60	0.00	462.31	-318.64
117	117	17.60	0.00	464.45	-315.53
117	118	18.70	0.00	515.18	-814.31
118	118	18.70	0.00	517.38	-808.22
118	119	19.80	0.00	568.69	-1376.60
119	119	19.80	0.00	571.11	-1324.15
119	120	20.90	0.00	622.93	-1961.73
120	120	20.90	0.00	625.37	-1949.41
120	121	22.00	0.00	679.55	-2657.49
121	1121	22.00	0.00	-157.81	490.59
121	122	23.40	0.00	-135.72	706.89
122	122	23.40	0.00	-136.81	706.67
122	123	24.80	0.00	-113.52	908.56

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-114.85	908.31
123	124	26.20	0.00	-90.30	1094.89
124	124	26.20	0.00	-91.88	1102.09
124	125	27.60	0.00	-66.05	1269.93
125	125	27.60	0.00	-67.76	1274.96
125	126	29.00	0.00	-40.48	1429.70
126	126	29.00	4.70	-41.69	1519.21
126	127	30.40	3.83	-13.34	1640.14
127	127	30.40	0.00	-15.47	1589.14
127	128	31.80	0.00	14.10	1679.84
128	128	31.80	0.00	12.19	1680.22
128	129	33.20	0.00	44.08	1803.51
129	129	33.20	0.00	41.40	1810.34
129	130	34.60	0.00	75.24	1847.66
130	130	34.60	0.00	73.48	1920.07
130	131	36.00	0.00	112.27	2207.97
131	131	36.00	0.00	111.61	2216.61
131	132	37.40	0.00	163.84	2371.27
132	132	37.40	0.00	165.15	2486.66
132	133	38.80	0.00	220.05	2342.42
133	133	38.80	0.00	223.22	2381.59
133	134	40.20	0.00	279.53	2149.65
134	134	40.20	0.00	282.61	2151.82
134	135	41.60	0.00	341.04	1826.17
135	135	41.60	3.28	342.96	1828.79
135	136	43.00	4.47	403.05	1387.82
136	136	43.00	0.00	406.88	1390.78
136	137	44.40	0.00	468.10	850.01
137	137	44.40	0.01	470.92	889.14
137	138	45.80	0.01	533.64	263.45
138	138	45.80	0.00	536.83	309.58
138	139	47.20	0.00	600.90	-442.60
139	139	47.20	0.00	604.23	-424.97
139	140	48.60	0.00	669.38	-1288.12
140	140	48.60	0.00	672.69	-1280.72
140	141	50.00	0.00	742.63	-2177.66
141	1141	50.00	0.01	-171.93	-341.73
141	142	51.40	0.01	-149.33	-44.07
142	142	51.40	0.00	-151.02	-36.64
142	143	52.80	0.00	-127.70	185.52
143	143	52.80	0.00	-129.52	202.96
143	144	54.20	0.00	-104.96	410.62
144	144	54.20	0.00	-106.77	456.50
144	145	55.60	0.00	-80.92	645.90
145	145	55.60	0.00	-82.37	684.64
145	146	57.00	0.00	-55.20	851.79
146	146	57.00	3.75	-55.80	853.56
146	147	58.40	2.88	-27.39	994.63
147	147	58.40	0.00	-29.85	997.00
147	148	59.80	0.00	-0.22	1108.48
148	148	59.80	-0.01	-2.22	1108.93

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY+

C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-0.01	30.22	1244.92
149	149	61.20	0.00	27.66	1279.54
149	150	62.60	0.00	62.37	1343.02
150	150	62.60	0.00	61.05	1408.32
150	151	64.00	0.00	97.79	1508.74
151	151	64.00	0.00	97.84	1564.84
151	152	65.40	0.00	150.19	1937.78
152	152	65.40	0.00	152.48	2012.09
152	153	66.80	0.00	207.58	1885.47
153	153	66.80	0.00	210.87	1893.81
153	154	68.20	0.00	267.33	1678.67
154	154	68.20	0.00	270.36	1679.18
154	155	69.60	0.00	329.07	1371.56
155	155	69.60	4.39	330.10	1320.76
155	156	71.00	5.56	390.20	897.28
156	156	71.00	0.00	395.19	987.99
156	157	72.40	0.00	456.30	488.96
157	157	72.40	0.00	459.22	494.30
157	158	73.80	0.00	522.11	-133.91
158	158	73.80	0.00	525.03	-126.46
158	159	75.20	0.00	589.06	-861.69
159	159	75.20	0.00	591.90	-861.75
159	160	76.60	0.00	656.94	-1706.67
160	160	76.60	0.00	659.59	-1706.85
160	161	78.00	0.00	730.20	-2650.52
161	1161	78.00	0.00	-133.44	498.18
161	162	79.10	0.00	-114.74	641.97
162	162	79.10	0.01	-115.92	655.27
162	163	80.20	0.01	-97.92	790.54
163	163	80.20	0.01	-99.13	843.60
163	164	81.30	0.01	-80.38	969.99
164	164	81.30	0.00	-81.40	976.52
164	165	82.40	0.00	-61.91	1093.78
165	165	82.40	0.00	-63.04	1096.72
165	166	83.50	0.00	-42.74	1202.60
166	166	83.50	0.00	-43.92	1206.22
166	167	84.60	0.00	-22.56	1303.33
167	167	84.60	6.93	-21.69	1305.46
167	168	85.70	6.06	0.19	1383.27
168	168	85.70	0.00	-3.21	1383.78
168	169	86.80	0.00	19.49	1445.01
169	169	86.80	0.00	17.85	1446.22
169	170	87.90	0.00	42.84	1500.02
170	170	87.90	0.00	40.92	1500.08
170	171	89.00	0.00	67.82	1610.46
171	171	89.00	0.00	66.38	1671.42
171	172	90.10	0.00	93.59	1775.67
172	172	90.10	0.00	93.01	1732.84
172	173	91.20	0.00	125.04	1792.19
173	173	91.20	0.00	125.87	1858.26
173	174	92.30	0.00	162.32	2068.42

CÁLCULO TENSIONAL

Hipótesis de cálculo:

INFRECUENTEST.Tinf.VY+

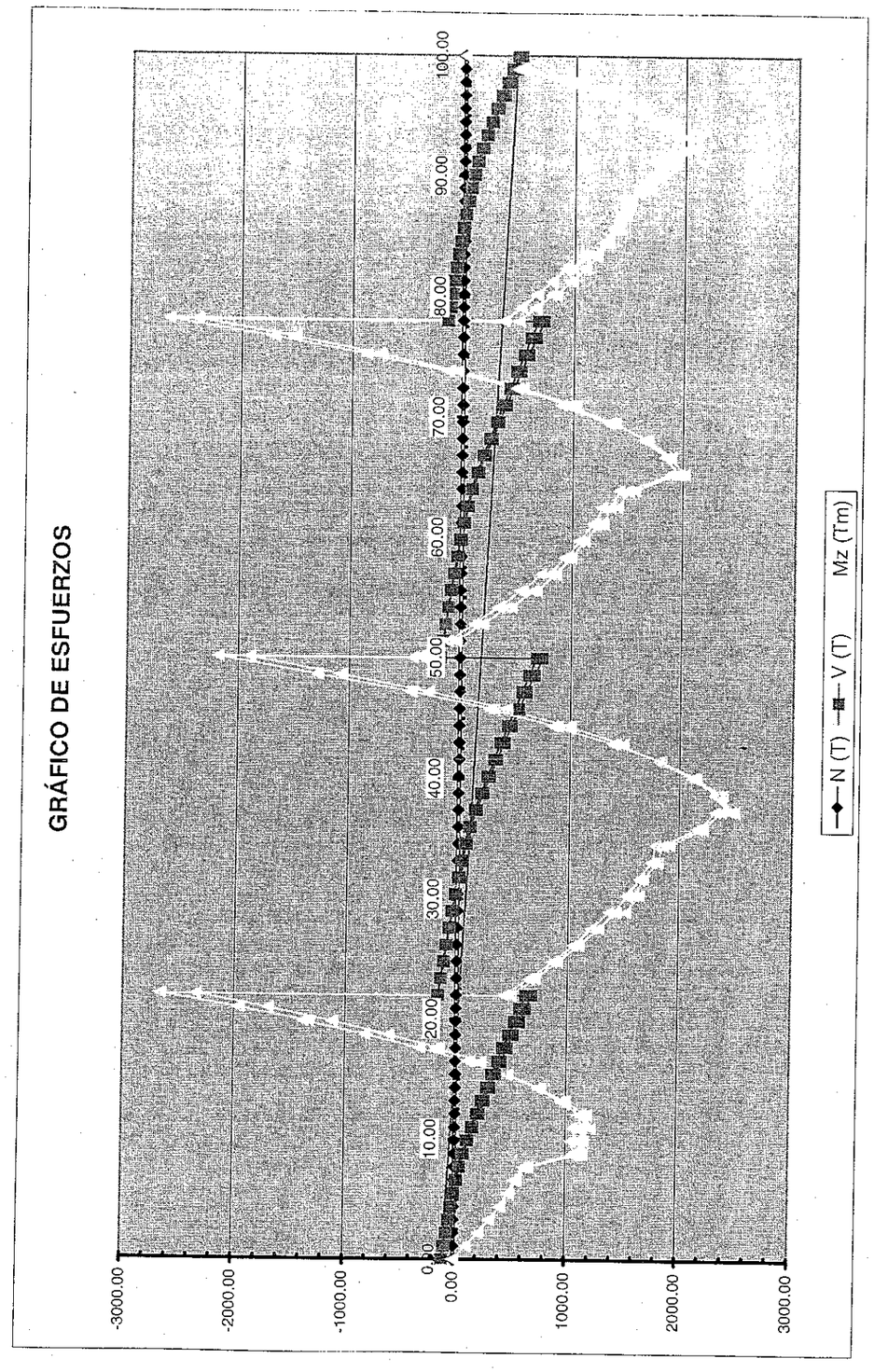
C. Infrecuentes dominante tren VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	163.78	2092.03
174	175	93.40	0.00	207.53	2018.52
175	175	93.40	0.00	209.13	2023.74
175	176	94.50	0.00	254.97	1850.14
176	176	94.50	0.00	256.55	1851.06
176	177	95.60	0.00	303.74	1614.00
177	177	95.60	0.00	305.32	1614.38
177	178	96.70	0.00	353.24	1321.42
178	178	96.70	0.00	354.94	1323.21
178	179	97.80	0.00	403.92	959.75
179	179	97.80	-0.01	405.78	960.33
179	180	98.90	-0.01	456.22	520.06
180	180	98.90	0.00	458.19	520.71
180	181	100.00	0.00	511.13	-0.32

05/09/03



Cortante.xls

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-474.20	0.18
1	2	1.10	0.00	-424.54	484.81
2	2	1.10	-0.01	-425.05	485.16
2	3	2.20	-0.01	-377.47	899.63
3	3	2.20	0.00	-377.67	899.92
3	4	3.30	0.00	-331.16	1246.34
4	4	3.30	0.00	-330.98	1245.55
4	5	4.40	0.00	-285.10	1527.38
5	5	4.40	0.00	-284.72	1527.74
5	6	5.50	0.00	-239.54	1759.00
6	6	5.50	0.00	-238.89	1757.07
6	7	6.60	0.00	-194.75	1929.86
7	7	6.60	0.00	-193.93	1927.32
7	8	7.70	0.00	-151.59	2004.01
8	8	7.70	0.00	-150.51	1999.33
8	9	8.80	0.00	-114.64	1812.08
9	9	8.80	-0.01	-113.78	1766.76
9	10	9.90	-0.01	-81.63	1801.23
10	10	9.90	0.00	-82.08	1748.85
10	11	11.00	0.00	-53.79	1665.58
11	11	11.00	0.00	-54.97	1611.64
11	12	12.10	0.00	-27.26	1506.52
12	12	12.10	0.00	-29.27	1489.76
12	13	13.20	0.00	-2.66	1439.05
13	13	13.20	0.00	-4.30	1425.65
13	14	14.30	0.00	19.99	1371.89
14	14	14.30	6.06	16.54	1366.52
14	15	15.40	6.93	40.16	1281.06
15	15	15.40	0.00	40.92	1279.46
15	16	16.50	0.00	64.17	1171.31
16	16	16.50	0.00	62.32	1080.45
16	17	17.60	0.00	84.69	960.24
17	17	17.60	0.00	82.41	901.15
17	18	18.70	0.00	104.14	766.55
18	18	18.70	0.00	101.74	760.80
18	19	19.80	0.00	121.46	609.43
19	19	19.80	0.00	120.73	603.88
19	20	20.90	0.00	138.30	466.62
20	20	20.90	0.00	138.13	466.61
20	21	22.00	0.00	156.53	304.54
21	1021	22.00	0.00	-677.46	-2389.63
21	22	23.40	0.00	-610.76	-1513.37
22	22	23.40	0.00	-610.83	-1521.19
22	23	24.80	0.00	-549.41	-734.41
23	23	24.80	0.00	-548.81	-733.31
23	24	26.20	0.00	-488.18	-45.03
24	24	26.20	0.00	-487.00	-44.14
24	25	27.60	0.00	-427.23	547.15
25	25	27.60	0.00	-425.57	544.81
25	26	29.00	0.00	-367.25	1018.75
26	26	29.00	5.56	-362.93	965.19

Cortante.xls Programa DINTEL PACADAR S.A. 05/09/03
INFRECUENTEST.Tinf.VY-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	4.39	-305.33	1367.09
27	27	30.40	0.00	-304.64	1376.34
27	28	31.80	0.00	-248.31	1672.39
28	28	31.80	0.00	-246.24	1643.39
28	29	33.20	0.00	-191.56	1852.38
29	29	33.20	0.00	-189.09	1840.03
29	30	34.60	0.00	-135.52	1965.16
30	30	34.60	0.00	-133.74	1889.47
30	31	36.00	0.00	-82.19	1538.15
31	31	36.00	0.00	-82.94	1434.44
31	32	37.40	0.00	-45.68	1393.41
32	32	37.40	0.00	-47.84	1314.76
32	33	38.80	0.00	-12.27	1253.86
33	33	38.80	0.00	-15.49	1228.74
33	34	40.20	0.00	18.51	1100.94
34	34	40.20	0.00	15.98	1100.68
34	35	41.60	0.00	47.41	982.57
35	35	41.60	2.87	44.42	958.54
35	36	43.00	3.75	74.88	807.03
36	36	43.00	0.00	73.09	734.16
36	37	44.40	0.00	102.58	553.00
37	37	44.40	0.00	99.31	526.90
37	38	45.80	0.00	127.75	319.96
38	38	45.80	0.00	124.60	305.34
38	39	47.20	0.00	152.03	75.11
39	39	47.20	0.00	149.25	70.62
39	40	48.60	0.00	175.72	-180.17
40	40	48.60	0.00	173.38	-188.73
40	41	50.00	0.00	199.44	-522.33
41	1041	50.00	0.00	-688.73	-1895.25
41	42	51.40	0.00	-622.66	-1066.84
42	42	51.40	0.00	-622.11	-1074.81
42	43	52.80	0.00	-560.58	-271.52
43	43	52.80	0.00	-559.39	-275.63
43	44	54.20	0.00	-498.67	427.76
44	44	54.20	0.00	-496.99	413.47
44	45	55.60	0.00	-437.36	1003.76
45	45	55.60	0.00	-435.32	977.82
45	46	57.00	0.00	-376.83	1487.28
46	46	57.00	4.47	-373.99	1413.47
46	47	58.40	3.28	-316.41	1830.40
47	47	58.40	0.00	-315.95	1806.74
47	48	59.80	0.00	-259.86	2119.60
48	48	59.80	0.01	-257.94	2117.84
48	49	61.20	0.01	-203.41	2342.99
49	49	61.20	0.00	-201.13	2313.05
49	50	62.60	0.00	-147.71	2455.15
50	50	62.60	0.00	-147.21	2321.73
50	51	64.00	0.00	-96.02	2223.99
51	51	64.00	0.00	-97.40	2169.49
51	52	65.40	0.00	-58.73	1907.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	-61.42	1835.95
52	53	66.80	0.00	-26.61	1800.78
53	53	66.80	0.00	-30.06	1789.75
53	54	68.20	0.00	3.48	1676.66
54	54	68.20	0.00	0.59	1686.00
54	55	69.60	0.00	32.22	1550.97
55	55	69.60	3.84	28.49	1560.93
55	56	71.00	4.71	58.90	1432.03
56	56	71.00	0.00	56.17	1378.34
56	57	72.40	0.00	85.77	1212.51
57	57	72.40	0.00	82.82	1209.81
57	58	73.80	0.00	111.26	1026.54
58	58	73.80	-0.01	108.71	1027.01
58	59	75.20	-0.01	136.15	819.69
59	59	75.20	0.00	133.97	820.43
59	60	76.60	0.00	160.45	591.29
60	60	76.60	0.00	158.81	583.17
60	61	78.00	0.00	184.32	332.25
61	1061	78.00	0.00	-623.16	-2340.56
61	62	79.10	0.00	-572.09	-1692.60
62	62	79.10	0.00	-571.84	-1695.74
62	63	80.20	0.00	-522.98	-1110.41
63	63	80.20	0.00	-522.31	-1118.25
63	64	81.30	0.00	-473.85	-594.85
64	64	81.30	0.00	-472.92	-600.38
64	65	82.40	0.00	-424.90	-140.01
65	65	82.40	0.00	-423.81	-171.53
65	66	83.50	0.00	-377.15	227.98
66	66	83.50	0.00	-376.28	132.04
66	67	84.60	0.00	-330.14	467.82
67	67	84.60	7.36	-327.38	466.63
67	68	85.70	6.19	-281.49	748.68
68	68	85.70	0.01	-282.86	741.26
68	69	86.80	0.01	-237.63	951.89
69	69	86.80	0.00	-236.84	946.58
69	70	87.90	0.00	-192.58	1133.89
70	70	87.90	0.00	-191.68	1112.35
70	71	89.00	0.00	-148.01	1143.64
71	71	89.00	0.00	-148.65	1058.14
71	72	90.10	0.00	-107.23	1097.46
72	72	90.10	0.00	-108.94	1045.02
72	73	91.20	0.00	-69.01	1081.37
73	73	91.20	0.00	-71.51	1056.49
73	74	92.30	0.00	-36.60	671.87
74	74	92.30	0.00	-38.44	667.20
74	75	93.40	0.00	-11.61	589.96
75	75	93.40	0.00	-13.37	587.27
75	76	94.50	0.00	11.79	528.63
76	76	94.50	0.00	10.26	527.23
76	77	95.60	0.00	34.56	449.05
77	77	95.60	0.00	33.14	449.13

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	56.51	354.20
78	78	96.70	0.00	55.30	353.09
78	79	97.80	0.00	77.74	244.46
79	79	97.80	0.01	76.69	244.48
79	80	98.90	0.01	98.18	126.30
80	80	98.90	0.00	97.34	126.31
80	81	100.00	0.00	117.89	-0.02
101	101	0.00	0.00	-511.15	-0.32
101	102	1.10	0.00	-458.21	520.69
102	102	1.10	-0.01	-456.23	520.07
102	103	2.20	-0.01	-405.80	960.35
103	103	2.20	0.00	-403.95	959.79
103	104	3.30	0.00	-354.98	1323.18
104	104	3.30	0.00	-353.23	1321.44
104	105	4.40	0.00	-305.35	1614.39
105	105	4.40	0.00	-303.77	1613.99
105	106	5.50	0.00	-256.57	1851.06
106	106	5.50	0.00	-255.01	1850.14
106	107	6.60	0.00	-209.17	2023.72
107	107	6.60	0.00	-207.55	2018.52
107	108	7.70	0.00	-163.80	2092.03
108	108	7.70	0.00	-162.33	2079.23
108	109	8.80	0.00	-124.67	1926.47
109	109	8.80	0.00	-123.72	1860.41
109	110	9.90	0.00	-89.51	1798.41
110	110	9.90	0.00	-90.00	1841.22
110	111	11.00	0.00	-60.67	1731.85
111	111	11.00	0.00	-61.99	1670.92
111	112	12.10	0.00	-32.92	1552.86
112	112	12.10	0.00	-34.73	1552.85
112	113	13.20	0.00	-7.58	1488.94
113	113	13.20	0.00	-9.13	1487.72
113	114	14.30	0.00	15.75	1413.85
114	114	14.30	6.06	12.48	1413.45
114	115	15.40	6.93	36.54	1320.49
115	115	15.40	0.00	37.49	1318.38
115	116	16.50	0.00	61.03	1203.68
116	116	16.50	0.00	59.99	1200.07
116	117	17.60	0.00	80.39	848.01
117	117	17.60	0.00	79.86	847.88
117	118	18.70	0.00	96.25	749.86
118	118	18.70	0.00	95.68	749.76
118	119	19.80	0.00	112.07	635.51
119	119	19.80	0.00	111.45	635.40
119	120	20.90	0.00	127.84	503.81
120	120	20.90	0.00	127.21	503.76
120	121	22.00	0.00	144.98	354.04
121	1121	22.00	0.00	-730.22	-2650.44
121	122	23.40	0.00	-659.59	-1706.82
122	122	23.40	0.00	-656.93	-1706.63
122	123	24.80	0.00	-591.89	-861.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-589.05	-861.65
123	124	26.20	0.00	-525.02	-126.44
124	124	26.20	0.00	-522.13	-133.91
124	125	27.60	0.00	-459.22	494.31
125	125	27.60	0.00	-456.29	488.94
125	126	29.00	0.00	-395.21	987.93
126	126	29.00	5.56	-390.19	897.24
126	127	30.40	4.38	-330.10	1320.70
127	127	30.40	0.00	-329.08	1371.52
127	128	31.80	0.00	-270.37	1679.14
128	128	31.80	0.00	-267.33	1678.65
128	129	33.20	0.00	-210.87	1893.77
129	129	33.20	0.00	-207.60	1885.47
129	130	34.60	0.00	-152.48	2012.07
130	130	34.60	0.00	-150.21	1937.81
130	131	36.00	0.00	-97.47	1621.35
131	131	36.00	0.00	-97.45	1520.98
131	132	37.40	0.00	-57.99	1474.69
132	132	37.40	0.00	-59.22	1409.42
132	133	38.80	0.00	-21.76	1339.63
133	133	38.80	0.00	-24.23	1305.07
133	134	40.20	0.00	10.97	1158.76
134	134	40.20	0.00	9.10	1158.31
134	135	41.60	0.00	41.49	1032.47
135	135	41.60	2.87	39.13	1030.19
135	136	43.00	3.75	70.30	870.73
136	136	43.00	0.00	69.87	868.99
136	137	44.40	0.00	99.78	679.39
137	137	44.40	0.01	98.49	640.71
137	138	45.80	0.01	127.10	424.74
138	138	45.80	0.00	125.50	378.93
138	139	47.20	0.00	152.82	140.55
139	139	47.20	0.00	151.22	123.13
139	140	48.60	0.00	177.29	-133.89
140	140	48.60	0.00	175.87	-141.29
140	141	50.00	0.00	201.23	-478.01
141	1141	50.00	0.01	-742.62	-2177.67
141	142	51.40	0.01	-672.70	-1280.72
142	142	51.40	0.00	-669.40	-1288.10
142	143	52.80	0.00	-604.24	-424.96
143	143	52.80	0.00	-600.94	-442.58
143	144	54.20	0.00	-536.83	309.56
144	144	54.20	0.00	-533.65	263.45
144	145	55.60	0.00	-470.93	889.18
145	145	55.60	0.00	-468.10	850.04
145	146	57.00	0.00	-406.88	1390.82
146	146	57.00	4.47	-403.06	1387.82
146	147	58.40	3.28	-342.99	1828.85
147	147	58.40	0.00	-341.05	1826.25
147	148	59.80	0.00	-282.60	2151.88
148	148	59.80	-0.01	-279.53	2149.72

CÁLCULO TENSIONAL
Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-
C. Infrecuentes dominante tren VY-
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-0.01	-223.22	2381.67
149	149	61.20	0.00	-220.05	2342.48
149	150	62.60	0.00	-165.15	2486.74
150	150	62.60	0.00	-163.84	2371.33
150	151	64.00	0.00	-111.57	2273.18
151	151	64.00	0.00	-112.09	2220.25
151	152	65.40	0.00	-70.94	1987.20
152	152	65.40	0.00	-72.63	1914.76
152	153	66.80	0.00	-36.01	1871.88
153	153	66.80	0.00	-38.61	1865.05
153	154	68.20	0.00	-3.97	1732.11
154	154	68.20	0.00	-5.76	1731.76
154	155	69.60	0.00	26.56	1627.48
155	155	69.60	3.84	24.57	1678.52
155	156	71.00	4.71	55.67	1539.94
156	156	71.00	0.00	54.61	1450.47
156	157	72.40	0.00	84.66	1274.02
157	157	72.40	0.00	83.11	1269.03
157	158	73.80	0.00	111.70	1075.36
158	158	73.80	0.00	110.31	1068.19
158	159	75.20	0.00	137.59	851.68
159	159	75.20	0.00	136.50	851.96
159	160	76.60	0.00	162.55	615.97
160	160	76.60	0.00	161.68	616.25
160	161	78.00	0.00	186.52	361.65
161	1161	78.00	0.00	-679.55	-2657.53
161	162	79.10	0.00	-625.42	-1949.45
162	162	79.10	0.01	-622.97	-1961.78
162	163	80.20	0.01	-571.15	-1324.17
163	163	80.20	0.01	-568.69	-1376.64
163	164	81.30	0.01	-517.38	-808.25
164	164	81.30	0.00	-515.21	-814.31
164	165	82.40	0.00	-464.49	-315.52
165	165	82.40	0.00	-462.32	-318.66
165	166	83.50	0.00	-412.98	112.99
166	166	83.50	0.00	-410.83	109.62
166	167	84.60	0.00	-362.40	471.75
167	167	84.60	7.36	-357.89	469.77
167	168	85.70	6.19	-309.86	771.96
168	168	85.70	0.00	-309.52	771.28
168	169	86.80	0.00	-262.42	993.63
169	169	86.80	0.00	-260.05	992.38
169	170	87.90	0.00	-213.82	1191.40
170	170	87.90	0.00	-211.34	1187.12
170	171	89.00	0.00	-166.13	1223.58
171	171	89.00	0.00	-164.72	1125.35
171	172	90.10	0.00	-121.95	1157.92
172	172	90.10	0.00	-122.01	1111.33
172	173	91.20	0.00	-81.10	1148.68
173	173	91.20	0.00	-82.19	1105.78
173	174	92.30	0.00	-46.34	721.49

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTEST.Tinf.VY-

C. Infrecuentes dominante tren VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-46.98	708.34
174	175	93.40	0.00	-19.06	624.65
175	175	93.40	0.00	-19.76	621.90
175	176	94.50	0.00	6.24	555.48
176	176	94.50	0.00	5.64	554.73
176	177	95.60	0.00	30.54	468.31
177	177	95.60	0.00	30.02	468.24
177	178	96.70	0.00	53.72	365.46
178	178	96.70	0.00	53.22	364.00
178	179	97.80	0.00	75.67	248.93
179	179	97.80	-0.01	75.15	248.68
179	180	98.90	-0.01	96.37	126.74
180	180	98.90	0.00	95.82	126.45
180	181	100.00	0.00	115.77	0.14

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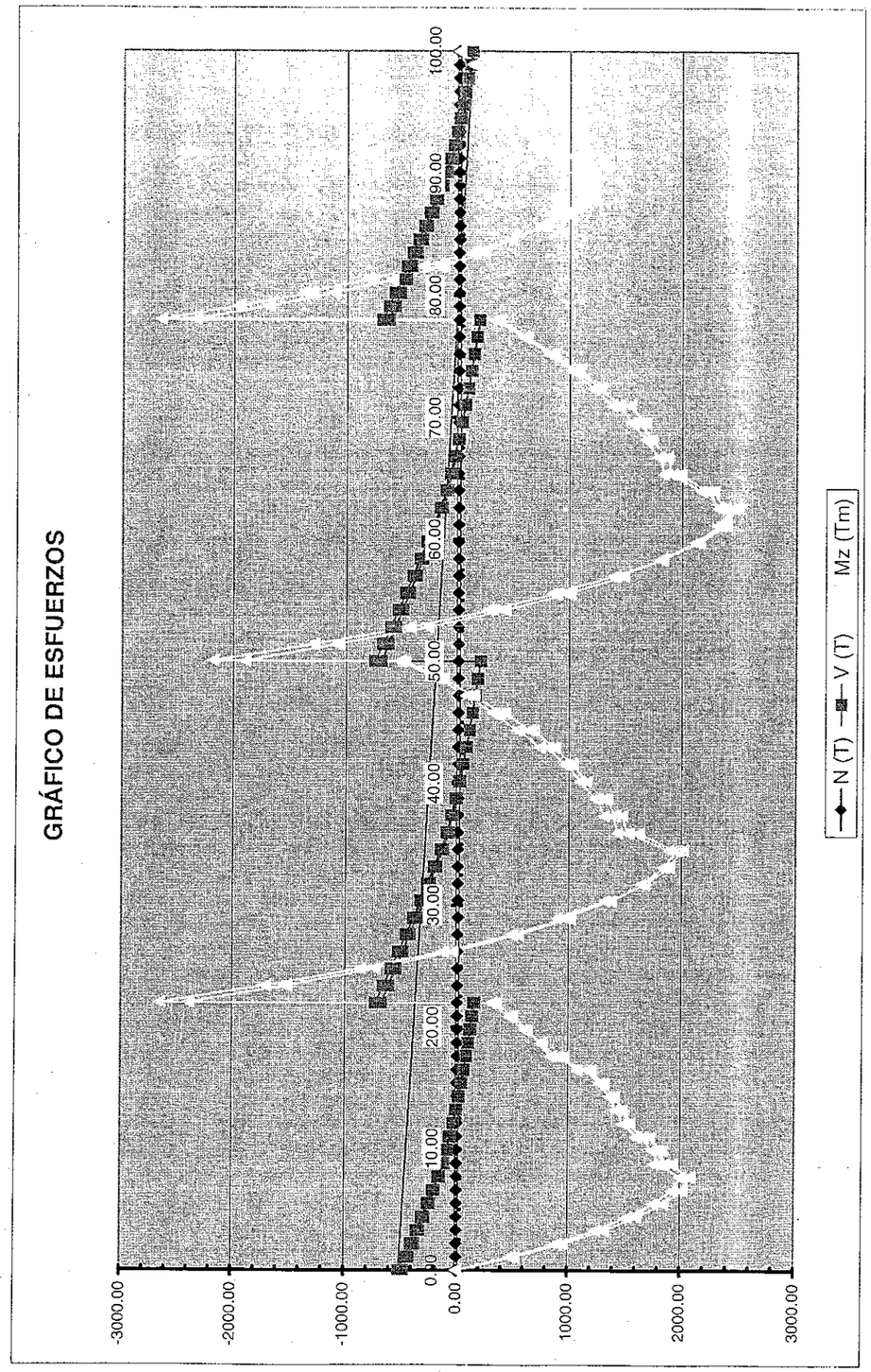
Programa DINTEL PACADAR S.A.
INFRECUENTEST.Tinf.VY-

Cortante.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-113.92	-0.04
1	2	1.10	0.00	-95.51	121.50
2	2	1.10	-0.01	-96.00	121.44
2	3	2.20	-0.01	-76.83	234.09
3	3	2.20	0.00	-77.51	234.03
3	4	3.30	0.00	-57.61	336.72
4	4	3.30	0.00	-58.43	337.54
4	5	4.40	0.00	-37.77	426.93
5	5	4.40	0.00	-38.77	426.84
5	6	5.50	0.00	-17.36	500.52
6	6	5.50	0.00	-18.48	501.64
6	7	6.60	0.00	3.62	557.41
7	7	6.60	0.00	2.31	559.55
7	8	7.70	0.00	25.91	636.08
8	8	7.70	0.00	24.55	646.03
8	9	8.80	0.00	56.56	1042.70
9	9	8.80	-0.01	54.61	1062.61
9	10	9.90	-0.01	91.96	1031.18
10	10	9.90	0.00	90.64	1073.12
10	11	11.00	0.00	129.17	1033.37
11	11	11.00	0.00	128.71	1101.76
11	12	12.10	0.00	169.36	1079.67
12	12	12.10	0.00	170.14	1096.92
12	13	13.20	0.00	211.27	926.27
13	13	13.20	0.00	211.94	930.51
13	14	14.30	0.00	253.85	734.80
14	14	14.30	6.19	252.43	740.76
14	15	15.40	7.36	294.87	481.54
15	15	15.40	0.00	297.60	482.52
15	16	16.50	0.00	340.18	174.77
16	16	16.50	0.00	340.97	251.54
16	17	17.60	0.00	384.03	-114.43
17	17	17.60	0.00	384.99	-89.17
17	18	18.70	0.00	429.13	-510.22
18	18	18.70	0.00	429.97	-505.72
18	19	19.80	0.00	474.46	-983.56
19	19	19.80	0.00	475.10	-977.28
19	20	20.90	0.00	519.90	-1511.09
20	20	20.90	0.00	520.22	-1508.59
20	21	22.00	0.00	567.15	-2099.11
21	1021	22.00	0.00	-170.56	583.16
21	22	23.40	0.00	-147.65	814.51
22	22	23.40	0.00	-148.73	820.97
22	23	24.80	0.00	-125.02	1031.02
23	23	24.80	0.00	-126.53	1030.39
23	24	26.20	0.00	-102.07	1219.18
24	24	26.20	0.00	-103.92	1218.73
24	25	27.60	0.00	-78.66	1384.48
25	25	27.60	0.00	-80.84	1386.57
25	26	29.00	0.00	-54.58	1536.33
26	26	29.00	4.71	-56.55	1589.30

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INFRECUENTESG.Tinf.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.84	-29.70	1704.17
27	27	30.40	0.00	-32.66	1685.90
27	28	31.80	0.00	-4.84	1801.76
28	28	31.80	0.00	-7.04	1794.25
28	29	33.20	0.00	22.33	1888.92
29	29	33.20	0.00	19.63	1897.69
29	30	34.60	0.00	50.00	1926.43
30	30	34.60	0.00	47.93	1983.58
30	31	36.00	0.00	81.89	2275.33
31	31	36.00	0.00	80.83	2292.72
31	32	37.40	0.00	128.83	2428.07
32	32	37.40	0.00	129.27	2534.80
32	33	38.80	0.00	179.29	2400.49
33	33	38.80	0.00	181.17	2424.46
33	34	40.20	0.00	232.06	2213.42
34	34	40.20	0.00	233.65	2214.85
34	35	41.60	0.00	285.81	1923.43
35	35	41.60	3.28	286.08	1942.37
35	36	43.00	4.47	339.43	1557.32
36	36	43.00	0.00	342.02	1616.43
36	37	44.40	0.00	396.10	1146.96
37	37	44.40	0.00	397.83	1167.75
37	38	45.80	0.00	452.79	623.36
38	38	45.80	0.00	454.27	634.82
38	39	47.20	0.00	510.14	-10.48
39	39	47.20	0.00	511.23	-7.16
39	40	48.60	0.00	567.73	-742.73
40	40	48.60	0.00	568.32	-736.32
40	41	50.00	0.00	629.19	-1490.57
41	1041	50.00	0.00	-186.41	-453.66
41	42	51.40	0.00	-162.96	-138.64
42	42	51.40	0.00	-164.58	-131.82
42	43	52.80	0.00	-140.89	100.67
43	43	52.80	0.00	-142.90	104.22
43	44	54.20	0.00	-118.45	316.41
44	44	54.20	0.00	-120.76	328.06
44	45	55.60	0.00	-95.50	517.88
45	45	55.60	0.00	-97.92	538.70
45	46	57.00	0.00	-71.82	704.03
46	46	57.00	3.75	-72.91	762.32
46	47	58.40	2.88	-46.03	900.19
47	47	58.40	0.00	-48.44	919.33
47	48	59.80	0.00	-20.78	1026.85
48	48	59.80	0.01	-22.69	1027.04
48	49	61.20	0.01	7.01	1138.52
49	49	61.20	0.00	4.53	1158.60
49	50	62.60	0.00	35.49	1212.94
50	50	62.60	0.00	33.85	1275.86
50	51	64.00	0.00	66.38	1349.89
51	51	64.00	0.00	65.89	1406.69
51	52	65.40	0.00	113.90	1796.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	3.84	-29.70	1704.17
27	27	30.40	0.00	-32.66	1685.90
27	28	31.80	0.00	-4.84	1801.76
28	28	31.80	0.00	-7.04	1794.25
28	29	33.20	0.00	22.33	1888.92
29	29	33.20	0.00	19.63	1897.69
29	30	34.60	0.00	50.00	1926.43
30	30	34.60	0.00	47.93	1983.58
30	31	36.00	0.00	81.89	2275.33
31	31	36.00	0.00	80.83	2292.72
31	32	37.40	0.00	128.83	2428.07
32	32	37.40	0.00	129.27	2534.80
32	33	38.80	0.00	179.29	2400.49
33	33	38.80	0.00	181.17	2424.46
33	34	40.20	0.00	232.06	2213.42
34	34	40.20	0.00	233.65	2214.85
34	35	41.60	0.00	285.81	1923.43
35	35	41.60	3.28	286.08	1942.37
35	36	43.00	4.47	339.43	1557.32
36	36	43.00	0.00	342.02	1616.43
36	37	44.40	0.00	396.10	1146.96
37	37	44.40	0.00	397.83	1167.75
37	38	45.80	0.00	452.79	623.36
38	38	45.80	0.00	454.27	634.82
38	39	47.20	0.00	510.14	-10.48
39	39	47.20	0.00	511.23	-7.16
39	40	48.60	0.00	567.73	-742.73
40	40	48.60	0.00	568.32	-736.32
40	41	50.00	0.00	629.19	-1490.57
41	1041	50.00	0.00	-186.41	-453.66
41	42	51.40	0.00	-162.96	-138.64
42	42	51.40	0.00	-164.58	-131.82
42	43	52.80	0.00	-140.89	100.67
43	43	52.80	0.00	-142.90	104.22
43	44	54.20	0.00	-118.45	316.41
44	44	54.20	0.00	-120.76	328.06
44	45	55.60	0.00	-95.50	517.88
45	45	55.60	0.00	-97.92	538.70
45	46	57.00	0.00	-71.82	704.03
46	46	57.00	3.75	-72.91	762.32
46	47	58.40	2.88	-46.03	900.19
47	47	58.40	0.00	-48.44	919.33
47	48	59.80	0.00	-20.78	1026.85
48	48	59.80	0.01	-22.69	1027.04
48	49	61.20	0.01	7.01	1138.52
49	49	61.20	0.00	4.53	1158.60
49	50	62.60	0.00	35.49	1212.94
50	50	62.60	0.00	33.85	1275.86
50	51	64.00	0.00	66.38	1349.89
51	51	64.00	0.00	65.89	1406.69
51	52	65.40	0.00	113.90	1796.71

Cortante.xls

Programa DINTEL PACADAR S.A.
INFRECUENTESG.Tinf.VY+

05/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	115.36	1857.25
52	53	66.80	0.00	165.50	1742.37
53	53	66.80	0.00	167.52	1752.29
53	54	68.20	0.00	218.53	1560.05
54	54	68.20	0.00	220.24	1583.26
54	55	69.60	0.00	272.58	1311.09
55	55	69.60	4.39	272.88	1293.49
55	56	71.00	5.56	326.24	926.49
56	56	71.00	0.00	330.22	979.40
56	57	72.40	0.00	384.10	546.02
57	57	72.40	0.00	385.56	547.92
57	58	73.80	0.00	440.65	8.52
58	58	73.80	-0.01	441.70	7.86
58	59	75.20	-0.01	497.48	-619.47
59	59	75.20	0.00	498.08	-620.31
59	60	76.60	0.00	554.47	-1336.78
60	60	76.60	0.00	554.57	-1330.54
60	61	78.00	0.00	616.05	-2129.58
61	1061	78.00	0.00	-135.24	540.83
61	62	79.10	0.00	-115.83	684.93
62	62	79.10	0.00	-117.12	687.44
62	63	80.20	0.00	-98.66	818.55
63	63	80.20	0.00	-100.21	826.55
63	64	81.30	0.00	-81.30	945.06
64	64	81.30	0.00	-83.06	949.63
64	65	82.40	0.00	-63.69	1055.90
65	65	82.40	0.00	-65.36	1103.14
65	66	83.50	0.00	-45.48	1195.58
66	66	83.50	0.00	-46.86	1268.25
66	67	84.60	0.00	-26.22	1349.55
67	67	84.60	6.93	-25.05	1350.82
67	68	85.70	6.06	-4.17	1410.73
68	68	85.70	0.01	-7.22	1414.99
68	69	86.80	0.01	14.20	1447.23
69	69	86.80	0.00	12.99	1457.93
69	70	87.90	0.00	36.25	1485.42
70	70	87.90	0.00	34.74	1498.80
70	71	89.00	0.00	58.88	1580.67
71	71	89.00	0.00	58.03	1623.82
71	72	90.10	0.00	82.95	1677.01
72	72	90.10	0.00	82.69	1718.88
72	73	91.20	0.00	110.70	1670.97
73	73	91.20	0.00	111.42	1707.22
73	74	92.30	0.00	143.74	1919.36
74	74	92.30	0.00	144.62	1929.34
74	75	93.40	0.00	184.04	1847.45
75	75	93.40	0.00	184.76	1849.55
75	76	94.50	0.00	225.81	1676.27
76	76	94.50	0.00	226.40	1677.82
76	77	95.60	0.00	268.26	1451.43
77	77	95.60	0.00	268.60	1451.19

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	311.03	1177.95
78	78	96.70	0.00	311.24	1178.66
78	79	97.80	0.00	354.17	847.36
79	79	97.80	0.01	354.12	847.17
79	80	98.90	0.01	397.89	455.08
80	80	98.90	0.00	397.58	454.86
80	81	100.00	0.00	443.25	0.13
101	101	0.00	0.00	-107.32	0.13
101	102	1.10	0.00	-89.82	116.50
102	102	1.10	-0.01	-90.43	116.79
102	103	2.20	-0.01	-71.91	228.18
103	103	2.20	0.00	-72.51	228.41
103	104	3.30	0.00	-53.00	332.72
104	104	3.30	0.00	-53.50	333.96
104	105	4.40	0.00	-33.01	426.91
105	105	4.40	0.00	-33.54	427.01
105	106	5.50	0.00	-12.08	505.30
106	106	5.50	0.00	-12.65	505.93
106	107	6.60	0.00	9.70	566.62
107	107	6.60	0.00	9.04	568.85
107	108	7.70	0.00	33.10	649.92
108	108	7.70	0.00	32.52	669.09
108	109	8.80	0.00	64.91	1069.19
109	109	8.80	0.00	64.02	1103.50
109	110	9.90	0.00	101.83	1071.77
110	110	9.90	0.00	101.74	1109.06
110	111	11.00	0.00	141.01	1075.58
111	111	11.00	0.00	142.12	1154.15
111	112	12.10	0.00	183.69	1129.29
112	112	12.10	0.00	185.60	1132.68
112	113	13.20	0.00	228.00	954.50
113	113	13.20	0.00	229.84	955.45
113	114	14.30	0.00	272.92	752.74
114	114	14.30	6.19	272.74	753.26
114	115	15.40	7.36	316.57	480.68
115	115	15.40	0.00	320.56	482.25
115	116	16.50	0.00	364.64	156.81
116	116	16.50	0.00	366.30	159.47
116	117	17.60	0.00	411.16	-228.35
117	117	17.60	0.00	412.78	-225.88
117	118	18.70	0.00	458.76	-673.22
118	118	18.70	0.00	460.42	-668.37
118	119	19.80	0.00	506.86	-1177.20
119	119	19.80	0.00	508.69	-1135.26
119	120	20.90	0.00	555.55	-1705.29
120	120	20.90	0.00	557.39	-1695.43
120	121	22.00	0.00	606.49	-2327.87
121	1121	22.00	0.00	-164.03	643.05
121	122	23.40	0.00	-142.20	866.06
122	122	23.40	0.00	-143.13	865.90
122	123	24.80	0.00	-120.32	1071.64

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-121.44	1071.46
123	124	26.20	0.00	-97.63	1259.17
124	124	26.20	0.00	-98.93	1264.94
124	125	27.60	0.00	-74.09	1431.89
125	125	27.60	0.00	-75.50	1435.92
125	126	29.00	0.00	-49.46	1588.36
126	126	29.00	4.70	-50.37	1670.05
126	127	30.40	3.83	-23.52	1788.00
127	127	30.40	0.00	-25.34	1736.97
127	128	31.80	0.00	2.50	1824.76
128	128	31.80	0.00	0.95	1825.07
128	129	33.20	0.00	30.64	1933.11
129	129	33.20	0.00	28.47	1938.58
129	130	34.60	0.00	59.72	1972.01
130	130	34.60	0.00	58.30	2029.95
130	131	36.00	0.00	93.70	2301.80
131	131	36.00	0.00	93.13	2308.72
131	132	37.40	0.00	141.67	2455.89
132	132	37.40	0.00	142.68	2548.19
132	133	38.80	0.00	193.47	2413.21
133	133	38.80	0.00	195.96	2444.53
133	134	40.20	0.00	247.88	2229.82
134	134	40.20	0.00	250.29	2231.54
134	135	41.60	0.00	303.91	1932.32
135	135	41.60	3.28	305.21	1934.39
135	136	43.00	4.47	360.14	1533.36
136	136	43.00	0.00	363.35	1535.68
136	137	44.40	0.00	419.20	1045.27
137	137	44.40	0.01	421.36	1076.53
137	138	45.80	0.01	478.40	508.72
138	138	45.80	0.00	480.83	545.59
138	139	47.20	0.00	538.96	-132.88
139	139	47.20	0.00	541.48	-118.81
139	140	48.60	0.00	600.48	-895.49
140	140	48.60	0.00	602.98	-889.58
140	141	50.00	0.00	666.54	-1690.83
141	1141	50.00	0.01	-179.39	-380.59
141	142	51.40	0.01	-157.04	-74.49
142	142	51.40	0.00	-158.45	-68.54
142	143	52.80	0.00	-135.63	158.96
143	143	52.80	0.00	-137.14	172.92
143	144	54.20	0.00	-113.32	383.06
144	144	54.20	0.00	-114.82	419.78
144	145	55.60	0.00	-89.96	609.53
145	145	55.60	0.00	-91.16	640.55
145	146	57.00	0.00	-65.26	806.72
146	146	57.00	3.75	-65.58	808.15
146	147	58.40	2.88	-38.68	947.63
147	147	58.40	0.00	-40.82	949.54
147	148	59.80	0.00	-12.94	1059.52
148	148	59.80	-0.01	-14.56	1059.89

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-0.01	15.56	1183.67
149	149	61.20	0.00	13.49	1211.37
149	150	62.60	0.00	45.43	1271.33
150	150	62.60	0.00	44.36	1323.57
150	151	64.00	0.00	78.05	1412.39
151	151	64.00	0.00	78.08	1457.27
151	152	65.40	0.00	126.62	1823.47
152	152	65.40	0.00	128.42	1882.92
152	153	66.80	0.00	179.37	1767.81
153	153	66.80	0.00	181.96	1774.47
153	154	68.20	0.00	233.99	1578.98
154	154	68.20	0.00	236.36	1579.36
154	155	69.60	0.00	290.20	1300.36
155	155	69.60	4.39	290.63	1249.45
155	156	71.00	5.56	345.58	868.33
156	156	71.00	0.00	349.92	950.93
156	157	72.40	0.00	405.64	501.44
157	157	72.40	0.00	407.87	505.68
157	158	73.80	0.00	465.05	-58.39
158	158	73.80	0.00	467.27	-52.46
158	159	75.20	0.00	525.36	-711.60
159	159	75.20	0.00	527.50	-711.67
159	160	76.60	0.00	586.40	-1467.99
160	160	76.60	0.00	588.37	-1468.15
160	161	78.00	0.00	652.57	-2313.47
161	1161	78.00	0.00	-127.76	657.95
161	162	79.10	0.00	-109.25	794.13
162	162	79.10	0.01	-110.24	804.77
162	163	80.20	0.01	-92.57	930.44
163	163	80.20	0.01	-93.58	972.89
163	164	81.30	0.01	-75.30	1087.90
164	164	81.30	0.00	-76.15	1093.14
164	165	82.40	0.00	-57.29	1197.28
165	165	82.40	0.00	-58.23	1199.64
165	166	83.50	0.00	-38.71	1291.11
166	166	83.50	0.00	-39.68	1294.01
166	167	84.60	0.00	-19.27	1375.73
167	167	84.60	6.93	-18.16	1377.44
167	168	85.70	6.06	2.62	1439.22
168	168	85.70	0.00	-0.51	1439.63
168	169	86.80	0.00	20.93	1484.54
169	169	86.80	0.00	19.59	1485.52
169	170	87.90	0.00	42.87	1520.90
170	170	87.90	0.00	41.32	1520.95
170	171	89.00	0.00	66.11	1611.12
171	171	89.00	0.00	64.95	1659.89
171	172	90.10	0.00	90.31	1732.60
172	172	90.10	0.00	89.83	1698.34
172	173	91.20	0.00	119.04	1726.87
173	173	91.20	0.00	119.69	1779.72
173	174	92.30	0.00	153.05	1967.86

CÁLCULO TENSIONAL

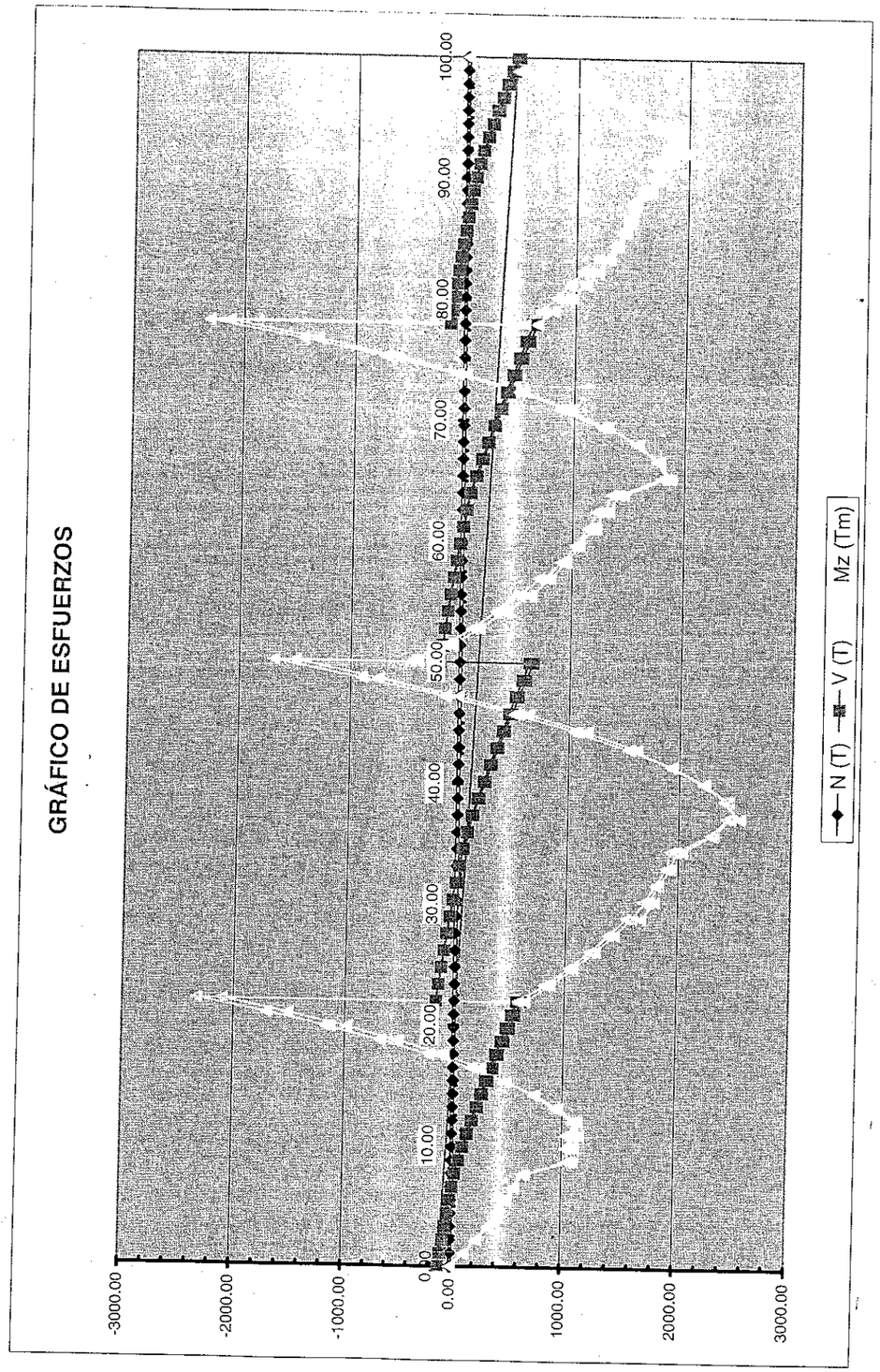
Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY+

C. Infrecuentes dominante GRAD VY+

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	154.18	1986.74
174	175	93.40	0.00	194.41	1907.83
175	175	93.40	0.00	195.64	1911.99
175	176	94.50	0.00	237.70	1738.97
176	176	94.50	0.00	238.92	1739.69
176	177	95.60	0.00	282.06	1510.03
177	177	95.60	0.00	283.26	1510.31
177	178	96.70	0.00	326.98	1230.06
178	178	96.70	0.00	328.27	1231.46
178	179	97.80	0.00	372.85	888.97
179	179	97.80	-0.01	374.25	889.39
179	180	98.90	-0.01	420.01	479.61
180	180	98.90	0.00	421.48	480.10
180	181	100.00	0.00	469.45	-0.24

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-443.28	0.13
1	2	1.10	0.00	-397.60	454.86
2	2	1.10	-0.01	-397.91	455.11
2	3	2.20	-0.01	-354.13	847.19
3	3	2.20	0.00	-354.20	847.39
3	4	3.30	0.00	-311.27	1178.63
4	4	3.30	0.00	-311.04	1177.98
4	5	4.40	0.00	-268.63	1451.17
5	5	4.40	0.00	-268.26	1451.43
5	6	5.50	0.00	-226.40	1677.82
6	6	5.50	0.00	-225.82	1676.26
6	7	6.60	0.00	-184.79	1849.51
7	7	6.60	0.00	-184.08	1847.47
7	8	7.70	0.00	-144.66	1929.35
8	8	7.70	0.00	-143.75	1925.59
8	9	8.80	0.00	-110.64	1747.96
9	9	8.80	-0.01	-109.93	1711.71
9	10	9.90	-0.01	-80.49	1758.05
10	10	9.90	0.00	-80.83	1716.14
10	11	11.00	0.00	-54.48	1659.85
11	11	11.00	0.00	-55.41	1616.69
11	12	12.10	0.00	-29.82	1530.19
12	12	12.10	0.00	-31.41	1516.79
12	13	13.20	0.00	-6.71	1483.14
13	13	13.20	0.00	-8.01	1472.43
13	14	14.30	0.00	14.84	1432.57
14	14	14.30	6.06	11.72	1428.28
14	15	15.40	6.93	34.02	1359.26
15	15	15.40	0.00	35.10	1357.99
15	16	16.50	0.00	57.16	1266.12
16	16	16.50	0.00	55.71	1193.44
16	17	17.60	0.00	77.01	1088.96
17	17	17.60	0.00	75.22	1041.70
17	18	18.70	0.00	96.02	921.92
18	18	18.70	0.00	94.14	917.33
18	19	19.80	0.00	113.32	780.34
19	19	19.80	0.00	112.78	775.91
19	20	20.90	0.00	130.24	646.42
20	20	20.90	0.00	130.15	646.41
20	21	22.00	0.00	148.55	493.13
21	1021	22.00	0.00	-616.06	-2129.57
21	22	23.40	0.00	-554.58	-1330.52
22	22	23.40	0.00	-554.49	-1336.79
22	23	24.80	0.00	-498.08	-620.30
23	23	24.80	0.00	-497.46	-619.44
23	24	26.20	0.00	-441.68	7.86
24	24	26.20	0.00	-440.63	8.54
24	25	27.60	0.00	-385.52	547.91
25	25	27.60	0.00	-384.10	546.00
25	26	29.00	0.00	-330.21	979.39
26	26	29.00	5.56	-326.24	926.45

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	4.39	-272.88	1293.48
27	27	30.40	0.00	-272.58	1311.08
27	28	31.80	0.00	-220.24	1583.25
28	28	31.80	0.00	-218.53	1560.02
28	29	33.20	0.00	-167.51	1752.27
29	29	33.20	0.00	-165.50	1742.37
29	30	34.60	0.00	-115.36	1857.29
30	30	34.60	0.00	-113.89	1796.72
30	31	36.00	0.00	-65.56	1440.79
31	31	36.00	0.00	-66.14	1357.83
31	32	37.40	0.00	-31.88	1316.36
32	32	37.40	0.00	-33.59	1253.44
32	33	38.80	0.00	-0.80	1195.14
33	33	38.80	0.00	-3.35	1175.05
33	34	40.20	0.00	28.19	1057.13
34	34	40.20	0.00	26.18	1056.93
34	35	41.60	0.00	55.66	940.65
35	35	41.60	2.87	53.14	921.44
35	36	43.00	3.75	81.85	772.31
36	36	43.00	0.00	80.64	714.03
36	37	44.40	0.00	108.57	535.02
37	37	44.40	0.00	106.00	514.15
37	38	45.80	0.00	133.09	308.40
38	38	45.80	0.00	130.62	296.72
38	39	47.20	0.00	156.89	66.19
39	39	47.20	0.00	154.72	62.60
39	40	48.60	0.00	180.24	-190.52
40	40	48.60	0.00	178.43	-197.35
40	41	50.00	0.00	203.71	-535.31
41	1041	50.00	0.00	-629.19	-1490.58
41	42	51.40	0.00	-568.32	-736.35
42	42	51.40	0.00	-567.72	-742.74
42	43	52.80	0.00	-511.22	-7.16
43	43	52.80	0.00	-510.14	-10.48
43	44	54.20	0.00	-454.27	634.81
44	44	54.20	0.00	-452.81	623.35
44	45	55.60	0.00	-397.83	1167.78
45	45	55.60	0.00	-396.09	1146.99
45	46	57.00	0.00	-342.01	1616.43
46	46	57.00	4.47	-339.43	1557.35
46	47	58.40	3.28	-286.08	1942.40
47	47	58.40	0.00	-285.81	1923.44
47	48	59.80	0.00	-233.66	2214.90
48	48	59.80	0.01	-232.07	2213.47
48	49	61.20	0.01	-181.16	2424.49
49	49	61.20	0.00	-179.29	2400.52
49	50	62.60	0.00	-129.27	2534.85
50	50	62.60	0.00	-128.83	2428.10
50	51	64.00	0.00	-80.72	2326.82
51	51	64.00	0.00	-81.79	2283.22
51	52	65.40	0.00	-46.33	2024.58

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	-48.46	1967.39
52	53	66.80	0.00	-16.27	1935.29
53	53	66.80	0.00	-19.02	1926.47
53	54	68.20	0.00	12.16	1825.92
54	54	68.20	0.00	9.87	1833.41
54	55	69.60	0.00	39.51	1709.19
55	55	69.60	3.84	36.46	1727.41
55	56	71.00	4.71	65.13	1601.82
56	56	71.00	0.00	63.06	1548.82
56	57	72.40	0.00	91.12	1385.92
57	57	72.40	0.00	88.81	1383.77
57	58	73.80	0.00	115.90	1202.55
58	58	73.80	-0.01	113.90	1202.94
58	59	75.20	-0.01	140.20	996.34
59	59	75.20	0.00	138.50	996.95
59	60	76.60	0.00	164.03	766.75
60	60	76.60	0.00	162.78	760.25
60	61	78.00	0.00	187.50	506.48
61	1061	78.00	0.00	-567.18	-2099.13
61	62	79.10	0.00	-520.24	-1508.60
62	62	79.10	0.00	-519.92	-1511.12
62	63	80.20	0.00	-475.11	-977.31
63	63	80.20	0.00	-474.47	-983.59
63	64	81.30	0.00	-429.98	-505.73
64	64	81.30	0.00	-429.13	-510.18
64	65	82.40	0.00	-384.99	-89.16
65	65	82.40	0.00	-384.03	-114.40
65	66	83.50	0.00	-340.98	251.54
66	66	83.50	0.00	-340.20	174.76
66	67	84.60	0.00	-297.63	482.50
67	67	84.60	7.36	-294.87	481.53
67	68	85.70	6.19	-252.45	740.76
68	68	85.70	0.01	-253.87	734.80
68	69	86.80	0.01	-211.96	930.50
69	69	86.80	0.00	-211.28	926.24
69	70	87.90	0.00	-170.14	1096.91
70	70	87.90	0.00	-169.37	1079.67
70	71	89.00	0.00	-128.73	1101.77
71	71	89.00	0.00	-129.19	1033.36
71	72	90.10	0.00	-90.65	1073.14
72	72	90.10	0.00	-91.97	1031.18
72	73	91.20	0.00	-54.62	1062.59
73	73	91.20	0.00	-56.58	1042.69
73	74	92.30	0.00	-23.94	680.63
74	74	92.30	0.00	-25.39	676.91
74	75	93.40	0.00	-0.35	599.00
75	75	93.40	0.00	-1.74	596.86
75	76	94.50	0.00	21.80	538.21
76	76	94.50	0.00	20.60	537.10
76	77	95.60	0.00	43.45	459.05
77	77	95.60	0.00	42.34	459.13

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	64.44	363.89
78	78	96.70	0.00	63.51	363.02
78	79	97.80	0.00	84.87	253.04
79	79	97.80	0.01	84.06	253.07
79	80	98.90	0.01	104.67	131.67
80	80	98.90	0.00	104.04	131.69
80	81	100.00	0.00	123.88	-0.02
101	101	0.00	0.00	-469.48	-0.24
101	102	1.10	0.00	-421.50	480.08
102	102	1.10	-0.01	-420.02	479.62
102	103	2.20	-0.01	-374.28	889.42
103	103	2.20	0.00	-372.89	889.01
103	104	3.30	0.00	-328.32	1231.44
104	104	3.30	0.00	-326.99	1230.08
104	105	4.40	0.00	-283.30	1510.32
105	105	4.40	0.00	-282.09	1510.02
105	106	5.50	0.00	-238.94	1739.69
106	106	5.50	0.00	-237.74	1738.97
106	107	6.60	0.00	-195.67	1911.98
107	107	6.60	0.00	-194.42	1907.83
107	108	7.70	0.00	-154.20	1986.75
108	108	7.70	0.00	-153.06	1976.52
108	109	8.80	0.00	-118.73	1834.31
109	109	8.80	0.00	-117.99	1781.46
109	110	9.90	0.00	-87.03	1750.79
110	110	9.90	0.00	-87.44	1785.04
110	111	11.00	0.00	-60.38	1708.23
111	111	11.00	0.00	-61.46	1659.49
111	112	12.10	0.00	-34.93	1563.18
112	112	12.10	0.00	-36.38	1563.16
112	113	13.20	0.00	-11.38	1519.70
113	113	13.20	0.00	-12.65	1518.72
113	114	14.30	0.00	10.53	1463.70
114	114	14.30	6.06	7.51	1463.37
114	115	15.40	6.93	30.04	1389.47
115	115	15.40	0.00	31.21	1387.77
115	116	16.50	0.00	53.37	1291.99
116	116	16.50	0.00	52.51	1289.08
116	117	17.60	0.00	72.11	1000.67
117	117	17.60	0.00	71.64	1000.56
117	118	18.70	0.00	88.03	911.81
118	118	18.70	0.00	87.54	911.72
118	119	19.80	0.00	103.93	806.42
119	119	19.80	0.00	103.39	806.32
119	120	20.90	0.00	119.77	683.61
120	120	20.90	0.00	119.23	683.57
120	121	22.00	0.00	136.99	542.63
121	1121	22.00	0.00	-652.59	-2313.41
121	122	23.40	0.00	-588.37	-1468.13
122	122	23.40	0.00	-586.39	-1467.97
122	123	24.80	0.00	-527.50	-711.64

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-525.35	-711.56
123	124	26.20	0.00	-467.27	-52.45
124	124	26.20	0.00	-465.07	-58.39
124	125	27.60	0.00	-407.87	505.69
125	125	27.60	0.00	-405.63	501.42
125	126	29.00	0.00	-349.94	950.87
126	126	29.00	5.56	-345.57	868.30
126	127	30.40	4.38	-290.63	1249.40
127	127	30.40	0.00	-290.20	1300.33
127	128	31.80	0.00	-236.37	1579.33
128	128	31.80	0.00	-233.99	1578.97
128	129	33.20	0.00	-181.96	1774.44
129	129	33.20	0.00	-179.38	1767.81
129	130	34.60	0.00	-128.42	1882.91
130	130	34.60	0.00	-126.64	1823.50
130	131	36.00	0.00	-77.77	1502.48
131	131	36.00	0.00	-77.78	1422.19
131	132	37.40	0.00	-41.91	1376.66
132	132	37.40	0.00	-42.91	1324.44
132	133	38.80	0.00	-8.77	1259.45
133	133	38.80	0.00	-10.76	1231.79
133	134	40.20	0.00	21.56	1099.76
134	134	40.20	0.00	20.05	1099.39
134	135	41.60	0.00	50.13	977.92
135	135	41.60	2.87	48.07	976.08
135	136	43.00	3.75	77.17	821.89
136	136	43.00	0.00	76.99	820.48
136	137	44.40	0.00	105.09	636.34
137	137	44.40	0.01	104.02	605.38
137	138	45.80	0.01	131.08	394.38
138	138	45.80	0.00	129.75	357.71
138	139	47.20	0.00	155.78	123.00
139	139	47.20	0.00	154.45	109.05
139	140	48.60	0.00	179.48	-146.34
140	140	48.60	0.00	178.28	-152.27
140	141	50.00	0.00	202.83	-489.61
141	1141	50.00	0.01	-666.53	-1690.84
141	142	51.40	0.01	-602.99	-889.58
142	142	51.40	0.00	-600.49	-895.47
142	143	52.80	0.00	-541.50	-118.80
143	143	52.80	0.00	-538.99	-132.87
143	144	54.20	0.00	-480.83	545.56
144	144	54.20	0.00	-478.41	508.71
144	145	55.60	0.00	-421.37	1076.56
145	145	55.60	0.00	-419.20	1045.30
145	146	57.00	0.00	-363.35	1535.72
146	146	57.00	4.47	-360.15	1533.36
146	147	58.40	3.28	-305.23	1934.43
147	147	58.40	0.00	-303.91	1932.39
147	148	59.80	0.00	-250.28	2231.59
148	148	59.80	-0.01	-247.88	2229.89

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	-0.01	-195.96	2444.59
149	149	61.20	0.00	-193.47	2413.25
149	150	62.60	0.00	-142.68	2548.26
150	150	62.60	0.00	-141.67	2455.94
150	151	64.00	0.00	-93.10	2353.97
151	151	64.00	0.00	-93.56	2311.63
151	152	65.40	0.00	-56.27	2083.65
152	152	65.40	0.00	-57.63	2025.69
152	153	66.80	0.00	-24.16	1987.81
153	153	66.80	0.00	-26.26	1982.34
153	154	68.20	0.00	5.63	1866.59
154	154	68.20	0.00	4.17	1866.29
154	155	69.60	0.00	34.21	1767.65
155	155	69.60	3.84	32.50	1818.71
155	156	71.00	4.71	61.56	1686.64
156	156	71.00	0.00	60.76	1604.99
156	157	72.40	0.00	89.02	1435.18
157	157	72.40	0.00	87.74	1431.17
157	158	73.80	0.00	114.79	1243.56
158	158	73.80	0.00	113.63	1237.81
158	159	75.20	0.00	139.63	1026.15
159	159	75.20	0.00	138.71	1026.36
159	160	76.60	0.00	163.73	793.34
160	160	76.60	0.00	162.96	793.56
160	161	78.00	0.00	187.00	539.89
161	1161	78.00	0.00	-606.50	-2327.90
161	162	79.10	0.00	-557.42	-1695.47
162	162	79.10	0.01	-555.58	-1705.33
162	163	80.20	0.01	-508.72	-1135.28
163	163	80.20	0.01	-506.86	-1177.24
163	164	81.30	0.01	-460.42	-668.39
164	164	81.30	0.00	-458.78	-673.22
164	165	82.40	0.00	-412.81	-225.88
165	165	82.40	0.00	-411.17	-228.36
165	166	83.50	0.00	-366.29	159.43
166	166	83.50	0.00	-364.65	156.75
166	167	84.60	0.00	-320.57	482.25
167	167	84.60	7.36	-316.57	480.70
167	168	85.70	6.19	-272.75	753.23
168	168	85.70	0.00	-272.93	752.71
168	169	86.80	0.00	-229.85	955.46
169	169	86.80	0.00	-228.01	954.48
169	170	87.90	0.00	-185.63	1132.69
170	170	87.90	0.00	-183.68	1129.28
170	171	89.00	0.00	-142.13	1154.14
171	171	89.00	0.00	-141.05	1075.57
171	172	90.10	0.00	-101.75	1109.02
172	172	90.10	0.00	-101.83	1071.74
172	173	91.20	0.00	-64.02	1103.47
173	173	91.20	0.00	-64.94	1069.16
173	174	92.30	0.00	-31.78	715.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:
INFRECUENTESG.Tinf.VY-

C. Infrecuentes dominante GRAD VY-

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1;
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	-32.31	704.62
174	175	93.40	0.00	-6.53	621.74
175	175	93.40	0.00	-7.11	619.53
175	176	94.50	0.00	16.97	555.01
176	176	94.50	0.00	16.47	554.41
176	177	95.60	0.00	39.68	470.31
177	177	95.60	0.00	39.23	470.25
177	178	96.70	0.00	61.47	369.47
178	178	96.70	0.00	61.04	368.29
178	179	97.80	0.00	82.28	254.11
179	179	97.80	-0.01	81.83	253.90
179	180	98.90	-0.01	102.09	130.66
180	180	98.90	0.00	101.61	130.41
180	181	100.00	0.00	120.85	0.12

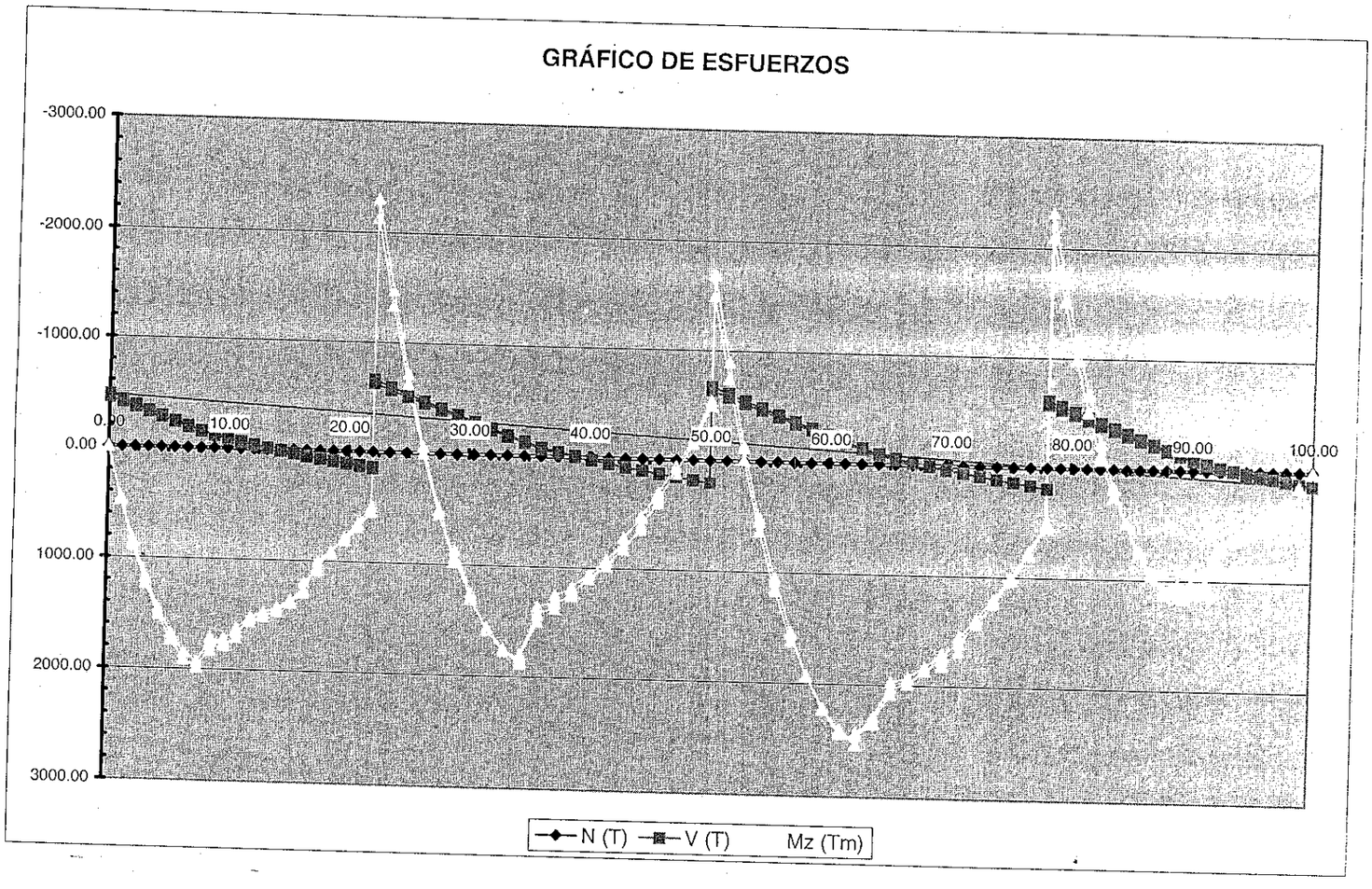


GRÁFICO DE ESFUERZOS
-3000.00
-2000.00
-1000.00
0.00
1000.00
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20.00
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80.00
90.00
100.00
N (T)
V (T)
Mz (Tm)

ENVOLVENTE DE ROTURA A CORTANTE

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-46.89	0.00
1	2	1.10	0.00	-40.48	48.05
2	2	1.10	0.00	-40.48	48.05
2	3	2.20	0.00	-36.00	90.12
3	3	2.20	0.00	-36.00	90.12
3	4	3.30	0.00	-31.50	127.24
4	4	3.30	0.00	-31.50	127.24
4	5	4.40	0.00	-27.02	159.43
5	5	4.40	0.00	-27.02	159.43
5	6	5.50	0.00	-22.53	186.68
6	6	5.50	0.00	-22.53	186.68
6	7	6.60	0.00	-18.04	209.00
7	7	6.60	0.00	-18.04	209.00
7	8	7.70	0.00	-13.56	226.38
8	8	7.70	0.00	-13.56	226.38
8	9	8.80	0.00	-9.06	238.81
9	9	8.80	0.00	-9.06	238.81
9	10	9.90	0.00	-4.58	246.31
10	10	9.90	0.00	-4.58	246.31
10	11	11.00	0.00	-0.09	248.88
11	11	11.00	0.00	-0.09	248.88
11	12	12.10	0.00	5.94	332.79
12	12	12.10	0.00	5.94	332.79
12	13	13.20	0.00	11.99	322.92
13	13	13.20	0.00	11.99	322.92
13	14	14.30	0.00	18.06	306.41
14	14	14.30	0.00	18.06	306.41
14	15	15.40	0.00	24.11	283.22
15	15	15.40	0.00	24.11	283.22
15	16	16.50	0.00	30.17	253.34
16	16	16.50	0.00	30.17	253.34
16	17	17.60	0.00	36.23	216.82
17	17	17.60	0.00	36.23	216.82
17	18	18.70	0.00	42.28	173.64
18	18	18.70	0.00	42.28	173.64
18	19	19.80	0.00	48.36	123.80
19	19	19.80	0.00	48.36	123.80
19	20	20.90	0.00	54.41	67.26
20	20	20.90	0.00	54.41	67.26
20	21	22.00	0.00	67.89	0.00
21	1021	22.00	0.00	-64.12	0.00
21	22	23.40	0.00	-51.41	80.87
22	22	23.40	0.00	-51.41	80.87
22	23	24.80	0.00	-45.69	148.85
23	23	24.80	0.00	-45.69	148.85
23	24	26.20	0.00	-39.99	208.82
24	24	26.20	0.00	-39.99	208.82
24	25	27.60	0.00	-34.27	260.80
25	25	27.60	0.00	-34.27	260.80
25	26	29.00	0.00	-28.56	304.78
26	26	29.00	0.00	-28.56	304.78

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-22.85	340.77
27	27	30.40	0.00	-22.85	340.77
27	28	31.80	0.00	-17.13	368.75
28	28	31.80	0.00	-17.13	368.75
28	29	33.20	0.00	-11.43	388.75
29	29	33.20	0.00	-11.43	388.75
29	30	34.60	0.00	-5.71	400.74
30	30	34.60	0.00	-5.71	400.74
30	31	36.00	0.00	0.00	404.74
31	31	36.00	0.00	0.00	404.74
31	32	37.40	0.00	7.71	541.00
32	32	37.40	0.00	7.71	541.00
32	33	38.80	0.00	15.43	524.81
33	33	38.80	0.00	15.43	524.81
33	34	40.20	0.00	23.13	497.81
34	34	40.20	0.00	23.13	497.81
34	35	41.60	0.00	30.85	460.04
35	35	41.60	0.00	30.85	460.04
35	36	43.00	0.00	38.56	411.45
36	36	43.00	0.00	38.56	411.45
36	37	44.40	0.00	46.26	352.08
37	37	44.40	0.00	46.26	352.08
37	38	45.80	0.00	53.99	281.91
38	38	45.80	0.00	53.99	281.91
38	39	47.20	0.00	61.68	200.95
39	39	47.20	0.00	61.68	200.95
39	40	48.60	0.00	69.40	109.17
40	40	48.60	0.00	69.40	109.17
40	41	50.00	0.00	86.56	0.00
41	1041	50.00	0.00	-64.12	0.00
41	42	51.40	0.00	-51.41	80.87
42	42	51.40	0.00	-51.41	80.87
42	43	52.80	0.00	-45.69	148.85
43	43	52.80	0.00	-45.69	148.85
43	44	54.20	0.00	-39.99	208.82
44	44	54.20	0.00	-39.99	208.82
44	45	55.60	0.00	-34.27	260.80
45	45	55.60	0.00	-34.27	260.80
45	46	57.00	0.00	-28.56	304.78
46	46	57.00	0.00	-28.56	304.78
46	47	58.40	0.00	-22.85	340.77
47	47	58.40	0.00	-22.85	340.77
47	48	59.80	0.00	-17.13	368.75
48	48	59.80	0.00	-17.13	368.75
48	49	61.20	0.00	-11.43	388.75
49	49	61.20	0.00	-11.43	388.75
49	50	62.60	0.00	-5.71	400.74
50	50	62.60	0.00	-5.71	400.74
50	51	64.00	0.00	0.00	404.74
51	51	64.00	0.00	0.00	404.74
51	52	65.40	0.00	7.71	541.00

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F2.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	7.71	541.00
52	53	66.80	0.00	15.43	524.81
53	53	66.80	0.00	15.43	524.81
53	54	68.20	0.00	23.13	497.81
54	54	68.20	0.00	23.13	497.81
54	55	69.60	0.00	30.85	460.04
55	55	69.60	0.00	30.85	460.04
55	56	71.00	0.00	38.56	411.45
56	56	71.00	0.00	38.56	411.45
56	57	72.40	0.00	46.26	352.08
57	57	72.40	0.00	46.26	352.08
57	58	73.80	0.00	53.99	281.91
58	58	73.80	0.00	53.99	281.91
58	59	75.20	0.00	61.68	200.95
59	59	75.20	0.00	61.68	200.95
59	60	76.60	0.00	69.40	109.17
60	60	76.60	0.00	69.40	109.17
60	61	78.00	0.00	86.56	0.00
61	1061	78.00	0.00	-50.29	0.00
61	62	79.10	0.00	-40.30	49.82
62	62	79.10	0.00	-40.30	49.82
62	63	80.20	0.00	-35.82	91.70
63	63	80.20	0.00	-35.82	91.70
63	64	81.30	0.00	-31.32	128.62
64	64	81.30	0.00	-31.32	128.62
64	65	82.40	0.00	-26.84	160.61
65	65	82.40	0.00	-26.84	160.61
65	66	83.50	0.00	-22.35	187.66
66	66	83.50	0.00	-22.35	187.66
66	67	84.60	0.00	-17.86	209.79
67	67	84.60	0.00	-17.86	209.79
67	68	85.70	0.00	-13.38	226.97
68	68	85.70	0.00	-13.38	226.97
68	69	86.80	0.00	-8.88	239.20
69	69	86.80	0.00	-8.88	239.20
69	70	87.90	0.00	-4.40	246.51
70	70	87.90	0.00	-4.40	246.51
70	71	89.00	0.00	0.12	314.39
71	71	89.00	0.00	0.12	314.39
71	72	90.10	0.00	6.18	332.52
72	72	90.10	0.00	6.18	332.52
72	73	91.20	0.00	12.23	322.39
73	73	91.20	0.00	12.23	322.39
73	74	92.30	0.00	18.31	305.61
74	74	92.30	0.00	18.31	305.61
74	75	93.40	0.00	24.35	282.15
75	75	93.40	0.00	24.35	282.15
75	76	94.50	0.00	30.42	252.02
76	76	94.50	0.00	30.42	252.02
76	77	95.60	0.00	36.48	215.23
77	77	95.60	0.00	36.48	215.23

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	42.53	171.77
78	78	96.70	0.00	42.53	171.77
78	79	97.80	0.00	48.60	121.66
79	79	97.80	0.00	48.60	121.66
79	80	98.90	0.00	54.65	64.87
80	80	98.90	0.00	54.65	64.87
80	81	100.00	0.00	63.30	0.00
101	101	0.00	0.00	-46.89	0.00
101	102	1.10	0.00	-40.48	48.05
102	102	1.10	0.00	-40.48	48.05
102	103	2.20	0.00	-36.00	90.12
103	103	2.20	0.00	-36.00	90.12
103	104	3.30	0.00	-31.50	127.24
104	104	3.30	0.00	-31.50	127.24
104	105	4.40	0.00	-27.02	159.43
105	105	4.40	0.00	-27.02	159.43
105	106	5.50	0.00	-22.53	186.68
106	106	5.50	0.00	-22.53	186.68
106	107	6.60	0.00	-18.04	209.00
107	107	6.60	0.00	-18.04	209.00
107	108	7.70	0.00	-13.56	226.38
108	108	7.70	0.00	-13.56	226.38
108	109	8.80	0.00	-9.06	238.81
109	109	8.80	0.00	-9.06	238.81
109	110	9.90	0.00	-4.58	246.31
110	110	9.90	0.00	-4.58	246.31
110	111	11.00	0.00	-0.09	248.88
111	111	11.00	0.00	-0.09	248.88
111	112	12.10	0.00	5.94	332.79
112	112	12.10	0.00	5.94	332.79
112	113	13.20	0.00	11.99	322.92
113	113	13.20	0.00	11.99	322.92
113	114	14.30	0.00	18.06	306.41
114	114	14.30	0.00	18.06	306.41
114	115	15.40	0.00	24.11	283.22
115	115	15.40	0.00	24.11	283.22
115	116	16.50	0.00	30.17	253.34
116	116	16.50	0.00	30.17	253.34
116	117	17.60	0.00	36.23	216.82
117	117	17.60	0.00	36.23	216.82
117	118	18.70	0.00	42.28	173.64
118	118	18.70	0.00	42.28	173.64
118	119	19.80	0.00	48.36	123.80
119	119	19.80	0.00	48.36	123.80
119	120	20.90	0.00	54.41	67.26
120	120	20.90	0.00	54.41	67.26
120	121	22.00	0.00	67.89	0.00
121	1121	22.00	0.00	-64.12	0.00
121	122	23.40	0.00	-51.41	80.87
122	122	23.40	0.00	-51.41	80.87
122	123	24.80	0.00	-45.69	148.85

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F2.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-45.69	148.85
123	124	26.20	0.00	-39.99	208.82
124	124	26.20	0.00	-39.99	208.82
124	125	27.60	0.00	-34.27	260.80
125	125	27.60	0.00	-34.27	260.80
125	126	29.00	0.00	-28.56	304.78
126	126	29.00	0.00	-28.56	304.78
126	127	30.40	0.00	-22.85	340.77
127	127	30.40	0.00	-22.85	340.77
127	128	31.80	0.00	-17.13	368.75
128	128	31.80	0.00	-17.13	368.75
128	129	33.20	0.00	-11.43	388.75
129	129	33.20	0.00	-11.43	388.75
129	130	34.60	0.00	-5.71	400.74
130	130	34.60	0.00	-5.71	400.74
130	131	36.00	0.00	0.00	404.74
131	131	36.00	0.00	0.00	404.74
131	132	37.40	0.00	7.71	541.00
132	132	37.40	0.00	7.71	541.00
132	133	38.80	0.00	15.43	524.81
133	133	38.80	0.00	15.43	524.81
133	134	40.20	0.00	23.13	497.81
134	134	40.20	0.00	23.13	497.81
134	135	41.60	0.00	30.85	460.04
135	135	41.60	0.00	30.85	460.04
135	136	43.00	0.00	38.56	411.45
136	136	43.00	0.00	38.56	411.45
136	137	44.40	0.00	46.26	352.08
137	137	44.40	0.00	46.26	352.08
137	138	45.80	0.00	53.99	281.91
138	138	45.80	0.00	53.99	281.91
138	139	47.20	0.00	61.68	200.95
139	139	47.20	0.00	61.68	200.95
139	140	48.60	0.00	69.40	109.17
140	140	48.60	0.00	69.40	109.17
140	141	50.00	0.00	86.56	0.00
141	1141	50.00	0.00	-64.12	0.00
141	142	51.40	0.00	-51.41	80.87
142	142	51.40	0.00	-51.41	80.87
142	143	52.80	0.00	-45.69	148.85
143	143	52.80	0.00	-45.69	148.85
143	144	54.20	0.00	-39.99	208.82
144	144	54.20	0.00	-39.99	208.82
144	145	55.60	0.00	-34.27	260.80
145	145	55.60	0.00	-34.27	260.80
145	146	57.00	0.00	-28.56	304.78
146	146	57.00	0.00	-28.56	304.78
146	147	58.40	0.00	-22.85	340.77
147	147	58.40	0.00	-22.85	340.77
147	148	59.80	0.00	-17.13	368.75
148	148	59.80	0.00	-17.13	368.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-11.43	388.75
149	149	61.20	0.00	-11.43	388.75
149	150	62.60	0.00	-5.71	400.74
150	150	62.60	0.00	-5.71	400.74
150	151	64.00	0.00	0.00	404.74
151	151	64.00	0.00	0.00	404.74
151	152	65.40	0.00	7.71	541.00
152	152	65.40	0.00	7.71	541.00
152	153	66.80	0.00	15.43	524.81
153	153	66.80	0.00	15.43	524.81
153	154	68.20	0.00	23.13	497.81
154	154	68.20	0.00	23.13	497.81
154	155	69.60	0.00	30.85	460.04
155	155	69.60	0.00	30.85	460.04
155	156	71.00	0.00	38.56	411.45
156	156	71.00	0.00	38.56	411.45
156	157	72.40	0.00	46.26	352.08
157	157	72.40	0.00	46.26	352.08
157	158	73.80	0.00	53.99	281.91
158	158	73.80	0.00	53.99	281.91
158	159	75.20	0.00	61.68	200.95
159	159	75.20	0.00	61.68	200.95
159	160	76.60	0.00	69.40	109.17
160	160	76.60	0.00	69.40	109.17
160	161	78.00	0.00	86.56	0.00
161	1161	78.00	0.00	-50.29	0.00
161	162	79.10	0.00	-40.30	49.82
162	162	79.10	0.00	-40.30	49.82
162	163	80.20	0.00	-35.82	91.70
163	163	80.20	0.00	-35.82	91.70
163	164	81.30	0.00	-31.32	128.62
164	164	81.30	0.00	-31.32	128.62
164	165	82.40	0.00	-26.84	160.61
165	165	82.40	0.00	-26.84	160.61
165	166	83.50	0.00	-22.35	187.66
166	166	83.50	0.00	-22.35	187.66
166	167	84.60	0.00	-17.86	209.79
167	167	84.60	0.00	-17.86	209.79
167	168	85.70	0.00	-13.38	226.97
168	168	85.70	0.00	-13.38	226.97
168	169	86.80	0.00	-8.88	239.20
169	169	86.80	0.00	-8.88	239.20
169	170	87.90	0.00	-4.40	246.51
170	170	87.90	0.00	-4.40	246.51
170	171	89.00	0.00	0.12	314.39
171	171	89.00	0.00	0.12	314.39
171	172	90.10	0.00	6.18	332.52
172	172	90.10	0.00	6.18	332.52
172	173	91.20	0.00	12.23	322.39
173	173	91.20	0.00	12.23	322.39
173	174	92.30	0.00	18.31	305.61

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F2.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY+

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	18.31	305.61
174	175	93.40	0.00	24.35	282.15
175	175	93.40	0.00	24.35	282.15
175	176	94.50	0.00	30.42	252.02
176	176	94.50	0.00	30.42	252.02
176	177	95.60	0.00	36.48	215.23
177	177	95.60	0.00	36.48	215.23
177	178	96.70	0.00	42.53	171.77
178	178	96.70	0.00	42.53	171.77
178	179	97.80	0.00	48.60	121.66
179	179	97.80	0.00	48.60	121.66
179	180	98.90	0.00	54.65	64.87
180	180	98.90	0.00	54.65	64.87
180	181	100.00	0.00	63.30	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-63.30	0.00
1	2	1.10	0.00	-54.65	64.87
2	2	1.10	0.00	-54.65	64.87
2	3	2.20	0.00	-48.60	121.66
3	3	2.20	0.00	-48.60	121.66
3	4	3.30	0.00	-42.53	171.77
4	4	3.30	0.00	-42.53	171.77
4	5	4.40	0.00	-36.48	215.23
5	5	4.40	0.00	-36.48	215.23
5	6	5.50	0.00	-30.42	252.02
6	6	5.50	0.00	-30.42	252.02
6	7	6.60	0.00	-24.35	282.15
7	7	6.60	0.00	-24.35	282.15
7	8	7.70	0.00	-18.31	305.61
8	8	7.70	0.00	-18.31	305.61
8	9	8.80	0.00	-12.23	322.39
9	9	8.80	0.00	-12.23	322.39
9	10	9.90	0.00	-6.18	332.52
10	10	9.90	0.00	-6.18	332.52
10	11	11.00	0.00	-0.12	314.39
11	11	11.00	0.00	-0.12	314.39
11	12	12.10	0.00	4.40	246.51
12	12	12.10	0.00	4.40	246.51
12	13	13.20	0.00	8.88	239.20
13	13	13.20	0.00	8.88	239.20
13	14	14.30	0.00	13.38	226.97
14	14	14.30	0.00	13.38	226.97
14	15	15.40	0.00	17.86	209.79
15	15	15.40	0.00	17.86	209.79
15	16	16.50	0.00	22.35	187.66
16	16	16.50	0.00	22.35	187.66
16	17	17.60	0.00	26.84	160.61
17	17	17.60	0.00	26.84	160.61
17	18	18.70	0.00	31.32	128.62
18	18	18.70	0.00	31.32	128.62
18	19	19.80	0.00	35.82	91.70
19	19	19.80	0.00	35.82	91.70
19	20	20.90	0.00	40.30	49.82
20	20	20.90	0.00	40.30	49.82
20	21	22.00	0.00	50.29	0.00
21	1021	22.00	0.00	-86.56	0.00
21	22	23.40	0.00	-69.40	109.17
22	22	23.40	0.00	-69.40	109.17
22	23	24.80	0.00	-61.68	200.95
23	23	24.80	0.00	-61.68	200.95
23	24	26.20	0.00	-53.99	281.91
24	24	26.20	0.00	-53.99	281.91
24	25	27.60	0.00	-46.26	352.08
25	25	27.60	0.00	-46.26	352.08
25	26	29.00	0.00	-38.56	411.45
26	26	29.00	0.00	-38.56	411.45

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F2.T0.VY-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-30.85	460.04
27	27	30.40	0.00	-30.85	460.04
27	28	31.80	0.00	-23.13	497.81
28	28	31.80	0.00	-23.13	497.81
28	29	33.20	0.00	-15.43	524.81
29	29	33.20	0.00	-15.43	524.81
29	30	34.60	0.00	-7.71	541.00
30	30	34.60	0.00	-7.71	541.00
30	31	36.00	0.00	0.00	404.74
31	31	36.00	0.00	0.00	404.74
31	32	37.40	0.00	5.71	400.74
32	32	37.40	0.00	5.71	400.74
32	33	38.80	0.00	11.43	388.75
33	33	38.80	0.00	11.43	388.75
33	34	40.20	0.00	17.13	368.75
34	34	40.20	0.00	17.13	368.75
34	35	41.60	0.00	22.85	340.77
35	35	41.60	0.00	22.85	340.77
35	36	43.00	0.00	28.56	304.78
36	36	43.00	0.00	28.56	304.78
36	37	44.40	0.00	34.27	260.80
37	37	44.40	0.00	34.27	260.80
37	38	45.80	0.00	39.99	208.82
38	38	45.80	0.00	39.99	208.82
38	39	47.20	0.00	45.69	148.85
39	39	47.20	0.00	45.69	148.85
39	40	48.60	0.00	51.41	80.87
40	40	48.60	0.00	51.41	80.87
40	41	50.00	0.00	64.12	0.00
41	1041	50.00	0.00	-86.56	0.00
41	42	51.40	0.00	-69.40	109.17
42	42	51.40	0.00	-69.40	109.17
42	43	52.80	0.00	-61.68	200.95
43	43	52.80	0.00	-61.68	200.95
43	44	54.20	0.00	-53.99	281.91
44	44	54.20	0.00	-53.99	281.91
44	45	55.60	0.00	-46.26	352.08
45	45	55.60	0.00	-46.26	352.08
45	46	57.00	0.00	-38.56	411.45
46	46	57.00	0.00	-38.56	411.45
46	47	58.40	0.00	-30.85	460.04
47	47	58.40	0.00	-30.85	460.04
47	48	59.80	0.00	-23.13	497.81
48	48	59.80	0.00	-23.13	497.81
48	49	61.20	0.00	-15.43	524.81
49	49	61.20	0.00	-15.43	524.81
49	50	62.60	0.00	-7.71	541.00
50	50	62.60	0.00	-7.71	541.00
50	51	64.00	0.00	0.00	404.74
51	51	64.00	0.00	0.00	404.74
51	52	65.40	0.00	5.71	400.74

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-
Construcción sin gradiente en fase constructiva 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	5.71	400.74
52	53	66.80	0.00	11.43	388.75
53	53	66.80	0.00	11.43	388.75
53	54	68.20	0.00	17.13	368.75
54	54	68.20	0.00	17.13	368.75
54	55	69.60	0.00	22.85	340.77
55	55	69.60	0.00	22.85	340.77
55	56	71.00	0.00	28.56	304.78
56	56	71.00	0.00	28.56	304.78
56	57	72.40	0.00	34.27	260.80
57	57	72.40	0.00	34.27	260.80
57	58	73.80	0.00	39.99	208.82
58	58	73.80	0.00	39.99	208.82
58	59	75.20	0.00	45.69	148.85
59	59	75.20	0.00	45.69	148.85
59	60	76.60	0.00	51.41	80.87
60	60	76.60	0.00	51.41	80.87
60	61	78.00	0.00	64.12	0.00
61	1061	78.00	0.00	-67.89	0.00
61	62	79.10	0.00	-54.41	67.26
62	62	79.10	0.00	-54.41	67.26
62	63	80.20	0.00	-48.36	123.80
63	63	80.20	0.00	-48.36	123.80
63	64	81.30	0.00	-42.28	173.64
64	64	81.30	0.00	-42.28	173.64
64	65	82.40	0.00	-36.23	216.82
65	65	82.40	0.00	-36.23	216.82
65	66	83.50	0.00	-30.17	253.34
66	66	83.50	0.00	-30.17	253.34
66	67	84.60	0.00	-24.11	283.22
67	67	84.60	0.00	-24.11	283.22
67	68	85.70	0.00	-18.06	306.41
68	68	85.70	0.00	-18.06	306.41
68	69	86.80	0.00	-11.99	322.92
69	69	86.80	0.00	-11.99	322.92
69	70	87.90	0.00	-5.94	332.79
70	70	87.90	0.00	-5.94	332.79
70	71	89.00	0.00	0.09	248.88
71	71	89.00	0.00	0.09	248.88
71	72	90.10	0.00	4.58	246.31
72	72	90.10	0.00	4.58	246.31
72	73	91.20	0.00	9.06	238.81
73	73	91.20	0.00	9.06	238.81
73	74	92.30	0.00	13.56	226.38
74	74	92.30	0.00	13.56	226.38
74	75	93.40	0.00	18.04	209.00
75	75	93.40	0.00	18.04	209.00
75	76	94.50	0.00	22.53	186.68
76	76	94.50	0.00	22.53	186.68
76	77	95.60	0.00	27.02	159.43
77	77	95.60	0.00	27.02	159.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-
Construcción sin gradiente en fase constructiva 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	31.50	127.24
78	78	96.70	0.00	31.50	127.24
78	79	97.80	0.00	36.00	90.12
79	79	97.80	0.00	36.00	90.12
79	80	98.90	0.00	40.48	48.05
80	80	98.90	0.00	40.48	48.05
80	81	100.00	0.00	46.89	0.00
101	101	0.00	0.00	-63.30	0.00
101	102	1.10	0.00	-54.65	64.87
102	102	1.10	0.00	-54.65	64.87
102	103	2.20	0.00	-48.60	121.66
103	103	2.20	0.00	-48.60	121.66
103	104	3.30	0.00	-42.53	171.77
104	104	3.30	0.00	-42.53	171.77
104	105	4.40	0.00	-36.48	215.23
105	105	4.40	0.00	-36.48	215.23
105	106	5.50	0.00	-30.42	252.02
106	106	5.50	0.00	-30.42	252.02
106	107	6.60	0.00	-24.35	282.15
107	107	6.60	0.00	-24.35	282.15
107	108	7.70	0.00	-18.31	305.61
108	108	7.70	0.00	-18.31	305.61
108	109	8.80	0.00	-12.23	322.39
109	109	8.80	0.00	-12.23	322.39
109	110	9.90	0.00	-6.18	332.52
110	110	9.90	0.00	-6.18	332.52
110	111	11.00	0.00	-0.12	314.39
111	111	11.00	0.00	-0.12	314.39
111	112	12.10	0.00	4.40	246.51
112	112	12.10	0.00	4.40	246.51
112	113	13.20	0.00	8.88	239.20
113	113	13.20	0.00	8.88	239.20
113	114	14.30	0.00	13.38	226.97
114	114	14.30	0.00	13.38	226.97
114	115	15.40	0.00	17.86	209.79
115	115	15.40	0.00	17.86	209.79
115	116	16.50	0.00	22.35	187.66
116	116	16.50	0.00	22.35	187.66
116	117	17.60	0.00	26.84	160.61
117	117	17.60	0.00	26.84	160.61
117	118	18.70	0.00	31.32	128.62
118	118	18.70	0.00	31.32	128.62
118	119	19.80	0.00	35.82	91.70
119	119	19.80	0.00	35.82	91.70
119	120	20.90	0.00	40.30	49.82
120	120	20.90	0.00	40.30	49.82
120	121	22.00	0.00	50.29	0.00
121	1121	22.00	0.00	-86.56	0.00
121	122	23.40	0.00	-69.40	109.17
122	122	23.40	0.00	-69.40	109.17
122	123	24.80	0.00	-61.68	200.95

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-61.68	200.95
123	124	26.20	0.00	-53.99	281.91
124	124	26.20	0.00	-53.99	281.91
124	125	27.60	0.00	-46.26	352.08
125	125	27.60	0.00	-46.26	352.08
125	126	29.00	0.00	-38.56	411.45
126	126	29.00	0.00	-38.56	411.45
126	127	30.40	0.00	-30.85	460.04
127	127	30.40	0.00	-30.85	460.04
127	128	31.80	0.00	-23.13	497.81
128	128	31.80	0.00	-23.13	497.81
128	129	33.20	0.00	-15.43	524.81
129	129	33.20	0.00	-15.43	524.81
129	130	34.60	0.00	-7.71	541.00
130	130	34.60	0.00	-7.71	541.00
130	131	36.00	0.00	0.00	404.74
131	131	36.00	0.00	0.00	404.74
131	132	37.40	0.00	5.71	400.74
132	132	37.40	0.00	5.71	400.74
132	133	38.80	0.00	11.43	388.75
133	133	38.80	0.00	11.43	388.75
133	134	40.20	0.00	17.13	368.75
134	134	40.20	0.00	17.13	368.75
134	135	41.60	0.00	22.85	340.77
135	135	41.60	0.00	22.85	340.77
135	136	43.00	0.00	28.56	304.78
136	136	43.00	0.00	28.56	304.78
136	137	44.40	0.00	34.27	260.80
137	137	44.40	0.00	34.27	260.80
137	138	45.80	0.00	39.99	208.82
138	138	45.80	0.00	39.99	208.82
138	139	47.20	0.00	45.69	148.85
139	139	47.20	0.00	45.69	148.85
139	140	48.60	0.00	51.41	80.87
140	140	48.60	0.00	51.41	80.87
140	141	50.00	0.00	64.12	0.00
141	1141	50.00	0.00	-86.56	0.00
141	142	51.40	0.00	-69.40	109.17
142	142	51.40	0.00	-69.40	109.17
142	143	52.80	0.00	-61.68	200.95
143	143	52.80	0.00	-61.68	200.95
143	144	54.20	0.00	-53.99	281.91
144	144	54.20	0.00	-53.99	281.91
144	145	55.60	0.00	-46.26	352.08
145	145	55.60	0.00	-46.26	352.08
145	146	57.00	0.00	-38.56	411.45
146	146	57.00	0.00	-38.56	411.45
146	147	58.40	0.00	-30.85	460.04
147	147	58.40	0.00	-30.85	460.04
147	148	59.80	0.00	-23.13	497.81
148	148	59.80	0.00	-23.13	497.81

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-15.43	524.81
149	149	61.20	0.00	-15.43	524.81
149	150	62.60	0.00	-7.71	541.00
150	150	62.60	0.00	-7.71	541.00
150	151	64.00	0.00	0.00	404.74
151	151	64.00	0.00	0.00	404.74
151	152	65.40	0.00	5.71	400.74
152	152	65.40	0.00	5.71	400.74
152	153	66.80	0.00	11.43	388.75
153	153	66.80	0.00	11.43	388.75
153	154	68.20	0.00	17.13	368.75
154	154	68.20	0.00	17.13	368.75
154	155	69.60	0.00	22.85	340.77
155	155	69.60	0.00	22.85	340.77
155	156	71.00	0.00	28.56	304.78
156	156	71.00	0.00	28.56	304.78
156	157	72.40	0.00	34.27	260.80
157	157	72.40	0.00	34.27	260.80
157	158	73.80	0.00	39.99	208.82
158	158	73.80	0.00	39.99	208.82
158	159	75.20	0.00	45.69	148.85
159	159	75.20	0.00	45.69	148.85
159	160	76.60	0.00	51.41	80.87
160	160	76.60	0.00	51.41	80.87
160	161	78.00	0.00	64.12	0.00
161	1161	78.00	0.00	-67.89	0.00
161	162	79.10	0.00	-54.41	67.26
162	162	79.10	0.00	-54.41	67.26
162	163	80.20	0.00	-48.36	123.80
163	163	80.20	0.00	-48.36	123.80
163	164	81.30	0.00	-42.28	173.64
164	164	81.30	0.00	-42.28	173.64
164	165	82.40	0.00	-36.23	216.82
165	165	82.40	0.00	-36.23	216.82
165	166	83.50	0.00	-30.17	253.34
166	166	83.50	0.00	-30.17	253.34
166	167	84.60	0.00	-24.11	283.22
167	167	84.60	0.00	-24.11	283.22
167	168	85.70	0.00	-18.06	306.41
168	168	85.70	0.00	-18.06	306.41
168	169	86.80	0.00	-11.99	322.92
169	169	86.80	0.00	-11.99	322.92
169	170	87.90	0.00	-5.94	332.79
170	170	87.90	0.00	-5.94	332.79
170	171	89.00	0.00	0.09	248.88
171	171	89.00	0.00	0.09	248.88
171	172	90.10	0.00	4.58	246.31
172	172	90.10	0.00	4.58	246.31
172	173	91.20	0.00	9.06	238.81
173	173	91.20	0.00	9.06	238.81
173	174	92.30	0.00	13.56	226.38

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F2.T0.VY-

Construcción sin gradiente en fase constructiva 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	13.56	226.38
174	175	93.40	0.00	18.04	209.00
175	175	93.40	0.00	18.04	209.00
175	176	94.50	0.00	22.53	186.68
176	176	94.50	0.00	22.53	186.68
176	177	95.60	0.00	27.02	159.43
177	177	95.60	0.00	27.02	159.43
177	178	96.70	0.00	31.50	127.24
178	178	96.70	0.00	31.50	127.24
178	179	97.80	0.00	36.00	90.12
179	179	97.80	0.00	36.00	90.12
179	180	98.90	0.00	40.48	48.05
180	180	98.90	0.00	40.48	48.05
180	181	100.00	0.00	46.89	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
1	1	0.00	-46.89	-63.30	63.30
1	2	1.10	-40.48	-54.65	54.65
2	2	1.10	-40.48	-54.65	54.65
2	3	2.20	-36.00	-48.60	48.60
3	3	2.20	-36.00	-48.60	48.60
3	4	3.30	-31.50	-42.53	42.53
4	4	3.30	-31.50	-42.53	42.53
4	5	4.40	-27.02	-36.48	36.48
5	5	4.40	-27.02	-36.48	36.48
5	6	5.50	-22.53	-30.42	30.42
6	6	5.50	-22.53	-30.42	30.42
6	7	6.60	-18.04	-24.35	24.35
7	7	6.60	-18.04	-24.35	24.35
7	8	7.70	-13.56	-18.31	18.31
8	8	7.70	-13.56	-18.31	18.31
8	9	8.80	-9.06	-12.23	12.23
9	9	8.80	-9.06	-12.23	12.23
9	10	9.90	-4.58	-6.18	6.18
10	10	9.90	-4.58	-6.18	6.18
10	11	11.00	-0.09	-0.12	0.12
11	11	11.00	-0.09	-0.12	0.12
11	12	12.10	5.94	4.40	5.94
12	12	12.10	5.94	4.40	5.94
12	13	13.20	11.99	8.88	11.99
13	13	13.20	11.99	8.88	11.99
13	14	14.30	18.06	13.38	18.06
14	14	14.30	18.06	13.38	18.06
14	15	15.40	24.11	17.86	24.11
15	15	15.40	24.11	17.86	24.11
15	16	16.50	30.17	22.35	30.17
16	16	16.50	30.17	22.35	30.17
16	17	17.60	36.23	26.84	36.23
17	17	17.60	36.23	26.84	36.23
17	18	18.70	42.28	31.32	42.28
18	18	18.70	42.28	31.32	42.28
18	19	19.80	48.36	35.82	48.36
19	19	19.80	48.36	35.82	48.36
19	20	20.90	54.41	40.30	54.41
20	20	20.90	54.41	40.30	54.41
20	21	22.00	67.89	50.29	67.89
21	1021	22.00	-64.12	-86.56	86.56
21	22	23.40	-51.41	-69.40	69.40
22	22	23.40	-51.41	-69.40	69.40
22	23	24.80	-45.69	-61.68	61.68
23	23	24.80	-45.69	-61.68	61.68
23	24	26.20	-39.99	-53.99	53.99
24	24	26.20	-39.99	-53.99	53.99
24	25	27.60	-34.27	-46.26	46.26
25	25	27.60	-34.27	-46.26	46.26
25	26	29.00	-28.56	-38.56	38.56
26	26	29.00	-28.56	-38.56	38.56

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
26	27	30.40	-22.85	-30.85	30.85
27	27	30.40	-22.85	-30.85	30.85
27	28	31.80	-17.13	-23.13	23.13
28	28	31.80	-17.13	-23.13	23.13
28	29	33.20	-11.43	-15.43	15.43
29	29	33.20	-11.43	-15.43	15.43
29	30	34.60	-5.71	-7.71	7.71
30	30	34.60	-5.71	-7.71	7.71
30	31	36.00	0.00	0.00	0.00
31	31	36.00	0.00	0.00	0.00
31	32	37.40	7.71	5.71	7.71
32	32	37.40	7.71	5.71	7.71
32	33	38.80	15.43	11.43	15.43
33	33	38.80	15.43	11.43	15.43
33	34	40.20	23.13	17.13	23.13
34	34	40.20	23.13	17.13	23.13
34	35	41.60	30.85	22.85	30.85
35	35	41.60	30.85	22.85	30.85
35	36	43.00	38.56	28.56	38.56
36	36	43.00	38.56	28.56	38.56
36	37	44.40	46.26	34.27	46.26
37	37	44.40	46.26	34.27	46.26
37	38	45.80	53.99	39.99	53.99
38	38	45.80	53.99	39.99	53.99
38	39	47.20	61.68	45.69	61.68
39	39	47.20	61.68	45.69	61.68
39	40	48.60	69.40	51.41	69.40
40	40	48.60	69.40	51.41	69.40
40	41	50.00	86.56	64.12	86.56
41	1041	50.00	-64.12	-86.56	86.56
41	42	51.40	-51.41	-69.40	69.40
42	42	51.40	-51.41	-69.40	69.40
42	43	52.80	-45.69	-61.68	61.68
43	43	52.80	-45.69	-61.68	61.68
43	44	54.20	-39.99	-53.99	53.99
44	44	54.20	-39.99	-53.99	53.99
44	45	55.60	-34.27	-46.26	46.26
45	45	55.60	-34.27	-46.26	46.26
45	46	57.00	-28.56	-38.56	38.56
46	46	57.00	-28.56	-38.56	38.56
46	47	58.40	-22.85	-30.85	30.85
47	47	58.40	-22.85	-30.85	30.85
47	48	59.80	-17.13	-23.13	23.13
48	48	59.80	-17.13	-23.13	23.13
48	49	61.20	-11.43	-15.43	15.43
49	49	61.20	-11.43	-15.43	15.43
49	50	62.60	-5.71	-7.71	7.71
50	50	62.60	-5.71	-7.71	7.71
50	51	64.00	0.00	0.00	0.00
51	51	64.00	0.00	0.00	0.00
51	52	65.40	7.71	5.71	7.71

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
52	52	65.40	7.71	5.71	7.71
52	53	66.80	15.43	11.43	15.43
53	53	66.80	15.43	11.43	15.43
53	54	68.20	23.13	17.13	23.13
54	54	68.20	23.13	17.13	23.13
54	55	69.60	30.85	22.85	30.85
55	55	69.60	30.85	22.85	30.85
55	56	71.00	38.56	28.56	38.56
56	56	71.00	38.56	28.56	38.56
56	57	72.40	46.26	34.27	46.26
57	57	72.40	46.26	34.27	46.26
57	58	73.80	53.99	39.99	53.99
58	58	73.80	53.99	39.99	53.99
58	59	75.20	61.68	45.69	61.68
59	59	75.20	61.68	45.69	61.68
59	60	76.60	69.40	51.41	69.40
60	60	76.60	69.40	51.41	69.40
60	61	78.00	86.56	64.12	86.56
61	1061	78.00	-50.29	-67.89	67.89
61	62	79.10	-40.30	-54.41	54.41
62	62	79.10	-40.30	-54.41	54.41
62	63	80.20	-35.82	-48.36	48.36
63	63	80.20	-35.82	-48.36	48.36
63	64	81.30	-31.32	-42.28	42.28
64	64	81.30	-31.32	-42.28	42.28
64	65	82.40	-26.84	-36.23	36.23
65	65	82.40	-26.84	-36.23	36.23
65	66	83.50	-22.35	-30.17	30.17
66	66	83.50	-22.35	-30.17	30.17
66	67	84.60	-17.86	-24.11	24.11
67	67	84.60	-17.86	-24.11	24.11
67	68	85.70	-13.38	-18.06	18.06
68	68	85.70	-13.38	-18.06	18.06
68	69	86.80	-8.88	-11.99	11.99
69	69	86.80	-8.88	-11.99	11.99
69	70	87.90	-4.40	-5.94	5.94
70	70	87.90	-4.40	-5.94	5.94
70	71	89.00	0.12	0.09	0.12
71	71	89.00	0.12	0.09	0.12
71	72	90.10	6.18	4.58	6.18
72	72	90.10	6.18	4.58	6.18
72	73	91.20	12.23	9.06	12.23
73	73	91.20	12.23	9.06	12.23
73	74	92.30	18.31	13.56	18.31
74	74	92.30	18.31	13.56	18.31
74	75	93.40	24.35	18.04	24.35
75	75	93.40	24.35	18.04	24.35
75	76	94.50	30.42	22.53	30.42
76	76	94.50	30.42	22.53	30.42
76	77	95.60	36.48	27.02	36.48
77	77	95.60	36.48	27.02	36.48

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	42.53	31.50	42.53
78	78	96.70	42.53	31.50	42.53
78	79	97.80	48.60	36.00	48.60
79	79	97.80	48.60	36.00	48.60
79	80	98.90	54.65	40.48	54.65
80	80	98.90	54.65	40.48	54.65
80	81	100.00	63.30	46.89	63.30
101	101	0.00	-46.89	-63.30	63.30
101	102	1.10	-40.48	-54.65	54.65
102	102	1.10	-40.48	-54.65	54.65
102	103	2.20	-36.00	-48.60	48.60
103	103	2.20	-36.00	-48.60	48.60
103	104	3.30	-31.50	-42.53	42.53
104	104	3.30	-31.50	-42.53	42.53
104	105	4.40	-27.02	-36.48	36.48
105	105	4.40	-27.02	-36.48	36.48
105	106	5.50	-22.53	-30.42	30.42
106	106	5.50	-22.53	-30.42	30.42
106	107	6.60	-18.04	-24.35	24.35
107	107	6.60	-18.04	-24.35	24.35
107	108	7.70	-13.56	-18.31	18.31
108	108	7.70	-13.56	-18.31	18.31
108	109	8.80	-9.06	-12.23	12.23
109	109	8.80	-9.06	-12.23	12.23
109	110	9.90	-4.58	-6.18	6.18
110	110	9.90	-4.58	-6.18	6.18
110	111	11.00	-0.09	-0.12	0.12
111	111	11.00	-0.09	-0.12	0.12
111	112	12.10	5.94	4.40	5.94
112	112	12.10	5.94	4.40	5.94
112	113	13.20	11.99	8.88	11.99
113	113	13.20	11.99	8.88	11.99
113	114	14.30	18.06	13.38	18.06
114	114	14.30	18.06	13.38	18.06
114	115	15.40	24.11	17.86	24.11
115	115	15.40	24.11	17.86	24.11
115	116	16.50	30.17	22.35	30.17
116	116	16.50	30.17	22.35	30.17
116	117	17.60	36.23	26.84	36.23
117	117	17.60	36.23	26.84	36.23
117	118	18.70	42.28	31.32	42.28
118	118	18.70	42.28	31.32	42.28
118	119	19.80	48.36	35.82	48.36
119	119	19.80	48.36	35.82	48.36
119	120	20.90	54.41	40.30	54.41
120	120	20.90	54.41	40.30	54.41
120	121	22.00	67.89	50.29	67.89
121	1121	22.00	-64.12	-86.56	86.56
121	122	23.40	-51.41	-69.40	69.40
122	122	23.40	-51.41	-69.40	69.40
122	123	24.80	-45.69	-61.68	61.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
123	123	24.80	-45.69	-61.68	61.68
123	124	26.20	-39.99	-53.99	53.99
124	124	26.20	-39.99	-53.99	53.99
124	125	27.60	-34.27	-46.26	46.26
125	125	27.60	-34.27	-46.26	46.26
125	126	29.00	-28.56	-38.56	38.56
126	126	29.00	-28.56	-38.56	38.56
126	127	30.40	-22.85	-30.85	30.85
127	127	30.40	-22.85	-30.85	30.85
127	128	31.80	-17.13	-23.13	23.13
128	128	31.80	-17.13	-23.13	23.13
128	129	33.20	-11.43	-15.43	15.43
129	129	33.20	-11.43	-15.43	15.43
129	130	34.60	-5.71	-7.71	7.71
130	130	34.60	-5.71	-7.71	7.71
130	131	36.00	0.00	0.00	0.00
131	131	36.00	0.00	0.00	0.00
131	132	37.40	7.71	5.71	7.71
132	132	37.40	7.71	5.71	7.71
132	133	38.80	15.43	11.43	15.43
133	133	38.80	15.43	11.43	15.43
133	134	40.20	23.13	17.13	23.13
134	134	40.20	23.13	17.13	23.13
134	135	41.60	30.85	22.85	30.85
135	135	41.60	30.85	22.85	30.85
135	136	43.00	38.56	28.56	38.56
136	136	43.00	38.56	28.56	38.56
136	137	44.40	46.26	34.27	46.26
137	137	44.40	46.26	34.27	46.26
137	138	45.80	53.99	39.99	53.99
138	138	45.80	53.99	39.99	53.99
138	139	47.20	61.68	45.69	61.68
139	139	47.20	61.68	45.69	61.68
139	140	48.60	69.40	51.41	69.40
140	140	48.60	69.40	51.41	69.40
140	141	50.00	86.56	64.12	86.56
141	1141	50.00	-64.12	-86.56	86.56
141	142	51.40	-51.41	-69.40	69.40
142	142	51.40	-51.41	-69.40	69.40
142	143	52.80	-45.69	-61.68	61.68
143	143	52.80	-45.69	-61.68	61.68
143	144	54.20	-39.99	-53.99	53.99
144	144	54.20	-39.99	-53.99	53.99
144	145	55.60	-34.27	-46.26	46.26
145	145	55.60	-34.27	-46.26	46.26
145	146	57.00	-28.56	-38.56	38.56
146	146	57.00	-28.56	-38.56	38.56
146	147	58.40	-22.85	-30.85	30.85
147	147	58.40	-22.85	-30.85	30.85
147	148	59.80	-17.13	-23.13	23.13
148	148	59.80	-17.13	-23.13	23.13

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
148	149	61.20	-11.43	-15.43	15.43
149	149	61.20	-11.43	-15.43	15.43
149	150	62.60	-5.71	-7.71	7.71
150	150	62.60	-5.71	-7.71	7.71
150	151	64.00	0.00	0.00	0.00
151	151	64.00	0.00	0.00	0.00
151	152	65.40	7.71	5.71	7.71
152	152	65.40	7.71	5.71	7.71
152	153	66.80	15.43	11.43	15.43
153	153	66.80	15.43	11.43	15.43
153	154	68.20	23.13	17.13	23.13
154	154	68.20	23.13	17.13	23.13
154	155	69.60	30.85	22.85	30.85
155	155	69.60	30.85	22.85	30.85
155	156	71.00	38.56	28.56	38.56
156	156	71.00	38.56	28.56	38.56
156	157	72.40	46.26	34.27	46.26
157	157	72.40	46.26	34.27	46.26
157	158	73.80	53.99	39.99	53.99
158	158	73.80	53.99	39.99	53.99
158	159	75.20	61.68	45.69	61.68
159	159	75.20	61.68	45.69	61.68
159	160	76.60	69.40	51.41	69.40
160	160	76.60	69.40	51.41	69.40
160	161	78.00	86.56	64.12	86.56
161	1161	78.00	-50.29	-67.89	67.89
161	162	79.10	-40.30	-54.41	54.41
162	162	79.10	-40.30	-54.41	54.41
162	163	80.20	-35.82	-48.36	48.36
163	163	80.20	-35.82	-48.36	48.36
163	164	81.30	-31.32	-42.28	42.28
164	164	81.30	-31.32	-42.28	42.28
164	165	82.40	-26.84	-36.23	36.23
165	165	82.40	-26.84	-36.23	36.23
165	166	83.50	-22.35	-30.17	30.17
166	166	83.50	-22.35	-30.17	30.17
166	167	84.60	-17.86	-24.11	24.11
167	167	84.60	-17.86	-24.11	24.11
167	168	85.70	-13.38	-18.06	18.06
168	168	85.70	-13.38	-18.06	18.06
168	169	86.80	-8.88	-11.99	11.99
169	169	86.80	-8.88	-11.99	11.99
169	170	87.90	-4.40	-5.94	5.94
170	170	87.90	-4.40	-5.94	5.94
170	171	89.00	0.12	0.09	0.12
171	171	89.00	0.12	0.09	0.12
171	172	90.10	6.18	4.58	6.18
172	172	90.10	6.18	4.58	6.18
172	173	91.20	12.23	9.06	12.23
173	173	91.20	12.23	9.06	12.23
173	174	92.30	18.31	13.56	18.31

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
ENVOLVENTE FASE 2

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
174	174	92.30	18.31	13.56	18.31
174	175	93.40	24.35	18.04	24.35
175	175	93.40	24.35	18.04	24.35
175	176	94.50	30.42	22.53	30.42
176	176	94.50	30.42	22.53	30.42
176	177	95.60	36.48	27.02	36.48
177	177	95.60	36.48	27.02	36.48
177	178	96.70	42.53	31.50	42.53
178	178	96.70	42.53	31.50	42.53
178	179	97.80	48.60	36.00	48.60
179	179	97.80	48.60	36.00	48.60
179	180	98.90	54.65	40.48	54.65
180	180	98.90	54.65	40.48	54.65
180	181	100.00	63.30	46.89	63.30

CÁLCULO TENSIONAL

Hipótesis de cálculo:

CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-47.66	0.00
1	2	1.10	0.00	-41.25	48.90
2	2	1.10	0.00	-41.25	48.90
2	3	2.20	0.00	-36.77	91.81
3	3	2.20	0.00	-36.77	91.81
3	4	3.30	0.00	-32.27	129.78
4	4	3.30	0.00	-32.27	129.78
4	5	4.40	0.00	-27.79	162.81
5	5	4.40	0.00	-27.79	162.81
5	6	5.50	0.00	-23.30	190.91
6	6	5.50	0.00	-23.30	190.91
6	7	6.60	0.00	-18.81	214.08
7	7	6.60	0.00	-18.81	214.08
7	8	7.70	0.00	-14.33	232.30
8	8	7.70	0.00	-14.33	232.30
8	9	8.80	0.00	-9.83	245.58
9	9	8.80	0.00	-9.83	245.58
9	10	9.90	0.00	-5.35	253.93
10	10	9.90	0.00	-5.35	253.93
10	11	11.00	0.00	-0.86	257.34
11	11	11.00	0.00	-0.86	257.34
11	12	12.10	0.00	5.17	342.10
12	12	12.10	0.00	5.17	342.10
12	13	13.20	0.00	11.22	333.07
13	13	13.20	0.00	11.22	333.07
13	14	14.30	0.00	17.29	317.41
14	14	14.30	0.00	17.29	317.41
14	15	15.40	0.00	23.34	295.07
15	15	15.40	0.00	23.34	295.07
15	16	16.50	0.00	35.90	266.76
16	16	16.50	0.00	35.90	266.76
16	17	17.60	0.00	48.71	220.24
17	17	17.60	0.00	48.71	220.24
17	18	18.70	0.00	61.52	159.61
18	18	18.70	0.00	61.52	159.61
18	19	19.80	0.00	74.34	84.90
19	19	19.80	0.00	74.34	84.90
19	20	20.90	0.00	87.16	-3.94
20	20	20.90	0.00	87.16	-3.94
20	21	22.00	0.00	107.39	-110.94
21	1021	22.00	0.00	-95.38	-82.18
21	22	23.40	0.00	-76.30	38.00
22	22	23.40	0.00	-76.30	38.00
22	23	24.80	0.00	-64.21	136.38
23	23	24.80	0.00	-64.21	136.38
23	24	26.20	0.00	-52.14	217.82
24	24	26.20	0.00	-52.14	217.82
24	25	27.60	0.00	-40.05	282.36
25	25	27.60	0.00	-40.05	282.36
25	26	29.00	0.00	-27.76	338.80
26	26	29.00	0.00	-27.76	338.80

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F3.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:

CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-22.05	373.68
27	27	30.40	0.00	-22.05	373.68
27	28	31.80	0.00	-16.33	400.54
28	28	31.80	0.00	-16.33	400.54
28	29	33.20	0.00	-10.63	419.44
29	29	33.20	0.00	-10.63	419.44
29	30	34.60	0.00	-4.91	430.32
30	30	34.60	0.00	-4.91	430.32
30	31	36.00	0.00	0.80	433.21
31	31	36.00	0.00	0.80	433.21
31	32	37.40	0.00	8.51	568.36
32	32	37.40	0.00	8.51	568.36
32	33	38.80	0.00	16.23	551.07
33	33	38.80	0.00	16.23	551.07
33	34	40.20	0.00	23.92	522.96
34	34	40.20	0.00	23.92	522.96
34	35	41.60	0.00	31.64	484.08
35	35	41.60	0.00	31.64	484.08
35	36	43.00	0.00	39.35	434.39
36	36	43.00	0.00	39.35	434.39
36	37	44.40	0.00	55.66	367.89
37	37	44.40	0.00	55.66	367.89
37	38	45.80	0.00	71.98	278.55
38	38	45.80	0.00	71.98	278.55
38	39	47.20	0.00	88.28	166.39
39	39	47.20	0.00	88.28	166.39
39	40	48.60	0.00	104.60	31.36
40	40	48.60	0.00	104.60	31.36
40	41	50.00	0.00	130.36	-133.10
41	1041	50.00	0.00	-96.56	-98.59
41	42	51.40	0.00	-77.48	23.23
42	42	51.40	0.00	-77.48	23.23
42	43	52.80	0.00	-65.39	123.25
43	43	52.80	0.00	-65.39	123.25
43	44	54.20	0.00	-53.32	206.33
44	44	54.20	0.00	-53.32	206.33
44	45	55.60	0.00	-41.23	272.51
45	45	55.60	0.00	-41.23	272.51
45	46	57.00	0.00	-29.15	321.77
46	46	57.00	0.00	-29.15	321.77
46	47	58.40	0.00	-23.44	358.58
47	47	58.40	0.00	-23.44	358.58
47	48	59.80	0.00	-17.72	387.38
48	48	59.80	0.00	-17.72	387.38
48	49	61.20	0.00	-12.02	408.20
49	49	61.20	0.00	-12.02	408.20
49	50	62.60	0.00	-6.30	421.01
50	50	62.60	0.00	-6.30	421.01
50	51	64.00	0.00	-0.59	425.83
51	51	64.00	0.00	-0.59	425.83
51	52	65.40	0.00	7.12	562.91

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	7.12	562.91
52	53	66.80	0.00	14.84	547.54
53	53	66.80	0.00	14.84	547.54
53	54	68.20	0.00	22.54	521.36
54	54	68.20	0.00	22.54	521.36
54	55	69.60	0.00	30.26	484.42
55	55	69.60	0.00	30.26	484.42
55	56	71.00	0.00	37.97	436.65
56	56	71.00	0.00	37.97	436.65
56	57	72.40	0.00	54.07	381.19
57	57	72.40	0.00	54.07	381.19
57	58	73.80	0.00	70.39	294.06
58	58	73.80	0.00	70.39	294.06
58	59	75.20	0.00	86.68	184.11
59	59	75.20	0.00	86.68	184.11
59	60	76.60	0.00	103.01	51.30
60	60	76.60	0.00	103.01	51.30
60	61	78.00	0.00	128.76	-110.94
61	1061	78.00	0.00	-79.55	-82.18
61	62	79.10	0.00	-64.56	-2.92
62	62	79.10	0.00	-64.56	-2.92
62	63	80.20	0.00	-55.07	62.89
63	63	80.20	0.00	-55.07	62.89
63	64	81.30	0.00	-45.57	118.23
64	64	81.30	0.00	-45.57	118.23
64	65	82.40	0.00	-36.08	163.14
65	65	82.40	0.00	-36.08	163.14
65	66	83.50	0.00	-26.59	197.60
66	66	83.50	0.00	-26.59	197.60
66	67	84.60	0.00	-16.82	225.79
67	67	84.60	0.00	-16.82	225.79
67	68	85.70	0.00	-12.34	241.82
68	68	85.70	0.00	-12.34	241.82
68	69	86.80	0.00	-7.84	252.90
69	69	86.80	0.00	-7.84	252.90
69	70	87.90	0.00	-3.36	259.08
70	70	87.90	0.00	-3.36	259.08
70	71	89.00	0.00	1.16	325.81
71	71	89.00	0.00	1.16	325.81
71	72	90.10	0.00	7.22	342.81
72	72	90.10	0.00	7.22	342.81
72	73	91.20	0.00	13.27	331.53
73	73	91.20	0.00	13.27	331.53
73	74	92.30	0.00	19.35	313.61
74	74	92.30	0.00	19.35	313.61
74	75	93.40	0.00	25.39	289.01
75	75	93.40	0.00	25.39	289.01
75	76	94.50	0.00	31.46	257.73
76	76	94.50	0.00	31.46	257.73
76	77	95.60	0.00	37.52	219.79
77	77	95.60	0.00	37.52	219.79

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	43.56	175.20
78	78	96.70	0.00	43.56	175.20
78	79	97.80	0.00	49.64	123.94
79	79	97.80	0.00	49.64	123.94
79	80	98.90	0.00	55.69	66.02
80	80	98.90	0.00	55.69	66.02
80	81	100.00	0.00	64.34	0.00
101	101	0.00	0.00	-47.66	0.00
101	102	1.10	0.00	-41.25	48.90
102	102	1.10	0.00	-41.25	48.90
102	103	2.20	0.00	-36.77	91.81
103	103	2.20	0.00	-36.77	91.81
103	104	3.30	0.00	-32.27	129.78
104	104	3.30	0.00	-32.27	129.78
104	105	4.40	0.00	-27.79	162.81
105	105	4.40	0.00	-27.79	162.81
105	106	5.50	0.00	-23.30	190.91
106	106	5.50	0.00	-23.30	190.91
106	107	6.60	0.00	-18.81	214.08
107	107	6.60	0.00	-18.81	214.08
107	108	7.70	0.00	-14.33	232.30
108	108	7.70	0.00	-14.33	232.30
108	109	8.80	0.00	-9.83	245.58
109	109	8.80	0.00	-9.83	245.58
109	110	9.90	0.00	-5.35	253.93
110	110	9.90	0.00	-5.35	253.93
110	111	11.00	0.00	-0.86	257.34
111	111	11.00	0.00	-0.86	257.34
111	112	12.10	0.00	5.17	342.10
112	112	12.10	0.00	5.17	342.10
112	113	13.20	0.00	11.22	333.07
113	113	13.20	0.00	11.22	333.07
113	114	14.30	0.00	17.29	317.41
114	114	14.30	0.00	17.29	317.41
114	115	15.40	0.00	23.34	295.07
115	115	15.40	0.00	23.34	295.07
115	116	16.50	0.00	35.90	266.76
116	116	16.50	0.00	35.90	266.76
116	117	17.60	0.00	48.71	220.24
117	117	17.60	0.00	48.71	220.24
117	118	18.70	0.00	61.52	159.61
118	118	18.70	0.00	61.52	159.61
118	119	19.80	0.00	74.34	84.90
119	119	19.80	0.00	74.34	84.90
119	120	20.90	0.00	87.16	-3.94
120	120	20.90	0.00	87.16	-3.94
120	121	22.00	0.00	107.39	-110.94
121	1121	22.00	0.00	-95.38	-82.18
121	122	23.40	0.00	-76.30	38.00
122	122	23.40	0.00	-76.30	38.00
122	123	24.80	0.00	-64.21	136.38

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-64.21	136.38
123	124	26.20	0.00	-52.14	217.82
124	124	26.20	0.00	-52.14	217.82
124	125	27.60	0.00	-40.05	282.36
125	125	27.60	0.00	-40.05	282.36
125	126	29.00	0.00	-27.76	338.80
126	126	29.00	0.00	-27.76	338.80
126	127	30.40	0.00	-22.05	373.68
127	127	30.40	0.00	-22.05	373.68
127	128	31.80	0.00	-16.33	400.54
128	128	31.80	0.00	-16.33	400.54
128	129	33.20	0.00	-10.63	419.44
129	129	33.20	0.00	-10.63	419.44
129	130	34.60	0.00	-4.91	430.32
130	130	34.60	0.00	-4.91	430.32
130	131	36.00	0.00	0.80	433.21
131	131	36.00	0.00	0.80	433.21
131	132	37.40	0.00	8.51	568.36
132	132	37.40	0.00	8.51	568.36
132	133	38.80	0.00	16.23	551.07
133	133	38.80	0.00	16.23	551.07
133	134	40.20	0.00	23.92	522.96
134	134	40.20	0.00	23.92	522.96
134	135	41.60	0.00	31.64	484.08
135	135	41.60	0.00	31.64	484.08
135	136	43.00	0.00	39.35	434.39
136	136	43.00	0.00	39.35	434.39
136	137	44.40	0.00	55.66	367.89
137	137	44.40	0.00	55.66	367.89
137	138	45.80	0.00	71.98	278.55
138	138	45.80	0.00	71.98	278.55
138	139	47.20	0.00	88.28	166.39
139	139	47.20	0.00	88.28	166.39
139	140	48.60	0.00	104.60	31.36
140	140	48.60	0.00	104.60	31.36
140	141	50.00	0.00	130.36	-133.10
141	1141	50.00	0.00	-96.56	-98.59
141	142	51.40	0.00	-77.48	23.23
142	142	51.40	0.00	-77.48	23.23
142	143	52.80	0.00	-65.39	123.25
143	143	52.80	0.00	-65.39	123.25
143	144	54.20	0.00	-53.32	206.33
144	144	54.20	0.00	-53.32	206.33
144	145	55.60	0.00	-41.23	272.51
145	145	55.60	0.00	-41.23	272.51
145	146	57.00	0.00	-29.15	321.77
146	146	57.00	0.00	-29.15	321.77
146	147	58.40	0.00	-23.44	358.58
147	147	58.40	0.00	-23.44	358.58
147	148	59.80	0.00	-17.72	387.38
148	148	59.80	0.00	-17.72	387.38

Cortante secc simple.xls Programa DINTEL PACADAR S.A. 09/09/03
CONST1.F3.T0.VY+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-12.02	408.20
149	149	61.20	0.00	-12.02	408.20
149	150	62.60	0.00	-6.30	421.01
150	150	62.60	0.00	-6.30	421.01
150	151	64.00	0.00	-0.59	425.83
151	151	64.00	0.00	-0.59	425.83
151	152	65.40	0.00	7.12	562.91
152	152	65.40	0.00	7.12	562.91
152	153	66.80	0.00	14.84	547.54
153	153	66.80	0.00	14.84	547.54
153	154	68.20	0.00	22.54	521.36
154	154	68.20	0.00	22.54	521.36
154	155	69.60	0.00	30.26	484.42
155	155	69.60	0.00	30.26	484.42
155	156	71.00	0.00	37.97	436.65
156	156	71.00	0.00	37.97	436.65
156	157	72.40	0.00	54.07	381.19
157	157	72.40	0.00	54.07	381.19
157	158	73.80	0.00	70.39	294.06
158	158	73.80	0.00	70.39	294.06
158	159	75.20	0.00	86.68	184.11
159	159	75.20	0.00	86.68	184.11
159	160	76.60	0.00	103.01	51.30
160	160	76.60	0.00	103.01	51.30
160	161	78.00	0.00	128.76	-110.94
161	1161	78.00	0.00	-79.55	-82.18
161	162	79.10	0.00	-64.56	-2.92
162	162	79.10	0.00	-64.56	-2.92
162	163	80.20	0.00	-55.07	62.89
163	163	80.20	0.00	-55.07	62.89
163	164	81.30	0.00	-45.57	118.23
164	164	81.30	0.00	-45.57	118.23
164	165	82.40	0.00	-36.08	163.14
165	165	82.40	0.00	-36.08	163.14
165	166	83.50	0.00	-26.59	197.60
166	166	83.50	0.00	-26.59	197.60
166	167	84.60	0.00	-16.82	225.79
167	167	84.60	0.00	-16.82	225.79
167	168	85.70	0.00	-12.34	241.82
168	168	85.70	0.00	-12.34	241.82
168	169	86.80	0.00	-7.84	252.90
169	169	86.80	0.00	-7.84	252.90
169	170	87.90	0.00	-3.36	259.08
170	170	87.90	0.00	-3.36	259.08
170	171	89.00	0.00	1.16	325.81
171	171	89.00	0.00	1.16	325.81
171	172	90.10	0.00	7.22	342.81
172	172	90.10	0.00	7.22	342.81
172	173	91.20	0.00	13.27	331.53
173	173	91.20	0.00	13.27	331.53
173	174	92.30	0.00	19.35	313.61

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY+

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	19.35	313.61
174	175	93.40	0.00	25.39	289.01
175	175	93.40	0.00	25.39	289.01
175	176	94.50	0.00	31.46	257.73
176	176	94.50	0.00	31.46	257.73
176	177	95.60	0.00	37.52	219.79
177	177	95.60	0.00	37.52	219.79
177	178	96.70	0.00	43.56	175.20
178	178	96.70	0.00	43.56	175.20
178	179	97.80	0.00	49.64	123.94
179	179	97.80	0.00	49.64	123.94
179	180	98.90	0.00	55.69	66.02
180	180	98.90	0.00	55.69	66.02
180	181	100.00	0.00	64.34	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-64.34	0.00
1	2	1.10	0.00	-55.69	66.02
2	2	1.10	0.00	-55.69	66.02
2	3	2.20	0.00	-49.64	123.94
3	3	2.20	0.00	-49.64	123.94
3	4	3.30	0.00	-43.56	175.20
4	4	3.30	0.00	-43.56	175.20
4	5	4.40	0.00	-37.52	219.79
5	5	4.40	0.00	-37.52	219.79
5	6	5.50	0.00	-31.46	257.73
6	6	5.50	0.00	-31.46	257.73
6	7	6.60	0.00	-25.39	289.01
7	7	6.60	0.00	-25.39	289.01
7	8	7.70	0.00	-19.35	313.61
8	8	7.70	0.00	-19.35	313.61
8	9	8.80	0.00	-13.27	331.53
9	9	8.80	0.00	-13.27	331.53
9	10	9.90	0.00	-7.22	342.81
10	10	9.90	0.00	-7.22	342.81
10	11	11.00	0.00	-1.16	325.81
11	11	11.00	0.00	-1.16	325.81
11	12	12.10	0.00	3.36	259.08
12	12	12.10	0.00	3.36	259.08
12	13	13.20	0.00	7.84	252.90
13	13	13.20	0.00	7.84	252.90
13	14	14.30	0.00	12.34	241.82
14	14	14.30	0.00	12.34	241.82
14	15	15.40	0.00	16.82	225.79
15	15	15.40	0.00	16.82	225.79
15	16	16.50	0.00	26.59	197.60
16	16	16.50	0.00	26.59	197.60
16	17	17.60	0.00	36.08	163.14
17	17	17.60	0.00	36.08	163.14
17	18	18.70	0.00	45.57	118.23
18	18	18.70	0.00	45.57	118.23
18	19	19.80	0.00	55.07	62.89
19	19	19.80	0.00	55.07	62.89
19	20	20.90	0.00	64.56	-2.92
20	20	20.90	0.00	64.56	-2.92
20	21	22.00	0.00	79.55	-82.18
21	1021	22.00	0.00	-128.76	-110.94
21	22	23.40	0.00	-103.01	51.30
22	22	23.40	0.00	-103.01	51.30
22	23	24.80	0.00	-86.68	184.11
23	23	24.80	0.00	-86.68	184.11
23	24	26.20	0.00	-70.39	294.06
24	24	26.20	0.00	-70.39	294.06
24	25	27.60	0.00	-54.07	381.19
25	25	27.60	0.00	-54.07	381.19
25	26	29.00	0.00	-37.97	436.65
26	26	29.00	0.00	-37.97	436.65

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	0.00	-30.26	484.42
27	27	30.40	0.00	-30.26	484.42
27	28	31.80	0.00	-22.54	521.36
28	28	31.80	0.00	-22.54	521.36
28	29	33.20	0.00	-14.84	547.54
29	29	33.20	0.00	-14.84	547.54
29	30	34.60	0.00	-7.12	562.91
30	30	34.60	0.00	-7.12	562.91
30	31	36.00	0.00	0.59	425.83
31	31	36.00	0.00	0.59	425.83
31	32	37.40	0.00	6.30	421.01
32	32	37.40	0.00	6.30	421.01
32	33	38.80	0.00	12.02	408.20
33	33	38.80	0.00	12.02	408.20
33	34	40.20	0.00	17.72	387.38
34	34	40.20	0.00	17.72	387.38
34	35	41.60	0.00	23.44	358.58
35	35	41.60	0.00	23.44	358.58
35	36	43.00	0.00	29.15	321.77
36	36	43.00	0.00	29.15	321.77
36	37	44.40	0.00	41.23	272.51
37	37	44.40	0.00	41.23	272.51
37	38	45.80	0.00	53.32	206.33
38	38	45.80	0.00	53.32	206.33
38	39	47.20	0.00	65.39	123.25
39	39	47.20	0.00	65.39	123.25
39	40	48.60	0.00	77.48	23.23
40	40	48.60	0.00	77.48	23.23
40	41	50.00	0.00	96.56	-98.59
41	1041	50.00	0.00	-130.36	-133.10
41	42	51.40	0.00	-104.60	31.36
42	42	51.40	0.00	-104.60	31.36
42	43	52.80	0.00	-88.28	166.39
43	43	52.80	0.00	-88.28	166.39
43	44	54.20	0.00	-71.98	278.55
44	44	54.20	0.00	-71.98	278.55
44	45	55.60	0.00	-55.66	367.89
45	45	55.60	0.00	-55.66	367.89
45	46	57.00	0.00	-39.35	434.39
46	46	57.00	0.00	-39.35	434.39
46	47	58.40	0.00	-31.64	484.08
47	47	58.40	0.00	-31.64	484.08
47	48	59.80	0.00	-23.92	522.96
48	48	59.80	0.00	-23.92	522.96
48	49	61.20	0.00	-16.23	551.07
49	49	61.20	0.00	-16.23	551.07
49	50	62.60	0.00	-8.51	568.36
50	50	62.60	0.00	-8.51	568.36
50	51	64.00	0.00	-0.80	433.21
51	51	64.00	0.00	-0.80	433.21
51	52	65.40	0.00	4.91	430.32

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	4.91	430.32
52	53	66.80	0.00	10.63	419.44
53	53	66.80	0.00	10.63	419.44
53	54	68.20	0.00	16.33	400.54
54	54	68.20	0.00	16.33	400.54
54	55	69.60	0.00	22.05	373.68
55	55	69.60	0.00	22.05	373.68
55	56	71.00	0.00	27.76	338.80
56	56	71.00	0.00	27.76	338.80
56	57	72.40	0.00	40.05	282.36
57	57	72.40	0.00	40.05	282.36
57	58	73.80	0.00	52.14	217.82
58	58	73.80	0.00	52.14	217.82
58	59	75.20	0.00	64.21	136.38
59	59	75.20	0.00	64.21	136.38
59	60	76.60	0.00	76.30	38.00
60	60	76.60	0.00	76.30	38.00
60	61	78.00	0.00	95.38	-82.18
61	1061	78.00	0.00	-107.39	-110.94
61	62	79.10	0.00	-87.16	-3.94
62	62	79.10	0.00	-87.16	-3.94
62	63	80.20	0.00	-74.34	84.90
63	63	80.20	0.00	-74.34	84.90
63	64	81.30	0.00	-61.52	159.61
64	64	81.30	0.00	-61.52	159.61
64	65	82.40	0.00	-48.71	220.24
65	65	82.40	0.00	-48.71	220.24
65	66	83.50	0.00	-35.90	266.76
66	66	83.50	0.00	-35.90	266.76
66	67	84.60	0.00	-23.34	295.07
67	67	84.60	0.00	-23.34	295.07
67	68	85.70	0.00	-17.29	317.41
68	68	85.70	0.00	-17.29	317.41
68	69	86.80	0.00	-11.22	333.07
69	69	86.80	0.00	-11.22	333.07
69	70	87.90	0.00	-5.17	342.10
70	70	87.90	0.00	-5.17	342.10
70	71	89.00	0.00	0.86	257.34
71	71	89.00	0.00	0.86	257.34
71	72	90.10	0.00	5.35	253.93
72	72	90.10	0.00	5.35	253.93
72	73	91.20	0.00	9.83	245.58
73	73	91.20	0.00	9.83	245.58
73	74	92.30	0.00	14.33	232.30
74	74	92.30	0.00	14.33	232.30
74	75	93.40	0.00	18.81	214.08
75	75	93.40	0.00	18.81	214.08
75	76	94.50	0.00	23.30	190.91
76	76	94.50	0.00	23.30	190.91
76	77	95.60	0.00	27.79	162.81
77	77	95.60	0.00	27.79	162.81

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	32.27	129.78
78	78	96.70	0.00	32.27	129.78
78	79	97.80	0.00	36.77	91.81
79	79	97.80	0.00	36.77	91.81
79	80	98.90	0.00	41.25	48.90
80	80	98.90	0.00	41.25	48.90
80	81	100.00	0.00	47.66	0.00
101	101	0.00	0.00	-64.34	0.00
101	102	1.10	0.00	-55.69	66.02
102	102	1.10	0.00	-55.69	66.02
102	103	2.20	0.00	-49.64	123.94
103	103	2.20	0.00	-49.64	123.94
103	104	3.30	0.00	-43.56	175.20
104	104	3.30	0.00	-43.56	175.20
104	105	4.40	0.00	-37.52	219.79
105	105	4.40	0.00	-37.52	219.79
105	106	5.50	0.00	-31.46	257.73
106	106	5.50	0.00	-31.46	257.73
106	107	6.60	0.00	-25.39	289.01
107	107	6.60	0.00	-25.39	289.01
107	108	7.70	0.00	-19.35	313.61
108	108	7.70	0.00	-19.35	313.61
108	109	8.80	0.00	-13.27	331.53
109	109	8.80	0.00	-13.27	331.53
109	110	9.90	0.00	-7.22	342.81
110	110	9.90	0.00	-7.22	342.81
110	111	11.00	0.00	-1.16	325.81
111	111	11.00	0.00	-1.16	325.81
111	112	12.10	0.00	3.36	259.08
112	112	12.10	0.00	3.36	259.08
112	113	13.20	0.00	7.84	252.90
113	113	13.20	0.00	7.84	252.90
113	114	14.30	0.00	12.34	241.82
114	114	14.30	0.00	12.34	241.82
114	115	15.40	0.00	16.82	225.79
115	115	15.40	0.00	16.82	225.79
115	116	16.50	0.00	26.59	197.60
116	116	16.50	0.00	26.59	197.60
116	117	17.60	0.00	36.08	163.14
117	117	17.60	0.00	36.08	163.14
117	118	18.70	0.00	45.57	118.23
118	118	18.70	0.00	45.57	118.23
118	119	19.80	0.00	55.07	62.89
119	119	19.80	0.00	55.07	62.89
119	120	20.90	0.00	64.56	-2.92
120	120	20.90	0.00	64.56	-2.92
120	121	22.00	0.00	79.55	-82.18
121	1121	22.00	0.00	-128.76	-110.94
121	122	23.40	0.00	-103.01	51.30
122	122	23.40	0.00	-103.01	51.30
122	123	24.80	0.00	-86.68	184.11

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-86.68	184.11
123	124	26.20	0.00	-70.39	294.06
124	124	26.20	0.00	-70.39	294.06
124	125	27.60	0.00	-54.07	381.19
125	125	27.60	0.00	-54.07	381.19
125	126	29.00	0.00	-37.97	436.65
126	126	29.00	0.00	-37.97	436.65
126	127	30.40	0.00	-30.26	484.42
127	127	30.40	0.00	-30.26	484.42
127	128	31.80	0.00	-22.54	521.36
128	128	31.80	0.00	-22.54	521.36
128	129	33.20	0.00	-14.84	547.54
129	129	33.20	0.00	-14.84	547.54
129	130	34.60	0.00	-7.12	562.91
130	130	34.60	0.00	-7.12	562.91
130	131	36.00	0.00	0.59	425.83
131	131	36.00	0.00	0.59	425.83
131	132	37.40	0.00	6.30	421.01
132	132	37.40	0.00	6.30	421.01
132	133	38.80	0.00	12.02	408.20
133	133	38.80	0.00	12.02	408.20
133	134	40.20	0.00	17.72	387.38
134	134	40.20	0.00	17.72	387.38
134	135	41.60	0.00	23.44	358.58
135	135	41.60	0.00	23.44	358.58
135	136	43.00	0.00	29.15	321.77
136	136	43.00	0.00	29.15	321.77
136	137	44.40	0.00	41.23	272.51
137	137	44.40	0.00	41.23	272.51
137	138	45.80	0.00	53.32	206.33
138	138	45.80	0.00	53.32	206.33
138	139	47.20	0.00	65.39	123.25
139	139	47.20	0.00	65.39	123.25
139	140	48.60	0.00	77.48	23.23
140	140	48.60	0.00	77.48	23.23
140	141	50.00	0.00	96.56	-98.59
141	1141	50.00	0.00	-130.36	-133.10
141	142	51.40	0.00	-104.60	31.36
142	142	51.40	0.00	-104.60	31.36
142	143	52.80	0.00	-88.28	166.39
143	143	52.80	0.00	-88.28	166.39
143	144	54.20	0.00	-71.98	278.55
144	144	54.20	0.00	-71.98	278.55
144	145	55.60	0.00	-55.66	367.89
145	145	55.60	0.00	-55.66	367.89
145	146	57.00	0.00	-39.35	434.39
146	146	57.00	0.00	-39.35	434.39
146	147	58.40	0.00	-31.64	484.08
147	147	58.40	0.00	-31.64	484.08
147	148	59.80	0.00	-23.92	522.96
148	148	59.80	0.00	-23.92	522.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-16.23	551.07
149	149	61.20	0.00	-16.23	551.07
149	150	62.60	0.00	-8.51	568.36
150	150	62.60	0.00	-8.51	568.36
150	151	64.00	0.00	-0.80	433.21
151	151	64.00	0.00	-0.80	433.21
151	152	65.40	0.00	4.91	430.32
152	152	65.40	0.00	4.91	430.32
152	153	66.80	0.00	10.63	419.44
153	153	66.80	0.00	10.63	419.44
153	154	68.20	0.00	16.33	400.54
154	154	68.20	0.00	16.33	400.54
154	155	69.60	0.00	22.05	373.68
155	155	69.60	0.00	22.05	373.68
155	156	71.00	0.00	27.76	338.80
156	156	71.00	0.00	27.76	338.80
156	157	72.40	0.00	40.05	282.36
157	157	72.40	0.00	40.05	282.36
157	158	73.80	0.00	52.14	217.82
158	158	73.80	0.00	52.14	217.82
158	159	75.20	0.00	64.21	136.38
159	159	75.20	0.00	64.21	136.38
159	160	76.60	0.00	76.30	38.00
160	160	76.60	0.00	76.30	38.00
160	161	78.00	0.00	95.38	-82.18
161	1161	78.00	0.00	-107.39	-110.94
161	162	79.10	0.00	-87.16	-3.94
162	162	79.10	0.00	-87.16	-3.94
162	163	80.20	0.00	-74.34	84.90
163	163	80.20	0.00	-74.34	84.90
163	164	81.30	0.00	-61.52	159.61
164	164	81.30	0.00	-61.52	159.61
164	165	82.40	0.00	-48.71	220.24
165	165	82.40	0.00	-48.71	220.24
165	166	83.50	0.00	-35.90	266.76
166	166	83.50	0.00	-35.90	266.76
166	167	84.60	0.00	-23.34	295.07
167	167	84.60	0.00	-23.34	295.07
167	168	85.70	0.00	-17.29	317.41
168	168	85.70	0.00	-17.29	317.41
168	169	86.80	0.00	-11.22	333.07
169	169	86.80	0.00	-11.22	333.07
170	170	87.90	0.00	-5.17	342.10
170	170	87.90	0.00	-5.17	342.10
171	171	89.00	0.00	0.86	257.34
171	171	89.00	0.00	0.86	257.34
172	172	90.10	0.00	5.35	253.93
172	173	90.10	0.00	5.35	253.93
173	173	90	0.00	9.83	245.58
173	174	92.	0.00	9.83	245.58
			0.00	14.33	232.30

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F3.T0.VY-

Construcción sin gradiente en fase constructiva 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	14.33	232.30
174	175	93.40	0.00	18.81	214.08
175	175	93.40	0.00	18.81	214.08
175	176	94.50	0.00	23.30	190.91
176	176	94.50	0.00	23.30	190.91
176	177	95.60	0.00	27.79	162.81
177	177	95.60	0.00	27.79	162.81
177	178	96.70	0.00	32.27	129.78
178	178	96.70	0.00	32.27	129.78
178	179	97.80	0.00	36.77	91.81
179	179	97.80	0.00	36.77	91.81
179	180	98.90	0.00	41.25	48.90
180	180	98.90	0.00	41.25	48.90
180	181	100.00	0.00	47.66	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
1	1	0.00	-47.66	-64.34	64.34
1	2	1.10	-41.25	-55.69	55.69
2	2	1.10	-41.25	-55.69	55.69
2	3	2.20	-36.77	-49.64	49.64
3	3	2.20	-36.77	-49.64	49.64
3	4	3.30	-32.27	-43.56	43.56
4	4	3.30	-32.27	-43.56	43.56
4	5	4.40	-27.79	-37.52	37.52
5	5	4.40	-27.79	-37.52	37.52
5	6	5.50	-23.30	-31.46	31.46
6	6	5.50	-23.30	-31.46	31.46
6	7	6.60	-18.81	-25.39	25.39
7	7	6.60	-18.81	-25.39	25.39
7	8	7.70	-14.33	-19.35	19.35
8	8	7.70	-14.33	-19.35	19.35
8	9	8.80	-9.83	-13.27	13.27
9	9	8.80	-9.83	-13.27	13.27
9	10	9.90	-5.35	-7.22	7.22
10	10	9.90	-5.35	-7.22	7.22
10	11	11.00	-0.86	-1.16	1.16
11	11	11.00	-0.86	-1.16	1.16
11	12	12.10	5.17	3.36	5.17
12	12	12.10	5.17	3.36	5.17
12	13	13.20	11.22	7.84	11.22
13	13	13.20	11.22	7.84	11.22
13	14	14.30	17.29	12.34	17.29
14	14	14.30	17.29	12.34	17.29
14	15	15.40	23.34	16.82	23.34
15	15	15.40	23.34	16.82	23.34
15	16	16.50	35.90	26.59	35.90
16	16	16.50	35.90	26.59	35.90
16	17	17.60	48.71	36.08	48.71
17	17	17.60	48.71	36.08	48.71
17	18	18.70	61.52	45.57	61.52
18	18	18.70	61.52	45.57	61.52
18	19	19.80	74.34	55.07	74.34
19	19	19.80	74.34	55.07	74.34
19	20	20.90	87.16	64.56	87.16
20	20	20.90	87.16	64.56	87.16
20	21	22.00	107.39	79.55	107.39
21	1021	22.00	-95.38	-128.76	128.76
21	22	23.40	-76.30	-103.01	103.01
22	22	23.40	-76.30	-103.01	103.01
22	23	24.80	-64.21	-86.68	86.68
23	23	24.80	-64.21	-86.68	86.68
23	24	26.20	-52.14	-70.39	70.39
24	24	26.20	-52.14	-70.39	70.39
24	25	27.60	-40.05	-54.07	54.07
25	25	27.60	-40.05	-54.07	54.07
25	26	29.00	-27.76	-37.97	37.97
26	26	29.00	-27.76	-37.97	37.97

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
26	27	30.40	-22.05	-30.26	30.26
27	27	30.40	-22.05	-30.26	30.26
27	28	31.80	-16.33	-22.54	22.54
28	28	31.80	-16.33	-22.54	22.54
28	29	33.20	-10.63	-14.84	14.84
29	29	33.20	-10.63	-14.84	14.84
29	30	34.60	-4.91	-7.12	7.12
30	30	34.60	-4.91	-7.12	7.12
30	31	36.00	0.80	0.59	0.80
31	31	36.00	0.80	0.59	0.80
31	32	37.40	8.51	6.30	8.51
32	32	37.40	8.51	6.30	8.51
32	33	38.80	16.23	12.02	16.23
33	33	38.80	16.23	12.02	16.23
33	34	40.20	23.92	17.72	23.92
34	34	40.20	23.92	17.72	23.92
34	35	41.60	31.64	23.44	31.64
35	35	41.60	31.64	23.44	31.64
35	36	43.00	39.35	29.15	39.35
36	36	43.00	39.35	29.15	39.35
36	37	44.40	55.66	41.23	55.66
37	37	44.40	55.66	41.23	55.66
37	38	45.80	71.98	53.32	71.98
38	38	45.80	71.98	53.32	71.98
38	39	47.20	88.28	65.39	88.28
39	39	47.20	88.28	65.39	88.28
39	40	48.60	104.60	77.48	104.60
40	40	48.60	104.60	77.48	104.60
40	41	50.00	130.36	96.56	130.36
41	1041	50.00	-96.56	-130.36	130.36
41	42	51.40	-77.48	-104.60	104.60
42	42	51.40	-77.48	-104.60	104.60
42	43	52.80	-65.39	-88.28	88.28
43	43	52.80	-65.39	-88.28	88.28
43	44	54.20	-53.32	-71.98	71.98
44	44	54.20	-53.32	-71.98	71.98
44	45	55.60	-41.23	-55.66	55.66
45	45	55.60	-41.23	-55.66	55.66
45	46	57.00	-29.15	-39.35	39.35
46	46	57.00	-29.15	-39.35	39.35
46	47	58.40	-23.44	-31.64	31.64
47	47	58.40	-23.44	-31.64	31.64
47	48	59.80	-17.72	-23.92	23.92
48	48	59.80	-17.72	-23.92	23.92
48	49	61.20	-12.02	-16.23	16.23
49	49	61.20	-12.02	-16.23	16.23
49	50	62.60	-6.30	-8.51	8.51
50	50	62.60	-6.30	-8.51	8.51
50	51	64.00	-0.59	-0.80	0.80
51	51	64.00	-0.59	-0.80	0.80
51	52	65.40	7.12	4.91	7.12

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
52	52	65.40	7.12	4.91	7.12
52	53	66.80	14.84	10.63	14.84
53	53	66.80	14.84	10.63	14.84
53	54	68.20	22.54	16.33	22.54
54	54	68.20	22.54	16.33	22.54
54	55	69.60	30.26	22.05	30.26
55	55	69.60	30.26	22.05	30.26
55	56	71.00	37.97	27.76	37.97
56	56	71.00	37.97	27.76	37.97
56	57	72.40	54.07	40.05	54.07
57	57	72.40	54.07	40.05	54.07
57	58	73.80	70.39	52.14	70.39
58	58	73.80	70.39	52.14	70.39
58	59	75.20	86.68	64.21	86.68
59	59	75.20	86.68	64.21	86.68
59	60	76.60	103.01	76.30	103.01
60	60	76.60	103.01	76.30	103.01
60	61	78.00	128.76	95.38	128.76
61	1061	78.00	-79.55	-107.39	107.39
61	62	79.10	-64.56	-87.16	87.16
62	62	79.10	-64.56	-87.16	87.16
62	63	80.20	-55.07	-74.34	74.34
63	63	80.20	-55.07	-74.34	74.34
63	64	81.30	-45.57	-61.52	61.52
64	64	81.30	-45.57	-61.52	61.52
64	65	82.40	-36.08	-48.71	48.71
65	65	82.40	-36.08	-48.71	48.71
65	66	83.50	-26.59	-35.90	35.90
66	66	83.50	-26.59	-35.90	35.90
66	67	84.60	-16.82	-23.34	23.34
67	67	84.60	-16.82	-23.34	23.34
67	68	85.70	-12.34	-17.29	17.29
68	68	85.70	-12.34	-17.29	17.29
68	69	86.80	-7.84	-11.22	11.22
69	69	86.80	-7.84	-11.22	11.22
69	70	87.90	-3.36	-5.17	5.17
70	70	87.90	-3.36	-5.17	5.17
70	71	89.00	1.16	0.86	1.16
71	71	89.00	1.16	0.86	1.16
71	72	90.10	7.22	5.35	7.22
72	72	90.10	7.22	5.35	7.22
72	73	91.20	13.27	9.83	13.27
73	73	91.20	13.27	9.83	13.27
73	74	92.30	19.35	14.33	19.35
74	74	92.30	19.35	14.33	19.35
74	75	93.40	25.39	18.81	25.39
75	75	93.40	25.39	18.81	25.39
75	76	94.50	31.46	23.30	31.46
76	76	94.50	31.46	23.30	31.46
76	77	95.60	37.52	27.79	37.52
77	77	95.60	37.52	27.79	37.52

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	43.56	32.27	43.56
78	78	96.70	43.56	32.27	43.56
78	79	97.80	49.64	36.77	49.64
79	79	97.80	49.64	36.77	49.64
79	80	98.90	55.69	41.25	55.69
80	80	98.90	55.69	41.25	55.69
80	81	100.00	64.34	47.66	64.34
101	101	0.00	-47.66	-64.34	64.34
101	102	1.10	-41.25	-55.69	55.69
102	102	1.10	-41.25	-55.69	55.69
102	103	2.20	-36.77	-49.64	49.64
103	103	2.20	-36.77	-49.64	49.64
103	104	3.30	-32.27	-43.56	43.56
104	104	3.30	-32.27	-43.56	43.56
104	105	4.40	-27.79	-37.52	37.52
105	105	4.40	-27.79	-37.52	37.52
105	106	5.50	-23.30	-31.46	31.46
106	106	5.50	-23.30	-31.46	31.46
106	107	6.60	-18.81	-25.39	25.39
107	107	6.60	-18.81	-25.39	25.39
107	108	7.70	-14.33	-19.35	19.35
108	108	7.70	-14.33	-19.35	19.35
108	109	8.80	-9.83	-13.27	13.27
109	109	8.80	-9.83	-13.27	13.27
109	110	9.90	-5.35	-7.22	7.22
110	110	9.90	-5.35	-7.22	7.22
110	111	11.00	-0.86	-1.16	1.16
111	111	11.00	-0.86	-1.16	1.16
111	112	12.10	5.17	3.36	5.17
112	112	12.10	5.17	3.36	5.17
112	113	13.20	11.22	7.84	11.22
113	113	13.20	11.22	7.84	11.22
113	114	14.30	17.29	12.34	17.29
114	114	14.30	17.29	12.34	17.29
114	115	15.40	23.34	16.82	23.34
115	115	15.40	23.34	16.82	23.34
115	116	16.50	35.90	26.59	35.90
116	116	16.50	35.90	26.59	35.90
116	117	17.60	48.71	36.08	48.71
117	117	17.60	48.71	36.08	48.71
117	118	18.70	61.52	45.57	61.52
118	118	18.70	61.52	45.57	61.52
118	119	19.80	74.34	55.07	74.34
119	119	19.80	74.34	55.07	74.34
119	120	20.90	87.16	64.56	87.16
120	120	20.90	87.16	64.56	87.16
120	121	22.00	107.39	79.55	107.39
121	1121	22.00	-95.38	-128.76	128.76
121	122	23.40	-76.30	-103.01	103.01
122	122	23.40	-76.30	-103.01	103.01
122	123	24.80	-64.21	-86.68	86.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	43.56	32.27	43.56
78	78	96.70	43.56	32.27	43.56
78	79	97.80	49.64	36.77	49.64
79	79	97.80	49.64	36.77	49.64
79	80	98.90	55.69	41.25	55.69
80	80	98.90	55.69	41.25	55.69
80	81	100.00	64.34	47.66	64.34
101	101	0.00	-47.66	-64.34	64.34
101	102	1.10	-41.25	-55.69	55.69
102	102	1.10	-41.25	-55.69	55.69
102	103	2.20	-36.77	-49.64	49.64
103	103	2.20	-36.77	-49.64	49.64
103	104	3.30	-32.27	-43.56	43.56
104	104	3.30	-32.27	-43.56	43.56
104	105	4.40	-27.79	-37.52	37.52
105	105	4.40	-27.79	-37.52	37.52
105	106	5.50	-23.30	-31.46	31.46
106	106	5.50	-23.30	-31.46	31.46
106	107	6.60	-18.81	-25.39	25.39
107	107	6.60	-18.81	-25.39	25.39
107	108	7.70	-14.33	-19.35	19.35
108	108	7.70	-14.33	-19.35	19.35
108	109	8.80	-9.83	-13.27	13.27
109	109	8.80	-9.83	-13.27	13.27
109	110	9.90	-5.35	-7.22	7.22
110	110	9.90	-5.35	-7.22	7.22
110	111	11.00	-0.86	-1.16	1.16
111	111	11.00	-0.86	-1.16	1.16
111	112	12.10	5.17	3.36	5.17
112	112	12.10	5.17	3.36	5.17
112	113	13.20	11.22	7.84	11.22
113	113	13.20	11.22	7.84	11.22
113	114	14.30	17.29	12.34	17.29
114	114	14.30	17.29	12.34	17.29
114	115	15.40	23.34	16.82	23.34
115	115	15.40	23.34	16.82	23.34
115	116	16.50	35.90	26.59	35.90
116	116	16.50	35.90	26.59	35.90
116	117	17.60	48.71	36.08	48.71
117	117	17.60	48.71	36.08	48.71
117	118	18.70	61.52	45.57	61.52
118	118	18.70	61.52	45.57	61.52
118	119	19.80	74.34	55.07	74.34
119	119	19.80	74.34	55.07	74.34
119	120	20.90	87.16	64.56	87.16
120	120	20.90	87.16	64.56	87.16
120	121	22.00	107.39	79.55	107.39
121	1121	22.00	-95.38	-128.76	128.76
121	122	23.40	-76.30	-103.01	103.01
122	122	23.40	-76.30	-103.01	103.01
122	123	24.80	-64.21	-86.68	86.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 3
ENVOLVENTE FASE 3
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
123	123	24.80	-64.21	-86.68	86.68
123	124	26.20	-52.14	-70.39	70.39
124	124	26.20	-52.14	-70.39	70.39
124	125	27.60	-40.05	-54.07	54.07
125	125	27.60	-40.05	-54.07	54.07
125	126	29.00	-27.76	-37.97	37.97
126	126	29.00	-27.76	-37.97	37.97
126	127	30.40	-22.05	-30.26	30.26
127	127	30.40	-22.05	-30.26	30.26
127	128	31.80	-16.33	-22.54	22.54
128	128	31.80	-16.33	-22.54	22.54
128	129	33.20	-10.63	-14.84	14.84
129	129	33.20	-10.63	-14.84	14.84
129	130	34.60	-4.91	-7.12	7.12
130	130	34.60	-4.91	-7.12	7.12
130	131	36.00	0.80	0.59	0.80
131	131	36.00	0.80	0.59	0.80
131	132	37.40	8.51	6.30	8.51
132	132	37.40	8.51	6.30	8.51
132	133	38.80	16.23	12.02	16.23
133	133	38.80	16.23	12.02	16.23
133	134	40.20	23.92	17.72	23.92
134	134	40.20	23.92	17.72	23.92
134	135	41.60	31.64	23.44	31.64
135	135	41.60	31.64	23.44	31.64
135	136	43.00	39.35	29.15	39.35
136	136	43.00	39.35	29.15	39.35
136	137	44.40	55.66	41.23	55.66
137	137	44.40	55.66	41.23	55.66
137	138	45.80	71.98	53.32	71.98
138	138	45.80	71.98	53.32	71.98
138	139	47.20	88.28	65.39	88.28
139	139	47.20	88.28	65.39	88.28
139	140	48.60	104.60	77.48	104.60
140	140	48.60	104.60	77.48	104.60
140	141	50.00	130.36	96.56	130.36
141	1141	50.00	-96.56	-130.36	130.36
141	142	51.40	-77.48	-104.60	104.60
142	142	51.40	-77.48	-104.60	104.60
142	143	52.80	-65.39	-88.28	88.28
143	143	52.80	-65.39	-88.28	88.28
143	144	54.20	-53.32	-71.98	71.98
144	144	54.20	-53.32	-71.98	71.98
144	145	55.60	-41.23	-55.66	55.66
145	145	55.60	-41.23	-55.66	55.66
145	146	57.00	-29.15	-39.35	39.35
146	146	57.00	-29.15	-39.35	39.35
146	147	58.40	-23.44	-31.64	31.64
147	147	58.40	-23.44	-31.64	31.64
147	148	59.80	-17.72	-23.92	23.92
148	148	59.80	-17.72	-23.92	23.92

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 3

ENVOLVENTE FASE 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
148	149	61.20	-12.02	-16.23	16.23
149	149	61.20	-12.02	-16.23	16.23
149	150	62.60	-6.30	-8.51	8.51
150	150	62.60	-6.30	-8.51	8.51
150	151	64.00	-0.59	-0.80	0.80
151	151	64.00	-0.59	-0.80	0.80
151	152	65.40	7.12	4.91	7.12
152	152	65.40	7.12	4.91	7.12
152	153	66.80	14.84	10.63	14.84
153	153	66.80	14.84	10.63	14.84
153	154	68.20	22.54	16.33	22.54
154	154	68.20	22.54	16.33	22.54
154	155	69.60	30.26	22.05	30.26
155	155	69.60	30.26	22.05	30.26
155	156	71.00	37.97	27.76	37.97
156	156	71.00	37.97	27.76	37.97
156	157	72.40	54.07	40.05	54.07
157	157	72.40	54.07	40.05	54.07
157	158	73.80	70.39	52.14	70.39
158	158	73.80	70.39	52.14	70.39
158	159	75.20	86.68	64.21	86.68
159	159	75.20	86.68	64.21	86.68
159	160	76.60	103.01	76.30	103.01
160	160	76.60	103.01	76.30	103.01
160	161	78.00	128.76	95.38	128.76
161	1161	78.00	-79.55	-107.39	107.39
161	162	79.10	-64.56	-87.16	87.16
162	162	79.10	-64.56	-87.16	87.16
162	163	80.20	-55.07	-74.34	74.34
163	163	80.20	-55.07	-74.34	74.34
163	164	81.30	-45.57	-61.52	61.52
164	164	81.30	-45.57	-61.52	61.52
164	165	82.40	-36.08	-48.71	48.71
165	165	82.40	-36.08	-48.71	48.71
165	166	83.50	-26.59	-35.90	35.90
166	166	83.50	-26.59	-35.90	35.90
166	167	84.60	-16.82	-23.34	23.34
167	167	84.60	-16.82	-23.34	23.34
167	168	85.70	-12.34	-17.29	17.29
168	168	85.70	-12.34	-17.29	17.29
168	169	86.80	-7.84	-11.22	11.22
169	169	86.80	-7.84	-11.22	11.22
169	170	87.90	-3.36	-5.17	5.17
170	170	87.90	-3.36	-5.17	5.17
170	171	89.00	1.16	0.86	1.16
171	171	89.00	1.16	0.86	1.16
171	172	90.10	7.22	5.35	7.22
172	172	90.10	7.22	5.35	7.22
172	173	91.20	13.27	9.83	13.27
173	173	91.20	13.27	9.83	13.27
173	174	92.30	19.35	14.33	19.35

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ENVOLVENTE FASE 3

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 3

ENVOLVENTE FASE 3

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
174	174	92.30	19.35	14.33	19.35
174	175	93.40	25.39	18.81	25.39
175	175	93.40	25.39	18.81	25.39
175	176	94.50	31.46	23.30	31.46
176	176	94.50	31.46	23.30	31.46
176	177	95.60	37.52	27.79	37.52
177	177	95.60	37.52	27.79	37.52
177	178	96.70	43.56	32.27	43.56
178	178	96.70	43.56	32.27	43.56
178	179	97.80	49.64	36.77	49.64
179	179	97.80	49.64	36.77	49.64
179	180	98.90	55.69	41.25	55.69
180	180	98.90	55.69	41.25	55.69
180	181	100.00	64.34	47.66	64.34

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-80.30	0.00
1	2	1.10	0.00	-68.88	82.05
2	2	1.10	0.00	-68.88	82.05
2	3	2.20	0.00	-59.40	152.60
3	3	2.20	0.00	-59.40	152.60
3	4	3.30	0.00	-49.89	212.71
4	4	3.30	0.00	-49.89	212.71
4	5	4.40	0.00	-40.41	262.37
5	5	4.40	0.00	-40.41	262.37
5	6	5.50	0.00	-30.91	301.59
6	6	5.50	0.00	-30.91	301.59
6	7	6.60	0.00	-21.42	330.38
7	7	6.60	0.00	-21.42	330.38
7	8	7.70	0.00	-11.09	389.47
8	8	7.70	0.00	-11.09	389.47
8	9	8.80	0.00	0.16	395.47
9	9	8.80	0.00	0.16	395.47
9	10	9.90	0.00	11.40	389.11
10	10	9.90	0.00	11.40	389.11
10	11	11.00	0.00	22.64	370.38
11	11	11.00	0.00	22.64	370.38
11	12	12.10	0.00	35.44	425.56
12	12	12.10	0.00	35.44	425.56
12	13	13.20	0.00	48.24	379.52
13	13	13.20	0.00	48.24	379.52
13	14	14.30	0.00	61.07	319.42
14	14	14.30	25.04	53.20	319.42
14	15	15.40	29.75	66.00	244.39
15	15	15.40	0.00	75.36	244.39
15	16	16.50	0.00	87.91	158.87
16	16	16.50	0.00	87.91	158.87
16	17	17.60	0.00	100.72	55.13
17	17	17.60	0.00	100.72	55.13
17	18	18.70	0.00	113.54	-62.72
18	18	18.70	0.00	113.54	-62.72
18	19	19.80	0.00	126.36	-194.64
19	19	19.80	0.00	126.36	-194.64
19	20	20.90	0.00	139.17	-340.71
20	20	20.90	0.00	139.17	-340.71
20	21	22.00	0.00	159.41	-504.93
21	1021	22.00	0.00	-129.84	-374.02
21	22	23.40	0.00	-110.76	-205.60
22	22	23.40	0.00	-110.76	-205.60
22	23	24.80	0.00	-98.67	-58.98
23	23	24.80	0.00	-98.67	-58.98
23	24	26.20	0.00	-86.60	70.70
24	24	26.20	0.00	-86.60	70.70
24	25	27.60	0.00	-74.51	183.48
25	25	27.60	0.00	-74.51	183.48
25	26	29.00	0.00	-62.22	288.16
26	26	29.00	16.56	-57.98	288.16

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	13.07	-45.90	366.20
27	27	30.40	0.00	-49.24	366.20
27	28	31.80	0.00	-37.15	426.67
28	28	31.80	0.00	-37.15	426.67
28	29	33.20	0.00	-25.08	470.26
29	29	33.20	0.00	-25.08	470.26
29	30	34.60	0.00	-12.99	496.92
30	30	34.60	0.00	-12.99	496.92
30	31	36.00	0.00	-0.91	506.67
31	31	36.00	0.00	-0.91	506.67
31	32	37.40	0.00	14.80	664.75
32	32	37.40	0.00	14.80	664.75
32	33	38.80	0.00	31.12	632.64
33	33	38.80	0.00	31.12	632.64
33	34	40.20	0.00	47.41	577.68
34	34	40.20	0.00	47.41	577.68
34	35	41.60	0.00	63.73	499.89
35	35	41.60	15.42	59.78	499.89
35	36	43.00	20.13	76.09	398.41
36	36	43.00	0.00	81.24	398.41
36	37	44.40	0.00	97.55	273.27
37	37	44.40	0.00	97.55	273.27
37	38	45.80	0.00	113.87	125.28
38	38	45.80	0.00	113.87	125.28
38	39	47.20	0.00	130.17	-45.52
39	39	47.20	0.00	130.17	-45.52
39	40	48.60	0.00	146.49	-239.19
40	40	48.60	0.00	146.49	-239.19
40	41	50.00	0.00	172.25	-462.29
41	1041	50.00	0.00	-127.59	-342.44
41	42	51.40	0.00	-108.51	-177.18
42	42	51.40	0.00	-108.51	-177.18
42	43	52.80	0.00	-96.42	-33.72
43	43	52.80	0.00	-96.42	-33.72
43	44	54.20	0.00	-84.35	92.80
44	44	54.20	0.00	-84.35	92.80
44	45	55.60	0.00	-72.26	202.42
45	45	55.60	0.00	-72.26	202.42
45	46	57.00	0.00	-60.18	295.12
46	46	57.00	14.91	-56.36	295.12
46	47	58.40	11.42	-44.28	370.29
47	47	58.40	0.00	-47.21	370.29
47	48	59.80	0.00	-35.12	427.91
48	48	59.80	0.00	-35.12	427.91
48	49	61.20	0.00	-23.05	468.62
49	49	61.20	0.00	-23.05	468.62
49	50	62.60	0.00	-10.96	492.41
50	50	62.60	0.00	-10.96	492.41
50	51	64.00	0.00	1.72	525.00
51	51	64.00	0.00	1.72	525.00
51	52	65.40	0.00	18.03	652.82

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	18.03	652.82
52	53	66.80	0.00	34.35	616.15
53	53	66.80	0.00	34.35	616.15
53	54	68.20	0.00	50.64	556.64
54	54	68.20	0.00	50.64	556.64
54	55	69.60	0.00	66.96	474.32
55	55	69.60	17.64	62.46	474.32
55	56	71.00	22.36	78.76	368.29
56	56	71.00	0.00	84.49	368.29
56	57	72.40	0.00	100.59	247.70
57	57	72.40	0.00	100.59	247.70
57	58	73.80	0.00	116.91	95.44
58	58	73.80	0.00	116.91	95.44
58	59	75.20	0.00	133.20	-79.62
59	59	75.20	0.00	133.20	-79.62
59	60	76.60	0.00	149.53	-277.56
60	60	76.60	0.00	149.53	-277.56
60	61	78.00	0.00	175.28	-504.93
61	1061	78.00	0.00	-118.08	-374.02
61	62	79.10	0.00	-103.09	-252.38
62	62	79.10	0.00	-103.09	-252.38
62	63	80.20	0.00	-93.60	-144.18
63	63	80.20	0.00	-93.60	-144.18
63	64	81.30	0.00	-84.10	-46.46
64	64	81.30	0.00	-84.10	-46.46
64	65	82.40	0.00	-74.61	40.84
65	65	82.40	0.00	-74.61	40.84
65	66	83.50	0.00	-65.12	117.68
66	66	83.50	0.00	-65.12	117.68
66	67	84.60	0.00	-55.35	188.25
67	67	84.60	22.04	-48.42	188.25
67	68	85.70	18.55	-38.94	243.31
68	68	85.70	0.00	-44.77	243.31
68	69	86.80	0.00	-35.26	287.31
69	69	86.80	0.00	-35.26	287.31
69	70	87.90	0.00	-25.78	320.90
70	70	87.90	0.00	-25.78	320.90
70	71	89.00	0.00	-16.25	409.54
71	71	89.00	0.00	-16.25	409.54
71	72	90.10	0.00	-5.19	442.94
72	72	90.10	0.00	-5.19	442.94
72	73	91.20	0.00	5.87	442.56
73	73	91.20	0.00	5.87	442.56
73	74	92.30	0.00	16.95	430.03
74	74	92.30	0.00	16.95	430.03
74	75	93.40	0.00	28.92	446.01
75	75	93.40	0.00	28.92	446.01
75	76	94.50	0.00	41.73	407.15
76	76	94.50	0.00	41.73	407.15
76	77	95.60	0.00	54.55	354.20
77	77	95.60	0.00	54.55	354.20

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2
ENVOLVENTE FASE 2
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	67.35	287.16
78	78	96.70	0.00	67.35	287.16
78	79	97.80	0.00	80.19	206.01
79	79	97.80	0.00	80.19	206.01
79	80	98.90	0.00	92.99	110.77
80	80	98.90	0.00	92.99	110.77
80	81	100.00	0.00	108.41	0.00
101	101	0.00	0.00	-80.30	0.00
101	102	1.10	0.00	-68.88	82.05
102	102	1.10	0.00	-68.88	82.05
102	103	2.20	0.00	-59.40	152.60
103	103	2.20	0.00	-59.40	152.60
103	104	3.30	0.00	-49.89	212.71
104	104	3.30	0.00	-49.89	212.71
104	105	4.40	0.00	-40.41	262.37
105	105	4.40	0.00	-40.41	262.37
105	106	5.50	0.00	-30.91	301.59
106	106	5.50	0.00	-30.91	301.59
106	107	6.60	0.00	-21.42	330.38
107	107	6.60	0.00	-21.42	330.38
107	108	7.70	0.00	-11.09	389.47
108	108	7.70	0.00	-11.09	389.47
108	109	8.80	0.00	0.16	395.47
109	109	8.80	0.00	0.16	395.47
109	110	9.90	0.00	11.40	389.11
110	110	9.90	0.00	11.40	389.11
110	111	11.00	0.00	22.64	370.38
111	111	11.00	0.00	22.64	370.38
111	112	12.10	0.00	35.44	425.56
112	112	12.10	0.00	35.44	425.56
112	113	13.20	0.00	48.24	379.52
113	113	13.20	0.00	48.24	379.52
113	114	14.30	0.00	61.07	319.42
114	114	14.30	25.04	53.20	319.42
114	115	15.40	29.75	66.00	244.39
115	115	15.40	0.00	75.36	244.39
115	116	16.50	0.00	87.91	158.87
116	116	16.50	0.00	87.91	158.87
116	117	17.60	0.00	100.72	55.12
117	117	17.60	0.00	100.72	55.12
117	118	18.70	0.00	113.54	-62.72
118	118	18.70	0.00	113.54	-62.72
118	119	19.80	0.00	126.36	-194.64
119	119	19.80	0.00	126.36	-194.64
119	120	20.90	0.00	139.17	-340.71
120	120	20.90	0.00	139.17	-340.71
120	121	22.00	0.00	159.41	-504.93
121	1121	22.00	0.00	-129.84	-374.02
121	122	23.40	0.00	-110.76	-205.60
122	122	23.40	0.00	-110.76	-205.60
122	123	24.80	0.00	-98.67	-58.98

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-98.67	-58.98
123	124	26.20	0.00	-86.60	70.70
124	124	26.20	0.00	-86.60	70.70
124	125	27.60	0.00	-74.51	183.48
125	125	27.60	0.00	-74.51	183.48
125	126	29.00	0.00	-62.22	288.16
126	126	29.00	16.56	-57.98	288.16
126	127	30.40	13.07	-45.90	366.20
127	127	30.40	0.00	-49.24	366.20
127	128	31.80	0.00	-37.15	426.67
128	128	31.80	0.00	-37.15	426.67
128	129	33.20	0.00	-25.08	470.27
129	129	33.20	0.00	-25.08	470.27
129	130	34.60	0.00	-12.99	496.92
130	130	34.60	0.00	-12.99	496.92
130	131	36.00	0.00	-0.91	506.67
131	131	36.00	0.00	-0.91	506.67
131	132	37.40	0.00	14.80	664.75
132	132	37.40	0.00	14.80	664.75
132	133	38.80	0.00	31.12	632.64
133	133	38.80	0.00	31.12	632.64
133	134	40.20	0.00	47.41	577.68
134	134	40.20	0.00	47.41	577.68
134	135	41.60	0.00	63.73	499.89
135	135	41.60	15.42	59.78	499.89
135	136	43.00	20.13	76.09	398.41
136	136	43.00	0.00	81.24	398.41
136	137	44.40	0.00	97.55	273.27
137	137	44.40	0.00	97.55	273.27
137	138	45.80	0.00	113.87	125.28
138	138	45.80	0.00	113.87	125.28
138	139	47.20	0.00	130.17	-45.52
139	139	47.20	0.00	130.17	-45.52
139	140	48.60	0.00	146.49	-239.21
140	140	48.60	0.00	146.49	-239.21
140	141	50.00	0.00	172.25	-462.31
141	1141	50.00	0.00	-127.59	-342.45
141	142	51.40	0.00	-108.51	-177.19
142	142	51.40	0.00	-108.51	-177.19
142	143	52.80	0.00	-96.42	-33.72
143	143	52.80	0.00	-96.42	-33.72
143	144	54.20	0.00	-84.35	92.80
144	144	54.20	0.00	-84.35	92.80
144	145	55.60	0.00	-72.26	202.42
145	145	55.60	0.00	-72.26	202.42
145	146	57.00	0.00	-60.18	295.12
146	146	57.00	14.91	-56.36	295.12
146	147	58.40	11.42	-44.28	370.29
147	147	58.40	0.00	-47.21	370.29
147	148	59.80	0.00	-35.12	427.91
148	148	59.80	0.00	-35.12	427.91

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-23.05	468.62
149	149	61.20	0.00	-23.05	468.62
149	150	62.60	0.00	-10.96	492.41
150	150	62.60	0.00	-10.96	492.41
150	151	64.00	0.00	1.72	525.00
151	151	64.00	0.00	1.72	525.00
151	152	65.40	0.00	18.03	652.82
152	152	65.40	0.00	18.03	652.82
152	153	66.80	0.00	34.35	616.16
153	153	66.80	0.00	34.35	616.16
153	154	68.20	0.00	50.64	556.64
154	154	68.20	0.00	50.64	556.64
154	155	69.60	0.00	66.96	474.32
155	155	69.60	17.64	62.46	474.32
155	156	71.00	22.36	78.76	368.29
156	156	71.00	0.00	84.49	368.29
156	157	72.40	0.00	100.59	247.70
157	157	72.40	0.00	100.59	247.70
157	158	73.80	0.00	116.91	95.44
158	158	73.80	0.00	116.91	95.44
158	159	75.20	0.00	133.20	-79.62
159	159	75.20	0.00	133.20	-79.62
159	160	76.60	0.00	149.53	-277.56
160	160	76.60	0.00	149.53	-277.56
160	161	78.00	0.00	175.28	-504.93
161	1161	78.00	0.00	-118.08	-374.02
161	162	79.10	0.00	-103.09	-252.38
162	162	79.10	0.00	-103.09	-252.38
162	163	80.20	0.00	-93.60	-144.18
163	163	80.20	0.00	-93.60	-144.18
163	164	81.30	0.00	-84.10	-46.46
164	164	81.30	0.00	-84.10	-46.46
164	165	82.40	0.00	-74.61	40.83
165	165	82.40	0.00	-74.61	40.83
165	166	83.50	0.00	-65.12	117.68
166	166	83.50	0.00	-65.12	117.68
166	167	84.60	0.00	-55.35	188.25
167	167	84.60	22.04	-48.42	188.25
167	168	85.70	18.55	-38.94	243.31
168	168	85.70	0.00	-44.77	243.31
168	169	86.80	0.00	-35.26	287.31
169	169	86.80	0.00	-35.26	287.31
169	170	87.90	0.00	-25.78	320.90
170	170	87.90	0.00	-25.78	320.90
170	171	89.00	0.00	-16.25	409.54
171	171	89.00	0.00	-16.25	409.54
171	172	90.10	0.00	-5.19	442.94
172	172	90.10	0.00	-5.19	442.94
172	173	91.20	0.00	5.87	442.56
173	173	91.20	0.00	5.87	442.56
173	174	92.30	0.00	16.95	430.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 2

ENVOLVENTE FASE 2

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	16.95	430.03
174	175	93.40	0.00	28.92	446.01
175	175	93.40	0.00	28.92	446.01
175	176	94.50	0.00	41.73	407.15
176	176	94.50	0.00	41.73	407.15
176	177	95.60	0.00	54.55	354.20
177	177	95.60	0.00	54:55	354.20
177	178	96.70	0.00	67.35	287.16
178	178	96.70	0.00	67.35	287.16
178	179	97.80	0.00	80.19	206.01
179	179	97.80	0.00	80.19	206.01
179	180	98.90	0.00	92.99	110.77
180	180	98.90	0.00	92.99	110.77
180	181	100.00	0.00	108.41	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
1	1	0.00	0.00	-108.41	0.00
1	2	1.10	0.00	-92.99	110.77
2	2	1.10	0.00	-92.99	110.77
2	3	2.20	0.00	-80.19	206.01
3	3	2.20	0.00	-80.19	206.01
3	4	3.30	0.00	-67.35	287.16
4	4	3.30	0.00	-67.35	287.16
4	5	4.40	0.00	-54.55	354.20
5	5	4.40	0.00	-54.55	354.20
5	6	5.50	0.00	-41.73	407.15
6	6	5.50	0.00	-41.73	407.15
6	7	6.60	0.00	-28.92	446.01
7	7	6.60	0.00	-28.92	446.01
7	8	7.70	0.00	-16.95	430.03
8	8	7.70	0.00	-16.95	430.03
8	9	8.80	0.00	-5.87	442.56
9	9	8.80	0.00	-5.87	442.56
9	10	9.90	0.00	5.19	442.94
10	10	9.90	0.00	5.19	442.94
10	11	11.00	0.00	16.25	409.54
11	11	11.00	0.00	16.25	409.54
11	12	12.10	0.00	25.78	320.90
12	12	12.10	0.00	25.78	320.90
12	13	13.20	0.00	35.26	287.31
13	13	13.20	0.00	35.26	287.31
13	14	14.30	0.00	44.77	243.31
14	14	14.30	18.55	38.94	243.31
14	15	15.40	22.04	48.42	188.25
15	15	15.40	0.00	55.35	188.25
15	16	16.50	0.00	65.12	117.68
16	16	16.50	0.00	65.12	117.68
16	17	17.60	0.00	74.61	40.84
17	17	17.60	0.00	74.61	40.84
17	18	18.70	0.00	84.10	-46.46
18	18	18.70	0.00	84.10	-46.46
18	19	19.80	0.00	93.60	-144.18
19	19	19.80	0.00	93.60	-144.18
19	20	20.90	0.00	103.09	-252.38
20	20	20.90	0.00	103.09	-252.38
20	21	22.00	0.00	118.08	-374.02
21	1021	22.00	0.00	-175.28	-504.93
21	22	23.40	0.00	-149.53	-277.56
22	22	23.40	0.00	-149.53	-277.56
22	23	24.80	0.00	-133.20	-79.62
23	23	24.80	0.00	-133.20	-79.62
23	24	26.20	0.00	-116.91	95.44
24	24	26.20	0.00	-116.91	95.44
24	25	27.60	0.00	-100.59	247.70
25	25	27.60	0.00	-100.59	247.70
25	26	29.00	0.00	-84.49	368.29
26	26	29.00	22.36	-78.76	368.29

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
26	27	30.40	17.64	-62.46	474.32
27	27	30.40	0.00	-66.96	474.32
27	28	31.80	0.00	-50.64	556.64
28	28	31.80	0.00	-50.64	556.64
28	29	33.20	0.00	-34.35	616.15
29	29	33.20	0.00	-34.35	616.15
29	30	34.60	0.00	-18.03	652.82
30	30	34.60	0.00	-18.03	652.82
30	31	36.00	0.00	-1.72	525.00
31	31	36.00	0.00	-1.72	525.00
31	32	37.40	0.00	10.96	492.41
32	32	37.40	0.00	10.96	492.41
32	33	38.80	0.00	23.05	468.62
33	33	38.80	0.00	23.05	468.62
33	34	40.20	0.00	35.12	427.91
34	34	40.20	0.00	35.12	427.91
34	35	41.60	0.00	47.21	370.29
35	35	41.60	11.42	44.28	370.29
35	36	43.00	14.91	56.36	295.12
36	36	43.00	0.00	60.18	295.12
36	37	44.40	0.00	72.26	202.42
37	37	44.40	0.00	72.26	202.42
37	38	45.80	0.00	84.35	92.80
38	38	45.80	0.00	84.35	92.80
38	39	47.20	0.00	96.42	-33.72
39	39	47.20	0.00	96.42	-33.72
39	40	48.60	0.00	108.51	-177.18
40	40	48.60	0.00	108.51	-177.18
40	41	50.00	0.00	127.59	-342.44
41	1041	50.00	0.00	-172.25	-462.29
41	42	51.40	0.00	-146.49	-239.19
42	42	51.40	0.00	-146.49	-239.19
42	43	52.80	0.00	-130.17	-45.52
43	43	52.80	0.00	-130.17	-45.52
43	44	54.20	0.00	-113.87	125.28
44	44	54.20	0.00	-113.87	125.28
44	45	55.60	0.00	-97.55	273.27
45	45	55.60	0.00	-97.55	273.27
45	46	57.00	0.00	-81.24	398.41
46	46	57.00	20.13	-76.09	398.41
46	47	58.40	15.42	-59.78	499.89
47	47	58.40	0.00	-63.73	499.89
47	48	59.80	0.00	-47.41	577.68
48	48	59.80	0.00	-47.41	577.68
48	49	61.20	0.00	-31.12	632.64
49	49	61.20	0.00	-31.12	632.64
49	50	62.60	0.00	-14.80	664.75
50	50	62.60	0.00	-14.80	664.75
50	51	64.00	0.00	0.91	506.67
51	51	64.00	0.00	0.91	506.67
51	52	65.40	0.00	12.99	496.92

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	12.99	496.92
52	53	66.80	0.00	25.08	470.26
53	53	66.80	0.00	25.08	470.26
53	54	68.20	0.00	37.15	426.67
54	54	68.20	0.00	37.15	426.67
54	55	69.60	0.00	49.24	366.20
55	55	69.60	13.07	45.90	366.20
55	56	71.00	16.56	57.98	288.16
56	56	71.00	0.00	62.22	288.16
56	57	72.40	0.00	74.51	183.48
57	57	72.40	0.00	74.51	183.48
57	58	73.80	0.00	86.60	70.70
58	58	73.80	0.00	86.60	70.70
58	59	75.20	0.00	98.67	-58.98
59	59	75.20	0.00	98.67	-58.98
59	60	76.60	0.00	110.76	-205.60
60	60	76.60	0.00	110.76	-205.60
60	61	78.00	0.00	129.84	-374.02
61	1061	78.00	0.00	-159.41	-504.93
61	62	79.10	0.00	-139.17	-340.71
62	62	79.10	0.00	-139.17	-340.71
62	63	80.20	0.00	-126.36	-194.64
63	63	80.20	0.00	-126.36	-194.64
63	64	81.30	0.00	-113.54	-62.72
64	64	81.30	0.00	-113.54	-62.72
64	65	82.40	0.00	-100.72	55.13
65	65	82.40	0.00	-100.72	55.13
65	66	83.50	0.00	-87.91	158.87
66	66	83.50	0.00	-87.91	158.87
66	67	84.60	0.00	-75.36	244.39
67	67	84.60	29.75	-66.00	244.39
67	68	85.70	25.04	-53.20	319.42
68	68	85.70	0.00	-61.07	319.42
68	69	86.80	0.00	-48.24	379.52
69	69	86.80	0.00	-48.24	379.52
69	70	87.90	0.00	-35.44	425.56
70	70	87.90	0.00	-35.44	425.56
70	71	89.00	0.00	-22.64	370.38
71	71	89.00	0.00	-22.64	370.38
71	72	90.10	0.00	-11.40	389.11
72	72	90.10	0.00	-11.40	389.11
72	73	91.20	0.00	-0.16	395.47
73	73	91.20	0.00	-0.16	395.47
73	74	92.30	0.00	11.09	389.47
74	74	92.30	0.00	11.09	389.47
74	75	93.40	0.00	21.42	330.38
75	75	93.40	0.00	21.42	330.38
75	76	94.50	0.00	30.91	301.59
76	76	94.50	0.00	30.91	301.59
76	77	95.60	0.00	40.41	262.37
77	77	95.60	0.00	40.41	262.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
52	52	65.40	0.00	12.99	496.92
52	53	66.80	0.00	25.08	470.26
53	53	66.80	0.00	25.08	470.26
53	54	68.20	0.00	37.15	426.67
54	54	68.20	0.00	37.15	426.67
54	55	69.60	0.00	49.24	366.20
55	55	69.60	13.07	45.90	366.20
55	56	71.00	16.56	57.98	288.16
56	56	71.00	0.00	62.22	288.16
56	57	72.40	0.00	74.51	183.48
57	57	72.40	0.00	74.51	183.48
57	58	73.80	0.00	86.60	70.70
58	58	73.80	0.00	86.60	70.70
58	59	75.20	0.00	98.67	-58.98
59	59	75.20	0.00	98.67	-58.98
59	60	76.60	0.00	110.76	-205.60
60	60	76.60	0.00	110.76	-205.60
60	61	78.00	0.00	129.84	-374.02
61	1061	78.00	0.00	-159.41	-504.93
61	62	79.10	0.00	-139.17	-340.71
62	62	79.10	0.00	-139.17	-340.71
62	63	80.20	0.00	-126.36	-194.64
63	63	80.20	0.00	-126.36	-194.64
63	64	81.30	0.00	-113.54	-62.72
64	64	81.30	0.00	-113.54	-62.72
64	65	82.40	0.00	-100.72	55.13
65	65	82.40	0.00	-100.72	55.13
65	66	83.50	0.00	-87.91	158.87
66	66	83.50	0.00	-87.91	158.87
66	67	84.60	0.00	-75.36	244.39
67	67	84.60	29.75	-66.00	244.39
67	68	85.70	25.04	-53.20	319.42
68	68	85.70	0.00	-61.07	319.42
68	69	86.80	0.00	-48.24	379.52
69	69	86.80	0.00	-48.24	379.52
69	70	87.90	0.00	-35.44	425.56
70	70	87.90	0.00	-35.44	425.56
70	71	89.00	0.00	-22.64	370.38
71	71	89.00	0.00	-22.64	370.38
71	72	90.10	0.00	-11.40	389.11
72	72	90.10	0.00	-11.40	389.11
72	73	91.20	0.00	-0.16	395.47
73	73	91.20	0.00	-0.16	395.47
73	74	92.30	0.00	11.09	389.47
74	74	92.30	0.00	11.09	389.47
74	75	93.40	0.00	21.42	330.38
75	75	93.40	0.00	21.42	330.38
75	76	94.50	0.00	30.91	301.59
76	76	94.50	0.00	30.91	301.59
76	77	95.60	0.00	40.41	262.37
77	77	95.60	0.00	40.41	262.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
77	78	96.70	0.00	49.89	212.71
78	78	96.70	0.00	49.89	212.71
78	79	97.80	0.00	59.40	152.60
79	79	97.80	0.00	59.40	152.60
79	80	98.90	0.00	68.88	82.05
80	80	98.90	0.00	68.88	82.05
80	81	100.00	0.00	80.30	0.00
101	101	0.00	0.00	-108.41	0.00
101	102	1.10	0.00	-92.99	110.77
102	102	1.10	0.00	-92.99	110.77
102	103	2.20	0.00	-80.19	206.01
103	103	2.20	0.00	-80.19	206.01
103	104	3.30	0.00	-67.35	287.16
104	104	3.30	0.00	-67.35	287.16
104	105	4.40	0.00	-54.55	354.20
105	105	4.40	0.00	-54.55	354.20
105	106	5.50	0.00	-41.73	407.15
106	106	5.50	0.00	-41.73	407.15
106	107	6.60	0.00	-28.92	446.01
107	107	6.60	0.00	-28.92	446.01
107	108	7.70	0.00	-16.95	430.03
108	108	7.70	0.00	-16.95	430.03
108	109	8.80	0.00	-5.87	442.56
109	109	8.80	0.00	-5.87	442.56
109	110	9.90	0.00	5.19	442.94
110	110	9.90	0.00	5.19	442.94
110	111	11.00	0.00	16.25	409.54
111	111	11.00	0.00	16.25	409.54
111	112	12.10	0.00	25.78	320.90
112	112	12.10	0.00	25.78	320.90
112	113	13.20	0.00	35.26	287.31
113	113	13.20	0.00	35.26	287.31
113	114	14.30	0.00	44.77	243.31
114	114	14.30	18.55	38.94	243.31
114	115	15.40	22.04	48.42	188.25
115	115	15.40	0.00	55.35	188.25
115	116	16.50	0.00	65.12	117.68
116	116	16.50	0.00	65.12	117.68
116	117	17.60	0.00	74.61	40.83
117	117	17.60	0.00	74.61	40.83
117	118	18.70	0.00	84.10	-46.46
118	118	18.70	0.00	84.10	-46.46
118	119	19.80	0.00	93.60	-144.18
119	119	19.80	0.00	93.60	-144.18
119	120	20.90	0.00	103.09	-252.38
120	120	20.90	0.00	103.09	-252.38
120	121	22.00	0.00	118.08	-374.02
121	1121	22.00	0.00	-175.28	-504.93
121	122	23.40	0.00	-149.53	-277.56
122	122	23.40	0.00	-149.53	-277.56
122	123	24.80	0.00	-133.20	-79.62

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
123	123	24.80	0.00	-133.20	-79.62
123	124	26.20	0.00	-116.91	95.44
124	124	26.20	0.00	-116.91	95.44
124	125	27.60	0.00	-100.59	247.70
125	125	27.60	0.00	-100.59	247.70
125	126	29.00	0.00	-84.49	368.29
126	126	29.00	22.36	-78.76	368.29
126	127	30.40	17.64	-62.46	474.32
127	127	30.40	0.00	-66.96	474.32
127	128	31.80	0.00	-50.64	556.64
128	128	31.80	0.00	-50.64	556.64
128	129	33.20	0.00	-34.35	616.16
129	129	33.20	0.00	-34.35	616.16
129	130	34.60	0.00	-18.03	652.82
130	130	34.60	0.00	-18.03	652.82
130	131	36.00	0.00	-1.72	525.00
131	131	36.00	0.00	-1.72	525.00
131	132	37.40	0.00	10.96	492.41
132	132	37.40	0.00	10.96	492.41
132	133	38.80	0.00	23.05	468.62
133	133	38.80	0.00	23.05	468.62
133	134	40.20	0.00	35.12	427.91
134	134	40.20	0.00	35.12	427.91
134	135	41.60	0.00	47.21	370.29
135	135	41.60	11.42	44.28	370.29
135	136	43.00	14.91	56.36	295.12
136	136	43.00	0.00	60.18	295.12
136	137	44.40	0.00	72.26	202.42
137	137	44.40	0.00	72.26	202.42
137	138	45.80	0.00	84.35	92.80
138	138	45.80	0.00	84.35	92.80
138	139	47.20	0.00	96.42	-33.72
139	139	47.20	0.00	96.42	-33.72
139	140	48.60	0.00	108.51	-177.19
140	140	48.60	0.00	108.51	-177.19
140	141	50.00	0.00	127.59	-342.45
141	1141	50.00	0.00	-172.25	-462.31
141	142	51.40	0.00	-146.49	-239.21
142	142	51.40	0.00	-146.49	-239.21
142	143	52.80	0.00	-130.17	-45.52
143	143	52.80	0.00	-130.17	-45.52
143	144	54.20	0.00	-113.87	125.28
144	144	54.20	0.00	-113.87	125.28
144	145	55.60	0.00	-97.55	273.27
145	145	55.60	0.00	-97.55	273.27
145	146	57.00	0.00	-81.24	398.41
146	146	57.00	20.13	-76.09	398.41
146	147	58.40	15.42	-59.78	499.89
147	147	58.40	0.00	-63.73	499.89
147	148	59.80	0.00	-47.41	577.68
148	148	59.80	0.00	-47.41	577.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
148	149	61.20	0.00	-31.12	632.64
149	149	61.20	0.00	-31.12	632.64
149	150	62.60	0.00	-14.80	664.75
150	150	62.60	0.00	-14.80	664.75
150	151	64.00	0.00	0.91	506.67
151	151	64.00	0.00	0.91	506.67
151	152	65.40	0.00	12.99	496.92
152	152	65.40	0.00	12.99	496.92
152	153	66.80	0.00	25.08	470.27
153	153	66.80	0.00	25.08	470.27
153	154	68.20	0.00	37.15	426.67
154	154	68.20	0.00	37.15	426.67
154	155	69.60	0.00	49.24	366.20
155	155	69.60	13.07	45.90	366.20
155	156	71.00	16.56	57.98	288.16
156	156	71.00	0.00	62.22	288.16
156	157	72.40	0.00	74.51	183.48
157	157	72.40	0.00	74.51	183.48
157	158	73.80	0.00	86.60	70.70
158	158	73.80	0.00	86.60	70.70
158	159	75.20	0.00	98.67	-58.98
159	159	75.20	0.00	98.67	-58.98
159	160	76.60	0.00	110.76	-205.60
160	160	76.60	0.00	110.76	-205.60
160	161	78.00	0.00	129.84	-374.02
161	1161	78.00	0.00	-159.41	-504.93
161	162	79.10	0.00	-139.17	-340.71
162	162	79.10	0.00	-139.17	-340.71
162	163	80.20	0.00	-126.36	-194.64
163	163	80.20	0.00	-126.36	-194.64
163	164	81.30	0.00	-113.54	-62.72
164	164	81.30	0.00	-113.54	-62.72
164	165	82.40	0.00	-100.72	55.12
165	165	82.40	0.00	-100.72	55.12
165	166	83.50	0.00	-87.91	158.87
166	166	83.50	0.00	-87.91	158.87
166	167	84.60	0.00	-75.36	244.39
167	167	84.60	29.75	-66.00	244.39
167	168	85.70	25.04	-53.20	319.42
168	168	85.70	0.00	-61.07	319.42
168	169	86.80	0.00	-48.24	379.52
169	169	86.80	0.00	-48.24	379.52
169	170	87.90	0.00	-35.44	425.56
170	170	87.90	0.00	-35.44	425.56
170	171	89.00	0.00	-22.64	370.38
171	171	89.00	0.00	-22.64	370.38
171	172	90.10	0.00	-11.40	389.11
172	172	90.10	0.00	-11.40	389.11
172	173	91.20	0.00	-0.16	395.47
173	173	91.20	0.00	-0.16	395.47
173	174	92.30	0.00	11.09	389.47

CÁLCULO TENSIONAL

Hipótesis de cálculo:

CONST1.F4.T0.VY-

Construcción sin gradiente en fase constructiva 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
174	174	92.30	0.00	11.09	389.47
174	175	93.40	0.00	21.42	330.38
175	175	93.40	0.00	21.42	330.38
175	176	94.50	0.00	30.91	301.59
176	176	94.50	0.00	30.91	301.59
176	177	95.60	0.00	40.41	262.37
177	177	95.60	0.00	40.41	262.37
177	178	96.70	0.00	49.89	212.71
178	178	96.70	0.00	49.89	212.71
178	179	97.80	0.00	59.40	152.60
179	179	97.80	0.00	59.40	152.60
179	180	98.90	0.00	68.88	82.05
180	180	98.90	0.00	68.88	82.05
180	181	100.00	0.00	80.30	0.00

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 4

ENVOLVENTE FASE 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
1	1	0.00	-80.30	-108.41	108.41
1	2	1.10	-68.88	-92.99	92.99
2	2	1.10	-68.88	-92.99	92.99
2	3	2.20	-59.40	-80.19	80.19
3	3	2.20	-59.40	-80.19	80.19
3	4	3.30	-49.89	-67.35	67.35
4	4	3.30	-49.89	-67.35	67.35
4	5	4.40	-40.41	-54.55	54.55
5	5	4.40	-40.41	-54.55	54.55
5	6	5.50	-30.91	-41.73	41.73
6	6	5.50	-30.91	-41.73	41.73
6	7	6.60	-21.42	-28.92	28.92
7	7	6.60	-21.42	-28.92	28.92
7	8	7.70	-11.09	-16.95	16.95
8	8	7.70	-11.09	-16.95	16.95
8	9	8.80	0.16	-5.87	5.87
9	9	8.80	0.16	-5.87	5.87
9	10	9.90	11.40	5.19	11.40
10	10	9.90	11.40	5.19	11.40
10	11	11.00	22.64	16.25	22.64
11	11	11.00	22.64	16.25	22.64
11	12	12.10	35.44	25.78	35.44
12	12	12.10	35.44	25.78	35.44
12	13	13.20	48.24	35.26	48.24
13	13	13.20	48.24	35.26	48.24
13	14	14.30	61.07	44.77	61.07
14	14	14.30	53.20	38.94	53.20
14	15	15.40	66.00	48.42	66.00
15	15	15.40	75.36	55.35	75.36
15	16	16.50	35.90	26.59	35.90
16	16	16.50	35.90	26.59	35.90
16	17	17.60	48.71	36.08	48.71
17	17	17.60	48.71	36.08	48.71
17	18	18.70	61.52	45.57	61.52
18	18	18.70	61.52	45.57	61.52
18	19	19.80	74.34	55.07	74.34
19	19	19.80	74.34	55.07	74.34
19	20	20.90	87.16	64.56	87.16
20	20	20.90	87.16	64.56	87.16
20	21	22.00	107.39	79.55	107.39
21	1021	22.00	-95.38	-128.76	128.76
21	22	23.40	-76.30	-103.01	103.01
22	22	23.40	-76.30	-103.01	103.01
22	23	24.80	-64.21	-86.68	86.68
23	23	24.80	-64.21	-86.68	86.68
23	24	26.20	-52.14	-70.39	70.39
24	24	26.20	-52.14	-70.39	70.39
24	25	27.60	-40.05	-54.07	54.07
25	25	27.60	-40.05	-54.07	54.07
25	26	29.00	-62.22	-84.49	84.49
26	26	29.00	-57.98	-78.76	78.76

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 4
ENVOLVENTE FASE 4
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
26	27	30.40	-45.90	-62.46	62.46
27	27	30.40	-49.24	-66.96	66.96
27	28	31.80	-37.15	-50.64	50.64
28	28	31.80	-37.15	-50.64	50.64
28	29	33.20	-25.08	-34.35	34.35
29	29	33.20	-25.08	-34.35	34.35
29	30	34.60	-12.99	-18.03	18.03
30	30	34.60	-12.99	-18.03	18.03
30	31	36.00	-0.91	-1.72	1.72
31	31	36.00	-0.91	-1.72	1.72
31	32	37.40	14.80	10.96	14.80
32	32	37.40	14.80	10.96	14.80
32	33	38.80	31.12	23.05	31.12
33	33	38.80	31.12	23.05	31.12
33	34	40.20	47.41	35.12	47.41
34	34	40.20	47.41	35.12	47.41
34	35	41.60	63.73	47.21	63.73
35	35	41.60	59.78	44.28	59.78
35	36	43.00	76.09	56.36	76.09
36	36	43.00	81.24	60.18	81.24
36	37	44.40	55.66	41.23	55.66
37	37	44.40	55.66	41.23	55.66
37	38	45.80	71.98	53.32	71.98
38	38	45.80	71.98	53.32	71.98
38	39	47.20	88.28	65.39	88.28
39	39	47.20	88.28	65.39	88.28
39	40	48.60	104.60	77.48	104.60
40	40	48.60	104.60	77.48	104.60
40	41	50.00	130.36	96.56	130.36
41	1041	50.00	-96.56	-130.36	130.36
41	42	51.40	-77.48	-104.60	104.60
42	42	51.40	-77.48	-104.60	104.60
42	43	52.80	-65.39	-88.28	88.28
43	43	52.80	-65.39	-88.28	88.28
43	44	54.20	-53.32	-71.98	71.98
44	44	54.20	-53.32	-71.98	71.98
44	45	55.60	-41.23	-55.66	55.66
45	45	55.60	-41.23	-55.66	55.66
45	46	57.00	-60.18	-81.24	81.24
46	46	57.00	-56.36	-76.09	76.09
46	47	58.40	-44.28	-59.78	59.78
47	47	58.40	-47.21	-63.73	63.73
47	48	59.80	-35.12	-47.41	47.41
48	48	59.80	-35.12	-47.41	47.41
48	49	61.20	-23.05	-31.12	31.12
49	49	61.20	-23.05	-31.12	31.12
49	50	62.60	-10.96	-14.80	14.80
50	50	62.60	-10.96	-14.80	14.80
50	51	64.00	1.72	0.91	1.72
51	51	64.00	1.72	0.91	1.72
51	52	65.40	18.03	12.99	18.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 4
ENVOLVENTE FASE 4
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
52	52	65.40	18.03	12.99	18.03
52	53	66.80	34.35	25.08	34.35
53	53	66.80	34.35	25.08	34.35
53	54	68.20	50.64	37.15	50.64
54	54	68.20	50.64	37.15	50.64
54	55	69.60	66.96	49.24	66.96
55	55	69.60	62.46	45.90	62.46
55	56	71.00	78.76	57.98	78.76
56	56	71.00	84.49	62.22	84.49
56	57	72.40	54.07	40.05	54.07
57	57	72.40	54.07	40.05	54.07
57	58	73.80	70.39	52.14	70.39
58	58	73.80	70.39	52.14	70.39
58	59	75.20	86.68	64.21	86.68
59	59	75.20	86.68	64.21	86.68
59	60	76.60	103.01	76.30	103.01
60	60	76.60	103.01	76.30	103.01
60	61	78.00	128.76	95.38	128.76
61	1061	78.00	-79.55	-107.39	107.39
61	62	79.10	-64.56	-87.16	87.16
62	62	79.10	-64.56	-87.16	87.16
62	63	80.20	-55.07	-74.34	74.34
63	63	80.20	-55.07	-74.34	74.34
63	64	81.30	-45.57	-61.52	61.52
64	64	81.30	-45.57	-61.52	61.52
64	65	82.40	-36.08	-48.71	48.71
65	65	82.40	-36.08	-48.71	48.71
65	66	83.50	-26.59	-35.90	35.90
66	66	83.50	-26.59	-35.90	35.90
66	67	84.60	-55.35	-75.36	75.36
67	67	84.60	-48.42	-66.00	66.00
67	68	85.70	-38.94	-53.20	53.20
68	68	85.70	-44.77	-61.07	61.07
68	69	86.80	-35.26	-48.24	48.24
69	69	86.80	-35.26	-48.24	48.24
69	70	87.90	-25.78	-35.44	35.44
70	70	87.90	-25.78	-35.44	35.44
70	71	89.00	-16.25	-22.64	22.64
71	71	89.00	-16.25	-22.64	22.64
71	72	90.10	-5.19	-11.40	11.40
72	72	90.10	-5.19	-11.40	11.40
72	73	91.20	5.87	-0.16	5.87
73	73	91.20	5.87	-0.16	5.87
73	74	92.30	16.95	11.09	16.95
74	74	92.30	16.95	11.09	16.95
74	75	93.40	28.92	21.42	28.92
75	75	93.40	28.92	21.42	28.92
75	76	94.50	41.73	30.91	41.73
76	76	94.50	41.73	30.91	41.73
76	77	95.60	54.55	40.41	54.55
77	77	95.60	54.55	40.41	54.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 4

ENVOLVENTE FASE 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
52	52	65.40	18.03	12.99	18.03
52	53	66.80	34.35	25.08	34.35
53	53	66.80	34.35	25.08	34.35
53	54	68.20	50.64	37.15	50.64
54	54	68.20	50.64	37.15	50.64
54	55	69.60	66.96	49.24	66.96
55	55	69.60	62.46	45.90	62.46
55	56	71.00	78.76	57.98	78.76
56	56	71.00	84.49	62.22	84.49
56	57	72.40	54.07	40.05	54.07
57	57	72.40	54.07	40.05	54.07
57	58	73.80	70.39	52.14	70.39
58	58	73.80	70.39	52.14	70.39
58	59	75.20	86.68	64.21	86.68
59	59	75.20	86.68	64.21	86.68
59	60	76.60	103.01	76.30	103.01
60	60	76.60	103.01	76.30	103.01
60	61	78.00	128.76	95.38	128.76
61	1061	78.00	-79.55	-107.39	107.39
61	62	79.10	-64.56	-87.16	87.16
62	62	79.10	-64.56	-87.16	87.16
62	63	80.20	-55.07	-74.34	74.34
63	63	80.20	-55.07	-74.34	74.34
63	64	81.30	-45.57	-61.52	61.52
64	64	81.30	-45.57	-61.52	61.52
64	65	82.40	-36.08	-48.71	48.71
65	65	82.40	-36.08	-48.71	48.71
65	66	83.50	-26.59	-35.90	35.90
66	66	83.50	-26.59	-35.90	35.90
66	67	84.60	-55.35	-75.36	75.36
67	67	84.60	-48.42	-66.00	66.00
67	68	85.70	-38.94	-53.20	53.20
68	68	85.70	-44.77	-61.07	61.07
68	69	86.80	-35.26	-48.24	48.24
69	69	86.80	-35.26	-48.24	48.24
69	70	87.90	-25.78	-35.44	35.44
70	70	87.90	-25.78	-35.44	35.44
70	71	89.00	-16.25	-22.64	22.64
71	71	89.00	-16.25	-22.64	22.64
71	72	90.10	-5.19	-11.40	11.40
72	72	90.10	-5.19	-11.40	11.40
72	73	91.20	5.87	-0.16	5.87
73	73	91.20	5.87	-0.16	5.87
73	74	92.30	16.95	11.09	16.95
74	74	92.30	16.95	11.09	16.95
74	75	93.40	28.92	21.42	28.92
75	75	93.40	28.92	21.42	28.92
75	76	94.50	41.73	30.91	41.73
76	76	94.50	41.73	30.91	41.73
76	77	95.60	54.55	40.41	54.55
77	77	95.60	54.55	40.41	54.55

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 4

ENVOLVENTE FASE 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	67.35	49.89	67.35
78	78	96.70	67.35	49.89	67.35
78	79	97.80	80.19	59.40	80.19
79	79	97.80	80.19	59.40	80.19
79	80	98.90	92.99	68.88	92.99
80	80	98.90	92.99	68.88	92.99
80	81	100.00	108.41	80.30	108.41
101	101	0.00	-80.30	-108.41	108.41
101	102	1.10	-68.88	-92.99	92.99
102	102	1.10	-68.88	-92.99	92.99
102	103	2.20	-59.40	-80.19	80.19
103	103	2.20	-59.40	-80.19	80.19
103	104	3.30	-49.89	-67.35	67.35
104	104	3.30	-49.89	-67.35	67.35
104	105	4.40	-40.41	-54.55	54.55
105	105	4.40	-40.41	-54.55	54.55
105	106	5.50	-30.91	-41.73	41.73
106	106	5.50	-30.91	-41.73	41.73
106	107	6.60	-21.42	-28.92	28.92
107	107	6.60	-21.42	-28.92	28.92
107	108	7.70	-11.09	-16.95	16.95
108	108	7.70	-11.09	-16.95	16.95
108	109	8.80	0.16	-5.87	5.87
109	109	8.80	0.16	-5.87	5.87
109	110	9.90	11.40	5.19	11.40
110	110	9.90	11.40	5.19	11.40
110	111	11.00	22.64	16.25	22.64
111	111	11.00	22.64	16.25	22.64
111	112	12.10	35.44	25.78	35.44
112	112	12.10	35.44	25.78	35.44
112	113	13.20	48.24	35.26	48.24
113	113	13.20	48.24	35.26	48.24
113	114	14.30	61.07	44.77	61.07
114	114	14.30	53.20	38.94	53.20
114	115	15.40	66.00	48.42	66.00
115	115	15.40	75.36	55.35	75.36
115	116	16.50	35.90	26.59	35.90
116	116	16.50	35.90	26.59	35.90
116	117	17.60	48.71	36.08	48.71
117	117	17.60	48.71	36.08	48.71
117	118	18.70	61.52	45.57	61.52
118	118	18.70	61.52	45.57	61.52
118	119	19.80	74.34	55.07	74.34
119	119	19.80	74.34	55.07	74.34
119	120	20.90	87.16	64.56	87.16
120	120	20.90	87.16	64.56	87.16
120	121	22.00	107.39	79.55	107.39
121	1121	22.00	-95.38	-128.76	128.76
121	122	23.40	-76.30	-103.01	103.01
122	122	23.40	-76.30	-103.01	103.01
122	123	24.80	-64.21	-86.68	86.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 4

ENVOLVENTE FASE 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	67.35	49.89	67.35
78	78	96.70	67.35	49.89	67.35
78	79	97.80	80.19	59.40	80.19
79	79	97.80	80.19	59.40	80.19
79	80	98.90	92.99	68.88	92.99
80	80	98.90	92.99	68.88	92.99
80	81	100.00	108.41	80.30	108.41
101	101	0.00	-80.30	-108.41	108.41
101	102	1.10	-68.88	-92.99	92.99
102	102	1.10	-68.88	-92.99	92.99
102	103	2.20	-59.40	-80.19	80.19
103	103	2.20	-59.40	-80.19	80.19
103	104	3.30	-49.89	-67.35	67.35
104	104	3.30	-49.89	-67.35	67.35
104	105	4.40	-40.41	-54.55	54.55
105	105	4.40	-40.41	-54.55	54.55
105	106	5.50	-30.91	-41.73	41.73
106	106	5.50	-30.91	-41.73	41.73
106	107	6.60	-21.42	-28.92	28.92
107	107	6.60	-21.42	-28.92	28.92
107	108	7.70	-11.09	-16.95	16.95
108	108	7.70	-11.09	-16.95	16.95
108	109	8.80	0.16	-5.87	5.87
109	109	8.80	0.16	-5.87	5.87
109	110	9.90	11.40	5.19	11.40
110	110	9.90	11.40	5.19	11.40
110	111	11.00	22.64	16.25	22.64
111	111	11.00	22.64	16.25	22.64
111	112	12.10	35.44	25.78	35.44
112	112	12.10	35.44	25.78	35.44
112	113	13.20	48.24	35.26	48.24
113	113	13.20	48.24	35.26	48.24
113	114	14.30	61.07	44.77	61.07
114	114	14.30	53.20	38.94	53.20
114	115	15.40	66.00	48.42	66.00
115	115	15.40	75.36	55.35	75.36
115	116	16.50	35.90	26.59	35.90
116	116	16.50	35.90	26.59	35.90
116	117	17.60	48.71	36.08	48.71
117	117	17.60	48.71	36.08	48.71
117	118	18.70	61.52	45.57	61.52
118	118	18.70	61.52	45.57	61.52
118	119	19.80	74.34	55.07	74.34
119	119	19.80	74.34	55.07	74.34
119	120	20.90	87.16	64.56	87.16
120	120	20.90	87.16	64.56	87.16
120	121	22.00	107.39	79.55	107.39
121	1121	22.00	-95.38	-128.76	128.76
121	122	23.40	-76.30	-103.01	103.01
122	122	23.40	-76.30	-103.01	103.01
122	123	24.80	-64.21	-86.68	86.68

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE FASE 4

ENVOLVENTE FASE 4

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV

Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
123	123	24.80	-64.21	-86.68	86.68
123	124	26.20	-52.14	-70.39	70.39
124	124	26.20	-52.14	-70.39	70.39
124	125	27.60	-40.05	-54.07	54.07
125	125	27.60	-40.05	-54.07	54.07
125	126	29.00	-62.22	-84.49	84.49
126	126	29.00	-57.98	-78.76	78.76
126	127	30.40	-45.90	-62.46	62.46
127	127	30.40	-49.24	-66.96	66.96
127	128	31.80	-37.15	-50.64	50.64
128	128	31.80	-37.15	-50.64	50.64
128	129	33.20	-25.08	-34.35	34.35
129	129	33.20	-25.08	-34.35	34.35
129	130	34.60	-12.99	-18.03	18.03
130	130	34.60	-12.99	-18.03	18.03
130	131	36.00	-0.91	-1.72	1.72
131	131	36.00	-0.91	-1.72	1.72
131	132	37.40	14.80	10.96	14.80
132	132	37.40	14.80	10.96	14.80
132	133	38.80	31.12	23.05	31.12
133	133	38.80	31.12	23.05	31.12
133	134	40.20	47.41	35.12	47.41
134	134	40.20	47.41	35.12	47.41
134	135	41.60	63.73	47.21	63.73
135	135	41.60	59.78	44.28	59.78
135	136	43.00	76.09	56.36	76.09
136	136	43.00	81.24	60.18	81.24
136	137	44.40	55.66	41.23	55.66
137	137	44.40	55.66	41.23	55.66
137	138	45.80	71.98	53.32	71.98
138	138	45.80	71.98	53.32	71.98
138	139	47.20	88.28	65.39	88.28
139	139	47.20	88.28	65.39	88.28
139	140	48.60	104.60	77.48	104.60
140	140	48.60	104.60	77.48	104.60
140	141	50.00	130.36	96.56	130.36
141	1141	50.00	-96.56	-130.36	130.36
141	142	51.40	-77.48	-104.60	104.60
142	142	51.40	-77.48	-104.60	104.60
142	143	52.80	-65.39	-88.28	88.28
143	143	52.80	-65.39	-88.28	88.28
143	144	54.20	-53.32	-71.98	71.98
144	144	54.20	-53.32	-71.98	71.98
144	145	55.60	-41.23	-55.66	55.66
145	145	55.60	-41.23	-55.66	55.66
145	146	57.00	-60.18	-81.24	81.24
146	146	57.00	-56.36	-76.09	76.09
146	147	58.40	-44.28	-59.78	59.78
147	147	58.40	-47.21	-63.73	63.73
147	148	59.80	-35.12	-47.41	47.41
148	148	59.80	-35.12	-47.41	47.41

CÁLCULO TENSIONAL

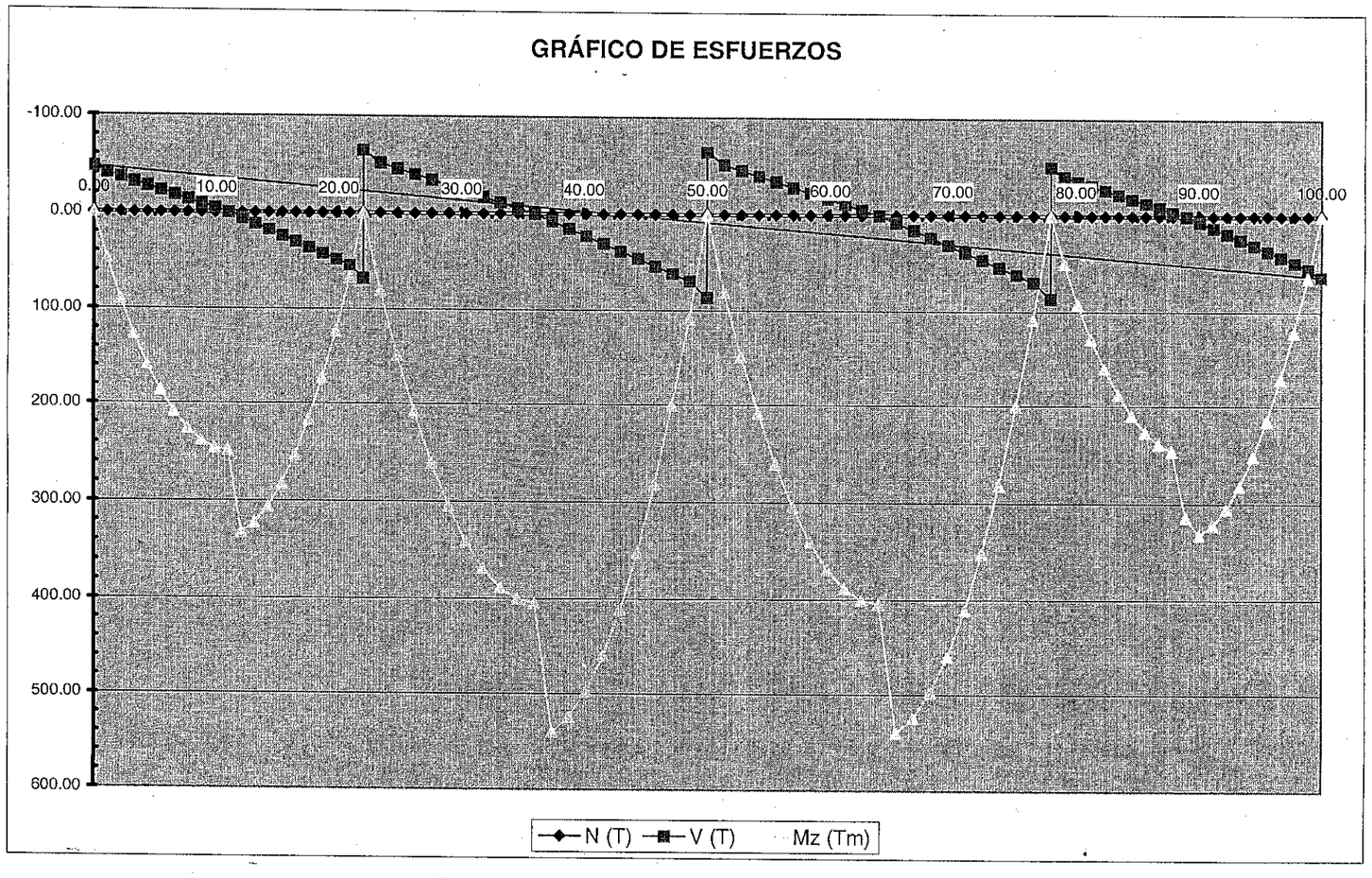
Hipótesis de cálculo:
ENVOLVENTE FASE 4
ENVOLVENTE FASE 4
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
148	149	61.20	-23.05	-31.12	31.12
149	149	61.20	-23.05	-31.12	31.12
149	150	62.60	-10.96	-14.80	14.80
150	150	62.60	-10.96	-14.80	14.80
150	151	64.00	1.72	0.91	1.72
151	151	64.00	1.72	0.91	1.72
151	152	65.40	18.03	12.99	18.03
152	152	65.40	18.03	12.99	18.03
152	153	66.80	34.35	25.08	34.35
153	153	66.80	34.35	25.08	34.35
153	154	68.20	50.64	37.15	50.64
154	154	68.20	50.64	37.15	50.64
154	155	69.60	66.96	49.24	66.96
155	155	69.60	62.46	45.90	62.46
155	156	71.00	78.76	57.98	78.76
156	156	71.00	84.49	62.22	84.49
156	157	72.40	54.07	40.05	54.07
157	157	72.40	54.07	40.05	54.07
157	158	73.80	70.39	52.14	70.39
158	158	73.80	70.39	52.14	70.39
158	159	75.20	86.68	64.21	86.68
159	159	75.20	86.68	64.21	86.68
159	160	76.60	103.01	76.30	103.01
160	160	76.60	103.01	76.30	103.01
160	161	78.00	128.76	95.38	128.76
161	1161	78.00	-79.55	-107.39	107.39
161	162	79.10	-64.56	-87.16	87.16
162	162	79.10	-64.56	-87.16	87.16
162	163	80.20	-55.07	-74.34	74.34
163	163	80.20	-55.07	-74.34	74.34
163	164	81.30	-45.57	-61.52	61.52
164	164	81.30	-45.57	-61.52	61.52
164	165	82.40	-36.08	-48.71	48.71
165	165	82.40	-36.08	-48.71	48.71
165	166	83.50	-26.59	-35.90	35.90
166	166	83.50	-26.59	-35.90	35.90
166	167	84.60	-55.35	-75.36	75.36
167	167	84.60	-48.42	-66.00	66.00
167	168	85.70	-38.94	-53.20	53.20
168	168	85.70	-44.77	-61.07	61.07
168	169	86.80	-35.26	-48.24	48.24
169	169	86.80	-35.26	-48.24	48.24
169	170	87.90	-25.78	-35.44	35.44
170	170	87.90	-25.78	-35.44	35.44
170	171	89.00	-16.25	-22.64	22.64
171	171	89.00	-16.25	-22.64	22.64
171	172	90.10	-5.19	-11.40	11.40
172	172	90.10	-5.19	-11.40	11.40
172	173	91.20	5.87	-0.16	5.87
173	173	91.20	5.87	-0.16	5.87
173	174	92.30	16.95	11.09	16.95

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE FASE 4
ENVOLVENTE FASE 4
[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1.35]HLCV
Coef. exc:

Barra	Nudo	X	Max Vy (T)	Min Vy (T)	|Vy| (T)
174	174	92.30	16.95	11.09	16.95
174	175	93.40	28.92	21.42	28.92
175	175	93.40	28.92	21.42	28.92
175	176	94.50	41.73	30.91	41.73
176	176	94.50	41.73	30.91	41.73
176	177	95.60	54.55	40.41	54.55
177	177	95.60	54.55	40.41	54.55
177	178	96.70	67.35	49.89	67.35
178	178	96.70	67.35	49.89	67.35
178	179	97.80	80.19	59.40	80.19
179	179	97.80	80.19	59.40	80.19
179	180	98.90	92.99	68.88	92.99
180	180	98.90	92.99	68.88	92.99
180	181	100.00	108.41	80.30	108.41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V (T)
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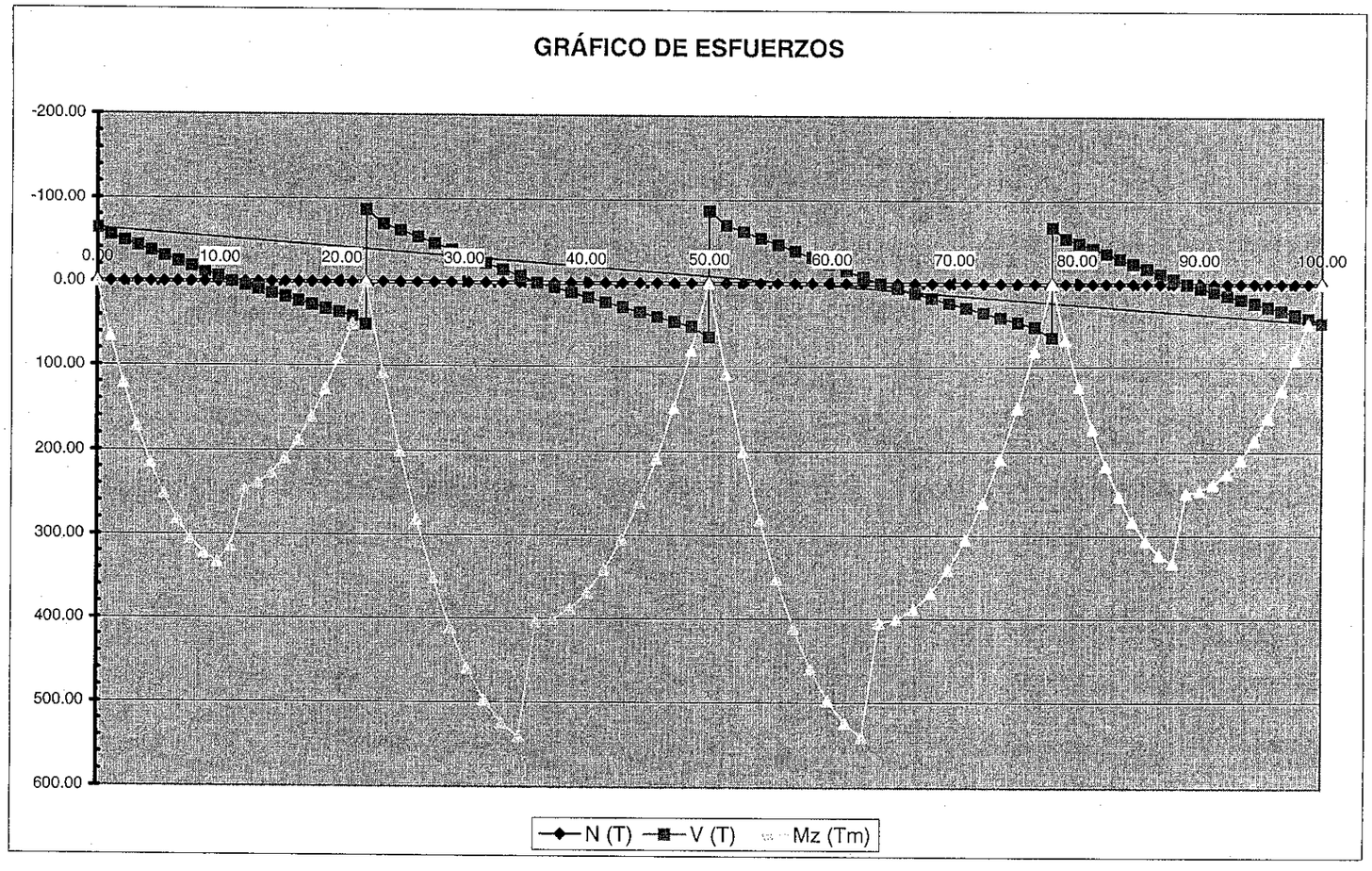
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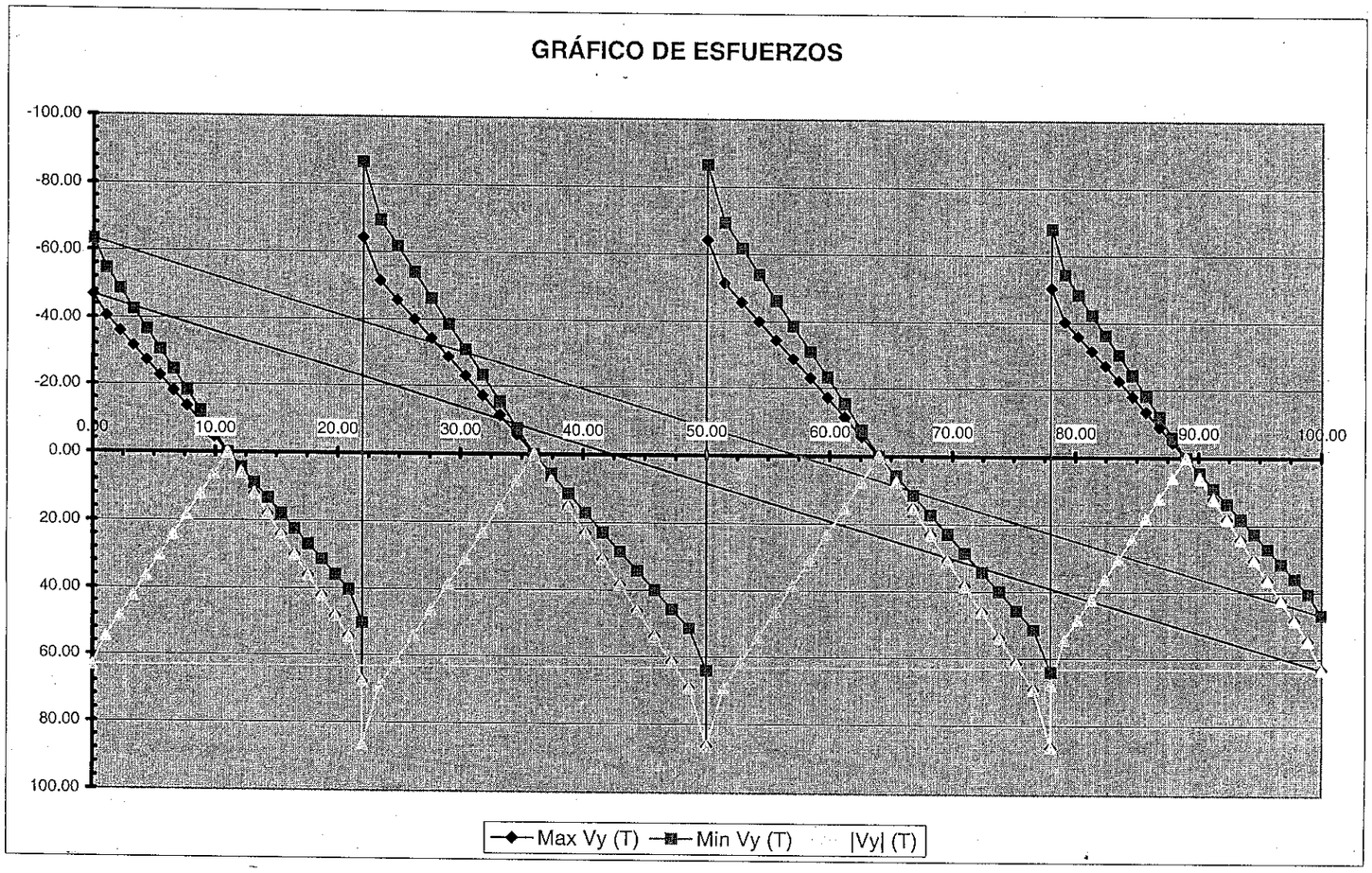
V (T)
Mz (Tm)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Min Vy (T)
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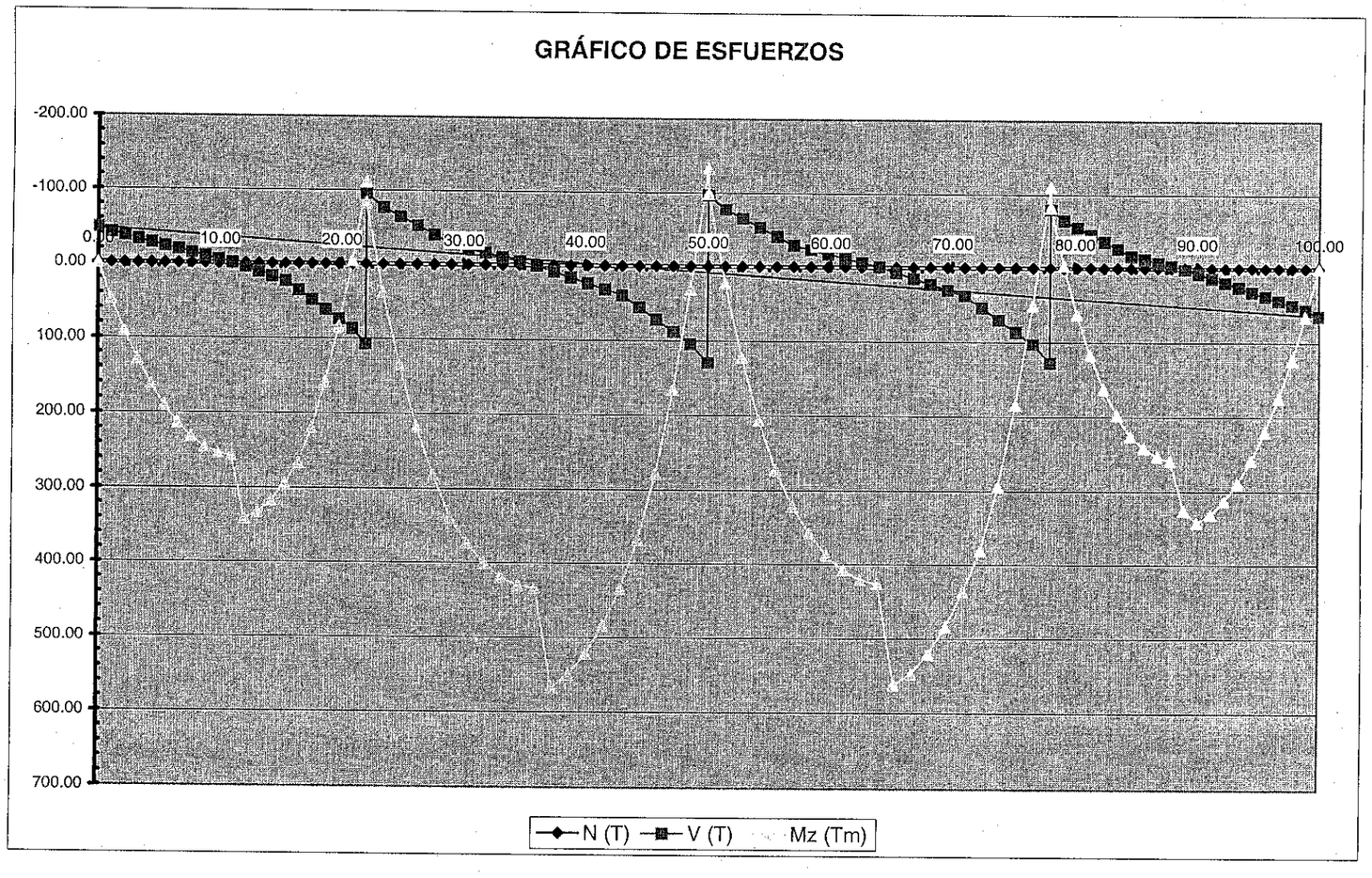
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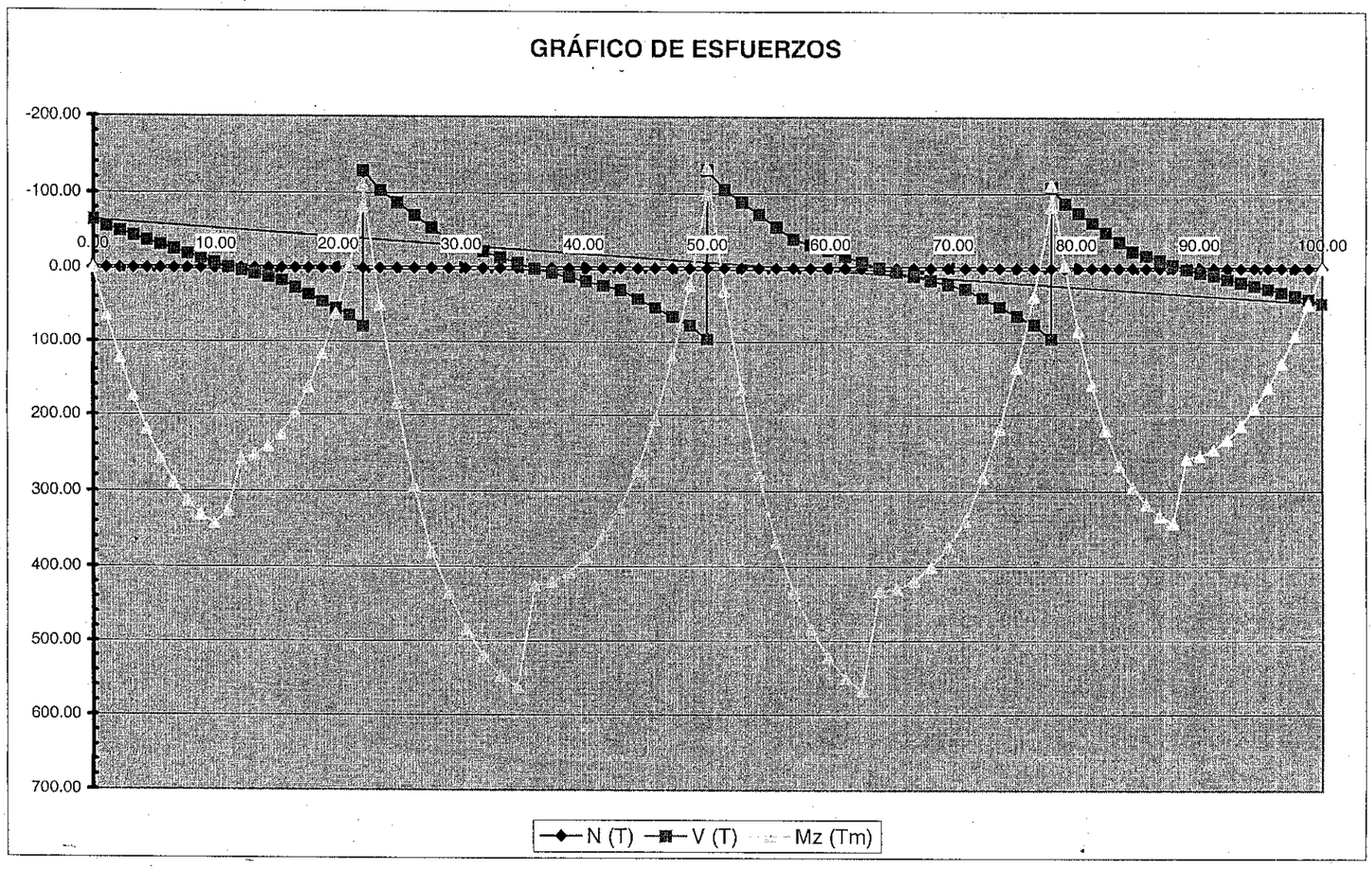
N (T)
V (T)
Mz (Tm)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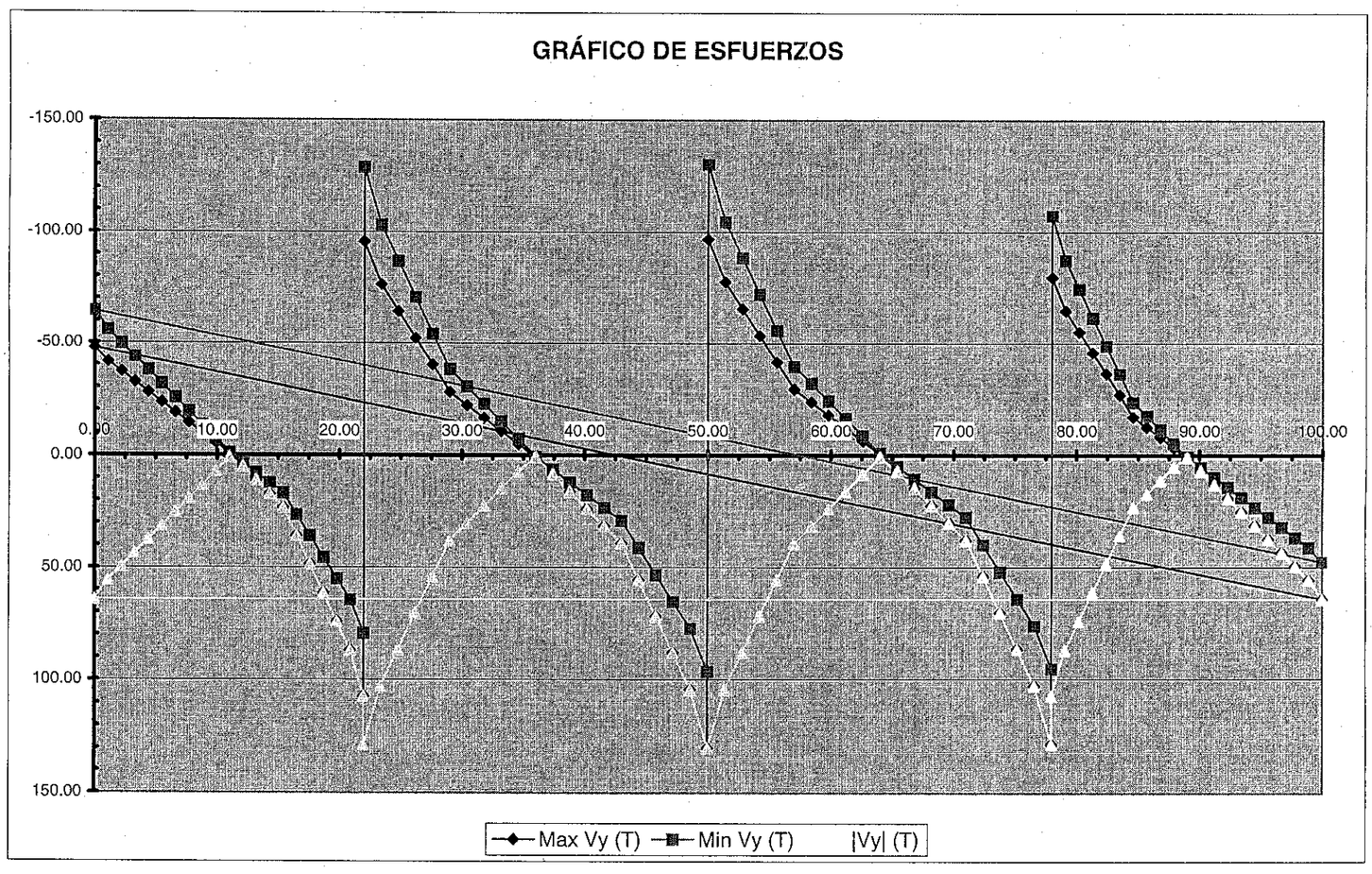
V (T)
Mz (Tm)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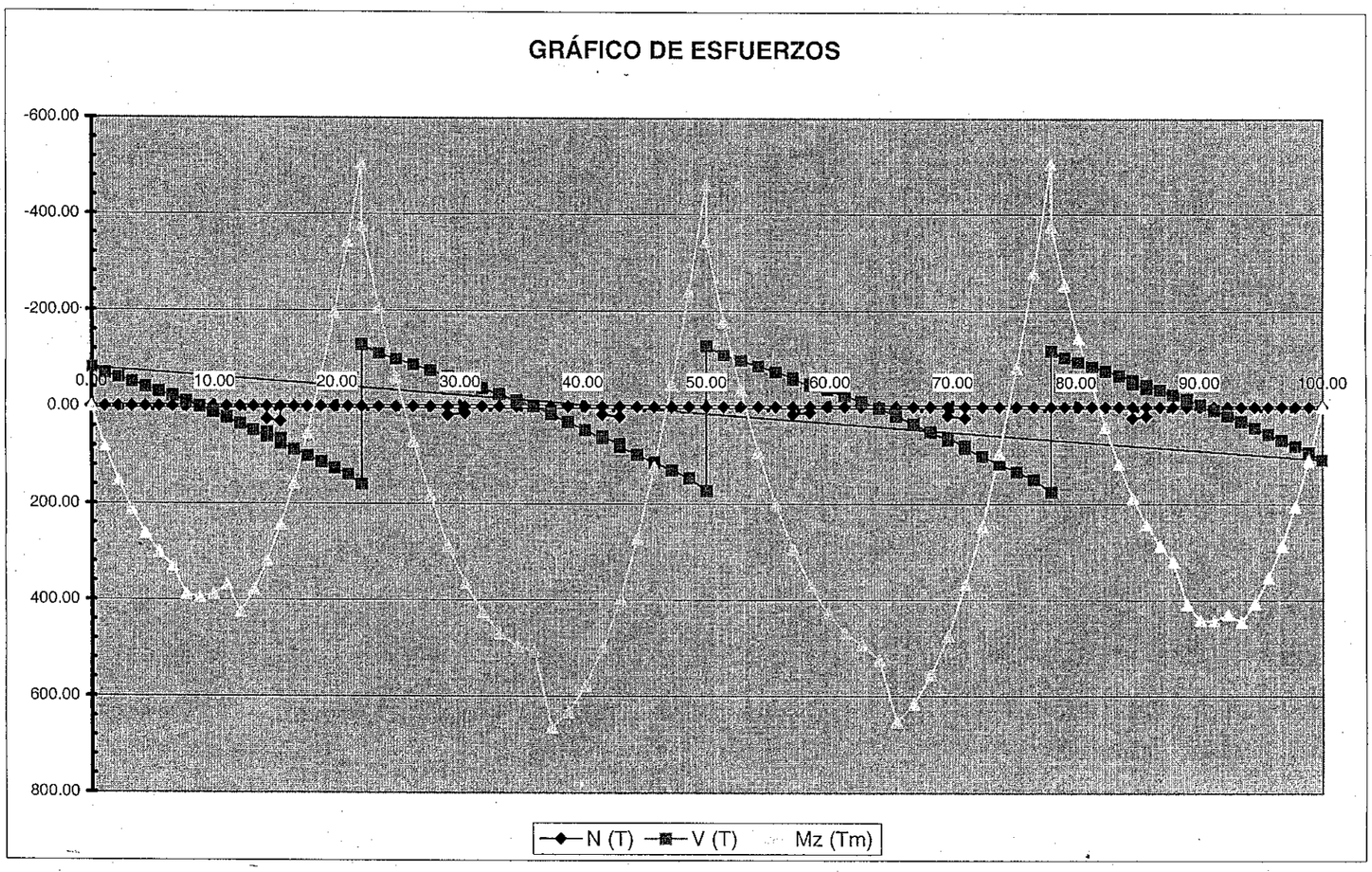
90.00
100.00
Max Vy (T)
Min Vy (T)
|Vy| (T)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V (T)
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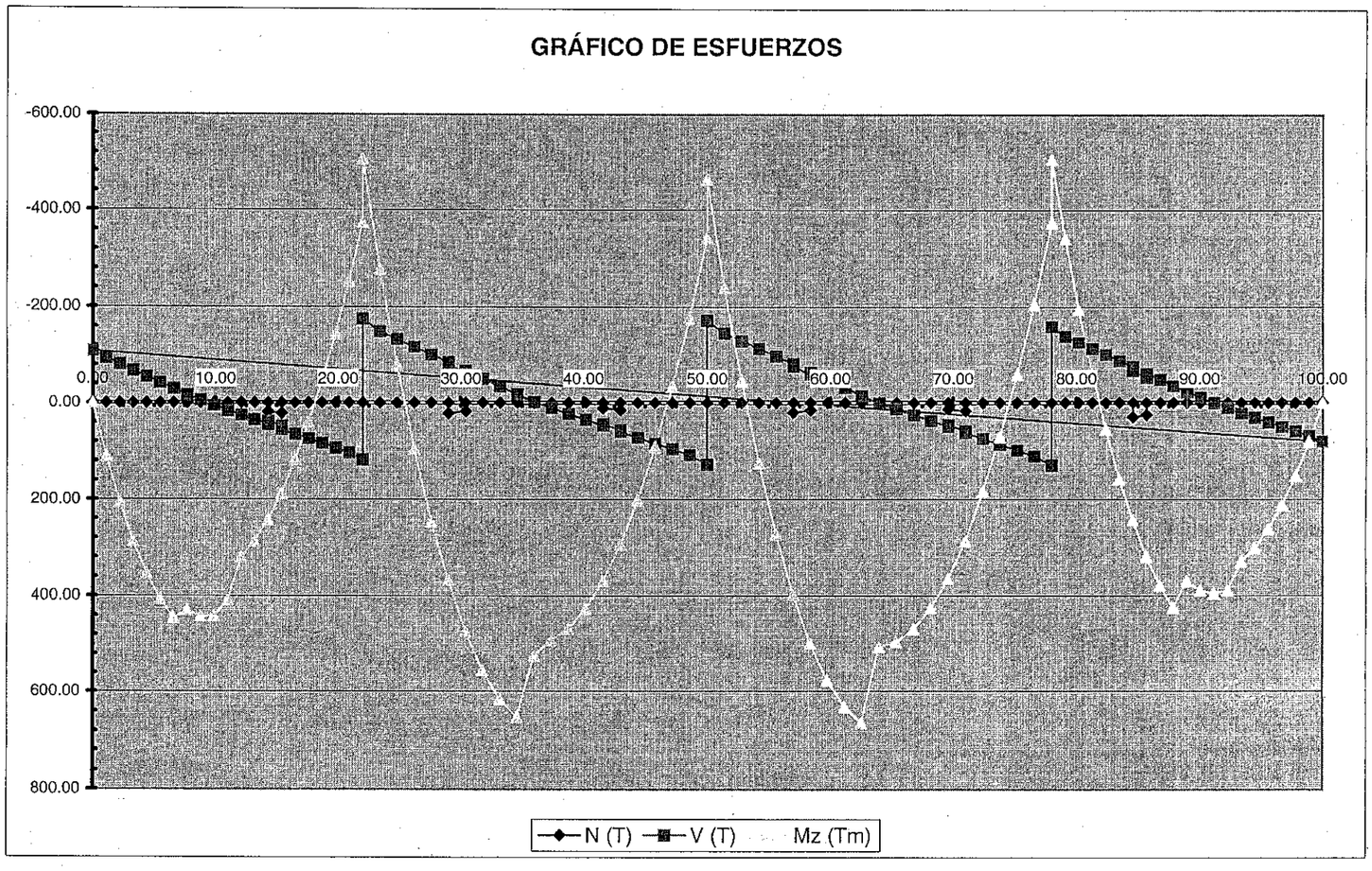
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60.00
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80.00
90.00
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N (T)
V (T)
Mz (Tm)

CÁLCULO TENSIONAL

Hipótesis de cálculo:
Envolvente CORTANTES

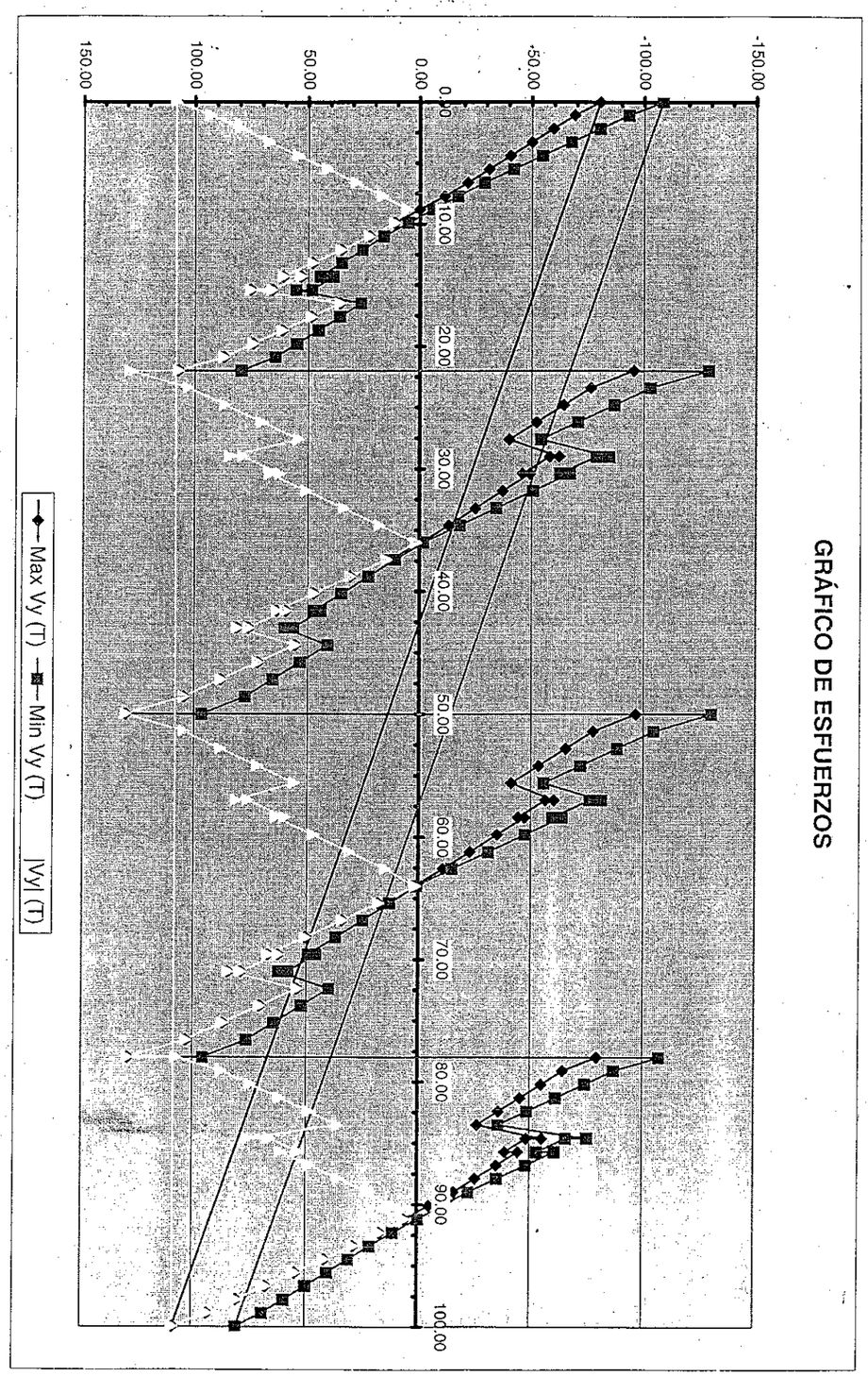
Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
1	1	0.00	0.00	-84.55	-474.20	474.20
1	2	1.10	0.00	-63.89	-424.54	424.54
2	2	1.10	-0.01	-64.55	-425.05	425.05
2	3	2.20	-0.01	-44.94	-377.47	377.47
3	3	2.20	0.00	-45.84	-377.67	377.67
3	4	3.30	0.00	-25.26	-331.16	331.16
4	4	3.30	0.00	-26.32	-330.98	330.98
4	5	4.40	0.00	-4.81	-285.10	285.10
5	5	4.40	0.00	-6.08	-284.72	284.72
5	6	5.50	0.00	16.36	-239.54	239.54
6	6	5.50	0.00	14.92	-238.89	238.89
6	7	6.60	0.00	38.23	-194.75	194.75
7	7	6.60	0.00	36.58	-193.93	193.93
7	8	7.70	0.00	61.55	-151.59	151.59
8	8	7.70	0.00	59.83	-150.51	150.51
8	9	8.80	0.00	93.89	-114.64	114.64
9	9	8.80	-0.01	91.40	-113.78	113.78
9	10	9.90	-0.01	131.27	-81.63	131.27
10	10	9.90	0.00	129.56	-82.08	129.56
10	11	11.00	0.00	170.91	-54.48	170.91
11	11	11.00	0.00	170.28	-55.41	170.28
11	12	12.10	0.00	213.89	-29.82	213.89
12	12	12.10	0.00	214.81	-31.41	214.81
12	13	13.20	0.00	258.99	-6.71	258.99
13	13	13.20	0.00	259.75	-8.01	259.75
13	14	14.30	0.00	304.94	14.84	304.94
14	14	14.30	6.06	295.89	11.72	295.89
14	15	15.40	6.93	341.72	34.02	341.72
15	15	15.40	0.00	353.28	35.10	353.28
15	16	16.50	0.00	399.38	57.16	399.38
16	16	16.50	0.00	400.24	55.71	400.24
16	17	17.60	0.00	446.85	77.01	446.85
17	17	17.60	0.00	447.95	75.22	447.95
17	18	18.70	0.00	495.92	96.02	495.92
18	18	18.70	0.00	496.84	94.14	496.84
18	19	19.80	0.00	545.24	113.32	545.24
19	19	19.80	0.00	545.91	112.78	545.91
19	20	20.90	0.00	594.72	130.24	594.72
20	20	20.90	0.00	594.97	130.15	594.97
20	21	22.00	0.00	651.54	148.55	651.54
21	1021	22.00	0.00	-163.14	-677.46	677.46
21	22	23.40	0.00	-139.90	-610.76	610.76
22	22	23.40	0.00	-141.33	-610.83	610.83
22	23	24.80	0.00	-117.11	-549.41	549.41
23	23	24.80	0.00	-119.07	-548.81	548.81
23	24	26.20	0.00	-93.92	-488.18	488.18
24	24	26.20	0.00	-96.28	-487.00	487.00
24	25	27.60	0.00	-70.13	-427.23	427.23
25	25	27.60	0.00	-72.92	-425.57	425.57
25	26	29.00	0.00	-45.57	-367.25	367.25
26	26	29.00	5.56	-48.18	-362.93	362.93

GRÁFICO DE ESFUERZOS



CÁLCULO TENSIONAL

Hipótesis de cálculo:
Envolvente CORTANTES

Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
26	27	30.40	4.39	-20.04	-305.33	305.33
27	27	30.40	0.00	-23.66	-304.64	304.64
27	28	31.80	0.00	5.69	-248.31	248.31
28	28	31.80	0.00	2.91	-246.24	246.24
28	29	33.20	0.00	34.19	-191.56	191.56
29	29	33.20	0.00	30.81	-189.09	189.09
29	30	34.60	0.00	63.34	-135.52	135.52
30	30	34.60	0.00	60.74	-133.74	133.74
30	31	36.00	0.00	97.53	-82.19	97.53
31	31	36.00	0.00	96.16	-82.94	96.16
31	32	37.40	0.00	147.20	-45.68	147.20
32	32	37.40	0.00	147.71	-47.84	147.71
32	33	38.80	0.00	201.13	-12.27	201.13
33	33	38.80	0.00	203.42	-15.49	203.42
33	34	40.20	0.00	257.93	18.51	257.93
34	34	40.20	0.00	259.86	15.98	259.86
34	35	41.60	0.00	315.95	47.41	315.95
35	35	41.60	2.87	316.41	44.42	316.41
35	36	43.00	3.75	373.99	73.41	373.99
36	36	43.00	0.00	376.84	73.09	376.84
36	37	44.40	0.00	435.33	102.34	435.33
37	37	44.40	0.00	437.36	99.31	437.36
37	38	45.80	0.00	496.97	126.82	496.97
38	38	45.80	0.00	498.67	124.35	498.67
38	39	47.20	0.00	559.39	150.57	559.39
39	39	47.20	0.00	560.59	148.40	560.59
39	40	48.60	0.00	622.12	173.86	622.12
40	40	48.60	0.00	622.66	172.05	622.66
40	41	50.00	0.00	688.73	199.44	688.73
41	1041	50.00	0.00	-177.82	-688.73	688.73
41	42	51.40	0.00	-147.67	-622.66	622.66
42	42	51.40	0.00	-149.78	-622.11	622.11
42	43	52.80	0.00	-125.64	-560.58	560.58
43	43	52.80	0.00	-128.20	-559.39	559.39
43	44	54.20	0.00	-103.13	-498.67	498.67
44	44	54.20	0.00	-106.07	-496.99	496.99
44	45	55.60	0.00	-79.96	-437.36	437.36
45	45	55.60	0.00	-83.04	-435.32	435.32
45	46	57.00	0.00	-55.90	-376.83	376.83
46	46	57.00	4.47	-55.27	-373.99	373.99
46	47	58.40	3.28	-27.15	-316.41	316.41
47	47	58.40	0.00	-31.62	-315.95	315.95
47	48	59.80	0.00	-2.50	-259.86	259.86
48	48	59.80	0.01	-4.91	-257.94	257.94
48	49	61.20	0.01	26.73	-203.41	203.41
49	49	61.20	0.00	23.61	-201.13	201.13
49	50	62.60	0.00	56.84	-147.71	147.71
50	50	62.60	0.00	54.76	-147.21	147.21
50	51	64.00	0.00	89.80	-96.02	96.02
51	51	64.00	0.00	89.15	-97.40	97.40
51	52	65.40	0.00	140.25	-58.73	140.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
Envolvente CORTANTES

Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
52	52	65.40	0.00	142.02	-61.42	142.02
52	53	66.80	0.00	195.54	-26.61	195.54
53	53	66.80	0.00	198.04	-30.06	198.04
53	54	68.20	0.00	252.63	3.48	252.63
54	54	68.20	0.00	254.69	0.59	254.69
54	55	69.60	0.00	310.98	32.22	310.98
55	55	69.60	3.84	308.23	28.49	308.23
55	56	71.00	4.71	365.75	58.90	365.75
56	56	71.00	0.00	374.22	56.17	374.22
56	57	72.40	0.00	432.49	85.77	432.49
57	57	72.40	0.00	434.18	82.82	434.18
57	58	73.80	0.00	493.89	111.26	493.89
58	58	73.80	-0.01	495.04	108.71	495.04
58	59	75.20	-0.01	555.59	136.15	555.59
59	59	75.20	0.00	556.20	133.97	556.20
59	60	76.60	0.00	617.55	160.45	617.55
60	60	76.60	0.00	617.51	158.81	617.51
60	61	78.00	0.00	689.41	184.32	689.41
61	1061	78.00	0.00	-135.24	-633.98	633.98
61	62	79.10	0.00	-115.83	-580.88	580.88
62	62	79.10	0.00	-117.12	-580.63	580.63
62	63	80.20	0.00	-98.66	-533.39	533.39
63	63	80.20	0.00	-100.21	-532.72	532.72
63	64	81.30	0.00	-81.30	-485.89	485.89
64	64	81.30	0.00	-83.06	-484.95	484.95
64	65	82.40	0.00	-63.69	-435.32	435.32
65	65	82.40	0.00	-65.36	-434.22	434.22
65	66	83.50	0.00	-45.48	-390.95	390.95
66	66	83.50	0.00	-46.86	-390.10	390.10
66	67	84.60	0.00	-26.22	-330.14	330.14
67	67	84.60	7.36	-25.05	-327.38	327.38
67	68	85.70	6.19	-4.17	-281.49	281.49
68	68	85.70	0.01	-7.22	-282.86	282.86
68	69	86.80	0.01	14.20	-237.63	237.63
69	69	86.80	0.00	12.99	-236.84	236.84
69	70	87.90	0.00	36.25	-192.58	192.58
70	70	87.90	0.00	34.74	-191.68	191.68
70	71	89.00	0.00	59.32	-151.01	151.01
71	71	89.00	0.00	58.24	-151.47	151.47
71	72	90.10	0.00	84.73	-112.99	112.99
72	72	90.10	0.00	84.39	-114.32	114.32
72	73	91.20	0.00	114.74	-77.02	114.74
73	73	91.20	0.00	115.63	-78.98	115.63
73	74	92.30	0.00	150.51	-56.04	150.51
74	74	92.30	0.00	151.55	-57.93	151.55
74	75	93.40	0.00	193.89	-32.24	193.89
75	75	93.40	0.00	194.72	-35.88	194.72
75	76	94.50	0.00	238.88	-10.78	238.88
76	76	94.50	0.00	239.54	-12.32	239.54
76	77	95.60	0.00	284.72	11.92	284.72
77	77	95.60	0.00	285.08	10.53	285.08

CÁLCULO TENSIONAL

Hipótesis de cálculo:

Envolvente CORTANTES

Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
77	78	96.70	0.00	330.98	33.84	330.98
78	78	96.70	0.00	331.15	32.63	331.15
78	79	97.80	0.00	377.65	55.02	377.65
79	79	97.80	0.01	377.48	53.97	377.48
79	80	98.90	0.01	425.04	75.38	425.04
80	80	98.90	0.00	424.52	74.55	424.52
80	81	100.00	0.00	474.18	102.99	474.18
101	101	0.00	0.00	-77.97	-511.15	511.15
101	102	1.10	0.00	-58.29	-458.21	458.21
102	102	1.10	-0.01	-59.00	-456.23	456.23
102	103	2.20	-0.01	-40.03	-405.80	405.80
103	103	2.20	0.00	-40.74	-403.95	403.95
103	104	3.30	0.00	-20.49	-354.98	354.98
104	104	3.30	0.00	-21.09	-353.23	353.23
104	105	4.40	0.00	0.37	-305.35	305.35
105	105	4.40	0.00	-0.25	-303.77	303.77
105	106	5.50	0.00	22.43	-256.57	256.57
106	106	5.50	0.00	21.73	-255.01	255.01
106	107	6.60	0.00	45.52	-209.17	209.17
107	107	6.60	0.00	44.71	-207.55	207.55
107	108	7.70	0.00	70.42	-163.80	163.80
108	108	7.70	0.00	69.71	-162.33	162.33
108	109	8.80	0.00	104.55	-124.67	124.67
109	109	8.80	0.00	103.49	-123.72	123.72
109	110	9.90	0.00	144.35	-89.51	144.35
110	110	9.90	0.00	144.28	-90.00	144.28
110	111	11.00	0.00	186.97	-60.67	186.97
111	111	11.00	0.00	188.39	-61.99	188.39
111	112	12.10	0.00	233.59	-34.93	233.59
112	112	12.10	0.00	236.03	-36.38	236.03
112	113	13.20	0.00	282.19	-11.38	282.19
113	113	13.20	0.00	284.57	-12.65	284.57
113	114	14.30	0.00	331.63	10.53	331.63
114	114	14.30	6.06	324.25	7.51	324.25
114	115	15.40	6.93	372.25	30.04	372.25
115	115	15.40	0.00	385.56	31.21	385.56
115	116	16.50	0.00	433.95	53.37	433.95
116	116	16.50	0.00	436.09	52.51	436.09
116	117	17.60	0.00	485.35	72.11	485.35
117	117	17.60	0.00	487.50	71.64	487.50
117	118	18.70	0.00	538.18	88.03	538.18
118	118	18.70	0.00	540.38	87.54	540.38
118	119	19.80	0.00	591.64	103.93	591.64
119	119	19.80	0.00	594.06	103.39	594.06
119	120	20.90	0.00	645.83	119.77	645.83
120	120	20.90	0.00	648.27	119.23	648.27
120	121	22.00	0.00	707.95	136.99	707.95
121	1121	22.00	0.00	-157.81	-730.22	730.22
121	122	23.40	0.00	-135.72	-659.59	659.59
122	122	23.40	0.00	-136.81	-656.93	656.93
122	123	24.80	0.00	-113.52	-591.89	591.89

CÁLCULO TENSIONAL

Hipótesis de cálculo:

Envolvente CORTANTES

Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
123	123	24.80	0.00	-114.85	-589.05	589.05
123	124	26.20	0.00	-90.30	-525.02	525.02
124	124	26.20	0.00	-91.88	-522.13	522.13
124	125	27.60	0.00	-66.05	-459.22	459.22
125	125	27.60	0.00	-67.76	-456.29	456.29
125	126	29.00	0.00	-40.48	-395.21	395.21
126	126	29.00	5.56	-41.69	-390.19	390.19
126	127	30.40	4.38	-13.34	-330.10	330.10
127	127	30.40	0.00	-15.47	-329.08	329.08
127	128	31.80	0.00	14.10	-270.37	270.37
128	128	31.80	0.00	12.19	-267.33	267.33
128	129	33.20	0.00	44.08	-210.87	210.87
129	129	33.20	0.00	41.40	-207.60	207.60
129	130	34.60	0.00	75.24	-152.48	152.48
130	130	34.60	0.00	73.48	-150.21	150.21
130	131	36.00	0.00	112.27	-97.47	112.27
131	131	36.00	0.00	111.61	-97.45	111.61
131	132	37.40	0.00	163.84	-57.99	163.84
132	132	37.40	0.00	165.15	-59.22	165.15
132	133	38.80	0.00	220.05	-21.76	220.05
133	133	38.80	0.00	223.22	-24.23	223.22
133	134	40.20	0.00	279.53	10.97	279.53
134	134	40.20	0.00	282.61	9.10	282.61
134	135	41.60	0.00	341.04	41.49	341.04
135	135	41.60	2.87	342.96	39.13	342.96
135	136	43.00	3.75	403.05	68.74	403.05
136	136	43.00	0.00	406.88	69.87	406.88
136	137	44.40	0.00	468.10	98.87	468.10
137	137	44.40	0.01	470.92	97.80	470.92
137	138	45.80	0.01	533.64	124.81	533.64
138	138	45.80	0.00	536.83	123.49	536.83
138	139	47.20	0.00	600.90	149.47	600.90
139	139	47.20	0.00	604.23	148.14	604.23
139	140	48.60	0.00	669.38	173.11	669.38
140	140	48.60	0.00	672.69	171.90	672.69
140	141	50.00	0.00	742.63	201.23	742.63
141	1141	50.00	0.01	-171.93	-742.62	742.62
141	142	51.40	0.01	-142.96	-672.70	672.70
142	142	51.40	0.00	-144.64	-669.40	669.40
142	143	52.80	0.00	-121.38	-604.24	604.24
143	143	52.80	0.00	-123.21	-600.94	600.94
143	144	54.20	0.00	-98.70	-536.83	536.83
144	144	54.20	0.00	-100.50	-533.65	533.65
144	145	55.60	0.00	-74.70	-470.93	470.93
145	145	55.60	0.00	-76.15	-468.10	468.10
145	146	57.00	0.00	-49.04	-406.88	406.88
146	146	57.00	4.47	-47.36	-403.06	403.06
146	147	58.40	3.28	-19.00	-342.99	342.99
147	147	58.40	0.00	-23.08	-341.05	341.05
147	148	59.80	0.00	6.51	-282.60	282.60
148	148	59.80	-0.01	4.51	-279.53	279.53

CÁLCULO TENSIONAL

Hipótesis de cálculo:

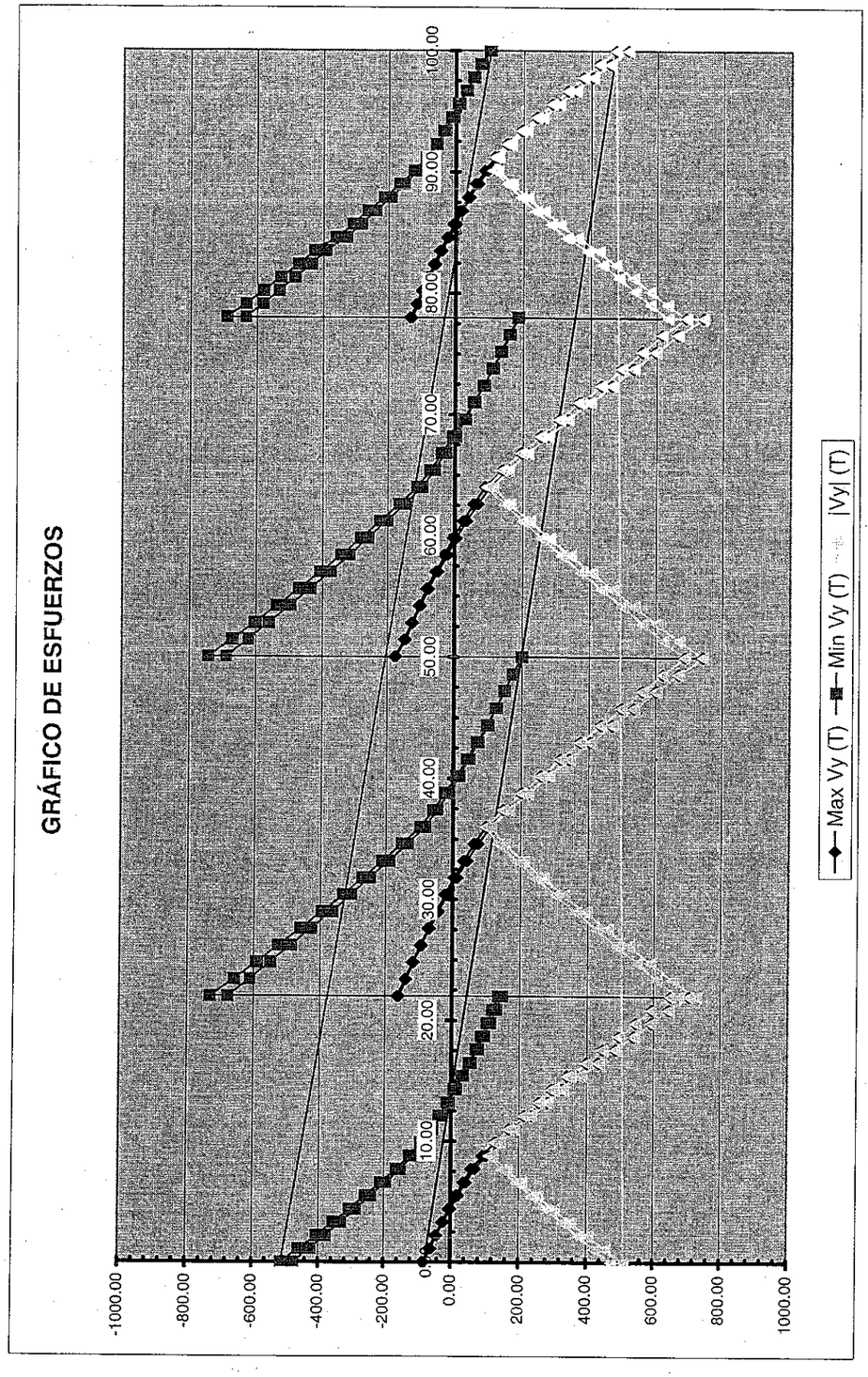
Envolvente CORTANTES

Envolvente CORTANTES

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Vy (T)	Min Vy (T)	|Vy| (T)
148	149	61.20	-0.01	36.89	-223.22	223.22
149	149	61.20	0.00	34.33	-220.05	220.05
149	150	62.60	0.00	68.99	-165.15	165.15
150	150	62.60	0.00	67.66	-163.84	163.84
150	151	64.00	0.00	104.35	-111.57	111.57
151	151	64.00	0.00	104.41	-112.09	112.09
151	152	65.40	0.00	156.70	-70.94	156.70
152	152	65.40	0.00	158.99	-72.63	158.99
152	153	66.80	0.00	214.03	-36.01	214.03
153	153	66.80	0.00	217.32	-38.61	217.32
153	154	68.20	0.00	273.73	-3.97	273.73
154	154	68.20	0.00	276.76	-5.76	276.76
154	155	69.60	0.00	335.42	26.56	335.42
155	155	69.60	3.84	333.00	24.57	333.00
155	156	71.00	4.71	393.01	55.67	393.01
156	156	71.00	0.00	402.17	54.61	402.17
156	157	72.40	0.00	463.23	84.66	463.23
157	157	72.40	0.00	466.13	83.11	466.13
157	158	73.80	0.00	528.97	111.70	528.97
158	158	73.80	0.00	531.88	110.31	531.88
158	159	75.20	0.00	595.85	137.59	595.85
159	159	75.20	0.00	598.69	136.50	598.69
159	160	76.60	0.00	663.69	162.55	663.69
160	160	76.60	0.00	666.35	161.68	666.35
160	161	78.00	0.00	742.16	186.52	742.16
161	1161	78.00	0.00	-127.76	-690.35	690.35
161	162	79.10	0.00	-109.25	-634.20	634.20
162	162	79.10	0.01	-110.24	-631.76	631.76
162	163	80.20	0.01	-92.57	-581.56	581.56
163	163	80.20	0.01	-93.58	-579.10	579.10
163	164	81.30	0.01	-75.30	-529.42	529.42
164	164	81.30	0.00	-76.15	-527.24	527.24
164	165	82.40	0.00	-57.29	-474.91	474.91
165	165	82.40	0.00	-58.23	-472.74	472.74
165	166	83.50	0.00	-38.71	-426.79	426.79
166	166	83.50	0.00	-39.68	-424.65	424.65
166	167	84.60	0.00	-19.27	-362.40	362.40
167	167	84.60	7.36	-18.16	-357.89	357.89
167	168	85.70	6.19	2.62	-309.86	309.86
168	168	85.70	0.00	-0.51	-309.52	309.52
168	169	86.80	0.00	20.93	-262.42	262.42
169	169	86.80	0.00	19.59	-260.05	260.05
169	170	87.90	0.00	42.87	-213.82	213.82
170	170	87.90	0.00	41.32	-211.34	211.34
170	171	89.00	0.00	67.82	-166.13	166.13
171	171	89.00	0.00	66.38	-164.72	164.72
171	172	90.10	0.00	93.59	-124.09	124.09
172	172	90.10	0.00	93.01	-124.18	124.18
172	173	91.20	0.00	125.04	-86.42	125.04
173	173	91.20	0.00	125.87	-87.33	125.87
173	174	92.30	0.00	162.32	-54.23	162.32



ENVOLVENTE DE ROTURA A TORSIÓN

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
1	1	0.00	0.00	12.47	-5.99	12.47
1	2	1.10	0.00	16.53	-31.88	31.88
2	2	1.10	-0.01	33.62	-34.70	34.70
2	3	2.20	-0.01	37.08	-48.64	48.64
3	3	2.20	0.00	51.56	-50.03	51.56
3	4	3.30	0.00	54.38	-62.79	62.79
4	4	3.30	0.00	71.60	-62.86	71.60
4	5	4.40	0.00	75.10	-85.39	85.39
5	5	4.40	0.00	86.78	-84.28	86.78
5	6	5.50	0.00	89.23	-95.66	95.66
6	6	5.50	0.00	101.06	-95.53	101.06
6	7	6.60	0.00	102.33	-107.38	107.38
7	7	6.60	0.00	113.21	-108.30	113.21
7	8	7.70	0.00	112.90	-117.93	117.93
8	8	7.70	0.00	126.72	-120.03	126.72
8	9	8.80	0.00	125.05	-136.88	136.88
9	9	8.80	-0.01	140.18	-139.52	140.18
9	10	9.90	-0.01	137.13	-147.15	147.15
10	10	9.90	0.00	152.61	-149.94	152.61
10	11	11.00	0.00	150.04	-159.42	159.42
11	11	11.00	0.00	165.73	-162.42	165.73
11	12	12.10	0.00	159.96	-168.26	168.26
12	12	12.10	0.00	175.27	-170.92	175.27
12	13	13.20	0.00	168.51	-182.67	182.67
13	13	13.20	0.00	183.40	-184.62	184.62
13	14	14.30	0.00	175.93	-189.04	189.04
14	14	14.30	1.19	190.22	-190.43	190.43
14	15	15.40	6.93	182.30	-199.15	199.15
15	15	15.40	0.00	195.82	-200.30	200.30
15	16	16.50	0.00	189.96	-203.98	203.98
16	16	16.50	0.00	202.79	-204.18	204.18
16	17	17.60	0.00	194.68	-213.44	213.44
17	17	17.60	0.00	206.38	-212.36	212.36
17	18	18.70	0.00	198.83	-216.35	216.35
18	18	18.70	0.00	209.24	-214.24	214.24
18	19	19.80	0.00	204.13	-218.97	218.97
19	19	19.80	0.00	213.29	-215.78	215.78
19	20	20.90	0.00	208.12	-221.49	221.49
20	20	20.90	0.00	216.14	-217.23	217.23
20	21	22.00	0.00	212.16	-228.58	228.58
21	1021	22.00	0.00	208.15	-222.71	222.71
21	22	23.40	0.00	202.69	-231.44	231.44
22	22	23.40	0.00	211.33	-222.98	222.98
22	23	24.80	0.00	208.22	-233.41	233.41
23	23	24.80	0.00	214.62	-223.45	223.45
23	24	26.20	0.00	212.80	-240.06	240.06
24	24	26.20	0.00	217.05	-228.24	228.24
24	25	27.60	0.00	215.89	-240.37	240.37
25	25	27.60	0.00	218.06	-227.25	227.25
25	26	29.00	0.00	217.06	-239.53	239.53
26	26	29.00	0.36	217.59	-225.56	225.56

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
26	27	30.40	3.84	216.36	-242.25	242.25
27	27	30.40	0.00	215.93	-227.64	227.64
27	28	31.80	0.00	214.05	-239.23	239.23
28	28	31.80	0.00	213.66	-225.07	225.07
28	29	33.20	0.00	226.03	-235.75	235.75
29	29	33.20	0.00	225.82	-222.75	225.82
29	30	34.60	0.00	222.27	-232.30	232.30
30	30	34.60	0.00	220.71	-222.13	222.13
30	31	36.00	0.00	215.42	-232.06	232.06
31	31	36.00	0.00	223.07	-224.87	224.87
31	32	37.40	0.00	215.95	-231.94	231.94
32	32	37.40	0.00	228.12	-228.52	228.52
32	33	38.80	0.00	219.25	-234.71	234.71
33	33	38.80	0.00	234.29	-234.07	234.29
33	34	40.20	0.00	223.92	-239.12	239.12
34	34	40.20	0.00	239.80	-239.36	239.80
34	35	41.60	0.00	228.26	-243.49	243.49
35	35	41.60	-0.72	243.78	-243.29	243.78
35	36	43.00	3.16	231.64	-246.86	246.86
36	36	43.00	0.00	246.32	-245.58	246.32
36	37	44.40	0.00	234.04	-249.00	249.00
37	37	44.40	0.00	247.45	-246.20	247.45
37	38	45.80	0.00	235.47	-249.93	249.93
38	38	45.80	0.00	247.57	-245.72	247.57
38	39	47.20	0.00	236.58	-250.16	250.16
39	39	47.20	0.00	247.22	-244.55	247.22
39	40	48.60	0.00	237.72	-250.16	250.16
40	40	48.60	0.00	246.47	-242.91	246.47
40	41	50.00	0.00	239.44	-250.56	250.56
41	1041	50.00	0.00	232.98	-241.71	241.71
41	42	51.40	0.00	225.66	-249.75	249.75
42	42	51.40	0.00	232.96	-239.60	239.60
42	43	52.80	0.00	228.17	-249.64	249.64
43	43	52.80	0.00	233.40	-238.11	238.11
43	44	54.20	0.00	230.20	-249.31	249.31
44	44	54.20	0.00	233.67	-236.81	236.81
44	45	55.60	0.00	231.43	-248.77	248.77
45	45	55.60	0.00	233.33	-235.32	235.32
45	46	57.00	0.00	231.41	-247.62	247.62
46	46	57.00	-0.75	231.58	-233.15	233.15
46	47	58.40	2.28	229.49	-245.29	245.29
47	47	58.40	0.00	228.45	-230.11	230.11
47	48	59.80	0.00	225.72	-241.73	241.73
48	48	59.80	0.01	224.33	-226.11	226.11
48	49	61.20	0.01	220.38	-236.82	236.82
49	49	61.20	0.00	234.71	-221.83	234.71
49	50	62.60	0.00	230.34	-231.40	231.40
50	50	62.60	0.00	227.41	-219.00	227.41
50	51	64.00	0.00	221.72	-227.23	227.23
51	51	64.00	0.00	228.16	-218.51	228.16
51	52	65.40	0.00	219.17	-225.33	225.33

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
52	52	65.40	0.00	229.23	-220.31	229.23
52	53	66.80	0.00	220.22	-225.83	225.83
53	53	66.80	0.00	233.43	-223.71	233.43
53	54	68.20	0.00	222.94	-228.01	228.01
54	54	68.20	0.00	237.52	-226.97	237.52
54	55	69.60	0.00	225.37	-230.28	230.28
55	55	69.60	0.41	240.39	-229.25	240.39
55	56	71.00	4.71	224.31	-231.92	231.92
56	56	71.00	0.00	238.57	-230.15	238.57
56	57	72.40	0.00	226.27	-232.57	232.57
57	57	72.40	0.00	239.47	-229.35	239.47
57	58	73.80	0.00	227.34	-231.91	231.91
58	58	73.80	-0.01	239.04	-226.78	239.04
58	59	75.20	-0.01	222.43	-229.96	229.96
59	59	75.20	0.00	232.06	-222.80	232.06
59	60	76.60	0.00	221.88	-226.96	226.96
60	60	76.60	0.00	229.63	-217.89	229.63
60	61	78.00	0.00	221.54	-223.88	223.88
61	1061	78.00	0.00	212.69	-213.76	213.76
61	62	79.10	0.00	201.31	-218.90	218.90
62	62	79.10	0.00	205.78	-209.35	209.35
62	63	80.20	0.00	200.45	-215.39	215.39
63	63	80.20	0.00	203.80	-204.86	204.86
63	64	81.30	0.00	199.76	-210.51	210.51
64	64	81.30	0.00	201.78	-199.15	201.78
64	65	82.40	0.00	198.77	-206.99	206.99
65	65	82.40	0.00	199.50	-194.70	199.50
65	66	83.50	0.00	191.42	-202.93	202.93
66	66	83.50	0.00	190.70	-189.77	190.70
66	67	84.60	0.00	188.31	-198.14	198.14
67	67	84.60	1.14	186.53	-184.20	186.53
67	68	85.70	6.06	179.12	-189.93	189.93
68	68	85.70	0.01	177.07	-175.58	177.07
68	69	86.80	0.01	173.93	-183.18	183.18
69	69	86.80	0.00	171.34	-168.25	171.34
69	70	87.90	0.00	160.75	-175.24	175.24
70	70	87.90	0.00	157.54	-159.85	159.85
70	71	89.00	0.00	152.71	-166.02	166.02
71	71	89.00	0.00	159.42	-150.17	159.42
71	72	90.10	0.00	151.32	-153.34	153.34
72	72	90.10	0.00	145.56	-137.49	145.56
72	73	91.20	0.00	139.06	-141.39	141.39
73	73	91.20	0.00	135.53	-125.53	135.53
73	74	92.30	0.00	119.59	-128.28	128.28
74	74	92.30	0.00	117.05	-113.28	117.05
74	75	93.40	0.00	108.11	-114.87	114.87
75	75	93.40	0.00	106.93	-100.87	106.93
75	76	94.50	0.00	95.61	-101.06	101.06
76	76	94.50	0.00	95.58	-87.65	95.58
76	77	95.60	0.00	84.60	-86.80	86.80
77	77	95.60	0.00	85.58	-73.47	85.58

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
77	78	96.70	0.00	63.39	-71.60	71.60
78	78	96.70	0.00	63.13	-57.50	63.13
78	79	97.80	0.00	50.75	-54.71	54.71
79	79	97.80	0.01	48.98	-39.04	48.98
79	80	98.90	0.01	35.56	-35.31	35.56
80	80	98.90	0.00	32.06	-17.15	32.06
80	81	100.00	0.00	6.47	-12.47	12.47
101	101	0.00	0.00	5.44	-8.15	8.15
101	102	1.10	0.00	20.75	-11.93	20.75
102	102	1.10	-0.01	23.69	-21.97	23.69
102	103	2.20	-0.01	30.97	-24.65	30.97
103	103	2.20	0.00	33.32	-34.33	34.33
103	104	3.30	0.00	39.76	-36.19	39.76
104	104	3.30	0.00	42.62	-46.81	46.81
104	105	4.40	0.00	55.09	-48.01	55.09
105	105	4.40	0.00	57.47	-58.92	58.92
105	106	5.50	0.00	63.15	-59.58	63.15
106	106	5.50	0.00	65.48	-70.85	70.85
106	107	6.60	0.00	71.52	-70.91	71.52
107	107	6.60	0.00	74.13	-82.54	82.54
107	108	7.70	0.00	78.96	-81.83	81.83
108	108	7.70	0.00	81.84	-93.56	93.56
108	109	8.80	0.00	91.01	-92.25	92.25
109	109	8.80	0.00	94.12	-103.92	103.92
109	110	9.90	0.00	97.41	-102.09	102.09
110	110	9.90	0.00	99.20	-113.60	113.60
110	111	11.00	0.00	103.59	-112.62	112.62
111	111	11.00	0.00	118.59	-123.76	123.76
111	112	12.10	0.00	120.22	-120.73	120.73
112	112	12.10	0.00	124.67	-131.17	131.17
112	113	13.20	0.00	130.09	-127.76	130.09
113	113	13.20	0.00	133.83	-137.36	137.36
113	114	14.30	0.00	134.70	-133.62	134.70
114	114	14.30	6.06	137.75	-142.17	142.17
114	115	15.40	1.14	141.83	-138.52	141.83
115	115	15.40	0.00	144.98	-147.15	147.15
115	116	16.50	0.00	145.45	-143.96	145.45
116	116	16.50	0.00	148.25	-151.23	151.23
116	117	17.60	0.00	152.11	-147.09	152.11
117	117	17.60	0.00	154.59	-154.43	154.59
117	118	18.70	0.00	154.96	-150.67	154.96
118	118	18.70	0.00	158.09	-158.22	158.22
118	119	19.80	0.00	159.68	-155.82	159.68
119	119	19.80	0.00	163.05	-162.52	163.05
119	120	20.90	0.00	164.43	-160.56	164.43
120	120	20.90	0.00	166.06	-166.17	166.17
120	121	22.00	0.00	170.38	-164.40	170.38
121	1121	22.00	0.00	156.90	-170.18	170.18
121	122	23.40	0.00	163.74	-168.39	168.39
122	122	23.40	0.00	160.66	-171.78	171.78
122	123	24.80	0.00	167.90	-170.43	170.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
123	123	24.80	0.00	161.71	-171.12	171.12
123	124	26.20	0.00	169.56	-170.12	170.12
124	124	26.20	0.00	161.99	-169.18	169.18
124	125	27.60	0.00	169.09	-168.39	169.09
125	125	27.60	0.00	159.96	-166.21	166.21
125	126	29.00	0.00	167.10	-165.48	167.10
126	126	29.00	4.70	158.15	-163.62	163.62
126	127	30.40	0.40	167.89	-162.83	167.89
127	127	30.40	0.00	160.43	-164.23	164.23
127	128	31.80	0.00	166.76	-162.52	166.76
128	128	31.80	0.00	161.11	-167.47	167.47
128	129	33.20	0.00	167.08	-165.31	167.08
129	129	33.20	0.00	161.31	-170.49	170.49
129	130	34.60	0.00	166.77	-167.73	167.73
130	130	34.60	0.00	161.20	-173.44	173.44
130	131	36.00	0.00	166.88	-170.10	170.10
131	131	36.00	0.00	161.96	-176.56	176.56
131	132	37.40	0.00	165.34	-172.58	172.58
132	132	37.40	0.00	157.31	-179.62	179.62
132	133	38.80	0.00	159.77	-175.05	175.05
133	133	38.80	0.00	173.10	-182.07	182.07
133	134	40.20	0.00	173.92	-176.95	176.95
134	134	40.20	0.00	173.67	-184.43	184.43
134	135	41.60	0.00	174.10	-178.92	178.92
135	135	41.60	2.28	176.53	-187.57	187.57
135	136	43.00	-0.75	176.01	-181.81	181.81
136	136	43.00	0.00	183.25	-194.05	194.05
136	137	44.40	0.00	182.68	-187.64	187.64
137	137	44.40	0.01	190.02	-200.60	200.60
137	138	45.80	0.01	189.54	-194.14	194.14
138	138	45.80	0.00	195.42	-205.01	205.01
138	139	47.20	0.00	195.16	-199.04	199.04
139	139	47.20	0.00	198.68	-207.31	207.31
139	140	48.60	0.00	198.79	-201.45	201.45
140	140	48.60	0.00	200.14	-207.14	207.14
140	141	50.00	0.00	201.10	-202.61	202.61
141	1141	50.00	0.01	184.23	-205.04	205.04
141	142	51.40	0.01	189.58	-202.92	202.92
142	142	51.40	0.00	183.01	-202.69	202.69
142	143	52.80	0.00	190.15	-201.04	201.04
143	143	52.80	0.00	181.03	-198.78	198.78
143	144	54.20	0.00	188.33	-197.48	197.48
144	144	54.20	0.00	176.61	-192.99	192.99
144	145	55.60	0.00	184.42	-191.94	191.94
145	145	55.60	0.00	170.57	-186.22	186.22
145	146	57.00	0.00	178.36	-185.24	185.24
146	146	57.00	3.16	165.16	-179.70	179.70
146	147	58.40	-0.72	172.30	-178.69	178.69
147	147	58.40	0.00	162.60	-178.03	178.03
147	148	59.80	0.00	169.47	-176.07	176.07
148	148	59.80	-0.01	160.91	-178.18	178.18

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1]eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
148	149	61.20	-0.01	167.35	-175.80	175.80
149	149	61.20	0.00	159.13	-179.10	179.10
149	150	62.60	0.00	165.00	-176.22	176.22
150	150	62.60	0.00	157.20	-180.05	180.05
150	151	64.00	0.00	161.89	-176.81	176.81
151	151	64.00	0.00	155.54	-181.44	181.44
151	152	65.40	0.00	158.90	-176.60	176.60
152	152	65.40	0.00	149.16	-181.16	181.16
152	153	66.80	0.00	151.52	-176.93	176.93
153	153	66.80	0.00	147.16	-181.42	181.42
153	154	68.20	0.00	163.27	-176.75	176.75
154	154	68.20	0.00	160.17	-181.16	181.16
154	155	69.60	0.00	160.35	-175.71	175.71
155	155	69.60	3.84	160.74	-181.97	181.97
155	156	71.00	0.36	160.01	-174.01	174.01
156	156	71.00	0.00	163.60	-181.93	181.93
156	157	72.40	0.00	162.79	-176.09	176.09
157	157	72.40	0.00	166.66	-184.24	184.24
157	158	73.80	0.00	165.91	-178.41	178.41
158	158	73.80	0.00	168.46	-184.99	184.99
158	159	75.20	0.00	167.93	-178.39	178.39
159	159	75.20	0.00	168.78	-183.60	183.60
159	160	76.60	0.00	168.60	-177.56	177.56
160	160	76.60	0.00	166.75	-179.59	179.59
160	161	78.00	0.00	166.98	-173.85	173.85
161	1161	78.00	0.00	148.39	-172.79	172.79
161	162	79.10	0.00	150.32	-168.14	168.14
162	162	79.10	0.01	144.26	-166.92	166.92
162	163	80.20	0.01	146.97	-164.71	164.71
163	163	80.20	0.01	139.70	-162.03	162.03
163	164	81.30	0.01	143.24	-159.21	159.21
164	164	81.30	0.00	135.11	-156.89	156.89
164	165	82.40	0.00	140.07	-155.31	155.31
165	165	82.40	0.00	132.19	-153.74	153.74
165	166	83.50	0.00	137.53	-148.66	148.66
166	166	83.50	0.00	129.70	-146.87	146.87
166	167	84.60	0.00	135.14	-145.20	145.20
167	167	84.60	6.93	126.50	-143.15	143.15
167	168	85.70	1.19	129.82	-137.87	137.87
168	168	85.70	0.00	120.67	-136.00	136.00
168	169	86.80	0.00	125.67	-133.88	133.88
169	169	86.80	0.00	115.43	-131.45	131.45
169	170	87.90	0.00	120.15	-124.82	124.82
170	170	87.90	0.00	109.06	-121.71	121.71
170	171	89.00	0.00	113.34	-118.90	118.90
171	171	89.00	0.00	101.57	-115.40	115.40
171	172	90.10	0.00	103.81	-110.44	110.44
172	172	90.10	0.00	91.99	-106.92	106.92
172	173	91.20	0.00	94.76	-103.39	103.39
173	173	91.20	0.00	83.24	-99.81	99.81
173	174	92.30	0.00	85.13	-90.71	90.71

CÁLCULO TENSIONAL

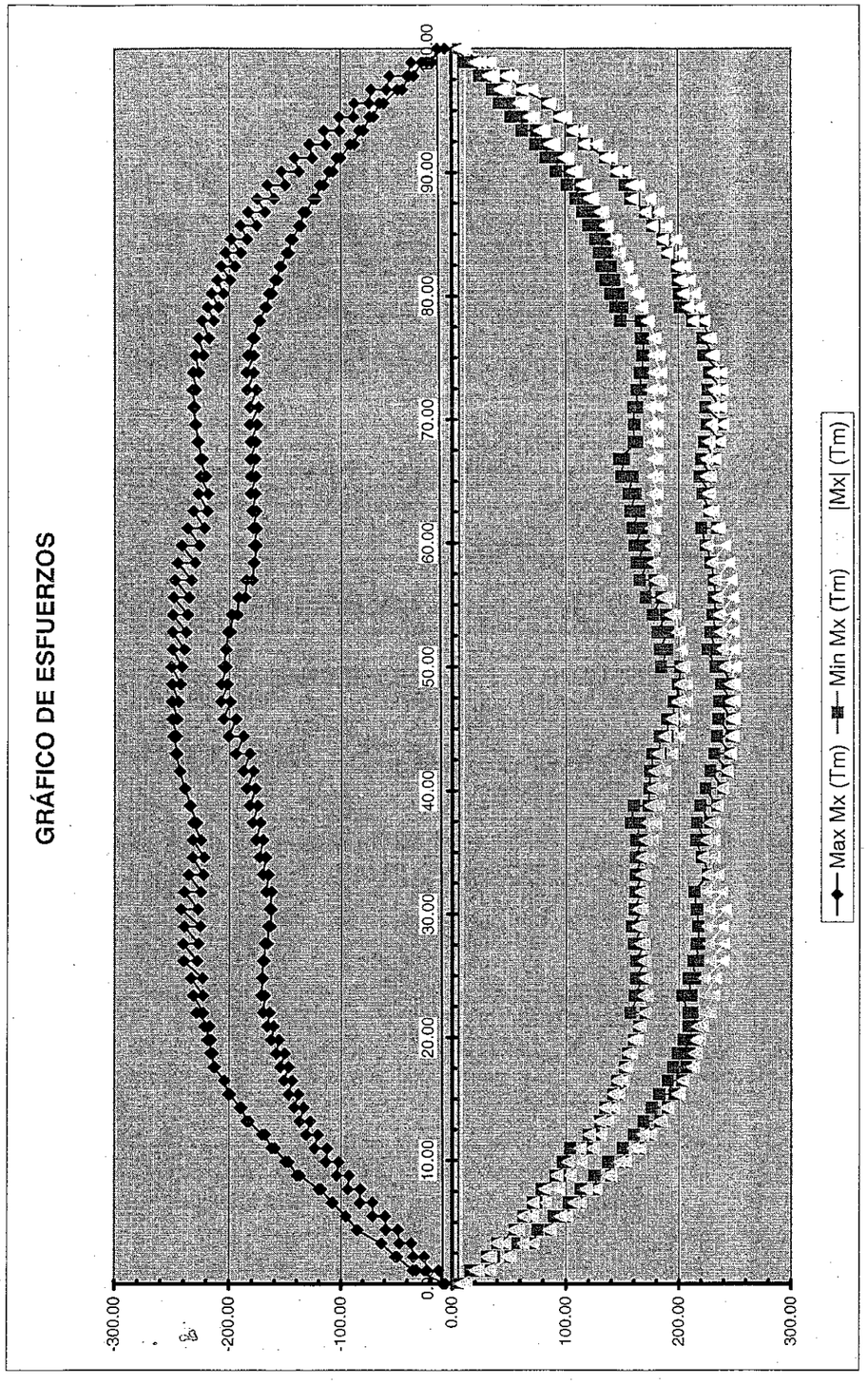
Hipótesis de cálculo:
ENVOLVENTE Torsores

ENVOLVENTE Torsores

[1; 1.35]PPVF1 + [1; 1.35]PPLACAS + [1; 1.35]HLP + [1; 1]eje1f3.HIP.To + [1; 1)eje2f3.HIP.To + [1; 1.35]HLCV + [.7; 1.

Coef. exc:

Barra	Nudo	X	N (T)	Max Mx (Tm)	Min Mx (Tm)	|Mx| (Tm)
174	174	92.30	0.00	74.02	-86.91	86.91
174	175	93.40	0.00	75.01	-82.49	82.49
175	175	93.40	0.00	62.62	-78.54	78.54
175	176	94.50	0.00	62.74	-73.01	73.01
176	176	94.50	0.00	52.49	-69.23	69.23
176	177	95.60	0.00	52.06	-63.99	63.99
177	177	95.60	0.00	42.22	-60.09	60.09
177	178	96.70	0.00	41.28	-48.01	48.01
178	178	96.70	0.00	36.49	-43.56	43.56
178	179	97.80	0.00	33.41	-37.42	37.42
179	179	97.80	-0.01	25.12	-33.43	33.43
179	180	98.90	-0.01	21.21	-26.35	26.35
180	180	98.90	0.00	12.50	-21.63	21.63
180	181	100.00	0.00	7.82	-6.09	7.82



REACCIONES EN ESTADOS INDIVIDUALES

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
PPVF1

Peso Propio Vigas Fase 1

[1; 1]PPVF1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	35.67	0.00
21	0.00	39.07	0.00
1021	0.00	49.84	0.00
41	0.00	49.84	0.00
1041	0.00	49.84	0.00
61	0.00	49.84	0.00
1061	0.00	39.07	0.00
81	0.00	35.67	0.00
101	0.00	35.67	0.00
121	0.00	39.07	0.00
1121	0.00	49.84	0.00
141	0.00	49.84	0.00
1141	0.00	49.84	0.00
161	0.00	49.84	0.00
1161	0.00	39.07	0.00
181	0.00	35.67	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	11.22	0.00
21	0.00	11.22	0.00
1021	0.00	14.28	0.00
41	0.00	14.28	0.00
1041	0.00	14.28	0.00
61	0.00	14.28	0.00
1061	0.00	11.22	0.00
81	0.00	11.22	0.00
101	0.00	11.22	0.00
121	0.00	11.22	0.00
1121	0.00	14.28	0.00
141	0.00	14.28	0.00
1141	0.00	14.28	0.00
161	0.00	14.28	0.00
1161	0.00	11.22	0.00
181	0.00	11.22	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.77	0.00
21	0.00	60.52	0.00
1021	0.00	0.00	0.00
41	0.00	64.87	0.00
1041	0.00	0.00	0.00
61	0.00	60.52	0.00
1061	0.00	0.00	0.00
81	0.00	0.77	0.00
101	0.00	0.77	0.00
121	0.00	60.52	0.00
1121	0.00	0.00	0.00
141	0.00	64.87	0.00
1141	0.00	0.00	0.00
161	0.00	60.52	0.00
1161	0.00	0.00	0.00
181	0.00	0.77	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.77	0.00
21	0.00	60.52	0.00
1021	0.00	0.00	0.00
41	0.00	64.87	0.00
1041	0.00	0.00	0.00
61	0.00	60.52	0.00
1061	0.00	0.00	0.00
81	0.00	0.77	0.00
101	0.00	0.77	0.00
121	0.00	60.52	0.00
1121	0.00	0.00	0.00
141	0.00	64.87	0.00
1141	0.00	0.00	0.00
161	0.00	60.52	0.00
1161	0.00	0.00	0.00
181	0.00	0.77	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
HLCV

Hormigonado losa centros de vano

[1; 1]HLCV

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	32.64	0.00
21	0.00	72.99	0.00
41	0.00	62.06	0.00
61	0.00	72.99	0.00
81	0.00	32.64	0.00
101	0.00	32.64	0.00
121	0.00	72.99	0.00
141	0.00	62.06	0.00
161	0.00	72.99	0.00
181	0.00	32.64	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
PPVEI

Peso propio vigas en estructura ideal

[1; 1]PPVEI

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	25.05	0.00
21	0.00	85.05	0.00
41	0.00	86.78	0.00
61	0.00	85.05	0.00
81	0.00	25.05	0.00
101	0.00	25.05	0.00
121	0.00	85.05	0.00
141	0.00	86.78	0.00
161	0.00	85.05	0.00
181	0.00	25.05	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	45.78	0.00
21	0.00	155.42	-1.25
41	0.00	158.57	-1.25
61	0.00	155.42	-0.98
81	0.00	45.78	0.00
101	0.00	45.78	0.00
121	0.00	155.42	1.25
141	0.00	158.58	1.25
161	0.00	155.42	0.98
181	0.00	45.78	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	52.95	0.00
21	0.00	179.62	1.15
41	0.00	183.08	1.54
61	0.00	179.62	1.64
81	0.00	52.95	0.00
101	0.00	43.03	0.00
121	0.00	146.17	-3.29
141	0.00	149.32	-2.90
161	0.00	146.18	-1.86
181	0.00	43.03	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	19.67	0.00
21	0.00	66.77	-4.29
41	0.00	68.13	-4.30
61	0.00	66.77	-3.38
81	0.00	19.67	0.00
101	0.00	19.67	0.00
121	0.00	66.77	4.29
141	0.00	68.13	4.30
161	0.00	66.77	3.38
181	0.00	19.67	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
GRAD

Gradiente térmico

[1; 1]GRAD

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	14.58	0.00
21	0.00	-18.02	0.00
41	0.00	6.88	0.00
61	0.00	-18.02	0.00
81	0.00	14.57	0.00
101	0.00	14.58	0.00
121	0.00	-18.02	0.00
141	0.00	6.88	0.00
161	0.00	-18.02	0.00
181	0.00	14.57	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.Mx- + [0; 1]SCI

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	9.81	0.00
21	0.00	31.68	-0.06
41	0.00	32.24	-1.74
61	0.00	31.68	-3.18
81	0.00	9.81	0.00
101	0.00	0.13	0.00
121	0.00	0.10	0.82
141	0.00	0.00	0.00
161	0.00	0.10	-0.77
181	0.00	0.13	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.Mx- + [0; 1]SCI

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-0.67	0.00
21	0.00	-0.80	-2.36
41	0.00	-0.96	-0.20
61	0.00	-0.80	2.18
81	0.00	-0.67	0.00
101	0.00	-3.15	0.00
121	0.00	-10.19	-1.65
141	0.00	-10.08	-0.34
161	0.00	-10.19	1.02
181	0.00	-3.15	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [(

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.13	0.00
21	0.00	0.10	-0.82
41	0.00	0.00	0.00
61	0.00	0.10	0.77
81	0.00	0.13	0.00
101	0.00	9.81	0.00
121	0.00	31.68	0.06
141	0.00	32.24	1.74
161	0.00	31.68	3.18
181	0.00	9.81	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [0

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-3.15	0.00
21	0.00	-10.19	1.65
41	0.00	-10.08	0.34
61	0.00	-10.19	-1.02
81	0.00	-3.15	0.00
101	0.00	-0.67	0.00
121	0.00	-0.80	2.36
141	0.00	-0.96	0.20
161	0.00	-0.80	-2.18
181	0.00	-0.67	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIA1

Carga uniforme tren A eje 1

[1; 1]CUNIA1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	6.70	0.00
21	0.00	22.68	0.27
41	0.00	23.04	0.49
61	0.00	22.68	0.62
81	0.00	6.70	0.00
101	0.00	1.17	0.00
121	0.00	4.03	-0.37
141	0.00	4.21	-0.16
161	0.00	4.03	0.11
181	0.00	1.17	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIA2

Carga uniforme tran A eje 2

[1; 1]CUNIA2

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.96	0.00
21	0.00	3.32	0.44
41	0.00	3.51	0.18
61	0.00	3.32	-0.14
81	0.00	0.96	0.00
101	0.00	7.50	0.00
121	0.00	25.38	-0.09
141	0.00	25.77	-0.35
161	0.00	25.38	-0.55
181	0.00	7.50	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	73.38	0.00
21	0.00	219.99	-13.24
41	0.00	231.66	2.94
61	0.00	220.00	19.79
81	0.00	73.38	0.00
101	0.00	15.58	0.00
121	0.00	41.67	-0.84
141	0.00	42.97	-1.23
161	0.00	41.67	-1.34
181	0.00	15.58	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-13.10	0.00
21	0.00	-15.88	15.67
41	0.00	-24.34	1.46
61	0.00	-15.88	-14.19
81	0.00	-13.10	0.00
101	0.00	-5.06	0.00
121	0.00	-5.43	-2.52
141	0.00	-5.08	-0.16
161	0.00	-5.43	2.37
181	0.00	-5.06	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra102.Mx- + [0

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	14.30	0.00
21	0.00	36.01	2.95
41	0.00	37.61	1.58
61	0.00	36.01	-0.27
81	0.00	14.30	0.00
101	0.00	81.15	0.00
121	0.00	244.83	13.30
141	0.00	257.08	-1.86
161	0.00	244.83	-17.82
181	0.00	81.15	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra102.Mx- + [0

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-5.69	0.00
21	0.00	-6.13	1.02
41	0.00	-6.04	0.07
61	0.00	-6.13	-0.96
81	0.00	-5.69	0.00
101	0.00	-13.67	0.00
121	0.00	-16.40	-14.11
141	0.00	-25.11	-1.27
161	0.00	-16.40	12.82
181	0.00	-13.67	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.Nudo1.Pos3.I

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	17.20	0.00
21	0.00	39.04	-4.48
41	0.00	39.73	0.51
61	0.00	39.04	5.54
81	0.00	17.20	0.00
101	0.00	2.85	0.00
121	0.00	6.06	-0.56
141	0.00	6.14	-0.09
161	0.00	6.06	0.36
181	0.00	2.85	0.00

TRENLA1.EnvTrenGen.FY-

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

TRENLA1.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.Nudo1.Pos3.I

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-2.44	0.00
21	0.00	-3.00	3.78
41	0.00	-2.39	4.54
61	0.00	-3.00	-3.51
81	0.00	-2.44	0.00
101	0.00	-0.80	0.00
121	0.00	-0.93	-0.80
141	0.00	-0.51	-0.97
161	0.00	-0.93	0.76
181	0.00	-0.80	0.00

TRENLA2.EnvTrenGen.FY+

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

TRENLA2.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	2.55	0.00
21	0.00	5.24	2.13
41	0.00	5.36	0.15
61	0.00	5.24	-1.84
81	0.00	2.55	0.00
101	0.00	18.97	0.00
121	0.00	43.27	4.04
141	0.00	43.94	-0.34
161	0.00	43.27	-4.78
181	0.00	18.97	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-0.92	0.00
21	0.00	-1.07	0.45
41	0.00	-0.60	0.63
61	0.00	-1.07	-0.42
81	0.00	-0.92	0.00
101	0.00	-2.53	0.00
121	0.00	-3.12	-3.34
141	0.00	-2.48	-3.48
161	0.00	-3.12	3.11
181	0.00	-2.53	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIE1

Carga uniforme tren E eje 1

[1; 1]CUNIE1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	7.32	0.00
21	0.00	24.79	0.14
41	0.00	25.18	0.39
61	0.00	24.79	0.58
81	0.00	7.32	0.00
101	0.00	1.02	0.00
121	0.00	3.55	-0.43
141	0.00	3.73	-0.18
161	0.00	3.55	0.13
181	0.00	1.02	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIE2

Carga uniforme Tren E eje 2

[1; 1]CUNIE2

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	1.11	0.00
21	0.00	3.84	0.39
41	0.00	4.03	0.16
61	0.00	3.84	-0.12
81	0.00	1.11	0.00
101	0.00	6.86	0.00
121	0.00	23.22	-0.23
141	0.00	23.59	-0.45
161	0.00	23.22	-0.60
181	0.00	6.86	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIE1.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIE1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIE1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	79.52	0.00
21	0.00	239.51	-13.38
41	0.00	251.69	2.19
61	0.00	239.52	18.51
81	0.00	79.53	0.00
101	0.00	14.77	0.00
121	0.00	37.89	-2.36
141	0.00	39.42	-1.49
161	0.00	37.89	-0.19
181	0.00	14.77	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIE1.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIE1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIE1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-13.61	0.00
21	0.00	-16.37	14.65
41	0.00	-25.07	1.33
61	0.00	-16.37	-13.31
81	0.00	-13.61	0.00
101	0.00	-5.55	0.00
121	0.00	-5.98	-1.46
141	0.00	-5.81	-0.10
161	0.00	-5.98	1.37
181	0.00	-5.55	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIE2.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIE2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIE2SCuniTneg.Barra102.Mx- + [0

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	15.22	0.00
21	0.00	40.17	1.33
41	0.00	41.54	1.31
61	0.00	40.17	0.95
81	0.00	15.22	0.00
101	0.00	74.91	0.00
121	0.00	224.94	13.20
141	0.00	236.70	-2.68
161	0.00	224.94	-19.25
181	0.00	74.91	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIE2.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIE2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIE2SCuniTneg.Barra102.Mx- + [0

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-5.19	0.00
21	0.00	-5.57	2.16
41	0.00	-5.28	0.14
61	0.00	-5.57	-2.03
81	0.00	-5.19	0.00
101	0.00	-13.18	0.00
121	0.00	-15.94	-15.24
141	0.00	-24.42	-1.41
161	0.00	-15.94	13.82
181	0.00	-13.18	0.00

TRENLE1.EnvTrenGen.FY+

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLE1.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLE1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLE1.PaseoTren.Nudo1.Pos3.

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	18.61	0.00
21	0.00	42.37	-4.19
41	0.00	43.05	0.39
61	0.00	42.37	5.03
81	0.00	18.60	0.00
101	0.00	2.65	0.00
121	0.00	5.51	-2.01
141	0.00	5.62	-0.13
161	0.00	5.51	1.74
181	0.00	2.65	0.00

TRENLE1.EnvTrenGen.FY-

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLE1.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLE1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLE1.PaseoTren.Nudo1.Pos3.

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-2.52	0.00
21	0.00	-3.11	3.49
41	0.00	-2.47	3.65
61	0.00	-3.11	-3.24
81	0.00	-2.52	0.00
101	0.00	-0.89	0.00
121	0.00	-1.04	-0.55
141	0.00	-0.58	-0.73
161	0.00	-1.04	0.52
181	0.00	-0.89	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLE2.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLE2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLE2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	3.33	0.00
21	0.00	7.02	0.87
41	0.00	7.12	0.15
61	0.00	7.03	-1.89
81	0.00	3.35	0.00
101	0.00	21.06	0.00
121	0.00	48.05	5.31
141	0.00	48.86	-0.49
161	0.00	48.04	-6.36
181	0.00	21.25	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLE2.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLE2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLE2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-1.01	0.00
21	0.00	-1.17	0.86
41	0.00	-0.64	1.07
61	0.00	-1.16	-0.81
81	0.00	-1.00	0.00
101	0.00	-2.97	0.00
121	0.00	-3.65	-4.39
141	0.00	-2.90	-5.26
161	0.00	-3.65	4.09
181	0.00	-2.96	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIM1

Carga uniforme Tren M eje 1

[1; 1]CUNIM1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	6.11	0.00
21	0.00	20.70	0.37
41	0.00	21.02	0.56
61	0.00	20.70	0.65
81	0.00	6.11	0.00
101	0.00	1.27	0.00
121	0.00	4.37	-0.33
141	0.00	4.55	-0.14
161	0.00	4.38	0.10
181	0.00	1.27	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIM2

Carga uniforme Tren M eje 2

[1; 1]CUNIM2

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.76	0.00
21	0.00	2.66	0.50
41	0.00	2.85	0.21
61	0.00	2.66	-0.15
81	0.00	0.76	0.00
101	0.00	8.18	0.00
121	0.00	27.67	0.07
141	0.00	28.10	-0.22
161	0.00	27.67	-0.49
181	0.00	8.18	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIM1.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIM1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIM1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	67.54	0.00
21	0.00	201.57	-12.98
41	0.00	212.69	3.53
61	0.00	201.58	20.61
81	0.00	67.54	0.00
101	0.00	16.06	0.00
121	0.00	44.30	0.29
141	0.00	45.44	-1.01
161	0.00	44.30	-2.12
181	0.00	16.07	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIM1.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIM1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIM1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-12.53	0.00
21	0.00	-15.31	16.33
41	0.00	-23.47	1.55
61	0.00	-15.31	-14.76
81	0.00	-12.54	0.00
101	0.00	-4.60	0.00
121	0.00	-4.93	-3.23
141	0.00	-4.45	-0.21
161	0.00	-4.93	3.03
181	0.00	-4.60	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIM2.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIM2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIM2SCuniTneg.Barra102.Mx- + [(

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	13.08	0.00
21	0.00	30.70	4.84
41	0.00	32.59	1.87
61	0.00	30.70	-1.71
81	0.00	13.08	0.00
101	0.00	87.69	0.00
121	0.00	265.86	12.56
141	0.00	278.60	-0.95
161	0.00	265.87	-15.28
181	0.00	87.70	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIM2.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIM2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIM2SCuniTneg.Barra102.Mx- + [(

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-6.23	0.00
21	0.00	-6.73	-0.33
41	0.00	-6.91	0.00
61	0.00	-6.73	0.32
81	0.00	-6.24	0.00
101	0.00	-14.11	0.00
121	0.00	-16.81	-11.90
141	0.00	-25.73	-1.03
161	0.00	-16.81	10.86
181	0.00	-14.11	0.00

TRENLM1.EnvTrenGen.FY+

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLM1.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLM1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLM1.PaseoTren.Nudo1.Pos3

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	15.86	0.00
21	0.00	35.87	-4.66
41	0.00	36.57	0.60
61	0.00	35.87	5.89
81	0.00	15.86	0.00
101	0.00	2.99	0.00
121	0.00	6.46	-0.28
141	0.00	6.50	-0.05
161	0.00	6.46	0.14
181	0.00	2.99	0.00

TRENLM1.EnvTrenGen.FY-

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLM1.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLM1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLM1.PaseoTren.Nudo1.Pos3

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-2.34	0.00
21	0.00	-2.88	3.98
41	0.00	-2.31	4.82
61	0.00	-2.88	-3.69
81	0.00	-2.34	0.00
101	0.00	-0.71	0.00
121	0.00	-0.83	-1.00
141	0.00	-0.45	-1.15
161	0.00	-0.83	0.94
181	0.00	-0.71	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLM2.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLM2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLM2.PaseoTren.Nudo101.F

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	2.25	0.00
21	0.00	4.47	3.63
41	0.00	4.62	0.20
61	0.00	4.47	-3.27
81	0.00	2.25	0.00
101	0.00	20.46	0.00
121	0.00	46.84	3.61
141	0.00	47.48	-0.20
161	0.00	46.84	-4.07
181	0.00	20.46	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLM2.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLM2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLM2.PaseoTren.Nudo101.F

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-1.03	0.00
21	0.00	-1.20	0.12
41	0.00	-0.68	0.31
61	0.00	-1.20	-0.11
81	0.00	-1.03	0.00
101	0.00	-2.61	0.00
121	0.00	-3.21	-2.92
141	0.00	-2.54	-3.02
161	0.00	-3.21	2.72
181	0.00	-2.61	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIH1

Carga uniforme tren H eje 1

[1; 1]CUNIH1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	6.38	0.00
21	0.00	21.61	0.43
41	0.00	21.95	0.63
61	0.00	21.61	0.71
81	0.00	6.38	0.00
101	0.00	1.40	0.00
121	0.00	4.82	-0.34
141	0.00	5.01	-0.14
161	0.00	4.82	0.10
181	0.00	1.40	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
CUNIH2

Carga uniforme tren H eje 2

[1; 1]CUNIH2

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.12	0.00
21	0.00	0.40	0.01
41	0.00	0.41	0.00
61	0.00	0.40	0.00
81	0.00	0.12	0.00
101	0.00	0.26	0.00
121	0.00	0.88	-0.05
141	0.00	0.89	-0.06
161	0.00	0.88	-0.05
181	0.00	0.26	0.00

SCUNIH1.ENV_TREN_GENERICO.FY+

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIH1.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIH1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIH1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	70.73	0.00
21	0.00	210.76	-13.88
41	0.00	222.54	3.98
61	0.00	210.76	22.44
81	0.00	70.73	0.00
101	0.00	17.44	0.00
121	0.00	48.52	0.71
141	0.00	49.68	-1.02
161	0.00	48.52	-2.57
181	0.00	17.44	0.00

SCUNIH1.ENV_TREN_GENERICO.FY-

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIH1.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIH1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIH1.SCuniTpos.Barra2.Mx+ + [0; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-13.30	0.00
21	0.00	-16.28	17.78
41	0.00	-24.95	1.69
61	0.00	-16.28	-16.06
81	0.00	-13.30	0.00
101	0.00	-4.80	0.00
121	0.00	-5.14	-3.73
141	0.00	-4.59	-0.24
161	0.00	-5.14	3.49
181	0.00	-4.80	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIH2.ENV_TREN_GENERICO.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]SCUNIH2SCuniTneg.Barra1.Mx- + [0; 1]SCUNIH2SCuniTneg.Barra2.Mx- + [0; 1]S

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	6.12	0.00
21	0.00	19.32	-0.35
41	0.00	19.72	-0.63
61	0.00	19.32	-0.81
81	0.00	6.12	0.00
101	0.00	3.13	0.00
121	0.00	8.89	1.02
141	0.00	9.42	-0.39
161	0.00	8.89	-1.79
181	0.00	3.13	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
SCUNIH2.ENV_TREN_GENERICO.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]SCUNIH2SCuniTneg.Barra1.Mx- + [0; 1]SCUNIH2SCuniTneg.Barra2.Mx- + [0; 1]S

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-0.62	0.00
21	0.00	-0.72	-0.50
41	0.00	-0.82	-0.05
61	0.00	-0.72	0.46
81	0.00	-0.62	0.00
101	0.00	-1.87	0.00
121	0.00	-4.55	-1.87
141	0.00	-4.93	-0.29
161	0.00	-4.55	1.44
181	0.00	-1.87	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLH1.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLH1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLH1.PaseoTren.Nudo1.Pos3.

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	16.63	0.00
21	0.00	37.56	-5.08
41	0.00	38.32	0.67
61	0.00	37.56	6.46
81	0.00	16.63	0.00
101	0.00	3.26	0.00
121	0.00	7.09	-0.21
141	0.00	7.11	-0.04
161	0.00	7.09	0.08
181	0.00	3.26	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLH1.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLH1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLH1.PaseoTren.Nudo1.Pos3.

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-2.48	0.00
21	0.00	-3.06	4.35
41	0.00	-2.46	5.28
61	0.00	-3.06	-4.03
81	0.00	-2.48	0.00
101	0.00	-0.74	0.00
121	0.00	-0.86	-1.15
141	0.00	-0.46	-1.30
161	0.00	-0.86	1.08
181	0.00	-0.74	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLH2.EnvTrenGen.FY+

Envolvente de tren de cargas plano genérico. FY+

[0; 1]TRENLH2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLH2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.24	0.00
21	0.00	0.55	-0.19
41	0.00	0.54	-0.01
61	0.00	0.55	0.18
81	0.00	0.24	0.00
101	0.00	0.72	0.00
121	0.00	1.60	0.37
141	0.00	1.65	-0.06
161	0.00	1.60	-0.50
181	0.00	0.72	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLH2.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLH2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLH2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-0.03	0.00
21	0.00	-0.03	0.12
41	0.00	-0.01	-0.13
61	0.00	-0.03	-0.11
81	0.00	-0.03	0.00
101	0.00	-0.13	0.00
121	0.00	-0.16	-0.33
141	0.00	-0.14	0.38
161	0.00	-0.16	0.32
181	0.00	-0.13	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
TRENLH2.EnvTrenGen.FY-

Envolvente de tren de cargas plano genérico. FY-

[0; 1]TRENLH2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLH2.PaseoTren.Nudo101.P

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-0.03	0.00
21	0.00	-0.03	0.12
41	0.00	-0.01	-0.13
61	0.00	-0.03	-0.11
81	0.00	-0.03	0.00
101	0.00	-0.13	0.00
121	0.00	-0.16	-0.33
141	0.00	-0.14	0.38
161	0.00	-0.16	0.32
181	0.00	-0.13	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
ej1preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	75.78	0.00
21	0.00	-82.43	-14.47
41	0.00	13.37	3.83
61	0.00	-82.43	22.64
81	0.00	75.78	0.00
101	0.00	-3.37	0.00
121	0.00	1.09	-14.47
141	0.00	4.56	3.83
161	0.00	1.09	22.65
181	0.00	-3.37	0.00

ej1preEl.TOT.Tinf

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej1preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1preEl.FAM1.TOT + [1; 1]ej1preEl.FAM2.TOT + [1; 1]ej1preEl.FAM3.TOT + [1; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	75.78	0.00
21	0.00	-82.43	-14.47
41	0.00	13.37	3.83
61	0.00	-82.43	22.64
81	0.00	75.78	0.00
101	0.00	-3.37	0.00
121	0.00	1.09	-14.47
141	0.00	4.56	3.83
161	0.00	1.09	22.65
181	0.00	-3.37	0.00

ej1posEl.TOT.To

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej1posEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1;

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-22.33	0.00
21	0.00	25.95	16.17
41	0.00	-7.18	2.73
61	0.00	25.94	-12.40
81	0.00	-22.33	0.00
101	0.00	2.00	0.00
121	0.00	0.16	16.17
141	0.00	-4.32	2.73
161	0.00	0.16	-12.39
181	0.00	2.00	0.00

ej1posEl.TOT.Tinf

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej1posEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej1posEl.FAM1.TOT + [1; 1]ej1posEl.FAM2.TOT + [1; 1]ej1posEl.FAM3.TOT + [1;

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-22.33	0.00
21	0.00	25.95	16.17
41	0.00	-7.18	2.73
61	0.00	25.94	-12.40
81	0.00	-22.33	0.00
101	0.00	2.00	0.00
121	0.00	0.16	16.17
141	0.00	-4.32	2.73
161	0.00	0.16	-12.39
181	0.00	2.00	0.00

ej2preEl.TOT.To

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej2preEl.TOT.To

Pretensado Total (t=0)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1;

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-3.37	0.00
21	0.00	1.09	14.47
41	0.00	4.56	-3.83
61	0.00	1.09	-22.65
81	0.00	-3.37	0.00
101	0.00	75.78	0.00
121	0.00	-82.44	14.47
141	0.00	13.36	-3.83
161	0.00	-82.45	-22.64
181	0.00	75.78	0.00

ej2preEl.TOT.Tinf

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej2preEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2preEl.FAM1.TOT + [1; 1]ej2preEl.FAM2.TOT + [1; 1]ej2preEl.FAM3.TOT + [1; 1

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-3.37	0.00
21	0.00	1.09	14.47
41	0.00	4.56	-3.83
61	0.00	1.09	-22.65
81	0.00	-3.37	0.00
101	0.00	75.78	0.00
121	0.00	-82.44	14.47
141	0.00	13.36	-3.83
161	0.00	-82.45	-22.64
181	0.00	75.78	0.00

ej2posEl.TOT.To

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

ej2posEl.TOT.To

Pretensado Total (t=0)

[1; 1)ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1;

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	2.00	0.00
21	0.00	0.16	-16.17
41	0.00	-4.32	-2.73
61	0.00	0.16	12.39
81	0.00	2.00	0.00
101	0.00	-22.33	0.00
121	0.00	25.94	-16.17
141	0.00	-7.19	-2.73
161	0.00	25.93	12.40
181	0.00	-22.33	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
ej2posEl.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]ej2posEl.FAM1.TOT + [1; 1]ej2posEl.FAM2.TOT + [1; 1]ej2posEl.FAM3.TOT + [1;

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	2.00	0.00
21	0.00	0.16	-16.17
41	0.00	-4.32	-2.73
61	0.00	0.16	12.39
81	0.00	2.00	0.00
101	0.00	-22.33	0.00
121	0.00	25.94	-16.17
141	0.00	-7.19	-2.73
161	0.00	25.93	12.40
181	0.00	-22.33	0.00

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
eje1f3.TOT.To

Pretensado Total (t=0)

[1; 1]eje1f3.FAM1.TOT + [1; 1]eje1f3.FAM2.TOT + [1; 1]eje1f3.FAM3.TOT + [1; 1]eje1f

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-10.89	0.05
21	0.00	21.92	-20.59
41	0.00	-0.13	-23.89
61	0.00	21.12	-23.50
81	0.00	-10.11	-0.50
101	0.00	0.94	-0.02
121	0.00	-7.23	-20.44
141	0.00	-9.31	-23.88
161	0.00	-6.44	-24.60
181	0.00	0.15	-0.01

eje1f3.TOT.Tinf

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

eje1f3.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje1f3.FAM1.TOT + [1; 1]eje1f3.FAM2.TOT + [1; 1]eje1f3.FAM3.TOT + [1; 1]eje1f

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	-10.89	0.05
21	0.00	21.92	-20.59
41	0.00	-0.13	-23.89
61	0.00	21.12	-23.50
81	0.00	-10.11	-0.50
101	0.00	0.94	-0.02
121	0.00	-7.23	-20.44
141	0.00	-9.31	-23.88
161	0.00	-6.44	-24.60
181	0.00	0.15	-0.01

eje2f3.TOT.To

CÁLCULO DE REACCIONES

Hipótesis de cálculo:

eje2f3.TOT.To

Pretensado Total (t=0)

[1; 1]eje2f3.FAM1.TOT + [1; 1]eje2f3.FAM2.TOT + [1; 1]eje2f3.FAM3.TOT + [1; 1]eje2f

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.94	-0.05
21	0.00	-7.23	20.59
41	0.00	-9.31	23.88
61	0.00	-6.44	23.49
81	0.00	0.15	0.50
101	0.00	-10.89	0.02
121	0.00	21.91	20.45
141	0.00	-0.13	23.88
161	0.00	21.12	24.60
181	0.00	-10.11	0.01

CÁLCULO DE REACCIONES

Hipótesis de cálculo:
eje2f3.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje2f3.FAM1.TOT + [1; 1]eje2f3.FAM2.TOT + [1; 1]eje2f3.FAM3.TOT + [1; 1]eje2f

Coef. exc:

Nudo	X	Fy (T)	Mx (Tm)
1	0.00	0.94	-0.05
21	0.00	-7.23	20.59
41	0.00	-9.31	23.88
61	0.00	-6.44	23.49
81	0.00	0.15	0.50
101	0.00	-10.89	0.02
121	0.00	21.91	20.45
141	0.00	-0.13	23.88
161	0.00	21.12	24.60
181	0.00	-10.11	0.01

DESPLAZAMIENTOS EN ESTADOS INDIVIDUALES

CÁLCULO DE DESPLAZÀMIENTOS

Hipótesis de cálculo:
PPVF1

Peso Propio Vigas Fase 1

[1; 1]PPVF1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0009
2	1.1000	-0.0968	-0.0009
3	2.2000	-0.1908	-0.0008
4	3.3000	-0.2796	-0.0008
5	4.4000	-0.3611	-0.0007
6	5.5000	-0.4335	-0.0006
7	6.6000	-0.4951	-0.0005
8	7.7000	-0.5445	-0.0004
9	8.8000	-0.5805	-0.0003
10	9.9000	-0.6025	-0.0001
11	11.0000	-0.6098	0.0000
12	12.1000	-0.6025	0.0001
13	13.2000	-0.5806	0.0003
14	14.3000	-0.5445	0.0004
15	15.4000	-0.4952	0.0005
16	16.5000	-0.4338	0.0006
17	17.6000	-0.3616	0.0007
18	18.7000	-0.2802	0.0008
19	19.8000	-0.1913	0.0008
20	20.9000	-0.0971	0.0009
21	22.0000	0.0000	0.0009
1021	22.0000	0.0000	-0.0018
22	23.4000	-0.2566	-0.0018
23	24.8000	-0.5057	-0.0017
24	26.2000	-0.7408	-0.0016
25	27.6000	-0.9564	-0.0015
26	29.0000	-1.1476	-0.0013
27	30.4000	-1.3103	-0.0011
28	31.8000	-1.4408	-0.0008
29	33.2000	-1.5359	-0.0006
30	34.6000	-1.5937	-0.0003
31	36.0000	-1.6131	0.0000
32	37.4000	-1.5937	0.0003
33	38.8000	-1.5359	0.0006
34	40.2000	-1.4408	0.0008
35	41.6000	-1.3103	0.0011
36	43.0000	-1.1476	0.0013
37	44.4000	-0.9564	0.0015
38	45.8000	-0.7408	0.0016
39	47.2000	-0.5057	0.0017
40	48.6000	-0.2566	0.0018
41	50.0000	0.0000	0.0018
1041	50.0000	0.0000	-0.0018
42	51.4000	-0.2566	-0.0018
43	52.8000	-0.5057	-0.0017
44	54.2000	-0.7408	-0.0016
45	55.6000	-0.9564	-0.0015
46	57.0000	-1.1476	-0.0013
47	58.4000	-1.3103	-0.0011
48	59.8000	-1.4408	-0.0008
49	61.2000	-1.5359	-0.0006
50	62.6000	-1.5937	-0.0003
51	64.0000	-1.6131	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVF1

Peso Propio Vigas Fase 1

[1; 1]PPVF1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.2566	-0.0018
123	24.8000	-0.5057	-0.0017
124	26.2000	-0.7408	-0.0016
125	27.6000	-0.9564	-0.0015
126	29.0000	-1.1476	-0.0013
127	30.4000	-1.3103	-0.0011
128	31.8000	-1.4408	-0.0008
129	33.2000	-1.5359	-0.0006
130	34.6000	-1.5937	-0.0003
131	36.0000	-1.6131	0.0000
132	37.4000	-1.5937	0.0003
133	38.8000	-1.5359	0.0006
134	40.2000	-1.4408	0.0008
135	41.6000	-1.3103	0.0011
136	43.0000	-1.1476	0.0013
137	44.4000	-0.9564	0.0015
138	45.8000	-0.7408	0.0016
139	47.2000	-0.5057	0.0017
140	48.6000	-0.2566	0.0018
141	50.0000	0.0000	0.0018
1141	50.0000	0.0000	-0.0018
142	51.4000	-0.2566	-0.0018
143	52.8000	-0.5057	-0.0017
144	54.2000	-0.7408	-0.0016
145	55.6000	-0.9564	-0.0015
146	57.0000	-1.1476	-0.0013
147	58.4000	-1.3103	-0.0011
148	59.8000	-1.4408	-0.0008
149	61.2000	-1.5359	-0.0006
150	62.6000	-1.5937	-0.0003
151	64.0000	-1.6131	0.0000
152	65.4000	-1.5937	0.0003
153	66.8000	-1.5359	0.0006
154	68.2000	-1.4408	0.0008
155	69.6000	-1.3103	0.0011
156	71.0000	-1.1476	0.0013
157	72.4000	-0.9564	0.0015
158	73.8000	-0.7408	0.0016
159	75.2000	-0.5057	0.0017
160	76.6000	-0.2566	0.0018
161	78.0000	0.0000	0.0018
1161	78.0000	0.0000	-0.0009
162	79.1000	-0.0971	-0.0009
163	80.2000	-0.1913	-0.0008
164	81.3000	-0.2802	-0.0008
165	82.4000	-0.3616	-0.0007
166	83.5000	-0.4338	-0.0006
167	84.6000	-0.4952	-0.0005
168	85.7000	-0.5445	-0.0004
169	86.8000	-0.5806	-0.0003
170	87.9000	-0.6025	-0.0001
171	89.0000	-0.6098	0.0000
172	90.1000	-0.6025	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVF1

Peso Propio Vigas Fase 1

[1; 1]PPVF1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.5805	0.0003
174	92.3000	-0.5445	0.0004
175	93.4000	-0.4951	0.0005
176	94.5000	-0.4335	0.0006
177	95.6000	-0.3611	0.0007
178	96.7000	-0.2796	0.0008
179	97.8000	-0.1908	0.0008
180	98.9000	-0.0968	0.0009
181	100.0000	0.0000	0.0009

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0003
2	1.1000	-0.0318	-0.0003
3	2.2000	-0.0628	-0.0003
4	3.3000	-0.0920	-0.0003
5	4.4000	-0.1189	-0.0002
6	5.5000	-0.1427	-0.0002
7	6.6000	-0.1630	-0.0002
8	7.7000	-0.1792	-0.0001
9	8.8000	-0.1911	-0.0001
10	9.9000	-0.1982	0.0000
11	11.0000	-0.2006	0.0000
12	12.1000	-0.1982	0.0000
13	13.2000	-0.1909	0.0001
14	14.3000	-0.1790	0.0001
15	15.4000	-0.1627	0.0002
16	16.5000	-0.1425	0.0002
17	17.6000	-0.1187	0.0002
18	18.7000	-0.0919	0.0003
19	19.8000	-0.0627	0.0003
20	20.9000	-0.0318	0.0003
21	22.0000	0.0000	0.0003
1021	22.0000	0.0000	-0.0006
22	23.4000	-0.0836	-0.0006
23	24.8000	-0.1649	-0.0006
24	26.2000	-0.2417	-0.0005
25	27.6000	-0.3122	-0.0005
26	29.0000	-0.3748	-0.0004
27	30.4000	-0.4281	-0.0003
28	31.8000	-0.4709	-0.0003
29	33.2000	-0.5021	-0.0002
30	34.6000	-0.5210	-0.0001
31	36.0000	-0.5274	0.0000
32	37.4000	-0.5210	0.0001
33	38.8000	-0.5021	0.0002
34	40.2000	-0.4709	0.0003
35	41.6000	-0.4281	0.0003
36	43.0000	-0.3748	0.0004
37	44.4000	-0.3122	0.0005
38	45.8000	-0.2417	0.0005
39	47.2000	-0.1649	0.0006
40	48.6000	-0.0836	0.0006
41	50.0000	0.0000	0.0006
1041	50.0000	0.0000	-0.0006
42	51.4000	-0.0836	-0.0006
43	52.8000	-0.1649	-0.0006
44	54.2000	-0.2417	-0.0005
45	55.6000	-0.3122	-0.0005
46	57.0000	-0.3748	-0.0004
47	58.4000	-0.4281	-0.0003
48	59.8000	-0.4709	-0.0003
49	61.2000	-0.5021	-0.0002
50	62.6000	-0.5210	-0.0001
51	64.0000	-0.5274	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.5210	0.0001
53	66.8000	-0.5021	0.0002
54	68.2000	-0.4709	0.0003
55	69.6000	-0.4281	0.0003
56	71.0000	-0.3748	0.0004
57	72.4000	-0.3122	0.0005
58	73.8000	-0.2417	0.0005
59	75.2000	-0.1649	0.0006
60	76.6000	-0.0836	0.0006
61	78.0000	0.0000	0.0006
1061	78.0000	0.0000	-0.0003
62	79.1000	-0.0318	-0.0003
63	80.2000	-0.0627	-0.0003
64	81.3000	-0.0919	-0.0003
65	82.4000	-0.1187	-0.0002
66	83.5000	-0.1425	-0.0002
67	84.6000	-0.1627	-0.0002
68	85.7000	-0.1790	-0.0001
69	86.8000	-0.1909	-0.0001
70	87.9000	-0.1982	0.0000
71	89.0000	-0.2006	0.0000
72	90.1000	-0.1982	0.0000
73	91.2000	-0.1911	0.0001
74	92.3000	-0.1792	0.0001
75	93.4000	-0.1630	0.0002
76	94.5000	-0.1427	0.0002
77	95.6000	-0.1189	0.0002
78	96.7000	-0.0920	0.0003
79	97.8000	-0.0628	0.0003
80	98.9000	-0.0318	0.0003
81	100.0000	0.0000	0.0003
101	0.0000	0.0000	-0.0003
102	1.1000	-0.0318	-0.0003
103	2.2000	-0.0628	-0.0003
104	3.3000	-0.0920	-0.0003
105	4.4000	-0.1189	-0.0002
106	5.5000	-0.1427	-0.0002
107	6.6000	-0.1630	-0.0002
108	7.7000	-0.1792	-0.0001
109	8.8000	-0.1911	-0.0001
110	9.9000	-0.1982	0.0000
111	11.0000	-0.2006	0.0000
112	12.1000	-0.1982	0.0000
113	13.2000	-0.1909	0.0001
114	14.3000	-0.1790	0.0001
115	15.4000	-0.1627	0.0002
116	16.5000	-0.1425	0.0002
117	17.6000	-0.1187	0.0002
118	18.7000	-0.0919	0.0003
119	19.8000	-0.0627	0.0003
120	20.9000	-0.0318	0.0003
121	22.0000	0.0000	0.0003
1121	22.0000	0.0000	-0.0006

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0836	-0.0006
123	24.8000	-0.1649	-0.0006
124	26.2000	-0.2417	-0.0005
125	27.6000	-0.3122	-0.0005
126	29.0000	-0.3748	-0.0004
127	30.4000	-0.4281	-0.0003
128	31.8000	-0.4709	-0.0003
129	33.2000	-0.5021	-0.0002
130	34.6000	-0.5210	-0.0001
131	36.0000	-0.5274	0.0000
132	37.4000	-0.5210	0.0001
133	38.8000	-0.5021	0.0002
134	40.2000	-0.4709	0.0003
135	41.6000	-0.4281	0.0003
136	43.0000	-0.3748	0.0004
137	44.4000	-0.3122	0.0005
138	45.8000	-0.2417	0.0005
139	47.2000	-0.1649	0.0006
140	48.6000	-0.0836	0.0006
141	50.0000	0.0000	0.0006
1141	50.0000	0.0000	-0.0006
142	51.4000	-0.0836	-0.0006
143	52.8000	-0.1649	-0.0006
144	54.2000	-0.2417	-0.0005
145	55.6000	-0.3122	-0.0005
146	57.0000	-0.3748	-0.0004
147	58.4000	-0.4281	-0.0003
148	59.8000	-0.4709	-0.0003
149	61.2000	-0.5021	-0.0002
150	62.6000	-0.5210	-0.0001
151	64.0000	-0.5274	0.0000
152	65.4000	-0.5210	0.0001
153	66.8000	-0.5021	0.0002
154	68.2000	-0.4709	0.0003
155	69.6000	-0.4281	0.0003
156	71.0000	-0.3748	0.0004
157	72.4000	-0.3122	0.0005
158	73.8000	-0.2417	0.0005
159	75.2000	-0.1649	0.0006
160	76.6000	-0.0836	0.0006
161	78.0000	0.0000	0.0006
1161	78.0000	0.0000	-0.0003
162	79.1000	-0.0318	-0.0003
163	80.2000	-0.0627	-0.0003
164	81.3000	-0.0919	-0.0003
165	82.4000	-0.1187	-0.0002
166	83.5000	-0.1425	-0.0002
167	84.6000	-0.1627	-0.0002
168	85.7000	-0.1790	-0.0001
169	86.8000	-0.1909	-0.0001
170	87.9000	-0.1982	0.0000
171	89.0000	-0.2006	0.0000
172	90.1000	-0.1982	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.1911	0.0001
174	92.3000	-0.1792	0.0001
175	93.4000	-0.1630	0.0002
176	94.5000	-0.1427	0.0002
177	95.6000	-0.1189	0.0002
178	96.7000	-0.0920	0.0003
179	97.8000	-0.0628	0.0003
180	98.9000	-0.0318	0.0003
181	100.0000	0.0000	0.0003

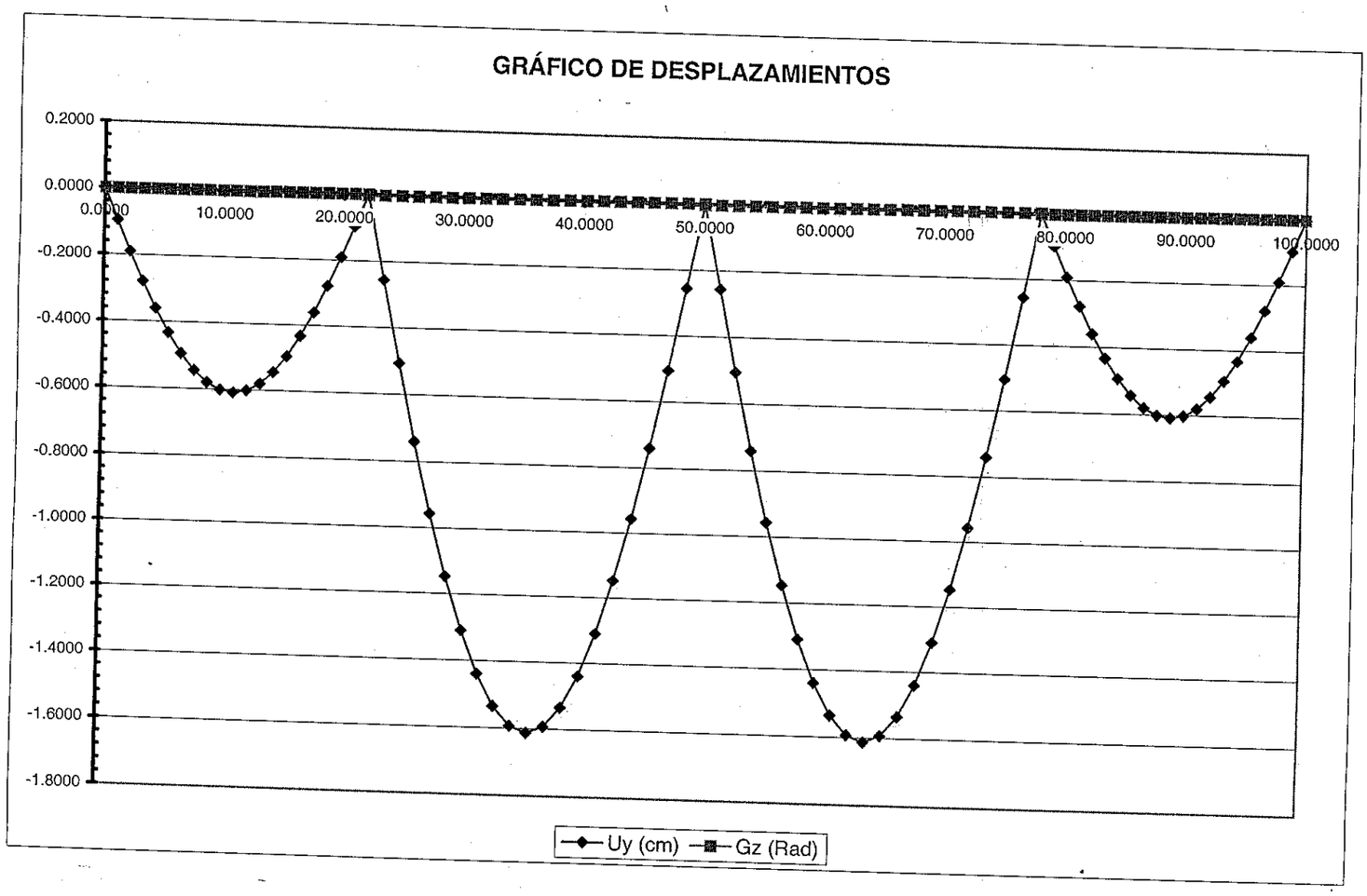


GRÁFICO DE DESPLAZAMIENTOS
0.2000
0.0000
-0.2000
-0.4000
-0.6000
-0.8000
-1.0000
-1.2000
-1.4000
-1.6000
-1.8000
0.0000
10.0000
20.0000
30.0000
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
100.0000
Uy (cm)
Gz (Rad)

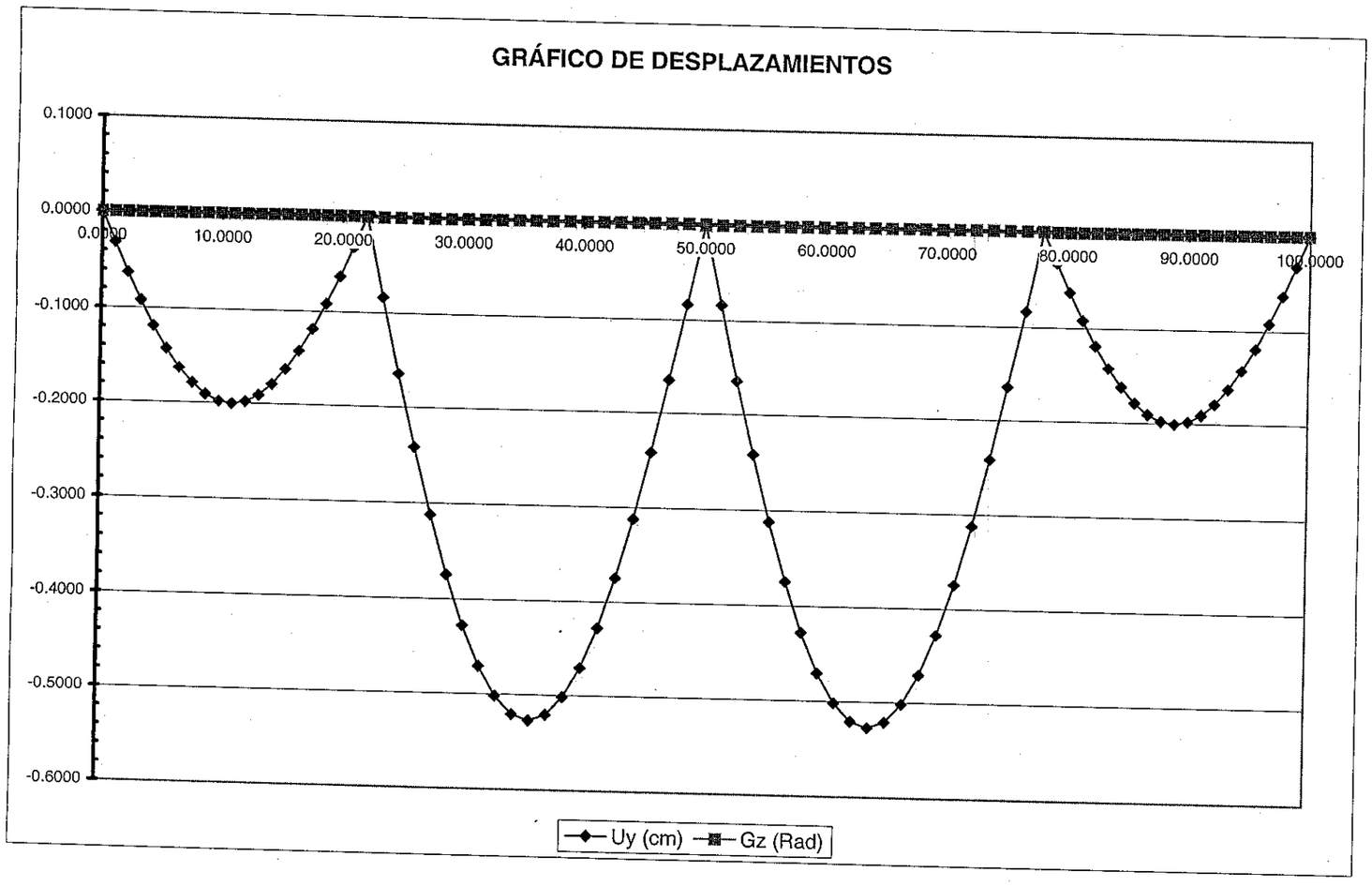


GRÁFICO DE DESPLAZAMIENTOS
0.1000
0.0000
-0.1000
-0.2000
-0.3000
-0.4000
-0.5000
-0.6000
0.0000
10.0000
20.0000
30.0000
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
100.0000
Uy (cm)
Gz (Rad)

eje1f1.TOT.To

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

eje1f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0035
2	1.1000	0.3757	0.0033
3	2.2000	0.7299	0.0031
4	3.3000	1.0558	0.0028
5	4.4000	1.3482	0.0025
6	5.5000	1.6023	0.0021
7	6.6000	1.8136	0.0017
8	7.7000	1.9764	0.0013
9	8.8000	2.0902	0.0008
10	9.9000	2.1548	0.0004
11	11.0000	2.1704	-0.0001
12	12.1000	2.1370	-0.0005
13	13.2000	2.0544	-0.0010
14	14.3000	1.9230	-0.0014
15	15.4000	1.7478	-0.0018
16	16.5000	1.5344	-0.0021
17	17.6000	1.2827	-0.0025
18	18.7000	0.9977	-0.0027
19	19.8000	0.6843	-0.0030
20	20.9000	0.3494	-0.0031
21	22.0000	0.0000	-0.0032
1021	22.0000	0.0000	0.0051
22	23.4000	0.7033	0.0049
23	24.8000	1.3797	0.0047
24	26.2000	2.0181	0.0044
25	27.6000	2.6073	0.0040
26	29.0000	3.1336	0.0035
27	30.4000	3.5834	0.0029
28	31.8000	3.9433	0.0022
29	33.2000	4.2004	0.0015
30	34.6000	4.3548	0.0007
31	36.0000	4.4062	0.0000
32	37.4000	4.3548	-0.0007
33	38.8000	4.2004	-0.0015
34	40.2000	3.9433	-0.0022
35	41.6000	3.5834	-0.0029
36	43.0000	3.1336	-0.0035
37	44.4000	2.6073	-0.0040
38	45.8000	2.0181	-0.0044
39	47.2000	1.3797	-0.0047
40	48.6000	0.7033	-0.0049
41	50.0000	0.0000	-0.0051
1041	50.0000	0.0000	0.0051
42	51.4000	0.7033	0.0049
43	52.8000	1.3797	0.0047
44	54.2000	2.0181	0.0044
45	55.6000	2.6073	0.0040
46	57.0000	3.1336	0.0035
47	58.4000	3.5834	0.0029
48	59.8000	3.9433	0.0022
49	61.2000	4.2004	0.0015
50	62.6000	4.3548	0.0007
51	64.0000	4.4062	0.0000

eje1f1.TOT.To

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

eje1f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	4.3548	-0.0007
53	66.8000	4.2004	-0.0015
54	68.2000	3.9433	-0.0022
55	69.6000	3.5834	-0.0029
56	71.0000	3.1336	-0.0035
57	72.4000	2.6073	-0.0040
58	73.8000	2.0181	-0.0044
59	75.2000	1.3797	-0.0047
60	76.6000	0.7033	-0.0049
61	78.0000	0.0000	-0.0051
1061	78.0000	0.0000	0.0032
62	79.1000	0.3494	0.0031
63	80.2000	0.6843	0.0030
64	81.3000	0.9977	0.0027
65	82.4000	1.2827	0.0025
66	83.5000	1.5343	0.0021
67	84.6000	1.7477	0.0018
68	85.7000	1.9229	0.0014
69	86.8000	2.0544	0.0010
70	87.9000	2.1369	0.0005
71	89.0000	2.1703	0.0001
72	90.1000	2.1548	-0.0004
73	91.2000	2.0901	-0.0008
74	92.3000	1.9764	-0.0013
75	93.4000	1.8136	-0.0017
76	94.5000	1.6023	-0.0021
77	95.6000	1.3482	-0.0025
78	96.7000	1.0558	-0.0028
79	97.8000	0.7299	-0.0031
80	98.9000	0.3757	-0.0033
81	100.0000	0.0000	-0.0035
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0035
2	1.1000	0.3757	0.0033
3	2.2000	0.7299	0.0031
4	3.3000	1.0558	0.0028
5	4.4000	1.3482	0.0025
6	5.5000	1.6023	0.0021
7	6.6000	1.8136	0.0017
8	7.7000	1.9764	0.0013
9	8.8000	2.0902	0.0008
10	9.9000	2.1548	0.0004
11	11.0000	2.1704	-0.0001
12	12.1000	2.1370	-0.0005
13	13.2000	2.0544	-0.0010
14	14.3000	1.9230	-0.0014
15	15.4000	1.7478	-0.0018
16	16.5000	1.5344	-0.0021
17	17.6000	1.2827	-0.0025
18	18.7000	0.9977	-0.0027
19	19.8000	0.6843	-0.0030
20	20.9000	0.3494	-0.0031
21	22.0000	0.0000	-0.0032
1021	22.0000	0.0000	0.0051
22	23.4000	0.7033	0.0049
23	24.8000	1.3797	0.0047
24	26.2000	2.0181	0.0044
25	27.6000	2.6073	0.0040
26	29.0000	3.1336	0.0035
27	30.4000	3.5834	0.0029
28	31.8000	3.9433	0.0022
29	33.2000	4.2004	0.0015
30	34.6000	4.3548	0.0007
31	36.0000	4.4062	0.0000
32	37.4000	4.3548	-0.0007
33	38.8000	4.2004	-0.0015
34	40.2000	3.9433	-0.0022
35	41.6000	3.5834	-0.0029
36	43.0000	3.1336	-0.0035
37	44.4000	2.6073	-0.0040
38	45.8000	2.0181	-0.0044
39	47.2000	1.3797	-0.0047
40	48.6000	0.7033	-0.0049
41	50.0000	0.0000	-0.0051
1041	50.0000	0.0000	0.0051
42	51.4000	0.7033	0.0049
43	52.8000	1.3797	0.0047
44	54.2000	2.0181	0.0044
45	55.6000	2.6073	0.0040
46	57.0000	3.1336	0.0035
47	58.4000	3.5834	0.0029
48	59.8000	3.9433	0.0022
49	61.2000	4.2004	0.0015
50	62.6000	4.3548	0.0007
51	64.0000	4.4062	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	4.3548	-0.0007
53	66.8000	4.2004	-0.0015
54	68.2000	3.9433	-0.0022
55	69.6000	3.5834	-0.0029
56	71.0000	3.1336	-0.0035
57	72.4000	2.6073	-0.0040
58	73.8000	2.0181	-0.0044
59	75.2000	1.3797	-0.0047
60	76.6000	0.7033	-0.0049
61	78.0000	0.0000	-0.0051
1061	78.0000	0.0000	0.0032
62	79.1000	0.3494	0.0031
63	80.2000	0.6843	0.0030
64	81.3000	0.9977	0.0027
65	82.4000	1.2827	0.0025
66	83.5000	1.5343	0.0021
67	84.6000	1.7477	0.0018
68	85.7000	1.9229	0.0014
69	86.8000	2.0544	0.0010
70	87.9000	2.1369	0.0005
71	89.0000	2.1703	0.0001
72	90.1000	2.1548	-0.0004
73	91.2000	2.0901	-0.0008
74	92.3000	1.9764	-0.0013
75	93.4000	1.8136	-0.0017
76	94.5000	1.6023	-0.0021
77	95.6000	1.3482	-0.0025
78	96.7000	1.0558	-0.0028
79	97.8000	0.7299	-0.0031
80	98.9000	0.3757	-0.0033
81	100.0000	0.0000	-0.0035
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje1f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje1f1.FAM1.TOT + [1; 1]eje1f1.FAM2.TOT + [1; 1]eje1f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0035
102	1.1000	0.3757	0.0033
103	2.2000	0.7299	0.0031
104	3.3000	1.0558	0.0028
105	4.4000	1.3482	0.0025
106	5.5000	1.6023	0.0021
107	6.6000	1.8136	0.0017
108	7.7000	1.9764	0.0013
109	8.8000	2.0902	0.0008
110	9.9000	2.1548	0.0004
111	11.0000	2.1704	-0.0001
112	12.1000	2.1370	-0.0005
113	13.2000	2.0544	-0.0010
114	14.3000	1.9230	-0.0014
115	15.4000	1.7478	-0.0018
116	16.5000	1.5344	-0.0021
117	17.6000	1.2827	-0.0025
118	18.7000	0.9977	-0.0027
119	19.8000	0.6843	-0.0030
120	20.9000	0.3494	-0.0031
121	22.0000	0.0000	-0.0032
1121	22.0000	0.0000	0.0051

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.7033	0.0049
123	24.8000	1.3797	0.0047
124	26.2000	2.0181	0.0044
125	27.6000	2.6073	0.0040
126	29.0000	3.1336	0.0035
127	30.4000	3.5834	0.0029
128	31.8000	3.9433	0.0022
129	33.2000	4.2004	0.0015
130	34.6000	4.3548	0.0007
131	36.0000	4.4062	0.0000
132	37.4000	4.3548	-0.0007
133	38.8000	4.2004	-0.0015
134	40.2000	3.9433	-0.0022
135	41.6000	3.5834	-0.0029
136	43.0000	3.1336	-0.0035
137	44.4000	2.6073	-0.0040
138	45.8000	2.0181	-0.0044
139	47.2000	1.3797	-0.0047
140	48.6000	0.7033	-0.0049
141	50.0000	0.0000	-0.0051
1141	50.0000	0.0000	0.0051
142	51.4000	0.7033	0.0049
143	52.8000	1.3797	0.0047
144	54.2000	2.0181	0.0044
145	55.6000	2.6073	0.0040
146	57.0000	3.1336	0.0035
147	58.4000	3.5834	0.0029
148	59.8000	3.9433	0.0022
149	61.2000	4.2004	0.0015
150	62.6000	4.3548	0.0007
151	64.0000	4.4062	0.0000
152	65.4000	4.3548	-0.0007
153	66.8000	4.2004	-0.0015
154	68.2000	3.9433	-0.0022
155	69.6000	3.5834	-0.0029
156	71.0000	3.1336	-0.0035
157	72.4000	2.6073	-0.0040
158	73.8000	2.0181	-0.0044
159	75.2000	1.3797	-0.0047
160	76.6000	0.7033	-0.0049
161	78.0000	0.0000	-0.0051
1161	78.0000	0.0000	0.0032
162	79.1000	0.3494	0.0031
163	80.2000	0.6843	0.0030
164	81.3000	0.9977	0.0027
165	82.4000	1.2827	0.0025
166	83.5000	1.5343	0.0021
167	84.6000	1.7477	0.0018
168	85.7000	1.9229	0.0014
169	86.8000	2.0544	0.0010
170	87.9000	2.1369	0.0005
171	89.0000	2.1703	0.0001
172	90.1000	2.1548	-0.0004

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.To

Pretensado Total (t=0)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	2.0901	-0.0008
174	92.3000	1.9764	-0.0013
175	93.4000	1.8136	-0.0017
176	94.5000	1.6023	-0.0021
177	95.6000	1.3482	-0.0025
178	96.7000	1.0558	-0.0028
179	97.8000	0.7299	-0.0031
180	98.9000	0.3757	-0.0033
181	100.0000	0.0000	-0.0035

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0035
102	1.1000	0.3757	0.0033
103	2.2000	0.7299	0.0031
104	3.3000	1.0558	0.0028
105	4.4000	1.3482	0.0025
106	5.5000	1.6023	0.0021
107	6.6000	1.8136	0.0017
108	7.7000	1.9764	0.0013
109	8.8000	2.0902	0.0008
110	9.9000	2.1548	0.0004
111	11.0000	2.1704	-0.0001
112	12.1000	2.1370	-0.0005
113	13.2000	2.0544	-0.0010
114	14.3000	1.9230	-0.0014
115	15.4000	1.7478	-0.0018
116	16.5000	1.5344	-0.0021
117	17.6000	1.2827	-0.0025
118	18.7000	0.9977	-0.0027
119	19.8000	0.6843	-0.0030
120	20.9000	0.3494	-0.0031
121	22.0000	0.0000	-0.0032
1121	22.0000	0.0000	0.0051

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
eje2f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.7033	0.0049
123	24.8000	1.3797	0.0047
124	26.2000	2.0181	0.0044
125	27.6000	2.6073	0.0040
126	29.0000	3.1336	0.0035
127	30.4000	3.5834	0.0029
128	31.8000	3.9433	0.0022
129	33.2000	4.2004	0.0015
130	34.6000	4.3548	0.0007
131	36.0000	4.4062	0.0000
132	37.4000	4.3548	-0.0007
133	38.8000	4.2004	-0.0015
134	40.2000	3.9433	-0.0022
135	41.6000	3.5834	-0.0029
136	43.0000	3.1336	-0.0035
137	44.4000	2.6073	-0.0040
138	45.8000	2.0181	-0.0044
139	47.2000	1.3797	-0.0047
140	48.6000	0.7033	-0.0049
141	50.0000	0.0000	-0.0051
1141	50.0000	0.0000	0.0051
142	51.4000	0.7033	0.0049
143	52.8000	1.3797	0.0047
144	54.2000	2.0181	0.0044
145	55.6000	2.6073	0.0040
146	57.0000	3.1336	0.0035
147	58.4000	3.5834	0.0029
148	59.8000	3.9433	0.0022
149	61.2000	4.2004	0.0015
150	62.6000	4.3548	0.0007
151	64.0000	4.4062	0.0000
152	65.4000	4.3548	-0.0007
153	66.8000	4.2004	-0.0015
154	68.2000	3.9433	-0.0022
155	69.6000	3.5834	-0.0029
156	71.0000	3.1336	-0.0035
157	72.4000	2.6073	-0.0040
158	73.8000	2.0181	-0.0044
159	75.2000	1.3797	-0.0047
160	76.6000	0.7033	-0.0049
161	78.0000	0.0000	-0.0051
1161	78.0000	0.0000	0.0032
162	79.1000	0.3494	0.0031
163	80.2000	0.6843	0.0030
164	81.3000	0.9977	0.0027
165	82.4000	1.2827	0.0025
166	83.5000	1.5343	0.0021
167	84.6000	1.7477	0.0018
168	85.7000	1.9229	0.0014
169	86.8000	2.0544	0.0010
170	87.9000	2.1369	0.0005
171	89.0000	2.1703	0.0001
172	90.1000	2.1548	-0.0004

CÁLCULO DE DESPLAZAMIENTOS

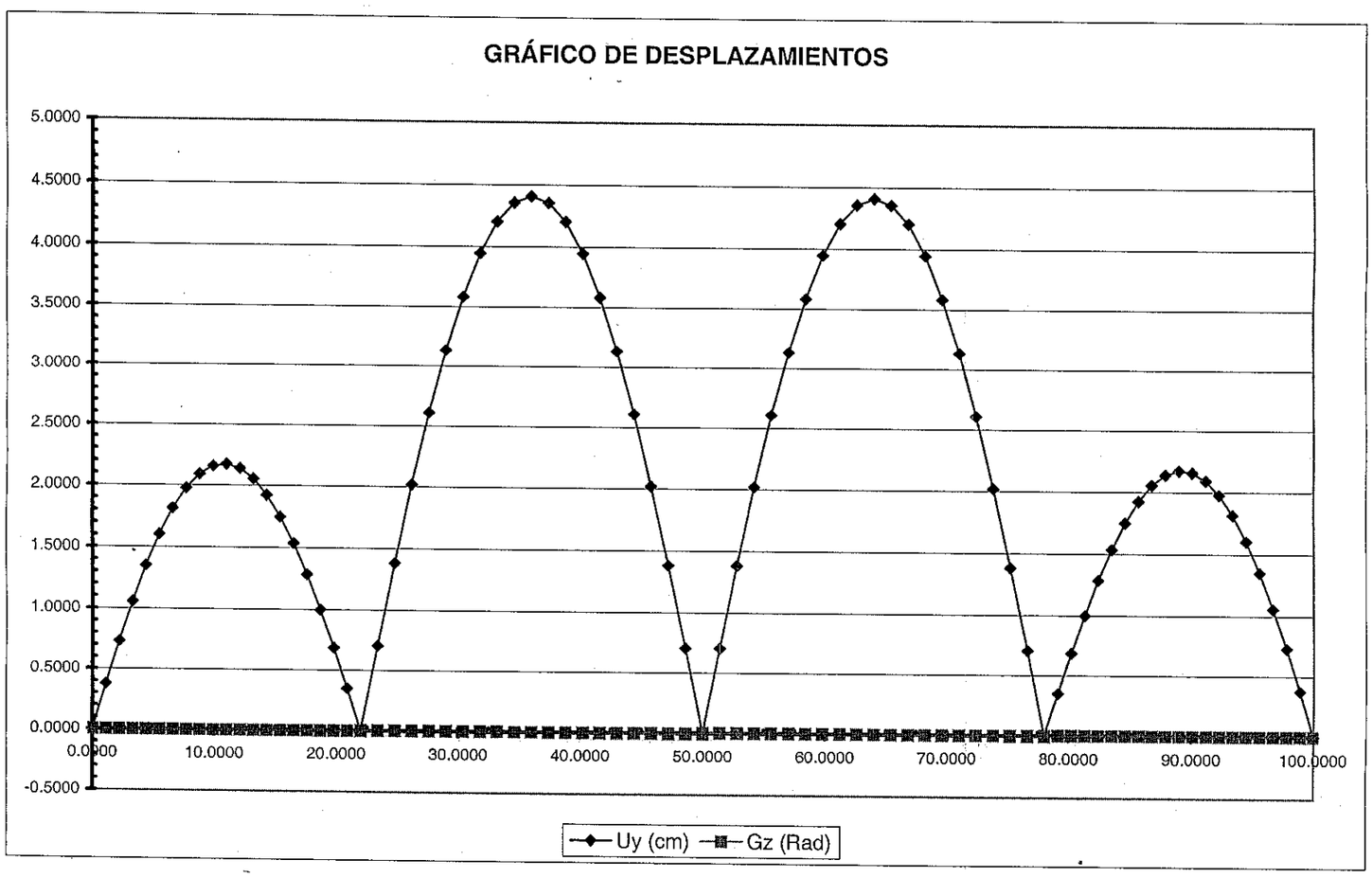
Hipótesis de cálculo:
eje2f1.TOT.Tinf

Pretensado Total (t=INF)

[1; 1]eje2f1.FAM1.TOT + [1; 1]eje2f1.FAM2.TOT + [1; 1]eje2f1.FAM3.TOT

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	2.0901	-0.0008
174	92.3000	1.9764	-0.0013
175	93.4000	1.8136	-0.0017
176	94.5000	1.6023	-0.0021
177	95.6000	1.3482	-0.0025
178	96.7000	1.0558	-0.0028
179	97.8000	0.7299	-0.0031
180	98.9000	0.3757	-0.0033
181	100.0000	0.0000	-0.0035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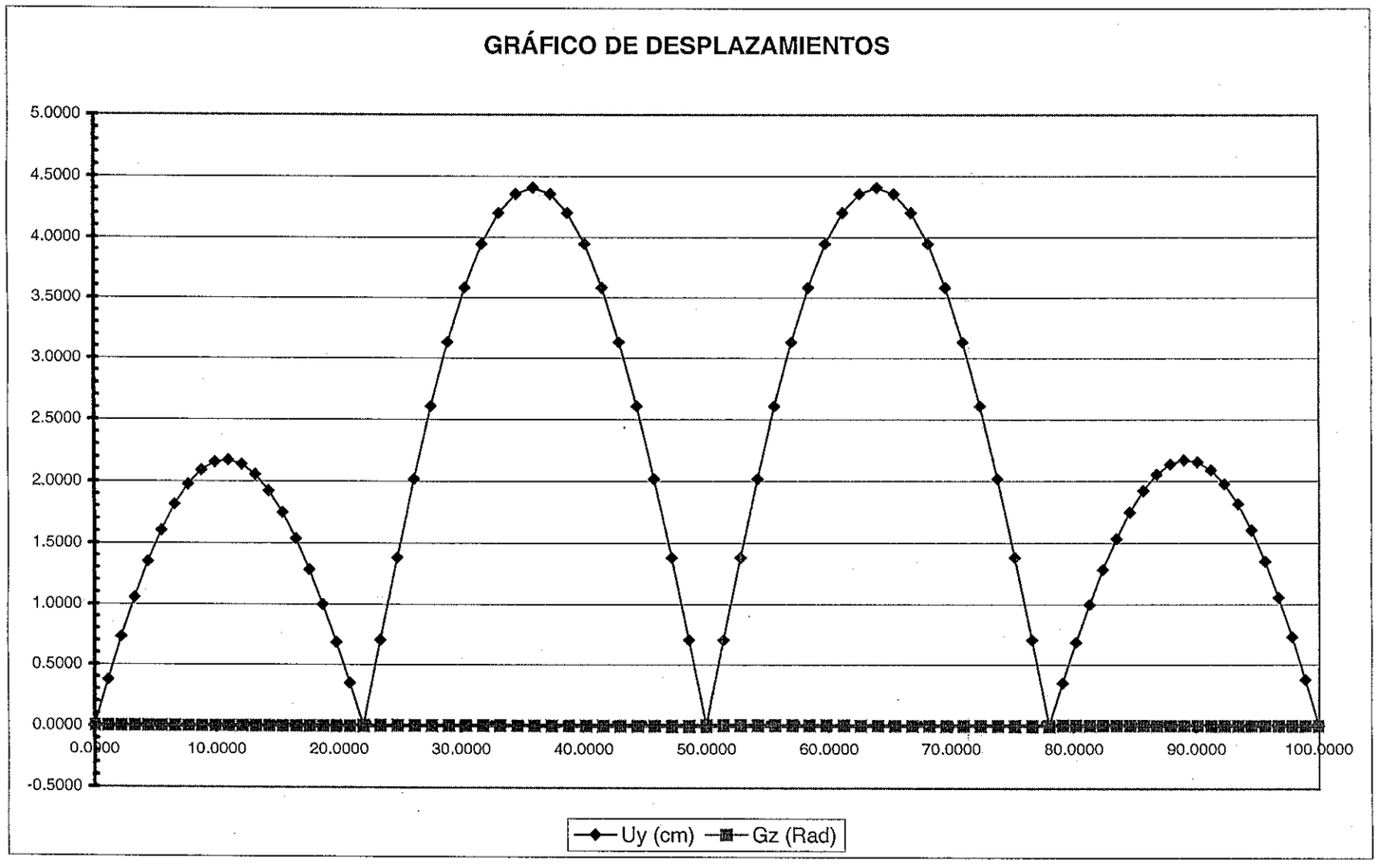
Uy (cm)
Gz (Rad)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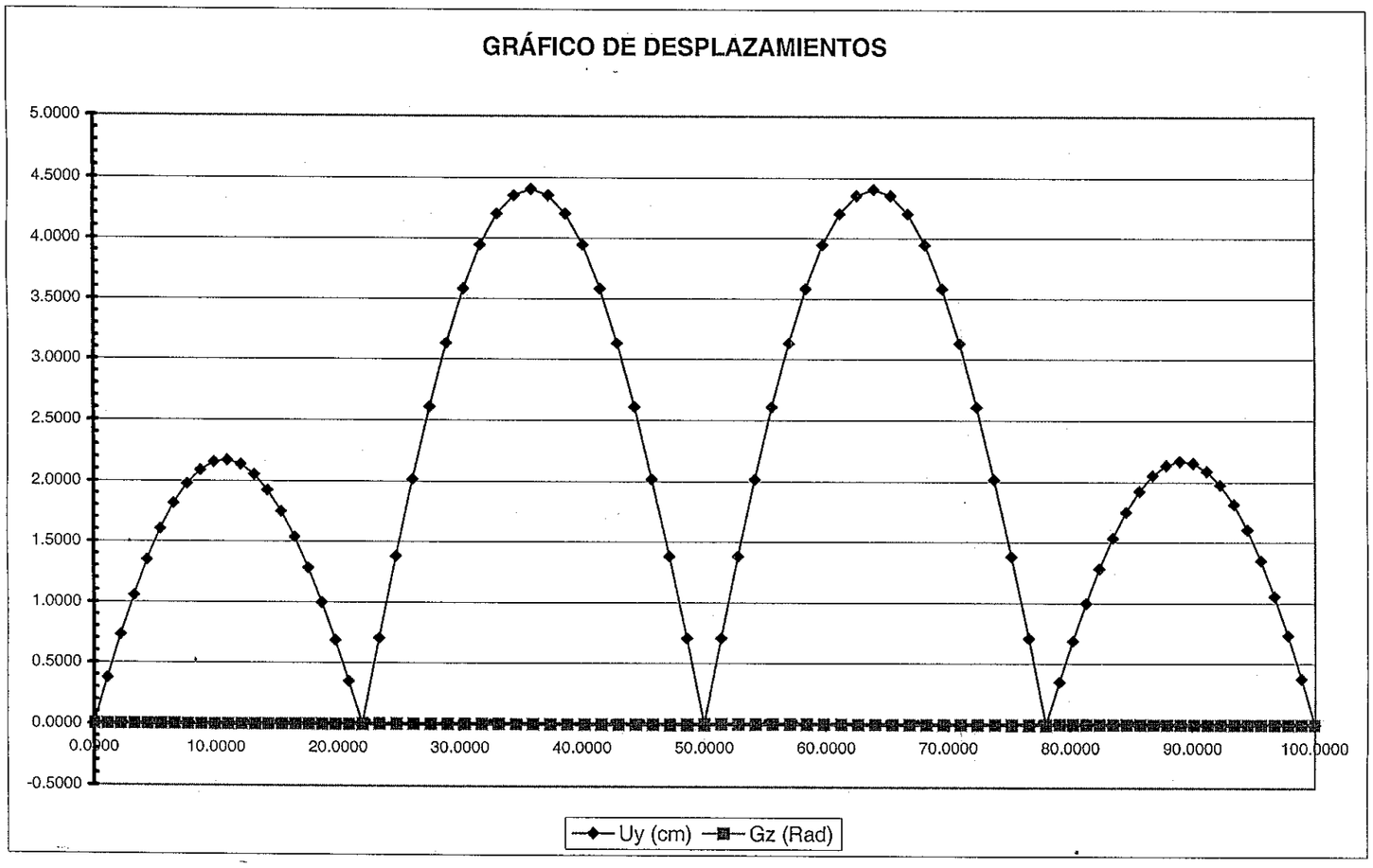
90.0000
100.0000
Uy (cm)
Gz (Rad)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0.0000
10.0000
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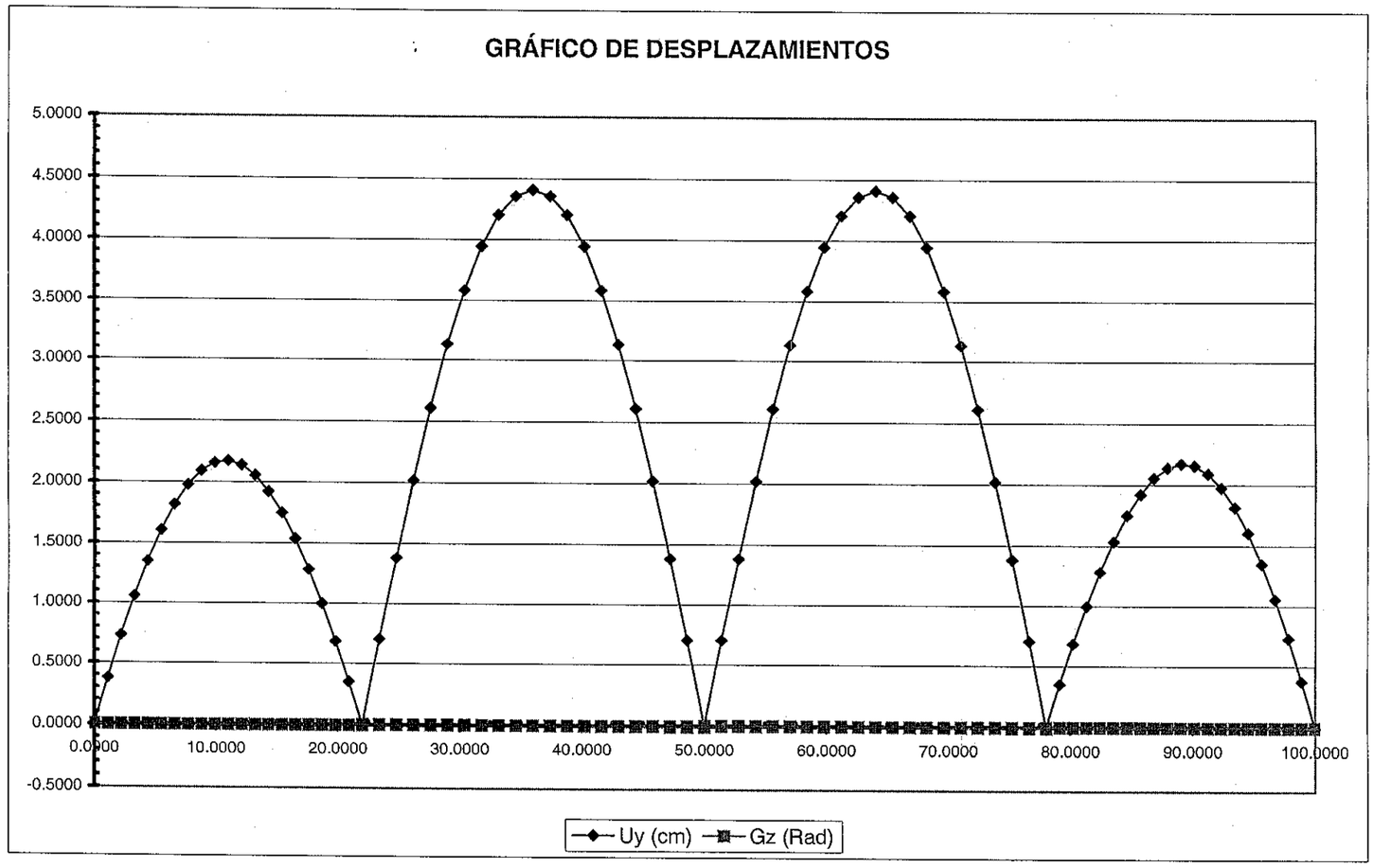
90.0000
100.0000
Uy (cm)
Gz (Rad)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2.5000
2.0000
1.5000
1.0000
0.5000
0.0000
-0.5000
0.0000
10.0000
20.0000
30.0000
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
100.0000
Uy (cm)
Gz (Rad)

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0032	0.0000
3	2.2000	-0.0064	0.0000
4	3.3000	-0.0094	0.0000
5	4.4000	-0.0123	0.0000
6	5.5000	-0.0149	0.0000
7	6.6000	-0.0171	0.0000
8	7.7000	-0.0190	0.0000
9	8.8000	-0.0204	0.0000
10	9.9000	-0.0213	0.0000
11	11.0000	-0.0215	0.0000
12	12.1000	-0.0211	0.0000
13	13.2000	-0.0200	0.0000
14	14.3000	-0.0181	0.0000
15	15.4000	-0.0153	0.0000
16	16.5000	-0.0116	0.0000
17	17.6000	-0.0072	0.0000
18	18.7000	-0.0026	0.0000
19	19.8000	0.0011	0.0000
20	20.9000	0.0026	0.0000
21	22.0000	0.0000	-0.0001
1021	22.0000	0.0000	-0.0001
22	23.4000	-0.0110	-0.0001
23	24.8000	-0.0275	-0.0001
24	26.2000	-0.0456	-0.0001
25	27.6000	-0.0627	-0.0001
26	29.0000	-0.0772	-0.0001
27	30.4000	-0.0886	-0.0001
28	31.8000	-0.0969	-0.0001
29	33.2000	-0.1023	0.0000
30	34.6000	-0.1047	0.0000
31	36.0000	-0.1044	0.0000
32	37.4000	-0.1013	0.0000
33	38.8000	-0.0957	0.0001
34	40.2000	-0.0876	0.0001
35	41.6000	-0.0771	0.0001
36	43.0000	-0.0644	0.0001
37	44.4000	-0.0496	0.0001
38	45.8000	-0.0335	0.0001
39	47.2000	-0.0177	0.0001
40	48.6000	-0.0052	0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0052	-0.0001
43	52.8000	-0.0177	-0.0001
44	54.2000	-0.0335	-0.0001
45	55.6000	-0.0496	-0.0001
46	57.0000	-0.0644	-0.0001
47	58.4000	-0.0771	-0.0001
48	59.8000	-0.0876	-0.0001
49	61.2000	-0.0957	-0.0001
50	62.6000	-0.1013	0.0000
51	64.0000	-0.1044	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.1047	0.0000
53	66.8000	-0.1023	0.0000
54	68.2000	-0.0969	0.0001
55	69.6000	-0.0886	0.0001
56	71.0000	-0.0772	0.0001
57	72.4000	-0.0627	0.0001
58	73.8000	-0.0456	0.0001
59	75.2000	-0.0275	0.0001
60	76.6000	-0.0110	0.0001
61	78.0000	0.0000	0.0001
1061	78.0000	0.0000	0.0001
62	79.1000	0.0026	0.0000
63	80.2000	0.0011	0.0000
64	81.3000	-0.0026	0.0000
65	82.4000	-0.0072	0.0000
66	83.5000	-0.0116	0.0000
67	84.6000	-0.0153	0.0000
68	85.7000	-0.0181	0.0000
69	86.8000	-0.0200	0.0000
70	87.9000	-0.0211	0.0000
71	89.0000	-0.0215	0.0000
72	90.1000	-0.0213	0.0000
73	91.2000	-0.0204	0.0000
74	92.3000	-0.0190	0.0000
75	93.4000	-0.0171	0.0000
76	94.5000	-0.0149	0.0000
77	95.6000	-0.0123	0.0000
78	96.7000	-0.0094	0.0000
79	97.8000	-0.0064	0.0000
80	98.9000	-0.0032	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0032	0.0000
103	2.2000	-0.0064	0.0000
104	3.3000	-0.0094	0.0000
105	4.4000	-0.0123	0.0000
106	5.5000	-0.0149	0.0000
107	6.6000	-0.0171	0.0000
108	7.7000	-0.0190	0.0000
109	8.8000	-0.0204	0.0000
110	9.9000	-0.0213	0.0000
111	11.0000	-0.0215	0.0000
112	12.1000	-0.0211	0.0000
113	13.2000	-0.0200	0.0000
114	14.3000	-0.0181	0.0000
115	15.4000	-0.0153	0.0000
116	16.5000	-0.0116	0.0000
117	17.6000	-0.0072	0.0000
118	18.7000	-0.0026	0.0000
119	19.8000	0.0011	0.0000
120	20.9000	0.0026	0.0000
121	22.0000	0.0000	-0.0001
1121	22.0000	0.0000	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0110	-0.0001
123	24.8000	-0.0275	-0.0001
124	26.2000	-0.0456	-0.0001
125	27.6000	-0.0627	-0.0001
126	29.0000	-0.0772	-0.0001
127	30.4000	-0.0886	-0.0001
128	31.8000	-0.0969	-0.0001
129	33.2000	-0.1023	0.0000
130	34.6000	-0.1047	0.0000
131	36.0000	-0.1044	0.0000
132	37.4000	-0.1013	0.0000
133	38.8000	-0.0957	0.0001
134	40.2000	-0.0876	0.0001
135	41.6000	-0.0771	0.0001
136	43.0000	-0.0644	0.0001
137	44.4000	-0.0496	0.0001
138	45.8000	-0.0335	0.0001
139	47.2000	-0.0177	0.0001
140	48.6000	-0.0052	0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0052	-0.0001
143	52.8000	-0.0177	-0.0001
144	54.2000	-0.0335	-0.0001
145	55.6000	-0.0496	-0.0001
146	57.0000	-0.0644	-0.0001
147	58.4000	-0.0771	-0.0001
148	59.8000	-0.0876	-0.0001
149	61.2000	-0.0957	-0.0001
150	62.6000	-0.1013	0.0000
151	64.0000	-0.1044	0.0000
152	65.4000	-0.1047	0.0000
153	66.8000	-0.1023	0.0000
154	68.2000	-0.0969	0.0001
155	69.6000	-0.0886	0.0001
156	71.0000	-0.0772	0.0001
157	72.4000	-0.0627	0.0001
158	73.8000	-0.0456	0.0001
159	75.2000	-0.0275	0.0001
160	76.6000	-0.0110	0.0001
161	78.0000	0.0000	0.0001
1161	78.0000	0.0000	0.0001
162	79.1000	0.0026	0.0000
163	80.2000	0.0011	0.0000
164	81.3000	-0.0026	0.0000
165	82.4000	-0.0072	0.0000
166	83.5000	-0.0116	0.0000
167	84.6000	-0.0153	0.0000
168	85.7000	-0.0181	0.0000
169	86.8000	-0.0200	0.0000
170	87.9000	-0.0211	0.0000
171	89.0000	-0.0215	0.0000
172	90.1000	-0.0213	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLP

Hormigonado losa sobre pilas

[1; 1]HLP

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0204	0.0000
174	92.3000	-0.0190	0.0000
175	93.4000	-0.0171	0.0000
176	94.5000	-0.0149	0.0000
177	95.6000	-0.0123	0.0000
178	96.7000	-0.0094	0.0000
179	97.8000	-0.0064	0.0000
180	98.9000	-0.0032	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0003
2	1.1000	-0.0318	-0.0003
3	2.2000	-0.0628	-0.0003
4	3.3000	-0.0920	-0.0003
5	4.4000	-0.1189	-0.0002
6	5.5000	-0.1427	-0.0002
7	6.6000	-0.1630	-0.0002
8	7.7000	-0.1792	-0.0001
9	8.8000	-0.1911	-0.0001
10	9.9000	-0.1982	0.0000
11	11.0000	-0.2006	0.0000
12	12.1000	-0.1982	0.0000
13	13.2000	-0.1909	0.0001
14	14.3000	-0.1790	0.0001
15	15.4000	-0.1627	0.0002
16	16.5000	-0.1425	0.0002
17	17.6000	-0.1187	0.0002
18	18.7000	-0.0919	0.0003
19	19.8000	-0.0627	0.0003
20	20.9000	-0.0318	0.0003
21	22.0000	0.0000	0.0003
1021	22.0000	0.0000	-0.0006
22	23.4000	-0.0836	-0.0006
23	24.8000	-0.1649	-0.0006
24	26.2000	-0.2417	-0.0005
25	27.6000	-0.3122	-0.0005
26	29.0000	-0.3748	-0.0004
27	30.4000	-0.4281	-0.0003
28	31.8000	-0.4709	-0.0003
29	33.2000	-0.5021	-0.0002
30	34.6000	-0.5210	-0.0001
31	36.0000	-0.5274	0.0000
32	37.4000	-0.5210	0.0001
33	38.8000	-0.5021	0.0002
34	40.2000	-0.4709	0.0003
35	41.6000	-0.4281	0.0003
36	43.0000	-0.3748	0.0004
37	44.4000	-0.3122	0.0005
38	45.8000	-0.2417	0.0005
39	47.2000	-0.1649	0.0006
40	48.6000	-0.0836	0.0006
41	50.0000	0.0000	0.0006
1041	50.0000	0.0000	-0.0006
42	51.4000	-0.0836	-0.0006
43	52.8000	-0.1649	-0.0006
44	54.2000	-0.2417	-0.0005
45	55.6000	-0.3122	-0.0005
46	57.0000	-0.3748	-0.0004
47	58.4000	-0.4281	-0.0003
48	59.8000	-0.4709	-0.0003
49	61.2000	-0.5021	-0.0002
50	62.6000	-0.5210	-0.0001
51	64.0000	-0.5274	0.0000

CÁLCULO DE DESPLAZAMIENTOS

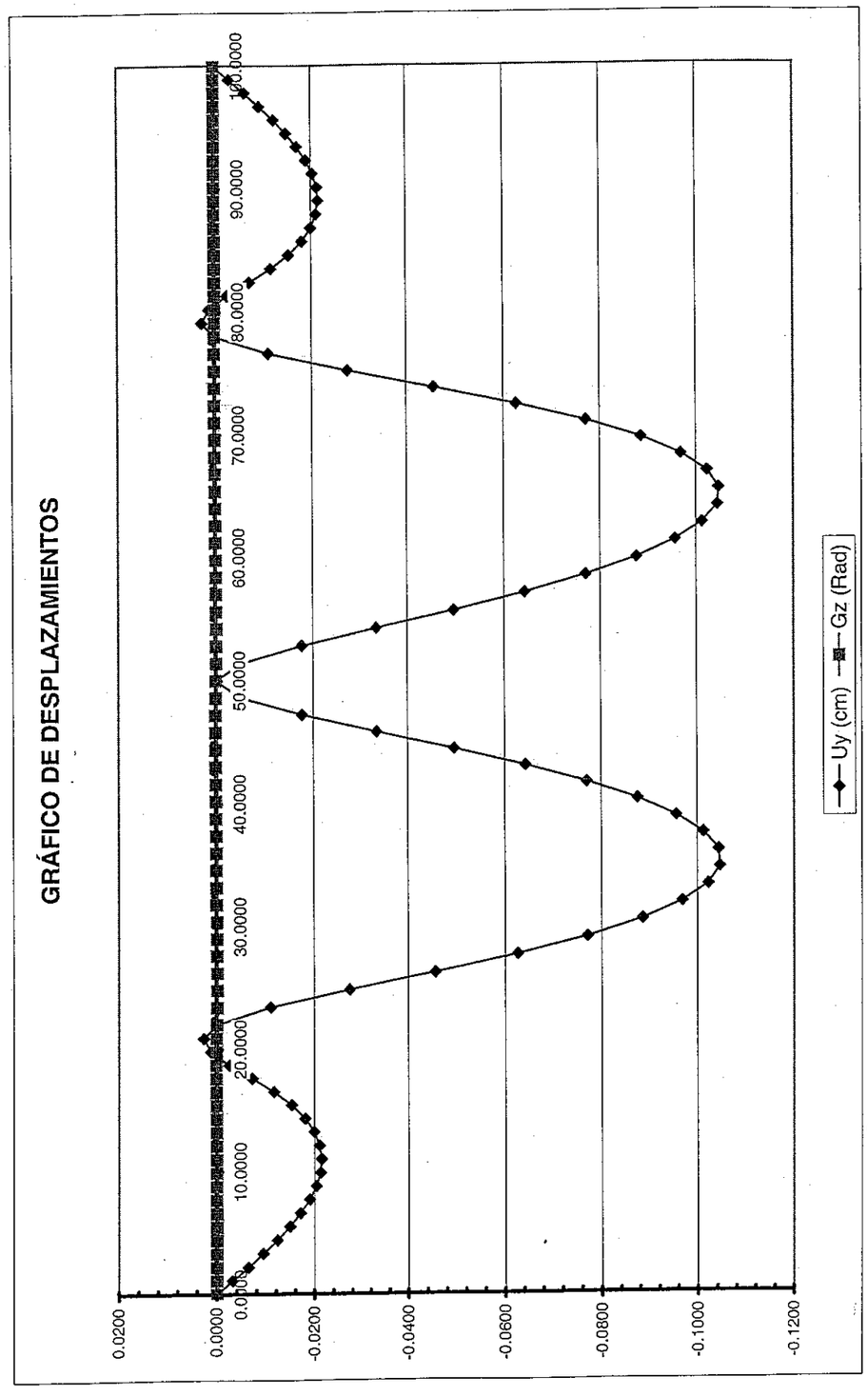
Hipótesis de cálculo:
PPLACAS

Peso placas fase 1

[1; 1]PPLACAS

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.5210	0.0001
53	66.8000	-0.5021	0.0002
54	68.2000	-0.4709	0.0003
55	69.6000	-0.4281	0.0003
56	71.0000	-0.3748	0.0004
57	72.4000	-0.3122	0.0005
58	73.8000	-0.2417	0.0005
59	75.2000	-0.1649	0.0006
60	76.6000	-0.0836	0.0006
61	78.0000	0.0000	0.0006
1061	78.0000	0.0000	-0.0003
62	79.1000	-0.0318	-0.0003
63	80.2000	-0.0627	-0.0003
64	81.3000	-0.0919	-0.0003
65	82.4000	-0.1187	-0.0002
66	83.5000	-0.1425	-0.0002
67	84.6000	-0.1627	-0.0002
68	85.7000	-0.1790	-0.0001
69	86.8000	-0.1909	-0.0001
70	87.9000	-0.1982	0.0000
71	89.0000	-0.2006	0.0000
72	90.1000	-0.1982	0.0000
73	91.2000	-0.1911	0.0001
74	92.3000	-0.1792	0.0001
75	93.4000	-0.1630	0.0002
76	94.5000	-0.1427	0.0002
77	95.6000	-0.1189	0.0002
78	96.7000	-0.0920	0.0003
79	97.8000	-0.0628	0.0003
80	98.9000	-0.0318	0.0003
81	100.0000	0.0000	0.0003
101	0.0000	0.0000	-0.0003
102	1.1000	-0.0318	-0.0003
103	2.2000	-0.0628	-0.0003
104	3.3000	-0.0920	-0.0003
105	4.4000	-0.1189	-0.0002
106	5.5000	-0.1427	-0.0002
107	6.6000	-0.1630	-0.0002
108	7.7000	-0.1792	-0.0001
109	8.8000	-0.1911	-0.0001
110	9.9000	-0.1982	0.0000
111	11.0000	-0.2006	0.0000
112	12.1000	-0.1982	0.0000
113	13.2000	-0.1909	0.0001
114	14.3000	-0.1790	0.0001
115	15.4000	-0.1627	0.0002
116	16.5000	-0.1425	0.0002
117	17.6000	-0.1187	0.0002
118	18.7000	-0.0919	0.0003
119	19.8000	-0.0627	0.0003
120	20.9000	-0.0318	0.0003
121	22.0000	0.0000	0.0003
1121	22.0000	0.0000	-0.0006



CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLCV

Hormigonado losa centros de vano

[1; 1]HLCV

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0005
2	1.1000	-0.0499	-0.0005
3	2.2000	-0.0974	-0.0004
4	3.3000	-0.1402	-0.0004
5	4.4000	-0.1766	-0.0003
6	5.5000	-0.2055	-0.0002
7	6.6000	-0.2260	-0.0002
8	7.7000	-0.2374	-0.0001
9	8.8000	-0.2397	0.0000
10	9.9000	-0.2333	0.0001
11	11.0000	-0.2191	0.0002
12	12.1000	-0.1983	0.0002
13	13.2000	-0.1726	0.0003
14	14.3000	-0.1443	0.0003
15	15.4000	-0.1156	0.0003
16	16.5000	-0.0891	0.0002
17	17.6000	-0.0642	0.0002
18	18.7000	-0.0419	0.0002
19	19.8000	-0.0232	0.0002
20	20.9000	-0.0089	0.0001
21	22.0000	0.0000	0.0001
1021	22.0000	0.0000	0.0001
22	23.4000	0.0028	0.0000
23	24.8000	-0.0029	-0.0001
24	26.2000	-0.0153	-0.0001
25	27.6000	-0.0328	-0.0001
26	29.0000	-0.0538	-0.0002
27	30.4000	-0.0788	-0.0002
28	31.8000	-0.1048	-0.0002
29	33.2000	-0.1275	-0.0001
30	34.6000	-0.1438	-0.0001
31	36.0000	-0.1518	0.0000
32	37.4000	-0.1504	0.0000
33	38.8000	-0.1401	0.0001
34	40.2000	-0.1221	0.0002
35	41.6000	-0.0991	0.0002
36	43.0000	-0.0744	0.0002
37	44.4000	-0.0516	0.0002
38	45.8000	-0.0313	0.0001
39	47.2000	-0.0149	0.0001
40	48.6000	-0.0040	0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0040	-0.0001
43	52.8000	-0.0149	-0.0001
44	54.2000	-0.0313	-0.0001
45	55.6000	-0.0516	-0.0002
46	57.0000	-0.0744	-0.0002
47	58.4000	-0.0991	-0.0002
48	59.8000	-0.1221	-0.0002
49	61.2000	-0.1401	-0.0001
50	62.6000	-0.1504	0.0000
51	64.0000	-0.1518	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLCV
Hormigonado losa centros de vano
[1; 1]HLCV
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.1438	0.0001
53	66.8000	-0.1275	0.0001
54	68.2000	-0.1048	0.0002
55	69.6000	-0.0788	0.0002
56	71.0000	-0.0538	0.0002
57	72.4000	-0.0328	0.0001
58	73.8000	-0.0153	0.0001
59	75.2000	-0.0029	0.0001
60	76.6000	0.0028	0.0000
61	78.0000	0.0000	-0.0001
1061	78.0000	0.0000	-0.0001
62	79.1000	-0.0089	-0.0001
63	80.2000	-0.0232	-0.0002
64	81.3000	-0.0419	-0.0002
65	82.4000	-0.0642	-0.0002
66	83.5000	-0.0891	-0.0002
67	84.6000	-0.1156	-0.0003
68	85.7000	-0.1443	-0.0003
69	86.8000	-0.1726	-0.0003
70	87.9000	-0.1983	-0.0002
71	89.0000	-0.2191	-0.0002
72	90.1000	-0.2333	-0.0001
73	91.2000	-0.2397	0.0000
74	92.3000	-0.2374	0.0001
75	93.4000	-0.2260	0.0002
76	94.5000	-0.2055	0.0002
77	95.6000	-0.1766	0.0003
78	96.7000	-0.1402	0.0004
79	97.8000	-0.0974	0.0004
80	98.9000	-0.0499	0.0005
81	100.0000	0.0000	0.0005
101	0.0000	0.0000	-0.0005
102	1.1000	-0.0499	-0.0005
103	2.2000	-0.0974	-0.0004
104	3.3000	-0.1402	-0.0004
105	4.4000	-0.1766	-0.0003
106	5.5000	-0.2055	-0.0002
107	6.6000	-0.2260	-0.0002
108	7.7000	-0.2374	-0.0001
109	8.8000	-0.2397	0.0000
110	9.9000	-0.2333	0.0001
111	11.0000	-0.2191	0.0002
112	12.1000	-0.1983	0.0002
113	13.2000	-0.1726	0.0003
114	14.3000	-0.1443	0.0003
115	15.4000	-0.1156	0.0003
116	16.5000	-0.0891	0.0002
117	17.6000	-0.0642	0.0002
118	18.7000	-0.0419	0.0002
119	19.8000	-0.0232	0.0002
120	20.9000	-0.0089	0.0001
121	22.0000	0.0000	0.0001
1121	22.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLCV
Hormigonado losa centros de vano
[1; 1]HLCV
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0028	0.0000
123	24.8000	-0.0029	-0.0001
124	26.2000	-0.0153	-0.0001
125	27.6000	-0.0328	-0.0001
126	29.0000	-0.0538	-0.0002
127	30.4000	-0.0788	-0.0002
128	31.8000	-0.1048	-0.0002
129	33.2000	-0.1275	-0.0001
130	34.6000	-0.1438	-0.0001
131	36.0000	-0.1518	0.0000
132	37.4000	-0.1504	0.0000
133	38.8000	-0.1401	0.0001
134	40.2000	-0.1221	0.0002
135	41.6000	-0.0991	0.0002
136	43.0000	-0.0744	0.0002
137	44.4000	-0.0516	0.0002
138	45.8000	-0.0313	0.0001
139	47.2000	-0.0149	0.0001
140	48.6000	-0.0040	0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0040	-0.0001
143	52.8000	-0.0149	-0.0001
144	54.2000	-0.0313	-0.0001
145	55.6000	-0.0516	-0.0002
146	57.0000	-0.0744	-0.0002
147	58.4000	-0.0991	-0.0002
148	59.8000	-0.1221	-0.0002
149	61.2000	-0.1401	-0.0001
150	62.6000	-0.1504	0.0000
151	64.0000	-0.1518	0.0000
152	65.4000	-0.1438	0.0001
153	66.8000	-0.1275	0.0001
154	68.2000	-0.1048	0.0002
155	69.6000	-0.0788	0.0002
156	71.0000	-0.0538	0.0002
157	72.4000	-0.0328	0.0001
158	73.8000	-0.0153	0.0001
159	75.2000	-0.0029	0.0001
160	76.6000	0.0028	0.0000
161	78.0000	0.0000	-0.0001
1161	78.0000	0.0000	-0.0001
162	79.1000	-0.0089	-0.0001
163	80.2000	-0.0232	-0.0002
164	81.3000	-0.0419	-0.0002
165	82.4000	-0.0642	-0.0002
166	83.5000	-0.0891	-0.0002
167	84.6000	-0.1156	-0.0003
168	85.7000	-0.1443	-0.0003
169	86.8000	-0.1726	-0.0003
170	87.9000	-0.1983	-0.0002
171	89.0000	-0.2191	-0.0002
172	90.1000	-0.2333	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
HLCV

Hormigonado losa centros de vano

[1; 1]HLCV

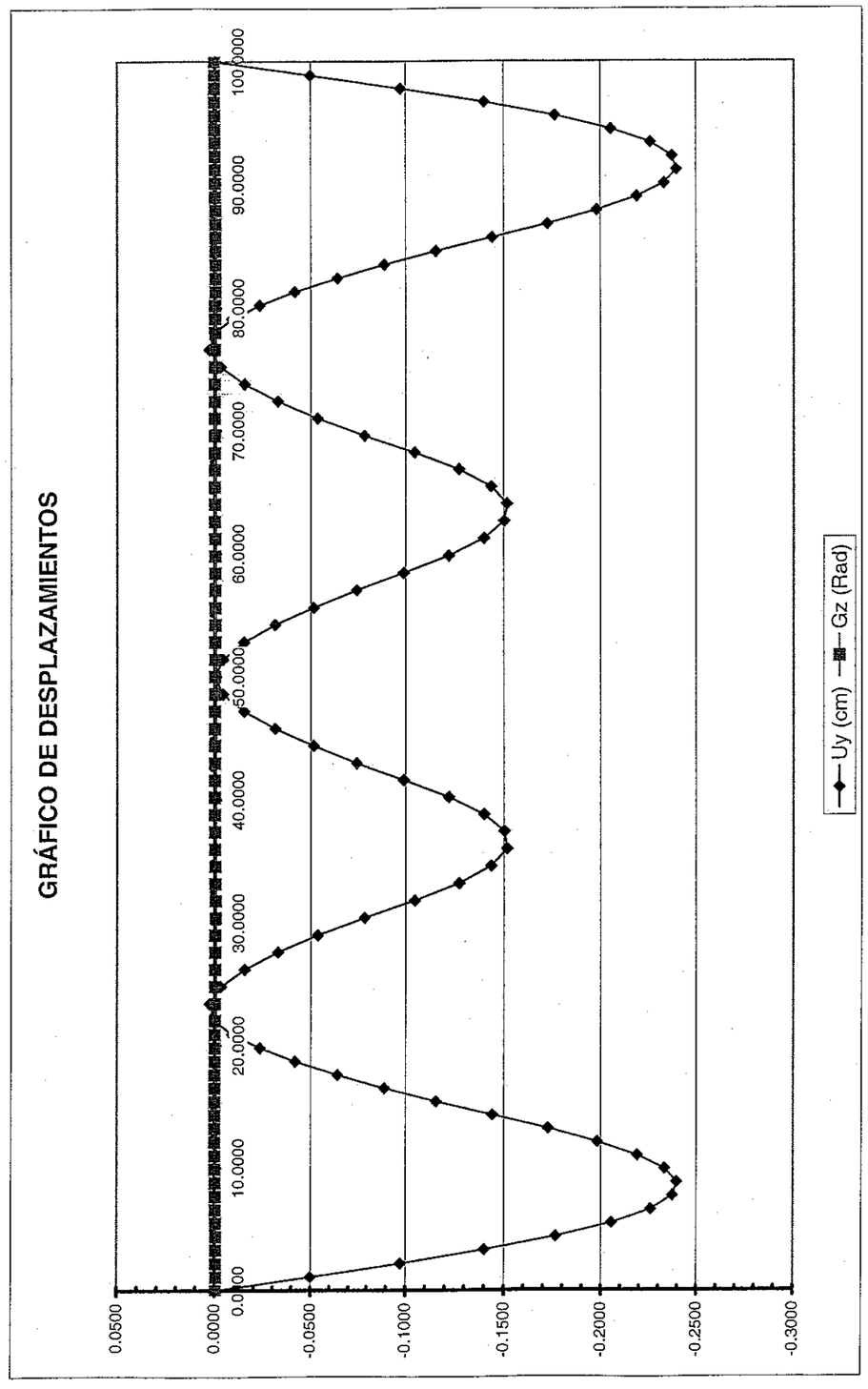
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.2397	0.0000
174	92.3000	-0.2374	0.0001
175	93.4000	-0.2260	0.0002
176	94.5000	-0.2055	0.0002
177	95.6000	-0.1766	0.0003
178	96.7000	-0.1402	0.0004
179	97.8000	-0.0974	0.0004
180	98.9000	-0.0499	0.0005
181	100.0000	0.0000	0.0005

23/09/03

Programa DINTEL PACADAR S.A.
HLCV

F3.desp.xls



CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVEI

Peso propio vigas en estructura ideal

[1; 1]PPVEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0001
2	1.1000	-0.0126	-0.0001
3	2.2000	-0.0246	-0.0001
4	3.3000	-0.0355	-0.0001
5	4.4000	-0.0451	-0.0001
6	5.5000	-0.0529	-0.0001
7	6.6000	-0.0588	0.0000
8	7.7000	-0.0626	0.0000
9	8.8000	-0.0643	0.0000
10	9.9000	-0.0639	0.0000
11	11.0000	-0.0614	0.0000
12	12.1000	-0.0572	0.0001
13	13.2000	-0.0513	0.0001
14	14.3000	-0.0441	0.0001
15	15.4000	-0.0359	0.0001
16	16.5000	-0.0273	0.0001
17	17.6000	-0.0189	0.0001
18	18.7000	-0.0111	0.0001
19	19.8000	-0.0048	0.0001
20	20.9000	-0.0008	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0043	-0.0001
23	24.8000	-0.0134	-0.0001
24	26.2000	-0.0253	-0.0001
25	27.6000	-0.0387	-0.0001
26	29.0000	-0.0522	-0.0001
27	30.4000	-0.0646	-0.0001
28	31.8000	-0.0750	-0.0001
29	33.2000	-0.0829	-0.0001
30	34.6000	-0.0876	0.0000
31	36.0000	-0.0890	0.0000
32	37.4000	-0.0870	0.0000
33	38.8000	-0.0816	0.0001
34	40.2000	-0.0732	0.0001
35	41.6000	-0.0624	0.0001
36	43.0000	-0.0497	0.0001
37	44.4000	-0.0362	0.0001
38	45.8000	-0.0230	0.0001
39	47.2000	-0.0114	0.0001
40	48.6000	-0.0032	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0032	0.0000
43	52.8000	-0.0114	-0.0001
44	54.2000	-0.0230	-0.0001
45	55.6000	-0.0362	-0.0001
46	57.0000	-0.0497	-0.0001
47	58.4000	-0.0624	-0.0001
48	59.8000	-0.0732	-0.0001
49	61.2000	-0.0816	-0.0001
50	62.6000	-0.0870	0.0000
51	64.0000	-0.0890	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVEI

Peso propio vigas en estructura ideal

[1; 1]PPVEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0876	0.0000
53	66.8000	-0.0829	0.0001
54	68.2000	-0.0750	0.0001
55	69.6000	-0.0646	0.0001
56	71.0000	-0.0522	0.0001
57	72.4000	-0.0387	0.0001
58	73.8000	-0.0253	0.0001
59	75.2000	-0.0134	0.0001
60	76.6000	-0.0043	0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0008	0.0000
63	80.2000	-0.0048	-0.0001
64	81.3000	-0.0111	-0.0001
65	82.4000	-0.0189	-0.0001
66	83.5000	-0.0273	-0.0001
67	84.6000	-0.0359	-0.0001
68	85.7000	-0.0441	-0.0001
69	86.8000	-0.0513	-0.0001
70	87.9000	-0.0572	-0.0001
71	89.0000	-0.0614	0.0000
72	90.1000	-0.0639	0.0000
73	91.2000	-0.0643	0.0000
74	92.3000	-0.0626	0.0000
75	93.4000	-0.0588	0.0000
76	94.5000	-0.0529	0.0001
77	95.6000	-0.0451	0.0001
78	96.7000	-0.0355	0.0001
79	97.8000	-0.0246	0.0001
80	98.9000	-0.0126	0.0001
81	100.0000	0.0000	0.0001
101	0.0000	0.0000	-0.0001
102	1.1000	-0.0126	-0.0001
103	2.2000	-0.0246	-0.0001
104	3.3000	-0.0355	-0.0001
105	4.4000	-0.0451	-0.0001
106	5.5000	-0.0529	-0.0001
107	6.6000	-0.0588	0.0000
108	7.7000	-0.0626	0.0000
109	8.8000	-0.0643	0.0000
110	9.9000	-0.0639	0.0000
111	11.0000	-0.0614	0.0000
112	12.1000	-0.0572	0.0001
113	13.2000	-0.0513	0.0001
114	14.3000	-0.0441	0.0001
115	15.4000	-0.0359	0.0001
116	16.5000	-0.0273	0.0001
117	17.6000	-0.0189	0.0001
118	18.7000	-0.0111	0.0001
119	19.8000	-0.0048	0.0001
120	20.9000	-0.0008	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVEI

Peso propio vigas en estructura ideal

[1; 1]PPVEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0043	-0.0001
123	24.8000	-0.0134	-0.0001
124	26.2000	-0.0253	-0.0001
125	27.6000	-0.0387	-0.0001
126	29.0000	-0.0522	-0.0001
127	30.4000	-0.0646	-0.0001
128	31.8000	-0.0750	-0.0001
129	33.2000	-0.0829	-0.0001
130	34.6000	-0.0876	0.0000
131	36.0000	-0.0890	0.0000
132	37.4000	-0.0870	0.0000
133	38.8000	-0.0816	0.0001
134	40.2000	-0.0732	0.0001
135	41.6000	-0.0624	0.0001
136	43.0000	-0.0497	0.0001
137	44.4000	-0.0362	0.0001
138	45.8000	-0.0230	0.0001
139	47.2000	-0.0114	0.0001
140	48.6000	-0.0032	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0032	0.0000
143	52.8000	-0.0114	-0.0001
144	54.2000	-0.0230	-0.0001
145	55.6000	-0.0362	-0.0001
146	57.0000	-0.0497	-0.0001
147	58.4000	-0.0624	-0.0001
148	59.8000	-0.0732	-0.0001
149	61.2000	-0.0816	-0.0001
150	62.6000	-0.0870	0.0000
151	64.0000	-0.0890	0.0000
152	65.4000	-0.0876	0.0000
153	66.8000	-0.0829	0.0001
154	68.2000	-0.0750	0.0001
155	69.6000	-0.0646	0.0001
156	71.0000	-0.0522	0.0001
157	72.4000	-0.0387	0.0001
158	73.8000	-0.0253	0.0001
159	75.2000	-0.0134	0.0001
160	76.6000	-0.0043	0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0008	0.0000
163	80.2000	-0.0048	-0.0001
164	81.3000	-0.0111	-0.0001
165	82.4000	-0.0189	-0.0001
166	83.5000	-0.0273	-0.0001
167	84.6000	-0.0359	-0.0001
168	85.7000	-0.0441	-0.0001
169	86.8000	-0.0513	-0.0001
170	87.9000	-0.0572	-0.0001
171	89.0000	-0.0614	0.0000
172	90.1000	-0.0639	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PPVEI

Peso propio vigas en estructura ideal

[1; 1]PPVEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0643	0.0000
174	92.3000	-0.0626	0.0000
175	93.4000	-0.0588	0.0000
176	94.5000	-0.0529	0.0001
177	95.6000	-0.0451	0.0001
178	96.7000	-0.0355	0.0001
179	97.8000	-0.0246	0.0001
180	98.9000	-0.0126	0.0001
181	100.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0002
2	1.1000	-0.0229	-0.0002
3	2.2000	-0.0449	-0.0002
4	3.3000	-0.0649	-0.0002
5	4.4000	-0.0824	-0.0002
6	5.5000	-0.0967	-0.0001
7	6.6000	-0.1074	-0.0001
8	7.7000	-0.1144	-0.0001
9	8.8000	-0.1174	0.0000
10	9.9000	-0.1167	0.0000
11	11.0000	-0.1123	0.0001
12	12.1000	-0.1044	0.0001
13	13.2000	-0.0937	0.0001
14	14.3000	-0.0805	0.0001
15	15.4000	-0.0657	0.0001
16	16.5000	-0.0500	0.0001
17	17.6000	-0.0345	0.0001
18	18.7000	-0.0203	0.0001
19	19.8000	-0.0089	0.0001
20	20.9000	-0.0015	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0079	-0.0001
23	24.8000	-0.0244	-0.0001
24	26.2000	-0.0463	-0.0002
25	27.6000	-0.0708	-0.0002
26	29.0000	-0.0954	-0.0002
27	30.4000	-0.1180	-0.0002
28	31.8000	-0.1371	-0.0001
29	33.2000	-0.1514	-0.0001
30	34.6000	-0.1602	0.0000
31	36.0000	-0.1627	0.0000
32	37.4000	-0.1590	0.0001
33	38.8000	-0.1491	0.0001
34	40.2000	-0.1338	0.0001
35	41.6000	-0.1140	0.0002
36	43.0000	-0.0908	0.0002
37	44.4000	-0.0661	0.0002
38	45.8000	-0.0420	0.0002
39	47.2000	-0.0209	0.0001
40	48.6000	-0.0058	0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0058	-0.0001
43	52.8000	-0.0209	-0.0001
44	54.2000	-0.0420	-0.0002
45	55.6000	-0.0661	-0.0002
46	57.0000	-0.0908	-0.0002
47	58.4000	-0.1140	-0.0002
48	59.8000	-0.1338	-0.0001
49	61.2000	-0.1491	-0.0001
50	62.6000	-0.1590	-0.0001
51	64.0000	-0.1627	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.1602	0.0000
53	66.8000	-0.1515	0.0001
54	68.2000	-0.1371	0.0001
55	69.6000	-0.1180	0.0002
56	71.0000	-0.0954	0.0002
57	72.4000	-0.0708	0.0002
58	73.8000	-0.0463	0.0002
59	75.2000	-0.0244	0.0001
60	76.6000	-0.0079	0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0015	0.0000
63	80.2000	-0.0089	-0.0001
64	81.3000	-0.0203	-0.0001
65	82.4000	-0.0345	-0.0001
66	83.5000	-0.0500	-0.0001
67	84.6000	-0.0657	-0.0001
68	85.7000	-0.0805	-0.0001
69	86.8000	-0.0937	-0.0001
70	87.9000	-0.1044	-0.0001
71	89.0000	-0.1123	-0.0001
72	90.1000	-0.1167	0.0000
73	91.2000	-0.1174	0.0000
74	92.3000	-0.1144	0.0001
75	93.4000	-0.1074	0.0001
76	94.5000	-0.0967	0.0001
77	95.6000	-0.0824	0.0002
78	96.7000	-0.0649	0.0002
79	97.8000	-0.0449	0.0002
80	98.9000	-0.0229	0.0002
81	100.0000	0.0000	0.0002
101	0.0000	0.0000	-0.0002
102	1.1000	-0.0229	-0.0002
103	2.2000	-0.0449	-0.0002
104	3.3000	-0.0649	-0.0002
105	4.4000	-0.0824	-0.0002
106	5.5000	-0.0967	-0.0001
107	6.6000	-0.1074	-0.0001
108	7.7000	-0.1144	-0.0001
109	8.8000	-0.1174	0.0000
110	9.9000	-0.1167	0.0000
111	11.0000	-0.1123	0.0001
112	12.1000	-0.1044	0.0001
113	13.2000	-0.0937	0.0001
114	14.3000	-0.0805	0.0001
115	15.4000	-0.0657	0.0001
116	16.5000	-0.0500	0.0001
117	17.6000	-0.0345	0.0001
118	18.7000	-0.0203	0.0001
119	19.8000	-0.0089	0.0001
120	20.9000	-0.0015	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0079	-0.0001
123	24.8000	-0.0244	-0.0001
124	26.2000	-0.0463	-0.0002
125	27.6000	-0.0708	-0.0002
126	29.0000	-0.0954	-0.0002
127	30.4000	-0.1180	-0.0002
128	31.8000	-0.1371	-0.0001
129	33.2000	-0.1515	-0.0001
130	34.6000	-0.1602	0.0000
131	36.0000	-0.1627	0.0000
132	37.4000	-0.1590	0.0001
133	38.8000	-0.1491	0.0001
134	40.2000	-0.1338	0.0001
135	41.6000	-0.1140	0.0002
136	43.0000	-0.0908	0.0002
137	44.4000	-0.0661	0.0002
138	45.8000	-0.0420	0.0002
139	47.2000	-0.0209	0.0001
140	48.6000	-0.0058	0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0058	-0.0001
143	52.8000	-0.0209	-0.0001
144	54.2000	-0.0420	-0.0002
145	55.6000	-0.0661	-0.0002
146	57.0000	-0.0908	-0.0002
147	58.4000	-0.1140	-0.0002
148	59.8000	-0.1338	-0.0001
149	61.2000	-0.1491	-0.0001
150	62.6000	-0.1590	-0.0001
151	64.0000	-0.1627	0.0000
152	65.4000	-0.1602	0.0000
153	66.8000	-0.1515	0.0001
154	68.2000	-0.1371	0.0001
155	69.6000	-0.1180	0.0002
156	71.0000	-0.0954	0.0002
157	72.4000	-0.0708	0.0002
158	73.8000	-0.0463	0.0002
159	75.2000	-0.0244	0.0001
160	76.6000	-0.0079	0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0015	0.0000
163	80.2000	-0.0089	-0.0001
164	81.3000	-0.0203	-0.0001
165	82.4000	-0.0345	-0.0001
166	83.5000	-0.0500	-0.0001
167	84.6000	-0.0657	-0.0001
168	85.7000	-0.0805	-0.0001
169	86.8000	-0.0937	-0.0001
170	87.9000	-0.1044	-0.0001
171	89.0000	-0.1123	-0.0001
172	90.1000	-0.1167	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.1174	0.0000
174	92.3000	-0.1144	0.0001
175	93.4000	-0.1074	0.0001
176	94.5000	-0.0967	0.0001
177	95.6000	-0.0824	0.0002
178	96.7000	-0.0649	0.0002
179	97.8000	-0.0449	0.0002
180	98.9000	-0.0229	0.0002
181	100.0000	0.0000	0.0002

CMBALASTO

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0002
2	1.1000	-0.0264	-0.0002
3	2.2000	-0.0516	-0.0002
4	3.3000	-0.0747	-0.0002
5	4.4000	-0.0948	-0.0002
6	5.5000	-0.1112	-0.0001
7	6.6000	-0.1235	-0.0001
8	7.7000	-0.1315	-0.0001
9	8.8000	-0.1351	0.0000
10	9.9000	-0.1342	0.0000
11	11.0000	-0.1292	0.0001
12	12.1000	-0.1202	0.0001
13	13.2000	-0.1079	0.0001
14	14.3000	-0.0928	0.0002
15	15.4000	-0.0758	0.0002
16	16.5000	-0.0577	0.0002
17	17.6000	-0.0399	0.0002
18	18.7000	-0.0236	0.0001
19	19.8000	-0.0104	0.0001
20	20.9000	-0.0019	0.0001
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0089	-0.0001
23	24.8000	-0.0278	-0.0002
24	26.2000	-0.0528	-0.0002
25	27.6000	-0.0807	-0.0002
26	29.0000	-0.1088	-0.0002
27	30.4000	-0.1347	-0.0002
28	31.8000	-0.1565	-0.0001
29	33.2000	-0.1728	-0.0001
30	34.6000	-0.1828	-0.0001
31	36.0000	-0.1857	0.0000
32	37.4000	-0.1815	0.0001
33	38.8000	-0.1703	0.0001
34	40.2000	-0.1529	0.0001
35	41.6000	-0.1302	0.0002
36	43.0000	-0.1038	0.0002
37	44.4000	-0.0756	0.0002
38	45.8000	-0.0480	0.0002
39	47.2000	-0.0239	0.0002
40	48.6000	-0.0067	0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0067	-0.0001
43	52.8000	-0.0239	-0.0002
44	54.2000	-0.0480	-0.0002
45	55.6000	-0.0756	-0.0002
46	57.0000	-0.1038	-0.0002
47	58.4000	-0.1302	-0.0002
48	59.8000	-0.1529	-0.0001
49	61.2000	-0.1703	-0.0001
50	62.6000	-0.1815	-0.0001
51	64.0000	-0.1857	0.0000

CMBALASTO

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.1828	0.0001
53	66.8000	-0.1728	0.0001
54	68.2000	-0.1565	0.0001
55	69.6000	-0.1347	0.0002
56	71.0000	-0.1088	0.0002
57	72.4000	-0.0807	0.0002
58	73.8000	-0.0528	0.0002
59	75.2000	-0.0278	0.0002
60	76.6000	-0.0089	0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0019	-0.0001
63	80.2000	-0.0104	-0.0001
64	81.3000	-0.0236	-0.0001
65	82.4000	-0.0399	-0.0002
66	83.5000	-0.0577	-0.0002
67	84.6000	-0.0758	-0.0002
68	85.7000	-0.0928	-0.0002
69	86.8000	-0.1079	-0.0001
70	87.9000	-0.1202	-0.0001
71	89.0000	-0.1292	-0.0001
72	90.1000	-0.1342	0.0000
73	91.2000	-0.1351	0.0000
74	92.3000	-0.1315	0.0001
75	93.4000	-0.1235	0.0001
76	94.5000	-0.1112	0.0001
77	95.6000	-0.0948	0.0002
78	96.7000	-0.0747	0.0002
79	97.8000	-0.0516	0.0002
80	98.9000	-0.0264	0.0002
81	100.0000	0.0000	0.0002
101	0.0000	0.0000	-0.0002
102	1.1000	-0.0217	-0.0002
103	2.2000	-0.0425	-0.0002
104	3.3000	-0.0615	-0.0002
105	4.4000	-0.0780	-0.0001
106	5.5000	-0.0915	-0.0001
107	6.6000	-0.1017	-0.0001
108	7.7000	-0.1082	0.0000
109	8.8000	-0.1111	0.0000
110	9.9000	-0.1104	0.0000
111	11.0000	-0.1062	0.0001
112	12.1000	-0.0987	0.0001
113	13.2000	-0.0885	0.0001
114	14.3000	-0.0760	0.0001
115	15.4000	-0.0619	0.0001
116	16.5000	-0.0470	0.0001
117	17.6000	-0.0324	0.0001
118	18.7000	-0.0190	0.0001
119	19.8000	-0.0082	0.0001
120	20.9000	-0.0014	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CMBALASTO

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0076	-0.0001
123	24.8000	-0.0234	-0.0001
124	26.2000	-0.0443	-0.0002
125	27.6000	-0.0676	-0.0002
126	29.0000	-0.0911	-0.0002
127	30.4000	-0.1127	-0.0001
128	31.8000	-0.1309	-0.0001
129	33.2000	-0.1446	-0.0001
130	34.6000	-0.1529	0.0000
131	36.0000	-0.1553	0.0000
132	37.4000	-0.1517	0.0001
133	38.8000	-0.1423	0.0001
134	40.2000	-0.1276	0.0001
135	41.6000	-0.1086	0.0002
136	43.0000	-0.0865	0.0002
137	44.4000	-0.0630	0.0002
138	45.8000	-0.0399	0.0002
139	47.2000	-0.0199	0.0001
140	48.6000	-0.0055	0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0055	-0.0001
143	52.8000	-0.0199	-0.0001
144	54.2000	-0.0399	-0.0002
145	55.6000	-0.0630	-0.0002
146	57.0000	-0.0865	-0.0002
147	58.4000	-0.1086	-0.0002
148	59.8000	-0.1276	-0.0001
149	61.2000	-0.1423	-0.0001
150	62.6000	-0.1517	-0.0001
151	64.0000	-0.1553	0.0000
152	65.4000	-0.1529	0.0000
153	66.8000	-0.1446	0.0001
154	68.2000	-0.1309	0.0001
155	69.6000	-0.1127	0.0001
156	71.0000	-0.0911	0.0002
157	72.4000	-0.0676	0.0002
158	73.8000	-0.0443	0.0002
159	75.2000	-0.0234	0.0001
160	76.6000	-0.0076	0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0014	0.0000
163	80.2000	-0.0082	-0.0001
164	81.3000	-0.0190	-0.0001
165	82.4000	-0.0324	-0.0001
166	83.5000	-0.0470	-0.0001
167	84.6000	-0.0619	-0.0001
168	85.7000	-0.0760	-0.0001
169	86.8000	-0.0885	-0.0001
170	87.9000	-0.0987	-0.0001
171	89.0000	-0.1062	-0.0001
172	90.1000	-0.1104	0.0000

CMBALASTO

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.1111	0.0000
174	92.3000	-0.1082	0.0000
175	93.4000	-0.1017	0.0001
176	94.5000	-0.0915	0.0001
177	95.6000	-0.0780	0.0001
178	96.7000	-0.0615	0.0002
179	97.8000	-0.0425	0.0002
180	98.9000	-0.0217	0.0002
181	100.0000	0.0000	0.0002

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0001
2	1.1000	-0.0099	-0.0001
3	2.2000	-0.0193	-0.0001
4	3.3000	-0.0279	-0.0001
5	4.4000	-0.0354	-0.0001
6	5.5000	-0.0415	-0.0001
7	6.6000	-0.0461	0.0000
8	7.7000	-0.0491	0.0000
9	8.8000	-0.0504	0.0000
10	9.9000	-0.0501	0.0000
11	11.0000	-0.0482	0.0000
12	12.1000	-0.0449	0.0000
13	13.2000	-0.0402	0.0001
14	14.3000	-0.0346	0.0001
15	15.4000	-0.0282	0.0001
16	16.5000	-0.0215	0.0001
17	17.6000	-0.0148	0.0001
18	18.7000	-0.0087	0.0001
19	19.8000	-0.0038	0.0000
20	20.9000	-0.0007	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0034	0.0000
23	24.8000	-0.0105	-0.0001
24	26.2000	-0.0199	-0.0001
25	27.6000	-0.0304	-0.0001
26	29.0000	-0.0410	-0.0001
27	30.4000	-0.0507	-0.0001
28	31.8000	-0.0589	-0.0001
29	33.2000	-0.0651	0.0000
30	34.6000	-0.0688	0.0000
31	36.0000	-0.0699	0.0000
32	37.4000	-0.0683	0.0000
33	38.8000	-0.0641	0.0000
34	40.2000	-0.0575	0.0001
35	41.6000	-0.0490	0.0001
36	43.0000	-0.0390	0.0001
37	44.4000	-0.0284	0.0001
38	45.8000	-0.0180	0.0001
39	47.2000	-0.0090	0.0001
40	48.6000	-0.0025	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0025	0.0000
43	52.8000	-0.0090	-0.0001
44	54.2000	-0.0180	-0.0001
45	55.6000	-0.0284	-0.0001
46	57.0000	-0.0390	-0.0001
47	58.4000	-0.0490	-0.0001
48	59.8000	-0.0575	-0.0001
49	61.2000	-0.0641	0.0000
50	62.6000	-0.0683	0.0000
51	64.0000	-0.0699	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0688	0.0000
53	66.8000	-0.0651	0.0000
54	68.2000	-0.0589	0.0001
55	69.6000	-0.0507	0.0001
56	71.0000	-0.0410	0.0001
57	72.4000	-0.0304	0.0001
58	73.8000	-0.0199	0.0001
59	75.2000	-0.0105	0.0001
60	76.6000	-0.0034	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0007	0.0000
63	80.2000	-0.0038	0.0000
64	81.3000	-0.0087	-0.0001
65	82.4000	-0.0148	-0.0001
66	83.5000	-0.0215	-0.0001
67	84.6000	-0.0282	-0.0001
68	85.7000	-0.0346	-0.0001
69	86.8000	-0.0402	-0.0001
70	87.9000	-0.0449	0.0000
71	89.0000	-0.0482	0.0000
72	90.1000	-0.0501	0.0000
73	91.2000	-0.0504	0.0000
74	92.3000	-0.0491	0.0000
75	93.4000	-0.0461	0.0000
76	94.5000	-0.0415	0.0001
77	95.6000	-0.0354	0.0001
78	96.7000	-0.0279	0.0001
79	97.8000	-0.0193	0.0001
80	98.9000	-0.0099	0.0001
81	100.0000	0.0000	0.0001
101	0.0000	0.0000	-0.0001
102	1.1000	-0.0099	-0.0001
103	2.2000	-0.0193	-0.0001
104	3.3000	-0.0279	-0.0001
105	4.4000	-0.0354	-0.0001
106	5.5000	-0.0415	-0.0001
107	6.6000	-0.0462	0.0000
108	7.7000	-0.0491	0.0000
109	8.8000	-0.0504	0.0000
110	9.9000	-0.0501	0.0000
111	11.0000	-0.0482	0.0000
112	12.1000	-0.0449	0.0000
113	13.2000	-0.0402	0.0001
114	14.3000	-0.0346	0.0001
115	15.4000	-0.0282	0.0001
116	16.5000	-0.0215	0.0001
117	17.6000	-0.0148	0.0001
118	18.7000	-0.0087	0.0001
119	19.8000	-0.0038	0.0000
120	20.9000	-0.0007	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0034	0.0000
123	24.8000	-0.0105	-0.0001
124	26.2000	-0.0199	-0.0001
125	27.6000	-0.0304	-0.0001
126	29.0000	-0.0410	-0.0001
127	30.4000	-0.0507	-0.0001
128	31.8000	-0.0589	-0.0001
129	33.2000	-0.0651	0.0000
130	34.6000	-0.0688	0.0000
131	36.0000	-0.0699	0.0000
132	37.4000	-0.0683	0.0000
133	38.8000	-0.0641	0.0000
134	40.2000	-0.0575	0.0001
135	41.6000	-0.0490	0.0001
136	43.0000	-0.0390	0.0001
137	44.4000	-0.0284	0.0001
138	45.8000	-0.0180	0.0001
139	47.2000	-0.0090	0.0001
140	48.6000	-0.0025	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0025	0.0000
143	52.8000	-0.0090	-0.0001
144	54.2000	-0.0180	-0.0001
145	55.6000	-0.0284	-0.0001
146	57.0000	-0.0390	-0.0001
147	58.4000	-0.0490	-0.0001
148	59.8000	-0.0575	-0.0001
149	61.2000	-0.0641	0.0000
150	62.6000	-0.0683	0.0000
151	64.0000	-0.0699	0.0000
152	65.4000	-0.0688	0.0000
153	66.8000	-0.0651	0.0000
154	68.2000	-0.0589	0.0001
155	69.6000	-0.0507	0.0001
156	71.0000	-0.0410	0.0001
157	72.4000	-0.0304	0.0001
158	73.8000	-0.0199	0.0001
159	75.2000	-0.0105	0.0001
160	76.6000	-0.0034	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0007	0.0000
163	80.2000	-0.0038	0.0000
164	81.3000	-0.0087	-0.0001
165	82.4000	-0.0148	-0.0001
166	83.5000	-0.0215	-0.0001
167	84.6000	-0.0282	-0.0001
168	85.7000	-0.0346	-0.0001
169	86.8000	-0.0402	-0.0001
170	87.9000	-0.0449	0.0000
171	89.0000	-0.0482	0.0000
172	90.1000	-0.0501	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0504	0.0000
174	92.3000	-0.0491	0.0000
175	93.4000	-0.0462	0.0000
176	94.5000	-0.0415	0.0001
177	95.6000	-0.0354	0.0001
178	96.7000	-0.0279	0.0001
179	97.8000	-0.0193	0.0001
180	98.9000	-0.0099	0.0001
181	100.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
GRAD

Gradiente térmico

[1; 1]GRAD

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0003
2	1.1000	0.0290	0.0002
3	2.2000	0.0529	0.0002
4	3.3000	0.0721	0.0002
5	4.4000	0.0869	0.0001
6	5.5000	0.0977	0.0001
7	6.6000	0.1047	0.0001
8	7.7000	0.1084	0.0000
9	8.8000	0.1090	0.0000
10	9.9000	0.1069	0.0000
11	11.0000	0.1022	-0.0001
12	12.1000	0.0955	-0.0001
13	13.2000	0.0871	-0.0001
14	14.3000	0.0771	-0.0001
15	15.4000	0.0662	-0.0001
16	16.5000	0.0547	-0.0001
17	17.6000	0.0429	-0.0001
18	18.7000	0.0312	-0.0001
19	19.8000	0.0199	-0.0001
20	20.9000	0.0094	-0.0001
21	22.0000	0.0000	-0.0001
1021	22.0000	0.0000	-0.0001
22	23.4000	-0.0100	-0.0001
23	24.8000	-0.0178	-0.0001
24	26.2000	-0.0236	0.0000
25	27.6000	-0.0275	0.0000
26	29.0000	-0.0297	0.0000
27	30.4000	-0.0304	0.0000
28	31.8000	-0.0299	0.0000
29	33.2000	-0.0286	0.0000
30	34.6000	-0.0265	0.0000
31	36.0000	-0.0240	0.0000
32	37.4000	-0.0211	0.0000
33	38.8000	-0.0180	0.0000
34	40.2000	-0.0148	0.0000
35	41.6000	-0.0118	0.0000
36	43.0000	-0.0089	0.0000
37	44.4000	-0.0062	0.0000
38	45.8000	-0.0037	0.0000
39	47.2000	-0.0018	0.0000
40	48.6000	-0.0005	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0005	0.0000
43	52.8000	-0.0018	0.0000
44	54.2000	-0.0037	0.0000
45	55.6000	-0.0062	0.0000
46	57.0000	-0.0089	0.0000
47	58.4000	-0.0118	0.0000
48	59.8000	-0.0148	0.0000
49	61.2000	-0.0180	0.0000
50	62.6000	-0.0211	0.0000
51	64.0000	-0.0240	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
GRAD

Gradiente térmico

[1; 1]GRAD

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0265	0.0000
53	66.8000	-0.0286	0.0000
54	68.2000	-0.0299	0.0000
55	69.6000	-0.0304	0.0000
56	71.0000	-0.0297	0.0000
57	72.4000	-0.0275	0.0000
58	73.8000	-0.0236	0.0000
59	75.2000	-0.0178	0.0001
60	76.6000	-0.0100	0.0001
61	78.0000	0.0000	0.0001
1061	78.0000	0.0000	0.0001
62	79.1000	0.0094	0.0001
63	80.2000	0.0199	0.0001
64	81.3000	0.0312	0.0001
65	82.4000	0.0429	0.0001
66	83.5000	0.0547	0.0001
67	84.6000	0.0662	0.0001
68	85.7000	0.0772	0.0001
69	86.8000	0.0871	0.0001
70	87.9000	0.0955	0.0001
71	89.0000	0.1022	0.0001
72	90.1000	0.1069	0.0000
73	91.2000	0.1090	0.0000
74	92.3000	0.1084	0.0000
75	93.4000	0.1047	-0.0001
76	94.5000	0.0977	-0.0001
77	95.6000	0.0869	-0.0001
78	96.7000	0.0721	-0.0002
79	97.8000	0.0529	-0.0002
80	98.9000	0.0290	-0.0002
81	100.0000	0.0000	-0.0003
101	0.0000	0.0000	0.0003
102	1.1000	0.0290	0.0002
103	2.2000	0.0529	0.0002
104	3.3000	0.0721	0.0002
105	4.4000	0.0869	0.0001
106	5.5000	0.0977	0.0001
107	6.6000	0.1047	0.0001
108	7.7000	0.1084	0.0000
109	8.8000	0.1090	0.0000
110	9.9000	0.1069	0.0000
111	11.0000	0.1023	-0.0001
112	12.1000	0.0955	-0.0001
113	13.2000	0.0871	-0.0001
114	14.3000	0.0772	-0.0001
115	15.4000	0.0662	-0.0001
116	16.5000	0.0547	-0.0001
117	17.6000	0.0429	-0.0001
118	18.7000	0.0312	-0.0001
119	19.8000	0.0199	-0.0001
120	20.9000	0.0094	-0.0001
121	22.0000	0.0000	-0.0001
1121	22.0000	0.0000	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
GRAD

Gradiente térmico

[1; 1]GRAD

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0100	-0.0001
123	24.8000	-0.0178	-0.0001
124	26.2000	-0.0236	0.0000
125	27.6000	-0.0275	0.0000
126	29.0000	-0.0297	0.0000
127	30.4000	-0.0304	0.0000
128	31.8000	-0.0299	0.0000
129	33.2000	-0.0286	0.0000
130	34.6000	-0.0265	0.0000
131	36.0000	-0.0240	0.0000
132	37.4000	-0.0211	0.0000
133	38.8000	-0.0180	0.0000
134	40.2000	-0.0148	0.0000
135	41.6000	-0.0118	0.0000
136	43.0000	-0.0089	0.0000
137	44.4000	-0.0062	0.0000
138	45.8000	-0.0037	0.0000
139	47.2000	-0.0018	0.0000
140	48.6000	-0.0005	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0005	0.0000
143	52.8000	-0.0018	0.0000
144	54.2000	-0.0037	0.0000
145	55.6000	-0.0062	0.0000
146	57.0000	-0.0089	0.0000
147	58.4000	-0.0118	0.0000
148	59.8000	-0.0148	0.0000
149	61.2000	-0.0180	0.0000
150	62.6000	-0.0211	0.0000
151	64.0000	-0.0240	0.0000
152	65.4000	-0.0265	0.0000
153	66.8000	-0.0286	0.0000
154	68.2000	-0.0299	0.0000
155	69.6000	-0.0304	0.0000
156	71.0000	-0.0297	0.0000
157	72.4000	-0.0275	0.0000
158	73.8000	-0.0236	0.0000
159	75.2000	-0.0178	0.0001
160	76.6000	-0.0100	0.0001
161	78.0000	0.0000	0.0001
1161	78.0000	0.0000	0.0001
162	79.1000	0.0094	0.0001
163	80.2000	0.0199	0.0001
164	81.3000	0.0312	0.0001
165	82.4000	0.0429	0.0001
166	83.5000	0.0547	0.0001
167	84.6000	0.0662	0.0001
168	85.7000	0.0772	0.0001
169	86.8000	0.0871	0.0001
170	87.9000	0.0955	0.0001
171	89.0000	0.1023	0.0001
172	90.1000	0.1069	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
GRAD

Gradiente térmico

[1; 1]GRAD

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.1090	0.0000
174	92.3000	0.1084	0.0000
175	93.4000	0.1047	-0.0001
176	94.5000	0.0977	-0.0001
177	95.6000	0.0869	-0.0001
178	96.7000	0.0721	-0.0002
179	97.8000	0.0529	-0.0002
180	98.9000	0.0290	-0.0002
181	100.0000	0.0000	-0.0003

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0014	0.0000
3	2.2000	0.0031	0.0000
4	3.3000	0.0047	0.0000
5	4.4000	0.0059	0.0000
6	5.5000	0.0074	0.0000
7	6.6000	0.0086	0.0000
8	7.7000	0.0098	0.0000
9	8.8000	0.0109	0.0000
10	9.9000	0.0117	0.0000
11	11.0000	0.0126	0.0000
12	12.1000	0.0134	0.0000
13	13.2000	0.0134	0.0000
14	14.3000	0.0134	0.0000
15	15.4000	0.0130	0.0000
16	16.5000	0.0120	0.0000
17	17.6000	0.0110	0.0000
18	18.7000	0.0091	0.0000
19	19.8000	0.0065	0.0000
20	20.9000	0.0037	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0048	0.0000
23	24.8000	0.0085	0.0000
24	26.2000	0.0118	0.0000
25	27.6000	0.0146	0.0000
26	29.0000	0.0167	0.0000
27	30.4000	0.0182	0.0000
28	31.8000	0.0194	0.0000
29	33.2000	0.0207	0.0000
30	34.6000	0.0217	0.0000
31	36.0000	0.0217	0.0000
32	37.4000	0.0221	0.0000
33	38.8000	0.0217	0.0000
34	40.2000	0.0210	0.0000
35	41.6000	0.0201	0.0000
36	43.0000	0.0183	0.0000
37	44.4000	0.0168	0.0000
38	45.8000	0.0136	0.0000
39	47.2000	0.0100	0.0000
40	48.6000	0.0053	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0053.	0.0000
43	52.8000	0.0100	0.0000
44	54.2000	0.0136	0.0000
45	55.6000	0.0168	0.0000
46	57.0000	0.0183	0.0000
47	58.4000	0.0201	0.0000
48	59.8000	0.0210	0.0000
49	61.2000	0.0217	0.0000
50	62.6000	0.0221	0.0000
51	64.0000	0.0217	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0217	0.0000
53	66.8000	0.0207	0.0000
54	68.2000	0.0194	0.0000
55	69.6000	0.0182	0.0000
56	71.0000	0.0167	0.0000
57	72.4000	0.0146	0.0000
58	73.8000	0.0118	0.0000
59	75.2000	0.0085	0.0000
60	76.6000	0.0048	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0037	0.0000
63	80.2000	0.0065	0.0000
64	81.3000	0.0091	0.0000
65	82.4000	0.0110	0.0000
66	83.5000	0.0120	0.0000
67	84.6000	0.0130	0.0000
68	85.7000	0.0134	0.0000
69	86.8000	0.0134	0.0000
70	87.9000	0.0134	0.0000
71	89.0000	0.0126	0.0000
72	90.1000	0.0117	0.0000
73	91.2000	0.0109	0.0000
74	92.3000	0.0098	0.0000
75	93.4000	0.0086	0.0000
76	94.5000	0.0074	0.0000
77	95.6000	0.0060	0.0000
78	96.7000	0.0047	0.0000
79	97.8000	0.0031	0.0000
80	98.9000	0.0014	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0010	0.0000
103	2.2000	0.0029	0.0000
104	3.3000	0.0045	0.0000
105	4.4000	0.0056	0.0000
106	5.5000	0.0063	0.0000
107	6.6000	0.0073	0.0000
108	7.7000	0.0076	0.0000
109	8.8000	0.0078	0.0000
110	9.9000	0.0078	0.0000
111	11.0000	0.0077	0.0000
112	12.1000	0.0076	0.0000
113	13.2000	0.0072	0.0000
114	14.3000	0.0068	0.0000
115	15.4000	0.0057	0.0000
116	16.5000	0.0044	0.0000
117	17.6000	0.0034	0.0000
118	18.7000	0.0021	0.0000
119	19.8000	0.0014	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0003	0.0000
123	24.8000	0.0022	0.0000
124	26.2000	0.0039	0.0000
125	27.6000	0.0047	0.0000
126	29.0000	0.0069	0.0000
127	30.4000	0.0077	0.0000
128	31.8000	0.0094	0.0000
129	33.2000	0.0104	0.0000
130	34.6000	0.0105	0.0000
131	36.0000	0.0111	0.0000
132	37.4000	0.0111	0.0000
133	38.8000	0.0104	0.0000
134	40.2000	0.0098	0.0000
135	41.6000	0.0087	0.0000
136	43.0000	0.0076	0.0000
137	44.4000	0.0061	0.0000
138	45.8000	0.0044	0.0000
139	47.2000	0.0028	0.0000
140	48.6000	0.0007	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0007	0.0000
143	52.8000	0.0028	0.0000
144	54.2000	0.0044	0.0000
145	55.6000	0.0061	0.0000
146	57.0000	0.0076	0.0000
147	58.4000	0.0087	0.0000
148	59.8000	0.0098	0.0000
149	61.2000	0.0104	0.0000
150	62.6000	0.0111	0.0000
151	64.0000	0.0111	0.0000
152	65.4000	0.0105	0.0000
153	66.8000	0.0104	0.0000
154	68.2000	0.0094	0.0000
155	69.6000	0.0077	0.0000
156	71.0000	0.0069	0.0000
157	72.4000	0.0047	0.0000
158	73.8000	0.0039	0.0000
159	75.2000	0.0022	0.0000
160	76.6000	0.0003	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0014	0.0000
164	81.3000	0.0021	0.0000
165	82.4000	0.0034	0.0000
166	83.5000	0.0044	0.0000
167	84.6000	0.0057	0.0000
168	85.7000	0.0068	0.0000
169	86.8000	0.0072	0.0000
170	87.9000	0.0076	0.0000
171	89.0000	0.0077	0.0000
172	90.1000	0.0078	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0078	0.0000
174	92.3000	0.0076	0.0000
175	93.4000	0.0073	0.0000
176	94.5000	0.0063	0.0000
177	95.6000	0.0056	0.0000
178	96.7000	0.0045	0.0000
179	97.8000	0.0029	0.0000
180	98.9000	0.0010	0.0000
181	100.0000	0.0000	0.0000

Programa DINTEL PACADAR S.A.
SCPAS1.ENV_TREN_GENERICO.GZ-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

Programa DINTEL PACADAR S.A.
SCPAS2.ENV_TREN_GENERICO.UY+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0010	0.0000
3	2.2000	0.0029	0.0000
4	3.3000	0.0045	0.0000
5	4.4000	0.0056	0.0000
6	5.5000	0.0063	0.0000
7	6.6000	0.0073	0.0000
8	7.7000	0.0076	0.0000
9	8.8000	0.0078	0.0000
10	9.9000	0.0078	0.0000
11	11.0000	0.0077	0.0000
12	12.1000	0.0075	0.0000
13	13.2000	0.0072	0.0000
14	14.3000	0.0068	0.0000
15	15.4000	0.0057	0.0000
16	16.5000	0.0044	0.0000
17	17.6000	0.0034	0.0000
18	18.7000	0.0021	0.0000
19	19.8000	0.0014	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0003	0.0000
23	24.8000	0.0022	0.0000
24	26.2000	0.0039	0.0000
25	27.6000	0.0047	0.0000
26	29.0000	0.0069	0.0000
27	30.4000	0.0077	0.0000
28	31.8000	0.0094	0.0000
29	33.2000	0.0104	0.0000
30	34.6000	0.0105	0.0000
31	36.0000	0.0111	0.0000
32	37.4000	0.0111	0.0000
33	38.8000	0.0104	0.0000
34	40.2000	0.0098	0.0000
35	41.6000	0.0087	0.0000
36	43.0000	0.0076	0.0000
37	44.4000	0.0061	0.0000
38	45.8000	0.0044	0.0000
39	47.2000	0.0028	0.0000
40	48.6000	0.0007	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0007	0.0000
43	52.8000	0.0028	0.0000
44	54.2000	0.0044	0.0000
45	55.6000	0.0061	0.0000
46	57.0000	0.0076	0.0000
47	58.4000	0.0087	0.0000
48	59.8000	0.0098	0.0000
49	61.2000	0.0104	0.0000
50	62.6000	0.0111	0.0000
51	64.0000	0.0111	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY+
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0105	0.0000
53	66.8000	0.0104	0.0000
54	68.2000	0.0094	0.0000
55	69.6000	0.0077	0.0000
56	71.0000	0.0069	0.0000
57	72.4000	0.0047	0.0000
58	73.8000	0.0039	0.0000
59	75.2000	0.0022	0.0000
60	76.6000	0.0003	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0014	0.0000
64	81.3000	0.0021	0.0000
65	82.4000	0.0034	0.0000
66	83.5000	0.0044	0.0000
67	84.6000	0.0057	0.0000
68	85.7000	0.0068	0.0000
69	86.8000	0.0072	0.0000
70	87.9000	0.0075	0.0000
71	89.0000	0.0077	0.0000
72	90.1000	0.0078	0.0000
73	91.2000	0.0078	0.0000
74	92.3000	0.0076	0.0000
75	93.4000	0.0073	0.0000
76	94.5000	0.0063	0.0000
77	95.6000	0.0056	0.0000
78	96.7000	0.0045	0.0000
79	97.8000	0.0029	0.0000
80	98.9000	0.0010	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0014	0.0000
103	2.2000	0.0031	0.0000
104	3.3000	0.0047	0.0000
105	4.4000	0.0060	0.0000
106	5.5000	0.0074	0.0000
107	6.6000	0.0086	0.0000
108	7.7000	0.0098	0.0000
109	8.8000	0.0109	0.0000
110	9.9000	0.0117	0.0000
111	11.0000	0.0126	0.0000
112	12.1000	0.0134	0.0000
113	13.2000	0.0134	0.0000
114	14.3000	0.0134	0.0000
115	15.4000	0.0130	0.0000
116	16.5000	0.0120	0.0000
117	17.6000	0.0110	0.0000
118	18.7000	0.0091	0.0000
119	19.8000	0.0065	0.0000
120	20.9000	0.0037	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY+
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0048	0.0000
123	24.8000	0.0085	0.0000
124	26.2000	0.0118	0.0000
125	27.6000	0.0146	0.0000
126	29.0000	0.0167	0.0000
127	30.4000	0.0182	0.0000
128	31.8000	0.0194	0.0000
129	33.2000	0.0207	0.0000
130	34.6000	0.0217	0.0000
131	36.0000	0.0217	0.0000
132	37.4000	0.0221	0.0000
133	38.8000	0.0217	0.0000
134	40.2000	0.0210	0.0000
135	41.6000	0.0201	0.0000
136	43.0000	0.0183	0.0000
137	44.4000	0.0168	0.0000
138	45.8000	0.0136	0.0000
139	47.2000	0.0100	0.0000
140	48.6000	0.0053	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0053	0.0000
143	52.8000	0.0100	0.0000
144	54.2000	0.0136	0.0000
145	55.6000	0.0168	0.0000
146	57.0000	0.0183	0.0000
147	58.4000	0.0201	0.0000
148	59.8000	0.0210	0.0000
149	61.2000	0.0217	0.0000
150	62.6000	0.0221	0.0000
151	64.0000	0.0217	0.0000
152	65.4000	0.0217	0.0000
153	66.8000	0.0207	0.0000
154	68.2000	0.0194	0.0000
155	69.6000	0.0182	0.0000
156	71.0000	0.0167	0.0000
157	72.4000	0.0146	0.0000
158	73.8000	0.0118	0.0000
159	75.2000	0.0085	0.0000
160	76.6000	0.0048	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0037	0.0000
163	80.2000	0.0065	0.0000
164	81.3000	0.0091	0.0000
165	82.4000	0.0110	0.0000
166	83.5000	0.0120	0.0000
167	84.6000	0.0130	0.0000
168	85.7000	0.0134	0.0000
169	86.8000	0.0134	0.0000
170	87.9000	0.0134	0.0000
171	89.0000	0.0126	0.0000
172	90.1000	0.0117	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0109	0.0000
174	92.3000	0.0098	0.0000
175	93.4000	0.0086	0.0000
176	94.5000	0.0074	0.0000
177	95.6000	0.0060	0.0000
178	96.7000	0.0047	0.0000
179	97.8000	0.0031	0.0000
180	98.9000	0.0014	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

SCPAS2.ENV_TREN_GENERICO.GZ+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

SCPAS2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

SCPAS2.ENV_TREN_GENERICO.UY-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

SCPAS2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	-0.0005	0.0000
5	4.4000	-0.0010	0.0000
6	5.5000	-0.0012	0.0000
7	6.6000	-0.0013	0.0000
8	7.7000	-0.0015	0.0000
9	8.8000	-0.0015	0.0000
10	9.9000	-0.0015	0.0000
11	11.0000	-0.0015	0.0000
12	12.1000	-0.0015	0.0000
13	13.2000	-0.0015	0.0000
14	14.3000	-0.0015	0.0000
15	15.4000	-0.0015	0.0000
16	16.5000	-0.0015	0.0000
17	17.6000	-0.0014	0.0000
18	18.7000	-0.0012	0.0000
19	19.8000	-0.0009	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	-0.0009	0.0000
24	26.2000	-0.0011	0.0000
25	27.6000	-0.0011	0.0000
26	29.0000	-0.0023	0.0000
27	30.4000	-0.0026	0.0000
28	31.8000	-0.0029	0.0000
29	33.2000	-0.0030	0.0000
30	34.6000	-0.0032	0.0000
31	36.0000	-0.0033	0.0000
32	37.4000	-0.0034	0.0000
33	38.8000	-0.0034	0.0000
34	40.2000	-0.0034	0.0000
35	41.6000	-0.0033	0.0000
36	43.0000	-0.0031	0.0000
37	44.4000	-0.0026	0.0000
38	45.8000	-0.0023	0.0000
39	47.2000	-0.0016	0.0000
40	48.6000	-0.0002	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0002	0.0000
43	52.8000	-0.0016	0.0000
44	54.2000	-0.0023	0.0000
45	55.6000	-0.0026	0.0000
46	57.0000	-0.0031	0.0000
47	58.4000	-0.0033	0.0000
48	59.8000	-0.0034	0.0000
49	61.2000	-0.0034	0.0000
50	62.6000	-0.0034	0.0000
51	64.0000	-0.0033	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY-
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0032	0.0000
53	66.8000	-0.0030	0.0000
54	68.2000	-0.0029	0.0000
55	69.6000	-0.0026	0.0000
56	71.0000	-0.0023	0.0000
57	72.4000	-0.0011	0.0000
58	73.8000	-0.0011	0.0000
59	75.2000	-0.0009	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	-0.0009	0.0000
64	81.3000	-0.0012	0.0000
65	82.4000	-0.0014	0.0000
66	83.5000	-0.0015	0.0000
67	84.6000	-0.0015	0.0000
68	85.7000	-0.0015	0.0000
69	86.8000	-0.0015	0.0000
70	87.9000	-0.0015	0.0000
71	89.0000	-0.0015	0.0000
72	90.1000	-0.0015	0.0000
73	91.2000	-0.0015	0.0000
74	92.3000	-0.0015	0.0000
75	93.4000	-0.0013	0.0000
76	94.5000	-0.0012	0.0000
77	95.6000	-0.0010	0.0000
78	96.7000	-0.0005	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0055	0.0000
103	2.2000	-0.0116	0.0000
104	3.3000	-0.0171	0.0000
105	4.4000	-0.0220	0.0000
106	5.5000	-0.0258	0.0000
107	6.6000	-0.0295	0.0000
108	7.7000	-0.0321	0.0000
109	8.8000	-0.0339	0.0000
110	9.9000	-0.0348	0.0000
111	11.0000	-0.0346	0.0000
112	12.1000	-0.0335	0.0000
113	13.2000	-0.0320	0.0000
114	14.3000	-0.0292	0.0000
115	15.4000	-0.0262	0.0000
116	16.5000	-0.0227	0.0000
117	17.6000	-0.0183	0.0000
118	18.7000	-0.0134	0.0000
119	19.8000	-0.0089	0.0000
120	20.9000	-0.0042	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY-
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0060	0.0000
123	24.8000	-0.0126	0.0000
124	26.2000	-0.0195	0.0000
125	27.6000	-0.0273	0.0000
126	29.0000	-0.0340	0.0000
127	30.4000	-0.0397	0.0000
128	31.8000	-0.0445	0.0000
129	33.2000	-0.0479	0.0000
130	34.6000	-0.0502	0.0000
131	36.0000	-0.0515	0.0000
132	37.4000	-0.0510	0.0000
133	38.8000	-0.0489	0.0000
134	40.2000	-0.0456	0.0000
135	41.6000	-0.0412	0.0000
136	43.0000	-0.0353	0.0000
137	44.4000	-0.0283	0.0000
138	45.8000	-0.0213	0.0000
139	47.2000	-0.0143	0.0000
140	48.6000	-0.0061	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0061	0.0000
143	52.8000	-0.0143	0.0000
144	54.2000	-0.0213	0.0000
145	55.6000	-0.0283	0.0000
146	57.0000	-0.0353	0.0000
147	58.4000	-0.0412	0.0000
148	59.8000	-0.0456	0.0000
149	61.2000	-0.0489	0.0000
150	62.6000	-0.0510	0.0000
151	64.0000	-0.0515	0.0000
152	65.4000	-0.0502	0.0000
153	66.8000	-0.0479	0.0000
154	68.2000	-0.0445	0.0000
155	69.6000	-0.0397	0.0000
156	71.0000	-0.0340	0.0000
157	72.4000	-0.0273	0.0000
158	73.8000	-0.0195	0.0000
159	75.2000	-0.0126	0.0000
160	76.6000	-0.0060	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0042	0.0000
163	80.2000	-0.0089	0.0000
164	81.3000	-0.0134	0.0000
165	82.4000	-0.0183	0.0000
166	83.5000	-0.0227	0.0000
167	84.6000	-0.0262	0.0000
168	85.7000	-0.0292	0.0000
169	86.8000	-0.0320	0.0000
170	87.9000	-0.0335	0.0000
171	89.0000	-0.0346	0.0000
172	90.1000	-0.0348	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0339	0.0000
174	92.3000	-0.0321	0.0000
175	93.4000	-0.0295	0.0000
176	94.5000	-0.0258	0.0000
177	95.6000	-0.0220	0.0000
178	96.7000	-0.0171	0.0000
179	97.8000	-0.0116	0.0000
180	98.9000	-0.0055	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS2.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA1

Carga uniforme tren A eje 1

[1; 1]CUNIA1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0033	0.0000
3	2.2000	-0.0064	0.0000
4	3.3000	-0.0093	0.0000
5	4.4000	-0.0118	0.0000
6	5.5000	-0.0138	0.0000
7	6.6000	-0.0153	0.0000
8	7.7000	-0.0163	0.0000
9	8.8000	-0.0168	0.0000
10	9.9000	-0.0167	0.0000
11	11.0000	-0.0161	0.0000
12	12.1000	-0.0150	0.0000
13	13.2000	-0.0135	0.0000
14	14.3000	-0.0116	0.0000
15	15.4000	-0.0095	0.0000
16	16.5000	-0.0073	0.0000
17	17.6000	-0.0051	0.0000
18	18.7000	-0.0030	0.0000
19	19.8000	-0.0014	0.0000
20	20.9000	-0.0003	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0011	0.0000
23	24.8000	-0.0033	0.0000
24	26.2000	-0.0063	0.0000
25	27.6000	-0.0097	0.0000
26	29.0000	-0.0131	0.0000
27	30.4000	-0.0163	0.0000
28	31.8000	-0.0189	0.0000
29	33.2000	-0.0209	0.0000
30	34.6000	-0.0221	0.0000
31	36.0000	-0.0225	0.0000
32	37.4000	-0.0220	0.0000
33	38.8000	-0.0206	0.0000
34	40.2000	-0.0185	0.0000
35	41.6000	-0.0158	0.0000
36	43.0000	-0.0126	0.0000
37	44.4000	-0.0092	0.0000
38	45.8000	-0.0059	0.0000
39	47.2000	-0.0029	0.0000
40	48.6000	-0.0008	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0008	0.0000
43	52.8000	-0.0029	0.0000
44	54.2000	-0.0059	0.0000
45	55.6000	-0.0092	0.0000
46	57.0000	-0.0126	0.0000
47	58.4000	-0.0158	0.0000
48	59.8000	-0.0185	0.0000
49	61.2000	-0.0206	0.0000
50	62.6000	-0.0220	0.0000
51	64.0000	-0.0225	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA1

Carga uniforme tren A eje 1

[1; 1]CUNIA1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0221	0.0000
53	66.8000	-0.0209	0.0000
54	68.2000	-0.0189	0.0000
55	69.6000	-0.0163	0.0000
56	71.0000	-0.0131	0.0000
57	72.4000	-0.0097	0.0000
58	73.8000	-0.0063	0.0000
59	75.2000	-0.0033	0.0000
60	76.6000	-0.0011	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0003	0.0000
63	80.2000	-0.0014	0.0000
64	81.3000	-0.0030	0.0000
65	82.4000	-0.0051	0.0000
66	83.5000	-0.0073	0.0000
67	84.6000	-0.0095	0.0000
68	85.7000	-0.0116	0.0000
69	86.8000	-0.0135	0.0000
70	87.9000	-0.0150	0.0000
71	89.0000	-0.0161	0.0000
72	90.1000	-0.0167	0.0000
73	91.2000	-0.0168	0.0000
74	92.3000	-0.0163	0.0000
75	93.4000	-0.0153	0.0000
76	94.5000	-0.0138	0.0000
77	95.6000	-0.0118	0.0000
78	96.7000	-0.0093	0.0000
79	97.8000	-0.0064	0.0000
80	98.9000	-0.0033	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0007	0.0000
103	2.2000	-0.0013	0.0000
104	3.3000	-0.0019	0.0000
105	4.4000	-0.0024	0.0000
106	5.5000	-0.0028	0.0000
107	6.6000	-0.0031	0.0000
108	7.7000	-0.0033	0.0000
109	8.8000	-0.0034	0.0000
110	9.9000	-0.0034	0.0000
111	11.0000	-0.0032	0.0000
112	12.1000	-0.0030	0.0000
113	13.2000	-0.0026	0.0000
114	14.3000	-0.0022	0.0000
115	15.4000	-0.0018	0.0000
116	16.5000	-0.0013	0.0000
117	17.6000	-0.0009	0.0000
118	18.7000	-0.0005	0.0000
119	19.8000	-0.0002	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA1

Carga uniforme tren A eje 1

[1; 1]CUNIA1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0003	0.0000
123	24.8000	-0.0009	0.0000
124	26.2000	-0.0016	0.0000
125	27.6000	-0.0024	0.0000
126	29.0000	-0.0033	0.0000
127	30.4000	-0.0040	0.0000
128	31.8000	-0.0047	0.0000
129	33.2000	-0.0051	0.0000
130	34.6000	-0.0054	0.0000
131	36.0000	-0.0055	0.0000
132	37.4000	-0.0054	0.0000
133	38.8000	-0.0050	0.0000
134	40.2000	-0.0045	0.0000
135	41.6000	-0.0038	0.0000
136	43.0000	-0.0030	0.0000
137	44.4000	-0.0021	0.0000
138	45.8000	-0.0013	0.0000
139	47.2000	-0.0007	0.0000
140	48.6000	-0.0002	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0002	0.0000
143	52.8000	-0.0007	0.0000
144	54.2000	-0.0013	0.0000
145	55.6000	-0.0021	0.0000
146	57.0000	-0.0030	0.0000
147	58.4000	-0.0038	0.0000
148	59.8000	-0.0045	0.0000
149	61.2000	-0.0050	0.0000
150	62.6000	-0.0054	0.0000
151	64.0000	-0.0055	0.0000
152	65.4000	-0.0054	0.0000
153	66.8000	-0.0051	0.0000
154	68.2000	-0.0047	0.0000
155	69.6000	-0.0040	0.0000
156	71.0000	-0.0033	0.0000
157	72.4000	-0.0024	0.0000
158	73.8000	-0.0016	0.0000
159	75.2000	-0.0009	0.0000
160	76.6000	-0.0003	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	-0.0002	0.0000
164	81.3000	-0.0005	0.0000
165	82.4000	-0.0009	0.0000
166	83.5000	-0.0013	0.0000
167	84.6000	-0.0018	0.0000
168	85.7000	-0.0022	0.0000
169	86.8000	-0.0026	0.0000
170	87.9000	-0.0030	0.0000
171	89.0000	-0.0032	0.0000
172	90.1000	-0.0034	0.0000

CUNIA1

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CUNIA1

Carga uniforme tren A eje 1

[1; 1]CUNIA1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0034	0.0000
174	92.3000	-0.0033	0.0000
175	93.4000	-0.0031	0.0000
176	94.5000	-0.0028	0.0000
177	95.6000	-0.0024	0.0000
178	96.7000	-0.0019	0.0000
179	97.8000	-0.0013	0.0000
180	98.9000	-0.0007	0.0000
181	100.0000	0.0000	0.0000

CUNIA2

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

CUNIA2

Carga uniforme tran A eje 2

[1; 1]CUNIA2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0006	0.0000
3	2.2000	-0.0011	0.0000
4	3.3000	-0.0016	0.0000
5	4.4000	-0.0021	0.0000
6	5.5000	-0.0024	0.0000
7	6.6000	-0.0027	0.0000
8	7.7000	-0.0029	0.0000
9	8.8000	-0.0029	0.0000
10	9.9000	-0.0029	0.0000
11	11.0000	-0.0028	0.0000
12	12.1000	-0.0025	0.0000
13	13.2000	-0.0022	0.0000
14	14.3000	-0.0019	0.0000
15	15.4000	-0.0015	0.0000
16	16.5000	-0.0011	0.0000
17	17.6000	-0.0007	0.0000
18	18.7000	-0.0004	0.0000
19	19.8000	-0.0001	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0003	0.0000
23	24.8000	-0.0008	0.0000
24	26.2000	-0.0015	0.0000
25	27.6000	-0.0022	0.0000
26	29.0000	-0.0030	0.0000
27	30.4000	-0.0037	0.0000
28	31.8000	-0.0042	0.0000
29	33.2000	-0.0047	0.0000
30	34.6000	-0.0049	0.0000
31	36.0000	-0.0050	0.0000
32	37.4000	-0.0049	0.0000
33	38.8000	-0.0045	0.0000
34	40.2000	-0.0040	0.0000
35	41.6000	-0.0034	0.0000
36	43.0000	-0.0027	0.0000
37	44.4000	-0.0019	0.0000
38	45.8000	-0.0012	0.0000
39	47.2000	-0.0006	0.0000
40	48.6000	-0.0002	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0002	0.0000
43	52.8000	-0.0006	0.0000
44	54.2000	-0.0012	0.0000
45	55.6000	-0.0019	0.0000
46	57.0000	-0.0027	0.0000
47	58.4000	-0.0034	0.0000
48	59.8000	-0.0040	0.0000
49	61.2000	-0.0045	0.0000
50	62.6000	-0.0049	0.0000
51	64.0000	-0.0050	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA2

Carga uniforme tran A eje 2

[1; 1]CUNIA2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0049	0.0000
53	66.8000	-0.0047	0.0000
54	68.2000	-0.0042	0.0000
55	69.6000	-0.0037	0.0000
56	71.0000	-0.0030	0.0000
57	72.4000	-0.0022	0.0000
58	73.8000	-0.0015	0.0000
59	75.2000	-0.0008	0.0000
60	76.6000	-0.0003	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	-0.0001	0.0000
64	81.3000	-0.0004	0.0000
65	82.4000	-0.0007	0.0000
66	83.5000	-0.0011	0.0000
67	84.6000	-0.0015	0.0000
68	85.7000	-0.0019	0.0000
69	86.8000	-0.0022	0.0000
70	87.9000	-0.0025	0.0000
71	89.0000	-0.0028	0.0000
72	90.1000	-0.0029	0.0000
73	91.2000	-0.0029	0.0000
74	92.3000	-0.0029	0.0000
75	93.4000	-0.0027	0.0000
76	94.5000	-0.0024	0.0000
77	95.6000	-0.0021	0.0000
78	96.7000	-0.0016	0.0000
79	97.8000	-0.0011	0.0000
80	98.9000	-0.0006	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0037	0.0000
103	2.2000	-0.0072	0.0000
104	3.3000	-0.0104	0.0000
105	4.4000	-0.0131	0.0000
106	5.5000	-0.0154	0.0000
107	6.6000	-0.0171	0.0000
108	7.7000	-0.0182	0.0000
109	8.8000	-0.0187	0.0000
110	9.9000	-0.0186	0.0000
111	11.0000	-0.0180	0.0000
112	12.1000	-0.0167	0.0000
113	13.2000	-0.0151	0.0000
114	14.3000	-0.0130	0.0000
115	15.4000	-0.0106	0.0000
116	16.5000	-0.0081	0.0000
117	17.6000	-0.0057	0.0000
118	18.7000	-0.0034	0.0000
119	19.8000	-0.0015	0.0000
120	20.9000	-0.0003	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA2

Carga uniforme tran A eje 2

[1; 1]CUNIA2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0012	0.0000
123	24.8000	-0.0037	0.0000
124	26.2000	-0.0071	0.0000
125	27.6000	-0.0109	0.0000
126	29.0000	-0.0146	0.0000
127	30.4000	-0.0181	0.0000
128	31.8000	-0.0211	0.0000
129	33.2000	-0.0233	0.0000
130	34.6000	-0.0246	0.0000
131	36.0000	-0.0251	0.0000
132	37.4000	-0.0245	0.0000
133	38.8000	-0.0230	0.0000
134	40.2000	-0.0207	0.0000
135	41.6000	-0.0176	0.0000
136	43.0000	-0.0141	0.0000
137	44.4000	-0.0103	0.0000
138	45.8000	-0.0065	0.0000
139	47.2000	-0.0033	0.0000
140	48.6000	-0.0009	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0009	0.0000
143	52.8000	-0.0033	0.0000
144	54.2000	-0.0065	0.0000
145	55.6000	-0.0103	0.0000
146	57.0000	-0.0141	0.0000
147	58.4000	-0.0176	0.0000
148	59.8000	-0.0207	0.0000
149	61.2000	-0.0230	0.0000
150	62.6000	-0.0245	0.0000
151	64.0000	-0.0251	0.0000
152	65.4000	-0.0246	0.0000
153	66.8000	-0.0233	0.0000
154	68.2000	-0.0211	0.0000
155	69.6000	-0.0181	0.0000
156	71.0000	-0.0146	0.0000
157	72.4000	-0.0109	0.0000
158	73.8000	-0.0071	0.0000
159	75.2000	-0.0037	0.0000
160	76.6000	-0.0012	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0003	0.0000
163	80.2000	-0.0015	0.0000
164	81.3000	-0.0034	0.0000
165	82.4000	-0.0057	0.0000
166	83.5000	-0.0081	0.0000
167	84.6000	-0.0106	0.0000
168	85.7000	-0.0130	0.0000
169	86.8000	-0.0151	0.0000
170	87.9000	-0.0167	0.0000
171	89.0000	-0.0180	0.0000
172	90.1000	-0.0186	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
CUNIA2

Carga uniforme tran A eje 2

[1; 1]CUNIA2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0187	0.0000
174	92.3000	-0.0182	0.0000
175	93.4000	-0.0171	0.0000
176	94.5000	-0.0154	0.0000
177	95.6000	-0.0131	0.0000
178	96.7000	-0.0104	0.0000
179	97.8000	-0.0072	0.0000
180	98.9000	-0.0037	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0192	0.0002
3	2.2000	0.0385	0.0002
4	3.3000	0.0570	0.0002
5	4.4000	0.0746	0.0001
6	5.5000	0.0909	0.0001
7	6.6000	0.1063	0.0001
8	7.7000	0.1191	0.0001
9	8.8000	0.1308	0.0001
10	9.9000	0.1404	0.0001
11	11.0000	0.1467	0.0000
12	12.1000	0.1503	0.0000
13	13.2000	0.1513	0.0000
14	14.3000	0.1487	0.0000
15	15.4000	0.1424	-0.0001
16	16.5000	0.1312	-0.0001
17	17.6000	0.1159	-0.0001
18	18.7000	0.0953	-0.0002
19	19.8000	0.0698	-0.0003
20	20.9000	0.0382	-0.0003
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0475	0.0003
23	24.8000	0.0896	0.0003
24	26.2000	0.1271	0.0003
25	27.6000	0.1600	0.0002
26	29.0000	0.1880	0.0001
27	30.4000	0.2109	0.0001
28	31.8000	0.2296	0.0001
29	33.2000	0.2442	0.0001
30	34.6000	0.2537	0.0001
31	36.0000	0.2589	0.0001
32	37.4000	0.2587	0.0000
33	38.8000	0.2535	-0.0001
34	40.2000	0.2437	-0.0001
35	41.6000	0.2282	-0.0001
36	43.0000	0.2068	-0.0002
37	44.4000	0.1793	-0.0002
38	45.8000	0.1452	-0.0003
39	47.2000	0.1046	-0.0003
40	48.6000	0.0558	-0.0003
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0558	0.0003
43	52.8000	0.1046	0.0003
44	54.2000	0.1452	0.0003
45	55.6000	0.1793	0.0002
46	57.0000	0.2068	0.0002
47	58.4000	0.2282	0.0001
48	59.8000	0.2437	0.0001
49	61.2000	0.2536	0.0001
50	62.6000	0.2587	0.0000
51	64.0000	0.2589	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY+
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.2537	-0.0001
53	66.8000	0.2442	-0.0001
54	68.2000	0.2296	-0.0001
55	69.6000	0.2109	-0.0001
56	71.0000	0.1880	-0.0001
57	72.4000	0.1600	-0.0002
58	73.8000	0.1271	-0.0003
59	75.2000	0.0896	-0.0003
60	76.6000	0.0475	-0.0003
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0382	0.0003
63	80.2000	0.0698	0.0003
64	81.3000	0.0953	0.0002
65	82.4000	0.1159	0.0001
66	83.5000	0.1312	0.0001
67	84.6000	0.1424	0.0001
68	85.7000	0.1487	0.0000
69	86.8000	0.1513	0.0000
70	87.9000	0.1503	0.0000
71	89.0000	0.1467	0.0000
72	90.1000	0.1404	-0.0001
73	91.2000	0.1308	-0.0001
74	92.3000	0.1192	-0.0001
75	93.4000	0.1064	-0.0001
76	94.5000	0.0909	-0.0001
77	95.6000	0.0746	-0.0001
78	96.7000	0.0570	-0.0002
79	97.8000	0.0385	-0.0002
80	98.9000	0.0192	-0.0002
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0074	0.0001
103	2.2000	0.0163	0.0001
104	3.3000	0.0238	0.0000
105	4.4000	0.0314	0.0000
106	5.5000	0.0379	0.0000
107	6.6000	0.0440	0.0000
108	7.7000	0.0497	0.0000
109	8.8000	0.0541	0.0000
110	9.9000	0.0575	0.0000
111	11.0000	0.0595	0.0000
112	12.1000	0.0608	0.0000
113	13.2000	0.0604	0.0000
114	14.3000	0.0587	0.0000
115	15.4000	0.0553	0.0000
116	16.5000	0.0503	0.0000
117	17.6000	0.0441	0.0000
118	18.7000	0.0355	-0.0001
119	19.8000	0.0253	-0.0001
120	20.9000	0.0139	-0.0001
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY+
Envolvente de tren de cargas plano genérico. UY
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0170	0.0000
123	24.8000	0.0337	0.0000
124	26.2000	0.0490	0.0000
125	27.6000	0.0637	0.0000
126	29.0000	0.0769	0.0000
127	30.4000	0.0884	0.0000
128	31.8000	0.0979	0.0000
129	33.2000	0.1052	0.0000
130	34.6000	0.1106	0.0000
131	36.0000	0.1128	0.0000
132	37.4000	0.1132	0.0000
133	38.8000	0.1106	0.0000
134	40.2000	0.1053	0.0000
135	41.6000	0.0978	0.0000
136	43.0000	0.0877	0.0000
137	44.4000	0.0747	0.0000
138	45.8000	0.0592	-0.0001
139	47.2000	0.0418	-0.0001
140	48.6000	0.0220	-0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0220	0.0001
143	52.8000	0.0418	0.0001
144	54.2000	0.0592	0.0001
145	55.6000	0.0747	0.0000
146	57.0000	0.0877	0.0000
147	58.4000	0.0978	0.0000
148	59.8000	0.1053	0.0000
149	61.2000	0.1106	0.0000
150	62.6000	0.1132	0.0000
151	64.0000	0.1128	0.0000
152	65.4000	0.1106	0.0000
153	66.8000	0.1052	0.0000
154	68.2000	0.0979	0.0000
155	69.6000	0.0884	0.0000
156	71.0000	0.0769	0.0000
157	72.4000	0.0637	0.0000
158	73.8000	0.0490	0.0000
159	75.2000	0.0337	0.0000
160	76.6000	0.0170	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0139	0.0001
163	80.2000	0.0253	0.0001
164	81.3000	0.0355	0.0001
165	82.4000	0.0441	0.0000
166	83.5000	0.0503	0.0000
167	84.6000	0.0553	0.0000
168	85.7000	0.0587	0.0000
169	86.8000	0.0604	0.0000
170	87.9000	0.0608	0.0000
171	89.0000	0.0595	0.0000
172	90.1000	0.0575	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0541	0.0000
174	92.3000	0.0497	0.0000
175	93.4000	0.0440	0.0000
176	94.5000	0.0379	0.0000
177	95.6000	0.0314	0.0000
178	96.7000	0.0238	0.0000
179	97.8000	0.0163	-0.0001
180	98.9000	0.0074	-0.0001
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0002
2	1.1000	0.0174	0.0002
3	2.2000	0.0345	0.0002
4	3.3000	0.0511	0.0002
5	4.4000	0.0647	0.0001
6	5.5000	0.0789	0.0001
7	6.6000	0.0841	0.0001
8	7.7000	0.0945	0.0001
9	8.8000	0.0907	0.0001
10	9.9000	0.0630	0.0001
11	11.0000	-0.1023	0.0001
12	12.1000	-0.1459	0.0001
13	13.2000	-0.1902	0.0001
14	14.3000	-0.1870	0.0002
15	15.4000	-0.1846	0.0002
16	16.5000	-0.1626	0.0003
17	17.6000	-0.1312	0.0003
18	18.7000	-0.1003	0.0003
19	19.8000	-0.0654	0.0003
20	20.9000	-0.0346	0.0003
21	22.0000	0.0000	0.0004
1021	22.0000	0.0000	0.0004
22	23.4000	0.0430	0.0003
23	24.8000	0.0818	0.0003
24	26.2000	0.1102	0.0003
25	27.6000	0.1246	0.0002
26	29.0000	0.0620	0.0001
27	30.4000	0.0756	0.0001
28	31.8000	0.0887	0.0001
29	33.2000	0.0951	0.0001
30	34.6000	0.0419	0.0001
31	36.0000	-0.1043	0.0001
32	37.4000	-0.2374	0.0001
33	38.8000	-0.2895	0.0002
34	40.2000	-0.3197	0.0002
35	41.6000	-0.3206	0.0003
36	43.0000	-0.2848	0.0004
37	44.4000	-0.2360	0.0004
38	45.8000	-0.1762	0.0004
39	47.2000	-0.1146	0.0005
40	48.6000	-0.0546	0.0004
41	50.0000	0.0000	0.0004
1041	50.0000	0.0000	0.0004
42	51.4000	0.0488	0.0003
43	52.8000	0.0925	0.0003
44	54.2000	0.1280	0.0003
45	55.6000	0.1476	0.0002
46	57.0000	0.1395	0.0002
47	58.4000	0.0485	0.0001
48	59.8000	0.0521	0.0001
49	61.2000	0.0475	0.0001
50	62.6000	-0.0499	0.0001
51	64.0000	-0.1740	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.2380	0.0001
53	66.8000	-0.2896	0.0002
54	68.2000	-0.3188	0.0003
55	69.6000	-0.3193	0.0003
56	71.0000	-0.2827	0.0004
57	72.4000	-0.2282	0.0004
58	73.8000	-0.1742	0.0004
59	75.2000	-0.1128	0.0005
60	76.6000	-0.0535	0.0004
61	78.0000	0.0000	0.0004
1061	78.0000	0.0000	0.0004
62	79.1000	0.0353	0.0003
63	80.2000	0.0645	0.0003
64	81.3000	0.0860	0.0002
65	82.4000	0.1008	0.0001
66	83.5000	0.1044	0.0001
67	84.6000	0.0827	0.0001
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	-0.0809	0.0001
73	91.2000	-0.1483	0.0001
74	92.3000	-0.1940	0.0001
75	93.4000	-0.2063	0.0002
76	94.5000	-0.1893	0.0003
77	95.6000	-0.1588	0.0003
78	96.7000	-0.1267	0.0004
79	97.8000	-0.0869	0.0004
80	98.9000	-0.0444	0.0004
81	100.0000	0.0000	0.0004
101	0.0000	0.0000	0.0001
102	1.1000	0.0036	0.0001
103	2.2000	0.0072	0.0001
104	3.3000	0.0073	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	-0.0064	0.0000
117	17.6000	-0.0175	0.0001
118	18.7000	-0.0149	0.0001
119	19.8000	-0.0099	0.0001
120	20.9000	-0.0048	0.0001
121	22.0000	0.0000	0.0001
1121	22.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0031	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	-0.0730	0.0001
135	41.6000	-0.0858	0.0001
136	43.0000	-0.0836	0.0001
137	44.4000	-0.0711	0.0001
138	45.8000	-0.0533	0.0001
139	47.2000	-0.0365	0.0002
140	48.6000	-0.0179	0.0002
141	50.0000	0.0000	0.0001
1141	50.0000	0.0000	0.0001
142	51.4000	0.0140	0.0001
143	52.8000	0.0248	0.0001
144	54.2000	0.0268	0.0001
145	55.6000	0.0174	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	-0.0809	0.0001
155	69.6000	-0.0844	0.0001
156	71.0000	-0.0811	0.0001
157	72.4000	-0.0688	0.0001
158	73.8000	-0.0516	0.0001
159	75.2000	-0.0337	0.0001
160	76.6000	-0.0160	0.0001
161	78.0000	0.0000	0.0001
1161	78.0000	0.0000	0.0001
162	79.1000	0.0097	0.0001
163	80.2000	0.0181	0.0001
164	81.3000	0.0196	0.0001
165	82.4000	0.0130	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.2380	0.0001
53	66.8000	-0.2896	0.0002
54	68.2000	-0.3188	0.0003
55	69.6000	-0.3193	0.0003
56	71.0000	-0.2827	0.0004
57	72.4000	-0.2282	0.0004
58	73.8000	-0.1742	0.0004
59	75.2000	-0.1128	0.0005
60	76.6000	-0.0535	0.0004
61	78.0000	0.0000	0.0004
1061	78.0000	0.0000	0.0004
62	79.1000	0.0353	0.0003
63	80.2000	0.0645	0.0003
64	81.3000	0.0860	0.0002
65	82.4000	0.1008	0.0001
66	83.5000	0.1044	0.0001
67	84.6000	0.0827	0.0001
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	-0.0809	0.0001
73	91.2000	-0.1483	0.0001
74	92.3000	-0.1940	0.0001
75	93.4000	-0.2063	0.0002
76	94.5000	-0.1893	0.0003
77	95.6000	-0.1588	0.0003
78	96.7000	-0.1267	0.0004
79	97.8000	-0.0869	0.0004
80	98.9000	-0.0444	0.0004
81	100.0000	0.0000	0.0004
101	0.0000	0.0000	0.0001
102	1.1000	0.0036	0.0001
103	2.2000	0.0072	0.0001
104	3.3000	0.0073	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	-0.0064	0.0000
117	17.6000	-0.0175	0.0001
118	18.7000	-0.0149	0.0001
119	19.8000	-0.0099	0.0001
120	20.9000	-0.0048	0.0001
121	22.0000	0.0000	0.0001
1121	22.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0031	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	-0.0730	0.0001
135	41.6000	-0.0858	0.0001
136	43.0000	-0.0836	0.0001
137	44.4000	-0.0711	0.0001
138	45.8000	-0.0533	0.0001
139	47.2000	-0.0365	0.0002
140	48.6000	-0.0179	0.0002
141	50.0000	0.0000	0.0001
1141	50.0000	0.0000	0.0001
142	51.4000	0.0140	0.0001
143	52.8000	0.0248	0.0001
144	54.2000	0.0268	0.0001
145	55.6000	0.0174	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	-0.0809	0.0001
155	69.6000	-0.0844	0.0001
156	71.0000	-0.0811	0.0001
157	72.4000	-0.0688	0.0001
158	73.8000	-0.0516	0.0001
159	75.2000	-0.0337	0.0001
160	76.6000	-0.0160	0.0001
161	78.0000	0.0000	0.0001
1161	78.0000	0.0000	0.0001
162	79.1000	0.0097	0.0001
163	80.2000	0.0181	0.0001
164	81.3000	0.0196	0.0001
165	82.4000	0.0130	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

SCUNIA1.ENV_TREN_GENERICO.GZ+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	-0.0197	0.0001
178	96.7000	-0.0208	0.0001
179	97.8000	-0.0144	0.0001
180	98.9000	-0.0084	0.0001
181	100.0000	0.0000	0.0001

SCUNIA1.ENV_TREN_GENERICO.UY-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0491	-0.0004
3	2.2000	-0.0961	-0.0004
4	3.3000	-0.1404	-0.0004
5	4.4000	-0.1802	-0.0003
6	5.5000	-0.2153	-0.0003
7	6.6000	-0.2440	-0.0002
8	7.7000	-0.2663	-0.0001
9	8.8000	-0.2820	-0.0001
10	9.9000	-0.2905	-0.0001
11	11.0000	-0.2918	0.0001
12	12.1000	-0.2850	0.0001
13	13.2000	-0.2724	0.0001
14	14.3000	-0.2529	0.0002
15	15.4000	-0.2275	0.0002
16	16.5000	-0.1967	0.0003
17	17.6000	-0.1611	0.0003
18	18.7000	-0.1226	0.0003
19	19.8000	-0.0817	0.0003
20	20.9000	-0.0402	0.0003
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0566	-0.0004
23	24.8000	-0.1192	-0.0005
24	26.2000	-0.1843	-0.0004
25	27.6000	-0.2473	-0.0004
26	29.0000	-0.3058	-0.0004
27	30.4000	-0.3576	-0.0003
28	31.8000	-0.4000	-0.0003
29	33.2000	-0.4323	-0.0002
30	34.6000	-0.4523	-0.0001
31	36.0000	-0.4608	0.0000
32	37.4000	-0.4559	0.0001
33	38.8000	-0.4391	0.0002
34	40.2000	-0.4108	0.0002
35	41.6000	-0.3705	0.0003
36	43.0000	-0.3206	0.0004
37	44.4000	-0.2624	0.0004
38	45.8000	-0.1982	0.0004
39	47.2000	-0.1309	0.0005
40	48.6000	-0.0637	0.0004
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0637	-0.0004
43	52.8000	-0.1309	-0.0005
44	54.2000	-0.1982	-0.0004
45	55.6000	-0.2624	-0.0004
46	57.0000	-0.3206	-0.0004
47	58.4000	-0.3705	-0.0003
48	59.8000	-0.4108	-0.0002
49	61.2000	-0.4391	-0.0002
50	62.6000	-0.4559	-0.0001
51	64.0000	-0.4608	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.4523	0.0001
53	66.8000	-0.4323	0.0002
54	68.2000	-0.4000	0.0003
55	69.6000	-0.3576	0.0003
56	71.0000	-0.3058	0.0004
57	72.4000	-0.2473	0.0004
58	73.8000	-0.1843	0.0004
59	75.2000	-0.1192	0.0005
60	76.6000	-0.0566	0.0004
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0402	-0.0003
63	80.2000	-0.0817	-0.0003
64	81.3000	-0.1226	-0.0003
65	82.4000	-0.1612	-0.0003
66	83.5000	-0.1967	-0.0003
67	84.6000	-0.2275	-0.0002
68	85.7000	-0.2529	-0.0002
69	86.8000	-0.2724	-0.0001
70	87.9000	-0.2850	-0.0001
71	89.0000	-0.2918	-0.0001
72	90.1000	-0.2905	0.0001
73	91.2000	-0.2820	0.0001
74	92.3000	-0.2663	0.0001
75	93.4000	-0.2441	0.0002
76	94.5000	-0.2153	0.0003
77	95.6000	-0.1802	0.0003
78	96.7000	-0.1404	0.0004
79	97.8000	-0.0961	0.0004
80	98.9000	-0.0492	0.0004
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0140	-0.0001
103	2.2000	-0.0280	-0.0001
104	3.3000	-0.0411	-0.0001
105	4.4000	-0.0531	-0.0001
106	5.5000	-0.0637	0.0000
107	6.6000	-0.0726	0.0000
108	7.7000	-0.0798	0.0000
109	8.8000	-0.0847	0.0000
110	9.9000	-0.0879	0.0000
111	11.0000	-0.0888	0.0000
112	12.1000	-0.0870	0.0000
113	13.2000	-0.0840	0.0000
114	14.3000	-0.0783	0.0000
115	15.4000	-0.0711	0.0000
116	16.5000	-0.0619	0.0000
117	17.6000	-0.0518	0.0001
118	18.7000	-0.0398	0.0001
119	19.8000	-0.0269	0.0001
120	20.9000	-0.0135	0.0001
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0196	-0.0001
123	24.8000	-0.0414	-0.0001
124	26.2000	-0.0639	-0.0001
125	27.6000	-0.0855	-0.0001
126	29.0000	-0.1063	-0.0001
127	30.4000	-0.1246	-0.0001
128	31.8000	-0.1399	-0.0001
129	33.2000	-0.1515	0.0000
130	34.6000	-0.1591	0.0000
131	36.0000	-0.1627	0.0000
132	37.4000	-0.1611	0.0000
133	38.8000	-0.1557	0.0000
134	40.2000	-0.1457	0.0001
135	41.6000	-0.1319	0.0001
136	43.0000	-0.1141	0.0001
137	44.4000	-0.0941	0.0001
138	45.8000	-0.0714	0.0001
139	47.2000	-0.0475	0.0002
140	48.6000	-0.0236	0.0002
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0236	-0.0002
143	52.8000	-0.0475	-0.0002
144	54.2000	-0.0714	-0.0001
145	55.6000	-0.0942	-0.0001
146	57.0000	-0.1141	-0.0001
147	58.4000	-0.1319	-0.0001
148	59.8000	-0.1457	-0.0001
149	61.2000	-0.1557	0.0000
150	62.6000	-0.1611	0.0000
151	64.0000	-0.1627	0.0000
152	65.4000	-0.1591	0.0000
153	66.8000	-0.1515	0.0000
154	68.2000	-0.1399	0.0001
155	69.6000	-0.1246	0.0001
156	71.0000	-0.1063	0.0001
157	72.4000	-0.0855	0.0001
158	73.8000	-0.0639	0.0001
159	75.2000	-0.0414	0.0001
160	76.6000	-0.0196	0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0135	-0.0001
163	80.2000	-0.0269	-0.0001
164	81.3000	-0.0398	-0.0001
165	82.4000	-0.0518	-0.0001
166	83.5000	-0.0619	0.0000
167	84.6000	-0.0711	0.0000
168	85.7000	-0.0783	0.0000
169	86.8000	-0.0840	0.0000
170	87.9000	-0.0870	0.0000
171	89.0000	-0.0888	0.0000
172	90.1000	-0.0879	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0847	0.0000
174	92.3000	-0.0798	0.0000
175	93.4000	-0.0727	0.0000
176	94.5000	-0.0637	0.0000
177	95.6000	-0.0531	0.0001
178	96.7000	-0.0411	0.0001
179	97.8000	-0.0280	0.0001
180	98.9000	-0.0140	0.0001
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0004
2	1.1000	-0.0443	-0.0004
3	2.2000	-0.0869	-0.0004
4	3.3000	-0.1267	-0.0004
5	4.4000	-0.1588	-0.0003
6	5.5000	-0.1893	-0.0003
7	6.6000	-0.2062	-0.0002
8	7.7000	-0.1940	-0.0001
9	8.8000	-0.1483	-0.0001
10	9.9000	-0.0809	-0.0001
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0827	-0.0001
16	16.5000	0.1044	-0.0001
17	17.6000	0.1008	-0.0001
18	18.7000	0.0860	-0.0002
19	19.8000	0.0645	-0.0003
20	20.9000	0.0353	-0.0003
21	22.0000	0.0000	-0.0004
1021	22.0000	0.0000	-0.0004
22	23.4000	-0.0535	-0.0004
23	24.8000	-0.1128	-0.0005
24	26.2000	-0.1742	-0.0004
25	27.6000	-0.2282	-0.0004
26	29.0000	-0.2827	-0.0004
27	30.4000	-0.3193	-0.0003
28	31.8000	-0.3188	-0.0003
29	33.2000	-0.2896	-0.0002
30	34.6000	-0.2380	-0.0001
31	36.0000	-0.1740	-0.0001
32	37.4000	-0.0499	-0.0001
33	38.8000	0.0474	-0.0001
34	40.2000	0.0521	-0.0001
35	41.6000	0.0485	-0.0001
36	43.0000	0.1395	-0.0002
37	44.4000	0.1476	-0.0002
38	45.8000	0.1280	-0.0003
39	47.2000	0.0925	-0.0003
40	48.6000	0.0488	-0.0003
41	50.0000	0.0000	-0.0004
1041	50.0000	0.0000	-0.0004
42	51.4000	-0.0546	-0.0004
43	52.8000	-0.1146	-0.0005
44	54.2000	-0.1762	-0.0004
45	55.6000	-0.2360	-0.0004
46	57.0000	-0.2848	-0.0004
47	58.4000	-0.3206	-0.0003
48	59.8000	-0.3197	-0.0002
49	61.2000	-0.2895	-0.0002
50	62.6000	-0.2374	-0.0001
51	64.0000	-0.1043	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0419	-0.0001
53	66.8000	0.0951	-0.0001
54	68.2000	0.0887	-0.0001
55	69.6000	0.0756	-0.0001
56	71.0000	0.0620	-0.0001
57	72.4000	0.1246	-0.0002
58	73.8000	0.1102	-0.0003
59	75.2000	0.0818	-0.0003
60	76.6000	0.0430	-0.0003
61	78.0000	0.0000	-0.0004
1061	78.0000	0.0000	-0.0004
62	79.1000	-0.0346	-0.0003
63	80.2000	-0.0654	-0.0003
64	81.3000	-0.1003	-0.0003
65	82.4000	-0.1313	-0.0003
66	83.5000	-0.1626	-0.0003
67	84.6000	-0.1846	-0.0002
68	85.7000	-0.1870	-0.0002
69	86.8000	-0.1902	-0.0001
70	87.9000	-0.1459	-0.0001
71	89.0000	-0.1023	-0.0001
72	90.1000	0.0630	-0.0001
73	91.2000	0.0907	-0.0001
74	92.3000	0.0946	-0.0001
75	93.4000	0.0842	-0.0001
76	94.5000	0.0789	-0.0001
77	95.6000	0.0647	-0.0001
78	96.7000	0.0511	-0.0002
79	97.8000	0.0345	-0.0002
80	98.9000	0.0174	-0.0002
81	100.0000	0.0000	-0.0002
101	0.0000	0.0000	-0.0001
102	1.1000	-0.0084	-0.0001
103	2.2000	-0.0144	-0.0001
104	3.3000	-0.0208	-0.0001
105	4.4000	-0.0197	-0.0001
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0130	0.0000
118	18.7000	0.0196	-0.0001
119	19.8000	0.0181	-0.0001
120	20.9000	0.0097	-0.0001
121	22.0000	0.0000	-0.0001
1121	22.0000	0.0000	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra1
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0160	-0.0001
123	24.8000	-0.0337	-0.0001
124	26.2000	-0.0516	-0.0001
125	27.6000	-0.0688	-0.0001
126	29.0000	-0.0811	-0.0001
127	30.4000	-0.0844	-0.0001
128	31.8000	-0.0809	-0.0001
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0174	0.0000
138	45.8000	0.0268	-0.0001
139	47.2000	0.0248	-0.0001
140	48.6000	0.0140	-0.0001
141	50.0000	0.0000	-0.0001
1141	50.0000	0.0000	-0.0001
142	51.4000	-0.0179	-0.0002
143	52.8000	-0.0365	-0.0002
144	54.2000	-0.0533	-0.0001
145	55.6000	-0.0712	-0.0001
146	57.0000	-0.0836	-0.0001
147	58.4000	-0.0858	-0.0001
148	59.8000	-0.0730	-0.0001
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0031	0.0000
161	78.0000	0.0000	-0.0001
1161	78.0000	0.0000	-0.0001
162	79.1000	-0.0048	-0.0001
163	80.2000	-0.0099	-0.0001
164	81.3000	-0.0149	-0.0001
165	82.4000	-0.0175	-0.0001
166	83.5000	-0.0064	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA1.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA1.SCuniTpos.Barra1.Mx+ + [0; 1]SCUNIA1.SCuniTpos.Barra2

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0073	0.0000
179	97.8000	0.0072	-0.0001
180	98.9000	0.0036	-0.0001
181	100.0000	0.0000	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0082	0.0001
3	2.2000	0.0173	0.0001
4	3.3000	0.0254	0.0001
5	4.4000	0.0339	0.0000
6	5.5000	0.0411	0.0000
7	6.6000	0.0475	0.0000
8	7.7000	0.0534	0.0000
9	8.8000	0.0580	0.0000
10	9.9000	0.0615	0.0000
11	11.0000	0.0638	0.0000
12	12.1000	0.0648	0.0000
13	13.2000	0.0644	0.0000
14	14.3000	0.0622	0.0000
15	15.4000	0.0586	0.0000
16	16.5000	0.0534	0.0000
17	17.6000	0.0463	-0.0001
18	18.7000	0.0372	-0.0001
19	19.8000	0.0268	-0.0001
20	20.9000	0.0142	-0.0001
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0179	0.0001
23	24.8000	0.0354	0.0000
24	26.2000	0.0521	0.0000
25	27.6000	0.0679	0.0000
26	29.0000	0.0819	0.0000
27	30.4000	0.0946	0.0000
28	31.8000	0.1049	0.0000
29	33.2000	0.1130	0.0000
30	34.6000	0.1186	0.0000
31	36.0000	0.1216	0.0000
32	37.4000	0.1216	0.0000
33	38.8000	0.1189	0.0000
34	40.2000	0.1136	0.0000
35	41.6000	0.1051	0.0000
36	43.0000	0.0938	0.0000
37	44.4000	0.0794	-0.0001
38	45.8000	0.0630	-0.0001
39	47.2000	0.0443	-0.0001
40	48.6000	0.0228	-0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0228	0.0001
43	52.8000	0.0443	0.0001
44	54.2000	0.0630	0.0001
45	55.6000	0.0794	0.0001
46	57.0000	0.0938	0.0000
47	58.4000	0.1051	0.0000
48	59.8000	0.1136	0.0000
49	61.2000	0.1189	0.0000
50	62.6000	0.1216	0.0000
51	64.0000	0.1216	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.1186	0.0000
53	66.8000	0.1130	0.0000
54	68.2000	0.1049	0.0000
55	69.6000	0.0947	0.0000
56	71.0000	0.0819	0.0000
57	72.4000	0.0679	0.0000
58	73.8000	0.0521	0.0000
59	75.2000	0.0354	0.0000
60	76.6000	0.0179	-0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0142	0.0001
63	80.2000	0.0268	0.0001
64	81.3000	0.0372	0.0001
65	82.4000	0.0463	0.0001
66	83.5000	0.0534	0.0000
67	84.6000	0.0586	0.0000
68	85.7000	0.0622	0.0000
69	86.8000	0.0644	0.0000
70	87.9000	0.0649	0.0000
71	89.0000	0.0639	0.0000
72	90.1000	0.0615	0.0000
73	91.2000	0.0580	0.0000
74	92.3000	0.0534	0.0000
75	93.4000	0.0475	0.0000
76	94.5000	0.0411	0.0000
77	95.6000	0.0339	0.0000
78	96.7000	0.0254	-0.0001
79	97.8000	0.0173	-0.0001
80	98.9000	0.0082	-0.0001
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0210	0.0002
103	2.2000	0.0410	0.0002
104	3.3000	0.0614	0.0002
105	4.4000	0.0798	0.0002
106	5.5000	0.0977	0.0001
107	6.6000	0.1139	0.0001
108	7.7000	0.1285	0.0001
109	8.8000	0.1407	0.0001
110	9.9000	0.1505	0.0001
111	11.0000	0.1578	0.0000
112	12.1000	0.1619	0.0000
113	13.2000	0.1628	0.0000
114	14.3000	0.1603	0.0000
115	15.4000	0.1532	-0.0001
116	16.5000	0.1420	-0.0001
117	17.6000	0.1249	-0.0002
118	18.7000	0.1033	-0.0002
119	19.8000	0.0755	-0.0003
120	20.9000	0.0409	-0.0003
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0510	0.0004
123	24.8000	0.0972	0.0003
124	26.2000	0.1373	0.0003
125	27.6000	0.1721	0.0002
126	29.0000	0.2019	0.0002
127	30.4000	0.2270	0.0001
128	31.8000	0.2466	0.0001
129	33.2000	0.2618	0.0001
130	34.6000	0.2723	0.0001
131	36.0000	0.2778	0.0001
132	37.4000	0.2775	-0.0001
133	38.8000	0.2725	-0.0001
134	40.2000	0.2618	-0.0001
135	41.6000	0.2453	-0.0001
136	43.0000	0.2231	-0.0002
137	44.4000	0.1933	-0.0003
138	45.8000	0.1570	-0.0003
139	47.2000	0.1127	-0.0003
140	48.6000	0.0607	-0.0004
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0607	0.0004
143	52.8000	0.1127	0.0003
144	54.2000	0.1570	0.0003
145	55.6000	0.1933	0.0003
146	57.0000	0.2230	0.0002
147	58.4000	0.2453	0.0001
148	59.8000	0.2618	0.0001
149	61.2000	0.2725	0.0001
150	62.6000	0.2775	0.0001
151	64.0000	0.2778	-0.0001
152	65.4000	0.2723	-0.0001
153	66.8000	0.2618	-0.0001
154	68.2000	0.2466	-0.0001
155	69.6000	0.2270	-0.0001
156	71.0000	0.2020	-0.0002
157	72.4000	0.1721	-0.0002
158	73.8000	0.1374	-0.0003
159	75.2000	0.0973	-0.0003
160	76.6000	0.0510	-0.0004
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0409	0.0003
163	80.2000	0.0755	0.0003
164	81.3000	0.1033	0.0002
165	82.4000	0.1249	0.0002
166	83.5000	0.1420	0.0001
167	84.6000	0.1532	0.0001
168	85.7000	0.1603	0.0000
169	86.8000	0.1628	0.0000
170	87.9000	0.1619	0.0000
171	89.0000	0.1578	0.0000
172	90.1000	0.1505	-0.0001

Programa DINTEL PACADAR S.A.
SCUNIA2.ENV_TREN_GENERICO.UY+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.1407	-0.0001
174	92.3000	0.1285	-0.0001
175	93.4000	0.1139	-0.0001
176	94.5000	0.0977	-0.0001
177	95.6000	0.0798	-0.0002
178	96.7000	0.0614	-0.0002
179	97.8000	0.0410	-0.0002
180	98.9000	0.0210	-0.0002
181	100.0000	0.0000	0.0000

Programa DINTEL PACADAR S.A.
SCUNIA2.ENV_TREN_GENERICO.GZ+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0001
2	1.1000	0.0046	0.0001
3	2.2000	0.0087	0.0001
4	3.3000	0.0114	0.0001
5	4.4000	0.0102	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	-0.0032	0.0000
17	17.6000	-0.0153	0.0001
18	18.7000	-0.0152	0.0001
19	19.8000	-0.0100	0.0001
20	20.9000	-0.0051	0.0001
21	22.0000	0.0000	0.0001
1021	22.0000	0.0000	0.0001
22	23.4000	0.0039	0.0001
23	24.8000	0.0013	0.0000
24	26.2000	0.0060	0.0000
25	27.6000	0.0107	0.0000
26	29.0000	0.0103	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	-0.0839	0.0001
35	41.6000	-0.0947	0.0001
36	43.0000	-0.0859	0.0001
37	44.4000	-0.0731	0.0001
38	45.8000	-0.0550	0.0001
39	47.2000	-0.0376	0.0002
40	48.6000	-0.0183	0.0002
41	50.0000	0.0000	0.0001
1041	50.0000	0.0000	0.0001
42	51.4000	0.0153	0.0001
43	52.8000	0.0260	0.0001
44	54.2000	0.0340	0.0001
45	55.6000	0.0270	0.0001
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	-0.0832	0.0001
55	69.6000	-0.0928	0.0001
56	71.0000	-0.0876	0.0001
57	72.4000	-0.0707	0.0001
58	73.8000	-0.0530	0.0001
59	75.2000	-0.0347	0.0001
60	76.6000	-0.0167	0.0001
61	78.0000	0.0000	0.0001
1061	78.0000	0.0000	0.0001
62	79.1000	0.0111	0.0001
63	80.2000	0.0189	0.0001
64	81.3000	0.0229	0.0001
65	82.4000	0.0198	0.0001
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	-0.0194	0.0001
78	96.7000	-0.0187	0.0001
79	97.8000	-0.0139	0.0001
80	98.9000	-0.0078	0.0001
81	100.0000	0.0000	0.0001
101	0.0000	0.0000	0.0002
102	1.1000	0.0188	0.0002
103	2.2000	0.0369	0.0002
104	3.3000	0.0549	0.0002
105	4.4000	0.0718	0.0002
106	5.5000	0.0848	0.0001
107	6.6000	0.0946	0.0001
108	7.7000	0.1016	0.0001
109	8.8000	0.1050	0.0001
110	9.9000	0.0778	0.0001
111	11.0000	-0.1122	0.0001
112	12.1000	-0.1825	0.0001
113	13.2000	-0.2085	0.0002
114	14.3000	-0.2180	0.0002
115	15.4000	-0.2020	0.0003
116	16.5000	-0.1779	0.0003
117	17.6000	-0.1435	0.0003
118	18.7000	-0.1095	0.0004
119	19.8000	-0.0713	0.0004
120	20.9000	-0.0389	0.0004
121	22.0000	0.0000	0.0004
1121	22.0000	0.0000	0.0004

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0472	0.0004
123	24.8000	0.0885	0.0003
124	26.2000	0.1189	0.0003
125	27.6000	0.1365	0.0002
126	29.0000	0.0881	0.0002
127	30.4000	0.0849	0.0001
128	31.8000	0.0951	0.0001
129	33.2000	0.1083	0.0001
130	34.6000	0.0342	0.0001
131	36.0000	-0.1040	0.0001
132	37.4000	-0.2591	0.0001
133	38.8000	-0.3160	0.0002
134	40.2000	-0.3486	0.0003
135	41.6000	-0.3536	0.0003
136	43.0000	-0.3136	0.0004
137	44.4000	-0.2575	0.0005
138	45.8000	-0.1918	0.0005
139	47.2000	-0.1247	0.0005
140	48.6000	-0.0594	0.0005
141	50.0000	0.0000	0.0004
1141	50.0000	0.0000	0.0004
142	51.4000	0.0553	0.0004
143	52.8000	0.1011	0.0003
144	54.2000	0.1402	0.0003
145	55.6000	0.1670	0.0003
146	57.0000	0.1539	0.0002
147	58.4000	0.0560	0.0001
148	59.8000	0.0608	0.0001
149	61.2000	0.0635	0.0001
150	62.6000	-0.0228	0.0001
151	64.0000	-0.1899	0.0001
152	65.4000	-0.2598	0.0001
153	66.8000	-0.3160	0.0002
154	68.2000	-0.3477	0.0003
155	69.6000	-0.3519	0.0003
156	71.0000	-0.3114	0.0004
157	72.4000	-0.2575	0.0005
158	73.8000	-0.1901	0.0005
159	75.2000	-0.1232	0.0005
160	76.6000	-0.0586	0.0005
161	78.0000	0.0000	0.0004
1161	78.0000	0.0000	0.0004
162	79.1000	0.0386	0.0003
163	80.2000	0.0698	0.0003
164	81.3000	0.0953	0.0002
165	82.4000	0.1128	0.0002
166	83.5000	0.1130	0.0001
167	84.6000	0.0892	0.0001
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	-0.1123	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.1622	0.0001
174	92.3000	-0.2177	0.0002
175	93.4000	-0.2262	0.0002
176	94.5000	-0.2077	0.0003
177	95.6000	-0.1785	0.0004
178	96.7000	-0.1392	0.0004
179	97.8000	-0.0954	0.0004
180	98.9000	-0.0486	0.0004
181	100.0000	0.0000	0.0005

CÁLCULO DE DESPLÀZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0138	-0.0001
3	2.2000	-0.0277	-0.0001
4	3.3000	-0.0405	-0.0001
5	4.4000	-0.0521	-0.0001
6	5.5000	-0.0632	0.0000
7	6.6000	-0.0719	0.0000
8	7.7000	-0.0791	0.0000
9	8.8000	-0.0846	0.0000
10	9.9000	-0.0878	0.0000
11	11.0000	-0.0886	0.0000
12	12.1000	-0.0879	0.0000
13	13.2000	-0.0845	0.0000
14	14.3000	-0.0790	0.0000
15	15.4000	-0.0720	0.0000
16	16.5000	-0.0630	0.0000
17	17.6000	-0.0527	0.0001
18	18.7000	-0.0410	0.0001
19	19.8000	-0.0276	0.0001
20	20.9000	-0.0143	0.0001
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0202	-0.0001
23	24.8000	-0.0428	-0.0001
24	26.2000	-0.0652	-0.0001
25	27.6000	-0.0878	-0.0001
26	29.0000	-0.1091	-0.0001
27	30.4000	-0.1276	-0.0001
28	31.8000	-0.1431	-0.0001
29	33.2000	-0.1552	0.0000
30	34.6000	-0.1628	0.0000
31	36.0000	-0.1666	0.0000
32	37.4000	-0.1651	0.0000
33	38.8000	-0.1597	0.0000
34	40.2000	-0.1495	0.0001
35	41.6000	-0.1359	0.0001
36	43.0000	-0.1177	0.0001
37	44.4000	-0.0970	0.0001
38	45.8000	-0.0737	0.0001
39	47.2000	-0.0491	0.0002
40	48.6000	-0.0240	0.0002
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0240	-0.0002
43	52.8000	-0.0491	-0.0002
44	54.2000	-0.0737	-0.0001
45	55.6000	-0.0970	-0.0001
46	57.0000	-0.1177	-0.0001
47	58.4000	-0.1359	-0.0001
48	59.8000	-0.1495	-0.0001
49	61.2000	-0.1597	0.0000
50	62.6000	-0.1651	0.0000
51	64.0000	-0.1666	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

SCPAS1.ENV_TREN_GENERICO.GZ+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

SCPAS1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

SCPAS1.ENV_TREN_GENERICO.GZ+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

SCPAS1.ENV_TREN_GENERICO.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	0.0000	0.0000
175	93.4000	0.0000	0.0000
176	94.5000	0.0000	0.0000
177	95.6000	0.0000	0.0000
178	96.7000	0.0000	0.0000
179	97.8000	0.0000	0.0000
180	98.9000	0.0000	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY-
Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0055	0.0000
3	2.2000	-0.0116	0.0000
4	3.3000	-0.0171	0.0000
5	4.4000	-0.0220	0.0000
6	5.5000	-0.0258	0.0000
7	6.6000	-0.0294	0.0000
8	7.7000	-0.0321	0.0000
9	8.8000	-0.0339	0.0000
10	9.9000	-0.0348	0.0000
11	11.0000	-0.0346	0.0000
12	12.1000	-0.0335	0.0000
13	13.2000	-0.0320	0.0000
14	14.3000	-0.0292	0.0000
15	15.4000	-0.0262	0.0000
16	16.5000	-0.0227	0.0000
17	17.6000	-0.0183	0.0000
18	18.7000	-0.0134	0.0000
19	19.8000	-0.0089	0.0000
20	20.9000	-0.0042	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0060	0.0000
23	24.8000	-0.0126	0.0000
24	26.2000	-0.0195	0.0000
25	27.6000	-0.0273	0.0000
26	29.0000	-0.0340	0.0000
27	30.4000	-0.0397	0.0000
28	31.8000	-0.0445	0.0000
29	33.2000	-0.0479	0.0000
30	34.6000	-0.0502	0.0000
31	36.0000	-0.0515	0.0000
32	37.4000	-0.0510	0.0000
33	38.8000	-0.0489	0.0000
34	40.2000	-0.0456	0.0000
35	41.6000	-0.0412	0.0000
36	43.0000	-0.0353	0.0000
37	44.4000	-0.0283	0.0000
38	45.8000	-0.0212	0.0000
39	47.2000	-0.0143	0.0000
40	48.6000	-0.0061	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0061	0.0000
43	52.8000	-0.0143	0.0000
44	54.2000	-0.0212	0.0000
45	55.6000	-0.0283	0.0000
46	57.0000	-0.0353	0.0000
47	58.4000	-0.0412	0.0000
48	59.8000	-0.0456	0.0000
49	61.2000	-0.0489	0.0000
50	62.6000	-0.0510	0.0000
51	64.0000	-0.0515	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY-
Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0502	0.0000
53	66.8000	-0.0479	0.0000
54	68.2000	-0.0445	0.0000
55	69.6000	-0.0397	0.0000
56	71.0000	-0.0340	0.0000
57	72.4000	-0.0273	0.0000
58	73.8000	-0.0195	0.0000
59	75.2000	-0.0126	0.0000
60	76.6000	-0.0060	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0042	0.0000
63	80.2000	-0.0089	0.0000
64	81.3000	-0.0134	0.0000
65	82.4000	-0.0183	0.0000
66	83.5000	-0.0227	0.0000
67	84.6000	-0.0262	0.0000
68	85.7000	-0.0292	0.0000
69	86.8000	-0.0320	0.0000
70	87.9000	-0.0335	0.0000
71	89.0000	-0.0346	0.0000
72	90.1000	-0.0348	0.0000
73	91.2000	-0.0339	0.0000
74	92.3000	-0.0321	0.0000
75	93.4000	-0.0294	0.0000
76	94.5000	-0.0258	0.0000
77	95.6000	-0.0220	0.0000
78	96.7000	-0.0171	0.0000
79	97.8000	-0.0116	0.0000
80	98.9000	-0.0055	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	-0.0005	0.0000
105	4.4000	-0.0010	0.0000
106	5.5000	-0.0012	0.0000
107	6.6000	-0.0013	0.0000
108	7.7000	-0.0015	0.0000
109	8.8000	-0.0015	0.0000
110	9.9000	-0.0015	0.0000
111	11.0000	-0.0015	0.0000
112	12.1000	-0.0015	0.0000
113	13.2000	-0.0015	0.0000
114	14.3000	-0.0015	0.0000
115	15.4000	-0.0015	0.0000
116	16.5000	-0.0015	0.0000
117	17.6000	-0.0014	0.0000
118	18.7000	-0.0012	0.0000
119	19.8000	-0.0009	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	-0.0009	0.0000
124	26.2000	-0.0011	0.0000
125	27.6000	-0.0011	0.0000
126	29.0000	-0.0023	0.0000
127	30.4000	-0.0026	0.0000
128	31.8000	-0.0029	0.0000
129	33.2000	-0.0030	0.0000
130	34.6000	-0.0032	0.0000
131	36.0000	-0.0033	0.0000
132	37.4000	-0.0034	0.0000
133	38.8000	-0.0034	0.0000
134	40.2000	-0.0034	0.0000
135	41.6000	-0.0033	0.0000
136	43.0000	-0.0031	0.0000
137	44.4000	-0.0026	0.0000
138	45.8000	-0.0023	0.0000
139	47.2000	-0.0016	0.0000
140	48.6000	-0.0002	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0002	0.0000
143	52.8000	-0.0016	0.0000
144	54.2000	-0.0023	0.0000
145	55.6000	-0.0026	0.0000
146	57.0000	-0.0031	0.0000
147	58.4000	-0.0033	0.0000
148	59.8000	-0.0034	0.0000
149	61.2000	-0.0034	0.0000
150	62.6000	-0.0034	0.0000
151	64.0000	-0.0033	0.0000
152	65.4000	-0.0032	0.0000
153	66.8000	-0.0030	0.0000
154	68.2000	-0.0029	0.0000
155	69.6000	-0.0026	0.0000
156	71.0000	-0.0023	0.0000
157	72.4000	-0.0011	0.0000
158	73.8000	-0.0011	0.0000
159	75.2000	-0.0009	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	-0.0009	0.0000
164	81.3000	-0.0012	0.0000
165	82.4000	-0.0014	0.0000
166	83.5000	-0.0015	0.0000
167	84.6000	-0.0015	0.0000
168	85.7000	-0.0015	0.0000
169	86.8000	-0.0015	0.0000
170	87.9000	-0.0015	0.0000
171	89.0000	-0.0015	0.0000
172	90.1000	-0.0015	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0000	0.0000
3	2.2000	0.0000	0.0000
4	3.3000	0.0000	0.0000
5	4.4000	0.0000	0.0000
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0000	0.0000
18	18.7000	0.0000	0.0000
19	19.8000	0.0000	0.0000
20	20.9000	0.0000	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0000	0.0000
23	24.8000	0.0000	0.0000
24	26.2000	0.0000	0.0000
25	27.6000	0.0000	0.0000
26	29.0000	0.0000	0.0000
27	30.4000	0.0000	0.0000
28	31.8000	0.0000	0.0000
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0000	0.0000
38	45.8000	0.0000	0.0000
39	47.2000	0.0000	0.0000
40	48.6000	0.0000	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0000	0.0000
43	52.8000	0.0000	0.0000
44	54.2000	0.0000	0.0000
45	55.6000	0.0000	0.0000
46	57.0000	0.0000	0.0000
47	58.4000	0.0000	0.0000
48	59.8000	0.0000	0.0000
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0000	0.0000
57	72.4000	0.0000	0.0000
58	73.8000	0.0000	0.0000
59	75.2000	0.0000	0.0000
60	76.6000	0.0000	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0000	0.0000
63	80.2000	0.0000	0.0000
64	81.3000	0.0000	0.0000
65	82.4000	0.0000	0.0000
66	83.5000	0.0000	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0000	0.0000
78	96.7000	0.0000	0.0000
79	97.8000	0.0000	0.0000
80	98.9000	0.0000	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0000	0.0000
103	2.2000	0.0000	0.0000
104	3.3000	0.0000	0.0000
105	4.4000	0.0000	0.0000
106	5.5000	0.0000	0.0000
107	6.6000	0.0000	0.0000
108	7.7000	0.0000	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0000	0.0000
116	16.5000	0.0000	0.0000
117	17.6000	0.0000	0.0000
118	18.7000	0.0000	0.0000
119	19.8000	0.0000	0.0000
120	20.9000	0.0000	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCPAS1.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCPAS1SCuniTneg.Barra1.Mx- + [0; 1]SCPAS1SCuniTneg.Barra2.M
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0000	0.0000
123	24.8000	0.0000	0.0000
124	26.2000	0.0000	0.0000
125	27.6000	0.0000	0.0000
126	29.0000	0.0000	0.0000
127	30.4000	0.0000	0.0000
128	31.8000	0.0000	0.0000
129	33.2000	0.0000	0.0000
130	34.6000	0.0000	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0000	0.0000
135	41.6000	0.0000	0.0000
136	43.0000	0.0000	0.0000
137	44.4000	0.0000	0.0000
138	45.8000	0.0000	0.0000
139	47.2000	0.0000	0.0000
140	48.6000	0.0000	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0000	0.0000
143	52.8000	0.0000	0.0000
144	54.2000	0.0000	0.0000
145	55.6000	0.0000	0.0000
146	57.0000	0.0000	0.0000
147	58.4000	0.0000	0.0000
148	59.8000	0.0000	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0000	0.0000
153	66.8000	0.0000	0.0000
154	68.2000	0.0000	0.0000
155	69.6000	0.0000	0.0000
156	71.0000	0.0000	0.0000
157	72.4000	0.0000	0.0000
158	73.8000	0.0000	0.0000
159	75.2000	0.0000	0.0000
160	76.6000	0.0000	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0000	0.0000
163	80.2000	0.0000	0.0000
164	81.3000	0.0000	0.0000
165	82.4000	0.0000	0.0000
166	83.5000	0.0000	0.0000
167	84.6000	0.0000	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.1628	0.0000
53	66.8000	-0.1552	0.0000
54	68.2000	-0.1431	0.0001
55	69.6000	-0.1276	0.0001
56	71.0000	-0.1091	0.0001
57	72.4000	-0.0878	0.0001
58	73.8000	-0.0652	0.0001
59	75.2000	-0.0428	0.0001
60	76.6000	-0.0202	0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0143	-0.0001
63	80.2000	-0.0276	-0.0001
64	81.3000	-0.0410	-0.0001
65	82.4000	-0.0527	-0.0001
66	83.5000	-0.0630	0.0000
67	84.6000	-0.0720	0.0000
68	85.7000	-0.0790	0.0000
69	86.8000	-0.0845	0.0000
70	87.9000	-0.0880	0.0000
71	89.0000	-0.0886	0.0000
72	90.1000	-0.0878	0.0000
73	91.2000	-0.0846	0.0000
74	92.3000	-0.0791	0.0000
75	93.4000	-0.0719	0.0000
76	94.5000	-0.0632	0.0000
77	95.6000	-0.0521	0.0001
78	96.7000	-0.0405	0.0001
79	97.8000	-0.0277	0.0001
80	98.9000	-0.0138	0.0001
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0537	-0.0004
103	2.2000	-0.1057	-0.0004
104	3.3000	-0.1540	-0.0004
105	4.4000	-0.1981	-0.0004
106	5.5000	-0.2364	-0.0003
107	6.6000	-0.2681	-0.0002
108	7.7000	-0.2926	-0.0002
109	8.8000	-0.3093	-0.0001
110	9.9000	-0.3186	-0.0001
111	11.0000	-0.3197	0.0001
112	12.1000	-0.3125	0.0001
113	13.2000	-0.2989	0.0002
114	14.3000	-0.2773	0.0002
115	15.4000	-0.2490	0.0003
116	16.5000	-0.2151	0.0003
117	17.6000	-0.1762	0.0003
118	18.7000	-0.1337	0.0004
119	19.8000	-0.0889	0.0004
120	20.9000	-0.0438	0.0004
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0622	-0.0005
123	24.8000	-0.1304	-0.0005
124	26.2000	-0.2011	-0.0005
125	27.6000	-0.2698	-0.0005
126	29.0000	-0.3339	-0.0004
127	30.4000	-0.3904	-0.0003
128	31.8000	-0.4366	-0.0003
129	33.2000	-0.4718	-0.0002
130	34.6000	-0.4942	-0.0001
131	36.0000	-0.5030	0.0000
132	37.4000	-0.4980	0.0001
133	38.8000	-0.4796	0.0002
134	40.2000	-0.4480	0.0003
135	41.6000	-0.4042	0.0003
136	43.0000	-0.3496	0.0004
137	44.4000	-0.2861	0.0005
138	45.8000	-0.2157	0.0005
139	47.2000	-0.1421	0.0005
140	48.6000	-0.0690	0.0005
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0690	-0.0005
143	52.8000	-0.1421	-0.0005
144	54.2000	-0.2157	-0.0005
145	55.6000	-0.2861	-0.0005
146	57.0000	-0.3496	-0.0004
147	58.4000	-0.4042	-0.0003
148	59.8000	-0.4481	-0.0003
149	61.2000	-0.4796	-0.0002
150	62.6000	-0.4980	-0.0001
151	64.0000	-0.5030	0.0000
152	65.4000	-0.4943	0.0001
153	66.8000	-0.4718	0.0002
154	68.2000	-0.4366	0.0003
155	69.6000	-0.3904	0.0003
156	71.0000	-0.3339	0.0004
157	72.4000	-0.2698	0.0005
158	73.8000	-0.2012	0.0005
159	75.2000	-0.1304	0.0005
160	76.6000	-0.0622	0.0005
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0438	-0.0004
163	80.2000	-0.0889	-0.0004
164	81.3000	-0.1337	-0.0004
165	82.4000	-0.1762	-0.0003
166	83.5000	-0.2151	-0.0003
167	84.6000	-0.2490	-0.0003
168	85.7000	-0.2773	-0.0002
169	86.8000	-0.2989	-0.0002
170	87.9000	-0.3127	-0.0001
171	89.0000	-0.3197	-0.0001
172	90.1000	-0.3186	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.3093	0.0001
174	92.3000	-0.2926	0.0002
175	93.4000	-0.2681	0.0002
176	94.5000	-0.2364	0.0003
177	95.6000	-0.1981	0.0004
178	96.7000	-0.1540	0.0004
179	97.8000	-0.1057	0.0004
180	98.9000	-0.0537	0.0004
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0001
2	1.1000	-0.0078	-0.0001
3	2.2000	-0.0139	-0.0001
4	3.3000	-0.0187	-0.0001
5	4.4000	-0.0194	-0.0001
6	5.5000	0.0000	0.0000
7	6.6000	0.0000	0.0000
8	7.7000	0.0000	0.0000
9	8.8000	0.0000	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0000	0.0000
16	16.5000	0.0000	0.0000
17	17.6000	0.0198	-0.0001
18	18.7000	0.0229	-0.0001
19	19.8000	0.0189	-0.0001
20	20.9000	0.0111	-0.0001
21	22.0000	0.0000	-0.0001
1021	22.0000	0.0000	-0.0001
22	23.4000	-0.0167	-0.0001
23	24.8000	-0.0347	-0.0001
24	26.2000	-0.0530	-0.0001
25	27.6000	-0.0707	-0.0001
26	29.0000	-0.0876	-0.0001
27	30.4000	-0.0928	-0.0001
28	31.8000	-0.0832	-0.0001
29	33.2000	0.0000	0.0000
30	34.6000	0.0000	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0000	0.0000
34	40.2000	0.0000	0.0000
35	41.6000	0.0000	0.0000
36	43.0000	0.0000	0.0000
37	44.4000	0.0270	-0.0001
38	45.8000	0.0340	-0.0001
39	47.2000	0.0260	-0.0001
40	48.6000	0.0153	-0.0001
41	50.0000	0.0000	-0.0001
1041	50.0000	0.0000	-0.0001
42	51.4000	-0.0183	-0.0002
43	52.8000	-0.0376	-0.0002
44	54.2000	-0.0550	-0.0001
45	55.6000	-0.0731	-0.0001
46	57.0000	-0.0859	-0.0001
47	58.4000	-0.0947	-0.0001
48	59.8000	-0.0839	-0.0001
49	61.2000	0.0000	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0000	0.0000
53	66.8000	0.0000	0.0000
54	68.2000	0.0000	0.0000
55	69.6000	0.0000	0.0000
56	71.0000	0.0103	0.0000
57	72.4000	0.0107	0.0000
58	73.8000	0.0060	0.0000
59	75.2000	0.0013	0.0000
60	76.6000	0.0039	-0.0001
61	78.0000	0.0000	-0.0001
1061	78.0000	0.0000	-0.0001
62	79.1000	-0.0051	-0.0001
63	80.2000	-0.0100	-0.0001
64	81.3000	-0.0152	-0.0001
65	82.4000	-0.0153	-0.0001
66	83.5000	-0.0032	0.0000
67	84.6000	0.0000	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0000	0.0000
74	92.3000	0.0000	0.0000
75	93.4000	0.0000	0.0000
76	94.5000	0.0000	0.0000
77	95.6000	0.0102	0.0000
78	96.7000	0.0114	-0.0001
79	97.8000	0.0087	-0.0001
80	98.9000	0.0046	-0.0001
81	100.0000	0.0000	-0.0001
101	0.0000	0.0000	-0.0005
102	1.1000	-0.0486	-0.0004
103	2.2000	-0.0954	-0.0004
104	3.3000	-0.1392	-0.0004
105	4.4000	-0.1785	-0.0004
106	5.5000	-0.2077	-0.0003
107	6.6000	-0.2262	-0.0002
108	7.7000	-0.2177	-0.0002
109	8.8000	-0.1622	-0.0001
110	9.9000	-0.1123	-0.0001
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0892	-0.0001
116	16.5000	0.1130	-0.0001
117	17.6000	0.1128	-0.0002
118	18.7000	0.0953	-0.0002
119	19.8000	0.0698	-0.0003
120	20.9000	0.0386	-0.0003
121	22.0000	0.0000	-0.0004
1121	22.0000	0.0000	-0.0004

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
SCUNIA2.ENV_TREN_GENERICO.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0586	-0.0005
123	24.8000	-0.1232	-0.0005
124	26.2000	-0.1900	-0.0005
125	27.6000	-0.2575	-0.0005
126	29.0000	-0.3114	-0.0004
127	30.4000	-0.3519	-0.0003
128	31.8000	-0.3477	-0.0003
129	33.2000	-0.3160	-0.0002
130	34.6000	-0.2598	-0.0001
131	36.0000	-0.1899	-0.0001
132	37.4000	-0.0228	-0.0001
133	38.8000	0.0635	-0.0001
134	40.2000	0.0608	-0.0001
135	41.6000	0.0560	-0.0001
136	43.0000	0.1539	-0.0002
137	44.4000	0.1670	-0.0003
138	45.8000	0.1402	-0.0003
139	47.2000	0.1011	-0.0003
140	48.6000	0.0553	-0.0004
141	50.0000	0.0000	-0.0004
1141	50.0000	0.0000	-0.0004
142	51.4000	-0.0594	-0.0005
143	52.8000	-0.1247	-0.0005
144	54.2000	-0.1918	-0.0005
145	55.6000	-0.2575	-0.0005
146	57.0000	-0.3136	-0.0004
147	58.4000	-0.3536	-0.0003
148	59.8000	-0.3487	-0.0003
149	61.2000	-0.3160	-0.0002
150	62.6000	-0.2591	-0.0001
151	64.0000	-0.1040	-0.0001
152	65.4000	0.0342	-0.0001
153	66.8000	0.1083	-0.0001
154	68.2000	0.0951	-0.0001
155	69.6000	0.0849	-0.0001
156	71.0000	0.0881	-0.0002
157	72.4000	0.1365	-0.0002
158	73.8000	0.1190	-0.0003
159	75.2000	0.0886	-0.0003
160	76.6000	0.0472	-0.0004
161	78.0000	0.0000	-0.0004
1161	78.0000	0.0000	-0.0004
162	79.1000	-0.0389	-0.0004
163	80.2000	-0.0713	-0.0004
164	81.3000	-0.1095	-0.0004
165	82.4000	-0.1435	-0.0003
166	83.5000	-0.1779	-0.0003
167	84.6000	-0.2020	-0.0003
168	85.7000	-0.2180	-0.0002
169	86.8000	-0.2085	-0.0002
170	87.9000	-0.1827	-0.0001
171	89.0000	-0.1122	-0.0001
172	90.1000	0.0778	-0.0001

SCUNIA2.ENV_TREN_GENERICO.GZ-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

SCUNIA2.ENV_TREN_GENERICO.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]SCUNIA2SCuniTneg.Barra101.Mx- + [0; 1]SCUNIA2SCuniTneg.Barra

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.1050	-0.0001
174	92.3000	0.1016	-0.0001
175	93.4000	0.0946	-0.0001
176	94.5000	0.0848	-0.0001
177	95.6000	0.0718	-0.0002
178	96.7000	0.0549	-0.0002
179	97.8000	0.0369	-0.0002
180	98.9000	0.0188	-0.0002
181	100.0000	0.0000	-0.0002

TRENLA1.EnvTrenGen.UY+

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

TRENLA1.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0035	0.0000
3	2.2000	0.0070	0.0000
4	3.3000	0.0104	0.0000
5	4.4000	0.0136	0.0000
6	5.5000	0.0167	0.0000
7	6.6000	0.0194	0.0000
8	7.7000	0.0218	0.0000
9	8.8000	0.0239	0.0000
10	9.9000	0.0255	0.0000
11	11.0000	0.0267	0.0000
12	12.1000	0.0274	0.0000
13	13.2000	0.0275	0.0000
14	14.3000	0.0270	0.0000
15	15.4000	0.0258	0.0000
16	16.5000	0.0239	0.0000
17	17.6000	0.0210	0.0000
18	18.7000	0.0173	0.0000
19	19.8000	0.0126	-0.0001
20	20.9000	0.0069	-0.0001
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0069	0.0000
23	24.8000	0.0125	0.0000
24	26.2000	0.0168	0.0000
25	27.6000	0.0200	0.0000
26	29.0000	0.0222	0.0000
27	30.4000	0.0235	0.0000
28	31.8000	0.0240	0.0000
29	33.2000	0.0239	0.0000
30	34.6000	0.0258	0.0000
31	36.0000	0.0279	0.0000
32	37.4000	0.0295	0.0000
33	38.8000	0.0304	0.0000
34	40.2000	0.0306	0.0000
35	41.6000	0.0299	0.0000
36	43.0000	0.0283	0.0000
37	44.4000	0.0255	0.0000
38	45.8000	0.0214	0.0000
39	47.2000	0.0159	0.0000
40	48.6000	0.0088	-0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0088	0.0001
43	52.8000	0.0159	0.0000
44	54.2000	0.0214	0.0000
45	55.6000	0.0255	0.0000
46	57.0000	0.0283	0.0000
47	58.4000	0.0299	0.0000
48	59.8000	0.0306	0.0000
49	61.2000	0.0304	0.0000
50	62.6000	0.0295	0.0000
51	64.0000	0.0279	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0258	0.0000
53	66.8000	0.0239	0.0000
54	68.2000	0.0240	0.0000
55	69.6000	0.0235	0.0000
56	71.0000	0.0222	0.0000
57	72.4000	0.0200	0.0000
58	73.8000	0.0168	0.0000
59	75.2000	0.0125	0.0000
60	76.6000	0.0069	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0069	0.0001
63	80.2000	0.0126	0.0001
64	81.3000	0.0173	0.0000
65	82.4000	0.0210	0.0000
66	83.5000	0.0239	0.0000
67	84.6000	0.0258	0.0000
68	85.7000	0.0270	0.0000
69	86.8000	0.0275	0.0000
70	87.9000	0.0274	0.0000
71	89.0000	0.0267	0.0000
72	90.1000	0.0255	0.0000
73	91.2000	0.0239	0.0000
74	92.3000	0.0218	0.0000
75	93.4000	0.0194	0.0000
76	94.5000	0.0167	0.0000
77	95.6000	0.0136	0.0000
78	96.7000	0.0104	0.0000
79	97.8000	0.0070	0.0000
80	98.9000	0.0035	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0014	0.0000
103	2.2000	0.0028	0.0000
104	3.3000	0.0041	0.0000
105	4.4000	0.0053	0.0000
106	5.5000	0.0065	0.0000
107	6.6000	0.0075	0.0000
108	7.7000	0.0085	0.0000
109	8.8000	0.0092	0.0000
110	9.9000	0.0098	0.0000
111	11.0000	0.0102	0.0000
112	12.1000	0.0104	0.0000
113	13.2000	0.0103	0.0000
114	14.3000	0.0100	0.0000
115	15.4000	0.0095	0.0000
116	16.5000	0.0087	0.0000
117	17.6000	0.0075	0.0000
118	18.7000	0.0061	0.0000
119	19.8000	0.0044	0.0000
120	20.9000	0.0024	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0020	0.0000
123	24.8000	0.0038	0.0000
124	26.2000	0.0053	0.0000
125	27.6000	0.0065	0.0000
126	29.0000	0.0075	0.0000
127	30.4000	0.0087	0.0000
128	31.8000	0.0100	0.0000
129	33.2000	0.0112	0.0000
130	34.6000	0.0122	0.0000
131	36.0000	0.0129	0.0000
132	37.4000	0.0134	0.0000
133	38.8000	0.0135	0.0000
134	40.2000	0.0133	0.0000
135	41.6000	0.0127	0.0000
136	43.0000	0.0117	0.0000
137	44.4000	0.0102	0.0000
138	45.8000	0.0083	0.0000
139	47.2000	0.0060	0.0000
140	48.6000	0.0032	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0032	0.0000
143	52.8000	0.0060	0.0000
144	54.2000	0.0083	0.0000
145	55.6000	0.0102	0.0000
146	57.0000	0.0117	0.0000
147	58.4000	0.0127	0.0000
148	59.8000	0.0133	0.0000
149	61.2000	0.0135	0.0000
150	62.6000	0.0134	0.0000
151	64.0000	0.0129	0.0000
152	65.4000	0.0122	0.0000
153	66.8000	0.0112	0.0000
154	68.2000	0.0100	0.0000
155	69.6000	0.0087	0.0000
156	71.0000	0.0075	0.0000
157	72.4000	0.0065	0.0000
158	73.8000	0.0053	0.0000
159	75.2000	0.0038	0.0000
160	76.6000	0.0020	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0024	0.0000
163	80.2000	0.0044	0.0000
164	81.3000	0.0061	0.0000
165	82.4000	0.0075	0.0000
166	83.5000	0.0087	0.0000
167	84.6000	0.0095	0.0000
168	85.7000	0.0100	0.0000
169	86.8000	0.0103	0.0000
170	87.9000	0.0104	0.0000
171	89.0000	0.0102	0.0000
172	90.1000	0.0098	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0092	0.0000
174	92.3000	0.0085	0.0000
175	93.4000	0.0075	0.0000
176	94.5000	0.0065	0.0000
177	95.6000	0.0053	0.0000
178	96.7000	0.0041	0.0000
179	97.8000	0.0028	0.0000
180	98.9000	0.0014	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0035	0.0000
3	2.2000	0.0070	0.0000
4	3.3000	0.0104	0.0000
5	4.4000	0.0136	0.0000
6	5.5000	0.0166	0.0000
7	6.6000	0.0193	0.0000
8	7.7000	0.0217	0.0000
9	8.8000	0.0237	0.0000
10	9.9000	0.0254	0.0000
11	11.0000	-0.0469	0.0000
12	12.1000	-0.0454	0.0000
13	13.2000	-0.0427	0.0000
14	14.3000	-0.0391	0.0000
15	15.4000	-0.0345	0.0001
16	16.5000	-0.0333	0.0001
17	17.6000	-0.0248	0.0001
18	18.7000	-0.0172	0.0001
19	19.8000	-0.0119	0.0001
20	20.9000	-0.0058	0.0001
21	22.0000	0.0000	0.0001
1021	22.0000	0.0000	0.0001
22	23.4000	0.0057	0.0000
23	24.8000	0.0125	0.0000
24	26.2000	0.0163	0.0000
25	27.6000	0.0165	0.0000
26	29.0000	0.0143	0.0000
27	30.4000	0.0174	0.0000
28	31.8000	0.0204	0.0000
29	33.2000	0.0232	0.0000
30	34.6000	0.0257	0.0000
31	36.0000	0.0277	0.0000
32	37.4000	-0.0800	0.0000
33	38.8000	-0.0765	0.0000
34	40.2000	-0.0709	0.0001
35	41.6000	-0.0634	0.0001
36	43.0000	-0.0543	0.0001
37	44.4000	-0.0438	0.0001
38	45.8000	-0.0325	0.0001
39	47.2000	-0.0210	0.0001
40	48.6000	-0.0099	0.0001
41	50.0000	0.0000	0.0001
1041	50.0000	0.0000	0.0001
42	51.4000	0.0088	0.0001
43	52.8000	0.0144	0.0000
44	54.2000	0.0194	0.0000
45	55.6000	0.0231	0.0000
46	57.0000	0.0275	0.0000
47	58.4000	0.0134	0.0000
48	59.8000	0.0157	0.0000
49	61.2000	0.0178	0.0000
50	62.6000	0.0197	0.0000
51	64.0000	0.0212	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0799	0.0000
53	66.8000	-0.0764	0.0000
54	68.2000	-0.0707	0.0001
55	69.6000	-0.0631	0.0001
56	71.0000	-0.0540	0.0001
57	72.4000	-0.0435	0.0001
58	73.8000	-0.0322	0.0001
59	75.2000	-0.0208	0.0001
60	76.6000	-0.0098	0.0001
61	78.0000	0.0000	0.0001
1061	78.0000	0.0000	0.0001
62	79.1000	0.0067	0.0001
63	80.2000	0.0123	0.0001
64	81.3000	0.0159	0.0000
65	82.4000	0.0191	0.0000
66	83.5000	0.0217	0.0000
67	84.6000	0.0096	0.0000
68	85.7000	0.0246	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	-0.0493	0.0000
73	91.2000	-0.0481	0.0000
74	92.3000	-0.0456	0.0000
75	93.4000	-0.0419	0.0000
76	94.5000	-0.0370	0.0001
77	95.6000	-0.0311	0.0001
78	96.7000	-0.0242	0.0001
79	97.8000	-0.0173	0.0001
80	98.9000	-0.0084	0.0001
81	100.0000	0.0000	0.0001
101	0.0000	0.0000	0.0000
102	1.1000	0.0014	0.0000
103	2.2000	0.0027	0.0000
104	3.3000	0.0040	0.0000
105	4.4000	0.0052	0.0000
106	5.5000	0.0064	0.0000
107	6.6000	0.0074	0.0000
108	7.7000	0.0084	0.0000
109	8.8000	0.0091	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	-0.0108	0.0000
114	14.3000	-0.0100	0.0000
115	15.4000	-0.0089	0.0000
116	16.5000	-0.0077	0.0000
117	17.6000	-0.0070	0.0000
118	18.7000	-0.0052	0.0000
119	19.8000	-0.0035	0.0000
120	20.9000	-0.0017	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0018	0.0000
123	24.8000	0.0033	0.0000
124	26.2000	0.0047	0.0000
125	27.6000	0.0058	0.0000
126	29.0000	0.0067	0.0000
127	30.4000	0.0086	0.0000
128	31.8000	0.0099	0.0000
129	33.2000	0.0111	0.0000
130	34.6000	0.0120	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	-0.0274	0.0000
133	38.8000	-0.0262	0.0000
134	40.2000	-0.0244	0.0000
135	41.6000	-0.0218	0.0000
136	43.0000	-0.0187	0.0000
137	44.4000	-0.0152	0.0000
138	45.8000	-0.0114	0.0000
139	47.2000	-0.0074	0.0000
140	48.6000	-0.0036	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0031	0.0000
143	52.8000	0.0057	0.0000
144	54.2000	0.0083	0.0000
145	55.6000	0.0045	0.0000
146	57.0000	0.0109	0.0000
147	58.4000	0.0112	0.0000
148	59.8000	0.0063	0.0000
149	61.2000	0.0000	0.0000
150	62.6000	0.0000	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	-0.0273	0.0000
153	66.8000	-0.0261	0.0000
154	68.2000	-0.0241	0.0000
155	69.6000	-0.0215	0.0000
156	71.0000	-0.0184	0.0000
157	72.4000	-0.0148	0.0000
158	73.8000	-0.0110	0.0000
159	75.2000	-0.0071	0.0000
160	76.6000	-0.0034	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0023	0.0000
163	80.2000	0.0043	0.0000
164	81.3000	0.0024	0.0000
165	82.4000	0.0072	0.0000
166	83.5000	0.0082	0.0000
167	84.6000	0.0090	0.0000
168	85.7000	0.0000	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0000	0.0000
174	92.3000	-0.0125	0.0000
175	93.4000	-0.0115	0.0000
176	94.5000	-0.0101	0.0000
177	95.6000	-0.0085	0.0000
178	96.7000	-0.0066	0.0000
179	97.8000	-0.0045	0.0000
180	98.9000	-0.0023	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0089	-0.0001
3	2.2000	-0.0175	-0.0001
4	3.3000	-0.0255	-0.0001
5	4.4000	-0.0327	-0.0001
6	5.5000	-0.0389	-0.0001
7	6.6000	-0.0439	0.0000
8	7.7000	-0.0477	0.0000
9	8.8000	-0.0503	0.0000
10	9.9000	-0.0515	0.0000
11	11.0000	-0.0515	0.0000
12	12.1000	-0.0501	0.0000
13	13.2000	-0.0475	0.0000
14	14.3000	-0.0438	0.0000
15	15.4000	-0.0390	0.0001
16	16.5000	-0.0333	0.0001
17	17.6000	-0.0270	0.0001
18	18.7000	-0.0202	0.0001
19	19.8000	-0.0132	0.0001
20	20.9000	-0.0064	0.0001
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0103	-0.0001
23	24.8000	-0.0216	-0.0001
24	26.2000	-0.0332	-0.0001
25	27.6000	-0.0445	-0.0001
26	29.0000	-0.0549	-0.0001
27	30.4000	-0.0640	-0.0001
28	31.8000	-0.0714	-0.0001
29	33.2000	-0.0768	0.0000
30	34.6000	-0.0803	0.0000
31	36.0000	-0.0814	0.0000
32	37.4000	-0.0804	0.0000
33	38.8000	-0.0771	0.0000
34	40.2000	-0.0717	0.0001
35	41.6000	-0.0644	0.0001
36	43.0000	-0.0553	0.0001
37	44.4000	-0.0449	0.0001
38	45.8000	-0.0336	0.0001
39	47.2000	-0.0219	0.0001
40	48.6000	-0.0105	0.0001
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0105	-0.0001
43	52.8000	-0.0219	-0.0001
44	54.2000	-0.0336	-0.0001
45	55.6000	-0.0449	-0.0001
46	57.0000	-0.0553	-0.0001
47	58.4000	-0.0644	-0.0001
48	59.8000	-0.0717	-0.0001
49	61.2000	-0.0771	0.0000
50	62.6000	-0.0804	0.0000
51	64.0000	-0.0815	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY-
Envolvente de tren de cargas plano genérico. UY
[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0803	0.0000
53	66.8000	-0.0768	0.0000
54	68.2000	-0.0714	0.0001
55	69.6000	-0.0640	0.0001
56	71.0000	-0.0549	0.0001
57	72.4000	-0.0445	0.0001
58	73.8000	-0.0332	0.0001
59	75.2000	-0.0216	0.0001
60	76.6000	-0.0103	0.0001
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0064	-0.0001
63	80.2000	-0.0132	-0.0001
64	81.3000	-0.0202	-0.0001
65	82.4000	-0.0270	-0.0001
66	83.5000	-0.0333	-0.0001
67	84.6000	-0.0390	-0.0001
68	85.7000	-0.0438	0.0000
69	86.8000	-0.0475	0.0000
70	87.9000	-0.0501	0.0000
71	89.0000	-0.0515	0.0000
72	90.1000	-0.0515	0.0000
73	91.2000	-0.0503	0.0000
74	92.3000	-0.0477	0.0000
75	93.4000	-0.0439	0.0000
76	94.5000	-0.0389	0.0001
77	95.6000	-0.0327	0.0001
78	96.7000	-0.0255	0.0001
79	97.8000	-0.0175	0.0001
80	98.9000	-0.0089	0.0001
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0023	0.0000
103	2.2000	-0.0045	0.0000
104	3.3000	-0.0066	0.0000
105	4.4000	-0.0085	0.0000
106	5.5000	-0.0102	0.0000
107	6.6000	-0.0115	0.0000
108	7.7000	-0.0126	0.0000
109	8.8000	-0.0133	0.0000
110	9.9000	-0.0137	0.0000
111	11.0000	-0.0137	0.0000
112	12.1000	-0.0133	0.0000
113	13.2000	-0.0127	0.0000
114	14.3000	-0.0117	0.0000
115	15.4000	-0.0104	0.0000
116	16.5000	-0.0089	0.0000
117	17.6000	-0.0073	0.0000
118	18.7000	-0.0055	0.0000
119	19.8000	-0.0036	0.0000
120	20.9000	-0.0017	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.UY-
Envolvente de tren de cargas plano genérico. UY
[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0035	0.0000
123	24.8000	-0.0072	0.0000
124	26.2000	-0.0111	0.0000
125	27.6000	-0.0149	0.0000
126	29.0000	-0.0185	0.0000
127	30.4000	-0.0217	0.0000
128	31.8000	-0.0243	0.0000
129	33.2000	-0.0262	0.0000
130	34.6000	-0.0274	0.0000
131	36.0000	-0.0279	0.0000
132	37.4000	-0.0276	0.0000
133	38.8000	-0.0264	0.0000
134	40.2000	-0.0246	0.0000
135	41.6000	-0.0221	0.0000
136	43.0000	-0.0190	0.0000
137	44.4000	-0.0154	0.0000
138	45.8000	-0.0116	0.0000
139	47.2000	-0.0076	0.0000
140	48.6000	-0.0037	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0037	0.0000
143	52.8000	-0.0076	0.0000
144	54.2000	-0.0116	0.0000
145	55.6000	-0.0154	0.0000
146	57.0000	-0.0190	0.0000
147	58.4000	-0.0221	0.0000
148	59.8000	-0.0246	0.0000
149	61.2000	-0.0264	0.0000
150	62.6000	-0.0276	0.0000
151	64.0000	-0.0279	0.0000
152	65.4000	-0.0274	0.0000
153	66.8000	-0.0262	0.0000
154	68.2000	-0.0243	0.0000
155	69.6000	-0.0217	0.0000
156	71.0000	-0.0185	0.0000
157	72.4000	-0.0149	0.0000
158	73.8000	-0.0111	0.0000
159	75.2000	-0.0072	0.0000
160	76.6000	-0.0035	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0017	0.0000
163	80.2000	-0.0036	0.0000
164	81.3000	-0.0055	0.0000
165	82.4000	-0.0073	0.0000
166	83.5000	-0.0089	0.0000
167	84.6000	-0.0104	0.0000
168	85.7000	-0.0117	0.0000
169	86.8000	-0.0127	0.0000
170	87.9000	-0.0133	0.0000
171	89.0000	-0.0137	0.0000
172	90.1000	-0.0137	0.0000

TRENLA1.EnvTrenGen.UY-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

TRENLA1.EnvTrenGen.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0133	0.0000
174	92.3000	-0.0126	0.0000
175	93.4000	-0.0115	0.0000
176	94.5000	-0.0102	0.0000
177	95.6000	-0.0085	0.0000
178	96.7000	-0.0066	0.0000
179	97.8000	-0.0045	0.0000
180	98.9000	-0.0023	0.0000
181	100.0000	0.0000	0.0000

TRENLA1.EnvTrenGen.GZ-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:

TRENLA1.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	-0.0001
2	1.1000	-0.0085	-0.0001
3	2.2000	-0.0175	-0.0001
4	3.3000	-0.0244	-0.0001
5	4.4000	-0.0304	-0.0001
6	5.5000	-0.0361	-0.0001
7	6.6000	-0.0407	0.0000
8	7.7000	-0.0441	0.0000
9	8.8000	-0.0479	0.0000
10	9.9000	-0.0507	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0269	0.0000
15	15.4000	0.0256	0.0000
16	16.5000	0.0237	0.0000
17	17.6000	0.0209	0.0000
18	18.7000	0.0172	0.0000
19	19.8000	0.0125	-0.0001
20	20.9000	0.0068	-0.0001
21	22.0000	0.0000	-0.0001
1021	22.0000	0.0000	-0.0001
22	23.4000	-0.0102	-0.0001
23	24.8000	-0.0215	-0.0001
24	26.2000	-0.0331	-0.0001
25	27.6000	-0.0444	-0.0001
26	29.0000	-0.0549	-0.0001
27	30.4000	-0.0640	-0.0001
28	31.8000	-0.0714	-0.0001
29	33.2000	-0.0768	0.0000
30	34.6000	-0.0802	0.0000
31	36.0000	0.0180	0.0000
32	37.4000	0.0167	0.0000
33	38.8000	0.0151	0.0000
34	40.2000	0.0148	0.0000
35	41.6000	0.0121	0.0000
36	43.0000	0.0099	0.0000
37	44.4000	0.0077	0.0000
38	45.8000	0.0212	0.0000
39	47.2000	0.0157	0.0000
40	48.6000	0.0087	-0.0001
41	50.0000	0.0000	-0.0001
1041	50.0000	0.0000	-0.0001
42	51.4000	-0.0104	-0.0001
43	52.8000	-0.0218	-0.0001
44	54.2000	-0.0335	-0.0001
45	55.6000	-0.0449	-0.0001
46	57.0000	-0.0553	-0.0001
47	58.4000	-0.0644	-0.0001
48	59.8000	-0.0717	-0.0001
49	61.2000	-0.0771	0.0000
50	62.6000	-0.0803	0.0000
51	64.0000	0.0109	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0237	0.0000
53	66.8000	0.0214	0.0000
54	68.2000	0.0188	0.0000
55	69.6000	0.0161	0.0000
56	71.0000	0.0132	0.0000
57	72.4000	0.0102	0.0000
58	73.8000	0.0160	0.0000
59	75.2000	0.0124	0.0000
60	76.6000	0.0065	0.0000
61	78.0000	0.0000	-0.0001
1061	78.0000	0.0000	-0.0001
62	79.1000	-0.0060	-0.0001
63	80.2000	-0.0125	-0.0001
64	81.3000	-0.0192	-0.0001
65	82.4000	-0.0257	-0.0001
66	83.5000	-0.0333	-0.0001
67	84.6000	-0.0372	-0.0001
68	85.7000	-0.0418	0.0000
69	86.8000	-0.0454	0.0000
70	87.9000	-0.0223	0.0000
71	89.0000	0.0244	0.0000
72	90.1000	0.0234	0.0000
73	91.2000	0.0219	0.0000
74	92.3000	0.0200	0.0000
75	93.4000	0.0178	0.0000
76	94.5000	0.0161	0.0000
77	95.6000	0.0125	0.0000
78	96.7000	0.0096	0.0000
79	97.8000	0.0065	0.0000
80	98.9000	0.0033	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0019	0.0000
103	2.2000	-0.0038	0.0000
104	3.3000	-0.0056	0.0000
105	4.4000	-0.0081	0.0000
106	5.5000	-0.0087	0.0000
107	6.6000	-0.0098	0.0000
108	7.7000	-0.0107	0.0000
109	8.8000	0.0000	0.0000
110	9.9000	0.0000	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0000	0.0000
115	15.4000	0.0095	0.0000
116	16.5000	0.0086	0.0000
117	17.6000	0.0075	0.0000
118	18.7000	0.0061	0.0000
119	19.8000	0.0044	0.0000
120	20.9000	0.0024	0.0000
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0035	0.0000
123	24.8000	-0.0072	0.0000
124	26.2000	-0.0111	0.0000
125	27.6000	-0.0149	0.0000
126	29.0000	-0.0185	0.0000
127	30.4000	-0.0216	0.0000
128	31.8000	-0.0242	0.0000
129	33.2000	-0.0084	0.0000
130	34.6000	-0.0273	0.0000
131	36.0000	0.0000	0.0000
132	37.4000	0.0000	0.0000
133	38.8000	0.0000	0.0000
134	40.2000	0.0061	0.0000
135	41.6000	0.0053	0.0000
136	43.0000	0.0044	0.0000
137	44.4000	0.0035	0.0000
138	45.8000	0.0083	0.0000
139	47.2000	0.0060	0.0000
140	48.6000	0.0032	0.0000
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0037	0.0000
143	52.8000	-0.0076	0.0000
144	54.2000	-0.0116	0.0000
145	55.6000	-0.0154	0.0000
146	57.0000	-0.0190	0.0000
147	58.4000	-0.0221	0.0000
148	59.8000	-0.0246	0.0000
149	61.2000	-0.0053	0.0000
150	62.6000	-0.0275	0.0000
151	64.0000	0.0000	0.0000
152	65.4000	0.0111	0.0000
153	66.8000	0.0102	0.0000
154	68.2000	0.0091	0.0000
155	69.6000	0.0079	0.0000
156	71.0000	0.0066	0.0000
157	72.4000	0.0052	0.0000
158	73.8000	0.0038	0.0000
159	75.2000	0.0024	0.0000
160	76.6000	0.0012	0.0000
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0017	0.0000
163	80.2000	-0.0036	0.0000
164	81.3000	-0.0054	0.0000
165	82.4000	-0.0072	0.0000
166	83.5000	-0.0010	0.0000
167	84.6000	-0.0016	0.0000
168	85.7000	-0.0021	0.0000
169	86.8000	-0.0126	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA1.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA1.PaseoTren.Nudo1.Pos2.Mx+ + [0; 1]TRENLA1.PaseoTren.

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0085	0.0000
174	92.3000	0.0078	0.0000
175	93.4000	0.0069	0.0000
176	94.5000	0.0060	0.0000
177	95.6000	0.0049	0.0000
178	96.7000	0.0037	0.0000
179	97.8000	0.0025	0.0000
180	98.9000	0.0006	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0015	0.0000
3	2.2000	0.0030	0.0000
4	3.3000	0.0044	0.0000
5	4.4000	0.0058	0.0000
6	5.5000	0.0070	0.0000
7	6.6000	0.0081	0.0000
8	7.7000	0.0091	0.0000
9	8.8000	0.0099	0.0000
10	9.9000	0.0105	0.0000
11	11.0000	0.0109	0.0000
12	12.1000	0.0111	0.0000
13	13.2000	0.0110	0.0000
14	14.3000	0.0107	0.0000
15	15.4000	0.0101	0.0000
16	16.5000	0.0092	0.0000
17	17.6000	0.0080	0.0000
18	18.7000	0.0064	0.0000
19	19.8000	0.0046	0.0000
20	20.9000	0.0025	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0021	0.0000
23	24.8000	0.0039	0.0000
24	26.2000	0.0055	0.0000
25	27.6000	0.0069	0.0000
26	29.0000	0.0079	0.0000
27	30.4000	0.0094	0.0000
28	31.8000	0.0109	0.0000
29	33.2000	0.0121	0.0000
30	34.6000	0.0132	0.0000
31	36.0000	0.0139	0.0000
32	37.4000	0.0144	0.0000
33	38.8000	0.0145	0.0000
34	40.2000	0.0142	0.0000
35	41.6000	0.0135	0.0000
36	43.0000	0.0124	0.0000
37	44.4000	0.0108	0.0000
38	45.8000	0.0088	0.0000
39	47.2000	0.0063	0.0000
40	48.6000	0.0034	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0034	0.0000
43	52.8000	0.0063	0.0000
44	54.2000	0.0088	0.0000
45	55.6000	0.0108	0.0000
46	57.0000	0.0124	0.0000
47	58.4000	0.0135	0.0000
48	59.8000	0.0142	0.0000
49	61.2000	0.0145	0.0000
50	62.6000	0.0144	0.0000
51	64.0000	0.0139	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0132	0.0000
53	66.8000	0.0121	0.0000
54	68.2000	0.0109	0.0000
55	69.6000	0.0094	0.0000
56	71.0000	0.0079	0.0000
57	72.4000	0.0069	0.0000
58	73.8000	0.0055	0.0000
59	75.2000	0.0039	0.0000
60	76.6000	0.0021	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0025	0.0000
63	80.2000	0.0046	0.0000
64	81.3000	0.0064	0.0000
65	82.4000	0.0080	0.0000
66	83.5000	0.0092	0.0000
67	84.6000	0.0101	0.0000
68	85.7000	0.0107	0.0000
69	86.8000	0.0110	0.0000
70	87.9000	0.0111	0.0000
71	89.0000	0.0109	0.0000
72	90.1000	0.0105	0.0000
73	91.2000	0.0099	0.0000
74	92.3000	0.0091	0.0000
75	93.4000	0.0081	0.0000
76	94.5000	0.0070	0.0000
77	95.6000	0.0058	0.0000
78	96.7000	0.0044	0.0000
79	97.8000	0.0030	0.0000
80	98.9000	0.0015	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0038	0.0000
103	2.2000	0.0075	0.0000
104	3.3000	0.0112	0.0000
105	4.4000	0.0146	0.0000
106	5.5000	0.0178	0.0000
107	6.6000	0.0208	0.0000
108	7.7000	0.0234	0.0000
109	8.8000	0.0256	0.0000
110	9.9000	0.0274	0.0000
111	11.0000	0.0288	0.0000
112	12.1000	0.0295	0.0000
113	13.2000	0.0297	0.0000
114	14.3000	0.0292	0.0000
115	15.4000	0.0279	0.0000
116	16.5000	0.0258	0.0000
117	17.6000	0.0228	0.0000
118	18.7000	0.0188	0.0000
119	19.8000	0.0137	-0.0001
120	20.9000	0.0075	-0.0001
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0075	0.0001
123	24.8000	0.0135	0.0000
124	26.2000	0.0182	0.0000
125	27.6000	0.0216	0.0000
126	29.0000	0.0240	0.0000
127	30.4000	0.0254	0.0000
128	31.8000	0.0259	0.0000
129	33.2000	0.0257	0.0000
130	34.6000	0.0277	0.0000
131	36.0000	0.0300	0.0000
132	37.4000	0.0317	0.0000
133	38.8000	0.0327	0.0000
134	40.2000	0.0329	0.0000
135	41.6000	0.0323	0.0000
136	43.0000	0.0305	0.0000
137	44.4000	0.0275	0.0000
138	45.8000	0.0232	0.0000
139	47.2000	0.0172	-0.0001
140	48.6000	0.0096	-0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	0.0096	0.0001
143	52.8000	0.0172	0.0001
144	54.2000	0.0232	0.0000
145	55.6000	0.0275	0.0000
146	57.0000	0.0305	0.0000
147	58.4000	0.0323	0.0000
148	59.8000	0.0329	0.0000
149	61.2000	0.0327	0.0000
150	62.6000	0.0317	0.0000
151	64.0000	0.0300	0.0000
152	65.4000	0.0277	0.0000
153	66.8000	0.0257	0.0000
154	68.2000	0.0259	0.0000
155	69.6000	0.0254	0.0000
156	71.0000	0.0240	0.0000
157	72.4000	0.0216	0.0000
158	73.8000	0.0182	0.0000
159	75.2000	0.0135	0.0000
160	76.6000	0.0075	-0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	0.0075	0.0001
163	80.2000	0.0137	0.0001
164	81.3000	0.0188	0.0000
165	82.4000	0.0228	0.0000
166	83.5000	0.0258	0.0000
167	84.6000	0.0279	0.0000
168	85.7000	0.0292	0.0000
169	86.8000	0.0297	0.0000
170	87.9000	0.0295	0.0000
171	89.0000	0.0288	0.0000
172	90.1000	0.0274	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY+

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0256	0.0000
174	92.3000	0.0234	0.0000
175	93.4000	0.0208	0.0000
176	94.5000	0.0178	0.0000
177	95.6000	0.0146	0.0000
178	96.7000	0.0112	0.0000
179	97.8000	0.0075	0.0000
180	98.9000	0.0038	0.0000
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ+

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	0.0015	0.0000
3	2.2000	0.0030	0.0000
4	3.3000	0.0044	0.0000
5	4.4000	0.0057	0.0000
6	5.5000	0.0070	0.0000
7	6.6000	0.0081	0.0000
8	7.7000	0.0090	0.0000
9	8.8000	0.0099	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	-0.0107	0.0000
14	14.3000	-0.0099	0.0000
15	15.4000	-0.0089	0.0000
16	16.5000	-0.0076	0.0000
17	17.6000	-0.0071	0.0000
18	18.7000	-0.0052	0.0000
19	19.8000	-0.0035	0.0000
20	20.9000	-0.0017	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	0.0018	0.0000
23	24.8000	0.0035	0.0000
24	26.2000	0.0049	0.0000
25	27.6000	0.0061	0.0000
26	29.0000	0.0070	0.0000
27	30.4000	0.0093	0.0000
28	31.8000	0.0107	0.0000
29	33.2000	0.0120	0.0000
30	34.6000	0.0130	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	-0.0278	0.0000
33	38.8000	-0.0267	0.0000
34	40.2000	-0.0248	0.0000
35	41.6000	-0.0222	0.0000
36	43.0000	-0.0191	0.0000
37	44.4000	-0.0155	0.0000
38	45.8000	-0.0116	0.0000
39	47.2000	-0.0076	0.0000
40	48.6000	-0.0037	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	0.0033	0.0000
43	52.8000	0.0060	0.0000
44	54.2000	0.0084	0.0000
45	55.6000	0.0046	0.0000
46	57.0000	0.0117	0.0000
47	58.4000	0.0127	0.0000
48	59.8000	0.0069	0.0000
49	61.2000	0.0080	0.0000
50	62.6000	0.0000	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0278	0.0000
53	66.8000	-0.0265	0.0000
54	68.2000	-0.0245	0.0000
55	69.6000	-0.0219	0.0000
56	71.0000	-0.0187	0.0000
57	72.4000	-0.0151	0.0000
58	73.8000	-0.0112	0.0000
59	75.2000	-0.0073	0.0000
60	76.6000	-0.0035	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	0.0024	0.0000
63	80.2000	0.0045	0.0000
64	81.3000	0.0064	0.0000
65	82.4000	0.0076	0.0000
66	83.5000	0.0088	0.0000
67	84.6000	0.0096	0.0000
68	85.7000	0.0000	0.0000
69	86.8000	0.0000	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	-0.0125	0.0000
74	92.3000	-0.0121	0.0000
75	93.4000	-0.0111	0.0000
76	94.5000	-0.0097	0.0000
77	95.6000	-0.0081	0.0000
78	96.7000	-0.0063	0.0000
79	97.8000	-0.0043	0.0000
80	98.9000	-0.0022	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	0.0038	0.0000
103	2.2000	0.0075	0.0000
104	3.3000	0.0111	0.0000
105	4.4000	0.0145	0.0000
106	5.5000	0.0177	0.0000
107	6.6000	0.0206	0.0000
108	7.7000	0.0232	0.0000
109	8.8000	0.0255	0.0000
110	9.9000	0.0273	0.0000
111	11.0000	-0.0515	0.0000
112	12.1000	-0.0498	0.0000
113	13.2000	-0.0469	0.0000
114	14.3000	-0.0429	0.0000
115	15.4000	-0.0378	0.0001
116	16.5000	-0.0320	0.0001
117	17.6000	-0.0296	0.0001
118	18.7000	-0.0206	0.0001
119	19.8000	-0.0134	0.0001
120	20.9000	-0.0070	0.0001
121	22.0000	0.0000	0.0001
1121	22.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	0.0073	0.0001
123	24.8000	0.0132	0.0000
124	26.2000	0.0161	0.0000
125	27.6000	0.0179	0.0000
126	29.0000	0.0152	0.0000
127	30.4000	0.0186	0.0000
128	31.8000	0.0218	0.0000
129	33.2000	0.0248	0.0000
130	34.6000	0.0275	0.0000
131	36.0000	0.0297	0.0000
132	37.4000	-0.0876	0.0000
133	38.8000	-0.0838	0.0000
134	40.2000	-0.0776	0.0001
135	41.6000	-0.0694	0.0001
136	43.0000	-0.0594	0.0001
137	44.4000	-0.0479	0.0001
138	45.8000	-0.0355	0.0001
139	47.2000	-0.0229	0.0001
140	48.6000	-0.0114	0.0001
141	50.0000	0.0000	0.0001
1141	50.0000	0.0000	0.0001
142	51.4000	0.0087	0.0001
143	52.8000	0.0168	0.0001
144	54.2000	0.0225	0.0000
145	55.6000	0.0268	0.0000
146	57.0000	0.0276	0.0000
147	58.4000	0.0143	0.0000
148	59.8000	0.0167	0.0000
149	61.2000	0.0190	0.0000
150	62.6000	0.0210	0.0000
151	64.0000	0.0227	0.0000
152	65.4000	-0.0875	0.0000
153	66.8000	-0.0837	0.0000
154	68.2000	-0.0774	0.0001
155	69.6000	-0.0691	0.0001
156	71.0000	-0.0590	0.0001
157	72.4000	-0.0475	0.0001
158	73.8000	-0.0352	0.0001
159	75.2000	-0.0227	0.0001
160	76.6000	-0.0112	0.0001
161	78.0000	0.0000	0.0001
1161	78.0000	0.0000	0.0001
162	79.1000	0.0068	0.0001
163	80.2000	0.0125	0.0001
164	81.3000	0.0170	0.0000
165	82.4000	0.0207	0.0000
166	83.5000	0.0234	0.0000
167	84.6000	0.0279	0.0000
168	85.7000	0.0265	0.0000
169	86.8000	0.0000	0.0000
170	87.9000	0.0000	0.0000
171	89.0000	0.0000	0.0000
172	90.1000	-0.0544	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ+
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0530	0.0000
174	92.3000	-0.0503	0.0000
175	93.4000	-0.0463	0.0000
176	94.5000	-0.0423	0.0001
177	95.6000	-0.0356	0.0001
178	96.7000	-0.0277	0.0001
179	97.8000	-0.0183	0.0001
180	98.9000	-0.0097	0.0001
181	100.0000	0.0000	0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY-
Envolvente de tren de cargas plano genérico. UY
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0022	0.0000
3	2.2000	-0.0043	0.0000
4	3.3000	-0.0064	0.0000
5	4.4000	-0.0082	0.0000
6	5.5000	-0.0098	0.0000
7	6.6000	-0.0111	0.0000
8	7.7000	-0.0122	0.0000
9	8.8000	-0.0129	0.0000
10	9.9000	-0.0132	0.0000
11	11.0000	-0.0133	0.0000
12	12.1000	-0.0130	0.0000
13	13.2000	-0.0124	0.0000
14	14.3000	-0.0114	0.0000
15	15.4000	-0.0102	0.0000
16	16.5000	-0.0088	0.0000
17	17.6000	-0.0072	0.0000
18	18.7000	-0.0054	0.0000
19	19.8000	-0.0036	0.0000
20	20.9000	-0.0018	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0035	0.0000
23	24.8000	-0.0074	0.0000
24	26.2000	-0.0114	0.0000
25	27.6000	-0.0152	0.0000
26	29.0000	-0.0188	0.0000
27	30.4000	-0.0220	0.0000
28	31.8000	-0.0246	0.0000
29	33.2000	-0.0266	0.0000
30	34.6000	-0.0279	0.0000
31	36.0000	-0.0283	0.0000
32	37.4000	-0.0280	0.0000
33	38.8000	-0.0268	0.0000
34	40.2000	-0.0250	0.0000
35	41.6000	-0.0224	0.0000
36	43.0000	-0.0193	0.0000
37	44.4000	-0.0157	0.0000
38	45.8000	-0.0118	0.0000
39	47.2000	-0.0078	0.0000
40	48.6000	-0.0038	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0038	0.0000
43	52.8000	-0.0078	0.0000
44	54.2000	-0.0118	0.0000
45	55.6000	-0.0157	0.0000
46	57.0000	-0.0193	0.0000
47	58.4000	-0.0224	0.0000
48	59.8000	-0.0250	0.0000
49	61.2000	-0.0269	0.0000
50	62.6000	-0.0280	0.0000
51	64.0000	-0.0283	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	-0.0279	0.0000
53	66.8000	-0.0266	0.0000
54	68.2000	-0.0246	0.0000
55	69.6000	-0.0220	0.0000
56	71.0000	-0.0188	0.0000
57	72.4000	-0.0152	0.0000
58	73.8000	-0.0114	0.0000
59	75.2000	-0.0074	0.0000
60	76.6000	-0.0035	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0018	0.0000
63	80.2000	-0.0036	0.0000
64	81.3000	-0.0054	0.0000
65	82.4000	-0.0072	0.0000
66	83.5000	-0.0088	0.0000
67	84.6000	-0.0102	0.0000
68	85.7000	-0.0114	0.0000
69	86.8000	-0.0124	0.0000
70	87.9000	-0.0130	0.0000
71	89.0000	-0.0133	0.0000
72	90.1000	-0.0133	0.0000
73	91.2000	-0.0129	0.0000
74	92.3000	-0.0122	0.0000
75	93.4000	-0.0111	0.0000
76	94.5000	-0.0098	0.0000
77	95.6000	-0.0082	0.0000
78	96.7000	-0.0064	0.0000
79	97.8000	-0.0043	0.0000
80	98.9000	-0.0022	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000
102	1.1000	-0.0098	-0.0001
103	2.2000	-0.0193	-0.0001
104	3.3000	-0.0280	-0.0001
105	4.4000	-0.0359	-0.0001
106	5.5000	-0.0427	-0.0001
107	6.6000	-0.0483	0.0000
108	7.7000	-0.0525	0.0000
109	8.8000	-0.0553	0.0000
110	9.9000	-0.0566	0.0000
111	11.0000	-0.0566	0.0000
112	12.1000	-0.0550	0.0000
113	13.2000	-0.0522	0.0000
114	14.3000	-0.0481	0.0000
115	15.4000	-0.0428	0.0001
116	16.5000	-0.0366	0.0001
117	17.6000	-0.0296	0.0001
118	18.7000	-0.0221	0.0001
119	19.8000	-0.0145	0.0001
120	20.9000	-0.0070	0.0001
121	22.0000	0.0000	0.0000
1121	22.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0112	-0.0001
123	24.8000	-0.0235	-0.0001
124	26.2000	-0.0363	-0.0001
125	27.6000	-0.0487	-0.0001
126	29.0000	-0.0601	-0.0001
127	30.4000	-0.0700	-0.0001
128	31.8000	-0.0781	-0.0001
129	33.2000	-0.0841	0.0000
130	34.6000	-0.0879	0.0000
131	36.0000	-0.0892	0.0000
132	37.4000	-0.0880	0.0000
133	38.8000	-0.0844	0.0000
134	40.2000	-0.0785	0.0001
135	41.6000	-0.0705	0.0001
136	43.0000	-0.0606	0.0001
137	44.4000	-0.0491	0.0001
138	45.8000	-0.0367	0.0001
139	47.2000	-0.0239	0.0001
140	48.6000	-0.0114	0.0001
141	50.0000	0.0000	0.0000
1141	50.0000	0.0000	0.0000
142	51.4000	-0.0114	-0.0001
143	52.8000	-0.0239	-0.0001
144	54.2000	-0.0367	-0.0001
145	55.6000	-0.0491	-0.0001
146	57.0000	-0.0606	-0.0001
147	58.4000	-0.0705	-0.0001
148	59.8000	-0.0785	-0.0001
149	61.2000	-0.0844	0.0000
150	62.6000	-0.0880	0.0000
151	64.0000	-0.0892	0.0000
152	65.4000	-0.0879	0.0000
153	66.8000	-0.0841	0.0000
154	68.2000	-0.0781	0.0001
155	69.6000	-0.0700	0.0001
156	71.0000	-0.0601	0.0001
157	72.4000	-0.0487	0.0001
158	73.8000	-0.0363	0.0001
159	75.2000	-0.0235	0.0001
160	76.6000	-0.0112	0.0001
161	78.0000	0.0000	0.0000
1161	78.0000	0.0000	0.0000
162	79.1000	-0.0070	-0.0001
163	80.2000	-0.0145	-0.0001
164	81.3000	-0.0221	-0.0001
165	82.4000	-0.0296	-0.0001
166	83.5000	-0.0366	-0.0001
167	84.6000	-0.0428	-0.0001
168	85.7000	-0.0481	0.0000
169	86.8000	-0.0522	0.0000
170	87.9000	-0.0550	0.0000
171	89.0000	-0.0566	0.0000
172	90.1000	-0.0566	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.UY-

Envolvente de tren de cargas plano genérico. UY

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	-0.0553	0.0000
174	92.3000	-0.0525	0.0000
175	93.4000	-0.0483	0.0000
176	94.5000	-0.0427	0.0001
177	95.6000	-0.0359	0.0001
178	96.7000	-0.0280	0.0001
179	97.8000	-0.0193	0.0001
180	98.9000	-0.0098	0.0001
181	100.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
1	0.0000	0.0000	0.0000
2	1.1000	-0.0019	0.0000
3	2.2000	-0.0037	0.0000
4	3.3000	-0.0055	0.0000
5	4.4000	-0.0078	0.0000
6	5.5000	-0.0084	0.0000
7	6.6000	-0.0096	0.0000
8	7.7000	-0.0105	0.0000
9	8.8000	-0.0125	0.0000
10	9.9000	0.0000	0.0000
11	11.0000	0.0000	0.0000
12	12.1000	0.0000	0.0000
13	13.2000	0.0000	0.0000
14	14.3000	0.0000	0.0000
15	15.4000	0.0100	0.0000
16	16.5000	0.0091	0.0000
17	17.6000	0.0079	0.0000
18	18.7000	0.0064	0.0000
19	19.8000	0.0046	0.0000
20	20.9000	0.0025	0.0000
21	22.0000	0.0000	0.0000
1021	22.0000	0.0000	0.0000
22	23.4000	-0.0035	0.0000
23	24.8000	-0.0074	0.0000
24	26.2000	-0.0114	0.0000
25	27.6000	-0.0152	0.0000
26	29.0000	-0.0188	0.0000
27	30.4000	-0.0220	0.0000
28	31.8000	-0.0246	0.0000
29	33.2000	-0.0082	0.0000
30	34.6000	-0.0277	0.0000
31	36.0000	0.0000	0.0000
32	37.4000	0.0000	0.0000
33	38.8000	0.0081	0.0000
34	40.2000	0.0065	0.0000
35	41.6000	0.0057	0.0000
36	43.0000	0.0048	0.0000
37	44.4000	0.0038	0.0000
38	45.8000	0.0088	0.0000
39	47.2000	0.0063	0.0000
40	48.6000	0.0034	0.0000
41	50.0000	0.0000	0.0000
1041	50.0000	0.0000	0.0000
42	51.4000	-0.0038	0.0000
43	52.8000	-0.0078	0.0000
44	54.2000	-0.0118	0.0000
45	55.6000	-0.0157	0.0000
46	57.0000	-0.0193	0.0000
47	58.4000	-0.0224	0.0000
48	59.8000	-0.0250	0.0000
49	61.2000	-0.0048	0.0000
50	62.6000	-0.0279	0.0000
51	64.0000	0.0000	0.0000

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
52	65.4000	0.0122	0.0000
53	66.8000	0.0112	0.0000
54	68.2000	0.0100	0.0000
55	69.6000	0.0087	0.0000
56	71.0000	0.0072	0.0000
57	72.4000	0.0027	0.0000
58	73.8000	0.0020	0.0000
59	75.2000	0.0027	0.0000
60	76.6000	0.0013	0.0000
61	78.0000	0.0000	0.0000
1061	78.0000	0.0000	0.0000
62	79.1000	-0.0017	0.0000
63	80.2000	-0.0036	0.0000
64	81.3000	-0.0054	0.0000
65	82.4000	-0.0071	0.0000
66	83.5000	-0.0087	0.0000
67	84.6000	-0.0102	0.0000
68	85.7000	-0.0114	0.0000
69	86.8000	-0.0123	0.0000
70	87.9000	0.0000	0.0000
71	89.0000	0.0000	0.0000
72	90.1000	0.0000	0.0000
73	91.2000	0.0093	0.0000
74	92.3000	0.0085	0.0000
75	93.4000	0.0076	0.0000
76	94.5000	0.0065	0.0000
77	95.6000	0.0054	0.0000
78	96.7000	0.0041	0.0000
79	97.8000	0.0012	0.0000
80	98.9000	0.0006	0.0000
81	100.0000	0.0000	0.0000
101	0.0000	0.0000	-0.0001
102	1.1000	-0.0096	-0.0001
103	2.2000	-0.0180	-0.0001
104	3.3000	-0.0275	-0.0001
105	4.4000	-0.0353	-0.0001
106	5.5000	-0.0421	-0.0001
107	6.6000	-0.0447	0.0000
108	7.7000	-0.0484	0.0000
109	8.8000	-0.0508	0.0000
110	9.9000	-0.0535	0.0000
111	11.0000	0.0000	0.0000
112	12.1000	0.0000	0.0000
113	13.2000	0.0000	0.0000
114	14.3000	0.0289	0.0000
115	15.4000	0.0277	0.0000
116	16.5000	0.0256	0.0000
117	17.6000	0.0226	0.0000
118	18.7000	0.0186	0.0000
119	19.8000	0.0135	-0.0001
120	20.9000	0.0074	-0.0001
121	22.0000	0.0000	-0.0001
1121	22.0000	0.0000	-0.0001

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ-
Envolvente de tren de cargas plano genérico. GZ
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre
Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
122	23.4000	-0.0112	-0.0001
123	24.8000	-0.0234	-0.0001
124	26.2000	-0.0362	-0.0001
125	27.6000	-0.0486	-0.0001
126	29.0000	-0.0600	-0.0001
127	30.4000	-0.0647	-0.0001
128	31.8000	-0.0781	-0.0001
129	33.2000	-0.0719	0.0000
130	34.6000	-0.0878	0.0000
131	36.0000	0.0194	0.0000
132	37.4000	0.0180	0.0000
133	38.8000	0.0191	0.0000
134	40.2000	0.0152	0.0000
135	41.6000	0.0122	0.0000
136	43.0000	0.0100	0.0000
137	44.4000	0.0273	0.0000
138	45.8000	0.0229	0.0000
139	47.2000	0.0170	-0.0001
140	48.6000	0.0094	-0.0001
141	50.0000	0.0000	-0.0001
1141	50.0000	0.0000	-0.0001
142	51.4000	-0.0113	-0.0001
143	52.8000	-0.0238	-0.0001
144	54.2000	-0.0366	-0.0001
145	55.6000	-0.0491	-0.0001
146	57.0000	-0.0605	-0.0001
147	58.4000	-0.0672	-0.0001
148	59.8000	-0.0785	-0.0001
149	61.2000	-0.0713	0.0000
150	62.6000	-0.0880	0.0000
151	64.0000	0.0118	0.0000
152	65.4000	0.0252	0.0000
153	66.8000	0.0228	0.0000
154	68.2000	0.0200	0.0000
155	69.6000	0.0171	0.0000
156	71.0000	0.0140	0.0000
157	72.4000	0.0109	0.0000
158	73.8000	0.0173	0.0000
159	75.2000	0.0129	0.0000
160	76.6000	0.0071	-0.0001
161	78.0000	0.0000	-0.0001
1161	78.0000	0.0000	-0.0001
162	79.1000	-0.0069	-0.0001
163	80.2000	-0.0137	-0.0001
164	81.3000	-0.0211	-0.0001
165	82.4000	-0.0294	-0.0001
166	83.5000	-0.0350	-0.0001
167	84.6000	-0.0410	-0.0001
168	85.7000	-0.0461	0.0000
169	86.8000	-0.0224	0.0000
170	87.9000	-0.0192	0.0000
171	89.0000	0.0262	0.0000
172	90.1000	0.0102	0.0000

Programa DINTEL PACADAR S.A.
TRENLA2.EnvTrenGen.GZ-

CÁLCULO DE DESPLAZAMIENTOS

Hipótesis de cálculo:
TRENLA2.EnvTrenGen.GZ-

Envolvente de tren de cargas plano genérico. GZ

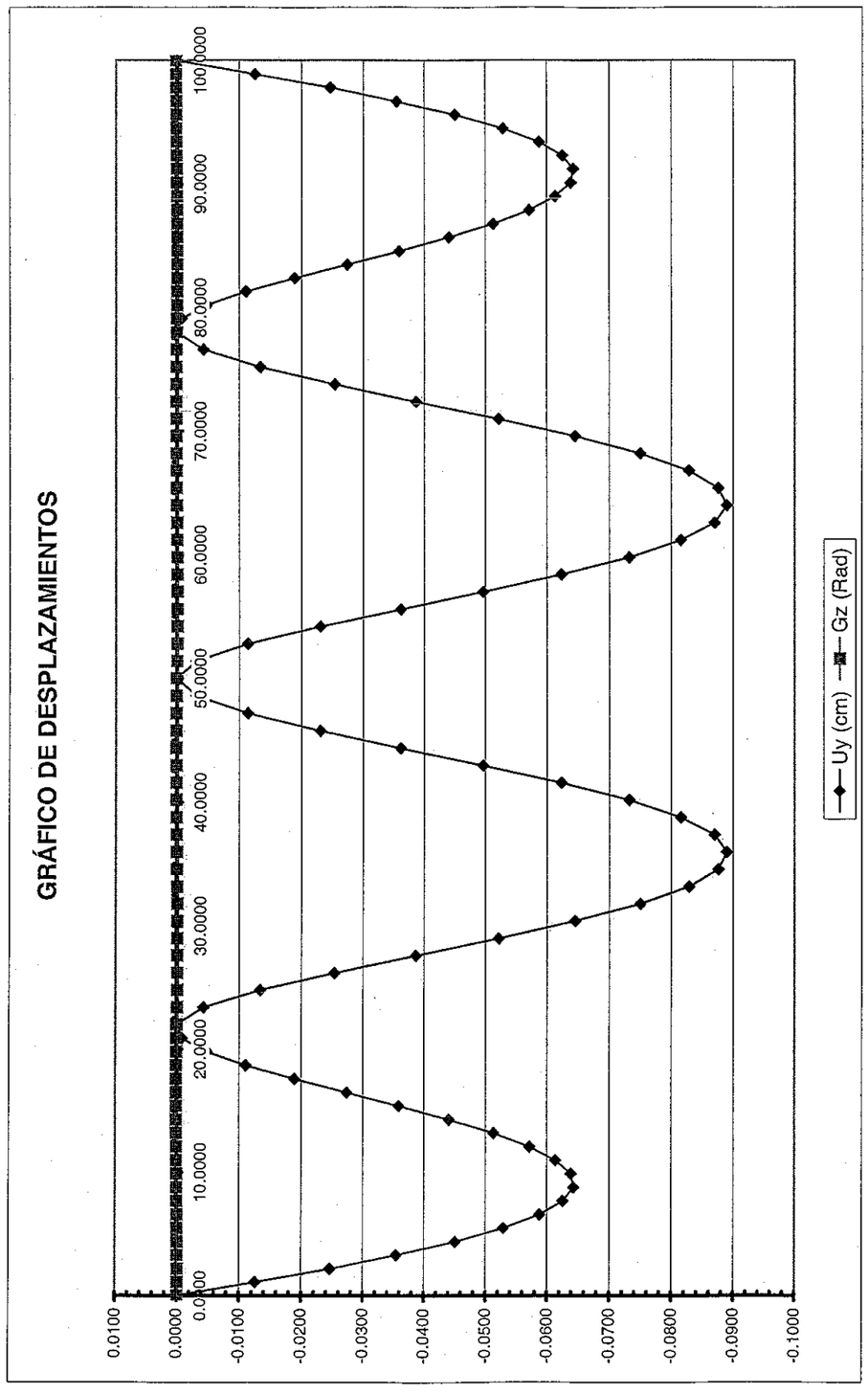
[0; 1]TRENLA2.PaseoTren.Nudo101.Pos2.Mx- + [0; 1]TRENLA2.PaseoTre

Coef. exc:

Nudo	X	Uy (cm)	Gz (Rad)
173	91.2000	0.0234	0.0000
174	92.3000	0.0213	0.0000
175	93.4000	0.0208	0.0000
176	94.5000	0.0163	0.0000
177	95.6000	0.0133	0.0000
178	96.7000	0.0102	0.0000
179	97.8000	0.0069	0.0000
180	98.9000	0.0035	0.0000
181	100.0000	0.0000	0.0000

23/09/03

Programa DINTEL PACADAR S.A.
PPVEI



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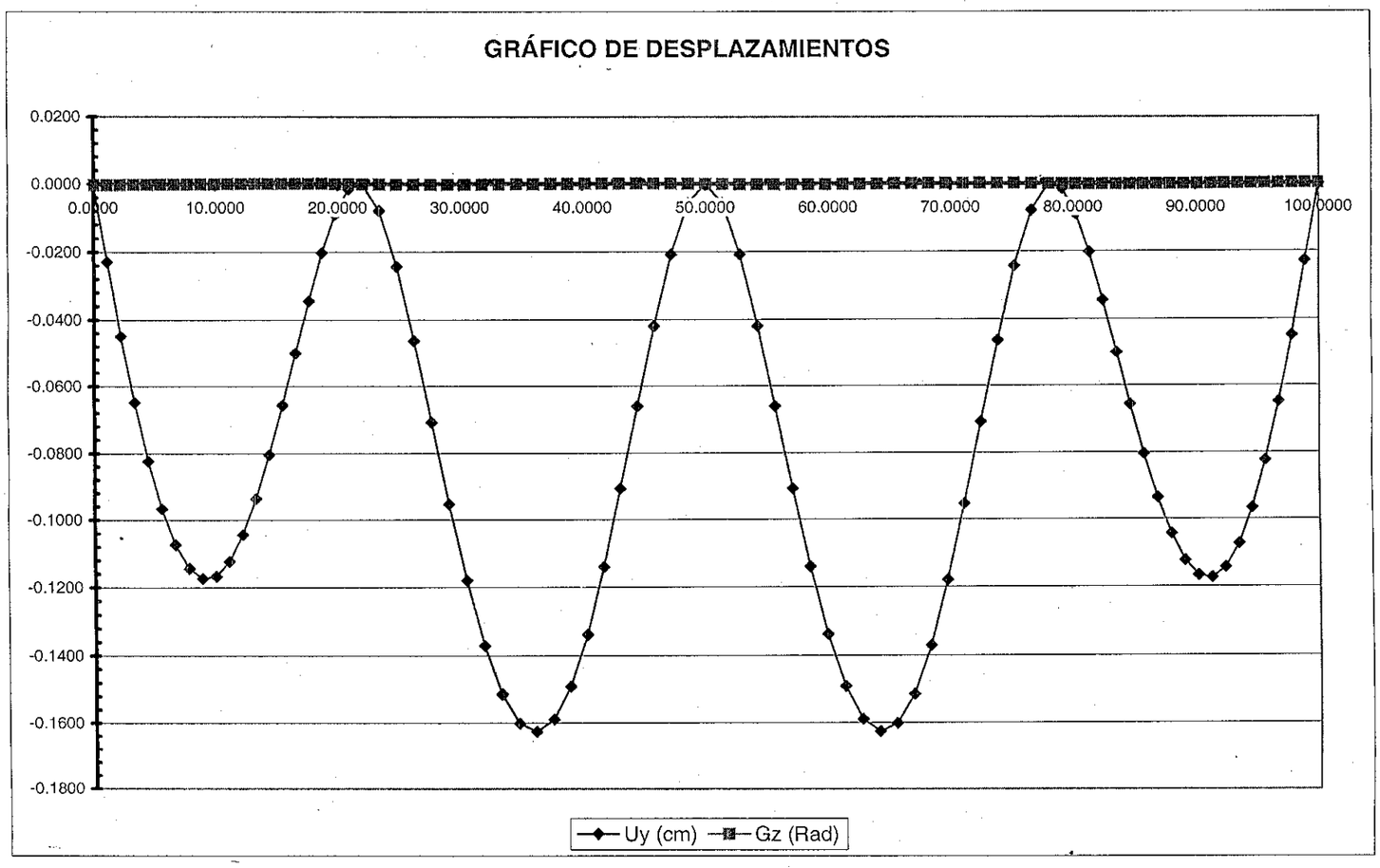
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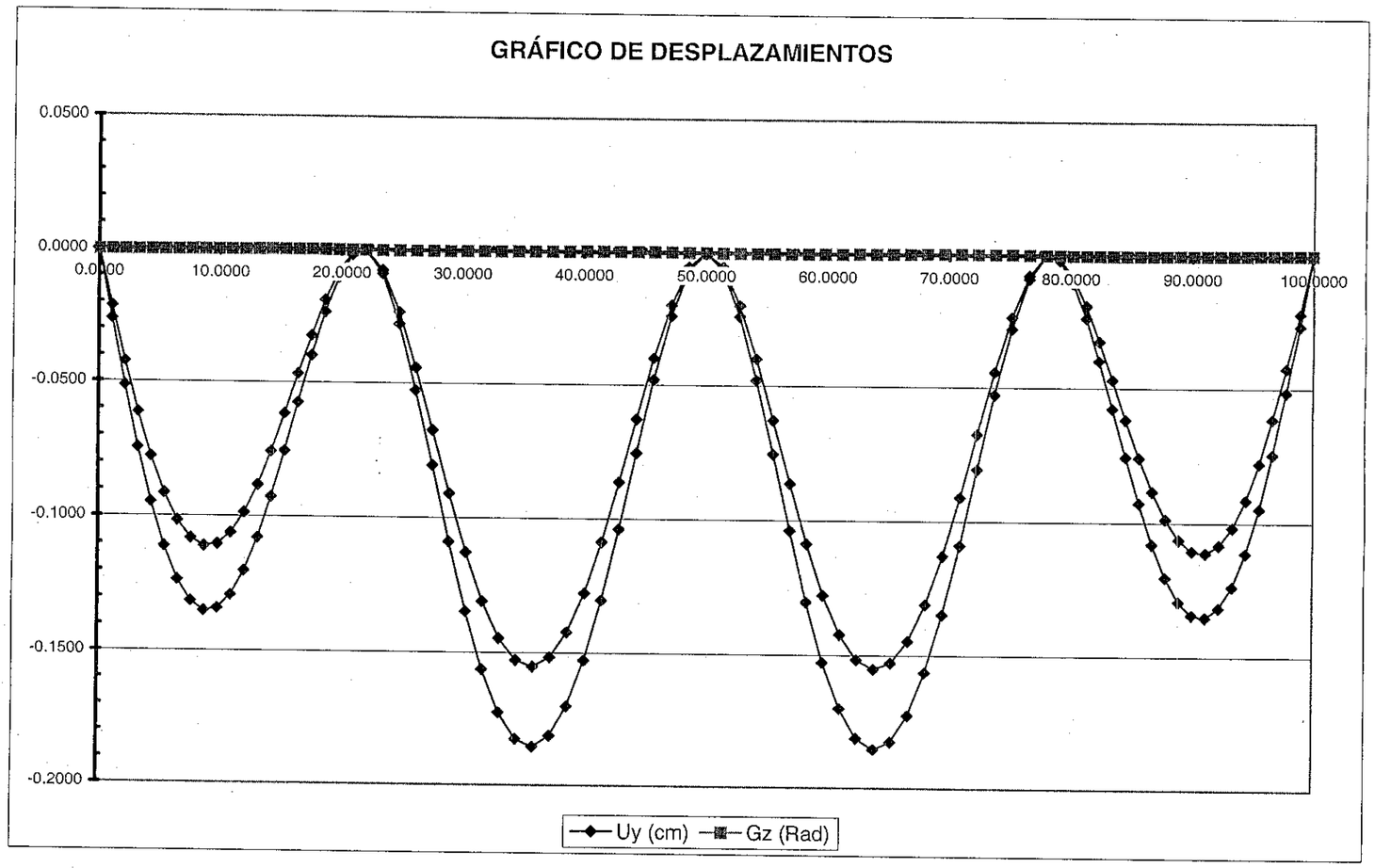
Uy (cm)
Gz (Rad)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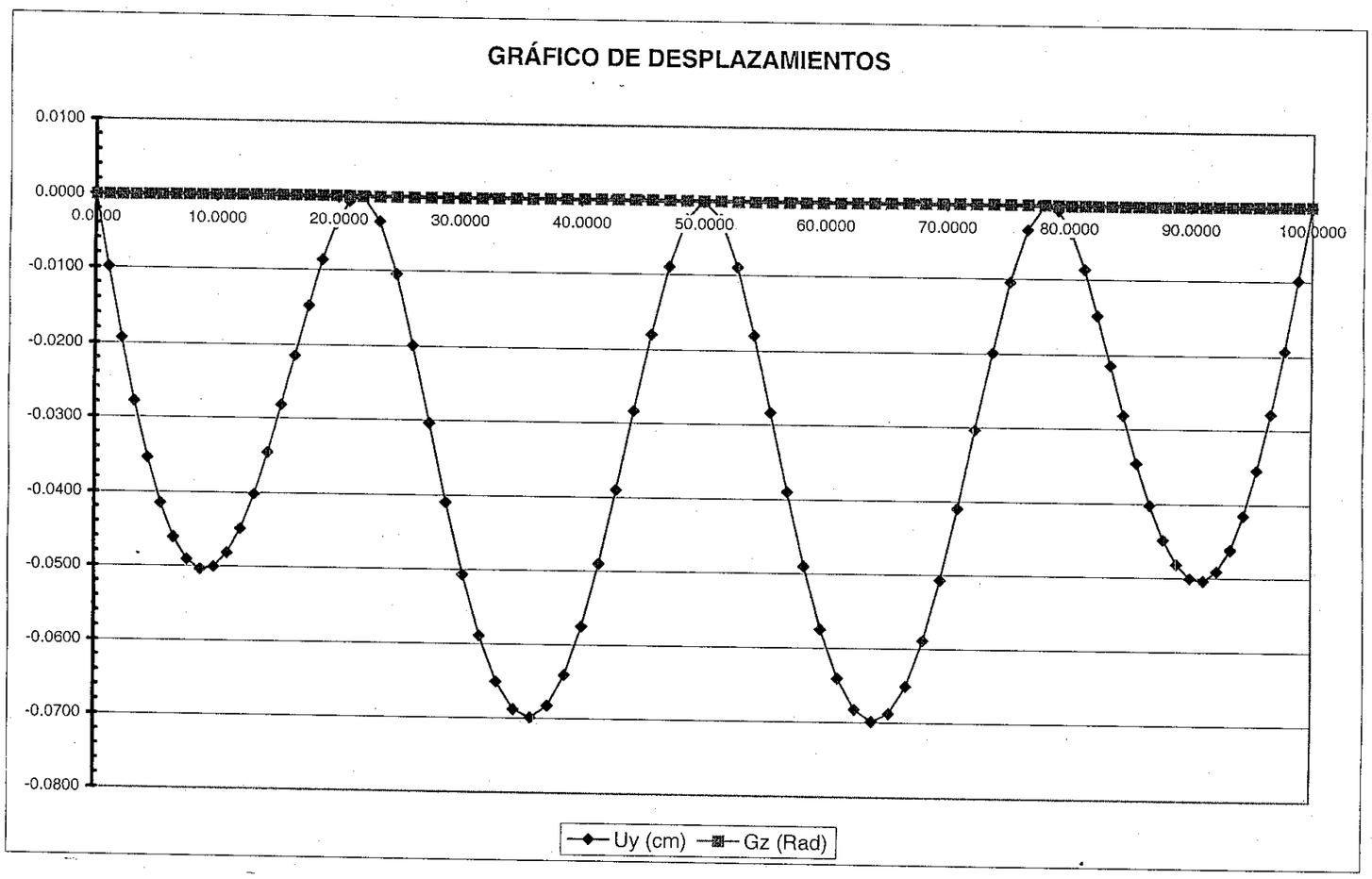
Uy (cm)
Gz (Rad)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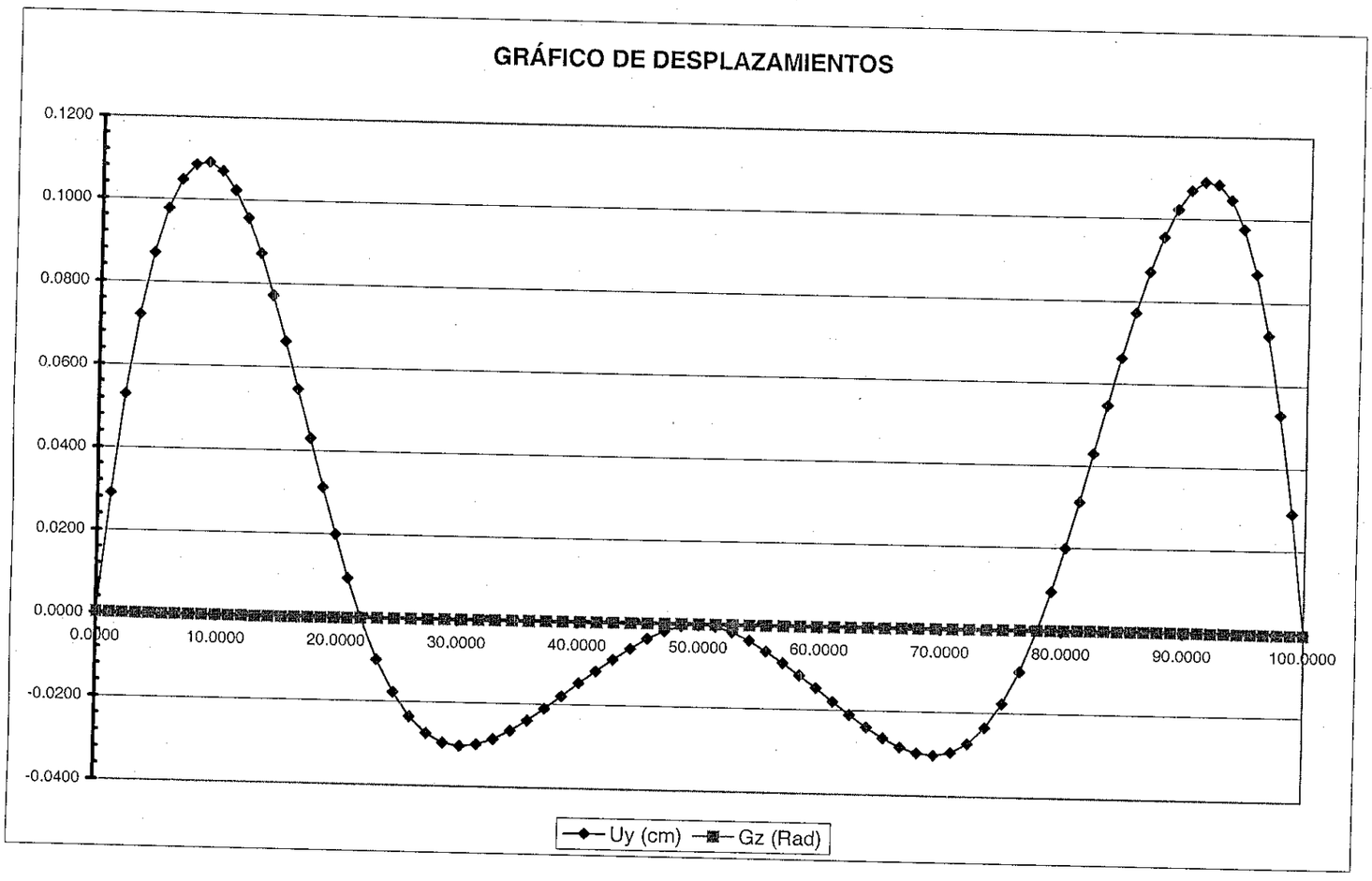
Uy (cm)
Gz (Rad)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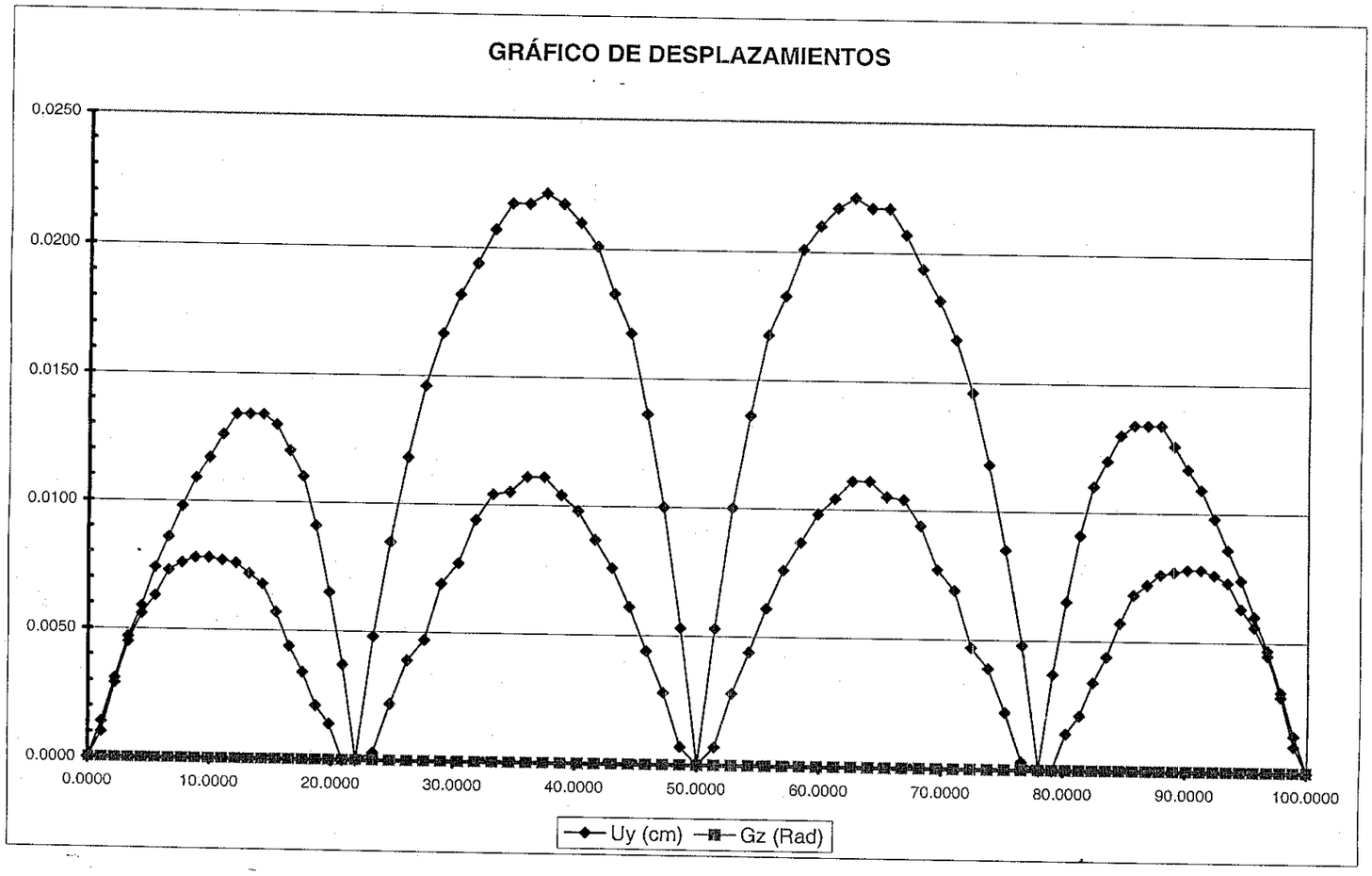
Uy (cm)
Gz (Rad)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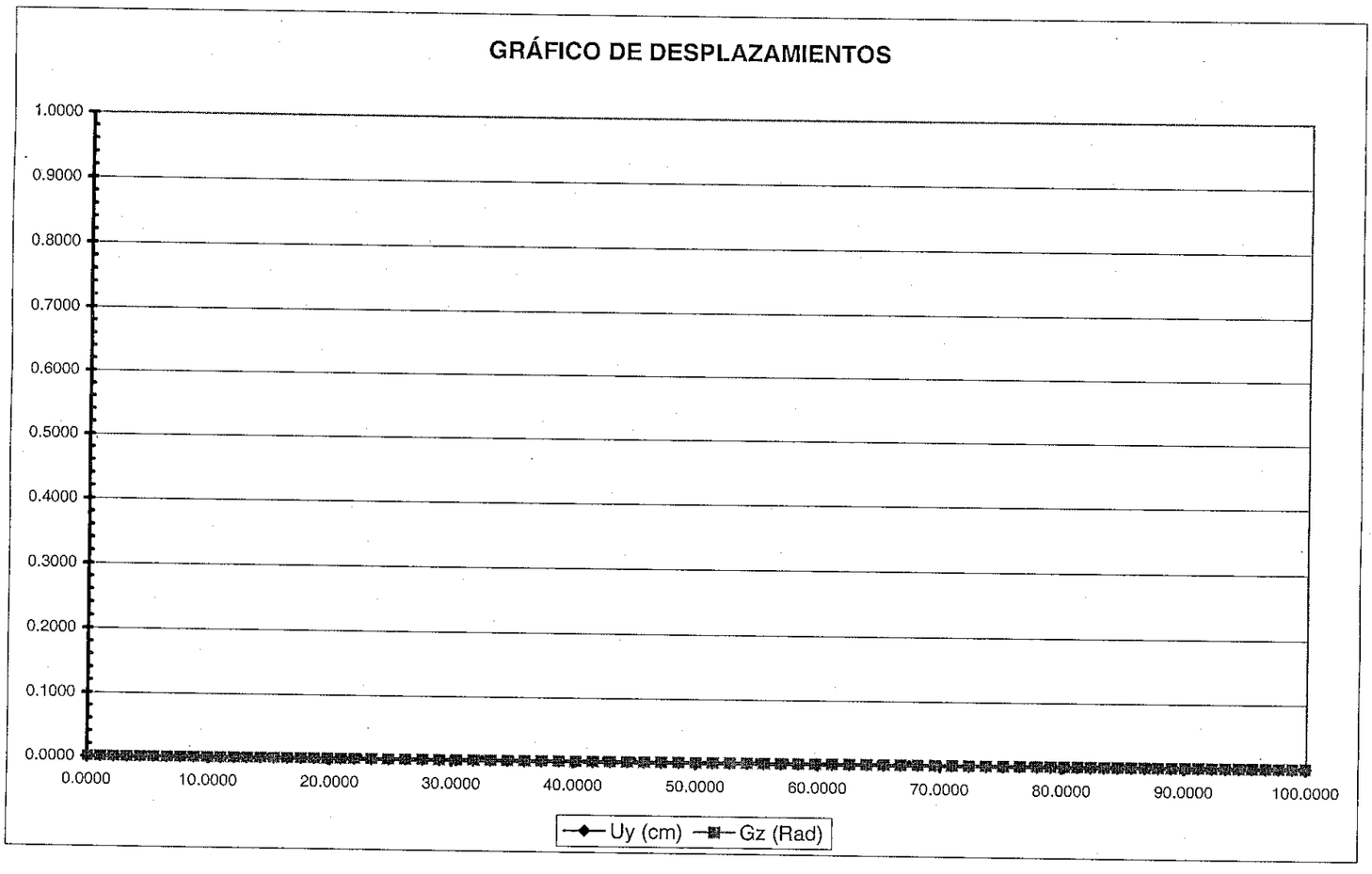
Uy (cm)
Gz (Rad)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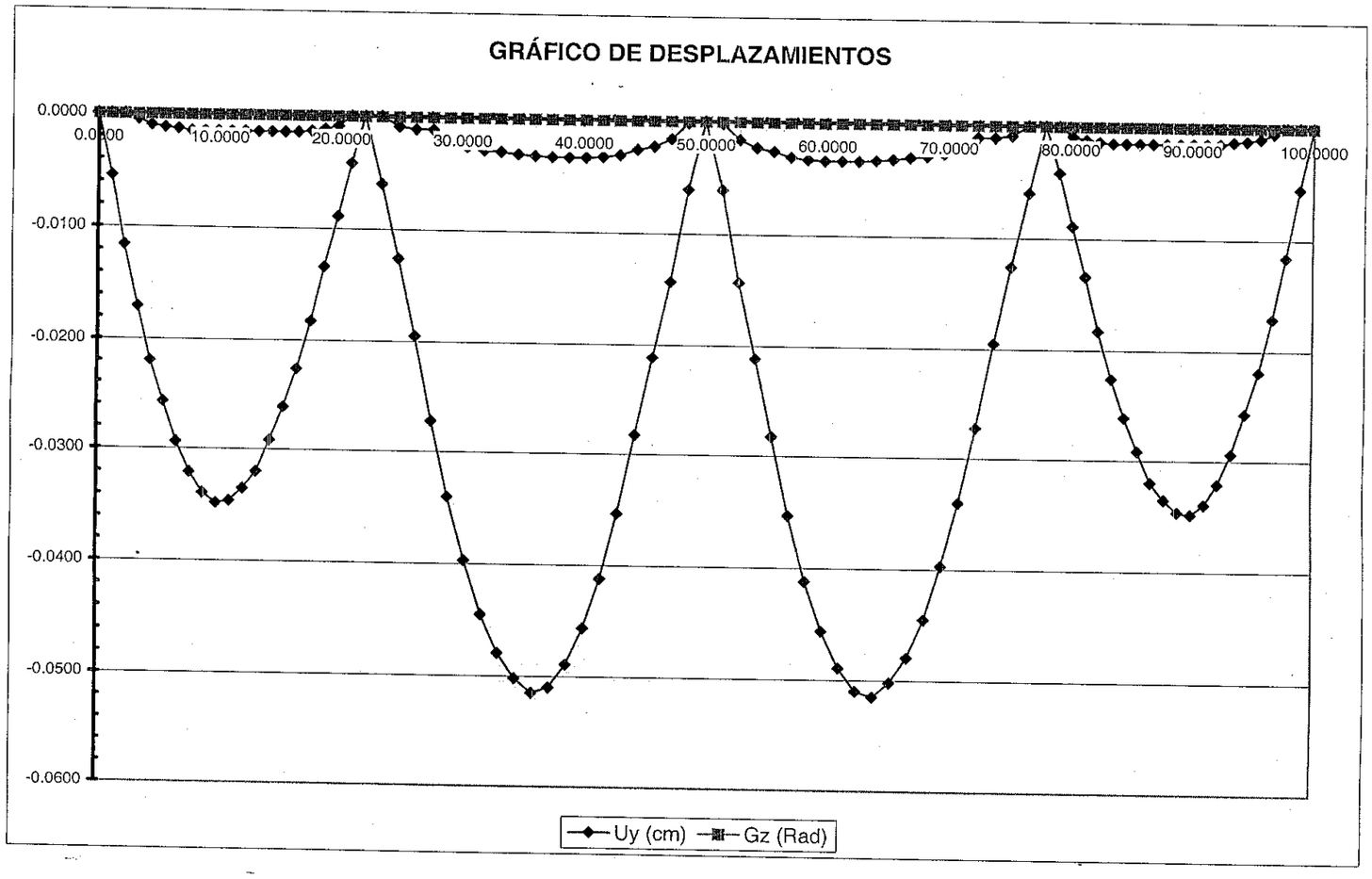
Uy (cm)
Gz (Rad)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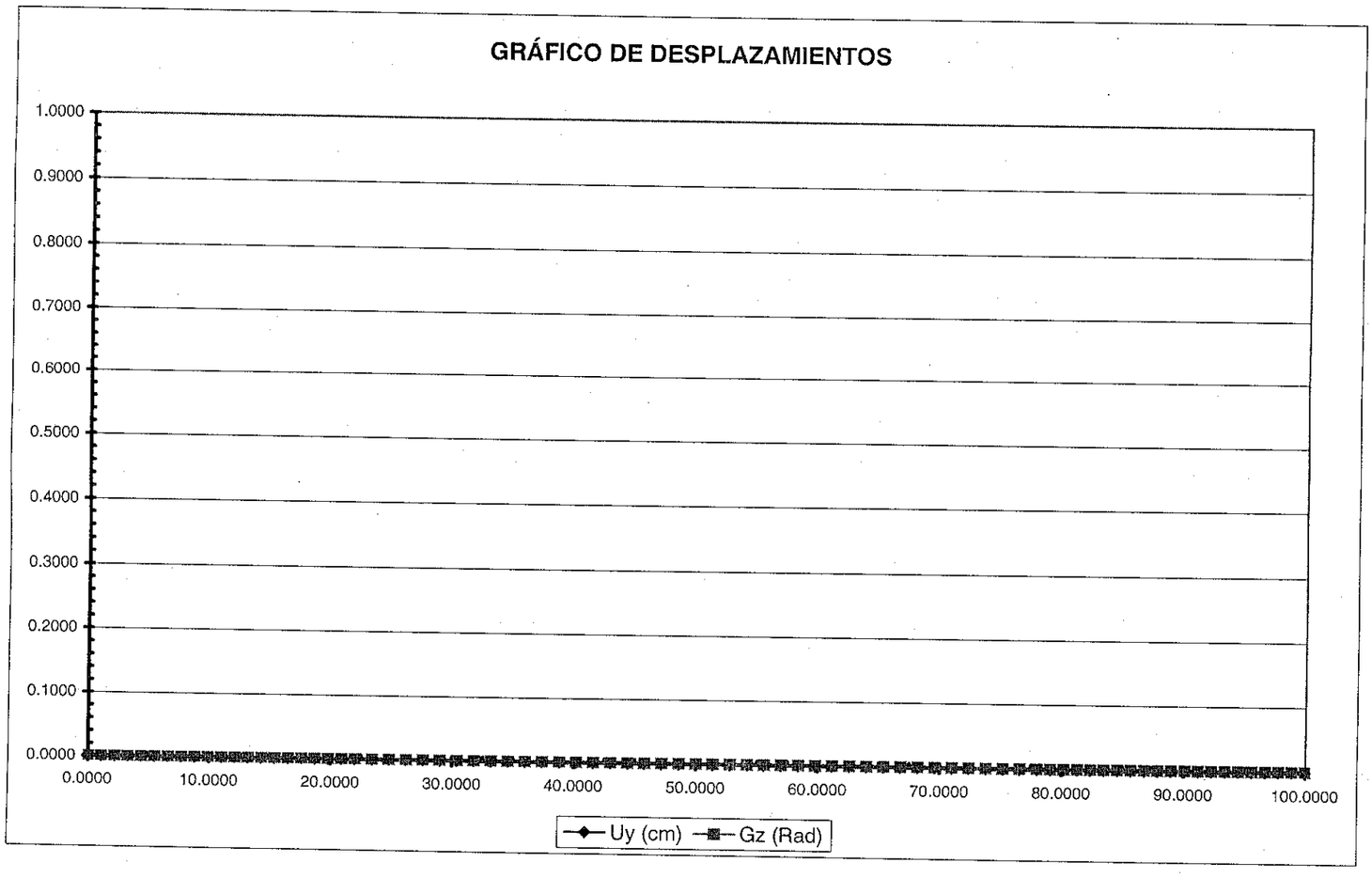
Uy (cm)
Gz (Rad)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60.0000
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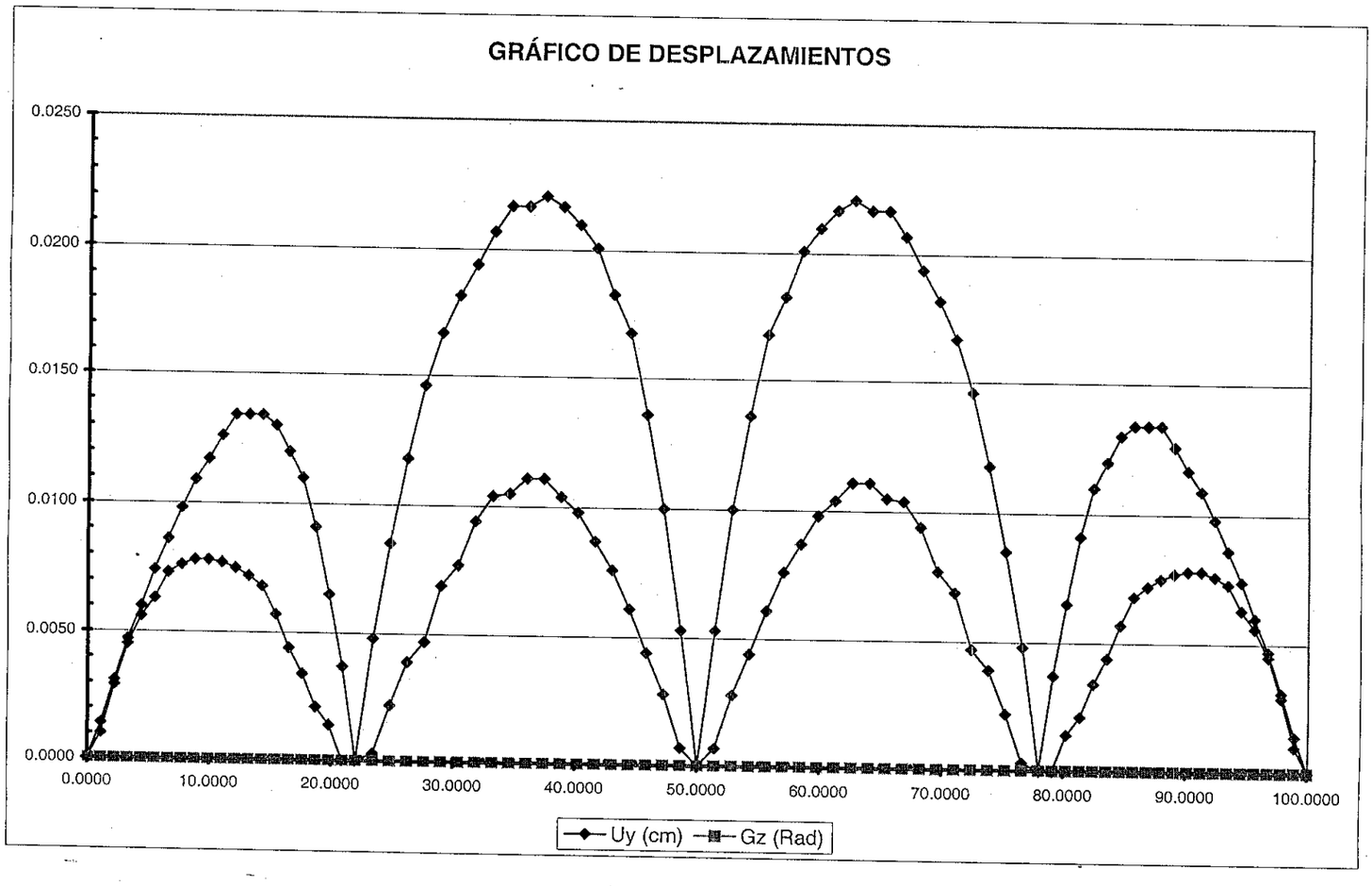
Uy (cm)
Gz (Rad)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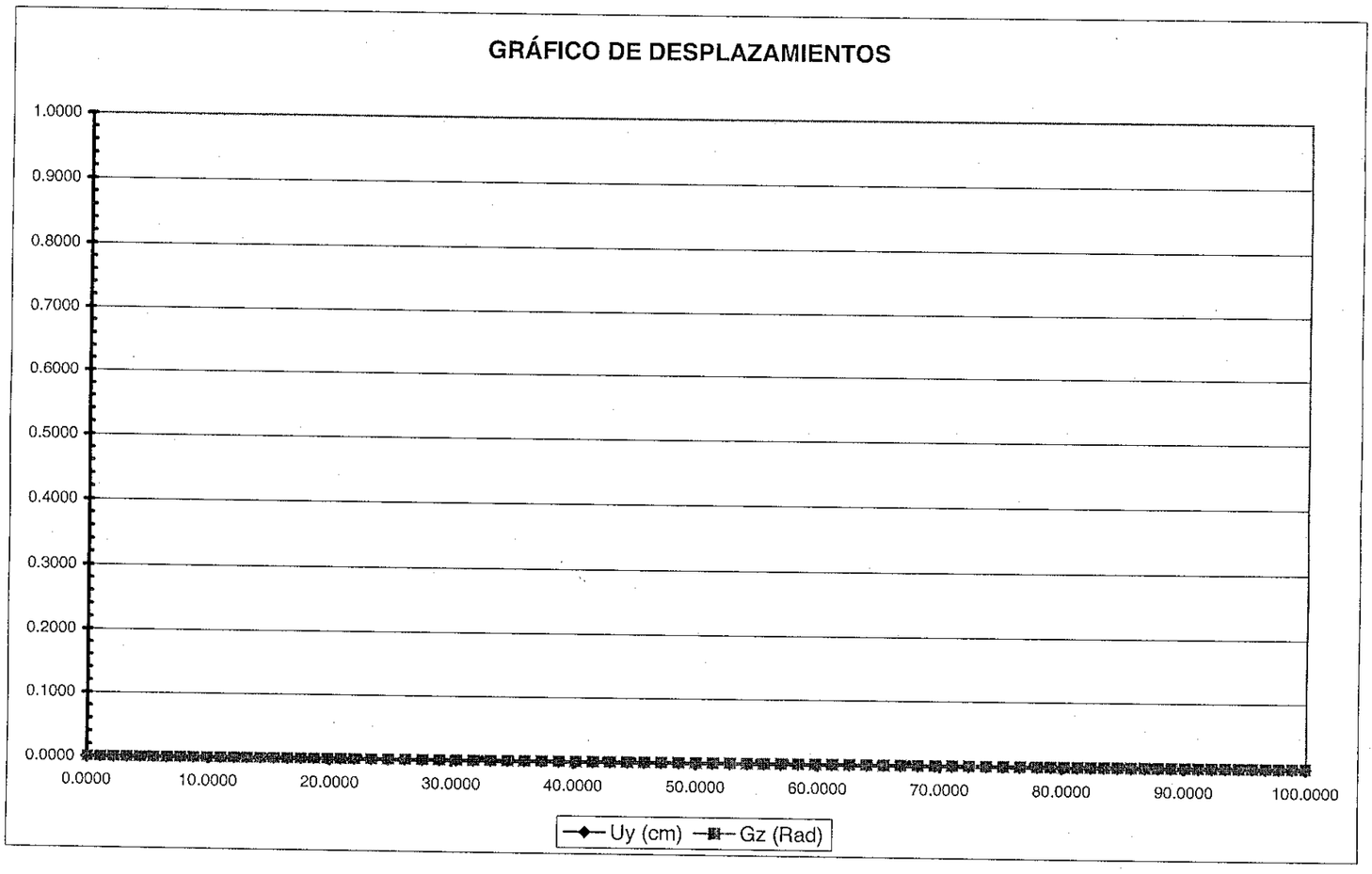
Uy (cm)
Gz (Rad)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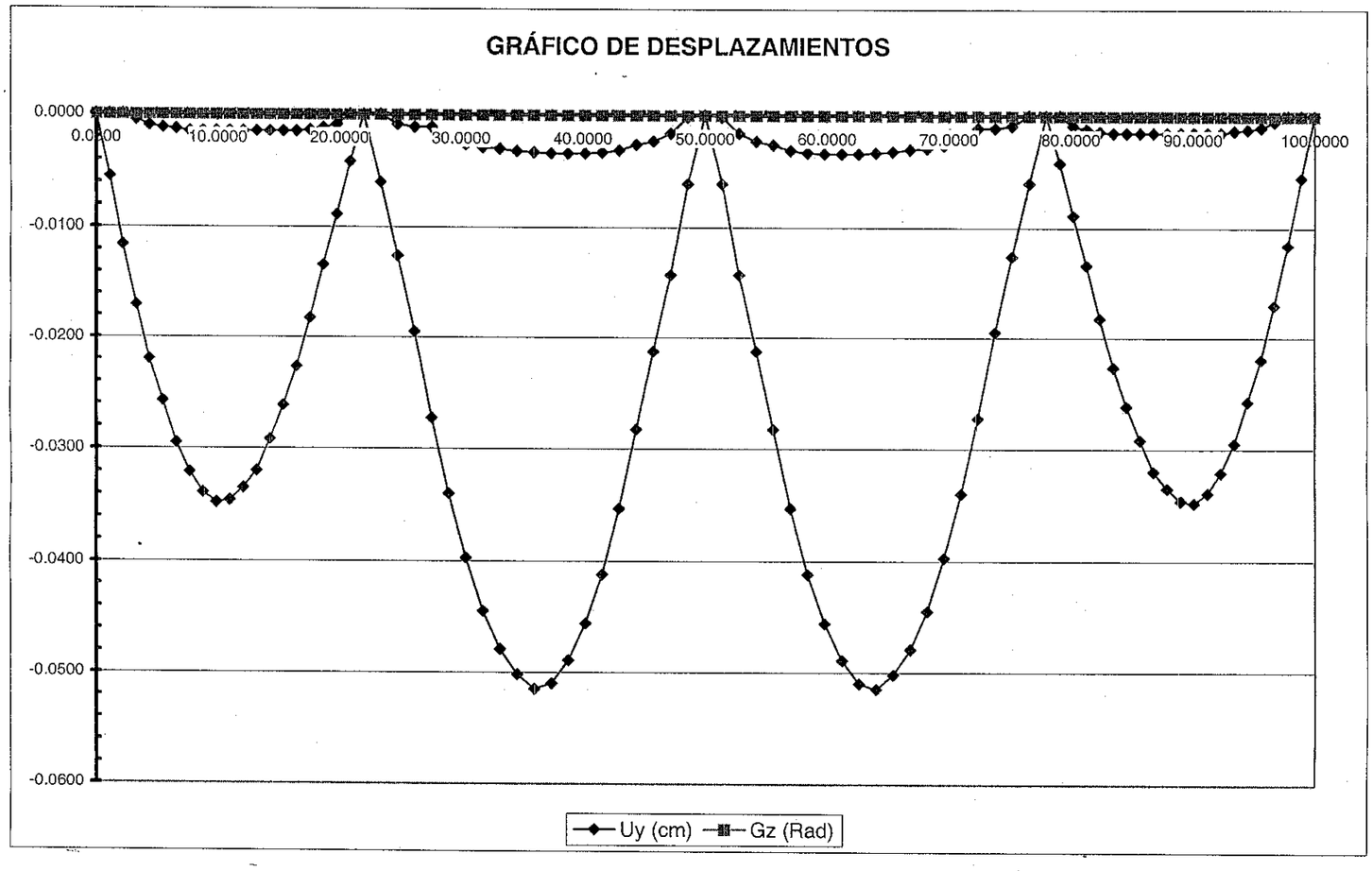
Uy (cm)
Gz (Rad)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10.0000
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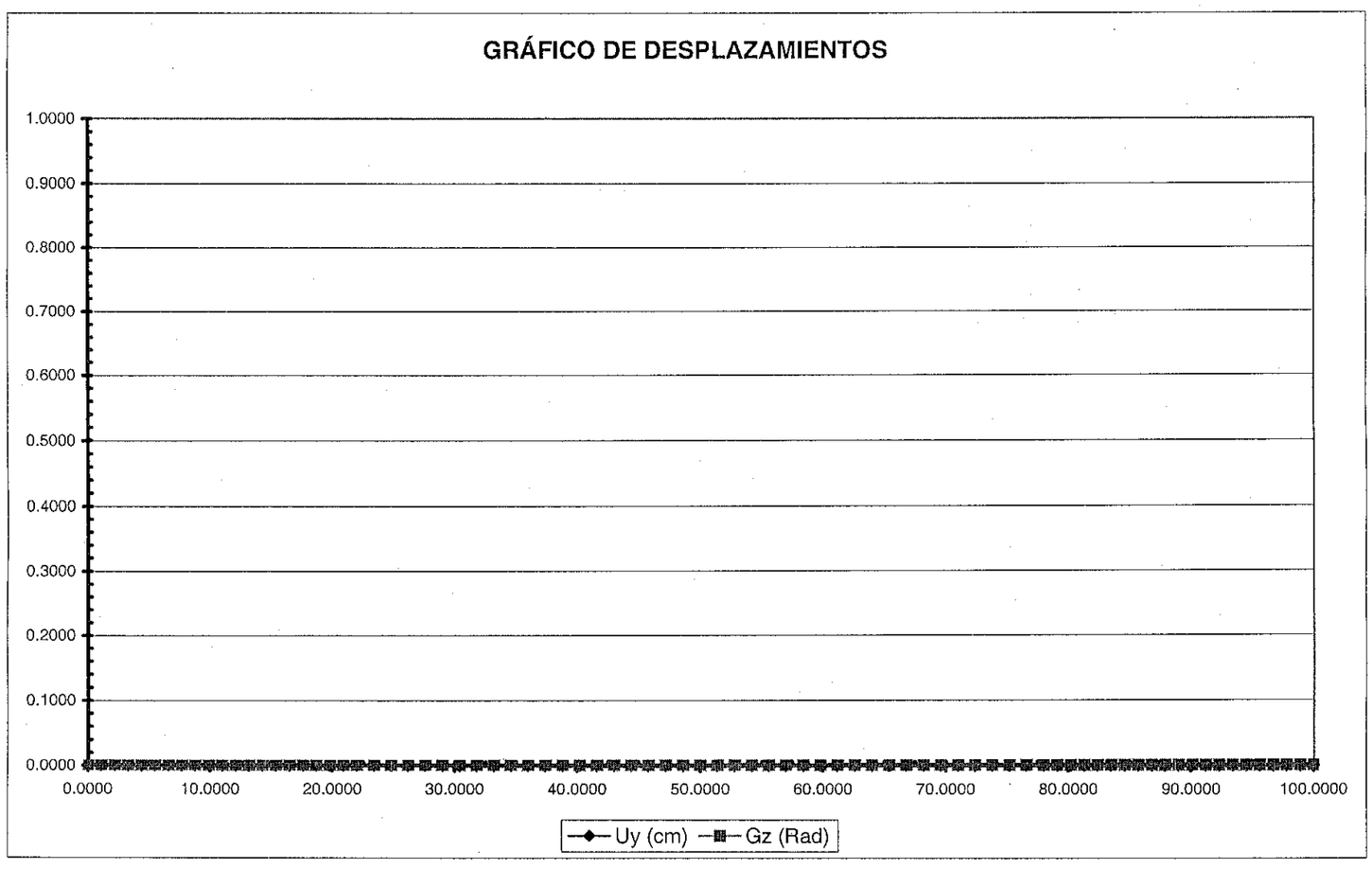
Uy (cm)
Gz (Rad)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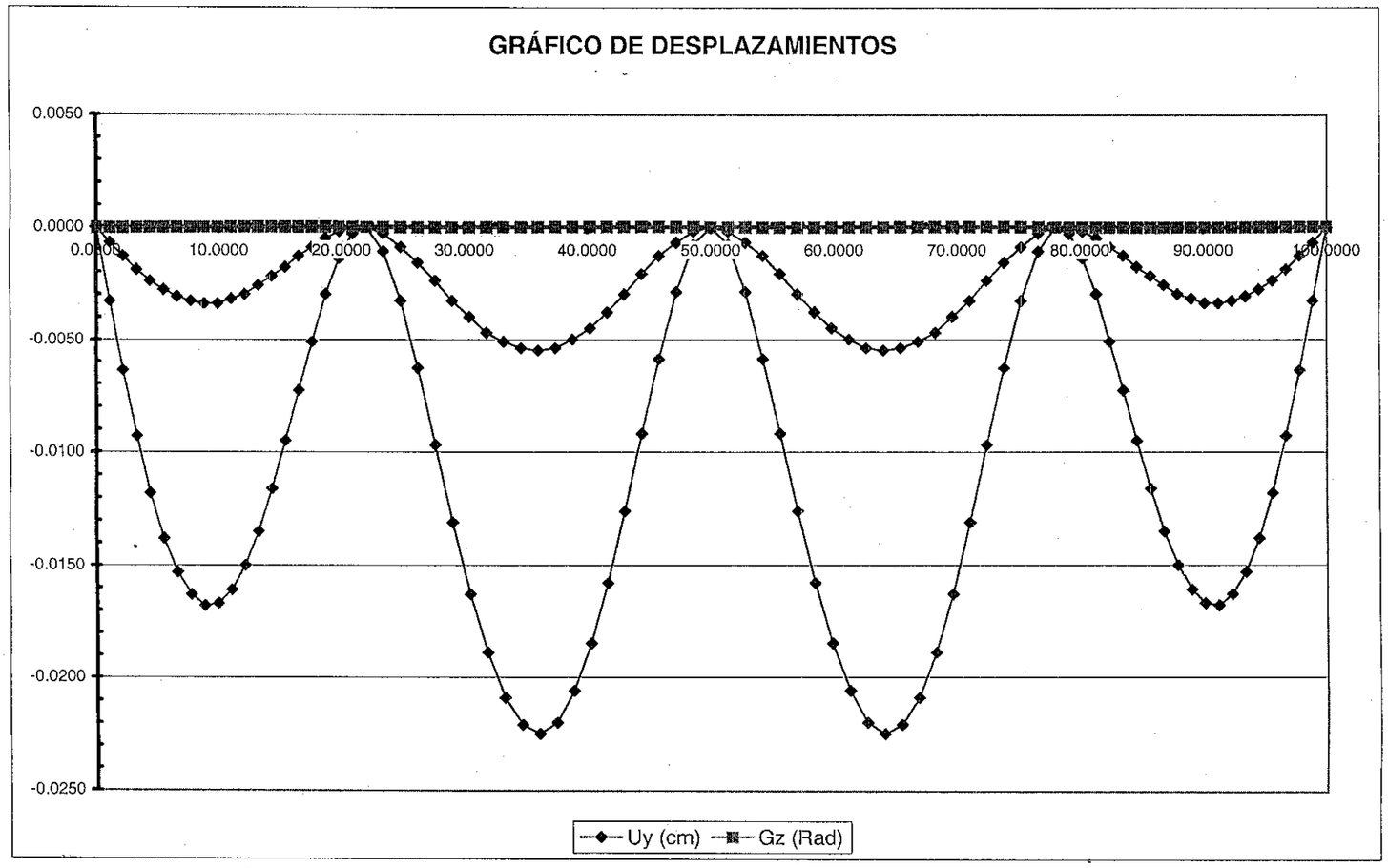
Uy (cm)
Gz (Rad)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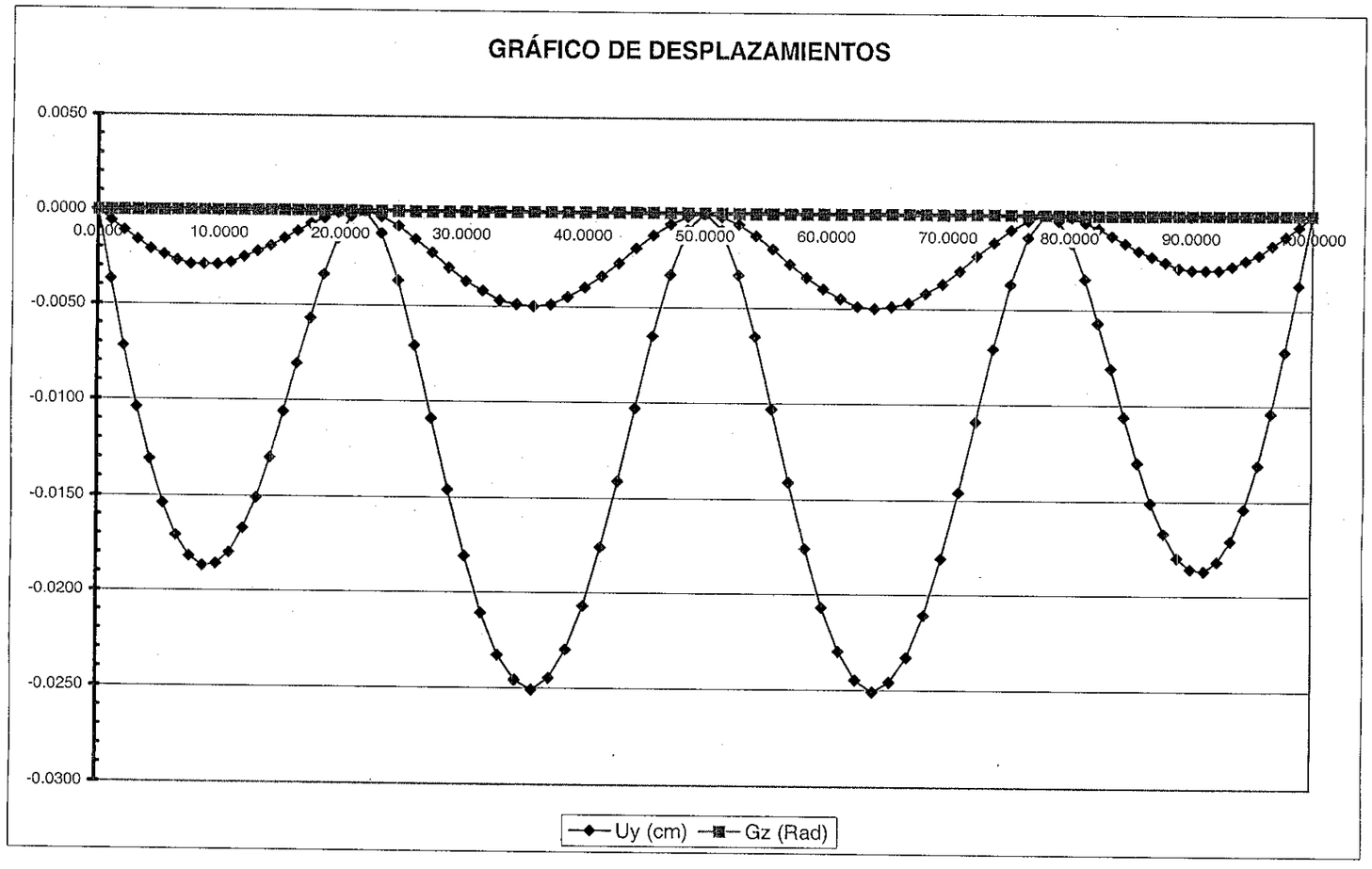
Uy (cm)
Gz (Rad)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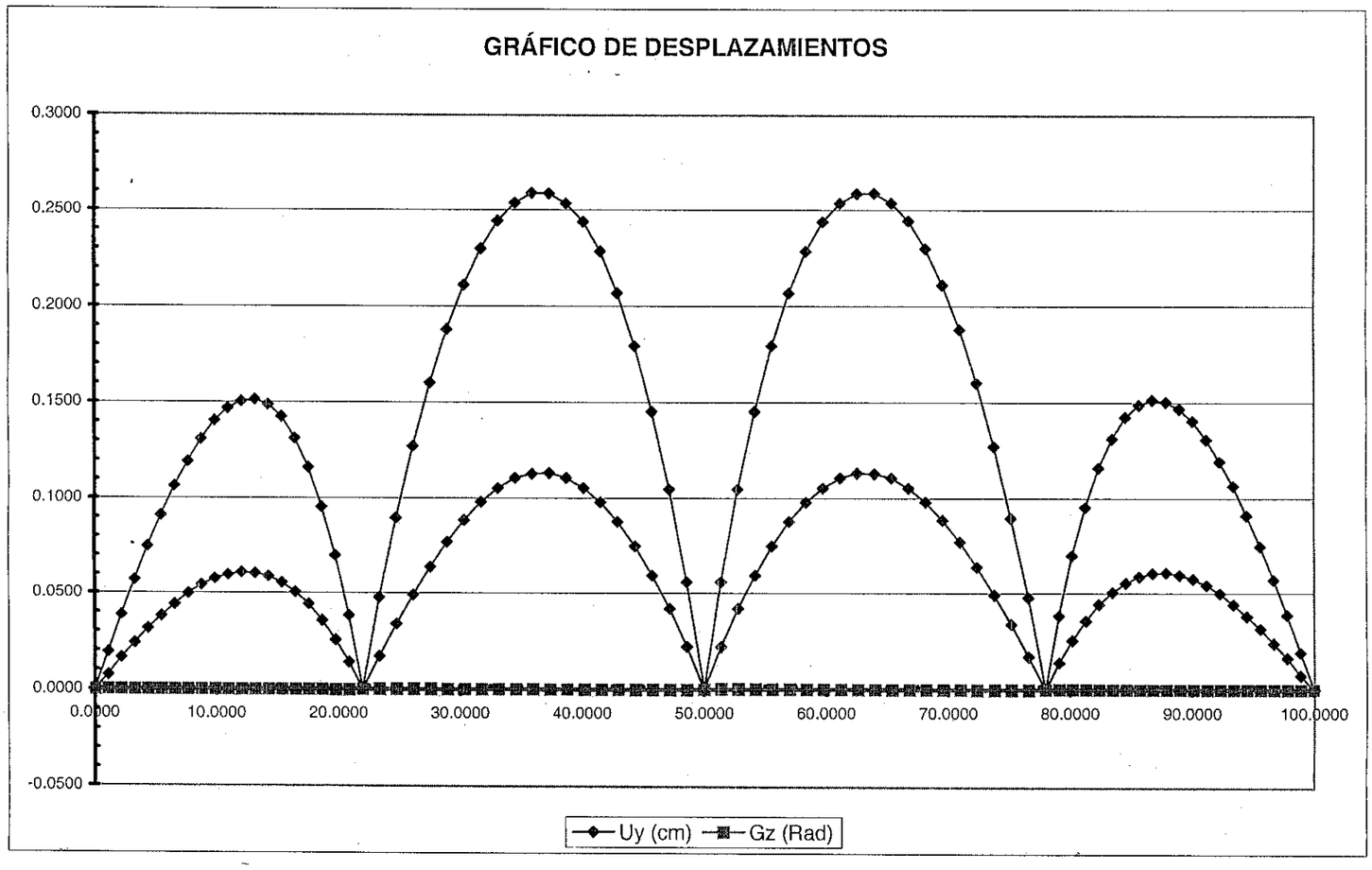
Uy (cm)
Gz (Rad)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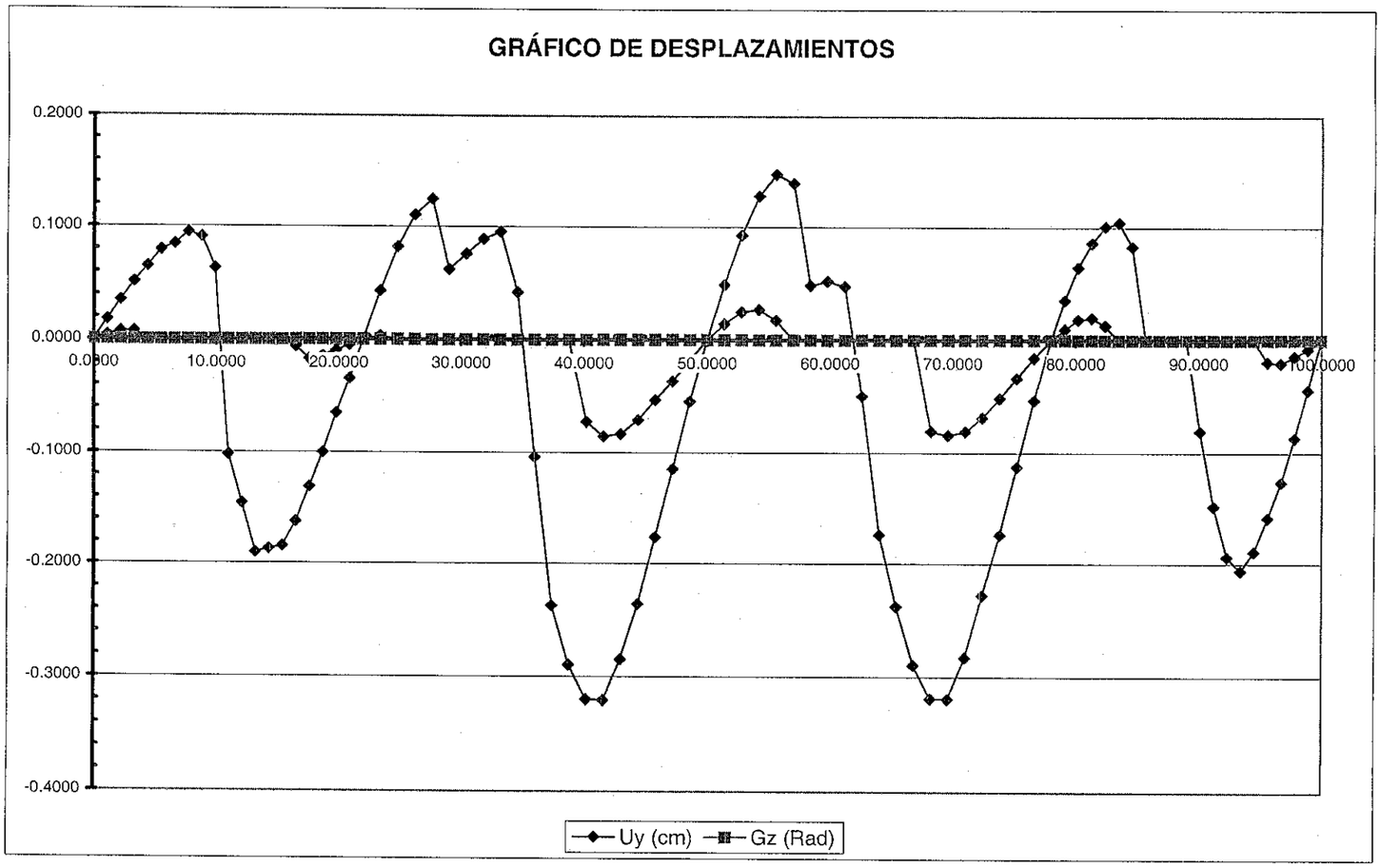
Uy (cm)
Gz (Rad)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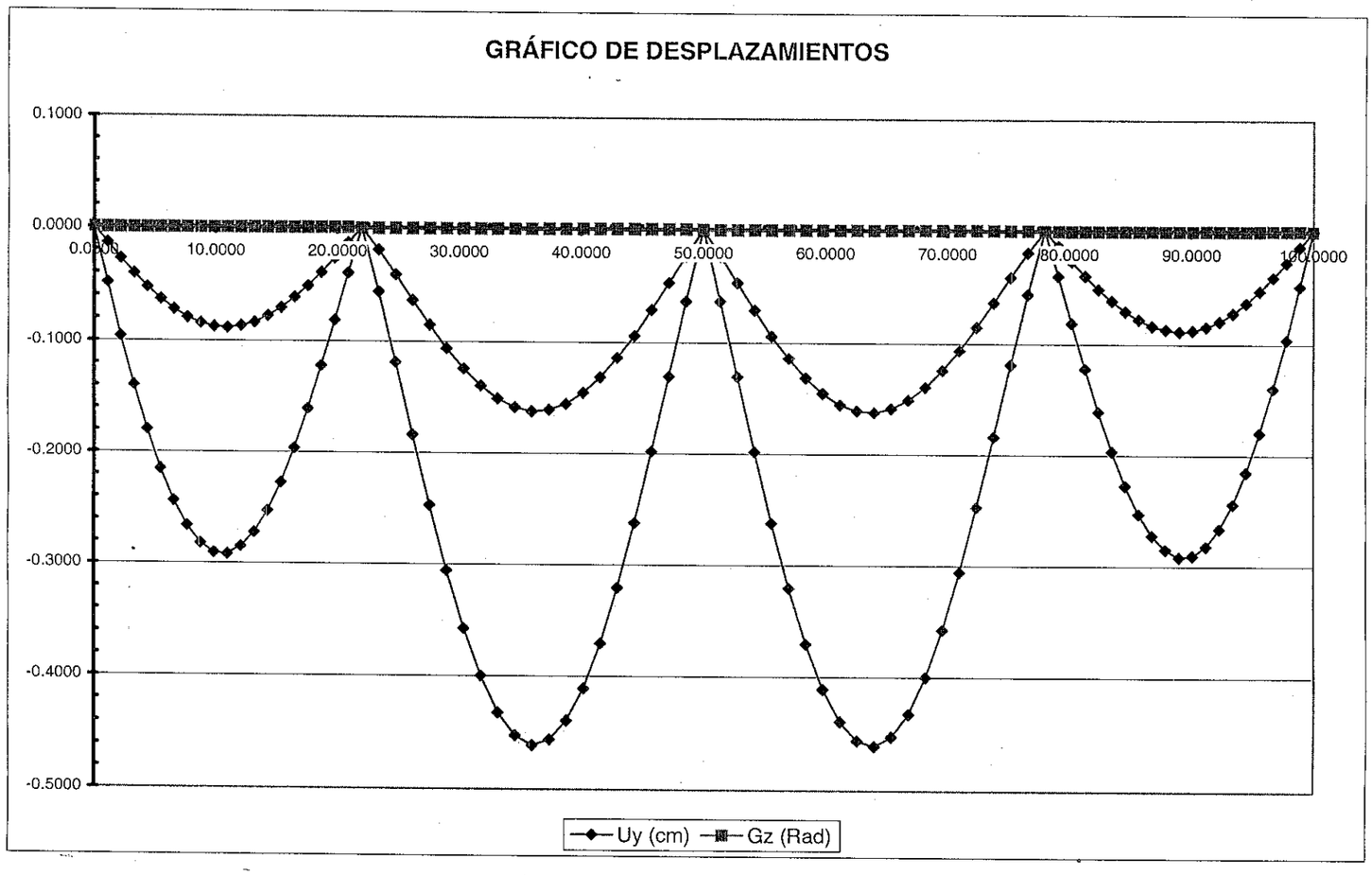
Uy (cm)
Gz (Rad)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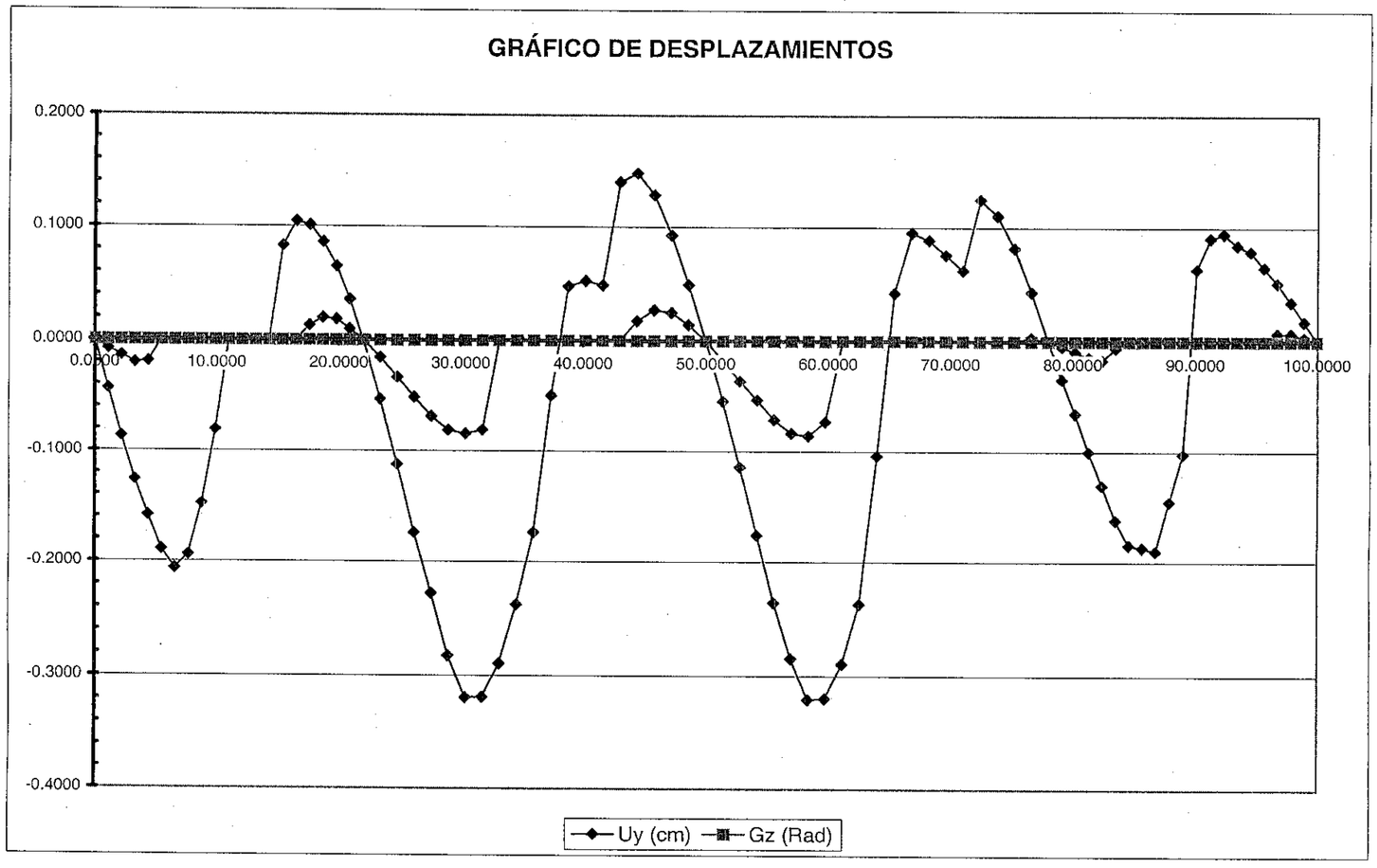
Uy (cm)
Gz (Rad)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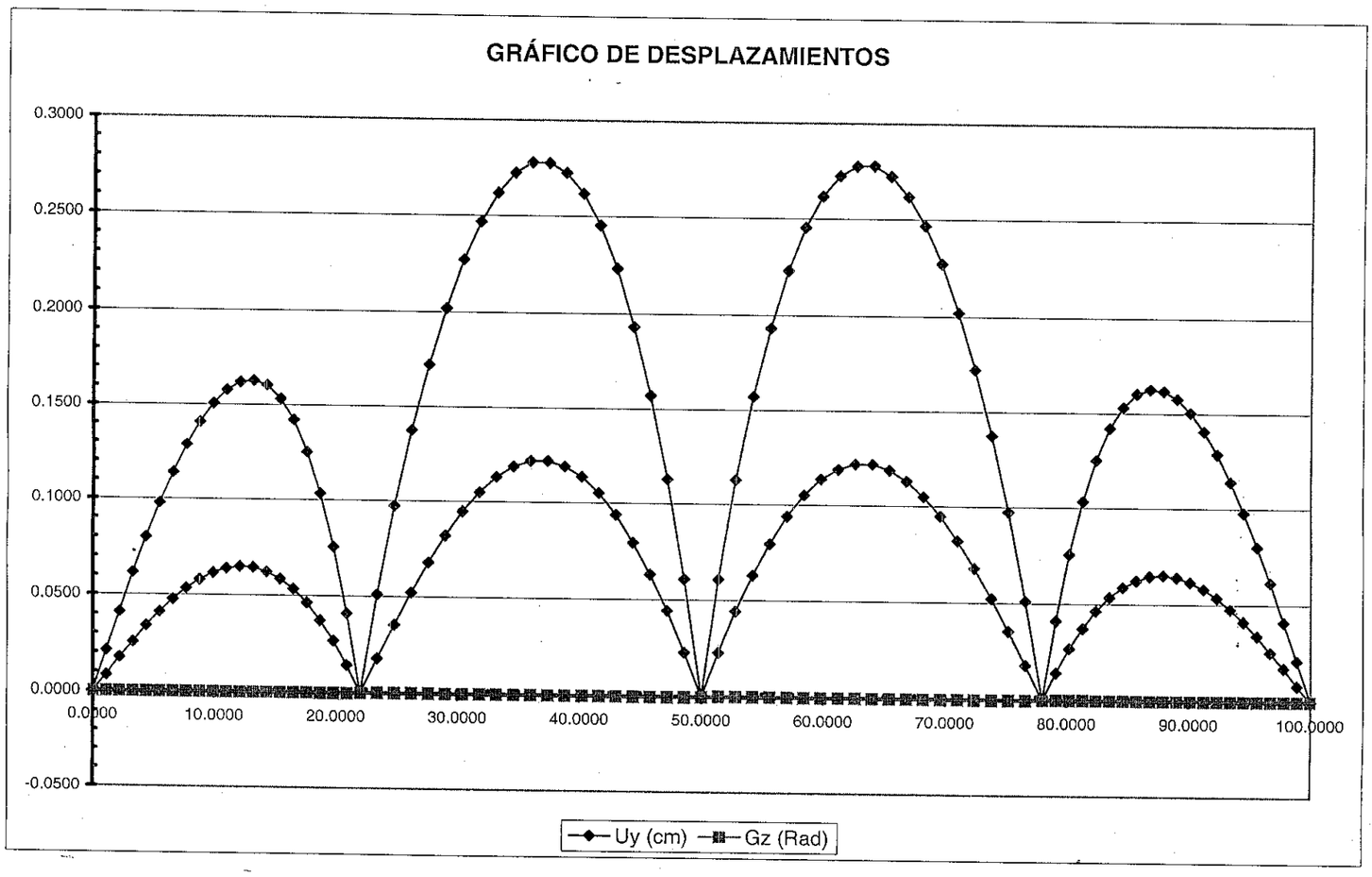
90.0000
100.0000
Uy (cm)
Gz (Rad)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10.0000
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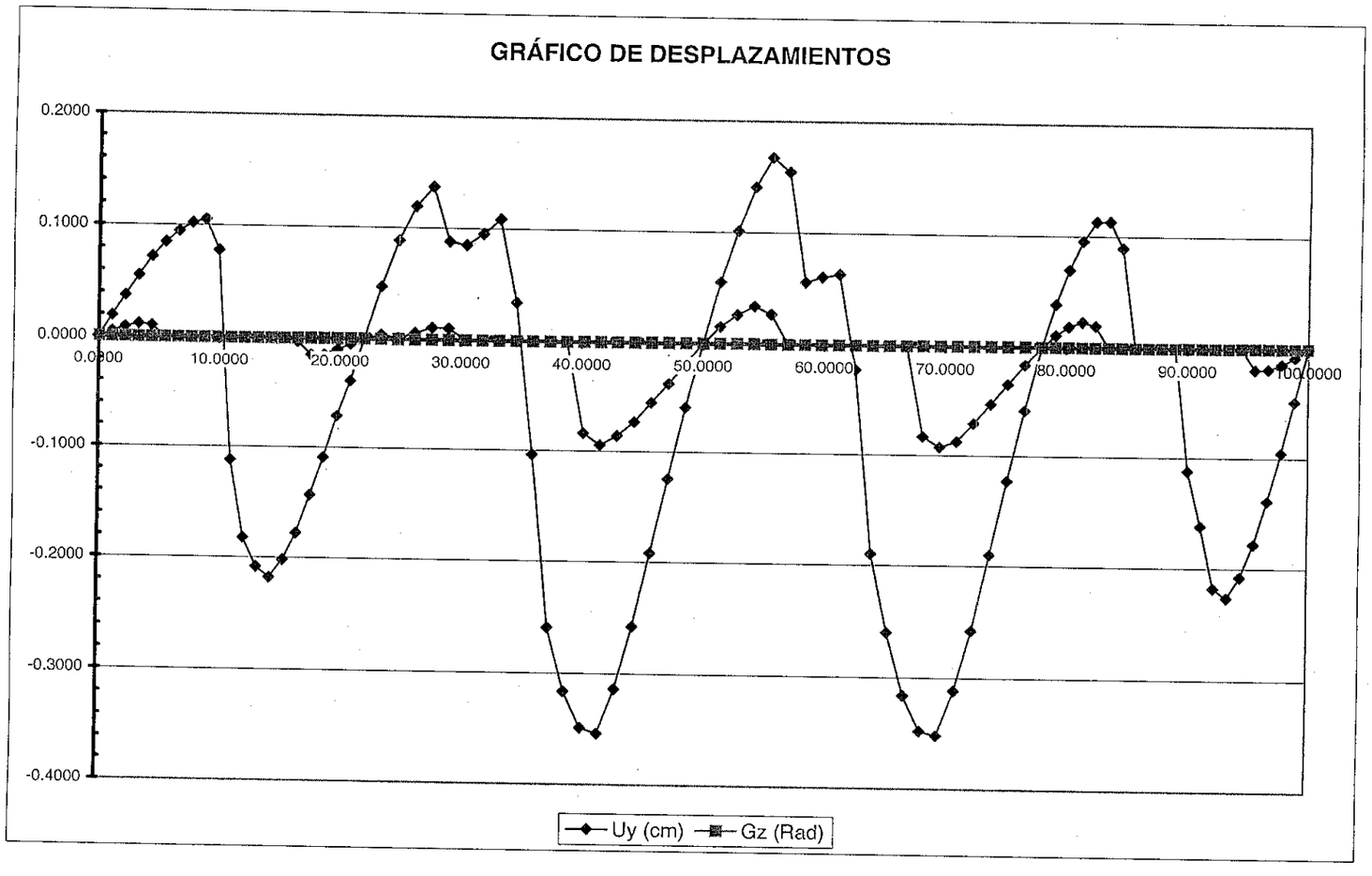
90.0000
100.0000
Uy (cm)
Gz (Rad)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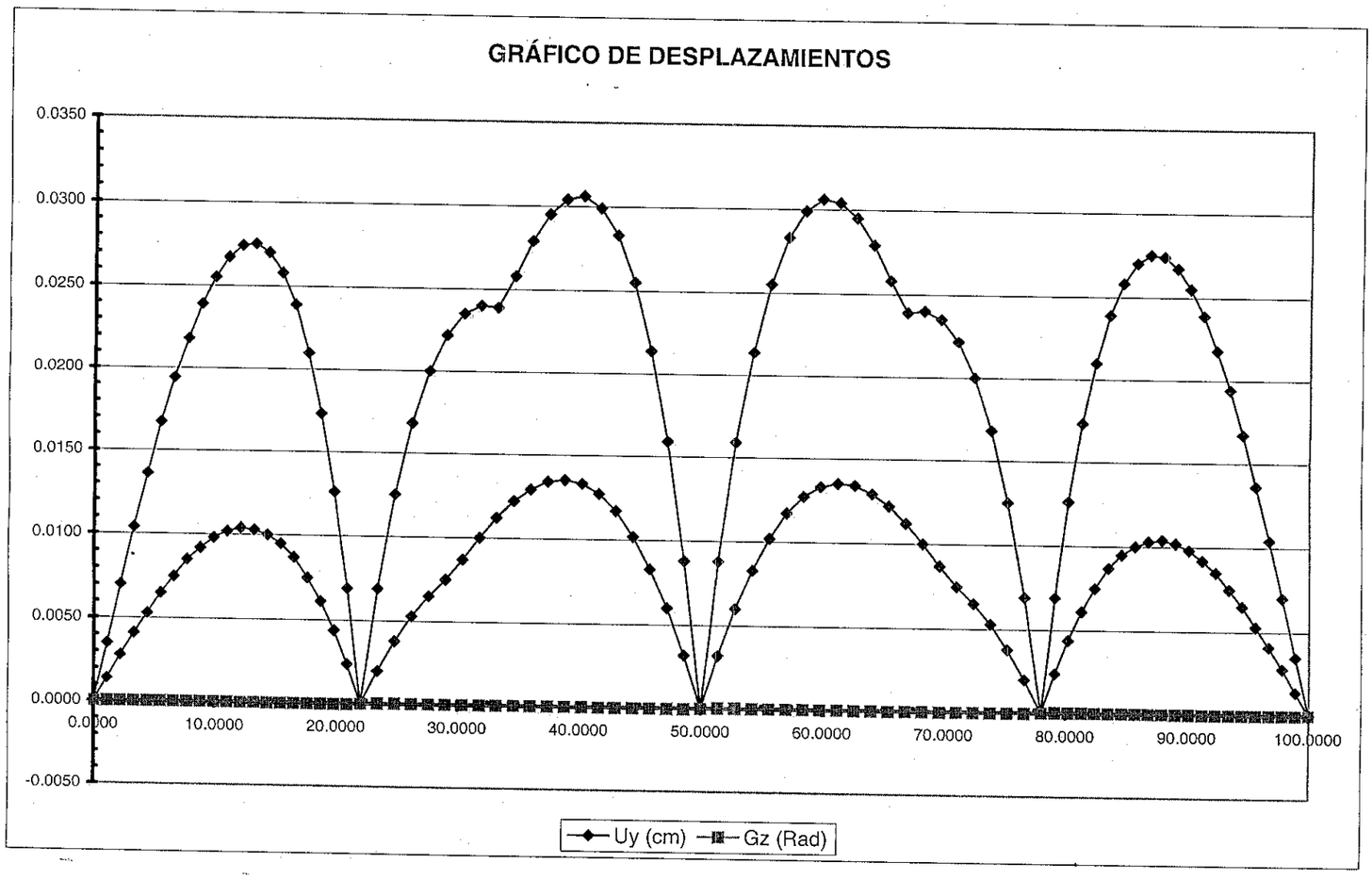
Uy (cm)
Gz (Rad)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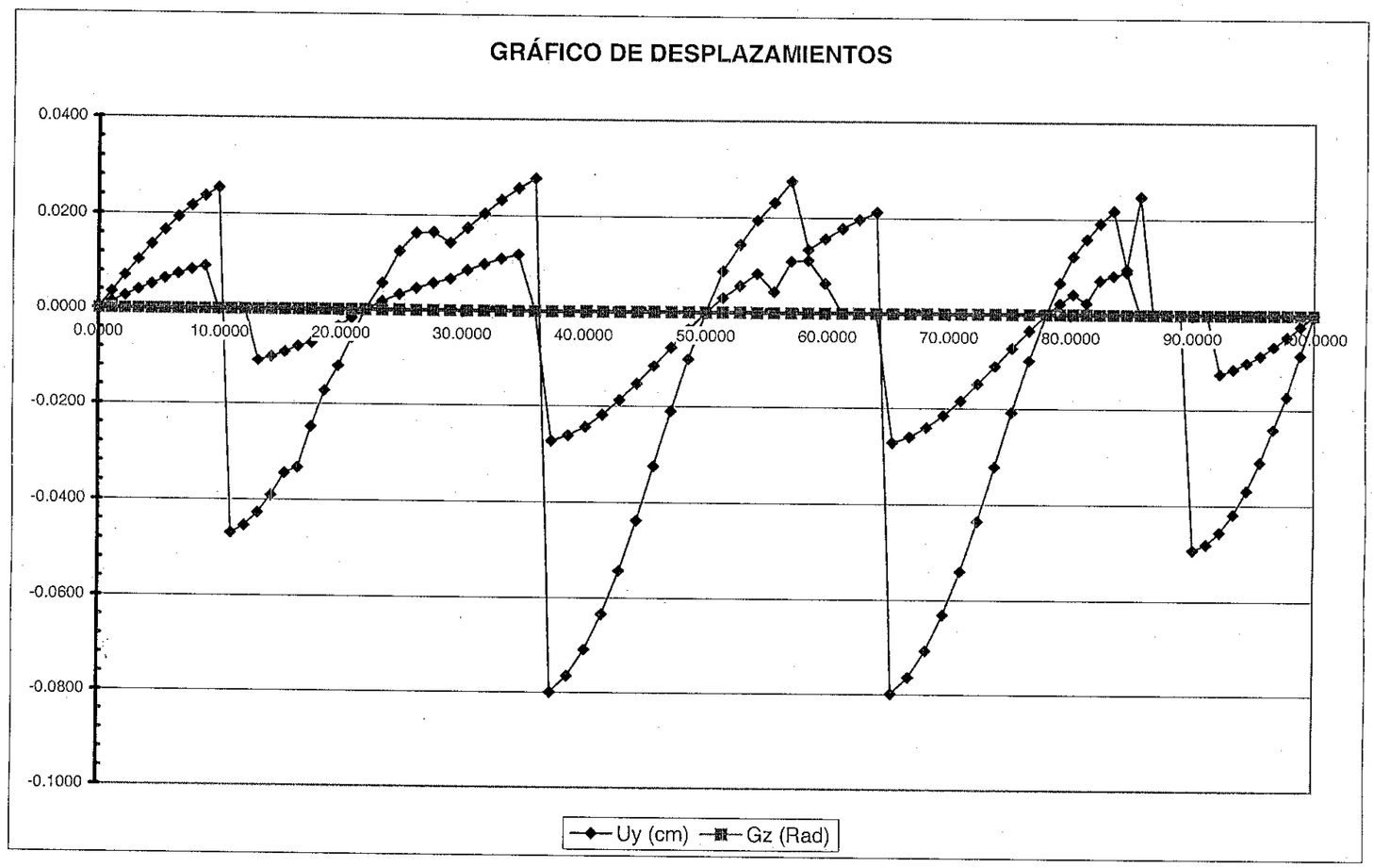
100.0000
Uy (cm)
Gz (Rad)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0.0000
10.0000
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40.0000
50.0000
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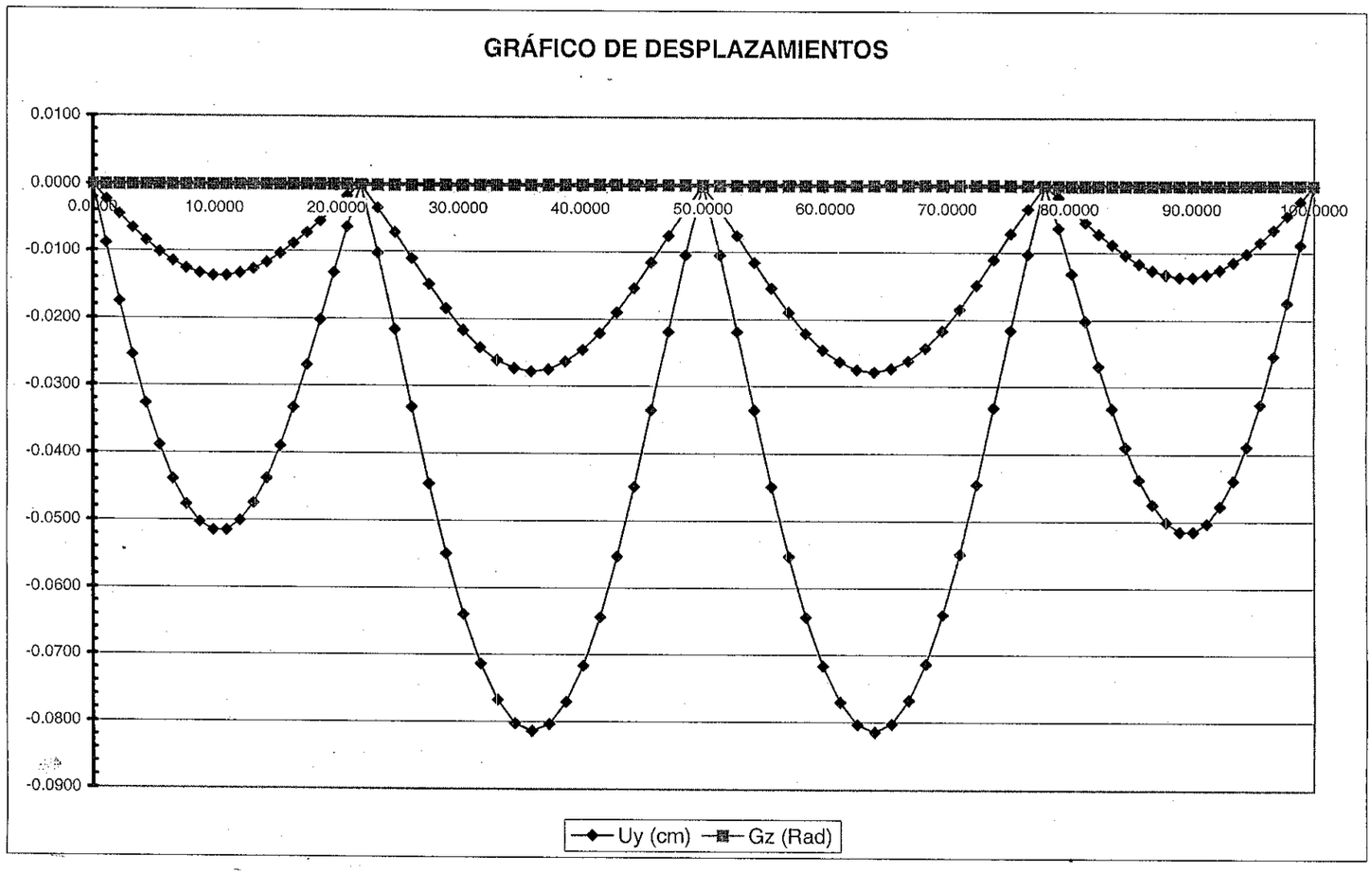
90.0000
100.0000
Uy (cm)
Gz (Rad)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0.0000
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90.0000
100.0000
Uy (cm)
Gz (Rad)

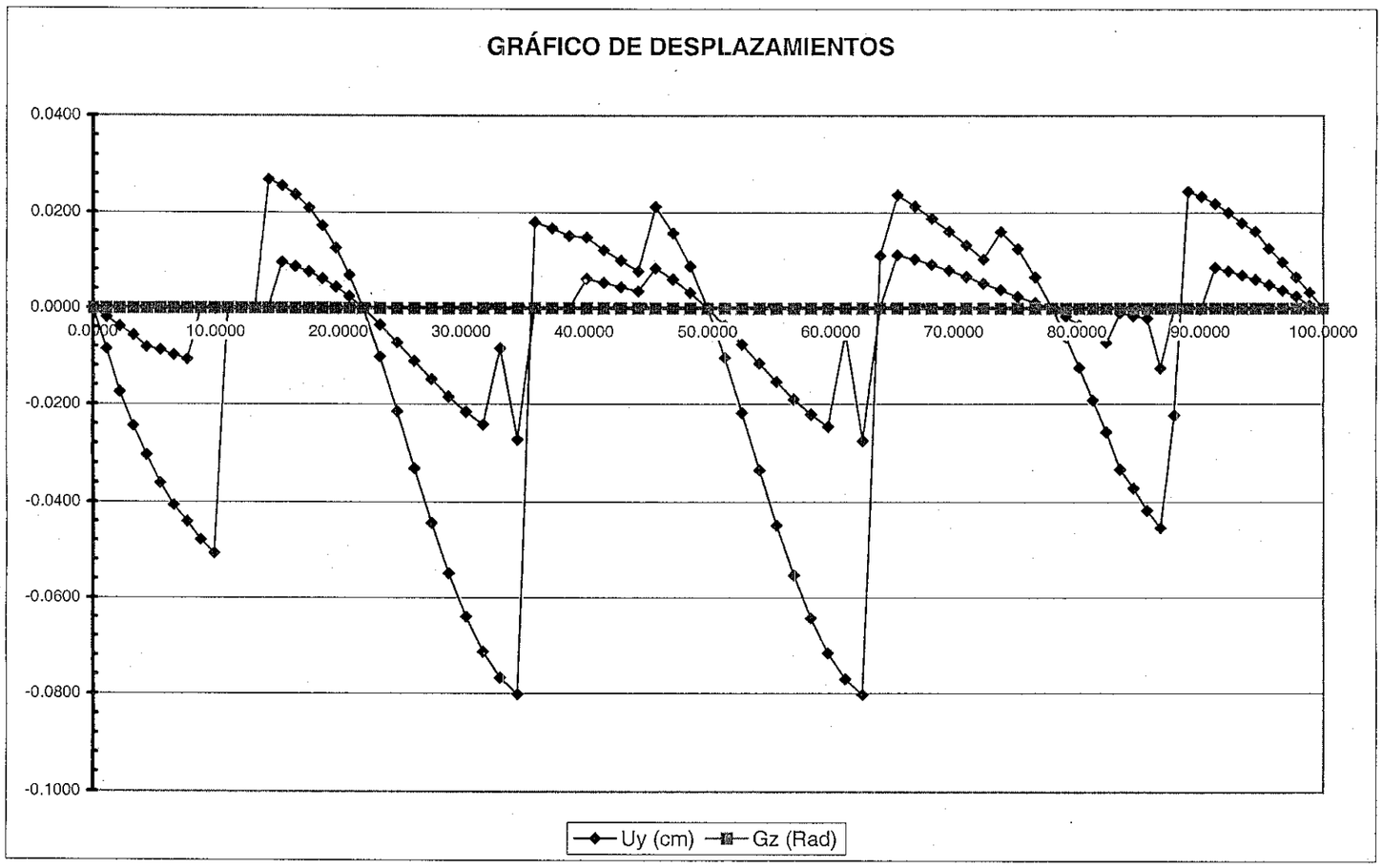
GRÁFICO DE DESPLAZAMIENTOS
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10.0000
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50.0000
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70.0000
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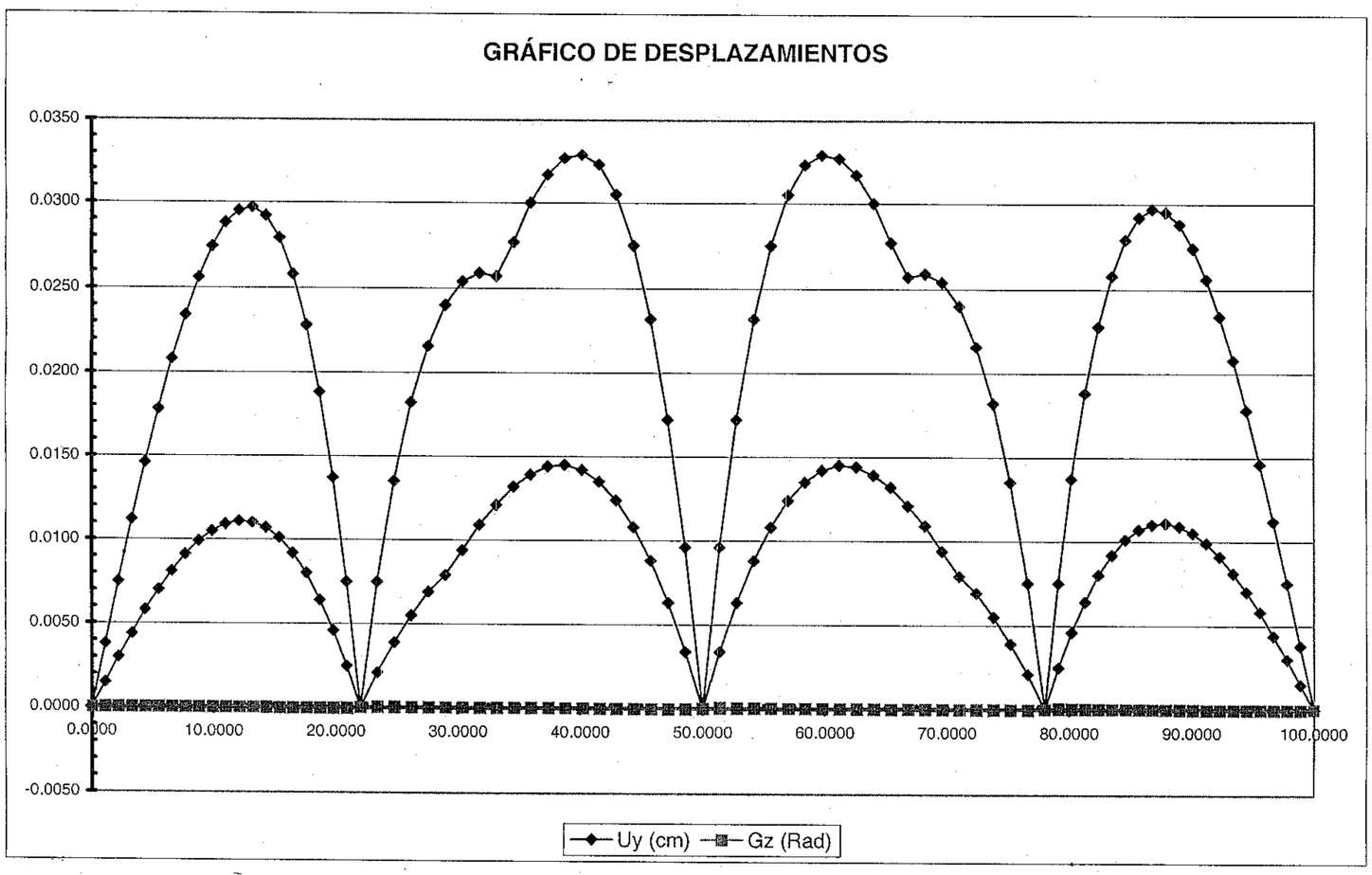
90.0000
100.0000
Uy (cm)
Gz (Rad)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10.0000
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50.0000
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90.0000
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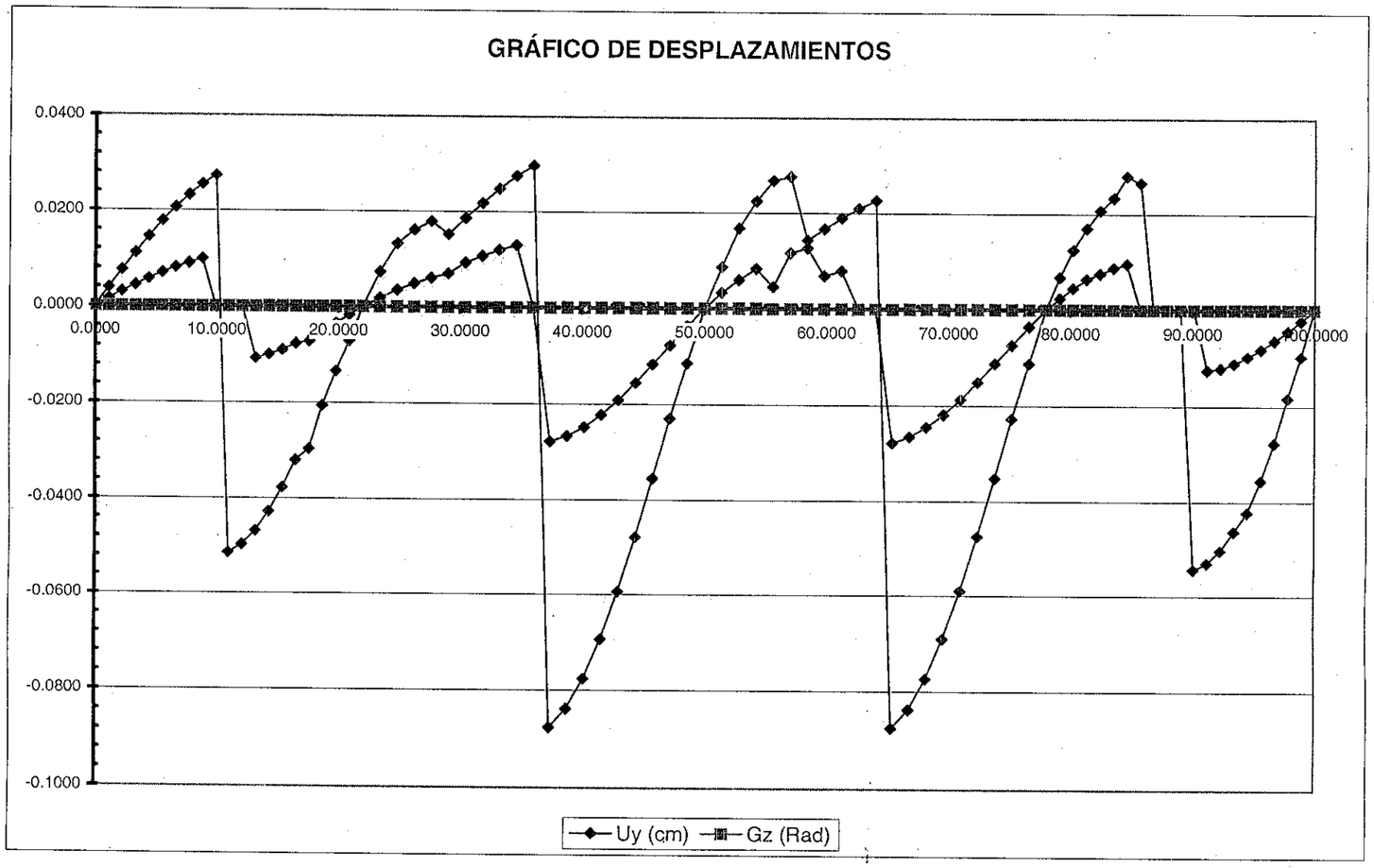
Uy (cm)
Gz (Rad)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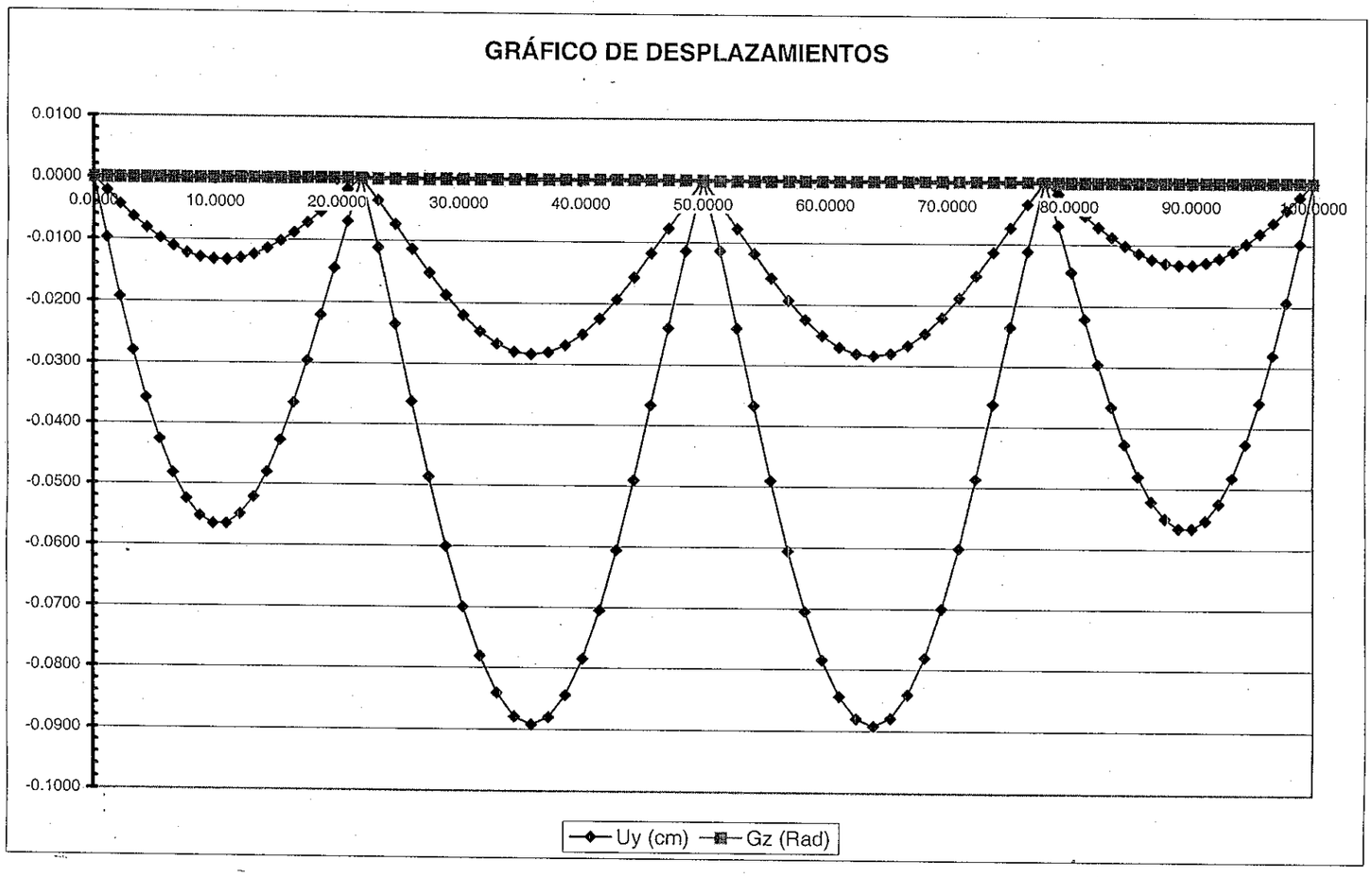
0.0000
10.0000
20.0000
30.0000
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
Uy (cm)
Gz (Rad)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0.0000
10.0000
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90.0000
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Uy (cm)
Gz (Rad)

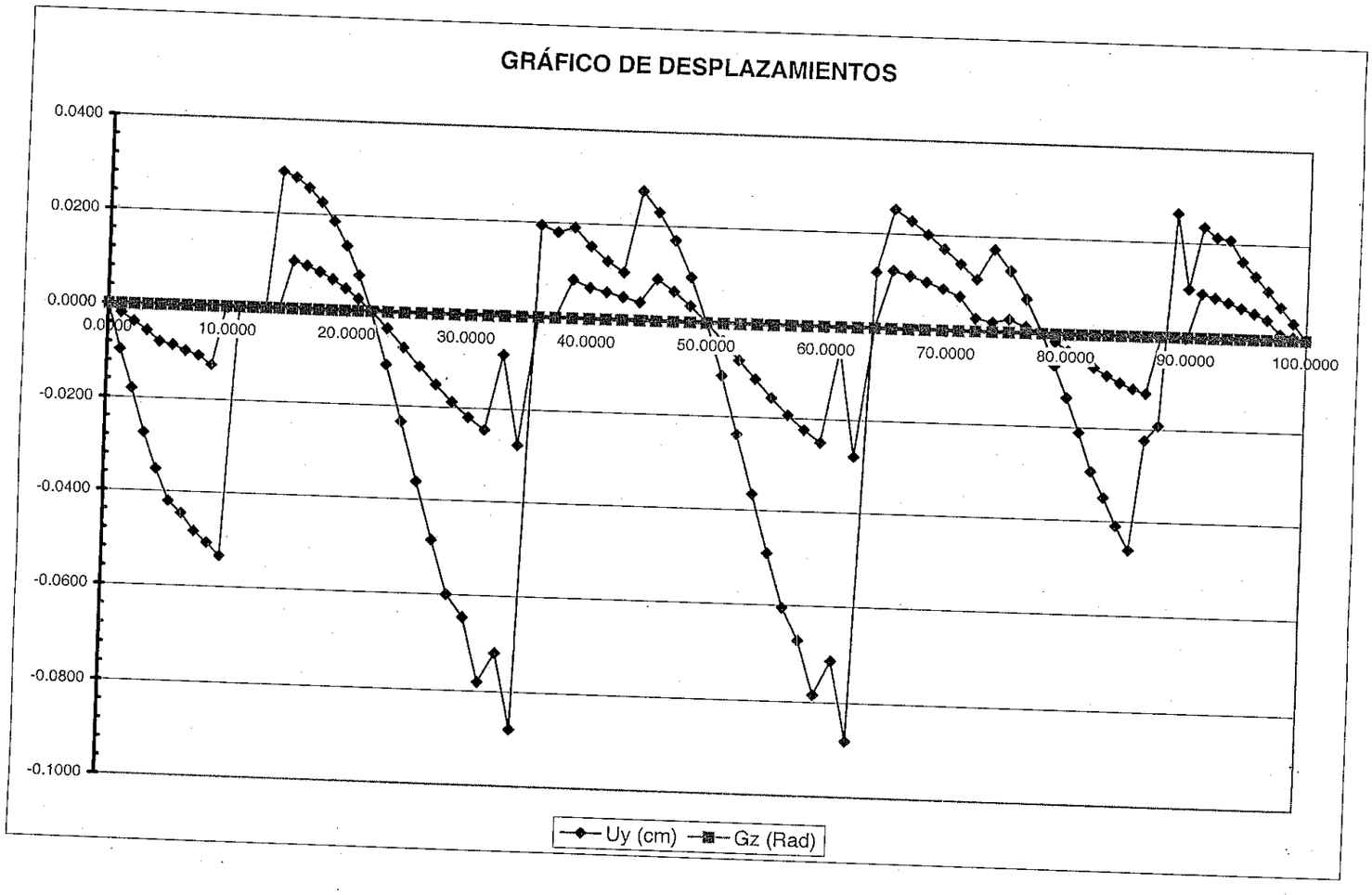
GRÁFICO DE DESPLAZAMIENTOS
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10.0000
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50.0000
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70.0000
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90.0000
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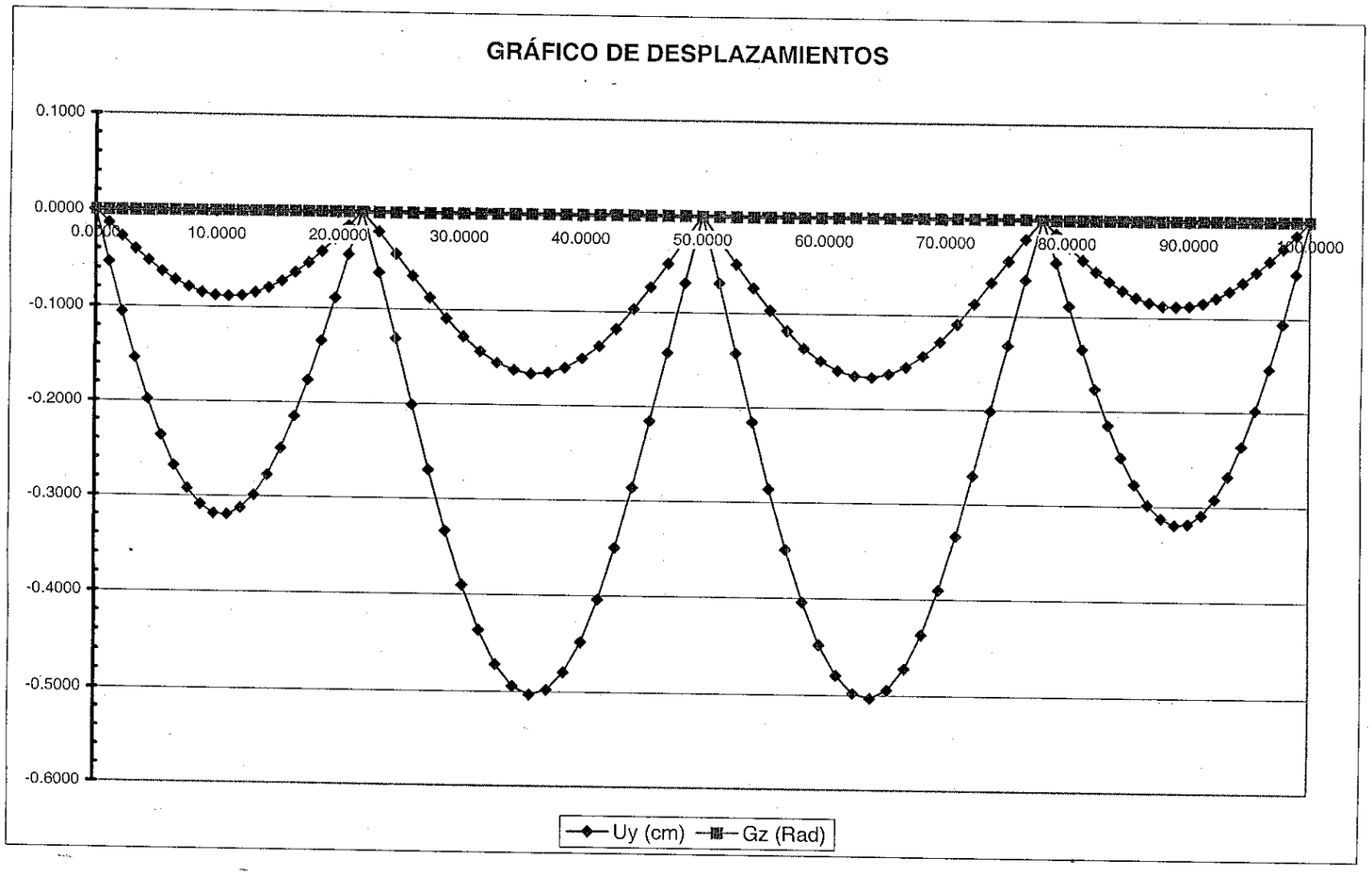
Uy (cm)
Gz (Rad)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0.0000
10.0000
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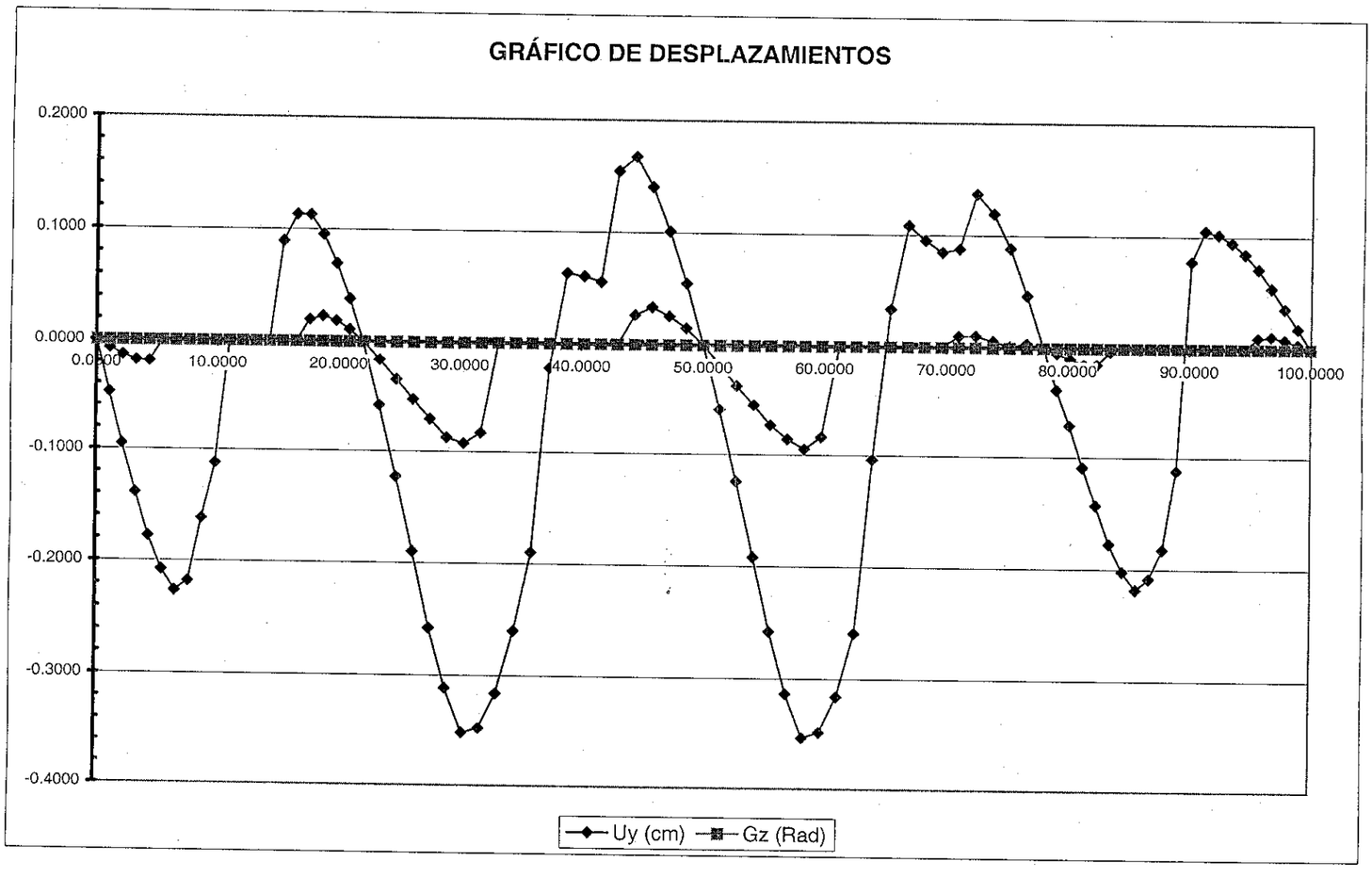
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
100.0000
Uy (cm)
Gz (Rad)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10.0000
20.0000
30.0000
40.0000
50.0000
60.0000
70.0000
80.0000
90.0000
100.0000
Uy (cm)
Gz (Rad)

ESFUERZOS EN LAS BARRAS

LOSA

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	-0.98
201	301	0.00	0.00	0.00	-0.98
202	202	1.10	0.00	0.00	-1.97
202	302	1.10	0.00	0.00	-1.97
203	203	2.20	0.00	0.00	-1.97
203	303	2.20	0.00	0.00	-1.97
204	204	3.30	0.00	0.00	-1.97
204	304	3.30	0.00	0.00	-1.97
205	205	4.40	0.00	0.00	-1.97
205	305	4.40	0.00	0.00	-1.97
206	206	5.50	0.00	0.00	-1.97
206	306	5.50	0.00	0.00	-1.97
207	207	6.60	0.00	0.00	-1.97
207	307	6.60	0.00	0.00	-1.97
208	208	7.70	0.00	0.00	-1.97
208	308	7.70	0.00	0.00	-1.97
209	209	8.80	0.00	0.00	-1.97
209	309	8.80	0.00	0.00	-1.97
210	210	9.90	0.00	0.00	-1.97
210	310	9.90	0.00	0.00	-1.97
211	211	11.00	0.00	0.00	-1.97
211	311	11.00	0.00	0.00	-1.97
212	212	12.10	0.00	0.00	-1.97
212	312	12.10	0.00	0.00	-1.97
213	213	13.20	0.00	0.00	-1.97
213	313	13.20	0.00	0.00	-1.97
214	214	14.30	0.00	0.00	-1.97
214	314	14.30	0.00	0.00	-1.97
215	215	15.40	0.00	0.00	-1.97
215	315	15.40	0.00	0.00	-1.97
216	216	16.50	0.00	0.00	-1.97
216	316	16.50	0.00	0.00	-1.97
217	217	17.60	0.00	0.00	-1.97
217	317	17.60	0.00	0.00	-1.97
218	218	18.70	0.00	0.00	-1.97
218	318	18.70	0.00	0.00	-1.97
219	219	19.80	0.00	0.00	-1.97
219	319	19.80	0.00	0.00	-1.97
220	220	20.90	0.00	0.00	-1.97
220	320	20.90	0.00	0.00	-1.97
221	221	22.00	0.00	0.00	-2.24
221	321	22.00	0.00	0.00	-2.24
222	222	23.40	0.00	0.00	-2.50
222	322	23.40	0.00	0.00	-2.50
223	223	24.80	0.00	0.00	-2.50
223	323	24.80	0.00	0.00	-2.50
224	224	26.20	0.00	0.00	-2.50
224	324	26.20	0.00	0.00	-2.50
225	225	27.60	0.00	0.00	-2.50
225	325	27.60	0.00	0.00	-2.50
226	226	29.00	0.00	0.00	-2.50

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-2.50
227	227	30.40	0.00	0.00	-2.50
227	327	30.40	0.00	0.00	-2.50
228	228	31.80	0.00	0.00	-2.50
228	328	31.80	0.00	0.00	-2.50
229	229	33.20	0.00	0.00	-2.50
229	329	33.20	0.00	0.00	-2.50
230	230	34.60	0.00	0.00	-2.50
230	330	34.60	0.00	0.00	-2.50
231	231	36.00	0.00	0.00	-2.50
231	331	36.00	0.00	0.00	-2.50
232	232	37.40	0.00	0.00	-2.50
232	332	37.40	0.00	0.00	-2.50
233	233	38.80	0.00	0.00	-2.50
233	333	38.80	0.00	0.00	-2.50
234	234	40.20	0.00	0.00	-2.50
234	334	40.20	0.00	0.00	-2.50
235	235	41.60	0.00	0.00	-2.50
235	335	41.60	0.00	0.00	-2.50
236	236	43.00	0.00	0.00	-2.50
236	336	43.00	0.00	0.00	-2.50
237	237	44.40	0.00	0.00	-2.50
237	337	44.40	0.00	0.00	-2.50
238	238	45.80	0.00	0.00	-2.50
238	338	45.80	0.00	0.00	-2.50
239	239	47.20	0.00	0.00	-2.50
239	339	47.20	0.00	0.00	-2.50
240	240	48.60	0.00	0.00	-2.50
240	340	48.60	0.00	0.00	-2.50
241	241	50.00	0.00	0.00	-2.50
241	341	50.00	0.00	0.00	-2.50
242	242	51.40	0.00	0.00	-2.50
242	342	51.40	0.00	0.00	-2.50
243	243	52.80	0.00	0.00	-2.50
243	343	52.80	0.00	0.00	-2.50
244	244	54.20	0.00	0.00	-2.50
244	344	54.20	0.00	0.00	-2.50
245	245	55.60	0.00	0.00	-2.50
245	345	55.60	0.00	0.00	-2.50
246	246	57.00	0.00	0.00	-2.50
246	346	57.00	0.00	0.00	-2.50
247	247	58.40	0.00	0.00	-2.50
247	347	58.40	0.00	0.00	-2.50
248	248	59.80	0.00	0.00	-2.50
248	348	59.80	0.00	0.00	-2.50
249	249	61.20	0.00	0.00	-2.50
249	349	61.20	0.00	0.00	-2.50
250	250	62.60	0.00	0.00	-2.50
250	350	62.60	0.00	0.00	-2.50
251	251	64.00	0.00	0.00	-2.50
251	351	64.00	0.00	0.00	-2.50

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-2.50
252	352	65.40	0.00	0.00	-2.50
253	253	66.80	0.00	0.00	-2.50
253	353	66.80	0.00	0.00	-2.50
254	254	68.20	0.00	0.00	-2.50
254	354	68.20	0.00	0.00	-2.50
255	255	69.60	0.00	0.00	-2.50
255	355	69.60	0.00	0.00	-2.50
256	256	71.00	0.00	0.00	-2.50
256	356	71.00	0.00	0.00	-2.50
257	257	72.40	0.00	0.00	-2.50
257	357	72.40	0.00	0.00	-2.50
258	258	73.80	0.00	0.00	-2.50
258	358	73.80	0.00	0.00	-2.50
259	259	75.20	0.00	0.00	-2.50
259	359	75.20	0.00	0.00	-2.50
260	260	76.60	0.00	0.00	-2.50
260	360	76.60	0.00	0.00	-2.50
261	261	78.00	0.00	0.00	-2.24
261	361	78.00	0.00	0.00	-2.24
262	262	79.10	0.00	0.00	-1.97
262	362	79.10	0.00	0.00	-1.97
263	263	80.20	0.00	0.00	-1.97
263	363	80.20	0.00	0.00	-1.97
264	264	81.30	0.00	0.00	-1.97
264	364	81.30	0.00	0.00	-1.97
265	265	82.40	0.00	0.00	-1.97
265	365	82.40	0.00	0.00	-1.97
266	266	83.50	0.00	0.00	-1.97
266	366	83.50	0.00	0.00	-1.97
267	267	84.60	0.00	0.00	-1.97
267	367	84.60	0.00	0.00	-1.97
268	268	85.70	0.00	0.00	-1.97
268	368	85.70	0.00	0.00	-1.97
269	269	86.80	0.00	0.00	-1.97
269	369	86.80	0.00	0.00	-1.97
270	270	87.90	0.00	0.00	-1.97
270	370	87.90	0.00	0.00	-1.97
271	271	89.00	0.00	0.00	-1.97
271	371	89.00	0.00	0.00	-1.97
272	272	90.10	0.00	0.00	-1.97
272	372	90.10	0.00	0.00	-1.97
273	273	91.20	0.00	0.00	-1.97
273	373	91.20	0.00	0.00	-1.97
274	274	92.30	0.00	0.00	-1.97
274	374	92.30	0.00	0.00	-1.97
275	275	93.40	0.00	0.00	-1.97
275	375	93.40	0.00	0.00	-1.97
276	276	94.50	0.00	0.00	-1.97
276	376	94.50	0.00	0.00	-1.97
277	277	95.60	0.00	0.00	-1.97

CÁLCULO TENSIONAL

Hipótesis de cálculo:
PLOSAEI

Peso losa estructura ideal

[1; 1]PLOSAEI

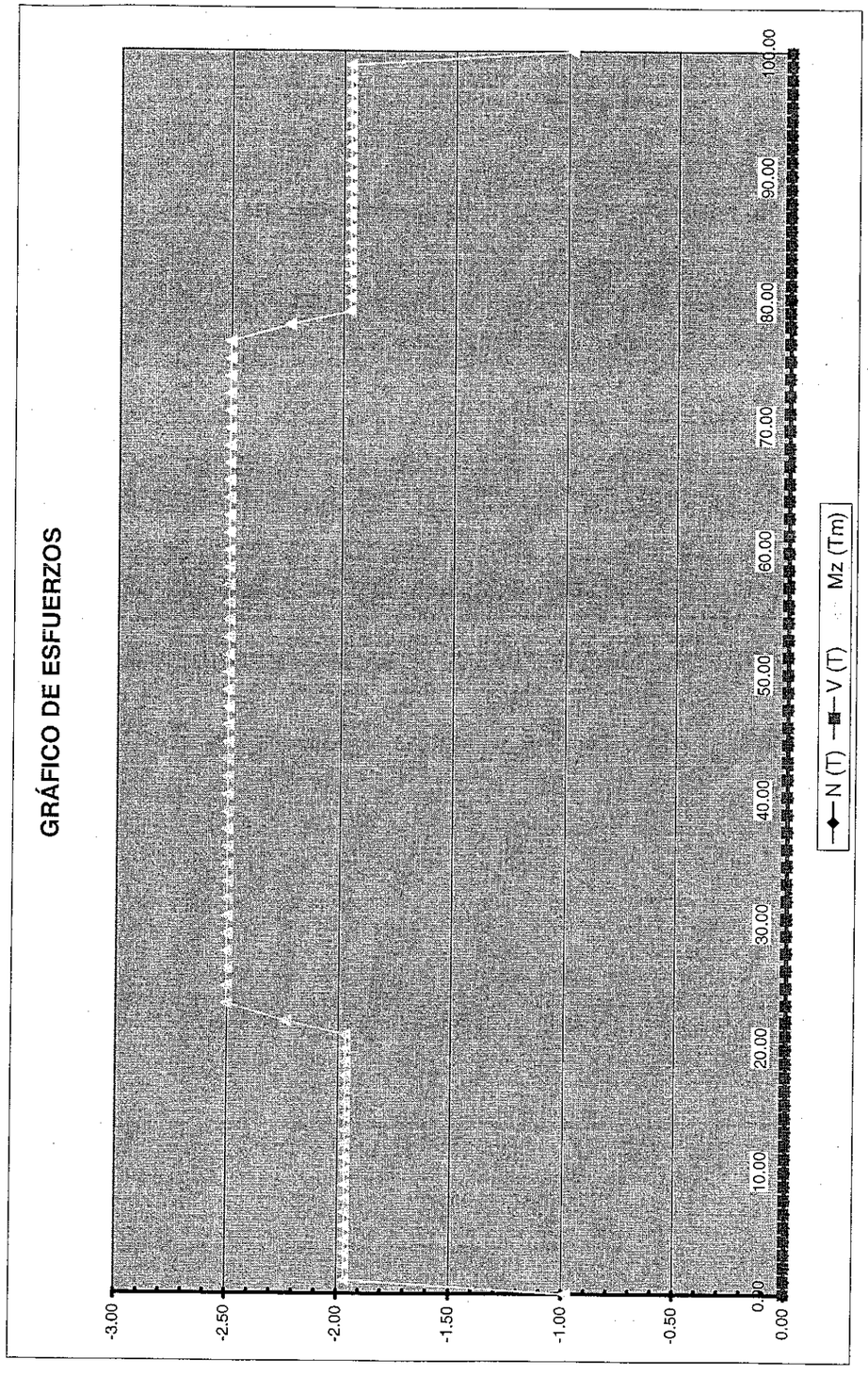
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-1.97
278	278	96.70	0.00	0.00	-1.97
278	378	96.70	0.00	0.00	-1.97
279	279	97.80	0.00	0.00	-1.97
279	379	97.80	0.00	0.00	-1.97
280	280	98.90	0.00	0.00	-1.97
280	380	98.90	0.00	0.00	-1.97
281	281	100.00	0.00	0.00	-0.98
281	381	100.00	0.00	0.00	-0.98

15/09/03

Programa DINTEL PACADAR S.A.
PLOSAEI

~csimp4.esv



CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	-0.17	1.32
201	301	0.00	0.00	-0.17	2.18
202	202	1.10	0.00	-0.30	2.74
202	302	1.10	0.00	-0.30	4.24
203	203	2.20	0.00	-0.25	2.85
203	303	2.20	0.00	-0.25	4.13
204	204	3.30	0.00	-0.22	2.95
204	304	3.30	0.00	-0.22	4.04
205	205	4.40	0.00	-0.18	3.03
205	305	4.40	0.00	-0.18	3.95
206	206	5.50	0.00	-0.16	3.10
206	306	5.50	0.00	-0.16	3.89
207	207	6.60	0.00	-0.14	3.15
207	307	6.60	0.00	-0.14	3.84
208	208	7.70	0.00	-0.12	3.18
208	308	7.70	0.00	-0.12	3.80
209	209	8.80	0.00	-0.12	3.20
209	309	8.80	0.00	-0.12	3.79
210	210	9.90	0.00	-0.12	3.20
210	310	9.90	0.00	-0.12	3.79
211	211	11.00	0.00	-0.12	3.18
211	311	11.00	0.00	-0.12	3.81
212	212	12.10	0.00	-0.14	3.15
212	312	12.10	0.00	-0.14	3.84
213	213	13.20	0.00	-0.16	3.10
213	313	13.20	0.00	-0.16	3.88
214	214	14.30	0.00	-0.18	3.04
214	314	14.30	0.00	-0.18	3.94
215	215	15.40	0.00	-0.20	2.98
215	315	15.40	0.00	-0.20	4.01
216	216	16.50	0.00	-0.23	2.91
216	316	16.50	0.00	-0.23	4.08
217	217	17.60	0.00	-0.26	2.84
217	317	17.60	0.00	-0.26	4.15
218	218	18.70	0.00	-0.29	2.77
218	318	18.70	0.00	-0.29	4.22
219	219	19.80	0.00	-0.31	2.71
219	319	19.80	0.00	-0.31	4.27
220	220	20.90	0.00	-0.32	2.67
220	320	20.90	0.00	-0.32	4.31
221	221	22.00	0.00	-0.38	3.02
221	321	22.00	0.00	-0.38	4.92
222	222	23.40	0.00	-0.41	3.42
222	322	23.40	0.00	-0.41	5.47
223	223	24.80	0.00	-0.37	3.50
223	323	24.80	0.00	-0.37	5.39
224	224	26.20	0.00	-0.33	3.61
224	324	26.20	0.00	-0.33	5.28
225	225	27.60	0.00	-0.28	3.74
225	325	27.60	0.00	-0.28	5.15
226	226	29.00	0.00	-0.23	3.86

~csimp4.esv Programa DINTEL PACADAR S.A. 15/09/03
CMBALASTO

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	-0.23	5.03
227	227	30.40	0.00	-0.19	3.97
227	327	30.40	0.00	-0.19	4.92
228	228	31.80	0.00	-0.15	4.07
228	328	31.80	0.00	-0.15	4.82
229	229	33.20	0.00	-0.12	4.14
229	329	33.20	0.00	-0.12	4.75
230	230	34.60	0.00	-0.11	4.18
230	330	34.60	0.00	-0.11	4.71
231	231	36.00	0.00	-0.10	4.19
231	331	36.00	0.00	-0.10	4.70
232	232	37.40	0.00	-0.11	4.17
232	332	37.40	0.00	-0.11	4.72
233	233	38.80	0.00	-0.13	4.13
233	333	38.80	0.00	-0.13	4.76
234	234	40.20	0.00	-0.16	4.05
234	334	40.20	0.00	-0.16	4.84
235	235	41.60	0.00	-0.20	3.95
235	335	41.60	0.00	-0.20	4.94
236	236	43.00	0.00	-0.24	3.83
236	336	43.00	0.00	-0.24	5.05
237	237	44.40	0.00	-0.29	3.71
237	337	44.40	0.00	-0.29	5.18
238	238	45.80	0.00	-0.34	3.58
238	338	45.80	0.00	-0.34	5.31
239	239	47.20	0.00	-0.39	3.47
239	339	47.20	0.00	-0.39	5.42
240	240	48.60	0.00	-0.42	3.39
240	340	48.60	0.00	-0.42	5.50
241	241	50.00	0.00	-0.43	3.35
241	341	50.00	0.00	-0.43	5.54
242	242	51.40	0.00	-0.42	3.39
242	342	51.40	0.00	-0.42	5.50
243	243	52.80	0.00	-0.39	3.47
243	343	52.80	0.00	-0.39	5.42
244	244	54.20	0.00	-0.34	3.58
244	344	54.20	0.00	-0.34	5.31
245	245	55.60	0.00	-0.29	3.71
245	345	55.60	0.00	-0.29	5.18
246	246	57.00	0.00	-0.24	3.83
246	346	57.00	0.00	-0.24	5.05
247	247	58.40	0.00	-0.20	3.95
247	347	58.40	0.00	-0.20	4.94
248	248	59.80	0.00	-0.16	4.05
248	348	59.80	0.00	-0.16	4.84
249	249	61.20	0.00	-0.13	4.13
249	349	61.20	0.00	-0.13	4.76
250	250	62.60	0.00	-0.11	4.17
250	350	62.60	0.00	-0.11	4.72
251	251	64.00	0.00	-0.10	4.19
251	351	64.00	0.00	-0.10	4.70

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMBALASTO

Carga muerta balasto

[1; 1]CMBALASTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	-0.11	4.18
252	352	65.40	0.00	-0.11	4.71
253	253	66.80	0.00	-0.12	4.14
253	353	66.80	0.00	-0.12	4.75
254	254	68.20	0.00	-0.15	4.07
254	354	68.20	0.00	-0.15	4.82
255	255	69.60	0.00	-0.19	3.97
255	355	69.60	0.00	-0.19	4.92
256	256	71.00	0.00	-0.23	3.86
256	356	71.00	0.00	-0.23	5.03
257	257	72.40	0.00	-0.28	3.74
257	357	72.40	0.00	-0.28	5.15
258	258	73.80	0.00	-0.33	3.61
258	358	73.80	0.00	-0.33	5.28
259	259	75.20	0.00	-0.37	3.50
259	359	75.20	0.00	-0.37	5.39
260	260	76.60	0.00	-0.41	3.42
260	360	76.60	0.00	-0.41	5.47
261	261	78.00	0.00	-0.38	3.02
261	361	78.00	0.00	-0.38	4.92
262	262	79.10	0.00	-0.32	2.67
262	362	79.10	0.00	-0.32	4.31
263	263	80.20	0.00	-0.31	2.71
263	363	80.20	0.00	-0.31	4.27
264	264	81.30	0.00	-0.29	2.77
264	364	81.30	0.00	-0.29	4.22
265	265	82.40	0.00	-0.26	2.84
265	365	82.40	0.00	-0.26	4.15
266	266	83.50	0.00	-0.23	2.91
266	366	83.50	0.00	-0.23	4.08
267	267	84.60	0.00	-0.20	2.98
267	367	84.60	0.00	-0.20	4.01
268	268	85.70	0.00	-0.18	3.04
268	368	85.70	0.00	-0.18	3.94
269	269	86.80	0.00	-0.16	3.10
269	369	86.80	0.00	-0.16	3.88
270	270	87.90	0.00	-0.14	3.15
270	370	87.90	0.00	-0.14	3.84
271	271	89.00	0.00	-0.12	3.18
271	371	89.00	0.00	-0.12	3.81
272	272	90.10	0.00	-0.12	3.20
272	372	90.10	0.00	-0.12	3.79
273	273	91.20	0.00	-0.12	3.20
273	373	91.20	0.00	-0.12	3.79
274	274	92.30	0.00	-0.12	3.18
274	374	92.30	0.00	-0.12	3.80
275	275	93.40	0.00	-0.14	3.15
275	375	93.40	0.00	-0.14	3.84
276	276	94.50	0.00	-0.16	3.10
276	376	94.50	0.00	-0.16	3.89
277	277	95.60	0.00	-0.18	3.03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMBALASTO

Carga muerta balasto

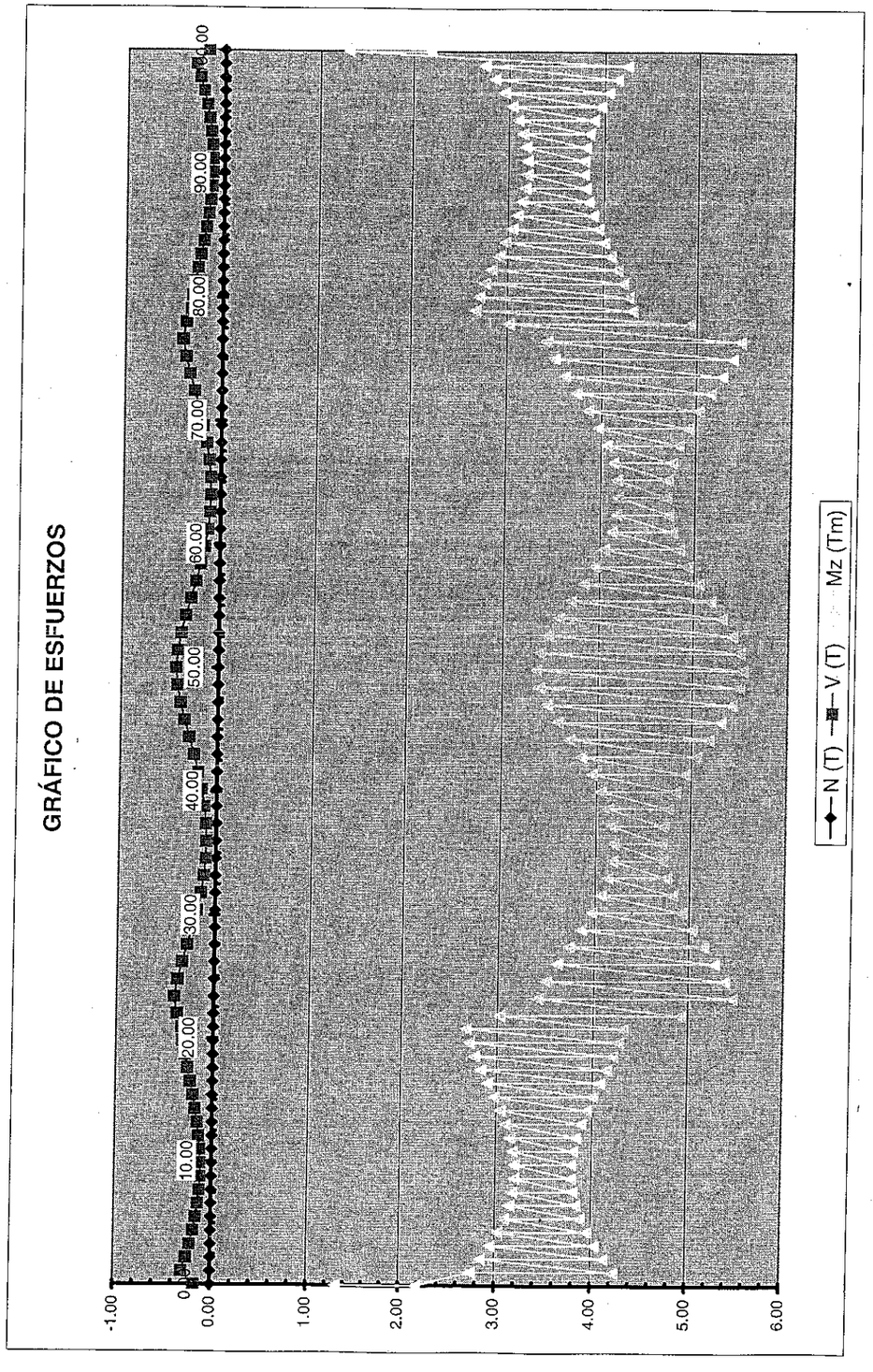
[1; 1]CMBALASTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	-0.18	3.95
278	278	96.70	0.00	-0.22	2.95
278	378	96.70	0.00	-0.22	4.04
279	279	97.80	0.00	-0.25	2.85
279	379	97.80	0.00	-0.25	4.13
280	280	98.90	0.00	-0.30	2.74
280	380	98.90	0.00	-0.30	4.24
281	281	100.00	0.00	-0.17	1.32
281	381	100.00	0.00	-0.17	2.18

15/09/03

Programa DINTEL PACADAR S.A.
CMBALASTO



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CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	-3.38
201	301	0.00	0.00	0.00	-3.38
202	202	1.10	0.00	0.00	-6.75
202	302	1.10	0.00	0.00	-6.75
203	203	2.20	0.00	0.00	-6.75
203	303	2.20	0.00	0.00	-6.75
204	204	3.30	0.00	0.00	-6.75
204	304	3.30	0.00	0.00	-6.75
205	205	4.40	0.00	0.00	-6.75
205	305	4.40	0.00	0.00	-6.75
206	206	5.50	0.00	0.00	-6.75
206	306	5.50	0.00	0.00	-6.75
207	207	6.60	0.00	0.00	-6.75
207	307	6.60	0.00	0.00	-6.75
208	208	7.70	0.00	0.00	-6.75
208	308	7.70	0.00	0.00	-6.75
209	209	8.80	0.00	0.00	-6.75
209	309	8.80	0.00	0.00	-6.75
210	210	9.90	0.00	0.00	-6.75
210	310	9.90	0.00	0.00	-6.75
211	211	11.00	0.00	0.00	-6.75
211	311	11.00	0.00	0.00	-6.75
212	212	12.10	0.00	0.00	-6.75
212	312	12.10	0.00	0.00	-6.75
213	213	13.20	0.00	0.00	-6.75
213	313	13.20	0.00	0.00	-6.75
214	214	14.30	0.00	0.00	-6.75
214	314	14.30	0.00	0.00	-6.75
215	215	15.40	0.00	0.00	-6.75
215	315	15.40	0.00	0.00	-6.75
216	216	16.50	0.00	0.00	-6.75
216	316	16.50	0.00	0.00	-6.75
217	217	17.60	0.00	0.00	-6.75
217	317	17.60	0.00	0.00	-6.75
218	218	18.70	0.00	0.00	-6.75
218	318	18.70	0.00	0.00	-6.75
219	219	19.80	0.00	0.00	-6.75
219	319	19.80	0.00	0.00	-6.75
220	220	20.90	0.00	0.00	-6.75
220	320	20.90	0.00	0.00	-6.75
221	221	22.00	0.00	0.00	-7.67
221	321	22.00	0.00	0.00	-7.67
222	222	23.40	0.00	0.00	-8.59
222	322	23.40	0.00	0.00	-8.59
223	223	24.80	0.00	0.00	-8.59
223	323	24.80	0.00	0.00	-8.59
224	224	26.20	0.00	0.00	-8.59
224	324	26.20	0.00	0.00	-8.59
225	225	27.60	0.00	0.00	-8.59
225	325	27.60	0.00	0.00	-8.59
226	226	29.00	0.00	0.00	-8.59

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-8.59
227	227	30.40	0.00	0.00	-8.59
227	327	30.40	0.00	0.00	-8.59
228	228	31.80	0.00	0.00	-8.59
228	328	31.80	0.00	0.00	-8.59
229	229	33.20	0.00	0.00	-8.59
229	329	33.20	0.00	0.00	-8.59
230	230	34.60	0.00	0.00	-8.59
230	330	34.60	0.00	0.00	-8.59
231	231	36.00	0.00	0.00	-8.59
231	331	36.00	0.00	0.00	-8.59
232	232	37.40	0.00	0.00	-8.59
232	332	37.40	0.00	0.00	-8.59
233	233	38.80	0.00	0.00	-8.59
233	333	38.80	0.00	0.00	-8.59
234	234	40.20	0.00	0.00	-8.59
234	334	40.20	0.00	0.00	-8.59
235	235	41.60	0.00	0.00	-8.59
235	335	41.60	0.00	0.00	-8.59
236	236	43.00	0.00	0.00	-8.59
236	336	43.00	0.00	0.00	-8.59
237	237	44.40	0.00	0.00	-8.59
237	337	44.40	0.00	0.00	-8.59
238	238	45.80	0.00	0.00	-8.59
238	338	45.80	0.00	0.00	-8.59
239	239	47.20	0.00	0.00	-8.59
239	339	47.20	0.00	0.00	-8.59
240	240	48.60	0.00	0.00	-8.59
240	340	48.60	0.00	0.00	-8.59
241	241	50.00	0.00	0.00	-8.59
241	341	50.00	0.00	0.00	-8.59
242	242	51.40	0.00	0.00	-8.59
242	342	51.40	0.00	0.00	-8.59
243	243	52.80	0.00	0.00	-8.59
243	343	52.80	0.00	0.00	-8.59
244	244	54.20	0.00	0.00	-8.59
244	344	54.20	0.00	0.00	-8.59
245	245	55.60	0.00	0.00	-8.59
245	345	55.60	0.00	0.00	-8.59
246	246	57.00	0.00	0.00	-8.59
246	346	57.00	0.00	0.00	-8.59
247	247	58.40	0.00	0.00	-8.59
247	347	58.40	0.00	0.00	-8.59
248	248	59.80	0.00	0.00	-8.59
248	348	59.80	0.00	0.00	-8.59
249	249	61.20	0.00	0.00	-8.59
249	349	61.20	0.00	0.00	-8.59
250	250	62.60	0.00	0.00	-8.59
250	350	62.60	0.00	0.00	-8.59
251	251	64.00	0.00	0.00	-8.59
251	351	64.00	0.00	0.00	-8.59

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-8.59
252	352	65.40	0.00	0.00	-8.59
253	253	66.80	0.00	0.00	-8.59
253	353	66.80	0.00	0.00	-8.59
254	254	68.20	0.00	0.00	-8.59
254	354	68.20	0.00	0.00	-8.59
255	255	69.60	0.00	0.00	-8.59
255	355	69.60	0.00	0.00	-8.59
256	256	71.00	0.00	0.00	-8.59
256	356	71.00	0.00	0.00	-8.59
257	257	72.40	0.00	0.00	-8.59
257	357	72.40	0.00	0.00	-8.59
258	258	73.80	0.00	0.00	-8.59
258	358	73.80	0.00	0.00	-8.59
259	259	75.20	0.00	0.00	-8.59
259	359	75.20	0.00	0.00	-8.59
260	260	76.60	0.00	0.00	-8.59
260	360	76.60	0.00	0.00	-8.59
261	261	78.00	0.00	0.00	-7.67
261	361	78.00	0.00	0.00	-7.67
262	262	79.10	0.00	0.00	-6.75
262	362	79.10	0.00	0.00	-6.75
263	263	80.20	0.00	0.00	-6.75
263	363	80.20	0.00	0.00	-6.75
264	264	81.30	0.00	0.00	-6.75
264	364	81.30	0.00	0.00	-6.75
265	265	82.40	0.00	0.00	-6.75
265	365	82.40	0.00	0.00	-6.75
266	266	83.50	0.00	0.00	-6.75
266	366	83.50	0.00	0.00	-6.75
267	267	84.60	0.00	0.00	-6.75
267	367	84.60	0.00	0.00	-6.75
268	268	85.70	0.00	0.00	-6.75
268	368	85.70	0.00	0.00	-6.75
269	269	86.80	0.00	0.00	-6.75
269	369	86.80	0.00	0.00	-6.75
270	270	87.90	0.00	0.00	-6.75
270	370	87.90	0.00	0.00	-6.75
271	271	89.00	0.00	0.00	-6.75
271	371	89.00	0.00	0.00	-6.75
272	272	90.10	0.00	0.00	-6.75
272	372	90.10	0.00	0.00	-6.75
273	273	91.20	0.00	0.00	-6.75
273	373	91.20	0.00	0.00	-6.75
274	274	92.30	0.00	0.00	-6.75
274	374	92.30	0.00	0.00	-6.75
275	275	93.40	0.00	0.00	-6.75
275	375	93.40	0.00	0.00	-6.75
276	276	94.50	0.00	0.00	-6.75
276	376	94.50	0.00	0.00	-6.75
277	277	95.60	0.00	0.00	-6.75

CÁLCULO TENSIONAL

Hipótesis de cálculo:
CMRESTO

Resto de carga muerta

[1; 1]CMRESTO

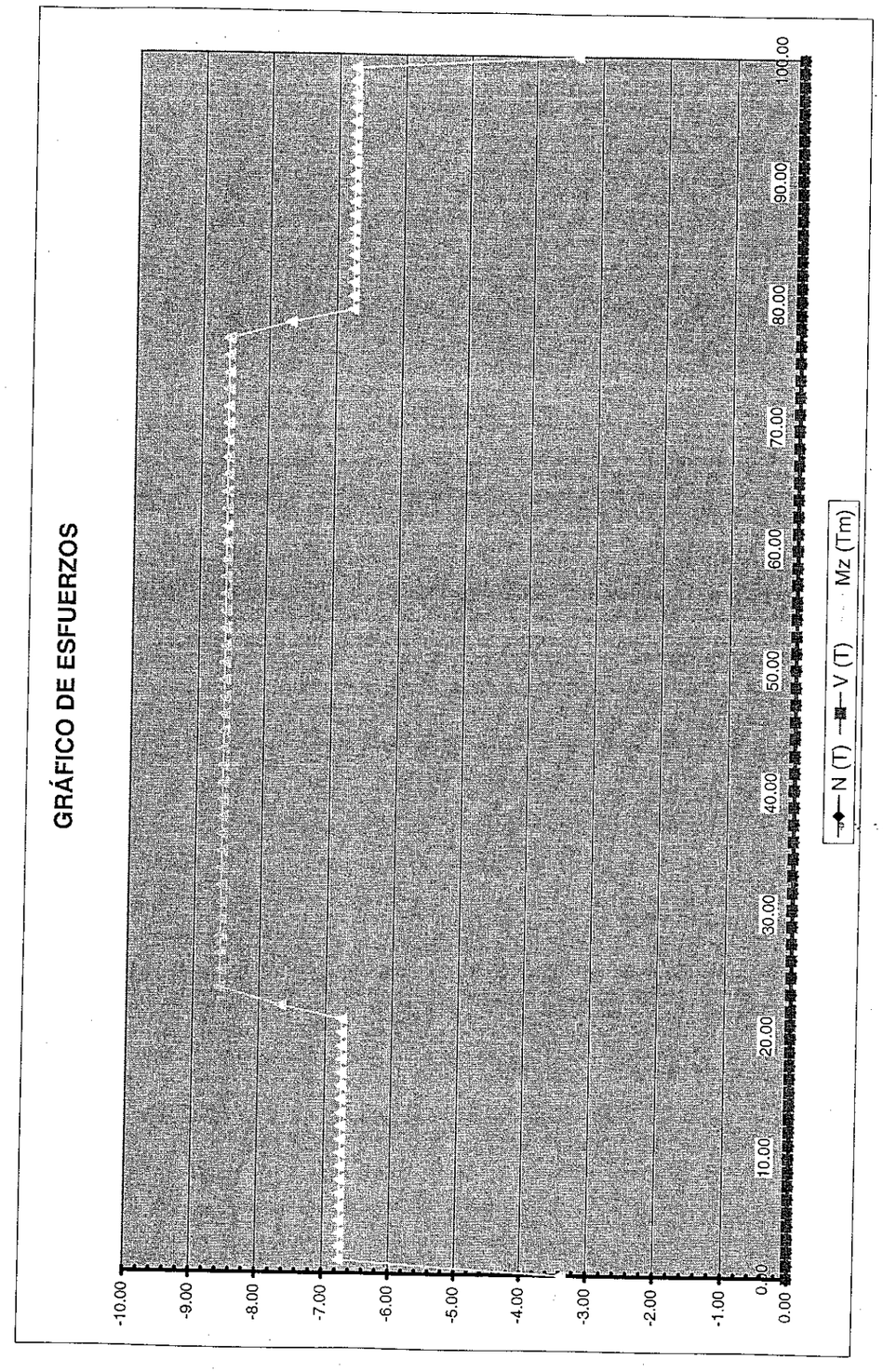
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-6.75
278	278	96.70	0.00	0.00	-6.75
278	378	96.70	0.00	0.00	-6.75
279	279	97.80	0.00	0.00	-6.75
279	379	97.80	0.00	0.00	-6.75
280	280	98.90	0.00	0.00	-6.75
280	380	98.90	0.00	0.00	-6.75
281	281	100.00	0.00	0.00	-3.38
281	381	100.00	0.00	0.00	-3.38

15/09/03

Programa DINTEL PACADAR S.A.
CMRESTO

~csimp4.esv



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ+
ENVOLVENTE SC PASEO MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	0.28
201	301	0.00	0.00	0.00	0.28
202	202	1.10	0.00	0.00	0.41
202	302	1.10	0.00	0.00	0.41
203	203	2.20	0.00	0.00	0.27
203	303	2.20	0.00	0.00	0.27
204	204	3.30	0.00	0.00	0.15
204	304	3.30	0.00	0.00	0.15
205	205	4.40	0.00	0.00	0.07
205	305	4.40	0.00	0.00	0.07
206	206	5.50	0.00	0.00	0.03
206	306	5.50	0.00	0.00	0.03
207	207	6.60	0.00	0.00	0.00
207	307	6.60	0.00	0.00	0.00
208	208	7.70	0.00	0.00	0.00
208	308	7.70	0.00	0.00	0.00
209	209	8.80	0.00	0.00	0.01
209	309	8.80	0.00	0.00	0.01
210	210	9.90	0.00	0.00	0.03
210	310	9.90	0.00	0.00	0.03
211	211	11.00	0.00	0.00	0.05
211	311	11.00	0.00	0.00	0.05
212	212	12.10	0.00	0.00	0.07
212	312	12.10	0.00	0.00	0.07
213	213	13.20	0.00	0.00	0.10
213	313	13.20	0.00	0.00	0.10
214	214	14.30	0.00	0.00	0.13
214	314	14.30	0.00	0.00	0.13
215	215	15.40	0.00	0.00	0.16
215	315	15.40	0.00	0.00	0.16
216	216	16.50	0.00	0.00	0.19
216	316	16.50	0.00	0.00	0.19
217	217	17.60	0.00	0.00	0.23
217	317	17.60	0.00	0.00	0.23
218	218	18.70	0.00	0.00	0.27
218	318	18.70	0.00	0.00	0.27
219	219	19.80	0.00	0.00	0.31
219	319	19.80	0.00	0.00	0.31
220	220	20.90	0.00	0.00	0.34
220	320	20.90	0.00	0.00	0.34
221	221	22.00	0.00	0.00	0.41
221	321	22.00	0.00	0.00	0.41
222	222	23.40	0.00	0.00	0.42
222	322	23.40	0.00	0.00	0.42
223	223	24.80	0.00	0.00	0.33
223	323	24.80	0.00	0.00	0.33
224	224	26.20	0.00	0.00	0.27
224	324	26.20	0.00	0.00	0.27
225	225	27.60	0.00	0.00	0.21
225	325	27.60	0.00	0.00	0.21
226	226	29.00	0.00	0.00	0.16

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Programa DINTEL PACADAR S.A.
ENVOLVENTE SC PASEO MZ+

15/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ+
ENVOLVENTE SC PASEO MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	0.16
227	227	30.40	0.00	0.00	0.12
227	327	30.40	0.00	0.00	0.12
228	228	31.80	0.00	0.00	0.08
228	328	31.80	0.00	0.00	0.08
229	229	33.20	0.00	0.00	0.06
229	329	33.20	0.00	0.00	0.06
230	230	34.60	0.00	0.00	0.05
230	330	34.60	0.00	0.00	0.05
231	231	36.00	0.00	0.00	0.06
231	331	36.00	0.00	0.00	0.06
232	232	37.40	0.00	0.00	0.08
232	332	37.40	0.00	0.00	0.08
233	233	38.80	0.00	0.00	0.12
233	333	38.80	0.00	0.00	0.12
234	234	40.20	0.00	0.00	0.16
234	334	40.20	0.00	0.00	0.16
235	235	41.60	0.00	0.00	0.21
235	335	41.60	0.00	0.00	0.21
236	236	43.00	0.00	0.00	0.25
236	336	43.00	0.00	0.00	0.25
237	237	44.40	0.00	0.00	0.32
237	337	44.40	0.00	0.00	0.32
238	238	45.80	0.00	0.00	0.39
238	338	45.80	0.00	0.00	0.39
239	239	47.20	0.00	0.00	0.46
239	339	47.20	0.00	0.00	0.46
240	240	48.60	0.00	0.00	0.55
240	340	48.60	0.00	0.00	0.55
241	241	50.00	0.00	0.00	0.59
241	341	50.00	0.00	0.00	0.59
242	242	51.40	0.00	0.00	0.55
242	342	51.40	0.00	0.00	0.55
243	243	52.80	0.00	0.00	0.46
243	343	52.80	0.00	0.00	0.46
244	244	54.20	0.00	0.00	0.39
244	344	54.20	0.00	0.00	0.39
245	245	55.60	0.00	0.00	0.32
245	345	55.60	0.00	0.00	0.32
246	246	57.00	0.00	0.00	0.25
246	346	57.00	0.00	0.00	0.25
247	247	58.40	0.00	0.00	0.21
247	347	58.40	0.00	0.00	0.21
248	248	59.80	0.00	0.00	0.16
248	348	59.80	0.00	0.00	0.16
249	249	61.20	0.00	0.00	0.12
249	349	61.20	0.00	0.00	0.12
250	250	62.60	0.00	0.00	0.08
250	350	62.60	0.00	0.00	0.08
251	251	64.00	0.00	0.00	0.06
251	351	64.00	0.00	0.00	0.06

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ+
ENVOLVENTE SC PASEO MZ+

Coef. exc:

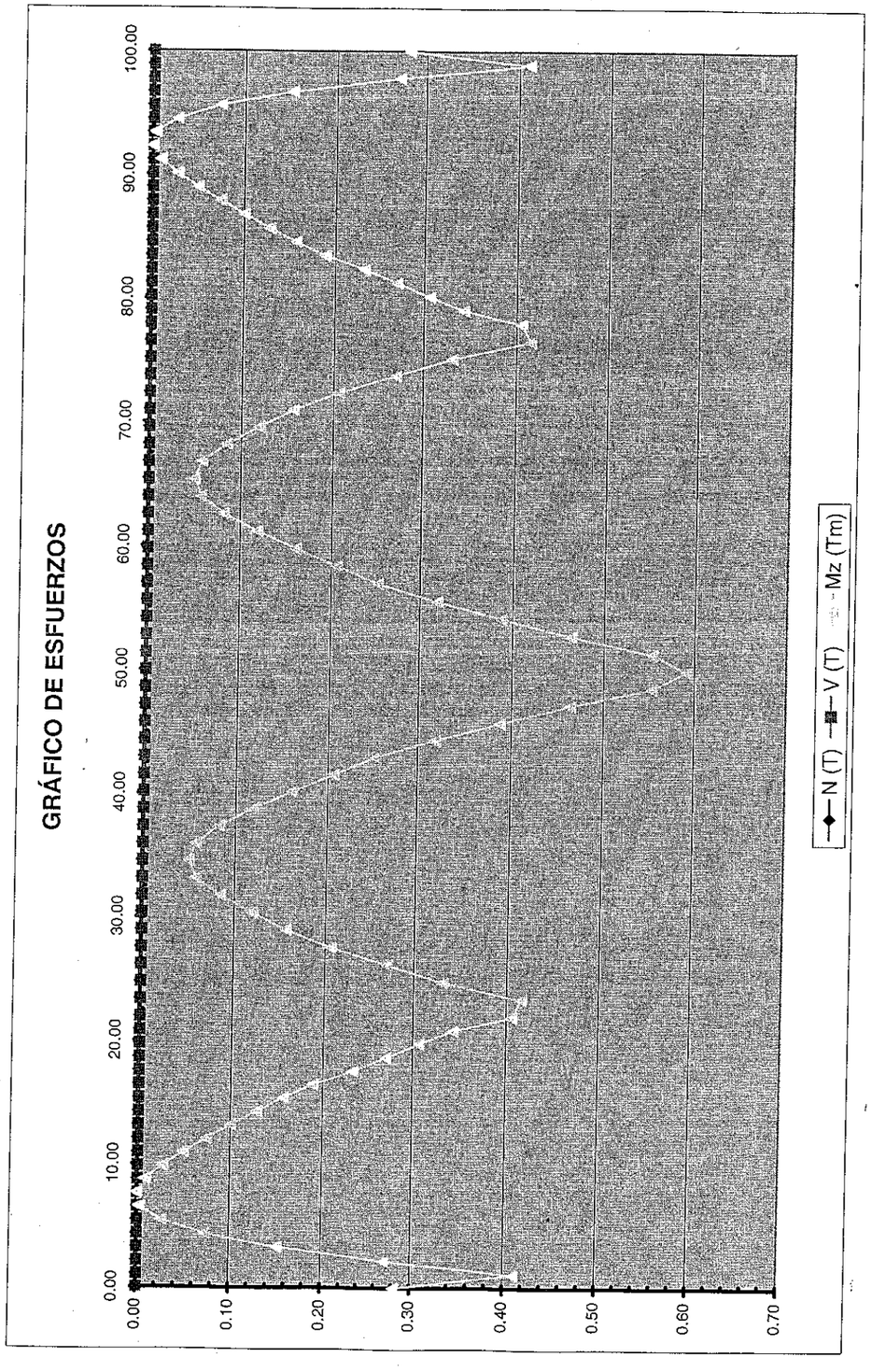
Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	0.05
252	352	65.40	0.00	0.00	0.05
253	253	66.80	0.00	0.00	0.06
253	353	66.80	0.00	0.00	0.06
254	254	68.20	0.00	0.00	0.08
254	354	68.20	0.00	0.00	0.08
255	255	69.60	0.00	0.00	0.12
255	355	69.60	0.00	0.00	0.12
256	256	71.00	0.00	0.00	0.16
256	356	71.00	0.00	0.00	0.16
257	257	72.40	0.00	0.00	0.21
257	357	72.40	0.00	0.00	0.21
258	258	73.80	0.00	0.00	0.27
258	358	73.80	0.00	0.00	0.27
259	259	75.20	0.00	0.00	0.33
259	359	75.20	0.00	0.00	0.33
260	260	76.60	0.00	0.00	0.42
260	360	76.60	0.00	0.00	0.42
261	261	78.00	0.00	0.00	0.41
261	361	78.00	0.00	0.00	0.41
262	262	79.10	0.00	0.00	0.34
262	362	79.10	0.00	0.00	0.34
263	263	80.20	0.00	0.00	0.31
263	363	80.20	0.00	0.00	0.31
264	264	81.30	0.00	0.00	0.27
264	364	81.30	0.00	0.00	0.27
265	265	82.40	0.00	0.00	0.23
265	365	82.40	0.00	0.00	0.23
266	266	83.50	0.00	0.00	0.19
266	366	83.50	0.00	0.00	0.19
267	267	84.60	0.00	0.00	0.16
267	367	84.60	0.00	0.00	0.16
268	268	85.70	0.00	0.00	0.13
268	368	85.70	0.00	0.00	0.13
269	269	86.80	0.00	0.00	0.10
269	369	86.80	0.00	0.00	0.10
270	270	87.90	0.00	0.00	0.07
270	370	87.90	0.00	0.00	0.07
271	271	89.00	0.00	0.00	0.05
271	371	89.00	0.00	0.00	0.05
272	272	90.10	0.00	0.00	0.03
272	372	90.10	0.00	0.00	0.03
273	273	91.20	0.00	0.00	0.01
273	373	91.20	0.00	0.00	0.01
274	274	92.30	0.00	0.00	0.00
274	374	92.30	0.00	0.00	0.00
275	275	93.40	0.00	0.00	0.00
275	375	93.40	0.00	0.00	0.00
276	276	94.50	0.00	0.00	0.03
276	376	94.50	0.00	0.00	0.03
277	277	95.60	0.00	0.00	0.07

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ+
ENVOLVENTE SC PASEO MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	0.07
278	278	96.70	0.00	0.00	0.15
278	378	96.70	0.00	0.00	0.15
279	279	97.80	0.00	0.00	0.27
279	379	97.80	0.00	0.00	0.27
280	280	98.90	0.00	0.00	0.41
280	380	98.90	0.00	0.00	0.41
281	281	100.00	0.00	0.00	0.28
281	381	100.00	0.00	0.00	0.28



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ-
ENVOLVENTE SC PASEO MZ-
[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [0; 1]SCPAS2.S
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	-1.54
201	301	0.00	0.00	0.00	-1.54
202	202	1.10	0.00	0.00	-2.93
202	302	1.10	0.00	0.00	-2.93
203	203	2.20	0.00	0.00	-2.79
203	303	2.20	0.00	0.00	-2.79
204	204	3.30	0.00	0.00	-2.67
204	304	3.30	0.00	0.00	-2.67
205	205	4.40	0.00	0.00	-2.59
205	305	4.40	0.00	0.00	-2.59
206	206	5.50	0.00	0.00	-2.54
206	306	5.50	0.00	0.00	-2.54
207	207	6.60	0.00	0.00	-2.52
207	307	6.60	0.00	0.00	-2.52
208	208	7.70	0.00	0.00	-2.52
208	308	7.70	0.00	0.00	-2.52
209	209	8.80	0.00	0.00	-2.53
209	309	8.80	0.00	0.00	-2.53
210	210	9.90	0.00	0.00	-2.54
210	310	9.90	0.00	0.00	-2.54
211	211	11.00	0.00	0.00	-2.57
211	311	11.00	0.00	0.00	-2.57
212	212	12.10	0.00	0.00	-2.59
212	312	12.10	0.00	0.00	-2.59
213	213	13.20	0.00	0.00	-2.62
213	313	13.20	0.00	0.00	-2.62
214	214	14.30	0.00	0.00	-2.65
214	314	14.30	0.00	0.00	-2.64
215	215	15.40	0.00	0.00	-2.67
215	315	15.40	0.00	0.00	-2.67
216	216	16.50	0.00	0.00	-2.71
216	316	16.50	0.00	0.00	-2.71
217	217	17.60	0.00	0.00	-2.75
217	317	17.60	0.00	0.00	-2.75
218	218	18.70	0.00	0.00	-2.79
218	318	18.70	0.00	0.00	-2.79
219	219	19.80	0.00	0.00	-2.82
219	319	19.80	0.00	0.00	-2.82
220	220	20.90	0.00	0.00	-2.86
220	320	20.90	0.00	0.00	-2.86
221	221	22.00	0.00	0.00	-3.27
221	321	22.00	0.00	0.00	-3.27
222	222	23.40	0.00	0.00	-3.62
222	322	23.40	0.00	0.00	-3.62
223	223	24.80	0.00	0.00	-3.53
223	323	24.80	0.00	0.00	-3.53
224	224	26.20	0.00	0.00	-3.47
224	324	26.20	0.00	0.00	-3.47
225	225	27.60	0.00	0.00	-3.41
225	325	27.60	0.00	0.00	-3.41
226	226	29.00	0.00	0.00	-3.36

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ-
ENVOLVENTE SC PASEO MZ-

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [0; 1]SCPAS2.S

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-3.36
227	227	30.40	0.00	0.00	-3.32
227	327	30.40	0.00	0.00	-3.32
228	228	31.80	0.00	0.00	-3.29
228	328	31.80	0.00	0.00	-3.29
229	229	33.20	0.00	0.00	-3.26
229	329	33.20	0.00	0.00	-3.26
230	230	34.60	0.00	0.00	-3.25
230	330	34.60	0.00	0.00	-3.25
231	231	36.00	0.00	0.00	-3.26
231	331	36.00	0.00	0.00	-3.26
232	232	37.40	0.00	0.00	-3.28
232	332	37.40	0.00	0.00	-3.28
233	233	38.80	0.00	0.00	-3.32
233	333	38.80	0.00	0.00	-3.32
234	234	40.20	0.00	0.00	-3.36
234	334	40.20	0.00	0.00	-3.36
235	235	41.60	0.00	0.00	-3.41
235	335	41.60	0.00	0.00	-3.41
236	236	43.00	0.00	0.00	-3.46
236	336	43.00	0.00	0.00	-3.46
237	237	44.40	0.00	0.00	-3.52
237	337	44.40	0.00	0.00	-3.52
238	238	45.80	0.00	0.00	-3.59
238	338	45.80	0.00	0.00	-3.59
239	239	47.20	0.00	0.00	-3.67
239	339	47.20	0.00	0.00	-3.67
240	240	48.60	0.00	0.00	-3.76
240	340	48.60	0.00	0.00	-3.76
241	241	50.00	0.00	0.00	-3.79
241	341	50.00	0.00	0.00	-3.79
242	242	51.40	0.00	0.00	-3.76
242	342	51.40	0.00	0.00	-3.76
243	243	52.80	0.00	0.00	-3.67
243	343	52.80	0.00	0.00	-3.67
244	244	54.20	0.00	0.00	-3.59
244	344	54.20	0.00	0.00	-3.59
245	245	55.60	0.00	0.00	-3.52
245	345	55.60	0.00	0.00	-3.52
246	246	57.00	0.00	0.00	-3.46
246	346	57.00	0.00	0.00	-3.46
247	247	58.40	0.00	0.00	-3.41
247	347	58.40	0.00	0.00	-3.41
248	248	59.80	0.00	0.00	-3.36
248	348	59.80	0.00	0.00	-3.36
249	249	61.20	0.00	0.00	-3.32
249	349	61.20	0.00	0.00	-3.32
250	250	62.60	0.00	0.00	-3.28
250	350	62.60	0.00	0.00	-3.28
251	251	64.00	0.00	0.00	-3.26
251	351	64.00	0.00	0.00	-3.26

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ-
ENVOLVENTE SC PASEO MZ-

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [0; 1]SCPAS2.S

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-3.25
252	352	65.40	0.00	0.00	-3.25
253	253	66.80	0.00	0.00	-3.26
253	353	66.80	0.00	0.00	-3.26
254	254	68.20	0.00	0.00	-3.29
254	354	68.20	0.00	0.00	-3.29
255	255	69.60	0.00	0.00	-3.32
255	355	69.60	0.00	0.00	-3.32
256	256	71.00	0.00	0.00	-3.36
256	356	71.00	0.00	0.00	-3.36
257	257	72.40	0.00	0.00	-3.41
257	357	72.40	0.00	0.00	-3.41
258	258	73.80	0.00	0.00	-3.47
258	358	73.80	0.00	0.00	-3.47
259	259	75.20	0.00	0.00	-3.53
259	359	75.20	0.00	0.00	-3.53
260	260	76.60	0.00	0.00	-3.62
260	360	76.60	0.00	0.00	-3.62
261	261	78.00	0.00	0.00	-3.27
261	361	78.00	0.00	0.00	-3.27
262	262	79.10	0.00	0.00	-2.86
262	362	79.10	0.00	0.00	-2.86
263	263	80.20	0.00	0.00	-2.82
263	363	80.20	0.00	0.00	-2.82
264	264	81.30	0.00	0.00	-2.79
264	364	81.30	0.00	0.00	-2.79
265	265	82.40	0.00	0.00	-2.75
265	365	82.40	0.00	0.00	-2.75
266	266	83.50	0.00	0.00	-2.71
266	366	83.50	0.00	0.00	-2.71
267	267	84.60	0.00	0.00	-2.67
267	367	84.60	0.00	0.00	-2.67
268	268	85.70	0.00	0.00	-2.65
268	368	85.70	0.00	0.00	-2.64
269	269	86.80	0.00	0.00	-2.62
269	369	86.80	0.00	0.00	-2.62
270	270	87.90	0.00	0.00	-2.59
270	370	87.90	0.00	0.00	-2.59
271	271	89.00	0.00	0.00	-2.57
271	371	89.00	0.00	0.00	-2.57
272	272	90.10	0.00	0.00	-2.54
272	372	90.10	0.00	0.00	-2.54
273	273	91.20	0.00	0.00	-2.53
273	373	91.20	0.00	0.00	-2.53
274	274	92.30	0.00	0.00	-2.52
274	374	92.30	0.00	0.00	-2.52
275	275	93.40	0.00	0.00	-2.52
275	375	93.40	0.00	0.00	-2.52
276	276	94.50	0.00	0.00	-2.54
276	376	94.50	0.00	0.00	-2.54
277	277	95.60	0.00	0.00	-2.59

CÁLCULO TENSIONAL

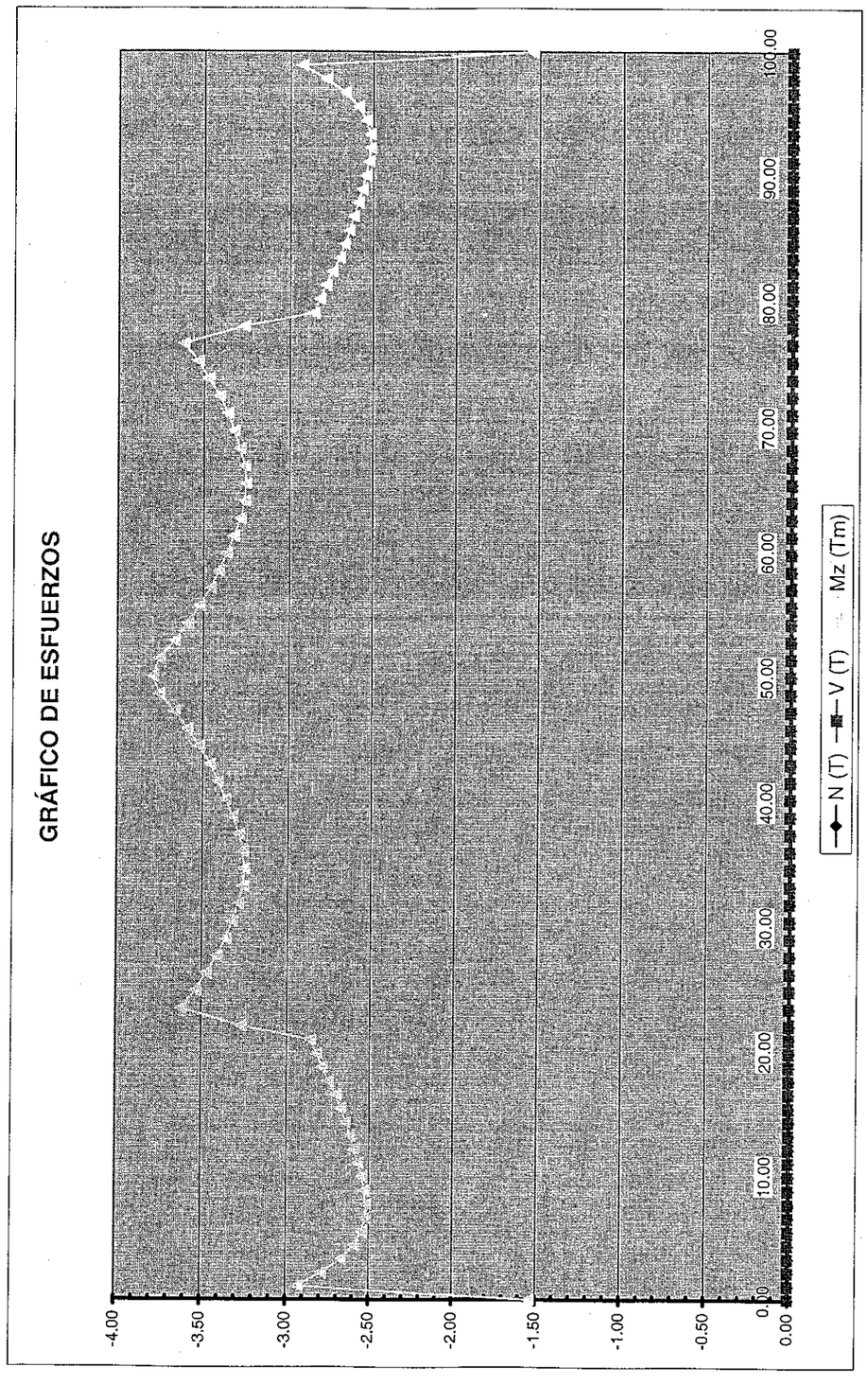
Hipótesis de cálculo:
ENVOLVENTE SC PASEO MZ-

ENVOLVENTE SC PASEO MZ-

[0; 1]SCPAS2.SCuniTpos.Barra101.Mx+ + [0; 1]SCPAS2.SCuniTpos.Barra102.Mx+ + [0; 1]SCPAS2.S

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-2.59
278	278	96.70	0.00	0.00	-2.67
278	378	96.70	0.00	0.00	-2.67
279	279	97.80	0.00	0.00	-2.79
279	379	97.80	0.00	0.00	-2.79
280	280	98.90	0.00	0.00	-2.93
280	380	98.90	0.00	0.00	-2.93
281	281	100.00	0.00	0.00	-1.54
281	381	100.00	0.00	0.00	-1.54



CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE TREN A MZ+

ENVOLVENTE TREN A MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	6.15
201	301	0.00	0.00	0.00	4.90
202	202	1.10	0.00	0.00	12.04
202	302	1.10	0.00	0.00	9.91
203	203	2.20	0.00	0.00	12.05
203	303	2.20	0.00	0.00	10.20
204	204	3.30	0.00	0.00	12.31
204	304	3.30	0.00	0.00	10.67
205	205	4.40	0.00	0.00	12.85
205	305	4.40	0.00	0.00	11.33
206	206	5.50	0.00	0.00	13.46
206	306	5.50	0.00	0.00	11.99
207	207	6.60	0.00	0.00	13.99
207	307	6.60	0.00	0.00	12.60
208	208	7.70	0.00	0.00	14.42
208	308	7.70	0.00	0.00	13.16
209	209	8.80	0.00	0.00	14.78
209	309	8.80	0.00	0.00	13.59
210	210	9.90	0.00	0.00	15.03
210	310	9.90	0.00	0.00	13.88
211	211	11.00	0.00	0.00	15.17
211	311	11.00	0.00	0.00	14.02
212	212	12.10	0.00	0.00	15.21
212	312	12.10	0.00	0.00	14.01
213	213	13.20	0.00	0.00	15.11
213	313	13.20	0.00	0.00	13.85
214	214	14.30	0.00	0.00	14.86
214	314	14.30	0.00	0.00	13.53
215	215	15.40	0.00	0.00	14.49
215	315	15.40	0.00	0.00	13.06
216	216	16.50	0.00	0.00	14.02
216	316	16.50	0.00	0.00	12.47
217	217	17.60	0.00	0.00	13.44
217	317	17.60	0.00	0.00	11.79
218	218	18.70	0.00	0.00	12.84
218	318	18.70	0.00	0.00	11.06
219	219	19.80	0.00	0.00	12.34
219	319	19.80	0.00	0.00	10.40
220	220	20.90	0.00	0.00	12.00
220	320	20.90	0.00	0.00	9.89
221	221	22.00	0.00	0.00	13.43
221	321	22.00	0.00	0.00	10.87
222	222	23.40	0.00	0.00	15.09
222	322	23.40	0.00	0.00	12.29
223	223	24.80	0.00	0.00	15.66
223	323	24.80	0.00	0.00	13.13
224	224	26.20	0.00	0.00	16.56
224	324	26.20	0.00	0.00	14.37
225	225	27.60	0.00	0.00	17.65
225	325	27.60	0.00	0.00	15.73
226	226	29.00	0.00	0.00	18.74

CÁLCULO TENSIONAL

Hipótesis de cálculo:

ENVOLVENTE TREN A MZ+

ENVOLVENTE TREN A MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	17.01
227	227	30.40	0.00	0.00	19.65
227	327	30.40	0.00	0.00	18.12
228	228	31.80	0.00	0.00	20.38
228	328	31.80	0.00	0.00	19.06
229	229	33.20	0.00	0.00	20.95
229	329	33.20	0.00	0.00	19.77
230	230	34.60	0.00	0.00	21.31
230	330	34.60	0.00	0.00	20.23
231	231	36.00	0.00	0.00	21.50
231	331	36.00	0.00	0.00	20.43
232	232	37.40	0.00	0.00	21.52
232	332	37.40	0.00	0.00	20.40
233	233	38.80	0.00	0.00	21.33
233	333	38.80	0.00	0.00	20.08
234	234	40.20	0.00	0.00	20.92
234	334	40.20	0.00	0.00	19.52
235	235	41.60	0.00	0.00	20.28
235	335	41.60	0.00	0.00	18.75
236	236	43.00	0.00	0.00	19.40
236	336	43.00	0.00	0.00	17.72
237	237	44.40	0.00	0.00	18.31
237	337	44.40	0.00	0.00	16.46
238	238	45.80	0.00	0.00	17.12
238	338	45.80	0.00	0.00	15.09
239	239	47.20	0.00	0.00	16.02
239	339	47.20	0.00	0.00	13.76
240	240	48.60	0.00	0.00	15.18
240	340	48.60	0.00	0.00	12.66
241	241	50.00	0.00	0.00	14.81
241	341	50.00	0.00	0.00	12.01
242	242	51.40	0.00	0.00	15.18
242	342	51.40	0.00	0.00	12.66
243	243	52.80	0.00	0.00	16.02
243	343	52.80	0.00	0.00	13.76
244	244	54.20	0.00	0.00	17.12
244	344	54.20	0.00	0.00	15.09
245	245	55.60	0.00	0.00	18.31
245	345	55.60	0.00	0.00	16.46
246	246	57.00	0.00	0.00	19.40
246	346	57.00	0.00	0.00	17.72
247	247	58.40	0.00	0.00	20.28
247	347	58.40	0.00	0.00	18.75
248	248	59.80	0.00	0.00	20.92
248	348	59.80	0.00	0.00	19.52
249	249	61.20	0.00	0.00	21.33
249	349	61.20	0.00	0.00	20.09
250	250	62.60	0.00	0.00	21.52
250	350	62.60	0.00	0.00	20.40
251	251	64.00	0.00	0.00	21.50
251	351	64.00	0.00	0.00	20.43

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN A MZ+
ENVOLVENTE TREN A MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	21.31
252	352	65.40	0.00	0.00	20.23
253	253	66.80	0.00	0.00	20.95
253	353	66.80	0.00	0.00	19.77
254	254	68.20	0.00	0.00	20.38
254	354	68.20	0.00	0.00	19.06
255	255	69.60	0.00	0.00	19.65
255	355	69.60	0.00	0.00	18.12
256	256	71.00	0.00	0.00	18.74
256	356	71.00	0.00	0.00	17.01
257	257	72.40	0.00	0.00	17.65
257	357	72.40	0.00	0.00	15.73
258	258	73.80	0.00	0.00	16.56
258	358	73.80	0.00	0.00	14.37
259	259	75.20	0.00	0.00	15.66
259	359	75.20	0.00	0.00	13.13
260	260	76.60	0.00	0.00	15.09
260	360	76.60	0.00	0.00	12.29
261	261	78.00	0.00	0.00	13.43
261	361	78.00	0.00	0.00	10.87
262	262	79.10	0.00	0.00	12.00
262	362	79.10	0.00	0.00	9.89
263	263	80.20	0.00	0.00	12.34
263	363	80.20	0.00	0.00	10.40
264	264	81.30	0.00	0.00	12.84
264	364	81.30	0.00	0.00	11.06
265	265	82.40	0.00	0.00	13.44
265	365	82.40	0.00	0.00	11.79
266	266	83.50	0.00	0.00	14.02
266	366	83.50	0.00	0.00	12.47
267	267	84.60	0.00	0.00	14.49
267	367	84.60	0.00	0.00	13.06
268	268	85.70	0.00	0.00	14.86
268	368	85.70	0.00	0.00	13.53
269	269	86.80	0.00	0.00	15.11
269	369	86.80	0.00	0.00	13.85
270	270	87.90	0.00	0.00	15.21
270	370	87.90	0.00	0.00	14.01
271	271	89.00	0.00	0.00	15.17
271	371	89.00	0.00	0.00	14.02
272	272	90.10	0.00	0.00	15.03
272	372	90.10	0.00	0.00	13.88
273	273	91.20	0.00	0.00	14.78
273	373	91.20	0.00	0.00	13.59
274	274	92.30	0.00	0.00	14.42
274	374	92.30	0.00	0.00	13.16
275	275	93.40	0.00	0.00	13.99
275	375	93.40	0.00	0.00	12.60
276	276	94.50	0.00	0.00	13.46
276	376	94.50	0.00	0.00	11.99
277	277	95.60	0.00	0.00	12.85

CÁLCULO TENSIONAL

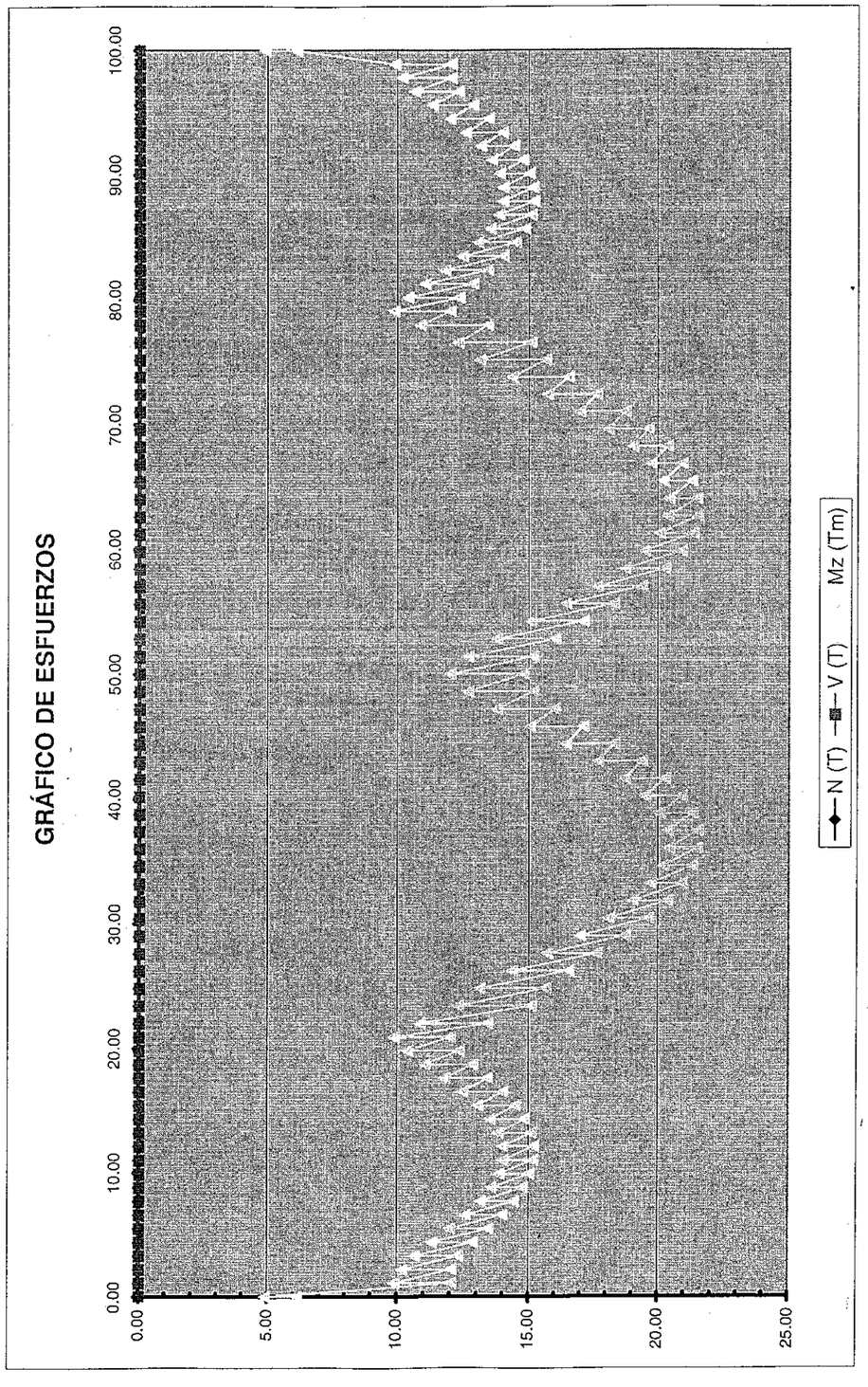
Hipótesis de cálculo:
ENVOLVENTE TREN A MZ+
ENVOLVENTE TREN A MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	11.33
278	278	96.70	0.00	0.00	12.31
278	378	96.70	0.00	0.00	10.67
279	279	97.80	0.00	0.00	12.05
279	379	97.80	0.00	0.00	10.20
280	280	98.90	0.00	0.00	12.04
280	380	98.90	0.00	0.00	9.91
281	281	100.00	0.00	0.00	6.15
281	381	100.00	0.00	0.00	4.90

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN A MZ+

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN A MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN A MZ-
ENVOLVENTE TREN A MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	0.35
201	301	0.00	0.00	0.00	0.23
202	202	1.10	0.00	0.00	0.78
202	302	1.10	0.00	0.00	0.50
203	203	2.20	0.00	0.00	0.66
203	303	2.20	0.00	0.00	0.38
204	204	3.30	0.00	0.00	0.26
204	304	3.30	0.00	0.00	0.00
205	205	4.40	0.00	0.00	-0.39
205	305	4.40	0.00	0.00	-0.54
206	206	5.50	0.00	0.00	-1.09
206	306	5.50	0.00	0.00	-1.12
207	207	6.60	0.00	0.00	-1.68
207	307	6.60	0.00	0.00	-1.65
208	208	7.70	0.00	0.00	-2.14
208	308	7.70	0.00	0.00	-2.14
209	209	8.80	0.00	0.00	-2.51
209	309	8.80	0.00	0.00	-2.53
210	210	9.90	0.00	0.00	-2.77
210	310	9.90	0.00	0.00	-2.82
211	211	11.00	0.00	0.00	-2.90
211	311	11.00	0.00	0.00	-2.99
212	212	12.10	0.00	0.00	-2.88
212	312	12.10	0.00	0.00	-3.02
213	213	13.20	0.00	0.00	-2.72
213	313	13.20	0.00	0.00	-2.91
214	214	14.30	0.00	0.00	-2.42
214	314	14.30	0.00	0.00	-2.68
215	215	15.40	0.00	0.00	-1.98
215	315	15.40	0.00	0.00	-2.31
216	216	16.50	0.00	0.00	-1.42
216	316	16.50	0.00	0.00	-1.81
217	217	17.60	0.00	0.00	-0.76
217	317	17.60	0.00	0.00	-1.22
218	218	18.70	0.00	0.00	-0.11
218	318	18.70	0.00	0.00	-0.62
219	219	19.80	0.00	0.00	0.43
219	319	19.80	0.00	0.00	-0.07
220	220	20.90	0.00	0.00	0.70
220	320	20.90	0.00	0.00	0.30
221	221	22.00	0.00	0.00	0.88
221	321	22.00	0.00	0.00	0.55
222	222	23.40	0.00	0.00	0.82
222	322	23.40	0.00	0.00	0.47
223	223	24.80	0.00	0.00	0.28
223	323	24.80	0.00	0.00	-0.11
224	224	26.20	0.00	0.00	-0.71
224	324	26.20	0.00	0.00	-1.16
225	225	27.60	0.00	0.00	-1.93
225	325	27.60	0.00	0.00	-2.35
226	226	29.00	0.00	0.00	-3.15

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN A MZ-
ENVOLVENTE TREN A MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-3.47
227	227	30.40	0.00	0.00	-4.22
227	327	30.40	0.00	0.00	-4.45
228	228	31.80	0.00	0.00	-5.07
228	328	31.80	0.00	0.00	-5.28
229	229	33.20	0.00	0.00	-5.75
229	329	33.20	0.00	0.00	-5.90
230	230	34.60	0.00	0.00	-6.20
230	330	34.60	0.00	0.00	-6.32
231	231	36.00	0.00	0.00	-6.40
231	331	36.00	0.00	0.00	-6.49
232	232	37.40	0.00	0.00	-6.36
232	332	37.40	0.00	0.00	-6.46
233	233	38.80	0.00	0.00	-6.08
233	333	38.80	0.00	0.00	-6.20
234	234	40.20	0.00	0.00	-5.55
234	334	40.20	0.00	0.00	-5.73
235	235	41.60	0.00	0.00	-4.78
235	335	41.60	0.00	0.00	-5.08
236	236	43.00	0.00	0.00	-3.74
236	336	43.00	0.00	0.00	-4.19
237	237	44.40	0.00	0.00	-2.53
237	337	44.40	0.00	0.00	-3.11
238	238	45.80	0.00	0.00	-1.23
238	338	45.80	0.00	0.00	-1.91
239	239	47.20	0.00	0.00	-0.04
239	339	47.20	0.00	0.00	-0.77
240	240	48.60	0.00	0.00	0.72
240	340	48.60	0.00	0.00	0.06
241	241	50.00	0.00	0.00	0.91
241	341	50.00	0.00	0.00	0.45
242	242	51.40	0.00	0.00	0.72
242	342	51.40	0.00	0.00	0.06
243	243	52.80	0.00	0.00	-0.04
243	343	52.80	0.00	0.00	-0.77
244	244	54.20	0.00	0.00	-1.23
244	344	54.20	0.00	0.00	-1.91
245	245	55.60	0.00	0.00	-2.53
245	345	55.60	0.00	0.00	-3.11
246	246	57.00	0.00	0.00	-3.75
246	346	57.00	0.00	0.00	-4.19
247	247	58.40	0.00	0.00	-4.78
247	347	58.40	0.00	0.00	-5.08
248	248	59.80	0.00	0.00	-5.55
248	348	59.80	0.00	0.00	-5.73
249	249	61.20	0.00	0.00	-6.08
249	349	61.20	0.00	0.00	-6.20
250	250	62.60	0.00	0.00	-6.36
250	350	62.60	0.00	0.00	-6.46
251	251	64.00	0.00	0.00	-6.40
251	351	64.00	0.00	0.00	-6.49

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ENVOLVENTE TREN A MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN A MZ-
ENVOLVENTE TREN A MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-6.20
252	352	65.40	0.00	0.00	-6.32
253	253	66.80	0.00	0.00	-5.75
253	353	66.80	0.00	0.00	-5.90
254	254	68.20	0.00	0.00	-5.07
254	354	68.20	0.00	0.00	-5.28
255	255	69.60	0.00	0.00	-4.22
255	355	69.60	0.00	0.00	-4.45
256	256	71.00	0.00	0.00	-3.15
256	356	71.00	0.00	0.00	-3.47
257	257	72.40	0.00	0.00	-1.93
257	357	72.40	0.00	0.00	-2.35
258	258	73.80	0.00	0.00	-0.71
258	358	73.80	0.00	0.00	-1.16
259	259	75.20	0.00	0.00	0.28
259	359	75.20	0.00	0.00	-0.11
260	260	76.60	0.00	0.00	0.82
260	360	76.60	0.00	0.00	0.47
261	261	78.00	0.00	0.00	0.88
261	361	78.00	0.00	0.00	0.55
262	262	79.10	0.00	0.00	0.70
262	362	79.10	0.00	0.00	0.30
263	263	80.20	0.00	0.00	0.43
263	363	80.20	0.00	0.00	-0.07
264	264	81.30	0.00	0.00	-0.11
264	364	81.30	0.00	0.00	-0.62
265	265	82.40	0.00	0.00	-0.76
265	365	82.40	0.00	0.00	-1.22
266	266	83.50	0.00	0.00	-1.42
266	366	83.50	0.00	0.00	-1.81
267	267	84.60	0.00	0.00	-1.98
267	367	84.60	0.00	0.00	-2.31
268	268	85.70	0.00	0.00	-2.42
268	368	85.70	0.00	0.00	-2.68
269	269	86.80	0.00	0.00	-2.72
269	369	86.80	0.00	0.00	-2.91
270	270	87.90	0.00	0.00	-2.88
270	370	87.90	0.00	0.00	-3.02
271	271	89.00	0.00	0.00	-2.90
271	371	89.00	0.00	0.00	-2.99
272	272	90.10	0.00	0.00	-2.77
272	372	90.10	0.00	0.00	-2.82
273	273	91.20	0.00	0.00	-2.51
273	373	91.20	0.00	0.00	-2.53
274	274	92.30	0.00	0.00	-2.14
274	374	92.30	0.00	0.00	-2.14
275	275	93.40	0.00	0.00	-1.68
275	375	93.40	0.00	0.00	-1.65
276	276	94.50	0.00	0.00	-1.09
276	376	94.50	0.00	0.00	-1.12
277	277	95.60	0.00	0.00	-0.39

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN A MZ-

ENVOLVENTE TREN A MZ-

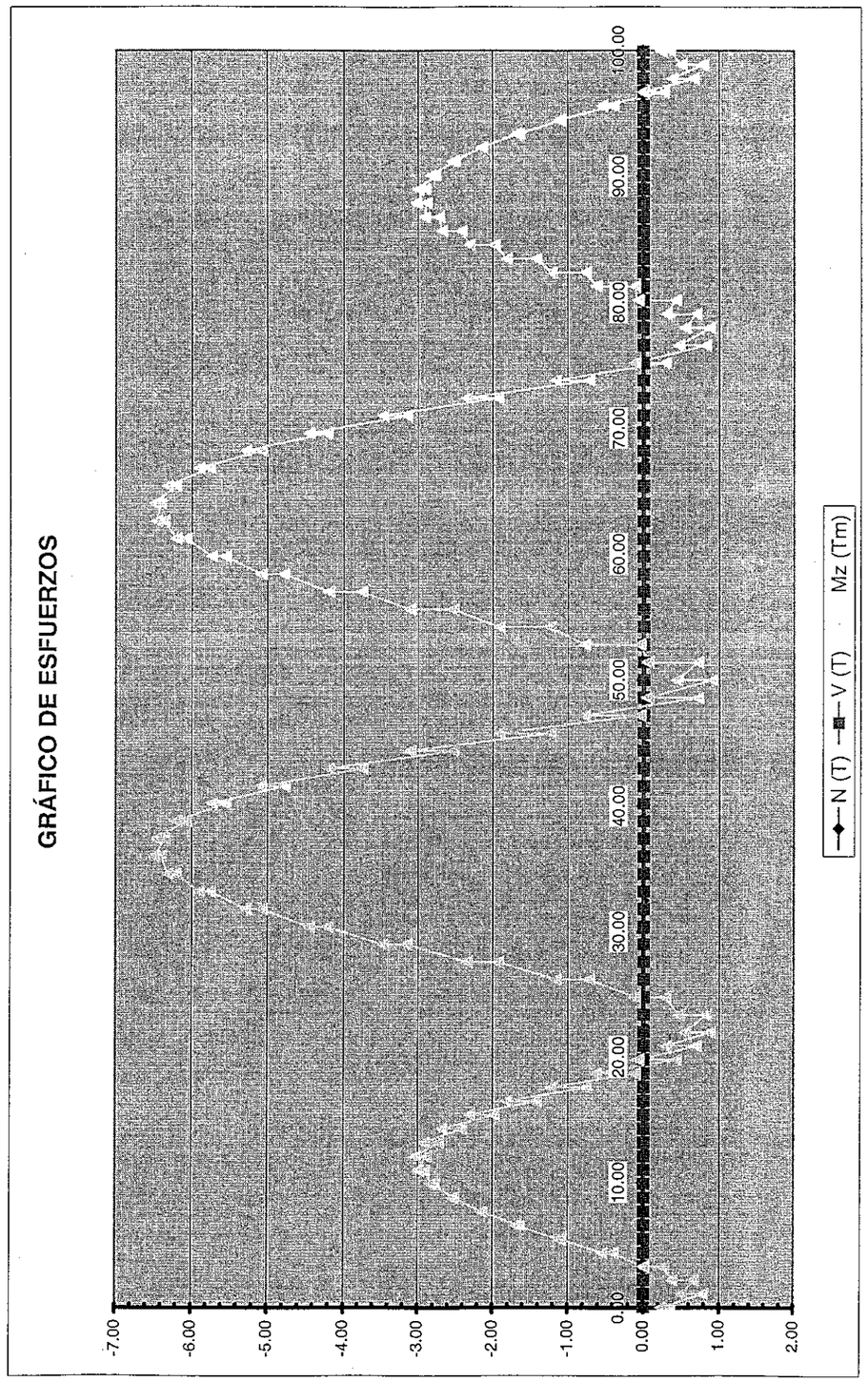
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-0.54
278	278	96.70	0.00	0.00	0.26
278	378	96.70	0.00	0.00	0.00
279	279	97.80	0.00	0.00	0.66
279	379	97.80	0.00	0.00	0.38
280	280	98.90	0.00	0.00	0.78
280	380	98.90	0.00	0.00	0.50
281	281	100.00	0.00	0.00	0.35
281	381	100.00	0.00	0.00	0.23

15/09/03

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN A MZ-

F4.esflosa.xls



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ+
ENVOLVENTE TREN E MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	5.30
201	301	0.00	0.00	0.00	5.94
202	202	1.10	0.00	0.00	10.62
202	302	1.10	0.00	0.00	11.74
203	203	2.20	0.00	0.00	10.83
203	303	2.20	0.00	0.00	11.84
204	204	3.30	0.00	0.00	11.25
204	304	3.30	0.00	0.00	12.17
205	205	4.40	0.00	0.00	11.89
205	305	4.40	0.00	0.00	12.77
206	206	5.50	0.00	0.00	12.55
206	306	5.50	0.00	0.00	13.42
207	207	6.60	0.00	0.00	13.13
207	307	6.60	0.00	0.00	13.97
208	208	7.70	0.00	0.00	13.65
208	308	7.70	0.00	0.00	14.43
209	209	8.80	0.00	0.00	14.08
209	309	8.80	0.00	0.00	14.82
210	210	9.90	0.00	0.00	14.36
210	310	9.90	0.00	0.00	15.07
211	211	11.00	0.00	0.00	14.50
211	311	11.00	0.00	0.00	15.21
212	212	12.10	0.00	0.00	14.51
212	312	12.10	0.00	0.00	15.23
213	213	13.20	0.00	0.00	14.37
213	313	13.20	0.00	0.00	15.11
214	214	14.30	0.00	0.00	14.06
214	314	14.30	0.00	0.00	14.82
215	215	15.40	0.00	0.00	13.62
215	315	15.40	0.00	0.00	14.41
216	216	16.50	0.00	0.00	13.05
216	316	16.50	0.00	0.00	13.89
217	217	17.60	0.00	0.00	12.39
217	317	17.60	0.00	0.00	13.27
218	218	18.70	0.00	0.00	11.69
218	318	18.70	0.00	0.00	12.63
219	219	19.80	0.00	0.00	11.06
219	319	19.80	0.00	0.00	12.06
220	220	20.90	0.00	0.00	10.56
220	320	20.90	0.00	0.00	11.65
221	221	22.00	0.00	0.00	11.69
221	321	22.00	0.00	0.00	13.01
222	222	23.40	0.00	0.00	13.20
222	322	23.40	0.00	0.00	14.63
223	223	24.80	0.00	0.00	13.94
223	323	24.80	0.00	0.00	15.30
224	224	26.20	0.00	0.00	15.12
224	324	26.20	0.00	0.00	16.30
225	225	27.60	0.00	0.00	16.42
225	325	27.60	0.00	0.00	17.51
226	226	29.00	0.00	0.00	17.66

F5.esflosa.xls Programa DINTEL PACADAR S.A. 15/09/03
ENVOLVENTE TREN E MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ+
ENVOLVENTE TREN E MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	18.68
227	227	30.40	0.00	0.00	18.71
227	327	30.40	0.00	0.00	19.66
228	228	31.80	0.00	0.00	19.60
228	328	31.80	0.00	0.00	20.46
229	229	33.20	0.00	0.00	20.28
229	329	33.20	0.00	0.00	21.09
230	230	34.60	0.00	0.00	20.71
230	330	34.60	0.00	0.00	21.49
231	231	36.00	0.00	0.00	20.91
231	331	36.00	0.00	0.00	21.67
232	232	37.40	0.00	0.00	20.90
232	332	37.40	0.00	0.00	21.66
233	233	38.80	0.00	0.00	20.62
233	333	38.80	0.00	0.00	21.43
234	234	40.20	0.00	0.00	20.10
234	334	40.20	0.00	0.00	20.97
235	235	41.60	0.00	0.00	19.38
235	335	41.60	0.00	0.00	20.28
236	236	43.00	0.00	0.00	18.38
236	336	43.00	0.00	0.00	19.33
237	237	44.40	0.00	0.00	17.16
237	337	44.40	0.00	0.00	18.16
238	238	45.80	0.00	0.00	15.83
238	338	45.80	0.00	0.00	16.89
239	239	47.20	0.00	0.00	14.54
239	339	47.20	0.00	0.00	15.69
240	240	48.60	0.00	0.00	13.47
240	340	48.60	0.00	0.00	14.75
241	241	50.00	0.00	0.00	12.86
241	341	50.00	0.00	0.00	14.31
242	242	51.40	0.00	0.00	13.47
242	342	51.40	0.00	0.00	14.76
243	243	52.80	0.00	0.00	14.54
243	343	52.80	0.00	0.00	15.71
244	244	54.20	0.00	0.00	15.83
244	344	54.20	0.00	0.00	16.91
245	245	55.60	0.00	0.00	17.16
245	345	55.60	0.00	0.00	18.18
246	246	57.00	0.00	0.00	18.38
246	346	57.00	0.00	0.00	19.35
247	247	58.40	0.00	0.00	19.37
247	347	58.40	0.00	0.00	20.30
248	248	59.80	0.00	0.00	20.10
248	348	59.80	0.00	0.00	20.98
249	249	61.20	0.00	0.00	20.62
249	349	61.20	0.00	0.00	21.44
250	250	62.60	0.00	0.00	20.90
250	350	62.60	0.00	0.00	21.67
251	251	64.00	0.00	0.00	20.91
251	351	64.00	0.00	0.00	21.67

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ+
ENVOLVENTE TREN E MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	20.71
252	352	65.40	0.00	0.00	21.48
253	253	66.80	0.00	0.00	20.29
253	353	66.80	0.00	0.00	21.08
254	254	68.20	0.00	0.00	19.60
254	354	68.20	0.00	0.00	20.45
255	255	69.60	0.00	0.00	18.72
255	355	69.60	0.00	0.00	19.64
256	256	71.00	0.00	0.00	17.67
256	356	71.00	0.00	0.00	18.66
257	257	72.40	0.00	0.00	16.43
257	357	72.40	0.00	0.00	17.49
258	258	73.80	0.00	0.00	15.12
258	358	73.80	0.00	0.00	16.28
259	259	75.20	0.00	0.00	13.95
259	359	75.20	0.00	0.00	15.28
260	260	76.60	0.00	0.00	13.21
260	360	76.60	0.00	0.00	14.65
261	261	78.00	0.00	0.00	11.68
261	361	78.00	0.00	0.00	13.02
262	262	79.10	0.00	0.00	10.56
262	362	79.10	0.00	0.00	11.67
263	263	80.20	0.00	0.00	11.05
263	363	80.20	0.00	0.00	12.08
264	264	81.30	0.00	0.00	11.69
264	364	81.30	0.00	0.00	12.64
265	265	82.40	0.00	0.00	12.38
265	365	82.40	0.00	0.00	13.28
266	266	83.50	0.00	0.00	13.05
266	366	83.50	0.00	0.00	13.90
267	267	84.60	0.00	0.00	13.62
267	367	84.60	0.00	0.00	14.43
268	268	85.70	0.00	0.00	14.06
268	368	85.70	0.00	0.00	14.83
269	269	86.80	0.00	0.00	14.37
269	369	86.80	0.00	0.00	15.12
270	270	87.90	0.00	0.00	14.51
270	370	87.90	0.00	0.00	15.23
271	271	89.00	0.00	0.00	14.50
271	371	89.00	0.00	0.00	15.21
272	272	90.10	0.00	0.00	14.36
272	372	90.10	0.00	0.00	15.06
273	273	91.20	0.00	0.00	14.08
273	373	91.20	0.00	0.00	14.81
274	274	92.30	0.00	0.00	13.65
274	374	92.30	0.00	0.00	14.42
275	275	93.40	0.00	0.00	13.13
275	375	93.40	0.00	0.00	13.96
276	276	94.50	0.00	0.00	12.55
276	376	94.50	0.00	0.00	13.41
277	277	95.60	0.00	0.00	11.89

CÁLCULO TENSIONAL

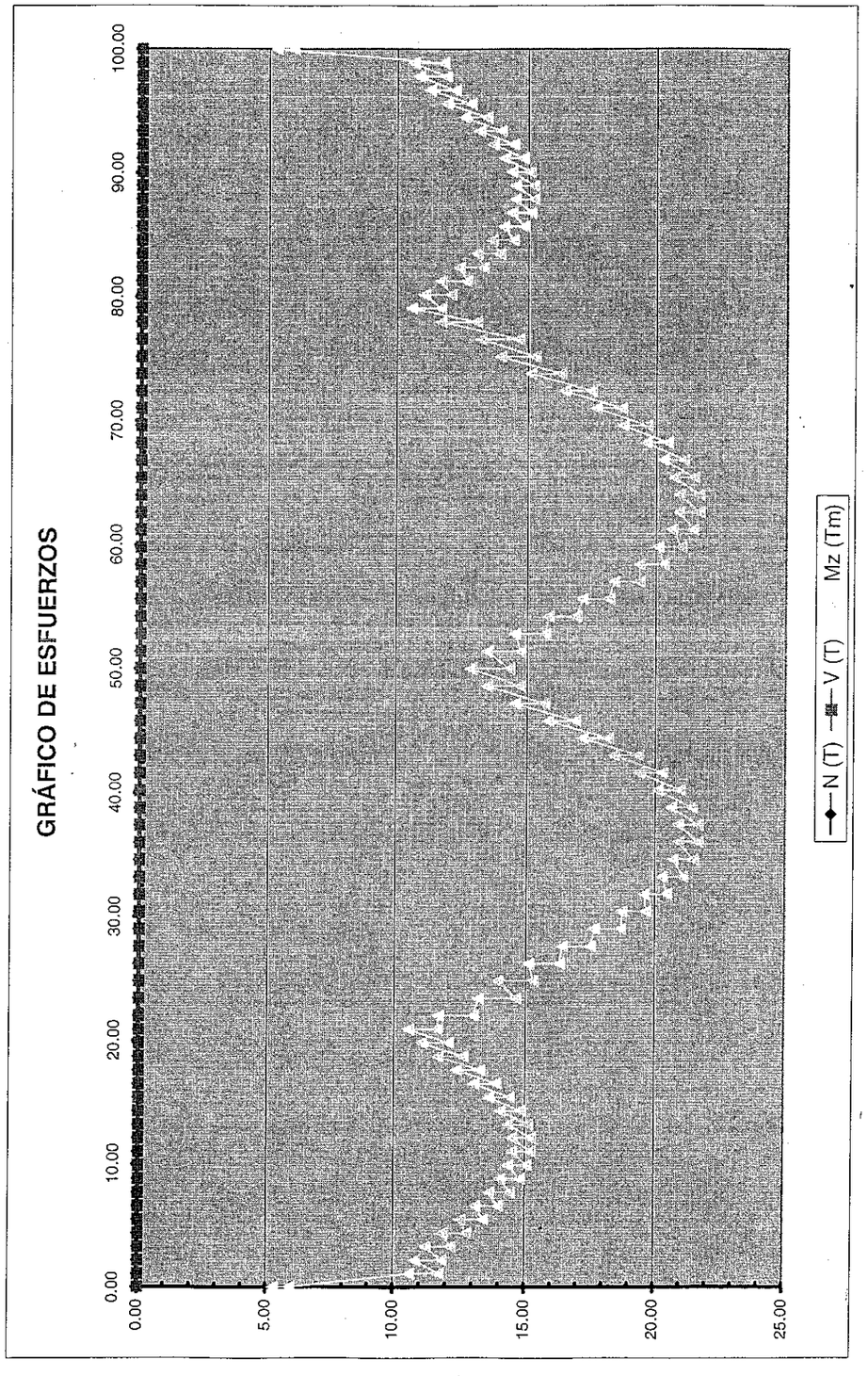
Hipótesis de cálculo:
ENVOLVENTE TREN E MZ+
ENVOLVENTE TREN E MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	12.78
278	278	96.70	0.00	0.00	11.25
278	378	96.70	0.00	0.00	12.19
279	279	97.80	0.00	0.00	10.83
279	379	97.80	0.00	0.00	11.86
280	280	98.90	0.00	0.00	10.62
280	380	98.90	0.00	0.00	11.76
281	281	100.00	0.00	0.00	5.30
281	381	100.00	0.00	0.00	5.95

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN E MZ+

GRÁFICO DE ESFUERZOS



Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN E MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ-
ENVOLVENTE TREN E MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	0.28
201	301	0.00	0.00	0.00	0.33
202	202	1.10	0.00	0.00	0.59
202	302	1.10	0.00	0.00	0.72
203	203	2.20	0.00	0.00	0.46
203	303	2.20	0.00	0.00	0.59
204	204	3.30	0.00	0.00	0.06
204	304	3.30	0.00	0.00	0.19
205	205	4.40	0.00	0.00	-0.54
205	305	4.40	0.00	0.00	-0.44
206	206	5.50	0.00	0.00	-1.15
206	306	5.50	0.00	0.00	-1.11
207	207	6.60	0.00	0.00	-1.69
207	307	6.60	0.00	0.00	-1.68
208	208	7.70	0.00	0.00	-2.19
208	308	7.70	0.00	0.00	-2.14
209	209	8.80	0.00	0.00	-2.59
209	309	8.80	0.00	0.00	-2.52
210	210	9.90	0.00	0.00	-2.87
210	310	9.90	0.00	0.00	-2.78
211	211	11.00	0.00	0.00	-3.03
211	311	11.00	0.00	0.00	-2.92
212	212	12.10	0.00	0.00	-3.03
212	312	12.10	0.00	0.00	-2.91
213	213	13.20	0.00	0.00	-2.90
213	313	13.20	0.00	0.00	-2.76
214	214	14.30	0.00	0.00	-2.64
214	314	14.30	0.00	0.00	-2.47
215	215	15.40	0.00	0.00	-2.24
215	315	15.40	0.00	0.00	-2.05
216	216	16.50	0.00	0.00	-1.72
216	316	16.50	0.00	0.00	-1.50
217	217	17.60	0.00	0.00	-1.11
217	317	17.60	0.00	0.00	-0.86
218	218	18.70	0.00	0.00	-0.48
218	318	18.70	0.00	0.00	-0.23
219	219	19.80	0.00	0.00	0.09
219	319	19.80	0.00	0.00	0.32
220	220	20.90	0.00	0.00	0.45
220	320	20.90	0.00	0.00	0.63
221	221	22.00	0.00	0.00	0.65
221	321	22.00	0.00	0.00	0.80
222	222	23.40	0.00	0.00	0.57
222	322	23.40	0.00	0.00	0.73
223	223	24.80	0.00	0.00	0.03
223	323	24.80	0.00	0.00	0.20
224	224	26.20	0.00	0.00	-1.04
224	324	26.20	0.00	0.00	-0.79
225	225	27.60	0.00	0.00	-2.27
225	325	27.60	0.00	0.00	-2.01
226	226	29.00	0.00	0.00	-3.46

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ-
ENVOLVENTE TREN E MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-3.21
227	227	30.40	0.00	0.00	-4.48
227	327	30.40	0.00	0.00	-4.25
228	228	31.80	0.00	0.00	-5.34
228	328	31.80	0.00	0.00	-5.11
229	229	33.20	0.00	0.00	-5.99
229	329	33.20	0.00	0.00	-5.78
230	230	34.60	0.00	0.00	-6.42
230	330	34.60	0.00	0.00	-6.22
231	231	36.00	0.00	0.00	-6.60
231	331	36.00	0.00	0.00	-6.41
232	232	37.40	0.00	0.00	-6.56
232	332	37.40	0.00	0.00	-6.36
233	233	38.80	0.00	0.00	-6.28
233	333	38.80	0.00	0.00	-6.08
234	234	40.20	0.00	0.00	-5.78
234	334	40.20	0.00	0.00	-5.59
235	235	41.60	0.00	0.00	-5.09
235	335	41.60	0.00	0.00	-4.84
236	236	43.00	0.00	0.00	-4.14
236	336	43.00	0.00	0.00	-3.84
237	237	44.40	0.00	0.00	-2.98
237	337	44.40	0.00	0.00	-2.65
238	238	45.80	0.00	0.00	-1.74
238	338	45.80	0.00	0.00	-1.38
239	239	47.20	0.00	0.00	-0.57
239	339	47.20	0.00	0.00	-0.21
240	240	48.60	0.00	0.00	0.27
240	340	48.60	0.00	0.00	0.58
241	241	50.00	0.00	0.00	0.62
241	341	50.00	0.00	0.00	0.81
242	242	51.40	0.00	0.00	0.27
242	342	51.40	0.00	0.00	0.58
243	243	52.80	0.00	0.00	-0.57
243	343	52.80	0.00	0.00	-0.21
244	244	54.20	0.00	0.00	-1.75
244	344	54.20	0.00	0.00	-1.38
245	245	55.60	0.00	0.00	-2.99
245	345	55.60	0.00	0.00	-2.65
246	246	57.00	0.00	0.00	-4.15
246	346	57.00	0.00	0.00	-3.84
247	247	58.40	0.00	0.00	-5.11
247	347	58.40	0.00	0.00	-4.84
248	248	59.80	0.00	0.00	-5.80
248	348	59.80	0.00	0.00	-5.59
249	249	61.20	0.00	0.00	-6.29
249	349	61.20	0.00	0.00	-6.08
250	250	62.60	0.00	0.00	-6.57
250	350	62.60	0.00	0.00	-6.36
251	251	64.00	0.00	0.00	-6.59
251	351	64.00	0.00	0.00	-6.41

F5.esflosa.xls Programa DINTEL PACADAR S.A. 15/09/03
ENVOLVENTE TREN E MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ-
ENVOLVENTE TREN E MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-6.42
252	352	65.40	0.00	0.00	-6.22
253	253	66.80	0.00	0.00	-5.98
253	353	66.80	0.00	0.00	-5.78
254	254	68.20	0.00	0.00	-5.32
254	354	68.20	0.00	0.00	-5.11
255	255	69.60	0.00	0.00	-4.46
255	355	69.60	0.00	0.00	-4.25
256	256	71.00	0.00	0.00	-3.44
256	356	71.00	0.00	0.00	-3.21
257	257	72.40	0.00	0.00	-2.25
257	357	72.40	0.00	0.00	-2.01
258	258	73.80	0.00	0.00	-1.04
258	358	73.80	0.00	0.00	-0.79
259	259	75.20	0.00	0.00	0.04
259	359	75.20	0.00	0.00	0.20
260	260	76.60	0.00	0.00	0.57
260	360	76.60	0.00	0.00	0.73
261	261	78.00	0.00	0.00	0.65
261	361	78.00	0.00	0.00	0.80
262	262	79.10	0.00	0.00	0.45
262	362	79.10	0.00	0.00	0.63
263	263	80.20	0.00	0.00	0.09
263	363	80.20	0.00	0.00	0.32
264	264	81.30	0.00	0.00	-0.48
264	364	81.30	0.00	0.00	-0.23
265	265	82.40	0.00	0.00	-1.10
265	365	82.40	0.00	0.00	-0.86
266	266	83.50	0.00	0.00	-1.72
266	366	83.50	0.00	0.00	-1.50
267	267	84.60	0.00	0.00	-2.25
267	367	84.60	0.00	0.00	-2.05
268	268	85.70	0.00	0.00	-2.65
268	368	85.70	0.00	0.00	-2.47
269	269	86.80	0.00	0.00	-2.91
269	369	86.80	0.00	0.00	-2.76
270	270	87.90	0.00	0.00	-3.05
270	370	87.90	0.00	0.00	-2.91
271	271	89.00	0.00	0.00	-3.04
271	371	89.00	0.00	0.00	-2.92
272	272	90.10	0.00	0.00	-2.89
272	372	90.10	0.00	0.00	-2.78
273	273	91.20	0.00	0.00	-2.60
273	373	91.20	0.00	0.00	-2.52
274	274	92.30	0.00	0.00	-2.20
274	374	92.30	0.00	0.00	-2.14
275	275	93.40	0.00	0.00	-1.70
275	375	93.40	0.00	0.00	-1.68
276	276	94.50	0.00	0.00	-1.16
276	376	94.50	0.00	0.00	-1.11
277	277	95.60	0.00	0.00	-0.54

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN E MZ-
ENVOLVENTE TREN E MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-0.44
278	278	96.70	0.00	0.00	0.06
278	378	96.70	0.00	0.00	0.19
279	279	97.80	0.00	0.00	0.46
279	379	97.80	0.00	0.00	0.59
280	280	98.90	0.00	0.00	0.59
280	380	98.90	0.00	0.00	0.72
281	281	100.00	0.00	0.00	0.28
281	381	100.00	0.00	0.00	0.33

15/09/03

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN E MZ-

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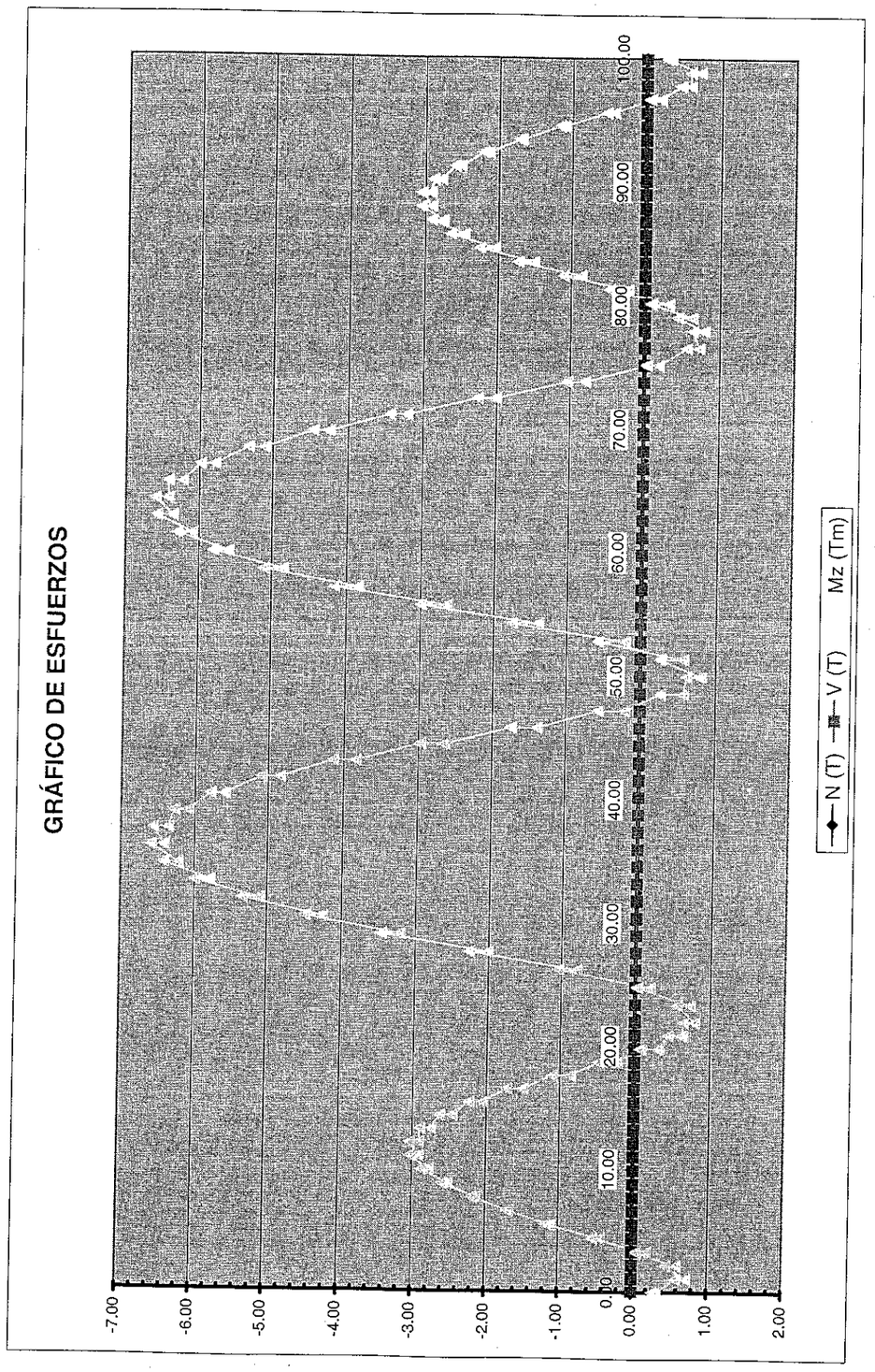

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ+
ENVOLVENTE TREN M MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	6.87
201	301	0.00	0.00	0.00	3.96
202	202	1.10	0.00	0.00	13.18
202	302	1.10	0.00	0.00	7.90
203	203	2.20	0.00	0.00	12.93
203	303	2.20	0.00	0.00	8.40
204	204	3.30	0.00	0.00	13.01
204	304	3.30	0.00	0.00	9.03
205	205	4.40	0.00	0.00	13.48
205	305	4.40	0.00	0.00	9.78
206	206	5.50	0.00	0.00	14.05
206	306	5.50	0.00	0.00	10.56
207	207	6.60	0.00	0.00	14.55
207	307	6.60	0.00	0.00	11.31
208	208	7.70	0.00	0.00	14.98
208	308	7.70	0.00	0.00	11.95
209	209	8.80	0.00	0.00	15.31
209	309	8.80	0.00	0.00	12.44
210	210	9.90	0.00	0.00	15.54
210	310	9.90	0.00	0.00	12.76
211	211	11.00	0.00	0.00	15.70
211	311	11.00	0.00	0.00	12.90
212	212	12.10	0.00	0.00	15.76
212	312	12.10	0.00	0.00	12.87
213	213	13.20	0.00	0.00	15.71
213	313	13.20	0.00	0.00	12.67
214	214	14.30	0.00	0.00	15.53
214	314	14.30	0.00	0.00	12.29
215	215	15.40	0.00	0.00	15.23
215	315	15.40	0.00	0.00	11.76
216	216	16.50	0.00	0.00	14.84
216	316	16.50	0.00	0.00	11.09
217	217	17.60	0.00	0.00	14.35
217	317	17.60	0.00	0.00	10.32
218	218	18.70	0.00	0.00	13.85
218	318	18.70	0.00	0.00	9.52
219	219	19.80	0.00	0.00	13.48
219	319	19.80	0.00	0.00	8.75
220	220	20.90	0.00	0.00	13.23
220	320	20.90	0.00	0.00	8.10
221	221	22.00	0.00	0.00	14.86
221	321	22.00	0.00	0.00	8.70
222	222	23.40	0.00	0.00	16.58
222	322	23.40	0.00	0.00	9.84
223	223	24.80	0.00	0.00	17.01
223	323	24.80	0.00	0.00	11.04
224	224	26.20	0.00	0.00	17.78
224	324	26.20	0.00	0.00	12.49
225	225	27.60	0.00	0.00	18.71
225	325	27.60	0.00	0.00	13.99
226	226	29.00	0.00	0.00	19.61

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ENVOLVENTE TREN M MZ+

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ+
ENVOLVENTE TREN M MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	15.44
227	227	30.40	0.00	0.00	20.38
227	327	30.40	0.00	0.00	16.76
228	228	31.80	0.00	0.00	20.99
228	328	31.80	0.00	0.00	17.83
229	229	33.20	0.00	0.00	21.43
229	329	33.20	0.00	0.00	18.64
230	230	34.60	0.00	0.00	21.73
230	330	34.60	0.00	0.00	19.15
231	231	36.00	0.00	0.00	21.92
231	331	36.00	0.00	0.00	19.37
232	232	37.40	0.00	0.00	22.00
232	332	37.40	0.00	0.00	19.32
233	233	38.80	0.00	0.00	21.87
233	333	38.80	0.00	0.00	18.94
234	234	40.20	0.00	0.00	21.52
234	334	40.20	0.00	0.00	18.26
235	235	41.60	0.00	0.00	20.97
235	335	41.60	0.00	0.00	17.31
236	236	43.00	0.00	0.00	20.21
236	336	43.00	0.00	0.00	16.13
237	237	44.40	0.00	0.00	19.25
237	337	44.40	0.00	0.00	14.76
238	238	45.80	0.00	0.00	18.21
238	338	45.80	0.00	0.00	13.27
239	239	47.20	0.00	0.00	17.29
239	339	47.20	0.00	0.00	11.77
240	240	48.60	0.00	0.00	16.70
240	340	48.60	0.00	0.00	10.47
241	241	50.00	0.00	0.00	16.43
241	341	50.00	0.00	0.00	9.84
242	242	51.40	0.00	0.00	16.70
242	342	51.40	0.00	0.00	10.47
243	243	52.80	0.00	0.00	17.29
243	343	52.80	0.00	0.00	11.78
244	244	54.20	0.00	0.00	18.20
244	344	54.20	0.00	0.00	13.27
245	245	55.60	0.00	0.00	19.25
245	345	55.60	0.00	0.00	14.76
246	246	57.00	0.00	0.00	20.21
246	346	57.00	0.00	0.00	16.13
247	247	58.40	0.00	0.00	20.97
247	347	58.40	0.00	0.00	17.31
248	248	59.80	0.00	0.00	21.52
248	348	59.80	0.00	0.00	18.26
249	249	61.20	0.00	0.00	21.87
249	349	61.20	0.00	0.00	18.94
250	250	62.60	0.00	0.00	22.00
250	350	62.60	0.00	0.00	19.32
251	251	64.00	0.00	0.00	21.92
251	351	64.00	0.00	0.00	19.37

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ+
ENVOLVENTE TREN M MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	21.73
252	352	65.40	0.00	0.00	19.15
253	253	66.80	0.00	0.00	21.44
253	353	66.80	0.00	0.00	18.64
254	254	68.20	0.00	0.00	21.00
254	354	68.20	0.00	0.00	17.83
255	255	69.60	0.00	0.00	20.38
255	355	69.60	0.00	0.00	16.76
256	256	71.00	0.00	0.00	19.61
256	356	71.00	0.00	0.00	15.44
257	257	72.40	0.00	0.00	18.71
257	357	72.40	0.00	0.00	13.99
258	258	73.80	0.00	0.00	17.78
258	358	73.80	0.00	0.00	12.49
259	259	75.20	0.00	0.00	17.01
259	359	75.20	0.00	0.00	11.04
260	260	76.60	0.00	0.00	16.58
260	360	76.60	0.00	0.00	9.84
261	261	78.00	0.00	0.00	14.86
261	361	78.00	0.00	0.00	8.70
262	262	79.10	0.00	0.00	13.23
262	362	79.10	0.00	0.00	8.10
263	263	80.20	0.00	0.00	13.48
263	363	80.20	0.00	0.00	8.75
264	264	81.30	0.00	0.00	13.85
264	364	81.30	0.00	0.00	9.52
265	265	82.40	0.00	0.00	14.35
265	365	82.40	0.00	0.00	10.32
266	266	83.50	0.00	0.00	14.84
266	366	83.50	0.00	0.00	11.09
267	267	84.60	0.00	0.00	15.23
267	367	84.60	0.00	0.00	11.76
268	268	85.70	0.00	0.00	15.53
268	368	85.70	0.00	0.00	12.29
269	269	86.80	0.00	0.00	15.71
269	369	86.80	0.00	0.00	12.67
270	270	87.90	0.00	0.00	15.76
270	370	87.90	0.00	0.00	12.87
271	271	89.00	0.00	0.00	15.70
271	371	89.00	0.00	0.00	12.90
272	272	90.10	0.00	0.00	15.54
272	372	90.10	0.00	0.00	12.76
273	273	91.20	0.00	0.00	15.31
273	373	91.20	0.00	0.00	12.44
274	274	92.30	0.00	0.00	14.98
274	374	92.30	0.00	0.00	11.95
275	275	93.40	0.00	0.00	14.55
275	375	93.40	0.00	0.00	11.31
276	276	94.50	0.00	0.00	14.05
276	376	94.50	0.00	0.00	10.56
277	277	95.60	0.00	0.00	13.48

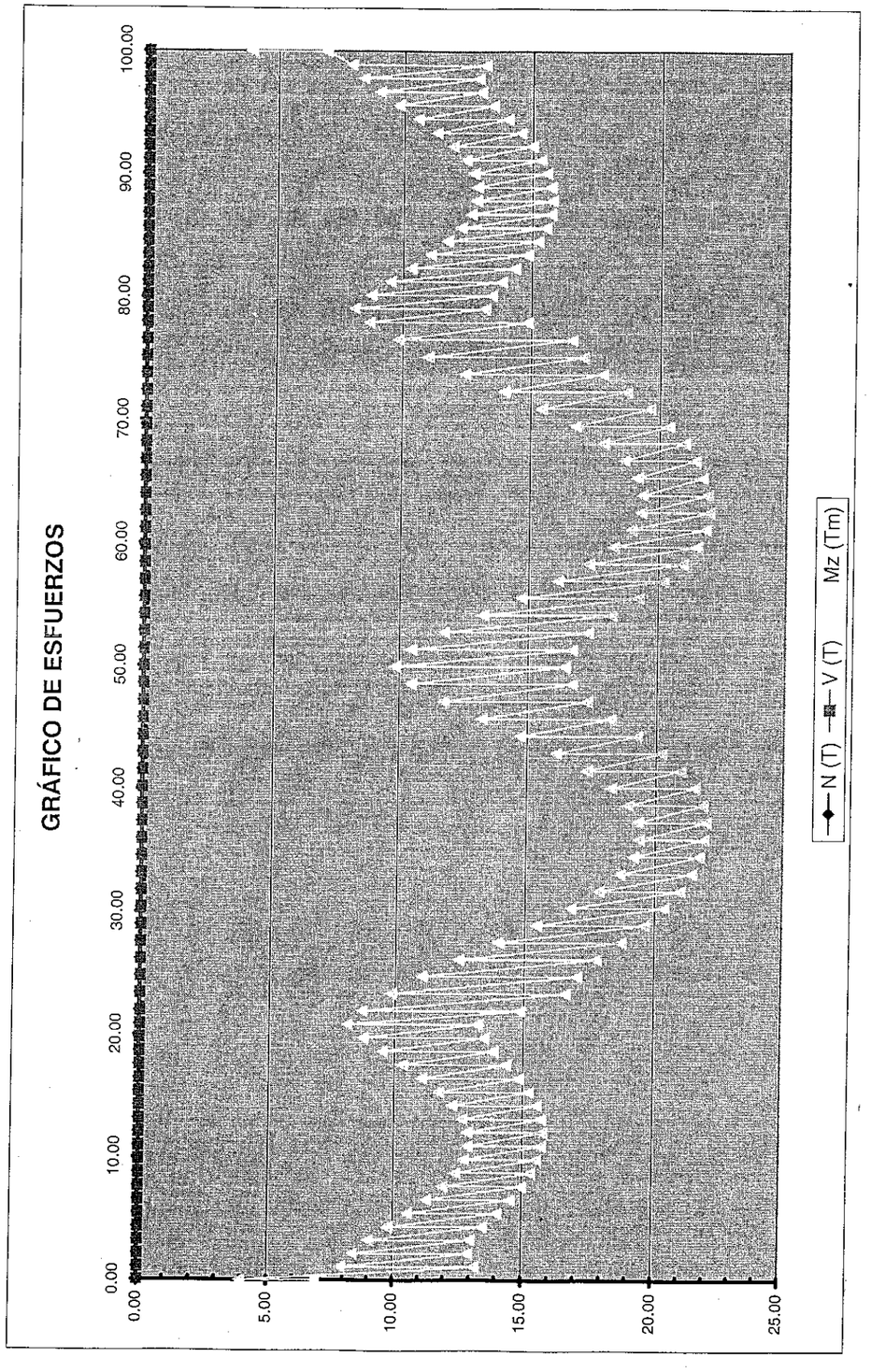
CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ+
ENVOLVENTE TREN M MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	9.78
278	278	96.70	0.00	0.00	13.01
278	378	96.70	0.00	0.00	9.03
279	279	97.80	0.00	0.00	12.93
279	379	97.80	0.00	0.00	8.40
280	280	98.90	0.00	0.00	13.18
280	380	98.90	0.00	0.00	7.90
281	281	100.00	0.00	0.00	6.87
281	381	100.00	0.00	0.00	3.96

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN M MZ+



Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN M MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ-
ENVOLVENTE TREN M MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	0.40
201	301	0.00	0.00	0.00	-0.07
202	202	1.10	0.00	0.00	0.92
202	302	1.10	0.00	0.00	0.27
203	203	2.20	0.00	0.00	0.83
203	303	2.20	0.00	0.00	0.15
204	204	3.30	0.00	0.00	0.43
204	304	3.30	0.00	0.00	-0.19
205	205	4.40	0.00	0.00	-0.31
205	305	4.40	0.00	0.00	-0.66
206	206	5.50	0.00	0.00	-1.12
206	306	5.50	0.00	0.00	-1.21
207	207	6.60	0.00	0.00	-1.79
207	307	6.60	0.00	0.00	-1.78
208	208	7.70	0.00	0.00	-2.32
208	308	7.70	0.00	0.00	-2.29
209	209	8.80	0.00	0.00	-2.70
209	309	8.80	0.00	0.00	-2.72
210	210	9.90	0.00	0.00	-2.93
210	310	9.90	0.00	0.00	-3.06
211	211	11.00	0.00	0.00	-3.04
211	311	11.00	0.00	0.00	-3.28
212	212	12.10	0.00	0.00	-2.99
212	312	12.10	0.00	0.00	-3.36
213	213	13.20	0.00	0.00	-2.79
213	313	13.20	0.00	0.00	-3.30
214	214	14.30	0.00	0.00	-2.43
214	314	14.30	0.00	0.00	-3.12
215	215	15.40	0.00	0.00	-1.94
215	315	15.40	0.00	0.00	-2.82
216	216	16.50	0.00	0.00	-1.32
216	316	16.50	0.00	0.00	-2.38
217	217	17.60	0.00	0.00	-0.61
217	317	17.60	0.00	0.00	-1.83
218	218	18.70	0.00	0.00	0.07
218	318	18.70	0.00	0.00	-1.25
219	219	19.80	0.00	0.00	0.59
219	319	19.80	0.00	0.00	-0.66
220	220	20.90	0.00	0.00	0.84
220	320	20.90	0.00	0.00	-0.22
221	221	22.00	0.00	0.00	1.05
221	321	22.00	0.00	0.00	0.08
222	222	23.40	0.00	0.00	1.05
222	322	23.40	0.00	0.00	0.03
223	223	24.80	0.00	0.00	0.48
223	323	24.80	0.00	0.00	-0.78
224	224	26.20	0.00	0.00	-0.62
224	324	26.20	0.00	0.00	-1.86
225	225	27.60	0.00	0.00	-1.93
225	325	27.60	0.00	0.00	-2.96
226	226	29.00	0.00	0.00	-3.22

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ-
ENVOLVENTE TREN M MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-3.98
227	227	30.40	0.00	0.00	-4.37
227	327	30.40	0.00	0.00	-4.94
228	228	31.80	0.00	0.00	-5.30
228	328	31.80	0.00	0.00	-5.70
229	229	33.20	0.00	0.00	-5.99
229	329	33.20	0.00	0.00	-6.27
230	230	34.60	0.00	0.00	-6.48
230	330	34.60	0.00	0.00	-6.65
231	231	36.00	0.00	0.00	-6.70
231	331	36.00	0.00	0.00	-6.82
232	232	37.40	0.00	0.00	-6.67
232	332	37.40	0.00	0.00	-6.82
233	233	38.80	0.00	0.00	-6.35
233	333	38.80	0.00	0.00	-6.60
234	234	40.20	0.00	0.00	-5.74
234	334	40.20	0.00	0.00	-6.17
235	235	41.60	0.00	0.00	-4.85
235	335	41.60	0.00	0.00	-5.55
236	236	43.00	0.00	0.00	-3.70
236	336	43.00	0.00	0.00	-4.76
237	237	44.40	0.00	0.00	-2.36
237	337	44.40	0.00	0.00	-3.82
238	238	45.80	0.00	0.00	-0.94
238	338	45.80	0.00	0.00	-2.74
239	239	47.20	0.00	0.00	0.29
239	339	47.20	0.00	0.00	-1.63
240	240	48.60	0.00	0.00	0.95
240	340	48.60	0.00	0.00	-0.65
241	241	50.00	0.00	0.00	1.13
241	341	50.00	0.00	0.00	-0.37
242	242	51.40	0.00	0.00	0.95
242	342	51.40	0.00	0.00	-0.65
243	243	52.80	0.00	0.00	0.29
243	343	52.80	0.00	0.00	-1.63
244	244	54.20	0.00	0.00	-0.94
244	344	54.20	0.00	0.00	-2.74
245	245	55.60	0.00	0.00	-2.36
245	345	55.60	0.00	0.00	-3.82
246	246	57.00	0.00	0.00	-3.70
246	346	57.00	0.00	0.00	-4.76
247	247	58.40	0.00	0.00	-4.85
247	347	58.40	0.00	0.00	-5.55
248	248	59.80	0.00	0.00	-5.74
248	348	59.80	0.00	0.00	-6.17
249	249	61.20	0.00	0.00	-6.35
249	349	61.20	0.00	0.00	-6.60
250	250	62.60	0.00	0.00	-6.67
250	350	62.60	0.00	0.00	-6.82
251	251	64.00	0.00	0.00	-6.70
251	351	64.00	0.00	0.00	-6.82

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Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN M MZ-
15/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ-
ENVOLVENTE TREN M MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	-6.48
252	352	65.40	0.00	0.00	-6.65
253	253	66.80	0.00	0.00	-5.99
253	353	66.80	0.00	0.00	-6.27
254	254	68.20	0.00	0.00	-5.30
254	354	68.20	0.00	0.00	-5.70
255	255	69.60	0.00	0.00	-4.37
255	355	69.60	0.00	0.00	-4.94
256	256	71.00	0.00	0.00	-3.22
256	356	71.00	0.00	0.00	-3.98
257	257	72.40	0.00	0.00	-1.93
257	357	72.40	0.00	0.00	-2.96
258	258	73.80	0.00	0.00	-0.62
258	358	73.80	0.00	0.00	-1.86
259	259	75.20	0.00	0.00	0.48
259	359	75.20	0.00	0.00	-0.78
260	260	76.60	0.00	0.00	1.05
260	360	76.60	0.00	0.00	0.03
261	261	78.00	0.00	0.00	1.05
261	361	78.00	0.00	0.00	0.08
262	262	79.10	0.00	0.00	0.84
262	362	79.10	0.00	0.00	-0.22
263	263	80.20	0.00	0.00	0.59
263	363	80.20	0.00	0.00	-0.66
264	264	81.30	0.00	0.00	0.07
264	364	81.30	0.00	0.00	-1.25
265	265	82.40	0.00	0.00	-0.61
265	365	82.40	0.00	0.00	-1.83
266	266	83.50	0.00	0.00	-1.32
266	366	83.50	0.00	0.00	-2.38
267	267	84.60	0.00	0.00	-1.94
267	367	84.60	0.00	0.00	-2.82
268	268	85.70	0.00	0.00	-2.43
268	368	85.70	0.00	0.00	-3.12
269	269	86.80	0.00	0.00	-2.79
269	369	86.80	0.00	0.00	-3.30
270	270	87.90	0.00	0.00	-2.99
270	370	87.90	0.00	0.00	-3.36
271	271	89.00	0.00	0.00	-3.04
271	371	89.00	0.00	0.00	-3.28
272	272	90.10	0.00	0.00	-2.93
272	372	90.10	0.00	0.00	-3.06
273	273	91.20	0.00	0.00	-2.70
273	373	91.20	0.00	0.00	-2.72
274	274	92.30	0.00	0.00	-2.32
274	374	92.30	0.00	0.00	-2.29
275	275	93.40	0.00	0.00	-1.79
275	375	93.40	0.00	0.00	-1.78
276	276	94.50	0.00	0.00	-1.12
276	376	94.50	0.00	0.00	-1.21
277	277	95.60	0.00	0.00	-0.31

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN M MZ-
ENVOLVENTE TREN M MZ-

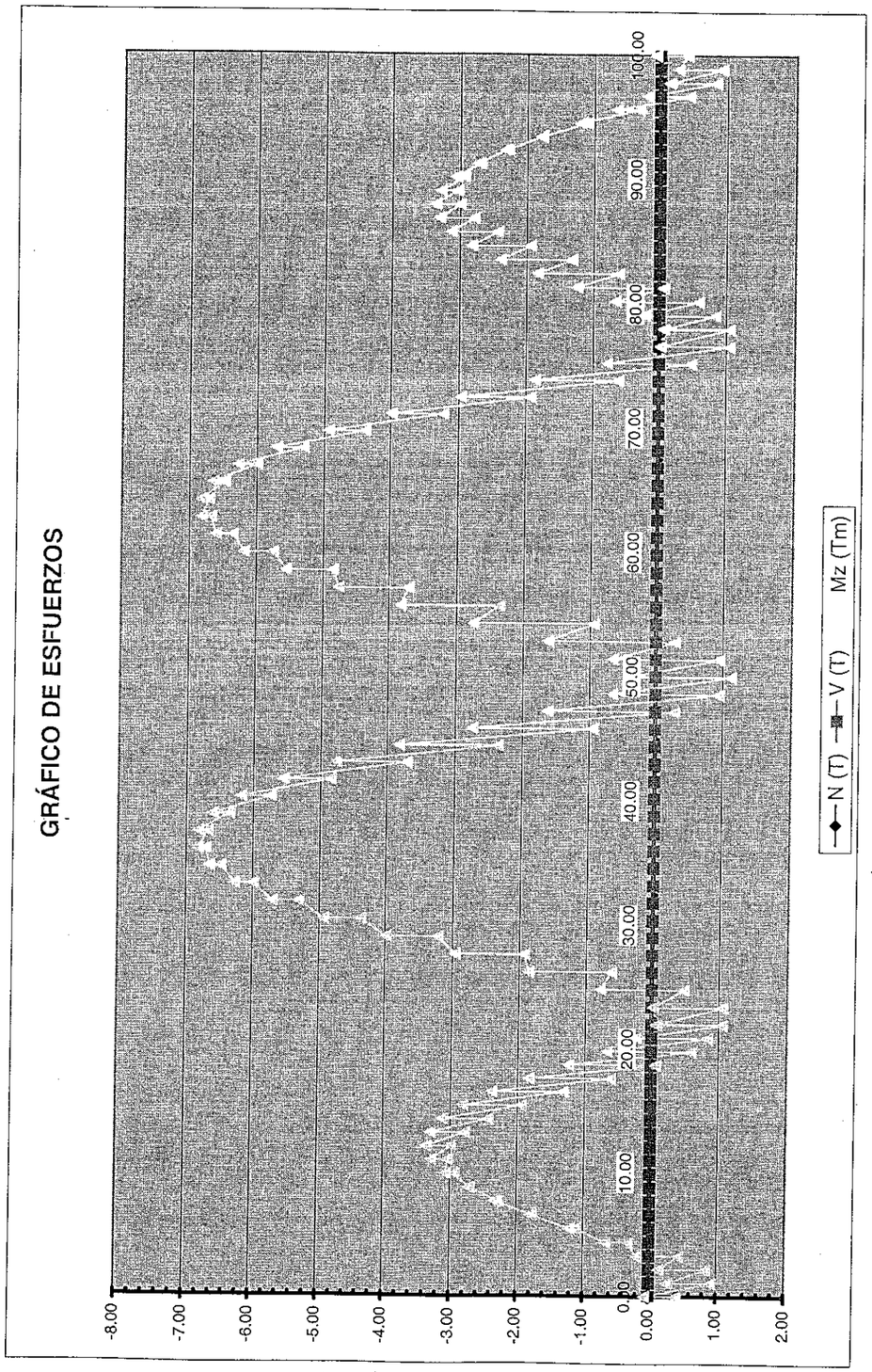
Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-0.66
278	278	96.70	0.00	0.00	0.43
278	378	96.70	0.00	0.00	-0.19
279	279	97.80	0.00	0.00	0.83
279	379	97.80	0.00	0.00	0.15
280	280	98.90	0.00	0.00	0.92
280	380	98.90	0.00	0.00	0.27
281	281	100.00	0.00	0.00	0.40
281	381	100.00	0.00	0.00	-0.07

15/09/03

Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN M MZ-

GRÁFICO DE ESFUERZOS



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CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ+
ENVOLVENTE TREN H MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	5.43
201	301	0.00	0.00	0.00	2.50
202	202	1.10	0.00	0.00	11.49
202	302	1.10	0.00	0.00	4.34
203	203	2.20	0.00	0.00	12.10
203	303	2.20	0.00	0.00	3.85
204	204	3.30	0.00	0.00	12.66
204	304	3.30	0.00	0.00	3.58
205	205	4.40	0.00	0.00	13.15
205	305	4.40	0.00	0.00	3.58
206	206	5.50	0.00	0.00	13.54
206	306	5.50	0.00	0.00	3.71
207	207	6.60	0.00	0.00	13.83
207	307	6.60	0.00	0.00	3.89
208	208	7.70	0.00	0.00	14.03
208	308	7.70	0.00	0.00	4.08
209	209	8.80	0.00	0.00	14.14
209	309	8.80	0.00	0.00	4.26
210	210	9.90	0.00	0.00	14.12
210	310	9.90	0.00	0.00	4.42
211	211	11.00	0.00	0.00	14.03
211	311	11.00	0.00	0.00	4.58
212	212	12.10	0.00	0.00	13.88
212	312	12.10	0.00	0.00	4.70
213	213	13.20	0.00	0.00	13.63
213	313	13.20	0.00	0.00	4.79
214	214	14.30	0.00	0.00	13.28
214	314	14.30	0.00	0.00	4.86
215	215	15.40	0.00	0.00	12.87
215	315	15.40	0.00	0.00	4.88
216	216	16.50	0.00	0.00	12.41
216	316	16.50	0.00	0.00	4.86
217	217	17.60	0.00	0.00	11.93
217	317	17.60	0.00	0.00	4.81
218	218	18.70	0.00	0.00	11.47
218	318	18.70	0.00	0.00	4.75
219	219	19.80	0.00	0.00	11.10
219	319	19.80	0.00	0.00	4.72
220	220	20.90	0.00	0.00	10.83
220	320	20.90	0.00	0.00	4.70
221	221	22.00	0.00	0.00	12.15
221	321	22.00	0.00	0.00	5.31
222	222	23.40	0.00	0.00	13.70
222	322	23.40	0.00	0.00	5.91
223	223	24.80	0.00	0.00	14.19
223	323	24.80	0.00	0.00	5.96
224	224	26.20	0.00	0.00	14.93
224	324	26.20	0.00	0.00	6.12
225	225	27.60	0.00	0.00	15.74
225	325	27.60	0.00	0.00	6.32
226	226	29.00	0.00	0.00	16.54

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Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN H MZ+

15/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ+
ENVOLVENTE TREN H MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	6.53
227	227	30.40	0.00	0.00	17.25
227	327	30.40	0.00	0.00	6.69
228	228	31.80	0.00	0.00	17.86
228	328	31.80	0.00	0.00	6.80
229	229	33.20	0.00	0.00	18.31
229	329	33.20	0.00	0.00	6.87
230	230	34.60	0.00	0.00	18.62
230	330	34.60	0.00	0.00	6.92
231	231	36.00	0.00	0.00	18.77
231	331	36.00	0.00	0.00	6.96
232	232	37.40	0.00	0.00	18.74
232	332	37.40	0.00	0.00	7.01
233	233	38.80	0.00	0.00	18.50
233	333	38.80	0.00	0.00	7.03
234	234	40.20	0.00	0.00	18.06
234	334	40.20	0.00	0.00	7.02
235	235	41.60	0.00	0.00	17.44
235	335	41.60	0.00	0.00	6.96
236	236	43.00	0.00	0.00	16.66
236	336	43.00	0.00	0.00	6.85
237	237	44.40	0.00	0.00	15.76
237	337	44.40	0.00	0.00	6.68
238	238	45.80	0.00	0.00	14.82
238	338	45.80	0.00	0.00	6.51
239	239	47.20	0.00	0.00	13.97
239	339	47.20	0.00	0.00	6.37
240	240	48.60	0.00	0.00	13.38
240	340	48.60	0.00	0.00	6.31
241	241	50.00	0.00	0.00	13.13
241	341	50.00	0.00	0.00	6.26
242	242	51.40	0.00	0.00	13.39
242	342	51.40	0.00	0.00	6.31
243	243	52.80	0.00	0.00	13.97
243	343	52.80	0.00	0.00	6.37
244	244	54.20	0.00	0.00	14.82
244	344	54.20	0.00	0.00	6.51
245	245	55.60	0.00	0.00	15.76
245	345	55.60	0.00	0.00	6.68
246	246	57.00	0.00	0.00	16.66
246	346	57.00	0.00	0.00	6.85
247	247	58.40	0.00	0.00	17.44
247	347	58.40	0.00	0.00	6.96
248	248	59.80	0.00	0.00	18.06
248	348	59.80	0.00	0.00	7.02
249	249	61.20	0.00	0.00	18.50
249	349	61.20	0.00	0.00	7.03
250	250	62.60	0.00	0.00	18.74
250	350	62.60	0.00	0.00	7.01
251	251	64.00	0.00	0.00	18.77
251	351	64.00	0.00	0.00	6.96

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ+
ENVOLVENTE TREN H MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	18.62
252	352	65.40	0.00	0.00	6.92
253	253	66.80	0.00	0.00	18.31
253	353	66.80	0.00	0.00	6.87
254	254	68.20	0.00	0.00	17.86
254	354	68.20	0.00	0.00	6.80
255	255	69.60	0.00	0.00	17.25
255	355	69.60	0.00	0.00	6.69
256	256	71.00	0.00	0.00	16.54
256	356	71.00	0.00	0.00	6.53
257	257	72.40	0.00	0.00	15.74
257	357	72.40	0.00	0.00	6.32
258	258	73.80	0.00	0.00	14.93
258	358	73.80	0.00	0.00	6.12
259	259	75.20	0.00	0.00	14.19
259	359	75.20	0.00	0.00	5.96
260	260	76.60	0.00	0.00	13.70
260	360	76.60	0.00	0.00	5.91
261	261	78.00	0.00	0.00	12.15
261	361	78.00	0.00	0.00	5.31
262	262	79.10	0.00	0.00	10.83
262	362	79.10	0.00	0.00	4.70
263	263	80.20	0.00	0.00	11.10
263	363	80.20	0.00	0.00	4.72
264	264	81.30	0.00	0.00	11.47
264	364	81.30	0.00	0.00	4.75
265	265	82.40	0.00	0.00	11.93
265	365	82.40	0.00	0.00	4.81
266	266	83.50	0.00	0.00	12.41
266	366	83.50	0.00	0.00	4.86
267	267	84.60	0.00	0.00	12.87
267	367	84.60	0.00	0.00	4.88
268	268	85.70	0.00	0.00	13.28
268	368	85.70	0.00	0.00	4.86
269	269	86.80	0.00	0.00	13.63
269	369	86.80	0.00	0.00	4.79
270	270	87.90	0.00	0.00	13.88
270	370	87.90	0.00	0.00	4.70
271	271	89.00	0.00	0.00	14.03
271	371	89.00	0.00	0.00	4.58
272	272	90.10	0.00	0.00	14.12
272	372	90.10	0.00	0.00	4.42
273	273	91.20	0.00	0.00	14.14
273	373	91.20	0.00	0.00	4.26
274	274	92.30	0.00	0.00	14.03
274	374	92.30	0.00	0.00	4.08
275	275	93.40	0.00	0.00	13.83
275	375	93.40	0.00	0.00	3.89
276	276	94.50	0.00	0.00	13.53
276	376	94.50	0.00	0.00	3.71
277	277	95.60	0.00	0.00	13.15

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Programa DINTEL PACADAR S.A.
ENVOLVENTE TREN H MZ+

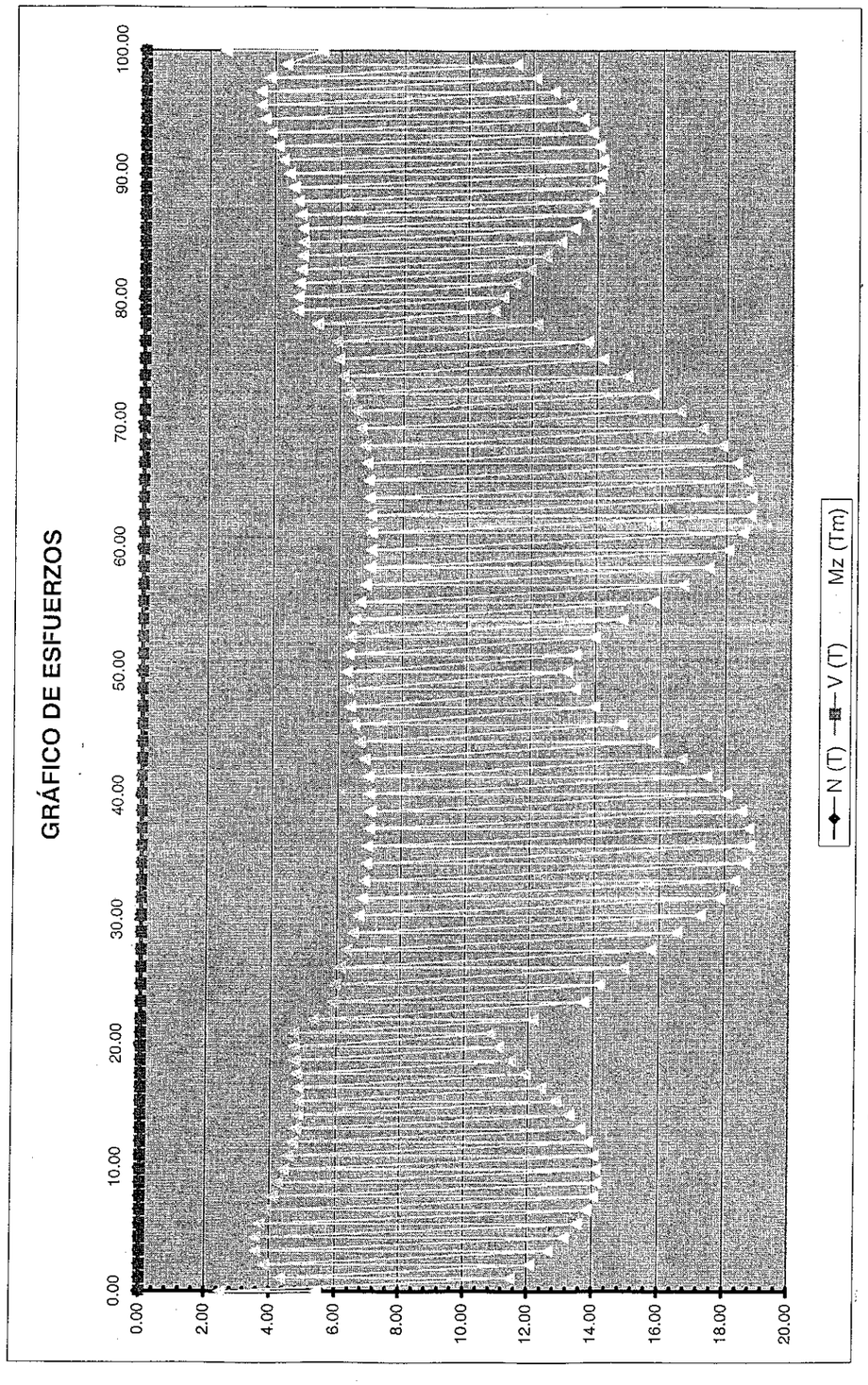
15/09/03

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ+
ENVOLVENTE TREN H MZ+

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	3.58
278	278	96.70	0.00	0.00	12.66
278	378	96.70	0.00	0.00	3.58
279	279	97.80	0.00	0.00	12.10
279	379	97.80	0.00	0.00	3.85
280	280	98.90	0.00	0.00	11.49
280	380	98.90	0.00	0.00	4.34
281	281	100.00	0.00	0.00	5.43
281	381	100.00	0.00	0.00	2.50



CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ-
ENVOLVENTE TREN H MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
201	201	0.00	0.00	0.00	-0.06
201	301	0.00	0.00	0.00	-0.07
202	202	1.10	0.00	0.00	-0.01
202	302	1.10	0.00	0.00	-0.23
203	203	2.20	0.00	0.00	0.10
203	303	2.20	0.00	0.00	-0.45
204	204	3.30	0.00	0.00	0.18
204	304	3.30	0.00	0.00	-0.87
205	205	4.40	0.00	0.00	0.25
205	305	4.40	0.00	0.00	-1.43
206	206	5.50	0.00	0.00	0.31
206	306	5.50	0.00	0.00	-2.01
207	207	6.60	0.00	0.00	0.34
207	307	6.60	0.00	0.00	-2.53
208	208	7.70	0.00	0.00	0.37
208	308	7.70	0.00	0.00	-2.93
209	209	8.80	0.00	0.00	0.37
209	309	8.80	0.00	0.00	-3.21
210	210	9.90	0.00	0.00	0.37
210	310	9.90	0.00	0.00	-3.37
211	211	11.00	0.00	0.00	0.33
211	311	11.00	0.00	0.00	-3.41
212	212	12.10	0.00	0.00	0.26
212	312	12.10	0.00	0.00	-3.31
213	213	13.20	0.00	0.00	0.20
213	313	13.20	0.00	0.00	-3.09
214	214	14.30	0.00	0.00	0.14
214	314	14.30	0.00	0.00	-2.77
215	215	15.40	0.00	0.00	0.09
215	315	15.40	0.00	0.00	-2.36
216	216	16.50	0.00	0.00	0.06
216	316	16.50	0.00	0.00	-1.87
217	217	17.60	0.00	0.00	0.04
217	317	17.60	0.00	0.00	-1.33
218	218	18.70	0.00	0.00	0.01
218	318	18.70	0.00	0.00	-0.82
219	219	19.80	0.00	0.00	-0.04
219	319	19.80	0.00	0.00	-0.41
220	220	20.90	0.00	0.00	-0.07
220	320	20.90	0.00	0.00	-0.18
221	221	22.00	0.00	0.00	-0.10
221	321	22.00	0.00	0.00	-0.15
222	222	23.40	0.00	0.00	-0.08
222	322	23.40	0.00	0.00	-0.34
223	223	24.80	0.00	0.00	-0.02
223	323	24.80	0.00	0.00	-0.89
224	224	26.20	0.00	0.00	0.06
224	324	26.20	0.00	0.00	-1.83
225	225	27.60	0.00	0.00	0.16
225	325	27.60	0.00	0.00	-2.89
226	226	29.00	0.00	0.00	0.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ-
ENVOLVENTE TREN H MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
226	326	29.00	0.00	0.00	-3.96
227	227	30.40	0.00	0.00	0.33
227	327	30.40	0.00	0.00	-4.92
228	228	31.80	0.00	0.00	0.40
228	328	31.80	0.00	0.00	-5.70
229	229	33.20	0.00	0.00	0.45
229	329	33.20	0.00	0.00	-6.28
230	230	34.60	0.00	0.00	0.43
230	330	34.60	0.00	0.00	-6.65
231	231	36.00	0.00	0.00	0.37
231	331	36.00	0.00	0.00	-6.78
232	232	37.40	0.00	0.00	0.28
232	332	37.40	0.00	0.00	-6.67
233	233	38.80	0.00	0.00	0.18
233	333	38.80	0.00	0.00	-6.33
234	234	40.20	0.00	0.00	0.08
234	334	40.20	0.00	0.00	-5.78
235	235	41.60	0.00	0.00	0.00
235	335	41.60	0.00	0.00	-5.03
236	236	43.00	0.00	0.00	-0.06
236	336	43.00	0.00	0.00	-4.09
237	237	44.40	0.00	0.00	-0.08
237	337	44.40	0.00	0.00	-3.04
238	238	45.80	0.00	0.00	-0.07
238	338	45.80	0.00	0.00	-2.00
239	239	47.20	0.00	0.00	-0.07
239	339	47.20	0.00	0.00	-1.08
240	240	48.60	0.00	0.00	-0.13
240	340	48.60	0.00	0.00	-0.49
241	241	50.00	0.00	0.00	-0.15
241	341	50.00	0.00	0.00	-0.34
242	242	51.40	0.00	0.00	-0.13
242	342	51.40	0.00	0.00	-0.49
243	243	52.80	0.00	0.00	-0.07
243	343	52.80	0.00	0.00	-1.08
244	244	54.20	0.00	0.00	-0.07
244	344	54.20	0.00	0.00	-2.00
245	245	55.60	0.00	0.00	-0.08
245	345	55.60	0.00	0.00	-3.04
246	246	57.00	0.00	0.00	-0.06
246	346	57.00	0.00	0.00	-4.09
247	247	58.40	0.00	0.00	0.00
247	347	58.40	0.00	0.00	-5.03
248	248	59.80	0.00	0.00	0.08
248	348	59.80	0.00	0.00	-5.78
249	249	61.20	0.00	0.00	0.18
249	349	61.20	0.00	0.00	-6.33
250	250	62.60	0.00	0.00	0.28
250	350	62.60	0.00	0.00	-6.67
251	251	64.00	0.00	0.00	0.37
251	351	64.00	0.00	0.00	-6.78

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ENVOLVENTE TREN H MZ-

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ-
ENVOLVENTE TREN H MZ-

Coef. exc:

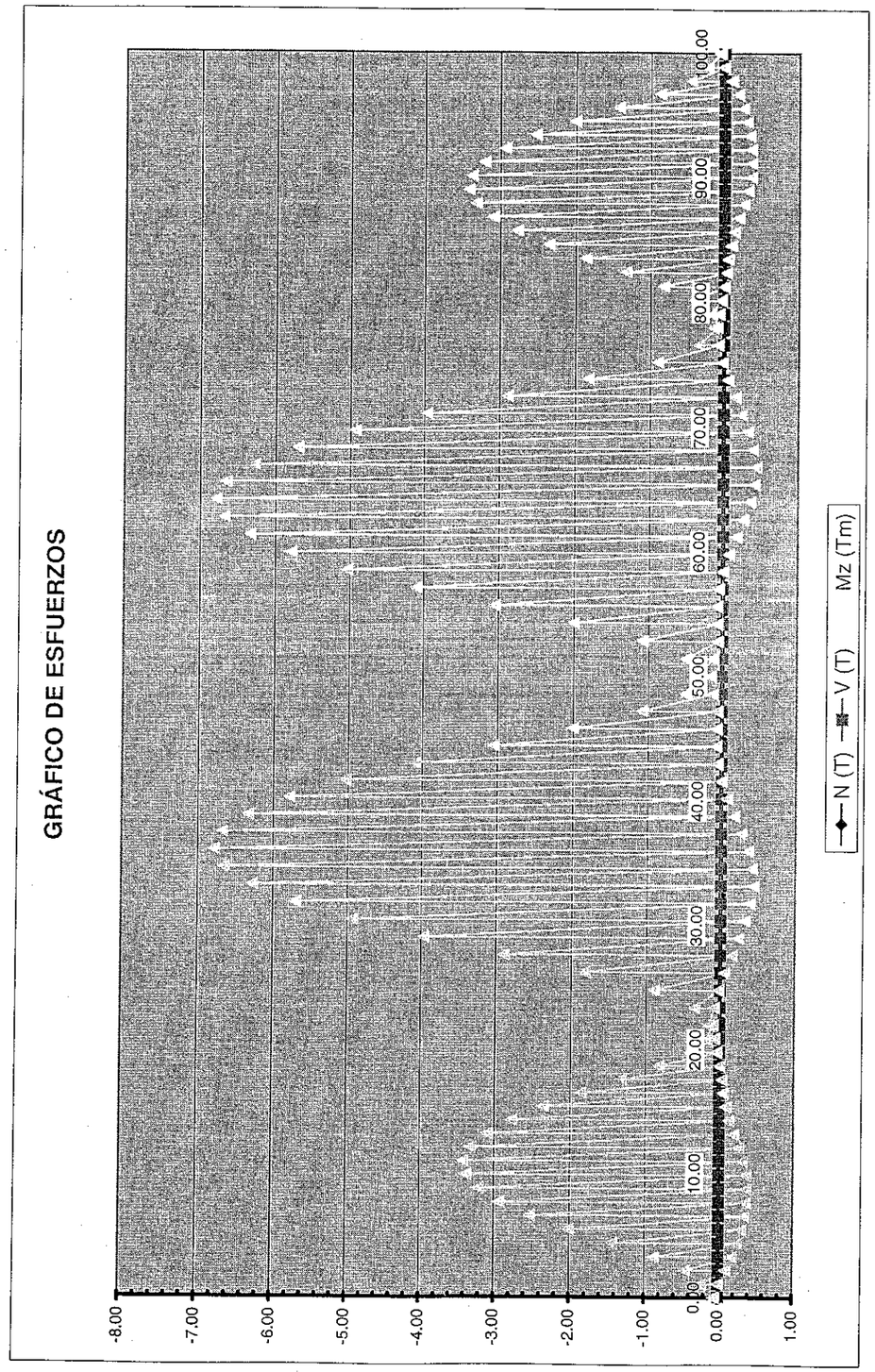
Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
252	252	65.40	0.00	0.00	0.43
252	352	65.40	0.00	0.00	-6.65
253	253	66.80	0.00	0.00	0.45
253	353	66.80	0.00	0.00	-6.28
254	254	68.20	0.00	0.00	0.40
254	354	68.20	0.00	0.00	-5.70
255	255	69.60	0.00	0.00	0.33
255	355	69.60	0.00	0.00	-4.92
256	256	71.00	0.00	0.00	0.25
256	356	71.00	0.00	0.00	-3.96
257	257	72.40	0.00	0.00	0.16
257	357	72.40	0.00	0.00	-2.89
258	258	73.80	0.00	0.00	0.06
258	358	73.80	0.00	0.00	-1.83
259	259	75.20	0.00	0.00	-0.02
259	359	75.20	0.00	0.00	-0.89
260	260	76.60	0.00	0.00	-0.08
260	360	76.60	0.00	0.00	-0.34
261	261	78.00	0.00	0.00	-0.10
261	361	78.00	0.00	0.00	-0.15
262	262	79.10	0.00	0.00	-0.07
262	362	79.10	0.00	0.00	-0.18
263	263	80.20	0.00	0.00	-0.04
263	363	80.20	0.00	0.00	-0.41
264	264	81.30	0.00	0.00	0.01
264	364	81.30	0.00	0.00	-0.82
265	265	82.40	0.00	0.00	0.04
265	365	82.40	0.00	0.00	-1.33
266	266	83.50	0.00	0.00	0.06
266	366	83.50	0.00	0.00	-1.87
267	267	84.60	0.00	0.00	0.09
267	367	84.60	0.00	0.00	-2.36
268	268	85.70	0.00	0.00	0.14
268	368	85.70	0.00	0.00	-2.77
269	269	86.80	0.00	0.00	0.20
269	369	86.80	0.00	0.00	-3.09
270	270	87.90	0.00	0.00	0.26
270	370	87.90	0.00	0.00	-3.31
271	271	89.00	0.00	0.00	0.33
271	371	89.00	0.00	0.00	-3.41
272	272	90.10	0.00	0.00	0.37
272	372	90.10	0.00	0.00	-3.37
273	273	91.20	0.00	0.00	0.37
273	373	91.20	0.00	0.00	-3.21
274	274	92.30	0.00	0.00	0.37
274	374	92.30	0.00	0.00	-2.93
275	275	93.40	0.00	0.00	0.34
275	375	93.40	0.00	0.00	-2.53
276	276	94.50	0.00	0.00	0.31
276	376	94.50	0.00	0.00	-2.01
277	277	95.60	0.00	0.00	0.25

CÁLCULO TENSIONAL

Hipótesis de cálculo:
ENVOLVENTE TREN H MZ-
ENVOLVENTE TREN H MZ-

Coef. exc:

Barra	Nudo	X	N (T)	Vy (T)	Mz (Tm)
277	377	95.60	0.00	0.00	-1.43
278	278	96.70	0.00	0.00	0.18
278	378	96.70	0.00	0.00	-0.87
279	279	97.80	0.00	0.00	0.10
279	379	97.80	0.00	0.00	-0.45
280	280	98.90	0.00	0.00	-0.01
280	380	98.90	0.00	0.00	-0.23
281	281	100.00	0.00	0.00	-0.06
281	381	100.00	0.00	0.00	-0.07



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PROYECTO VIADUCTO TORRENTE DEL BÓ

FECHA

HOJA N.º

APARATOJ DE APOYO

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 1

APARATOS DE APOYO

REACCIONES TRANSMITIDAS POR EL TABLERO

ELEMENTO	APOYO	PESO PROPIO	CARGA PERMANENTE	SOBRECARGA MAX.	SOBRECARGA MIN.	ΔT
ESTRIBOS	1	128,-	86,-	145,-	-26,-	13,-
	2	128,-	86,-	145,-	-26,-	13,-
PILAS	1-3	285,-	212,-	409,-	-38,-	-16,-
	2	293,-	217,-	426,-	-44,-	6,-

REACCIONES MAXIMAS Y MINIMAS

ESTRIBOS $\begin{cases} R_{max} = 128 + 86 + 145 + 13 = 372,- \text{ t} \\ R_{mi} = 128 + 86 - 26 = 188,- \text{ t} \end{cases}$

PILAS 1-3 $\begin{cases} R_{max} = 285 + 212 + 409 = 906,- \text{ t} \\ R_{mi} = 285 + 212 - 38 - 16 = 443,- \text{ t} \end{cases}$

PILA-2 $\begin{cases} R_{max} = 293 + 217 + 426 + 6 = 942,- \text{ t} \\ R_{mi} = 293 + 217 - 44 = 466,- \text{ t} \end{cases}$

Se disponen los siguientes apoyos:

ESTRIBOS: POT de 400,- t (libres)

PILAS: POT de 1000,- t (unidireccionales)

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PROYECTO .....

FECHA .....

HOJA N.º 2

FUERZAS HORIZONTALES

FRENADO Y ARRANQUE

$Q_{LK} = \alpha \cdot 20\,(KN/m) \times L(m) \leq \alpha \cdot 6000\,(KN)$

$Q'_{LK} = \alpha \cdot 33\,(KN/m) \times L'(m) \leq \alpha \cdot 1000\,(KN)$

$L = 22.50 + 28.00 + 28.00 + 22.50 = 101.-\,m < 300.-\,m.$

$L' = 30.-\,m. \qquad \alpha = 1.21$

$Q_{LK} = 1.21 \times 20 \times 101.- = 2444.-\,KN = 249.-\,t < 7260\,KN$

$Q'_{LK} = 1.21 \times 33 \times 30.- = 1198.-\,KN = 122.-\,t < 1210\,KN$

$F_{LTOTAL} = 249 + 122 = 371.-\,t$ (resistida por entero en el estribo-1)

DEFORMACIONES DIFERIDAS

Los apoyos de neopreno teflón (POT) pueden llegar a transmitir un 5% de la carga vertical debida a peso propio y carga permanente:

P_1 y P_3 : $F_{LP} = 2 \times 0.05\,(130 + 154.78 + 145.34 + 66.47) = 48.-\,t$

P_2 : $F_{LE} = 2 \times 0.05\,(133 + 159.78 + 149.15 + 68.23) = 50.-\,t$

ESTRIBO-2 : $F_{LE} = 2 \times 0.05\,(65 + 63 + 59. + 27.-) = 21.-\,t$

Estas fuerzas tienen que ser resistidas por el anclaje en el estribo-1

$F_{LE-1} = 2 \times 48 + 50 + 21.- = 167.-\,t$

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PROYECTO .....

FECHA .....

HOJA N.º 3

EFECTO LAZO

$F_T = 10.-\,t$ puntuales, actuando en cualquier punto de la estructura, a la altura superior del carril.

INTERACCION CARRIL-TABLERO

Se supone vía con balasto, con mantenimiento bueno. En este caso, la fuerza de interacción es de 2.- t/m. a todo lo largo del puente.

Por tanto:

$F_{LE-1} = 2.00 \times 101.- = 202.-\,t/VIA \quad (404.-\,t/2\,VIAS)$

que absorbe totalmente el apoyo fijo en el estribo-1.

Ahora bien, el incremento de tensión longitudinal en los carriles no debe sobrepasar el valor 72 MPa = 720 kg/cm² en compresión y 92 MPa = 920 kg/cm² en tracción.

El carril UIC 60 tiene un area de 76.86 cm² por tanto los valores anteriores son una fuerza de 55,36 t en compresión y 70,71 t en tracción por carril.

Como, en nuestro caso, tenemos 4 carriles, la fuerza máxima a todo lo ancho es de 221,36 t. en compresión y 282.84 t en tracción.

No obstante, el tablero siempre tesado a comprimir el carril (retracción fluencia en tablero y dilatación en carriles), por tanto el valor a tomar como fuerza sobre el estribo-1, debido a la interacción carril-tablero

s de 221,3C t

RESUMEN DE ESFUERZOS LONGITUDINALES

. Frenado y arranque	371.- t
. Deformaciones diferidas	167.- t
. Interacción carril-tablero	221.- t
TOTAL	759.- t

FUERZA CENTRIFUGA

$f = 0,5$

$Q_{tk} = \frac{250 \times 69^2}{9,8 \times 3000} \times 0,5 = 20\ kN = 2.- t$

$q_{tk} = \frac{80 \times 69^2}{9,8 \times 3000} \times 0,5 = 6\ kN/m = 0,6\ t/m.$

FUERZA EN ESTRIBO:

$F = 2\left[2 \times 4 + 0,6\left(\frac{22,5}{2} - 6,4\right)\right] = 22.- t$

L CLOTOIDE = 220.- m.

$F_{ESTRIBO} = \frac{22 \times 90}{220} = 9.- t$

FUERZA EN PILAS 1 y 3

$F = 2\left[2 \times 4 + 0,6\left(25,25 - 6,4\right)\right] = 38.- t$

L CLOTOIDE = 220.- m.

$F_{PILAS\ 1\ y\ 3} = \frac{38 \times 62}{220} = 10.- t$

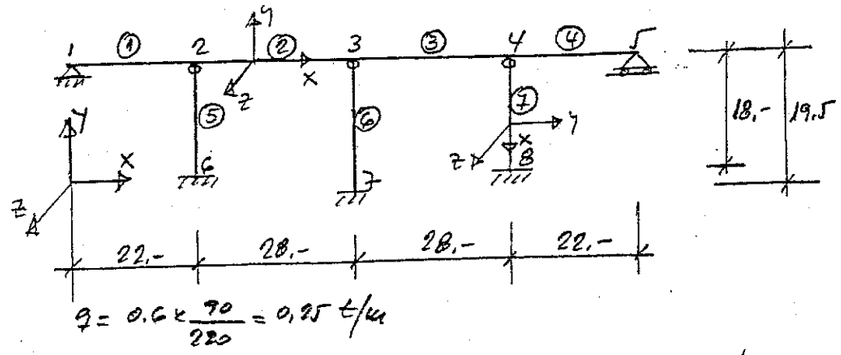
FUERZA EN PILA-2

$F = 2\left[2 \times 4 + 0,6\left(28,00 - 6,4\right)\right] = 42.- t$

$F_{PILA-2} = \frac{42 \times 90}{220} = 17.- t$

Si tenemos en cuenta la flexibilidad del tablero en dirección horizontal, tenemos los siguientes esfuerzos.

Estudiamos el siguiente modelo:



$q = 0,6 \times \frac{90}{220} = 0,25\ t/m$

Del cálculo realizado, que se acompaña al final de este apartado, tenemos los siguientes esfuerzos en estribos y pilas debido a la fuerza centrífuga.

ESTRIBO	$F_{TE} = 2 \times 11 + 6 = 28.- t$
PILAS	$F_{TP} = 2 \times 1 + 6 = 8.- t$

A los resultados del cálculo de ordenador se les ha sumado $p = 2 \times 2 \times 4 \times \frac{90}{220} = 6.- t$

VIENTO

. VELOCIDAD DE REFERENCIA

$V_{ref} = 28.-\ m/s$

. VELOCIDAD DE CALCULO

$V_c = C_t \cdot C_r \times C_z \times C_s \times V_{ref.}$

$C_t = 1.00$

$C_r = 1.04$

$C_z = 0.17 \ln \frac{16}{0.01} = 1.25$

$C_s = \sqrt{\left(1 + \frac{7 \times 0.17}{1.25 \times 1}\right)} = 1.40$

$V_c = 1.00 \times 1.04 \times 1.25 \times 1.40 \times 28.- = 50.-\ m/s$

. EMPUJE DE VIENTO

$F = C_D\ A \left(\frac{1}{2} \rho V_c^2\right)$

$C_D = 2.5 - 0.3 \frac{B}{h}$ $\qquad B = 14.00$

$h_{VACIO} = 1.80 + 0.39 + 0.50 = 2.69 m \rightarrow C_{D\,VACIO} = 0.94 \ \& \ 1.30$

$h_{CARGADO} = 1.80 + 0.39 + 0.50 + 4.00 = 6.69 m \rightarrow C_{D\,CARGADO} = 1.87$

$A_{EXP.\ VACIO} = 1.80 + 0.39 + 2 \times 0.50 + 1.80 \times 0.38 = 3.87\ m^2/m.$

RELACION SOLIDEZ $= 1.00$

ESPACIAMIENTO RELATIVO $= \frac{6.30}{1.80} = 3.5$ $\Big\}\ \eta = 0.38$

$A_{EXP.\ CARGADO} = 1.80 + 0.39 + 0.50 + 1.80 \times 0.38 + 4.00 = 7.37\ m^2/m.$

PRESION BASICA CALCULO TABLERO VACIO $= \frac{1}{2} \rho V_c^2 C_D = 2031.-\ N/m^2$

PRESION BASICA CALCULO TABLERO CARGADO $= 0.5 \frac{1}{2} \rho V_c^2 C_D = 1460.-\ N/m^2$

EMPUJE VIENTO TABLERO VACIO $= 2.031 \times 3.87 = 7.86\ KN/ml.$

EMPUJE VIENTO TABLERO CARGADO $= 1.460 \times 7.37 = 10.76\ KN/ml$

EMPUJE VIENTO SOBRE PILAS $= 1.2 \times 1.7 \left(\frac{1}{2} \rho V_c^2\right) = 3.200.-\ KN/ml$

Por tanto tenemos las siguientes cargas sobre estribos y pilas:

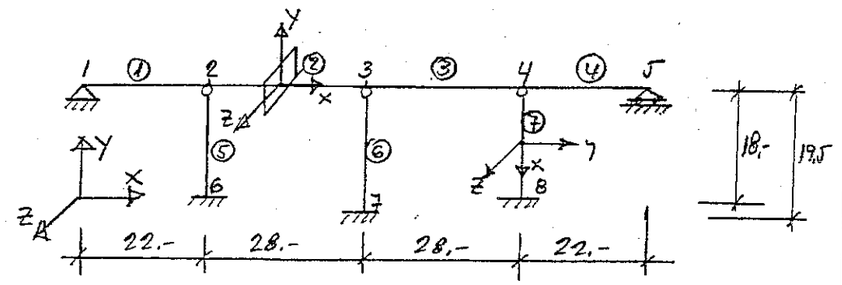
VIA DESCARGADA

- ESTRIBOS: $F_{TE} = 0.786 \times \frac{22.5}{2} = 9.-\ t$
- PILAS 1/3: $F_{TP} = 0.786 \times \frac{28 + 22.50}{2} = 20.-\ t$
- PILAS 2: $F_{TP} = 0.786 \times 28.- = 22.-\ t$

VIA CARGADA

- ESTRIBOS: $F_{TE} = 1.076 \times \frac{22.5}{2} = 12.-\ t$
- PILAS 1/3: $F_{TP} = 1.076 \times \frac{28 + 22.50}{2} = 27.-\ t$
- PILAS 2: $F_{TP} = 1.076 \times 28.- = 30.-\ t$

Si tenemos en cuenta la flexibilidad del tablero en dirección horizontal, tenemos los siguiente esfuerzos:
Estudiamos el siguiente modelo.



① T⌀④ $A_x = 6.928\ m^2$ $I_y = 89.-\ m^4$ $I_z = 3.4529\ m^4$

⑤⑥⑦ $A_x = 4.54\ m^2$ $I_y = 0.82\ m^4$ $I_z = 0.82\ m^4$

Del cálculo realizado, que se acompaña al final de este apartado, tenemos las siguientes cargas en estribos y pilas debido al viento.

VIA DESCARGADA
- ESTRIBO 1: $F_{TE} = 35.-\ t$
- PILAS: $F_{TP} = 3.-\ t$

VIA CARGADA
- ESTRIBO 5: $F_{TE} = 48.-\ t$
- PILAS 1 y 3: $F_{TP} = 4.-\ t$
- PILA 2: $F_{TP} = 5.-\ t$

DESPLAZAMIENTO EN APARATOS DE APOYO

$\Delta T_{max} = K \cdot z^a \cdot h^b \cdot S^c = 36.50\ ^\circ C$

$z = 3$ (zona -3)

$h = 2.05$

$S = 1$

$K = 29.13$ $a = 0.301$ $b = -0.148$ $c = 0$

$\Delta T_{calculo} = \frac{2}{3} \Delta T_{max} = \pm 24\ ^\circ C$

RETRACCION $= -30 \times 10^{-5}$

FLUENCIA $= -1.65 \times 500 \times \frac{1}{3 \times 10^6} = -27 \times 10^{-5}$

TOTAL $\begin{cases} 24 \times 10^{-5} \\ -81 \times 10^{-5} \end{cases}$

MOVIMIENTOS
- E-1: $\delta = 0$
- P-1: $\begin{cases} \delta = 22 \times 24 \times 10^{-5} = 0.0053\ m. \\ \delta = -22 \times 81 \times 10^{-5} = -0.0178\ m. \end{cases}$
- P-2: $\begin{cases} \delta = 50 \times 24 \times 10^{-5} = 0.0120\ m. \\ \delta = -50 \times 81 \times 10^{-5} = -0.0405\ m. \end{cases}$
- P-3: $\begin{cases} \delta = 78 \times 24 \times 10^{-5} = 0.0187\ m. \\ \delta = -78 \times 81 \times 10^{-5} = -0.0632\ m. \end{cases}$
- E-2: $\begin{cases} \delta = 100 \times 24 \times 10^{-5} = 0.0240\ m. \\ \delta = -100 \times 81 \times 10^{-5} = -0.0810\ m. \end{cases}$

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PROYECTO .....

FECHA .....

HOJA N.º 10

APOYOS EN EL PUNTO FIJO

$F_L = 759,- t$

Se disponen 4 apoyos de neopreno zunchado de $300 \times 800 \times 30$ (21)

$\sigma_{max} = \frac{759 \times 10^3}{4 \times 80 \times 30} = 79,- kg/cm^2$

APOYOS EN LOS TOPES TRANSVERSALES DE LOS ESTRIBOS

$F_T = 10 + 28 + 0,6 \times 48 = 67,- t$

$F_T = (10 + 28) \times 0,8 + 48 = 78,- t$

Se disponen unos apoyos de $250 \times 400 \times 30$ (21)

$\sigma_{max} = \frac{78 \times 10^3}{25 \times 40} = 80,- kg/cm^2$

FUERZAS HORIZONTALES EN APOYOS DE LAS PILAS

$F_T = 10 + 17 + 0,6 \times 30,- = 45,- t$

$F_T = (10 + 17) \times 0,8 + 30,- = 50,- t$

Se disponen apoyos POT unidireccionales capaces de transmitir una carga horizontal de 50,- t.


```
 1. STAAD SPACE REPARTO F.CENTRIFUGA
 2. * FICHERO (CENTRI)
 3. UNITS MET MTON
 4. JOINT COORDINATES
 5.    1   0.000  19.500    0.00
 6.    2  22.000  19.500    0.00
 7.    3  50.000  19.500    0.00
 8.    4  78.000  19.500    0.00
 9.    5 100.000  19.500    0.00
10.    6  22.000   1.500    0.00
11.    7  50.000   0.000    0.00
12.    8  78.000   1.500    0.00
13. MEMBER INCIDENCES
14. 1   1  2
15. 2   2  3
16. 3   3  4
17. 4   4  5
18. 5   2  6
19. 6   3  7
20. 7   4  8
21. MEMBER PROPERTIES
22. 1 2 3 4        PRIS AX 6.9280 IX  7.000 IY 89.000 IZ 3.4529
23. 5 6 7          PRIS AX 3.6000 IX  1.600 IY 0.8200 IZ 0.8200
24. CONSTANTS
25. E 3000000.    ALL
26. POISSON 0.15  ALL
27. BETA 0.0  ALL
28. SUPPORTS
29. 1        FIX BUT MY MZ
30. 6 7 8    FIX
31. 5        FIX BUT FX MY MZ
32. MEMBER RELEASES
33. 5 6 7    STA FY MX MY MX
34. LOADING  1 F.CENTRIFUGA
35. MEMBER LOAD
36. 1 2 3 4   UNI GZ -0.25
37. PERFORM ANALYSIS
```

P R O B L E M S T A T I S T I C S

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS = 8/ 7/ 5
ORIGINAL/FINAL BAND-WIDTH = 4/ 3
TOTAL PRIMARY LOAD CASES = 1, TOTAL DEGREES OF FREEDOM = 23
SIZE OF STIFFNESS MATRIX = 276 DOUBLE PREC. WORDS
TOTAL REQUIRED DISK SPACE = 12.02 MEGA-BYTES

++ PROCESSING ELEMENT STIFFNESS MATRIX. 19:49:53
++ PROCESSING GLOBAL STIFFNESS MATRIX. 19:49:53
++ PROCESSING TRIANGULAR FACTORIZATION. 19:49:53
++ CALCULATING JOINT DISPLACEMENTS. 19:49:53
++ CALCULATING MEMBER FORCES. 19:49:53

38. PRINT SUPPORT REAC

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = SPACE

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
1	1	0.00	0.00	11.12	0.00	0.00	0.00
6	1	0.00	0.00	0.86	15.46	0.00	0.00
7	1	0.00	0.00	1.05	20.47	0.00	0.00
8	1	0.00	0.00	0.86	15.46	0.00	0.00
5	1	0.00	0.00	11.12	0.00	0.00	0.00

********** END OF LATEST ANALYSIS RESULT **********

39. FINISH

********** END OF STAAD-III **********

```
 **************************************************
 *                                                *
 *          S T A A D - III                       *
 *                                                *
 **************************************************
```

```
 1. STAAD SPACE REPARTO VIENTO
 2. * FICHERO (VIENTO)
 3. UNITS MET MTON
 4. JOINT COORDINATES
 5.    1   0.000  19.500   0.00
 6.    2  22.000  19.500   0.00
 7.    3  50.000  19.500   0.00
 8.    4  78.000  19.500   0.00
 9.    5 100.000  19.500   0.00
10.    6  22.000   1.500   0.00
11.    7  50.000   0.000   0.00
12.    8  78.000   1.500   0.00
13. MEMBER INCIDENCES
14. 1   1  2
15. 2   2  3
16. 3   3  4
17. 4   4  5
18. 5   2  6
19. 6   3  7
20. 7   4  8
21. MEMBER PROPERTIES
22. 1 2 3 4         PRIS AX 6.9280 IX  7.000 IY 89.000 IZ 3.4529
23. 5 6 7           PRIS AX 3.6000 IX  1.600 IY 0.8200 IZ 0.8200
24. CONSTANTS
25. E 3000000.     ALL
26. POISSON 0.15  ALL
27. BETA 0.0  ALL
28. SUPPORTS
29. 1         FIX BUT MY MZ
30. 6 7 8     FIX
31. 5         FIX BUT FX MY MZ
32. MEMBER RELEASES
33. 5 6 7     STA FY MX MY MX
34. LOADING  1 VIENTO Z EN VACIO
35. MEMBER LOAD
36. 1 2 3 4    UNI GZ -0.786
37. LOADING  2 VIENTO Z CON SOBRECARGA
38. MEMBER LOAD
39. 1 2 3 4    UNI GZ -1.076
40. PERFORM ANALYSIS
```


P R O B L E M S T A T I S T I C S

```
 NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS =     8/    7/    5
 ORIGINAL/FINAL BAND-WIDTH =     4/    3
 TOTAL PRIMARY LOAD CASES  =     2, TOTAL DEGREES OF FREEDOM =    23
 SIZE OF STIFFNESS MATRIX =     276 DOUBLE PREC. WORDS
 TOTAL REQUIRED DISK SPACE =   12.02 MEGA-BYTES
```

```
++ PROCESSING ELEMENT STIFFNESS MATRIX.              18:14: 9
++ PROCESSING GLOBAL STIFFNESS MATRIX.               18:14: 9
++ PROCESSING TRIANGULAR FACTORIZATION.              18:14: 9
++ CALCULATING JOINT DISPLACEMENTS.                  18:14: 9
++ CALCULATING MEMBER  FORCES.                       18:14: 9
```

```
41. PRINT SUPPORT REAC
```

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = SPACE

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
1	1	0.00	0.00	34.95	0.00	0.00	0.00
	2	0.00	0.00	47.84	0.00	0.00	0.00
6	1	0.00	0.00	2.70	48.61	0.00	0.00
	2	0.00	0.00	3.70	66.54	0.00	0.00
7	1	0.00	0.00	3.30	64.35	0.00	0.00
	2	0.00	0.00	4.52	88.09	0.00	0.00
8	1	0.00	0.00	2.70	48.61	0.00	0.00
	2	0.00	0.00	3.70	66.54	0.00	0.00
5	1	0.00	0.00	34.95	0.00	0.00	0.00
	2	0.00	0.00	47.84	0.00	0.00	0.00

********** END OF LATEST ANALYSIS RESULT **********

42. FINISH

********** END OF STAAD-III **********

********** END OF STAAD-III **********

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PROYECTO VERDUCTO TORRENTE DEL BÓ

FECHA

HOJA N.º

PILAS

PILAS

PILAS 1 y 3

CARGAS

P_p FUSTE $= 2.5 \times 18.00 \times 0{,}85^2 \times \pi = 102.- t$

(P_p+C_p) TABLERO $\begin{cases} N_{max} = 130.- + 154.78 + 1.3 \times 145.34 + 66.47 = 540.- t \\ N_{mi} = 130.- + 154.78 + 0.7 \times 145.34 + 66.47 = 453.- t \end{cases}$

GRADIENTE TERMICO : $N = -16.- t$

S/ PILAS $\begin{cases} N_{max} = 81.7\ t \\ N_{mi} = -11.- t \end{cases}$

Sc $\begin{cases} N_{max} = 375.- t \\ N_{mi} = -27.- t \end{cases}$

EFECTO LAZO $\begin{cases} N = \pm \dfrac{10 \times 3.18}{6.30} = \pm 5.00\ t \\ M_T = \dfrac{10.00 \times 18.00}{2} = 90.- mt \\ F_T = \dfrac{10.00}{2} = 5.- t \end{cases}$

VIENTO EN YACIO $\begin{cases} N = \pm \dfrac{20.00 \times 1.14}{6.30} = \pm 4.- t \\ M_T = \dfrac{20.00 \times 18.00}{2} + 0.32 \times \dfrac{18^2}{2} = 232.- mt \\ F_T = \dfrac{20.00}{2} + 0{,}32 \times 18.00 = 16.- t \end{cases}$

VIENTO EN SERVICIO $\begin{cases} N = \pm \dfrac{27.00 \times 3.06}{6.30} = \pm 13.- t \\ M_T = \dfrac{27.00 \times 18.00}{2} + 0{,}32 \times \dfrac{18^2}{2} = 295.- mt \\ F_T = \dfrac{27.00}{2} + 0{,}32 \times 18.00 = 19.- t \end{cases}$

REOL. y TERMICA $\begin{cases} M_L = 24.00 \times 18.00 = 432.- mt \\ F_L = (120 + 154.78 + 145.34 + 66.47) \times 0{,}05 = 24.- t \end{cases}$

F. CENTRIFUGA

$f = 0.5$

$Q_{tc} = \dfrac{250 \times 69^2}{9.8 \times 3000} \times 0{,}5 = 30\ kN = 2.- t$

$q_{tc} = \dfrac{80 \times 69^2}{9.8 \times 3000} \times 0.5 = 6\ kN/m = 0.6\ t/m$

$F = 2\left[2.- \times 4 + 0{,}6\left(25.25 - 6.4\right)\right] = 38.- t$

$L_{CLOTOIDE} = 220.- m.$

FUERZA SOBRE PILAS 1 y 3 $\quad F = \dfrac{38 \times 62}{220} = 10.- t$

$F_{FUSTE} = \dfrac{10}{2} = 5.- t$

$M_{T\,FUSTE} = 5.00 \times 18.00 = 90.- mt$

$N_{FUSTE} = \pm \dfrac{10.00 \times (1.80 + 3.18)}{6.30} = \pm 8.- t.$

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 3

ESFUERZOS EN CABEZA DE FUSTE

① $1.35\left(P_p + C_p + Q\right) + 1.5\, W_T$

$N_d = (453 - 16) \times 1.35 - 1.5 \times 4 = 584.- t$

$F_{Ld} = 1.35 \times 24{,}00 = 32.- t$

$F_{Td} = 1.5 \times \frac{20.00}{2} = 15.- t$

② $1.35\left(P_p + C_p + Q\right) + \left(S_c + 0.6\, W\right) \times 1.5$ Max

$N_d = 540 \times 1.35 + \left(31.7 + 37.5 + 13 \times 0.6\right) \times 1.5 = 1350.- t$

$F_{Ld} = 1.35 \times 24.00 = 32.- t$

$F_{Td} = \left(5 + 0.6 \times \frac{27.-}{2}\right) \times 1.5 = 20.- t$

③ $1.35\left(P_p + C_p + R\right) + \left(S_c + 0.6\, W\right) \times 1.5$ Min

$N_d = (458 - 16) \times 1.35 + \left(-11 - 27 - 13 \times 0.6\right) \times 1.5 = 528.- t$

$F_{Ld} = 32.- t$

$F_{Td} = 20.- t$

④ $1.35\left(P_p + C_p + Q\right) + \left(S_c + 0.6\, W\right) \times 1.5$ F. CENTRIFUGA

$N_d = 548 \times 1.35 + \left(0.5 \times 31.7 + 0.5 \times 37.5 + 13 \times 0.6 + 8.00\right) = 959.- t$

$F_{Ld} = 32.- t$

$F_{Td} = 20.- + 5 \times 1.5 = 28.- t$

VTO. TORRENTE DEL BO. FUSTE DE PILAS 1 Y 3

MATERIALES:	HORMIGON	ACERO
"RESIST. CARACT. (kp/cm2):"	300	5100
"COEFICIENTE MINOR. GAMMA:"	1.50	1.15

"ALTURA DE LA PILA (m):" 18.000

DIMENSIONES DE LAS SECCIONES DE HORMIGON:

SECCION:	BASE	CABEZA
"DIAMETRO EXTERIOR (cm):"	170	170
"ESPESOR DE LA PARED(cm):"	85	85

"ARMADURA EXTERIOR: Recubrimiento r (cm):" 5
ARMADURAS TOTALES (cm2) EN 11 SECCIONES A DECIMOS DE LA ALTURA:

Sec: 0	1	2	3	4	5	6	7	8	9	10
482.4	482.4	482.4	241.2	241.2	241.2	241.2	241.2	241.2	241.2	241.2

"ARMADURA INTERIOR: Recubrimiento r (cm):" 5
ARMADURAS TOTALES (cm2) EN 11 SECCIONES A DECIMOS DE LA ALTURA:

Sec: 0	1	2	3	4	5	6	7	8	9	10
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

"NUM. DE HIPOTESIS DE CARGA:" 4

ACCIONES MAYORADAS EN LAS DISTINTAS HIPOTESIS:

	FUERZAS Y MOMENTOS EN LA CABEZA				FUERZAS EN EL FUSTE (t/m)					COEF.
	FUERZAS (t)		MOMENTOS (mt)		SEC.BASE		SEC.CABEZA			GAMMA
HIP.	Fx	Fy	Fz	Mx	My	fx0	fy0	fx1	fy1	PP
1	32.0	15.0	584.0	0.0	0.0	0.000	0.480	0.000	0.480	1.00
2	32.0	20.0	1350.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00
3	32.0	20.0	528.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00
4	32.0	28.0	959.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00

AREAS DE ARMADURAS CONSIDERADAS EN EL CALCULO

Secc.	Ae (cm2)	Ai (cm2)
0	482.40	0.00
1	482.40	0.00
2	482.40	0.00
3	241.20	0.00
4	241.20	0.00
5	241.20	0.00
6	241.20	0.00
7	241.20	0.00
8	241.20	0.00
9	241.20	0.00
10	241.20	0.00

VTO. TORRENTE DEL BO. FUSTE DE PILAS 1 Y 3

HIPOTESIS NUM. 1

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	399.50	728.37	686.14	7.076	12.900
1	0.002	0.001	356.94	669.34	675.93	6.172	11.573
2	0.008	0.004	314.61	607.82	665.71	5.287	10.215
3	0.017	0.009	272.74	544.18	655.50	7.078	14.122
4	0.031	0.016	230.98	477.65	645.28	5.585	11.549
5	0.048	0.025	189.69	408.87	635.07	4.181	9.012
6	0.069	0.036	149.19	338.42	624.86	2.908	6.597
7	0.091	0.047	109.77	266.86	614.64	1.829	4.447
8	0.115	0.059	71.66	194.65	604.43	1.017	2.763
9	0.140	0.071	35.02	122.15	594.21	0.465	1.621
10	0.165	0.083	-0.02	49.60	584.00	0.465	0.657

Exc. totales result. cabeza 0.08493 -0.00003
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 10

VTO. TORRENTE DEL BO. FUSTE DE PILAS 1 Y 3

HIPOTESIS NUM. 2

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	573.76	1008.51	1350.00	10.008	17.592
1	0.003	0.002	526.71	947.06	1350.00	8.917	16.034
2	0.011	0.006	476.69	878.60	1350.00	7.789	14.356
3	0.024	0.013	424.19	803.86	1350.00	10.797	20.460
4	0.043	0.024	367.91	720.17	1350.00	8.493	16.624
5	0.068	0.037	308.84	629.21	1350.00	6.363	12.964
6	0.097	0.052	247.93	532.58	1350.00	4.500	9.667
7	0.129	0.069	185.98	431.72	1350.00	2.985	6.929
8	0.163	0.087	123.65	327.83	1350.00	1.831	4.854
9	0.199	0.105	61.46	221.82	1350.00	0.898	3.243
10	0.236	0.124	-0.19	114.38	1350.00	0.898	1.669

Exc. totales result. cabeza 0.08473 -0.00014
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 18

VTO. TORRENTE DEL BO. FUSTE DE PILAS 1 Y 3

HIPOTESIS NUM. 3

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	462.75	712.47	528.00	8.616	13.266
1	0.002	0.001	417.14	653.74	528.00	7.601	11.912
2	0.008	0.005	371.18	592.97	528.00	6.591	10.529
3	0.018	0.011	325.01	530.39	528.00	9.204	15.020
4	0.032	0.020	278.21	465.25	528.00	7.397	12.370
5	0.050	0.032	231.07	397.99	528.00	5.646	9.725
6	0.072	0.045	183.90	329.07	528.00	3.992	7.144
7	0.095	0.059	136.98	258.92	528.00	2.514	4.752
8	0.121	0.075	90.57	187.96	528.00	1.351	2.804
9	0.147	0.090	44.85	116.53	528.00	0.591	1.535
10	0.174	0.106	-0.03	44.83	528.00	0.591	0.590

Exc. totales result. cabeza 0.08490 -0.00006
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 9

VTO. TORRENTE DEL BO. FUSTE DE PILAS 1 Y 3

HIPOTESIS NUM. 4

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	702.42	854.54	959.00	12.798	15.570
1	0.003	0.002	641.17	794.52	959.00	11.365	14.083
2	0.010	0.008	577.32	730.12	959.00	9.903	12.524
3	0.021	0.017	511.32	661.84	959.00	13.823	17.892
4	0.038	0.030	441.96	587.99	959.00	10.977	14.604
5	0.059	0.047	370.13	509.61	959.00	8.261	11.374
6	0.085	0.067	296.66	427.69	959.00	5.779	8.332
7	0.113	0.088	222.33	343.19	959.00	3.693	5.700
8	0.143	0.111	147.79	256.91	959.00	2.133	3.709
9	0.174	0.135	73.51	169.48	959.00	1.019	2.350
10	0.206	0.158	-0.15	81.32	959.00	1.019	1.127

Exc. totales result. cabeza 0.08480 -0.00015
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 13

PILA-2

CARGAS.

P_p FUSTE $= 2.5 \times 19.50 \times 0.85^2 \times \pi = 110.- t$

(P_p+C_p) TABLERO $\begin{cases} N_{max} = 133.- + 159.78 + 1.3 \times 149.15 + 68.23 = 555.- t \\ N_{min} = 133.- + 159.78 + 0.70 \times 149.15 + 68.23 = 465.- t \end{cases}$

GRADIENTE TERMICO: $N = 6.00 t$

Sc. PARED $\begin{cases} H_{max} = 32.5 t \\ H_{min} = -11.0 t \end{cases}$

Sc $\begin{cases} H_{max} = 390.- t \\ H_{min} = -33.- t \end{cases}$

EFECTO LAZO $\begin{cases} N = \pm \frac{10.00 \times 3.18}{6.30} = \pm 5.00 t \\ M_T = \frac{10.00 \times 19.50}{2} = 98.- mt \\ F_T = \frac{10.00}{2} = 5.- t \end{cases}$

VIENTO EN VACIO $\begin{cases} N = \pm \frac{22.00 \times 1.14}{6.30} = \pm 4.- t \\ M_T = \frac{22.00 \times 19.50}{2} + 0.32 \times \frac{19.50^2}{2} = 275.- mt \\ F_T = \frac{22.00}{2} + 0.32 \times 19.50 = 17.- t \end{cases}$

VIENTO EN SERVICIO $\begin{cases} N = \pm \frac{30.00 \times 3.06}{6.30} = \pm 14.5 t \\ M_T = \frac{30.00 \times 19.50}{2} + 0.32 \times \frac{19.5^2}{2} = 353.- mt \\ F_T = \frac{30.00}{2} + 0.32 \times 19.50 = 21.- t \end{cases}$

GOL. Y TECH. $\begin{cases} M_L = 25.00 \times 19.50 = 488.- mt \\ F_L = (133.- + 159.78 + 149.15 + 68.23) \times 0.05 = 25.- t \end{cases}$

F. CENTRIFUGA

$f = 0.5$

$Q_{tt} = \frac{250 \times 69^2}{9.8 \times 3000} \times 0.5 = 20 kN = 2.- t$

$g_{tt} = \frac{80 \times 69^2}{9.8 \times 3000} \times 0.5 = 6 kN/m = 0.6 t/m.$

$F = 2\left[2.- \times 4 + 0.6(28.00 - 6.4)\right] = 42.- t$

$L_{CATENARIA} = 220.- m.$

FUERZA SOBRE PILA-2 $F = \frac{42 \times 90}{220} = 17.- t$

$F_{FUSTE} = \frac{17}{2} = 8.5 t$

$M_{T_{FUSTE}} = 8.5 \times 19.50 = 166.- mt$

$N_{FUSTE} = \pm \frac{17.00 \times (1.80 + 3.18)}{6.30} = \pm 13.- t$

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 9

ESFUERZOS EN CABEZA DE FUSTE

① $1.35\,(P_p + C_p + R) + 1.5\,W_T$

$N_d = (465 + 6) \times 1.35 - 1.5 \times 4 = 630,- \text{ t}$

$F_{Ld} = 1.35 \times 25.00 = 38,- \text{ t}$

$F_{Td} = 1.5 \times \frac{22,-}{2} = 17,- \text{ t}$

② $1.35(P_p + C_p + R) + (S_c + 0.6\,W) \times 1.5$ N max

$N_d = (555 + 6) \times 1.35 + (32.5 + 390 + 4 \times 0.6) \times 1.5 = 1394,- \text{ t}$

$F_{Ld} = 1.35 \times 25,00 = 38,- \text{ t}$

$F_{Td} = \left(5 + 0.6 \times \frac{30,-}{2}\right) \times 1.5 = 21,- \text{ t}$

③ $1.35\,(P_p + C_p + R) + (S_c + 0.6\,W) \times 1.5$ N min

$N_d = 465 \times 1.35 + (-11 - 33 - 4 \times 0.6) \times 1.5 = 558,- \text{ t}$

$F_{Ld} = 38,- \text{ t}$

$F_{Td} = 21,- \text{ t}$

④ $1.35\,(P_p + C_p + R) + (S_c + 0.6\,W) \times 1.5$ F. CENTRIFUGA

$N_d = (555 + 6)\,1.35 + (0.5 \times 32.5 + 0.5 \times 390 + 4 \times 0.6 + 13,-) \times 1.5 = 1097,- \text{ t}$

$F_{Ld} = 38,- \text{ t}$

$F_{Td} = 21,- + 8.5 \times 1.5 = 34,- \text{ t}$

Siegrist y Moreno S.L.

PROYECTO TORRENTE DEL BS

FECHA 14. VII. 03

HOJA N.º 10

CÁLCULO DE FUSTES DE PILAS.

Cargas mayoradas en cota de apoyo / fuste:

HIP.	F_{Ld} (t)	F_{Td} (t)	N_d (t)	q_t (t/m) en fuste.
H-1	38	17	630	0,480
H-2	38	21	1394	0,288
H-3	38	21	558	0,288
H-4.	38	34	1097	0,288.

Diámetro exterior fuste $\varnothing = 1,70$ m.

Hormigón HA-30.

Acero B500S.

Altura de cálculo: 19,50 m.

Necesito 60 ϕ32 en 13,65 m. (+ adherencia) = 15.00 m.

Cortante: $V_d = 51$ t. $\rho_L = \frac{30 \times 8.04}{\pi \times 85^2} = 0.01$

$b_o = 1,507$ m.

$d = 1,4$ m. $\xi = 1,378$

$\sigma'_{cd} = \frac{558}{\pi \times 0,85^2} = 246 \text{ t/m}^2 = 2,458 \text{ N/mm}^2$.

$V_{cu} = \left[0.1 \times 1,378 \times (100 \times 0.01 \times 30)^{1/3} + 0.15 \times 2,458\right] 1507 \times 1400 =$

$= 168,13$ t. >> V_d.

Despreciando el efecto favorable de las compresiones: $V_{cu} = 90$ t

$\rightarrow A_{st} = 0.02 \times \frac{3000}{1.5} \times 1,507 \times \frac{d}{4} = 15,07 \text{ cm}^2/\text{m}$.

c ϕ16 / 0.25.

VTO. TORRENTE DEL BO. FUSTE DE PILA 2

MATERIALES:	HORMIGON	ACERO
"RESIST. CARACT. (kp/cm2):"	300	5100
"COEFICIENTE MINOR. GAMMA:"	1.50	1.15

"ALTURA DE LA PILA (m):" 19.500

DIMENSIONES DE LAS SECCIONES DE HORMIGON:

SECCION:	BASE	CABEZA
"DIAMETRO EXTERIOR (cm):"	170	170
"ESPESOR DE LA PARED(cm):"	85	85

"ARMADURA EXTERIOR: Recubrimiento r (cm):" 5
ARMADURAS TOTALES (cm2) EN 11 SECCIONES A DECIMOS DE LA ALTURA:

Sec: 0	1	2	3	4	5	6	7	8	9	10
482.4	482.4	482.4	482.4	482.4	482.4	482.4	241.2	241.2	241.2	241.2

"ARMADURA INTERIOR: Recubrimiento r (cm):" 5
ARMADURAS TOTALES (cm2) EN 11 SECCIONES A DECIMOS DE LA ALTURA:

Sec: 0	1	2	3	4	5	6	7	8	9	10
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

"NUM. DE HIPOTESIS DE CARGA:" 4

ACCIONES MAYORADAS EN LAS DISTINTAS HIPOTESIS:

	FUERZAS Y MOMENTOS EN LA CABEZA					FUERZAS EN EL FUSTE (t/m)				COEF.
	FUERZAS (t)			MOMENTOS (mt)		SEC.BASE		SEC.CABEZA		GAMMA
HIP.	Fx	Fy	Fz	Mx	My	fx0	fy0	fx1	fy1	pp
1	38.0	17.0	630.0	0.0	0.0	0.000	0.480	0.000	0.480	1.00
2	38.0	21.0	1394.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00
3	38.0	21.0	558.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00
4	38.0	34.0	1097.0	0.0	0.0	0.000	0.288	0.000	0.288	0.00

AREAS DE ARMADURAS CONSIDERADAS EN EL CALCULO

Secc.	Ae (cm2)	Ai (cm2)
0	482.40	0.00
1	482.40	0.00
2	482.40	0.00
3	482.40	0.00
4	482.40	0.00
5	482.40	0.00
6	482.40	0.00
7	241.20	0.00
8	241.20	0.00
9	241.20	0.00
10	241.20	0.00

VTO. TORRENTE DEL BO. FUSTE DE PILA 2

HIPOTESIS NUM. 1

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	495.90	943.91	740.65	9.308	17.717
1	0.003	0.002	444.11	867.34	729.59	8.146	15.908
2	0.013	0.007	391.92	786.42	718.52	6.995	14.036
3	0.028	0.014	339.72	701.80	707.46	5.867	12.120
4	0.047	0.024	287.85	614.10	696.39	4.770	10.177
5	0.070	0.035	236.67	523.95	685.33	3.718	8.231
6	0.097	0.048	186.48	431.93	674.26	2.726	6.314
7	0.125	0.063	137.56	338.59	663.20	2.569	6.323
8	0.156	0.078	89.99	243.99	652.13	1.373	3.722
9	0.189	0.093	44.06	148.83	641.07	0.589	1.989
10	0.222	0.109	-0.01	53.54	630.00	0.589	0.713

Exc. totales result. cabeza 0.08498 -0.00001
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 10

VTO. TORRENTE DEL BO. FUSTE DE PILA 2

HIPOTESIS NUM. 2

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	695.76	1329.04	1394.00	14.372	27.454
1	0.005	0.003	640.60	1247.66	1394.00	12.217	23.795
2	0.019	0.010	580.06	1153.67	1394.00	10.551	20.985
3	0.042	0.022	515.02	1048.56	1394.00	8.958	18.238
4	0.071	0.036	446.32	933.78	1394.00	7.355	15.387
5	0.106	0.054	374.82	810.84	1394.00	5.781	12.505
6	0.146	0.074	301.36	681.28	1394.00	4.285	9.687
7	0.189	0.095	226.71	546.58	1394.00	4.090	9.860
8	0.236	0.118	151.00	406.65	1394.00	2.343	6.310
9	0.286	0.142	75.14	263.38	1394.00	1.106	3.879
10	0.337	0.166	-0.22	118.06	1394.00	1.106	1.734

Exc. totales result. cabeza 0.08469 -0.00016
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 21

VTO. TORRENTE DEL BO. FUSTE DE PILA 2

HIPOTESIS NUM. 3

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	533.66	913.20	558.00	10.370	17.746
1	0.003	0.002	481.21	837.22	558.00	9.159	15.935
2	0.013	0.007	427.90	757.85	558.00	7.948	14.077
3	0.028	0.016	374.01	675.50	558.00	6.744	12.181
4	0.047	0.027	319.78	590.57	558.00	5.556	10.260
5	0.070	0.040	265.47	503.46	558.00	4.391	8.328
6	0.097	0.055	211.32	414.58	558.00	3.266	6.407
7	0.126	0.071	157.57	324.34	558.00	3.222	6.631
8	0.157	0.088	104.24	232.69	558.00	1.693	3.780
9	0.190	0.106	51.64	140.25	558.00	0.688	1.870
10	0.224	0.124	-0.01	47.40	558.00	0.688	0.626

Exc. totales result. cabeza 0.08495 -0.00003
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 9

VTO. TORRENTE DEL BO. FUSTE DE PILA 2

HIPOTESIS NUM. 4

Sec.	flch.x	flch.y	Mom.x	Mom.y	Axil	curv.x	curv.y
0	0.000	0.000	997.02	1181.42	1097.00	24.811	29.400
1	0.006	0.005	915.14	1101.19	1097.00	18.382	22.119
2	0.020	0.016	826.69	1011.73	1097.00	15.654	19.157
3	0.041	0.034	732.81	914.28	1097.00	13.322	16.621
4	0.068	0.057	634.46	809.90	1097.00	10.981	14.017
5	0.101	0.084	532.63	699.67	1097.00	8.666	11.383
6	0.139	0.114	428.27	584.69	1097.00	6.429	8.778
7	0.179	0.147	322.33	466.05	1097.00	6.241	9.023
8	0.223	0.182	214.89	343.65	1097.00	3.387	5.417
9	0.269	0.218	107.12	218.98	1097.00	1.514	3.094
10	0.317	0.255	-0.18	93.03	1097.00	1.514	1.312

Exc. totales result. cabeza 0.08480 -0.00016
Exc. reales 1er ord. cabeza 0.08500 0.00000

Convergencia del equilibrio sin agotamiento
NÈmero de iteraciones: 35

13

Siegrist y Moreno S.L.

PROYECTO: VIADUCTO TORRENTE DEL BÓ

FECHA:

HOJA N.º:

CIMENTACION PILA

Siegrist y Moreno S.L.

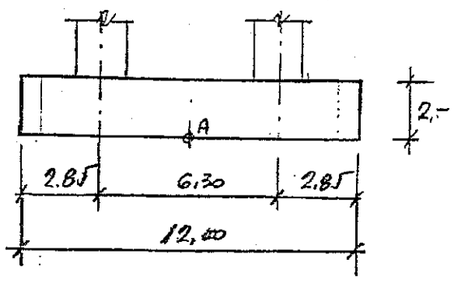
PROYECTO .....

FECHA .....

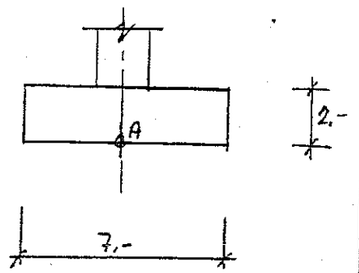
HOJA N.º .....

CIMENTACION PILAS

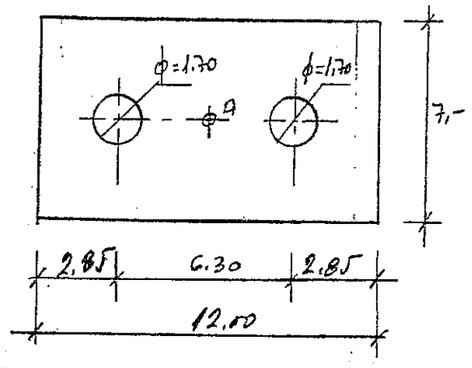
• DEFINICION GEOMETRICA



ALZADO



ALZADO LATERAL



PLANTA

• CARGAS REDUCIDAS AL PUNTO Ⓐ

P_p. FUSTES $= 2 \times 2,5 \times 19,50 \times 0,85^2 \times \pi = 221,-\ t$

P_p. ZAPATA $= 2,5 \times 12,00 \times 7,00 \times 2,00 = 420,-\ t$

P_p. TIERRAS $= 2,00 \times 12,00 \times 7,00 \times 5,00 = 840,-\ t$

(P_p+C_p) TABLERO $\begin{cases} MAX = 2(133,- + 159,78 + 1,3 \times 149,15 + 68,23) = 1110,-\ t \\ MIN = 2(133,- + 159,78 + 0,70 \times 149,15 + 68,23) = 930,-\ t \end{cases}$

GRADIENTE TERMICO $= 2 \times 6,00 = 12,-\ t$

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º .....

Sc PASEO $\begin{cases} N_{MAX} = 2 \times 32,5 = 65,-\ t \\ N_{MIN} = -2 \times 11,- = -22,-\ t \end{cases}$

Sc $\begin{cases} N_{MAX} = 716,-\ t & M_T = 210,-\ mt \\ N_{MIN} = -66,-\ t & M_T = 70,-\ mt \\ N = 325,-\ t & M_{T\,MAX} = 1036,-\ mt \end{cases}$

EFECTO LAZO $\begin{cases} M_T = 10(19,50 + 3,18 + 2,00) = 247,-\ mt \\ F_T = 10,-\ t \end{cases}$

VIENTO VACIO $\begin{cases} M_T = 22(19,50 + 1,14 + 2,00) + 2 \times 0,32 \times 19,50 \times 11,75 = 645,-\ mt \\ F_T = 22 + 2 \times 0,32 \times 19,50 = 34,-\ t \end{cases}$

VIENTO LLENO $\begin{cases} M_T = 30(19,50 + 3,06 + 2,00) + 2 \times 0,32 \times 19,50 \times 11,75 = 883,-\ mt \\ F_T = 30 + 2 \times 0,32 \times 19,50 = 42,-\ t \end{cases}$

DESC. y TERMICA $\begin{cases} M_L = 50(19,50 + 2,00) = 1075,-\ mt \\ F_L = 2(133 + 159,78 + 149,15 + 68,23)\,0,05 = 50,-\ t \end{cases}$

F. CENTRIFUGA

$f = 0,5$

$Q_{tn} = \dfrac{250 \times 69^2}{9,8 \times 3000} \times 0,5 = 20\ KN = 2,-\ t$

$q_{tn} = \dfrac{80 \times 69^2}{9,8 \times 3000} \times 0,5 = 6\ KN/m = 0,6\ t/m.$

$F = 2\left[2 \times 4 + 0,6(28,00 - 6,4)\right] = 42,-\ t$

$\angle$ CLOTOIDE $= 220,-\ m.$

FUERZA SOBRE PILA - 2 $\quad F = \dfrac{42 \times 90}{220} = 17,-\ t$

$M_T = 17(19,50 + 3,18 + 1,80 + 2,00) = 450,-\ mt.$

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º .....

• COMPROBACION DE TENSIONES

① $P_p + C_p + Q + W_T$

$N = 221,- + 420,- + 840,- + 1110,- = 2591,- t$

$M_L = 1075,- mt$

$M_T = 644,- mt$

$$\sigma = \frac{2591,-}{12,00 \times 7,00} \pm \frac{1075,-}{98,-} \pm \frac{644,-}{168,-} = \begin{cases} 46,- t/m^2 \\ 16,- t/m^2 \end{cases}$$

② $P_p + C_p + R + S_c + 0.6\,W$ Nmax

$N = 221 + 420 + 840 + 1110 + 65 + 716 = 3372,- t$

$M_L = 1075,- mt$

$M_T = 210,- + 0.6 \times 883,- + 247,- = 987,- mt$

$$\sigma = \frac{3372,-}{12,00 \times 7,00} \pm \frac{1075,-}{98,-} \pm \frac{987,-}{168,-} = \begin{cases} 57,- t/m^2 \\ 23,- t/m^2 \end{cases}$$

③ $P_p + C_p + R + S_c + 0.6\,W$ Nmin

$N = 221 + 420 + 840 + 930 + 65 - 66 = 2410,- t$

$M_L = 1075,- mt$

$M_T = 70,- + 0.6 \times 883,- + 247,- = 847,- mt$

$$\sigma = \frac{2410,-}{12,00 \times 7,00} \pm \frac{1075,-}{98,-} \pm \frac{847,-}{168,-} = \begin{cases} 45,- t/m^2 \\ 13,- t/m^2 \end{cases}$$

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PROYECTO .....

FECHA .....

HOJA N.º .....

④ $P_p + C_p + R + S_c + 0.6\,W$ $M_{T\,max}$

$N = 221 + 420 + 840 + 1110 + 65 + 325 = 2981,- t$

$M_L = 1075,- mt$

$M_T = 1036 + 0.6 \times 883 + 247,- = 1813,- mt$

$$\sigma = \frac{2981}{12,00 \times 7,00} \pm \frac{1075}{98,-} \pm \frac{1813}{168,-} = \begin{cases} 57,- t/m^2 \\ 14,- t/m^2 \end{cases}$$

⑤ $P_p + C_p + R + S_c + 0.6\,W$ F. CENTRIFUGA

$N = 221 + 420 + 840 + 1110 + 65 + 0.5 \times 325 = 2818,- t$

$M_L = 1075,- mt$

$M_T = 0,5 \times 1036 + 450 + 0.6 \times 883 + 247 = 1745,- mt$

$$\sigma = \frac{2818}{12,00 \times 7,00} \pm \frac{1075}{98,-} \pm \frac{1745}{168,-} = \begin{cases} 55,- t/m^2 \\ 12,- t/m^2 \end{cases}$$

TENSIONES MAYORADAS PARA CALCULO DE ARMADURAS

② $(P_p + C_p + R) \times 1.35 + 1.5\,S_c + 1.5 \times 0.6 \times W$

$N_d = (221 + 420 + 840 + 1110) \times 1.35 + (65 + 716) \times 1.5 = 4669,- t$

$M_d = 1,35 \times 1075,- = 1451,- mt$

$M_{Td} = 1.5 \times 987,- = 1480,- mt$

$$\sigma = \frac{4669}{12,00 \times 7,00} \pm \frac{1451}{98} = \begin{cases} 70,- t/m^2 \\ 42,- t/m^2 \end{cases}$$

$$\sigma = \frac{4669}{12,00 \times 7,00} \pm \frac{1480}{168} = \begin{cases} 64,- t/m^2 \\ 48,- t/m^2 \end{cases}$$

Siegrist y Moreno S.L.

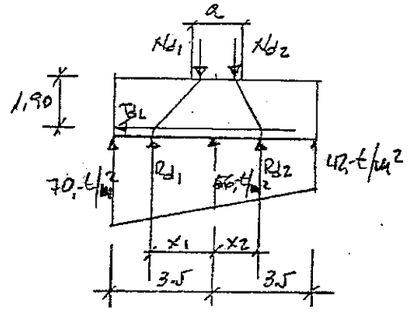
PROYECTO.....

FECHA.....

HOJA N.º.....

ARMADURA ZAPATA

• LONGITUDINAL



Ancho = 12.- m.

$R_{d1} = \frac{70+56}{2} \times \frac{12.00}{2} \times 3,50 = 1323,-t$

$R_{d2} = \frac{56+42}{2} \times \frac{12.00}{2} \times 3,50 = 1029,-t$

$N_{d1} = 1323 - 6.00 \times 3,50 \times 2,00 \times 2,5 \times 1,35 - 6,00 \times 3,50 \times 5,00 \times 2,00 \times 1,35 = 898,-t$

$N_{d2} = 1029 - 6,00 \times 3,50 \times 2,00 \times 2,5 \times 1,35 - 6,00 \times 3,50 \times 5,00 \times 2,00 \times 1,35 = 604,-t$

$x_1 = \frac{56+2\times70}{56+70} \times \frac{3,50}{3} = 1,82$ m

$x_2 = \frac{56+2\times42}{56+42} \times \frac{3,50}{3} = 1,66$ m.

$T_{d1} = \frac{1323}{0,85 \times 1,90}\left(1,82 - 0,25 \times 1,50\right) = 1183,-t \rightarrow 267,-cm^2 \rightarrow 44,5 cm^2/m$

$A_c = 0,75 \cos\left(\operatorname{arctg} \frac{1,90}{1,145}\right) \times 1,50 = 0,90\ m^2$

$B_d = 0,90 \times 0,85 \times \frac{2500}{1,5} = 1275,-t > N_{d1}$

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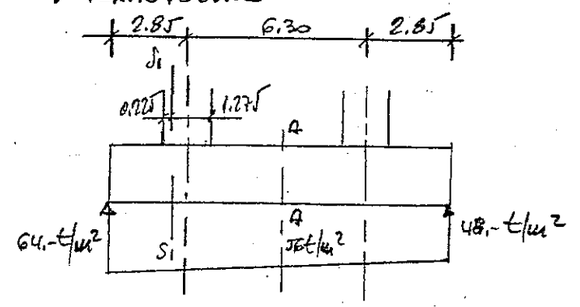
PROYECTO.....

FECHA.....

HOJA N.º.....

• TRANSVERSAL



Ancho = 7.- m.

$M_{dS1} = \left(64 - 2\times2,5 - 2\times5,00\right) \times \frac{2,325^2}{2} = 132,-\ mt/m.$

$M_{dA} = \left(56 - 2\times2,5 - 2\times5,00\right)\left(\frac{6,30^2}{8} - \frac{3,35^2}{2}\right) = -27,-\ mt/m.$

$U_c = \frac{0,85 \times 2500}{1,5} \times 1,00 \times 1,90 = 2692,-$

$A = 2692\left(1 - \sqrt{1 - \frac{2\times132}{2692\times1,90}}\right) \times \frac{1,15}{5,1} = 15,18\ cm^2/m. \rightarrow 29,-\ cm^2/m.$

• COMPROBACION DE BIELAS Y TIRANTES

$R_{d1} = \frac{64+60}{2} \times 7,00 \times 3,35 = 1454,-t$

$N_{d1} = 1454,- - 7,00 \times 3,35 \times 2,00 \times 2,5 \times 1,35 - 7,00 \times 3,35 \times 5,00 \times 2,00 \times 1,35 = 979,-t$

$x_1 = \frac{60+2\times64}{60+64} \times \frac{3,35}{3} = 1,69$

$T_{d1} = \frac{1454}{0,85 \times 1,90}\left(1,69 - 0,25 \times 1,50\right) = 1184,-t \rightarrow 267,-cm^2 \rightarrow 38,-\ cm^2/m$

$A_c = 0,75 \cos\left(\operatorname{arctg} \frac{1,90}{1,315}\right) \times 1,50 = 0,93\ m^2$

$B_d = 0,93 \times 0,85 \times \frac{2500}{1,5} = 1317,-t > N_{d1}$

Siegrist y Moreno S.L.

PROYECTO: VIADUCTO TORRENTE DEL BO'

FECHA:

HOJA N.º:

ESTRIBO - 1 (FIJO)

Siegrist y Moreno S.L.

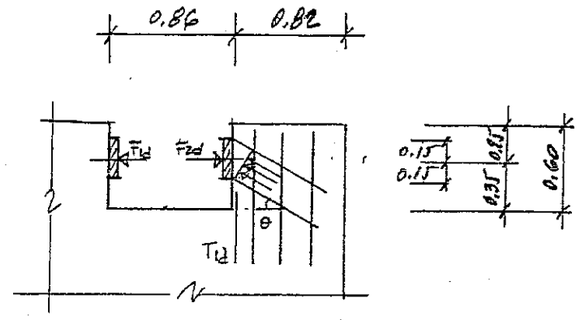
PROYECTO:

FECHA:

HOJA N.º: 1

ESTRIBO - 1 (FIJO)

ARMADURA PARA RESISTIR, LOCALMENTE, LA FUERZA LONGETUDENAL



$F_{1d} = 1.5 \times 371 + 1.35(167 + 221) = 1080,- t = F_{2d}$

Estas fuerzas se transmiten mediante 4 apoyos de neopreno separados 0,80 m.

Por tanto $f_{d\,máx} = \frac{1080,-}{4 \times 0.80} = 338,- t/m.$

Se calcula como una ménsula corta.

$\cot g\,\theta = 1.4 \quad d \geq \frac{a}{0,85} \cot g\,\theta = \frac{0.35}{0,85} \times 1,40 = 0,576 < 0.72$

$T_{1d} = f_{d\,máx} \times \cot g\,\theta + F_{hd} = A_s f_{yd} \quad (F_{hd} = 0)$

$T_{1d} = 338 \times \frac{1}{1.4} = 241,- t/m. \quad A_s = \frac{241}{4} = 60,25\ cm^2/m.$

$T_{2d} = 0,20 \times f_{d\,máx} = A_{sc} f_{yd}$

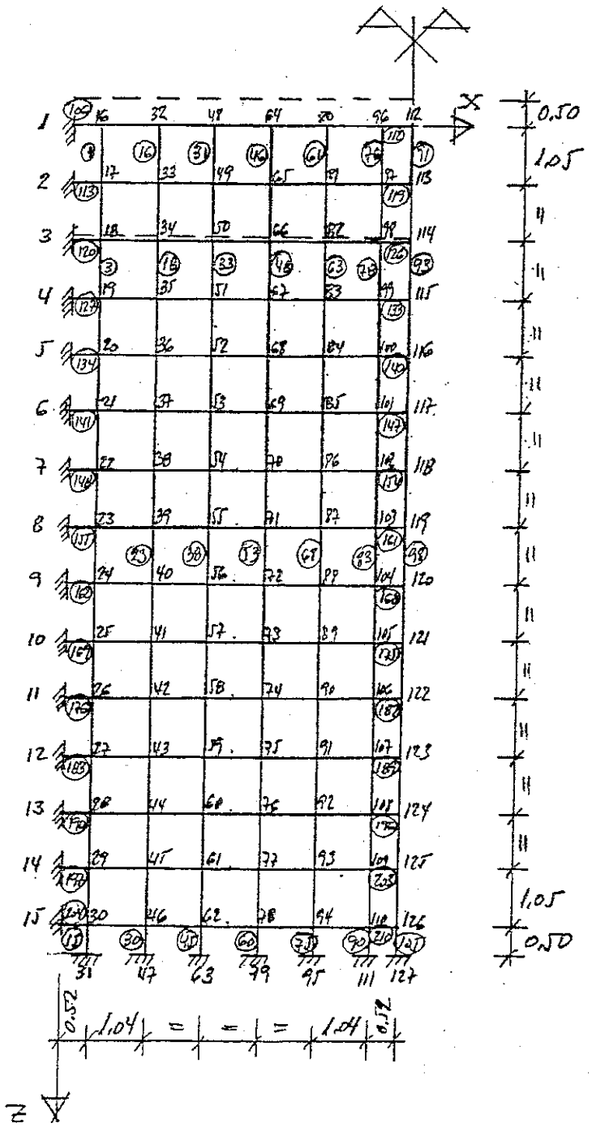
$T_{2d} = 0,20 \times 338 = 67.60\ t/m. \quad A_{sc} = \frac{67,60}{4} = 16,9\ cm^2/m.$

$\frac{1080}{4} \times \frac{1}{0,80 \times 0,30} = 1125,- \text{ t/m}^2 < f_{1cd} = 0,7 \times \frac{2.500}{1,5} = 1167,- \text{ t/m}^2$

Los apoyos se disponen de 800 x 300.

ARMADURA EN ALZADO

Calculamos el siguiente empotrillado.



Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 4

- CARACTERISTICAS DE CADA BARRA

BARRA	a	h	A	I	J
1-2-16-17-31-32 / 46-47-61-62-76-77	1,04	0.65	0.520	0.01083	0,02166
91-92	0.52	0.65	0.260	0.00542	0,01084
3 a 15 - 18 a 30 / 33 a 45 - 48 a 60 / 63 a 75 - 78 a 90	1.04	2.50	2,444	1,12475	2,24950
93 a 105	0.52	2,50	1.222	0,56237	1.12474
106 a 119	1.05	0.65	0.525	0.01094	0,02188
120 a 126	1.05	1.575	1,496	0,25319	0.50638
127 a 210	1.05	2.50	2,468	1,13556	2.27112

- HIPOTESIS DE CARGA

H-1 EMPUJE DE TIERRAS

$$e = 0{,}33\,(3.00 + z \times 2.00)\ t/m^2$$

z	0.50	1.55	2,60	3,65	4,70	5,75
e	1.320	2.013	2,706	3,399	4,092	4,785

z	6.80	7.85	8,90	9.95	11.00	12.05
e	5.478	6.171	6.864	7.557	8,250	8,943

z	13.10	14.15	15.20
e	9,636	10,329	11.022

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 5

H-2 FRENADO + ARRANQUE

NUDOS 82 y 98

$$F_y = \frac{371}{2 \times 2} = 93{,}-\ t$$

H-3 DIFERENCIA + INT. CARRIL TABLERO

NUDOS 82 y 98

$$F_y = \frac{167 + 221}{2 \times 2} = 97{,}-\ t$$

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 6

ARMADURA

FLEXION

$$U_c = \frac{0,85 \times 2500}{1,5} \times d$$

$$A = U_c \left[1 - \sqrt{1 - \frac{2 M_d^*}{U_c \times d}}\right] \times \frac{1.15}{5.1} \ cm^2/m.$$

$$M_d^* = \frac{M_d + T_d}{a} \quad \text{(con el mismo signo del } M_d\text{)}$$

DIRECCION	NUDO	a	d	M_d	T_d	M_d^*	ARMADURA cm^2/m A INT.	A EXT.
VERTICAL	34	1,04	0,60	4,53	3,23	7,46	2,82	—
	66	1,04	0,60	6,37	1,21	7,29	2,76	—
	98	1,04	0,60	9,09	0,59	9,31	3,53	—
	114	0,52	0,60	4,21	0,0	8,10	3,07	—
	40	1,04	2,45	-44,50 22,99	97,80 165,15	-136,83 188,60	17,56	12,70
	72	1,04	2,45	63,80 -96,29	116,16 67,65	173,04 -157,63	16,09	14,64
	104	1,04	2,45	78,88 -120,95	26,10 15,13	100,94 -130,85	7,35	12,14
	120	0,52	2,45	37,70 -59,84	0,0 0,0	72,50 -115,08	6,70	10,66
	47	1,04	2,45	143,14	21,36	158,17	14,70	—
	79	1,04	2,45	269,78	11,88	270,83	25,24	—
	111	1,04	2,45	313,63	1,18	302,70	28,37	—
	127	0,52	2,45	156,98	0,0	301,90	28,30	—

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 7

DIRECCION	NUDO	a	d	M_d	T_d	M_d^*	ARMADURA cm^2/m A. INT.	A. EXT.
HORIZONTAL	1	1,05	0,60	-15,20 3,67	0,36 0,24	-15,40 3,72	5,88	1,40
	2	1,05	0,60	-11,37 5,07	0,76 0,26	-11,46 5,08	4,36	1,92
	3	0,525	0,60	-2,04 1,40	0,10 0,08	-4,08 2,80	1,54	1,06
	3a6	1,05	2,45	-487,50 277,10	35,00 31,95	-497,60 293,67	49,02	29,38
	7	1,05	2,45	-270,60 69,91	19,92 19,10	-276,70 76,20	27,65	7,50
	8	1,05	2,45	-207,93	14,45	-211,80	19,74	—
	9	1,05	2,45	-163,13	10,60	-165,46	15,38	—
	10	1,05	2,45	-129,92	8,72	-131,56	12,20	—
	11	1,05	2,45	-102,87	7,07	-104,70	9,70	—
	112	1,05	0,60	-8,66 -6,50	0,14 0,0	8,38 -6,20	2,34	3,18
	113	1,05	0,60	7,87 -5,74	0,22 0,26	7,70 -5,70	2,15	2,92
	114	0,525	0,60	1,40 -0,80	0,73 0,02	2,70 -1,56	0,59	1,02
	114a117	1,05	2,45	506,60 -278,56	20,18 16,40	501,12 -280,90	26,29	42,57
	118	1,05	2,45	360,24 -153,33	17,48 12,49	359,73 -157,92	14,67	33,84
	119	1,05	2,45	290,43 -106,37	15,30 9,60	291,17 -110,45	10,23	27,27
	120	1,05	2,45	229,78 -79,75	13,70 7,23	230,93 -74,87	6,87	21,55
	121	1,05	2,45	173,10 -44,56	12,50 5,20	176,76 -47,39	4,37	16,44
	122	1,05	2,45	122,50 -26,30	11,28 3,50	187,41 -28,38	2,62	11,82

CORTANTE

$$V_{cu} = \left[0.10 \times \xi \left(100 \rho f_{ck}\right)^{1/3} - 0.15\,\sigma'_{cd}\right] b_o \times d \times \beta$$

$$\xi = 1 + \sqrt{\frac{200}{d}} \qquad h = 0.65 \quad \xi = 1.555 \qquad h = 2.50 \quad \xi = 1.283$$

ρ (armadura mínima) { Vertical 0.0009 < 0,02 ; Horizontal 0.0016 < 0,02

$f_{ck} = 25\ N/mm^2$, $b_o = 1000$ mm $\beta = 1$

V_{cu} Vertical { $h = 0.65$ $V_{cu} = 122.258\ N/m = 12.22\ t/m$; $h = 2.50$ $V_{cu} = 411.895\ N/m = 41.18\ t/m$

V_{cu} Horizontal { $h = 0.65$ $V_{cu} = 148.105\ N/m = 14.81\ t/m$; $h = 2.50$ $V_{cu} = 498.976\ N/m = 49.90\ t/m$

DIRECCION	NUDO	a	d	V_d	V_d^*	A_{st} (cm²/m)
VERTICAL	47	1,04	2.45	74,60	71.73	3.46
	63	1,04	2.45	99,50	95.67	6.18
	79	1,04	2.45	115,10	110,67	7.88
	95	1,04	2.45	121,20	116,54	8,54
	111	1,04	2.45	110,40	106,15	7.37
	127	0.52	2,45	52.84	50.81	1,09
	45	1.04	2.45	52,-	50,-	1,-
	61	1,04	2.45	75,30	72.40	3.54
	77	1,04	2.45	89.90	86.44	5.13
	93	1,04	2.45	95.98	92.29	5.79
	109	1,04	2,45	92,93	89.36	5.46
	125	0,52	2,45	45.30	43.56	0.27

$$A_{st} = \frac{V_d^* - V_{cu}}{0.9 \times d \times 4} \ cm^2/m$$

$$V_d^* = \frac{V_d}{a}$$

DIRECCION	NUDO	a	d	V_d	V_d^*	A_{st} (cm²/m)
V E R T I C A L	41	1,04	2.45	15,30	14.70	—
	57	1,04	2,45	24,90	23.94	—
	73	1,04	2.45	33,11	31,84	—
	89	1,04	2.45	38,80	37.31	—
	105	1,04	2.45	32,84	31.58	—
	121	0,52	2,45	13,04	25,-	—
	35	1,04	2.45	11.6	11,15	-
	51	1,04	2.45	27,40	26.35	—
	67	1,04	2.45	55,71	53.58	1.41
	83	1.04	2.45	145.25	139.66	11.17
	99	1,04	2.45	77,07	74.11	3.73
	115	0.52	2.45	50,76	97.62	6.40
	36	1,04	2.45	16,70	16,06	—
	52	1,04	2.45	30,70	29,52	—
	68	1,04	2.45	55,70	53.56	1.40
	84	1,04	2.45	71.08	68,35	3.08
	100	1,04	2.45	75,60	72,69	3.57
	116	0,52	2.45	36,25	69.71	3.23
	70	1,04	2.45	36,46	35,06	—
	86	1,04	2.45	44,46	42,75	0.18
	102	1,04	2.45	36,08	34.69	—
	118	0,52	2.45	12,08	23.23	—

Siegrist y Moreno S.L.

PROYECTO .....

FECHA .....

HOJA N.º 10

SECCION	NUDO	a	d	V_d	V_d^+	A_{st} (cm²/m)
ZONTAL	3a6	1,05	2,45	209,50	199,5	16,96
	7	1,05	2,45	79,64	75,85	2,94
	8	1,05	2,45	65,02	61,92	1,36
	9	1,05	2,45	57,36	54,63	0,54
	10	1,05	2,45	59,57	56,71	0,77
	11	1,05	2,45	59,57	56,68	0,77
	12	1,05	2,45	53,72	51,16	0,14
	13	1,05	2,45	41,59	39,61	—
	14	1,05	2,45	22,43	21,42	—
	15	1,05	2,45	4,39	4,18	—
	116a117	1,05	2,45	29,50	28,10	—
	118	1,05	2,45	6,-	5,71	—
	119	1,05	2,45	2,-	1,90	—


```
 1. STAAD FLOOR ESTRIBO 1  ALZADO (EMPOTRADO)
 2. * FICHERO (EMPA1)
 3. UNITS MET MTON
 4. JOINT COORDINATES
 5.  1  0.00 0.0 0.0 15  0.00 0.0 14.70
 6. 16  0.52 0.0 0.0 30  0.52 0.0 14.70
 7. 31  0.52 0.0 15.20
 8. 32  1.56 0.0 0.0 46  1.56 0.0 14.70
 9. 47  1.56 0.0 15.20
10. 48  2.60 0.0 0.0 62  2.60 0.0 14.70
11. 63  2.60 0.0 15.20
12. 64  3.64 0.0 0.0 78  3.64 0.0 14.70
13. 79  3.64 0.0 15.20
14. 80  4.68 0.0 0.0 94  4.68 0.0 14.70
15. 95  4.68 0.0 15.20
16. 96  5.72 0.0 0.0 110 5.72 0.0 14.70
17. 111 5.72 0.0 15.20
18. 112 6.24 0.0 0.0 126 6.24 0.0 14.70
19. 127 6.24 0.0 15.20
20. MEMBER INCIDENCES
21.  1  16  17  15
22. R 6 15 16
23. 107 16 32 112 1 16
24. R 14 7 1
25. 106 1 16
26. R 14 7 1
27. MEMBER PROPERTIES
28.   1 2 16 17 31 32          PRIS AX 0.520 IX 0.02166 IZ 0.01083
29.  46 47 61 62 76 77          PRIS AX 0.520 IX 0.02166 IZ 0.01083
30.  91 92                      PRIS AX 0.260 IX 0.01084 IZ 0.00542
31.   3 TO 15 18 TO 30 33 TO 45 PRIS AX 2.444 IX 2.24950 IZ 1.12475
32.  48 TO 60 63 TO 75 78 TO 90 PRIS AX 2.444 IX 2.24950 IZ 1.12475
33.  93 TO 105                  PRIS AX 1.222 IX 1.12474 IZ 0.56237
34. 106 TO 119                  PRIS AX 0.525 IX 0.02188 IZ 0.01094
35. 120 TO 126                  PRIS AX 1.496 IX 0.50638 IZ 0.25319
36. 127 TO 210                  PRIS AX 2.468 IX 2.27112 IZ 1.13556
37. CONSTANTS
38. E 3000000. ALL
39. POISSON 0.15 ALL
40. SUPPORTS
41.  1 TO 15        FIXED
42. 31 TO 127 BY 16 FIXED
43. 112 TO 126      FIXED BUT FY MX
44. LOADING  1 EMPUJE DE TIERRAS
45. MEMBER LOADS
46. 106 TO 112    UNI GY  1.320
47. 113 TO 119    UNI GY  2.013
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48. 120 TO 126    UNI GY  2.706
49. 127 TO 133    UNI GY  3.399
50. 134 TO 140    UNI GY  4.092
51. 141 TO 147    UNI GY  4.785
52. 148 TO 154    UNI GY  5.478
53. 155 TO 161    UNI GY  6.171
54. 162 TO 168    UNI GY  6.864
55. 169 TO 175    UNI GY  7.557
56. 176 TO 182    UNI GY  8.250
57. 183 TO 189    UNI GY  8.943
58. 190 TO 196    UNI GY  9.636
59. 197 TO 203    UNI GY 10.329
60. 204 TO 210    UNI GY 11.022
61. LOADING  2 FRENADO+ARRANQE
62. JOINT LOADS
63.  82 98        FY 93.00
64. LOADING  3 DIF.+INTE. CARRIL-TABLERO
65. JOINT LOADS
66.  82 98        FY 97.00
67. LOAD COMB 4
68. 1 1.5 2 1.5 3 1.35
69. LOAD COMB 5
70. 1 1.35 2 -1.5 3 -1.35
71. PERFORM ANALYSIS
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P R O B L E M S T A T I S T I C S

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NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS =   127/  210/   37
ORIGINAL/FINAL BAND-WIDTH =   16/    9
TOTAL PRIMARY LOAD CASES  =    3, TOTAL DEGREES OF FREEDOM =   300
SIZE OF STIFFNESS MATRIX  =   7800 DOUBLE PREC. WORDS
TOTAL REQUIRED DISK SPACE =   12.47 MEGA-BYTES

++ PROCESSING ELEMENT STIFFNESS MATRIX.          15:16: 1
++ PROCESSING GLOBAL STIFFNESS MATRIX.           15:16: 1
++ PROCESSING TRIANGULAR FACTORIZATION.          15:16: 1
++ CALCULATING JOINT DISPLACEMENTS.              15:16: 1
++ CALCULATING MEMBER  FORCES.                   15:16: 2

 72. LOAD LIST 4 5
 73. PRINT MEMBER FORCES
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MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	4	16	0.00	-1.31	0.00	1.14	0.00	-0.80
		17	0.00	1.31	0.00	-1.14	0.00	-0.58
	5	16	0.00	-0.26	0.00	0.32	0.00	-0.13
		17	0.00	0.26	0.00	-0.32	0.00	-0.15
2	4	17	0.00	-0.46	0.00	1.13	0.00	-0.42
		18	0.00	0.46	0.00	-1.13	0.00	-0.06
	5	17	0.00	0.90	0.00	0.01	0.00	0.12
		18	0.00	-0.90	0.00	-0.01	0.00	0.82
3	4	18	0.00	-34.75	0.00	62.61	0.00	-16.25
		19	0.00	34.75	0.00	-62.61	0.00	-20.24
	5	18	0.00	30.66	0.00	-52.30	0.00	13.09
		19	0.00	-30.66	0.00	52.30	0.00	19.11
4	4	19	0.00	-59.40	0.00	61.57	0.00	-38.67
		20	0.00	59.40	0.00	-61.57	0.00	-23.71
	5	19	0.00	52.37	0.00	-54.33	0.00	32.93
		20	0.00	-52.37	0.00	54.33	0.00	22.06
5	4	20	0.00	-46.97	0.00	46.50	0.00	-29.79
		21	0.00	46.97	0.00	-46.50	0.00	-19.53
	5	20	0.00	42.86	0.00	-43.04	0.00	26.62
		21	0.00	-42.86	0.00	43.04	0.00	18.39
6	4	21	0.00	-36.29	0.00	34.42	0.00	-23.09
		22	0.00	36.29	0.00	-34.42	0.00	-15.01
	5	21	0.00	33.56	0.00	-32.82	0.00	21.30
		22	0.00	-33.56	0.00	32.82	0.00	13.95
7	4	22	0.00	-27.32	0.00	25.09	0.00	-17.43
		23	0.00	27.32	0.00	-25.09	0.00	-11.26
	5	22	0.00	24.72	0.00	-23.76	0.00	16.24
		23	0.00	-24.72	0.00	23.76	0.00	9.72
8	4	23	0.00	-20.42	0.00	18.24	0.00	-12.89
		24	0.00	20.42	0.00	-18.24	0.00	-8.55
	5	23	0.00	16.74	0.00	-15.83	0.00	11.61
		24	0.00	-16.74	0.00	15.83	0.00	5.97
9	4	24	0.00	-15.60	0.00	13.68	0.00	-9.53
		25	0.00	15.60	0.00	-13.68	0.00	-6.85
	5	24	0.00	9.80	0.00	-9.02	0.00	7.56
		25	0.00	-9.80	0.00	9.02	0.00	2.73
10	4	25	0.00	-12.63	0.00	11.12	0.00	-7.28
		26	0.00	12.63	0.00	-11.12	0.00	-5.98

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	25	0.00	3.89	0.00	-3.20	0.00	4.10
		26	0.00	-3.89	0.00	3.20	0.00	-0.01
11	4	26	0.00	-11.05	0.00	10.11	0.00	-5.96
		27	0.00	11.05	0.00	-10.11	0.00	-5.64
	5	26	0.00	-0.94	0.00	1.71	0.00	1.22
		27	0.00	0.94	0.00	-1.71	0.00	-2.20
12	4	27	0.00	-10.16	0.00	9.99	0.00	-5.31
		28	0.00	10.16	0.00	-9.99	0.00	-5.36
	5	27	0.00	-4.47	0.00	5.61	0.00	-1.09
		28	0.00	4.47	0.00	-5.61	0.00	-3.61
13	4	28	0.00	-8.81	0.00	9.66	0.00	-4.96
		29	0.00	8.81	0.00	-9.66	0.00	-4.30
	5	28	0.00	-6.03	0.00	7.86	0.00	-2.73
		29	0.00	6.03	0.00	-7.86	0.00	-3.61
14	4	29	0.00	-5.04	0.00	7.26	0.00	-4.37
		30	0.00	5.04	0.00	-7.26	0.00	-0.92
	5	29	0.00	-3.89	0.00	6.92	0.00	-3.42
		30	0.00	3.89	0.00	-6.92	0.00	-0.67
15	4	30	0.00	2.59	0.00	3.35	0.00	-3.13
		31	0.00	-2.59	0.00	-3.35	0.00	4.43
	5	30	0.00	2.96	0.00	3.35	0.00	-3.07
		31	0.00	-2.96	0.00	-3.35	0.00	4.55
16	4	32	0.00	-0.31	0.00	2.04	0.00	-0.27
		33	0.00	0.31	0.00	-2.04	0.00	-0.06
	5	32	0.00	0.59	0.00	0.18	0.00	0.22
		33	0.00	-0.59	0.00	-0.18	0.00	0.40
17	4	33	0.00	0.98	0.00	2.26	0.00	-0.36
		34	0.00	-0.98	0.00	-2.26	0.00	1.39
	5	33	0.00	3.47	0.00	-0.66	0.00	0.07
		34	0.00	-3.47	0.00	0.66	0.00	3.57
18	4	34	0.00	2.92	0.00	104.44	0.00	-8.54
		35	0.00	-2.92	0.00	-104.44	0.00	11.61
	5	34	0.00	2.03	0.00	-90.49	0.00	3.72
		35	0.00	-2.03	0.00	90.49	0.00	-1.59
19	4	35	0.00	-37.14	0.00	123.48	0.00	-48.04
		36	0.00	37.14	0.00	-123.48	0.00	9.04
	5	35	0.00	32.13	0.00	-110.73	0.00	36.96
		36	0.00	-32.13	0.00	110.73	0.00	-3.23
20	4	36	0.00	-40.94	0.00	105.05	0.00	-49.18
		37	0.00	40.94	0.00	-105.05	0.00	6.19

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	36	0.00	34.56	0.00	-96.77	0.00	40.63
		37	0.00	-34.56	0.00	96.77	0.00	-4.35
21	4	37	0.00	-35.67	0.00	82.29	0.00	-42.32
		38	0.00	35.67	0.00	-82.29	0.00	4.86
	5	37	0.00	29.55	0.00	-76.70	0.00	37.26
		38	0.00	-29.55	0.00	76.70	0.00	-6.23
22	4	38	0.00	-29.53	0.00	62.04	0.00	-34.11
		39	0.00	29.53	0.00	-62.04	0.00	3.10
	5	38	0.00	23.32	0.00	-56.54	0.00	32.01
		39	0.00	-23.32	0.00	56.54	0.00	-7.53
23	4	39	0.00	-23.85	0.00	46.27	0.00	-25.89
		40	0.00	23.85	0.00	-46.27	0.00	0.85
	5	39	0.00	16.93	0.00	-38.24	0.00	26.16
		40	0.00	-16.93	0.00	38.24	0.00	-8.39
24	4	40	0.00	-19.08	0.00	35.27	0.00	-18.51
		41	0.00	19.08	0.00	-35.27	0.00	-1.53
	5	40	0.00	11.00	0.00	-22.32	0.00	20.57
		41	0.00	-11.00	0.00	22.32	0.00	-9.02
25	4	41	0.00	-15.24	0.00	28.54	0.00	-12.41
		42	0.00	15.24	0.00	-28.54	0.00	-3.59
	5	41	0.00	6.02	0.00	-8.81	0.00	15.67
		42	0.00	-6.02	0.00	8.81	0.00	-9.34
26	4	42	0.00	-11.89	0.00	25.07	0.00	-7.83
		43	0.00	11.89	0.00	-25.07	0.00	-4.65
	5	42	0.00	2.49	0.00	2.29	0.00	11.51
		43	0.00	-2.49	0.00	-2.29	0.00	-8.90
27	4	43	0.00	-8.13	0.00	23.32	0.00	-4.92
		44	0.00	8.13	0.00	-23.32	0.00	-3.62
	5	43	0.00	1.14	0.00	10.58	0.00	7.82
		44	0.00	-1.14	0.00	-10.58	0.00	-6.62
28	4	44	0.00	-2.55	0.00	20.94	0.00	-4.18
		45	0.00	2.55	0.00	-20.94	0.00	1.51
	5	44	0.00	3.23	0.00	14.81	0.00	3.80
		45	0.00	-3.23	0.00	-14.81	0.00	-0.41
29	4	45	0.00	6.45	0.00	14.74	0.00	-6.98
		46	0.00	-6.45	0.00	-14.74	0.00	13.76
	5	45	0.00	10.32	0.00	12.60	0.00	-2.42
		46	0.00	-10.32	0.00	-12.60	0.00	13.25
30	4	46	0.00	20.60	0.00	6.13	0.00	-15.80
		47	0.00	-20.60	0.00	-6.13	0.00	26.10

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	46	0.00	23.62	0.00	5.57	0.00	-14.39
		47	0.00	-23.62	0.00	-5.57	0.00	26.20
31	4	48	0.00	0.65	0.00	1.89	0.00	0.42
		49	0.00	-0.65	0.00	-1.89	0.00	0.26
	5	48	0.00	1.32	0.00	-0.18	0.00	0.21
		49	0.00	-1.32	0.00	0.18	0.00	1.18
32	4	49	0.00	3.65	0.00	2.30	0.00	0.21
		50	0.00	-3.65	0.00	-2.30	0.00	3.62
	5	49	0.00	3.84	0.00	-1.16	0.00	-0.95
		50	0.00	-3.84	0.00	1.16	0.00	4.98
33	4	50	0.00	17.04	0.00	121.65	0.00	-8.27
		51	0.00	-17.04	0.00	-121.65	0.00	26.17
	5	50	0.00	-8.85	0.00	-109.80	0.00	0.69
		51	0.00	8.85	0.00	109.80	0.00	-9.98
34	4	51	0.00	6.86	0.00	145.95	0.00	-41.82
		52	0.00	-6.86	0.00	-145.95	0.00	49.03
	5	51	0.00	-8.00	0.00	-133.70	0.00	28.26
		52	0.00	8.00	0.00	133.70	0.00	-36.66
35	4	52	0.00	-7.15	0.00	127.48	0.00	-58.50
		53	0.00	7.15	0.00	-127.48	0.00	51.00
	5	52	0.00	1.58	0.00	-117.73	0.00	46.77
		53	0.00	-1.58	0.00	117.73	0.00	-45.11
36	4	53	0.00	-14.55	0.00	102.29	0.00	-58.54
		54	0.00	14.55	0.00	-102.29	0.00	43.26
	5	53	0.00	7.33	0.00	-94.08	0.00	51.70
		54	0.00	-7.33	0.00	94.08	0.00	-44.01
37	4	54	0.00	-16.64	0.00	78.73	0.00	-50.14
		55	0.00	16.64	0.00	-78.73	0.00	32.67
	5	54	0.00	8.97	0.00	-69.91	0.00	49.06
		55	0.00	-8.97	0.00	69.91	0.00	-39.64
38	4	55	0.00	-16.00	0.00	59.75	0.00	-38.76
		56	0.00	16.00	0.00	-59.75	0.00	21.96
	5	55	0.00	8.54	0.00	-47.74	0.00	43.50
		56	0.00	-8.54	0.00	47.74	0.00	-34.53
39	4	56	0.00	-13.90	0.00	46.03	0.00	-27.11
		57	0.00	13.90	0.00	-46.03	0.00	12.52
	5	56	0.00	7.41	0.00	-28.40	0.00	37.31
		57	0.00	-7.41	0.00	28.40	0.00	-29.53
40	4	57	0.00	-10.76	0.00	37.10	0.00	-16.69
		58	0.00	10.76	0.00	-37.10	0.00	5.39

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	57	0.00	6.55	0.00	-12.11	0.00	31.45
		58	0.00	-6.55	0.00	12.11	0.00	-24.57
41	4	58	0.00	-6.48	0.00	31.76	0.00	-8.50
		59	0.00	6.48	0.00	-31.76	0.00	1.69
	5	58	0.00	6.88	0.00	0.96	0.00	25.97
		59	0.00	-6.88	0.00	-0.96	0.00	-18.75
42	4	59	0.00	-0.46	0.00	28.18	0.00	-3.57
		60	0.00	0.46	0.00	-28.18	0.00	3.09
	5	59	0.00	9.44	0.00	10.24	0.00	20.10
		60	0.00	-9.44	0.00	-10.24	0.00	-10.18
43	4	60	0.00	8.41	0.00	23.87	0.00	-3.57
		61	0.00	-8.41	0.00	-23.87	0.00	12.41
	5	60	0.00	15.57	0.00	14.52	0.00	11.95
		61	0.00	-15.57	0.00	-14.52	0.00	4.40
44	4	61	0.00	21.43	0.00	15.84	0.00	-11.64
		62	0.00	-21.43	0.00	-15.84	0.00	34.14
	5	61	0.00	26.76	0.00	11.96	0.00	-2.15
		62	0.00	-26.76	0.00	-11.96	0.00	30.24
45	4	62	0.00	38.80	0.00	6.32	0.00	-33.26
		63	0.00	-38.80	0.00	-6.32	0.00	52.66
	5	62	0.00	42.98	0.00	5.11	0.00	-28.74
		63	0.00	-42.98	0.00	-5.11	0.00	50.22
46	4	64	0.00	0.83	0.00	1.22	0.00	0.64
		65	0.00	-0.83	0.00	-1.22	0.00	0.23
	5	64	0.00	1.90	0.00	-0.25	0.00	0.08
		65	0.00	-1.90	0.00	0.25	0.00	1.91
47	4	65	0.00	4.54	0.00	1.80	0.00	0.61
		66	0.00	-4.54	0.00	-1.80	0.00	4.15
	5	65	0.00	4.13	0.00	-1.21	0.00	-2.03
		66	0.00	-4.13	0.00	1.21	0.00	6.37
48	4	66	0.00	47.61	0.00	134.74	0.00	-5.23
		67	0.00	-47.61	0.00	-134.74	0.00	55.22
	5	66	0.00	-38.46	0.00	-126.32	0.00	-4.08
		67	0.00	38.46	0.00	126.32	0.00	-36.30
49	4	67	0.00	46.47	0.00	146.96	0.00	-44.88
		68	0.00	-46.47	0.00	-146.96	0.00	93.68
	5	67	0.00	-46.00	0.00	-137.37	0.00	29.88
		68	0.00	46.00	0.00	137.37	0.00	-78.18
50	4	68	0.00	20.88	0.00	121.83	0.00	-73.03
		69	0.00	-20.88	0.00	-121.83	0.00	94.96

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	68	0.00	-25.42	0.00	-113.10	0.00	60.01
		69	0.00	25.42	0.00	113.10	0.00	-86.70
51	4	69	0.00	4.93	0.00	96.95	0.00	-76.37
		70	0.00	-4.93	0.00	-96.95	0.00	81.55
	5	69	0.00	-12.00	0.00	-88.55	0.00	69.40
		70	0.00	12.00	0.00	88.55	0.00	-82.00
52	4	70	0.00	-3.80	0.00	75.12	0.00	-67.10
		71	0.00	3.80	0.00	-75.12	0.00	63.11
	5	70	0.00	-3.90	0.00	-65.59	0.00	68.24
		71	0.00	3.90	0.00	65.59	0.00	-72.34
53	4	71	0.00	-7.66	0.00	57.54	0.00	-52.42
		72	0.00	7.66	0.00	-57.54	0.00	44.38
	5	71	0.00	0.97	0.00	-44.94	0.00	62.46
		72	0.00	-0.97	0.00	44.94	0.00	-61.45
54	4	72	0.00	-8.06	0.00	44.59	0.00	-36.49
		73	0.00	8.06	0.00	-44.59	0.00	28.03
	5	72	0.00	4.15	0.00	-27.03	0.00	55.19
		73	0.00	-4.15	0.00	27.03	0.00	-50.84
55	4	73	0.00	-5.77	0.00	35.83	0.00	-21.90
		74	0.00	5.77	0.00	-35.83	0.00	15.83
	5	73	0.00	6.97	0.00	-12.08	0.00	47.76
		74	0.00	-6.97	0.00	12.08	0.00	-40.45
56	4	74	0.00	-1.07	0.00	30.11	0.00	-10.53
		75	0.00	1.07	0.00	-30.11	0.00	9.42
	5	74	0.00	10.57	0.00	-0.35	0.00	40.12
		75	0.00	-10.57	0.00	0.35	0.00	-29.03
57	4	75	0.00	6.29	0.00	25.78	0.00	-4.27
		76	0.00	-6.29	0.00	-25.78	0.00	10.88
	5	75	0.00	16.08	0.00	7.63	0.00	31.03
		76	0.00	-16.08	0.00	-7.63	0.00	-14.14
58	4	76	0.00	17.05	0.00	20.76	0.00	-5.60
		77	0.00	-17.05	0.00	-20.76	0.00	23.50
	5	76	0.00	24.77	0.00	10.94	0.00	17.90
		77	0.00	-24.77	0.00	-10.94	0.00	8.11
59	4	77	0.00	32.46	0.00	12.99	0.00	-18.49
		78	0.00	-32.46	0.00	-12.99	0.00	52.57
	5	77	0.00	38.13	0.00	8.69	0.00	-3.70
		78	0.00	-38.13	0.00	-8.69	0.00	43.73
60	4	78	0.00	51.78	0.00	5.02	0.00	-49.93
		79	0.00	-51.78	0.00	-5.02	0.00	75.82

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	78	0.00	55.48	0.00	3.61	0.00	-41.22
		79	0.00	-55.48	0.00	-3.61	0.00	68.96
61	4	80	0.00	0.70	0.00	0.65	0.00	0.47
		81	0.00	-0.70	0.00	-0.65	0.00	0.26
	5	80	0.00	2.19	0.00	-0.29	0.00	0.04
		81	0.00	-2.19	0.00	0.29	0.00	2.26
62	4	81	0.00	1.77	0.00	1.12	0.00	0.09
		82	0.00	-1.77	0.00	-1.12	0.00	1.77
	5	81	0.00	6.77	0.00	-0.99	0.00	-2.12
		82	0.00	-6.77	0.00	0.99	0.00	9.23
63	4	82	0.00	151.98	0.00	100.83	0.00	19.43
		83	0.00	-151.98	0.00	-100.83	0.00	140.15
	5	82	0.00	-142.83	0.00	-96.16	0.00	-29.27
		83	0.00	142.83	0.00	96.16	0.00	-120.70
64	4	83	0.00	65.71	0.00	108.36	0.00	-70.26
		84	0.00	-65.71	0.00	-108.36	0.00	139.26
	5	83	0.00	-64.53	0.00	-102.34	0.00	54.98
		84	0.00	64.53	0.00	102.34	0.00	-122.73
65	4	84	0.00	39.22	0.00	88.40	0.00	-90.33
		85	0.00	-39.22	0.00	-88.40	0.00	131.51
	5	84	0.00	-42.95	0.00	-82.35	0.00	77.24
		85	0.00	42.95	0.00	82.35	0.00	-122.33
66	4	85	0.00	19.14	0.00	69.66	0.00	-92.31
		86	0.00	-19.14	0.00	-69.66	0.00	112.41
	5	85	0.00	-25.63	0.00	-63.36	0.00	86.10
		86	0.00	25.63	0.00	63.36	0.00	-113.01
67	4	86	0.00	5.84	0.00	53.89	0.00	-81.48
		87	0.00	-5.84	0.00	-53.89	0.00	87.62
	5	86	0.00	-12.95	0.00	-46.53	0.00	85.04
		87	0.00	12.95	0.00	46.53	0.00	-98.63
68	4	87	0.00	-1.20	0.00	41.41	0.00	-63.91
		88	0.00	1.20	0.00	-41.41	0.00	62.65
	5	87	0.00	-4.29	0.00	-31.81	0.00	78.57
		88	0.00	4.29	0.00	31.81	0.00	-83.07
69	4	88	0.00	-3.40	0.00	32.19	0.00	-44.51
		89	0.00	3.40	0.00	-32.19	0.00	40.94
	5	88	0.00	2.02	0.00	-19.19	0.00	70.08
		89	0.00	-2.02	0.00	19.19	0.00	-67.97
70	4	89	0.00	-1.79	0.00	25.82	0.00	-26.69
		90	0.00	1.79	0.00	-25.82	0.00	24.81

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	89	0.00	7.49	0.00	-8.75	0.00	61.03
		90	0.00	-7.49	0.00	8.75	0.00	-53.17
71	4	90	0.00	3.13	0.00	21.46	0.00	-13.04
		91	0.00	-3.13	0.00	-21.46	0.00	16.32
	5	90	0.00	13.38	0.00	-0.69	0.00	51.20
		91	0.00	-13.38	0.00	0.69	0.00	-37.15
72	4	91	0.00	11.17	0.00	17.90	0.00	-6.13
		92	0.00	-11.17	0.00	-17.90	0.00	17.86
	5	91	0.00	20.74	0.00	4.57	0.00	38.94
		92	0.00	-20.74	0.00	-4.57	0.00	-17.16
73	4	92	0.00	22.48	0.00	13.71	0.00	-8.99
		93	0.00	-22.48	0.00	-13.71	0.00	32.60
	5	92	0.00	30.48	0.00	6.44	0.00	21.26
		93	0.00	-30.48	0.00	-6.44	0.00	10.74
74	4	93	0.00	37.94	0.00	7.83	0.00	-25.58
		94	0.00	-37.94	0.00	-7.83	0.00	65.42
	5	93	0.00	43.75	0.00	4.67	0.00	-6.11
		94	0.00	-43.75	0.00	-4.67	0.00	52.04
75	4	94	0.00	58.14	0.00	2.82	0.00	-62.01
		95	0.00	-58.14	0.00	-2.82	0.00	91.08
	5	94	0.00	61.27	0.00	1.81	0.00	-49.44
		95	0.00	-61.27	0.00	-1.81	0.00	80.08
76	4	96	0.00	0.43	0.00	0.28	0.00	0.35
		97	0.00	-0.43	0.00	-0.28	0.00	0.10
	5	96	0.00	2.50	0.00	-0.22	0.00	-0.11
		97	0.00	-2.50	0.00	0.22	0.00	2.74
77	4	97	0.00	1.42	0.00	0.42	0.00	0.20
		98	0.00	-1.42	0.00	-0.42	0.00	1.29
	5	97	0.00	5.85	0.00	-0.55	0.00	-2.95
		98	0.00	-5.85	0.00	0.55	0.00	9.09
78	4	98	0.00	147.25	0.00	23.58	0.00	15.23
		99	0.00	-147.25	0.00	-23.58	0.00	139.38
	5	98	0.00	-139.08	0.00	-22.34	0.00	-24.94
		99	0.00	139.08	0.00	22.34	0.00	-121.09
79	4	99	0.00	75.06	0.00	36.43	0.00	-77.18
		100	0.00	-75.06	0.00	-36.43	0.00	156.00
	5	99	0.00	-74.11	0.00	-34.36	0.00	61.95
		100	0.00	74.11	0.00	34.36	0.00	-139.77
80	4	100	0.00	39.29	0.00	32.53	0.00	-106.23
		101	0.00	-39.29	0.00	-32.53	0.00	147.48

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	100	0.00	-43.27	0.00	-30.29	0.00	93.05
		101	0.00	43.27	0.00	30.29	0.00	-138.49
81	4	101	0.00	16.40	0.00	25.74	0.00	-107.82
		102	0.00	-16.40	0.00	-25.74	0.00	125.04
	5	101	0.00	-23.26	0.00	-23.32	0.00	101.88
		102	0.00	23.26	0.00	23.32	0.00	-126.31
82	4	102	0.00	3.02	0.00	19.85	0.00	-94.28
		103	0.00	-3.02	0.00	-19.85	0.00	97.45
	5	102	0.00	-10.60	0.00	-16.99	0.00	98.89
		103	0.00	10.60	0.00	16.99	0.00	-110.01
83	4	103	0.00	-3.77	0.00	15.25	0.00	-73.85
		104	0.00	3.77	0.00	-15.25	0.00	69.89
	5	103	0.00	-2.17	0.00	-11.56	0.00	90.56
		104	0.00	2.17	0.00	11.56	0.00	-92.84
84	4	104	0.00	-5.55	0.00	11.87	0.00	-51.73
		105	0.00	5.55	0.00	-11.87	0.00	45.90
	5	104	0.00	3.95	0.00	-6.94	0.00	80.27
		105	0.00	-3.95	0.00	6.94	0.00	-76.13
85	4	105	0.00	-3.32	0.00	9.53	0.00	-31.58
		106	0.00	3.32	0.00	-9.53	0.00	28.09
	5	105	0.00	9.32	0.00	-3.14	0.00	69.39
		106	0.00	-9.32	0.00	3.14	0.00	-59.60
86	4	106	0.00	2.38	0.00	7.89	0.00	-16.36
		107	0.00	-2.38	0.00	-7.89	0.00	18.86
	5	106	0.00	15.27	0.00	-0.23	0.00	57.54
		107	0.00	-15.27	0.00	0.23	0.00	-41.51
87	4	107	0.00	11.32	0.00	6.50	0.00	-8.95
		108	0.00	-11.32	0.00	-6.50	0.00	20.84
	5	107	0.00	22.81	0.00	1.60	0.00	42.87
		108	0.00	-22.81	0.00	-1.60	0.00	-18.92
88	4	108	0.00	23.31	0.00	4.77	0.00	-12.74
		109	0.00	-23.31	0.00	-4.77	0.00	37.21
	5	108	0.00	32.55	0.00	2.12	0.00	22.12
		109	0.00	-32.55	0.00	-2.12	0.00	12.06
89	4	109	0.00	37.50	0.00	2.29	0.00	-31.69
		110	0.00	-37.50	0.00	-2.29	0.00	71.06
	5	109	0.00	44.20	0.00	1.21	0.00	-8.95
		110	0.00	-44.20	0.00	-1.21	0.00	55.36
90	4	110	0.00	52.06	0.00	0.28	0.00	-69.14
		111	0.00	-52.06	0.00	-0.28	0.00	95.17

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	110	0.00	56.68	0.00	0.03	0.00	-54.09
		111	0.00	-56.68	0.00	-0.03	0.00	82.43
91	4	112	0.00	0.12	0.00	0.00	0.00	0.15
		113	0.00	-0.12	0.00	0.00	0.00	-0.02
	5	112	0.00	1.35	0.00	0.00	0.00	-0.06
		113	0.00	-1.35	0.00	0.00	0.00	1.47
92	4	113	0.00	1.05	0.00	0.00	0.00	0.24
		114	0.00	-1.05	0.00	0.00	0.00	0.87
	5	113	0.00	2.38	0.00	0.00	0.00	-1.72
		114	0.00	-2.38	0.00	0.00	0.00	4.21
93	4	114	0.00	55.13	0.00	0.00	0.00	0.83
		115	0.00	-55.13	0.00	0.00	0.00	57.06
	5	114	0.00	-51.50	0.00	0.00	0.00	-5.79
		115	0.00	51.50	0.00	0.00	0.00	-48.29
94	4	115	0.00	35.60	0.00	0.00	0.00	-39.06
		116	0.00	-35.60	0.00	0.00	0.00	76.44
	5	115	0.00	-35.39	0.00	0.00	0.00	31.34
		116	0.00	35.39	0.00	0.00	0.00	-68.51
95	4	116	0.00	15.36	0.00	0.00	0.00	-56.50
		117	0.00	-15.36	0.00	0.00	0.00	72.62
	5	116	0.00	-17.63	0.00	0.00	0.00	49.78
		117	0.00	17.63	0.00	0.00	0.00	-68.29
96	4	117	0.00	4.78	0.00	0.00	0.00	-56.71
		118	0.00	-4.78	0.00	0.00	0.00	61.73
	5	117	0.00	-8.51	0.00	0.00	0.00	53.63
		118	0.00	8.51	0.00	0.00	0.00	-62.56
97	4	118	0.00	-1.20	0.00	0.00	0.00	-49.37
		119	0.00	1.20	0.00	0.00	0.00	48.12
	5	118	0.00	-2.93	0.00	0.00	0.00	51.59
		119	0.00	2.93	0.00	0.00	0.00	-54.67
98	4	119	0.00	-3.98	0.00	0.00	0.00	-38.64
		120	0.00	3.98	0.00	0.00	0.00	34.46
	5	119	0.00	0.57	0.00	0.00	0.00	46.92
		120	0.00	-0.57	0.00	0.00	0.00	-46.33
99	4	120	0.00	-4.41	0.00	0.00	0.00	-27.16
		121	0.00	4.41	0.00	0.00	0.00	22.53
	5	120	0.00	3.01	0.00	0.00	0.00	41.33
		121	0.00	-3.01	0.00	0.00	0.00	-38.17
100	4	121	0.00	-2.96	0.00	0.00	0.00	-16.77
		122	0.00	2.96	0.00	0.00	0.00	13.66

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	121	0.00	5.19	0.00	0.00	0.00	35.50
		122	0.00	-5.19	0.00	0.00	0.00	-30.04
101	4	122	0.00	0.14	0.00	0.00	0.00	-8.95
		123	0.00	-0.14	0.00	0.00	0.00	9.09
	5	122	0.00	7.78	0.00	0.00	0.00	29.22
		123	0.00	-7.78	0.00	0.00	0.00	-21.06
102	4	123	0.00	4.82	0.00	0.00	0.00	-5.14
		124	0.00	-4.82	0.00	0.00	0.00	10.20
	5	123	0.00	11.30	0.00	0.00	0.00	21.57
		124	0.00	-11.30	0.00	0.00	0.00	-9.71
103	4	124	0.00	11.02	0.00	0.00	0.00	-7.02
		125	0.00	-11.02	0.00	0.00	0.00	18.59
	5	124	0.00	16.05	0.00	0.00	0.00	10.92
		125	0.00	-16.05	0.00	0.00	0.00	5.94
104	4	125	0.00	18.33	0.00	0.00	0.00	-16.52
		126	0.00	-18.33	0.00	0.00	0.00	35.77
	5	125	0.00	21.88	0.00	0.00	0.00	-4.84
		126	0.00	-21.88	0.00	0.00	0.00	27.81
105	4	126	0.00	24.07	0.00	0.00	0.00	-35.32
		127	0.00	-24.07	0.00	0.00	0.00	47.36
	5	126	0.00	26.61	0.00	0.00	0.00	-27.60
		127	0.00	-26.61	0.00	0.00	0.00	40.91
107	4	16	0.00	-8.91	0.00	-1.76	0.00	-10.75
		32	0.00	6.85	0.00	1.76	0.00	2.55
	5	16	0.00	-0.34	0.00	-0.37	0.00	3.89
		32	0.00	-1.51	0.00	0.37	0.00	-3.28
108	4	32	0.00	-6.54	0.00	-2.03	0.00	-4.59
		48	0.00	4.48	0.00	2.03	0.00	-1.14
	5	32	0.00	0.93	0.00	-0.16	0.00	3.11
		48	0.00	-2.78	0.00	0.16	0.00	-1.18
109	4	48	0.00	-5.14	0.00	-1.60	0.00	-0.75
		64	0.00	3.08	0.00	1.60	0.00	-3.52
	5	48	0.00	1.46	0.00	0.05	0.00	1.36
		64	0.00	-3.31	0.00	-0.05	0.00	1.12
110	4	64	0.00	-3.90	0.00	-0.97	0.00	2.31
		80	0.00	1.84	0.00	0.97	0.00	-5.29
	5	64	0.00	1.41	0.00	0.13	0.00	-0.87
		80	0.00	-3.26	0.00	-0.13	0.00	3.29
111	4	80	0.00	-2.54	0.00	-0.50	0.00	4.65
		96	0.00	0.48	0.00	0.50	0.00	-6.22

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	80	0.00	1.07	0.00	0.17	0.00	-3.01
		96	0.00	-2.92	0.00	-0.17	0.00	5.08
112	4	96	0.00	-0.91	0.00	-0.15	0.00	5.94
		112	0.00	-0.12	0.00	0.15	0.00	-6.14
	5	96	0.00	0.42	0.00	0.06	0.00	-4.86
		112	0.00	-1.35	0.00	-0.06	0.00	5.32
114	4	17	0.00	-6.27	0.00	-1.77	0.00	-8.14
		33	0.00	3.13	0.00	1.77	0.00	3.25
	5	17	0.00	1.05	0.00	-0.28	0.00	4.61
		33	0.00	-3.87	0.00	0.28	0.00	-2.05
115	4	33	0.00	-4.43	0.00	-2.19	0.00	-3.47
		49	0.00	1.29	0.00	2.19	0.00	0.50
	5	33	0.00	0.99	0.00	0.19	0.00	2.89
		49	0.00	-3.82	0.00	-0.19	0.00	-0.39
116	4	49	0.00	-4.28	0.00	-1.72	0.00	-0.91
		65	0.00	1.14	0.00	1.72	0.00	-1.91
	5	49	0.00	1.30	0.00	0.43	0.00	1.37
		65	0.00	-4.13	0.00	-0.43	0.00	1.45
117	4	65	0.00	-4.85	0.00	-0.88	0.00	1.33
		81	0.00	1.71	0.00	0.88	0.00	-4.75
	5	65	0.00	1.89	0.00	0.31	0.00	-0.49
		81	0.00	-4.72	0.00	-0.31	0.00	3.93
118	4	81	0.00	-2.79	0.00	-0.52	0.00	4.28
		97	0.00	-0.35	0.00	0.52	0.00	-5.54
	5	81	0.00	0.14	0.00	0.45	0.00	-3.23
		97	0.00	-2.97	0.00	-0.45	0.00	4.85
119	4	97	0.00	-0.63	0.00	-0.22	0.00	5.40
		113	0.00	-0.94	0.00	0.22	0.00	-5.32
	5	97	0.00	-0.39	0.00	0.24	0.00	-4.52
		113	0.00	-1.03	0.00	-0.24	0.00	4.69
121	4	18	0.00	-155.60	0.00	-26.54	0.00	-174.93
		34	0.00	151.38	0.00	26.54	0.00	15.30
	5	18	0.00	114.87	0.00	22.21	0.00	124.96
		34	0.00	-118.67	0.00	-22.21	0.00	-3.52
122	4	34	0.00	-153.31	0.00	-33.69	0.00	-117.48
		50	0.00	149.09	0.00	33.69	0.00	-39.77
	5	34	0.00	120.11	0.00	29.50	0.00	93.35
		50	0.00	-123.91	0.00	-29.50	0.00	33.55
123	4	50	0.00	-162.49	0.00	-38.34	0.00	-79.57
		66	0.00	158.26	0.00	38.34	0.00	-87.22

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	50	0.00	136.60	0.00	35.18	0.00	75.09
		66	0.00	-140.40	0.00	-35.18	0.00	68.95
124	4	66	0.00	-201.33	0.00	-39.42	0.00	-45.73
		82	0.00	197.11	0.00	39.42	0.00	-161.46
	5	66	0.00	182.99	0.00	37.47	0.00	56.16
		82	0.00	-186.79	0.00	-37.47	0.00	136.12
125	4	82	0.00	-76.87	0.00	-18.22	0.00	61.75
		98	0.00	72.65	0.00	18.22	0.00	-139.50
	5	82	0.00	65.94	0.00	17.43	0.00	-40.95
		98	0.00	-69.74	0.00	-17.43	0.00	111.51
126	4	98	0.00	51.97	0.00	-1.70	0.00	116.35
		114	0.00	-54.08	0.00	1.70	0.00	-88.77
	5	98	0.00	-55.78	0.00	1.58	0.00	-89.72
		114	0.00	53.88	0.00	-1.58	0.00	61.21
128	4	19	0.00	-258.52	0.00	-108.34	0.00	-509.43
		35	0.00	253.22	0.00	108.34	0.00	243.33
	5	19	0.00	156.53	0.00	94.58	0.00	327.05
		35	0.00	-161.30	0.00	-94.58	0.00	-161.78
129	4	35	0.00	-213.17	0.00	-144.77	0.00	-262.37
		51	0.00	207.86	0.00	144.77	0.00	43.43
	5	35	0.00	131.21	0.00	129.95	0.00	182.01
		51	0.00	-135.98	0.00	-129.95	0.00	-43.08
130	4	51	0.00	-197.68	0.00	-160.42	0.00	-67.74
		67	0.00	192.38	0.00	160.42	0.00	-135.10
	5	51	0.00	135.13	0.00	148.23	0.00	66.98
		67	0.00	-139.90	0.00	-148.23	0.00	76.03
131	4	67	0.00	-191.25	0.00	-150.08	0.00	122.88
		83	0.00	185.95	0.00	150.08	0.00	-319.03
	5	67	0.00	147.45	0.00	141.81	0.00	-64.99
		83	0.00	-152.22	0.00	-141.81	0.00	220.81
132	4	83	0.00	-99.69	0.00	-80.19	0.00	311.49
		99	0.00	94.39	0.00	80.19	0.00	-412.41
	5	83	0.00	73.92	0.00	76.08	0.00	-214.63
		99	0.00	-78.69	0.00	-76.08	0.00	293.99
133	4	99	0.00	-22.19	0.00	-18.00	0.00	399.57
		115	0.00	19.53	0.00	18.00	0.00	-410.41
	5	99	0.00	13.73	0.00	16.94	0.00	-281.97
		115	0.00	-16.12	0.00	-16.94	0.00	289.73
135	4	20	0.00	-161.01	0.00	-89.67	0.00	-385.98
		36	0.00	154.63	0.00	89.67	0.00	221.84

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	20	0.00	71.17	0.00	81.59	0.00	216.72
		36	0.00	-76.92	0.00	-81.59	0.00	-139.72
136	4	36	0.00	-150.83	0.00	-129.81	0.00	-203.41
		52	0.00	144.45	0.00	129.81	0.00	49.87
	5	36	0.00	74.49	0.00	119.00	0.00	125.76
		52	0.00	-80.23	0.00	-119.00	0.00	-45.30
137	4	52	0.00	-130.44	0.00	-139.28	0.00	-31.40
		68	0.00	124.06	0.00	139.28	0.00	-100.94
	5	52	0.00	70.66	0.00	129.11	0.00	29.33
		68	0.00	-76.40	0.00	-129.11	0.00	47.14
138	4	68	0.00	-98.46	0.00	-118.64	0.00	126.07
		84	0.00	92.08	0.00	118.64	0.00	-225.15
	5	68	0.00	55.81	0.00	110.94	0.00	-71.41
		84	0.00	-61.56	0.00	-110.94	0.00	132.44
139	4	84	0.00	-65.58	0.00	-69.71	0.00	245.10
		100	0.00	59.20	0.00	69.71	0.00	-309.99
	5	84	0.00	39.97	0.00	65.44	0.00	-152.43
		100	0.00	-45.72	0.00	-65.44	0.00	196.99
140	4	100	0.00	-23.43	0.00	-19.94	0.00	313.88
		116	0.00	20.24	0.00	19.94	0.00	-325.24
	5	100	0.00	14.85	0.00	18.73	0.00	-201.07
		116	0.00	-17.73	0.00	-18.73	0.00	209.55
142	4	21	0.00	-112.69	0.00	-69.69	0.00	-292.03
		37	0.00	105.22	0.00	69.69	0.00	178.71
	5	21	0.00	23.67	0.00	65.30	0.00	129.21
		37	0.00	-30.38	0.00	-65.30	0.00	-101.10
143	4	37	0.00	-110.49	0.00	-105.82	0.00	-155.96
		53	0.00	103.03	0.00	105.82	0.00	44.92
	5	37	0.00	35.40	0.00	98.21	0.00	81.03
		53	0.00	-42.11	0.00	-98.21	0.00	-40.73
144	4	53	0.00	-95.62	0.00	-113.36	0.00	-19.73
		69	0.00	88.16	0.00	113.36	0.00	-75.84
	5	53	0.00	36.36	0.00	104.81	0.00	17.08
		69	0.00	-43.08	0.00	-104.81	0.00	24.23
145	4	69	0.00	-72.21	0.00	-94.77	0.00	100.72
		85	0.00	64.74	0.00	94.77	0.00	-171.93
	5	69	0.00	29.66	0.00	87.51	0.00	-48.78
		85	0.00	-36.38	0.00	-87.51	0.00	83.12
146	4	85	0.00	-44.66	0.00	-55.58	0.00	190.68
		101	0.00	37.20	0.00	55.58	0.00	-233.25

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	85	0.00	19.06	0.00	51.27	0.00	-102.11
		101	0.00	-25.78	0.00	-51.27	0.00	125.43
147	4	101	0.00	-14.31	0.00	-15.92	0.00	240.03
		117	0.00	10.58	0.00	15.92	0.00	-246.51
	5	101	0.00	5.78	0.00	14.66	0.00	-132.39
		117	0.00	-9.14	0.00	-14.66	0.00	136.27
149	4	22	0.00	-84.33	0.00	-52.36	0.00	-220.98
		38	0.00	75.78	0.00	52.36	0.00	137.72
	5	22	0.00	-7.87	0.00	49.29	0.00	61.54
		38	0.00	0.18	0.00	-49.29	0.00	-65.73
150	4	38	0.00	-81.92	0.00	-81.61	0.00	-117.47
		54	0.00	73.38	0.00	81.61	0.00	36.71
	5	38	0.00	6.05	0.00	75.07	0.00	45.57
		54	0.00	-13.74	0.00	-75.07	0.00	-35.28
151	4	54	0.00	-71.29	0.00	-88.49	0.00	-13.15
		70	0.00	62.74	0.00	88.49	0.00	-56.55
	5	54	0.00	12.10	0.00	80.12	0.00	11.11
		70	0.00	-19.79	0.00	-80.12	0.00	5.47
152	4	70	0.00	-54.01	0.00	-74.03	0.00	78.38
		86	0.00	45.47	0.00	74.03	0.00	-130.11
	5	70	0.00	11.69	0.00	66.36	0.00	-28.43
		86	0.00	-19.38	0.00	-66.36	0.00	44.60
153	4	86	0.00	-32.17	0.00	-43.11	0.00	145.88
		102	0.00	23.63	0.00	43.11	0.00	-174.90
	5	86	0.00	6.70	0.00	38.39	0.00	-61.43
		102	0.00	-14.39	0.00	-38.39	0.00	72.40
154	4	102	0.00	-10.26	0.00	-12.35	0.00	180.78
		118	0.00	5.99	0.00	12.35	0.00	-185.01
	5	102	0.00	1.73	0.00	10.96	0.00	-78.73
		118	0.00	-5.57	0.00	-10.96	0.00	80.62
156	4	23	0.00	-67.11	0.00	-38.60	0.00	-168.52
		39	0.00	57.49	0.00	38.60	0.00	103.73
	5	23	0.00	-29.02	0.00	34.65	0.00	12.29
		39	0.00	20.35	0.00	-34.65	0.00	-37.96
157	4	39	0.00	-63.17	0.00	-61.40	0.00	-87.96
		55	0.00	53.54	0.00	61.40	0.00	27.28
	5	39	0.00	-13.96	0.00	53.28	0.00	19.67
		55	0.00	5.30	0.00	-53.28	0.00	-29.68
158	4	55	0.00	-54.17	0.00	-67.48	0.00	-8.30
		71	0.00	44.55	0.00	67.48	0.00	-43.04

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	55	0.00	-4.87	0.00	57.14	0.00	7.52
		71	0.00	-3.79	0.00	-57.14	0.00	-8.08
159	4	71	0.00	-40.68	0.00	-56.79	0.00	60.62
		87	0.00	31.06	0.00	56.79	0.00	-97.92
	5	71	0.00	-1.08	0.00	47.26	0.00	-12.57
		87	0.00	-7.59	0.00	-47.26	0.00	15.95
160	4	87	0.00	-24.02	0.00	-33.08	0.00	110.41
		103	0.00	14.39	0.00	33.08	0.00	-130.38
	5	87	0.00	-1.07	0.00	27.20	0.00	-30.68
		103	0.00	-7.60	0.00	-27.20	0.00	34.07
161	4	103	0.00	-7.60	0.00	-9.48	0.00	134.98
		119	0.00	2.78	0.00	9.48	0.00	-137.68
	5	103	0.00	-0.83	0.00	7.75	0.00	-39.51
		119	0.00	-3.50	0.00	-7.75	0.00	40.20
163	4	24	0.00	-56.83	0.00	-28.68	0.00	-130.13
		40	0.00	46.12	0.00	28.68	0.00	76.60
	5	24	0.00	-42.01	0.00	21.84	0.00	-20.56
		40	0.00	32.38	0.00	-21.84	0.00	-18.12
164	4	40	0.00	-50.89	0.00	-46.34	0.00	-65.60
		56	0.00	40.18	0.00	46.34	0.00	18.24
	5	40	0.00	-26.45	0.00	34.02	0.00	2.20
		56	0.00	16.81	0.00	-34.02	0.00	-24.70
165	4	56	0.00	-42.29	0.00	-51.49	0.00	-4.52
		72	0.00	31.58	0.00	51.49	0.00	-33.89
	5	56	0.00	-15.68	0.00	36.80	0.00	5.36
		72	0.00	6.04	0.00	-36.80	0.00	-16.65
166	4	72	0.00	-31.19	0.00	-43.60	0.00	46.84
		88	0.00	20.48	0.00	43.60	0.00	-73.70
	5	72	0.00	-9.23	0.00	30.55	0.00	-1.25
		88	0.00	-0.41	0.00	-30.55	0.00	-3.34
167	4	88	0.00	-18.27	0.00	-25.47	0.00	82.92
		104	0.00	7.56	0.00	25.47	0.00	-96.35
	5	88	0.00	-5.90	0.00	17.56	0.00	-9.28
		104	0.00	-3.74	0.00	-17.56	0.00	8.16
168	4	104	0.00	-5.78	0.00	-7.30	0.00	99.74
		120	0.00	0.42	0.00	7.30	0.00	-101.35
	5	104	0.00	-2.37	0.00	4.89	0.00	-12.77
		120	0.00	-2.45	0.00	-4.99	0.00	12.79
170	4	25	0.00	-50.27	0.00	-22.35	0.00	-101.23
		41	0.00	38.48	0.00	22.35	0.00	55.08

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	25	0.00	-48.35	0.00	10.86	0.00	-39.29
		41	0.00	37.74	0.00	-10.86	0.00	-5.48
171	4	41	0.00	-42.33	0.00	-36.29	0.00	-48.35
		57	0.00	30.54	0.00	36.29	0.00	10.46
	5	41	0.00	-32.76	0.00	17.51	0.00	-8.04
		57	0.00	22.15	0.00	-17.51	0.00	-20.52
172	4	57	0.00	-33.68	0.00	-40.46	0.00	-1.53
		73	0.00	21.89	0.00	40.46	0.00	-27.37
	5	57	0.00	-21.29	0.00	19.43	0.00	4.22
		73	0.00	10.68	0.00	-19.43	0.00	-20.84
173	4	73	0.00	-24.17	0.00	-34.33	0.00	36.13
		89	0.00	12.38	0.00	34.33	0.00	-55.14
	5	73	0.00	-13.50	0.00	16.36	0.00	5.89
		89	0.00	2.89	0.00	-16.36	0.00	-14.41
174	4	89	0.00	-14.00	0.00	-20.07	0.00	61.51
		105	0.00	2.21	0.00	20.07	0.00	-69.94
	5	89	0.00	-8.36	0.00	9.42	0.00	3.97
		105	0.00	-2.25	0.00	-9.42	0.00	-7.14
175	4	105	0.00	-4.44	0.00	-5.76	0.00	72.29
		121	0.00	-1.45	0.00	5.76	0.00	-73.07
	5	105	0.00	-3.12	0.00	2.68	0.00	3.34
		121	0.00	-2.18	0.00	-2.68	0.00	-3.59
177	4	26	0.00	-44.74	0.00	-19.01	0.00	-77.74
		42	0.00	31.87	0.00	19.01	0.00	37.91
	5	26	0.00	-48.89	0.00	1.60	0.00	-45.98
		42	0.00	37.31	0.00	-1.60	0.00	1.15
178	4	42	0.00	-35.22	0.00	-30.42	0.00	-34.44
		58	0.00	22.35	0.00	30.42	0.00	4.50
	5	42	0.00	-33.77	0.00	3.77	0.00	-12.26
		58	0.00	22.19	0.00	-3.77	0.00	-16.84
179	4	58	0.00	-26.63	0.00	-33.52	0.00	0.84
		74	0.00	13.76	0.00	33.52	0.00	-21.84
	5	58	0.00	-22.52	0.00	5.17	0.00	3.77
		74	0.00	10.93	0.00	-5.17	0.00	-21.17
180	4	74	0.00	-18.46	0.00	-28.22	0.00	27.55
		90	0.00	5.59	0.00	28.22	0.00	-40.06
	5	74	0.00	-14.53	0.00	4.84	0.00	9.43
		90	0.00	2.95	0.00	-4.84	0.00	-18.52
181	4	90	0.00	-10.51	0.00	-16.45	0.00	44.42
		106	0.00	-2.36	0.00	16.45	0.00	-48.66

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	90	0.00	-8.84	0.00	2.87	0.00	10.46
		106	0.00	-2.74	0.00	-2.87	0.00	-13.63
182	4	106	0.00	-3.34	0.00	-4.71	0.00	50.29
		122	0.00	-3.10	0.00	4.71	0.00	-50.35
	5	106	0.00	-3.20	0.00	0.82	0.00	10.73
		122	0.00	-2.59	0.00	-0.82	0.00	-10.89
184	4	27	0.00	-37.93	0.00	-17.74	0.00	-56.48
		43	0.00	23.98	0.00	17.74	0.00	24.28
	5	27	0.00	-43.91	0.00	-5.93	0.00	-42.54
		43	0.00	31.35	0.00	5.93	0.00	3.40
185	4	43	0.00	-27.74	0.00	-27.31	0.00	-22.53
		59	0.00	13.79	0.00	27.31	0.00	0.94
	5	43	0.00	-30.01	0.00	-7.01	0.00	-11.69
		59	0.00	17.45	0.00	7.01	0.00	-12.99
186	4	59	0.00	-19.81	0.00	-29.20	0.00	2.64
		75	0.00	5.86	0.00	29.20	0.00	-15.99
	5	59	0.00	-20.01	0.00	-5.66	0.00	3.71
		75	0.00	7.46	0.00	5.66	0.00	-17.99
187	4	75	0.00	-13.22	0.00	-24.05	0.00	20.32
		91	0.00	-0.73	0.00	24.05	0.00	-26.82
	5	75	0.00	-12.97	0.00	-3.67	0.00	10.02
		91	0.00	0.41	0.00	3.67	0.00	-16.97
188	4	91	0.00	-7.31	0.00	-13.86	0.00	30.37
		107	0.00	-6.64	0.00	13.86	0.00	-30.72
	5	91	0.00	-7.78	0.00	-1.88	0.00	11.72
		107	0.00	-4.78	0.00	1.88	0.00	-13.27
189	4	107	0.00	-2.30	0.00	-3.95	0.00	32.11
		123	0.00	-4.68	0.00	3.95	0.00	-31.49
	5	107	0.00	-2.76	0.00	-0.52	0.00	11.43
		123	0.00	-3.52	0.00	0.52	0.00	-11.24
191	4	28	0.00	-27.97	0.00	-17.14	0.00	-35.49
		44	0.00	12.93	0.00	17.14	0.00	14.22
	5	28	0.00	-33.26	0.00	-11.21	0.00	-30.99
		44	0.00	19.73	0.00	11.21	0.00	3.44
192	4	44	0.00	-18.52	0.00	-24.94	0.00	-11.85
		60	0.00	3.48	0.00	24.94	0.00	0.41
	5	44	0.00	-21.82	0.00	-14.03	0.00	-7.66
		60	0.00	8.29	0.00	14.03	0.00	-7.99
193	4	60	0.00	-12.35	0.00	-25.43	0.00	3.90
		76	0.00	-2.68	0.00	25.43	0.00	-8.93

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	60	0.00	-14.42	0.00	-12.26	0.00	3.72
		76	0.00	0.89	0.00	12.26	0.00	-11.68
194	4	76	0.00	-8.08	0.00	-20.14	0.00	13.95
		92	0.00	-6.96	0.00	20.14	0.00	-14.53
	5	76	0.00	-9.59	0.00	-8.51	0.00	8.36
		92	0.00	-3.94	0.00	8.51	0.00	-11.30
195	4	92	0.00	-4.36	0.00	-11.28	0.00	18.73
		108	0.00	-10.67	0.00	11.28	0.00	-15.44
	5	92	0.00	-5.79	0.00	-4.41	0.00	9.43
		108	0.00	-7.74	0.00	4.41	0.00	-8.42
196	4	108	0.00	-1.32	0.00	-3.18	0.00	17.17
		124	0.00	-6.20	0.00	3.18	0.00	-15.90
	5	108	0.00	-2.01	0.00	-1.21	0.00	7.91
		124	0.00	-4.76	0.00	1.21	0.00	-7.20
198	4	29	0.00	-14.24	0.00	-14.91	0.00	-14.94
		45	0.00	-1.87	0.00	14.91	0.00	8.50
	5	29	0.00	-17.39	0.00	-12.68	0.00	-14.42
		45	0.00	2.88	0.00	12.68	0.00	3.88
199	4	45	0.00	-7.13	0.00	-20.38	0.00	-2.31
		61	0.00	-8.98	0.00	20.38	0.00	3.27
	5	45	0.00	-9.98	0.00	-15.51	0.00	-1.67
		61	0.00	-4.53	0.00	15.51	0.00	-1.16
200	4	61	0.00	-4.03	0.00	-19.61	0.00	4.76
		77	0.00	-12.08	0.00	19.61	0.00	-0.58
	5	61	0.00	-6.66	0.00	-13.25	0.00	3.72
		77	0.00	-7.84	0.00	13.25	0.00	-3.11
201	4	77	0.00	-3.33	0.00	-14.60	0.00	8.34
		93	0.00	-12.79	0.00	14.60	0.00	-3.42
	5	77	0.00	-5.51	0.00	-8.84	0.00	5.37
		93	0.00	-8.99	0.00	8.84	0.00	-3.56
202	4	93	0.00	-2.67	0.00	-7.58	0.00	9.31
		109	0.00	-13.44	0.00	7.58	0.00	-3.71
	5	93	0.00	-4.28	0.00	-4.21	0.00	5.33
		109	0.00	-10.22	0.00	4.21	0.00	-2.24
203	4	109	0.00	-0.75	0.00	-2.06	0.00	6.19
		125	0.00	-7.31	0.00	2.06	0.00	-4.48
	5	109	0.00	-1.43	0.00	-1.10	0.00	3.14
		125	0.00	-5.82	0.00	1.10	0.00	-2.00
205	4	30	0.00	-3.21	0.00	-7.25	0.00	-0.24
		46	0.00	-13.98	0.00	7.25	0.00	5.84

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	30	0.00	-3.51	0.00	-6.96	0.00	-0.38
		46	0.00	-11.97	0.00	6.96	0.00	4.78
206	4	46	0.00	-0.17	0.00	-9.29	0.00	2.78
		62	0.00	-17.02	0.00	9.29	0.00	5.98
	5	46	0.00	-1.34	0.00	-8.10	0.00	2.25
		62	0.00	-14.14	0.00	8.10	0.00	4.41
207	4	62	0.00	-0.35	0.00	-8.41	0.00	3.53
		78	0.00	-16.85	0.00	8.41	0.00	5.05
	5	62	0.00	-2.08	0.00	-6.59	0.00	2.44
		78	0.00	-13.40	0.00	6.59	0.00	3.45
208	4	78	0.00	-2.47	0.00	-5.77	0.00	2.92
		94	0.00	-14.72	0.00	5.77	0.00	3.45
	5	78	0.00	-3.95	0.00	-4.08	0.00	1.63
		94	0.00	-11.52	0.00	4.08	0.00	2.30
209	4	94	0.00	-5.47	0.00	-2.37	0.00	1.55
		110	0.00	-11.72	0.00	2.37	0.00	1.69
	5	94	0.00	-6.00	0.00	-1.48	0.00	0.55
		110	0.00	-9.47	0.00	1.48	0.00	1.25
210	4	110	0.00	-2.85	0.00	-0.44	0.00	0.32
		126	0.00	-5.75	0.00	0.44	0.00	0.44
	5	110	0.00	-3.01	0.00	-0.21	0.00	-0.07
		126	0.00	-4.73	0.00	0.21	0.00	0.52
106	4	1	0.00	-11.25	0.00	-0.96	0.00	-15.20
		16	0.00	10.22	0.00	0.96	0.00	9.61
	5	1	0.00	-1.53	0.00	-0.24	0.00	3.67
		16	0.00	0.60	0.00	0.24	0.00	-4.22
113	4	2	0.00	-6.99	0.00	-0.76	0.00	-11.37
		17	0.00	5.42	0.00	0.76	0.00	8.15
	5	2	0.00	0.80	0.00	-0.26	0.00	5.07
		17	0.00	-2.21	0.00	0.26	0.00	-4.29
120	4	3	0.00	-192.00	0.00	-10.23	0.00	-212.75
		18	0.00	189.89	0.00	10.23	0.00	113.45
	5	3	0.00	142.73	0.00	8.30	0.00	147.37
		18	0.00	-144.63	0.00	-8.30	0.00	-72.66
127	4	4	0.00	-285.83	0.00	-49.43	0.00	-658.41
		19	0.00	283.18	0.00	49.43	0.00	510.46
	5	4	0.00	175.86	0.00	42.55	0.00	417.09
		19	0.00	-178.24	0.00	-42.55	0.00	-325.03
134	4	5	0.00	-151.78	0.00	-36.17	0.00	-479.15
		20	0.00	148.59	0.00	36.17	0.00	401.06

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	5	0.00	58.79	0.00	32.91	0.00	259.33
		20	0.00	-61.66	0.00	-32.91	0.00	-228.01
141	4	6	0.00	-105.73	0.00	-27.07	0.00	-358.12
		21	0.00	102.00	0.00	27.07	0.00	304.11
	5	6	0.00	11.01	0.00	25.62	0.00	146.03
		21	0.00	-14.37	0.00	-25.62	0.00	-139.43
148	4	7	0.00	-79.64	0.00	-19.92	0.00	-270.60
		22	0.00	75.37	0.00	19.92	0.00	230.30
	5	7	0.00	-20.56	0.00	19.10	0.00	60.91
		22	0.00	16.72	0.00	-19.10	0.00	-70.61
155	4	8	0.00	-65.02	0.00	-14.45	0.00	-207.93
		23	0.00	60.21	0.00	14.45	0.00	175.37
	5	8	0.00	-41.33	0.00	13.32	0.00	-0.14
		23	0.00	36.99	0.00	-13.32	0.00	-20.22
162	4	9	0.00	-57.36	0.00	-10.60	0.00	-163.13
		24	0.00	52.01	0.00	10.60	0.00	134.69
	5	9	0.00	-53.78	0.00	8.31	0.00	-40.46
		24	0.00	48.96	0.00	-8.31	0.00	13.75
169	4	10	0.00	-53.19	0.00	-8.22	0.00	-129.92
		25	0.00	47.30	0.00	8.22	0.00	103.79
	5	10	0.00	-59.55	0.00	4.04	0.00	-63.06
		25	0.00	54.25	0.00	-4.04	0.00	33.47
176	4	11	0.00	-49.60	0.00	-7.07	0.00	-102.87
		26	0.00	43.17	0.00	7.07	0.00	78.75
	5	11	0.00	-59.51	0.00	0.39	0.00	-70.51
		26	0.00	53.72	0.00	-0.39	0.00	41.07
183	4	12	0.00	-44.01	0.00	-6.79	0.00	-77.67
		27	0.00	37.03	0.00	6.79	0.00	56.59
	5	12	0.00	-53.72	0.00	-2.64	0.00	-64.95
		27	0.00	47.45	0.00	2.64	0.00	38.64
190	4	13	0.00	-34.14	0.00	-6.83	0.00	-51.62
		28	0.00	26.62	0.00	6.83	0.00	35.83
	5	13	0.00	-41.59	0.00	-4.87	0.00	-48.61
		28	0.00	34.82	0.00	4.87	0.00	28.74
197	4	14	0.00	-18.53	0.00	-6.25	0.00	-24.88
		29	0.00	10.47	0.00	6.25	0.00	17.34
	5	14	0.00	-22.49	0.00	-5.66	0.00	-25.18
		29	0.00	15.24	0.00	5.66	0.00	15.37
204	4	15	0.00	-4.18	0.00	-3.19	0.00	-4.08
		30	0.00	-4.42	0.00	3.19	0.00	4.15

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	15	0.00	-4.39	0.00	-3.22	0.00	-4.22
		30	0.00	-3.34	0.00	3.22	0.00	3.94

********** END OF LATEST ANALYSIS RESULT **********

74. PRINT SUPPORT REACTIONS

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = FLOOR

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
1	4	0.00	-11.25	0.00	-0.96	0.00	-15.20
	5	0.00	-1.53	0.00	-0.24	0.00	3.67
2	4	0.00	-6.99	0.00	-0.76	0.00	-11.37
	5	0.00	0.80	0.00	-0.26	0.00	5.07
3	4	0.00	-192.00	0.00	-10.23	0.00	-212.75
	5	0.00	142.73	0.00	8.30	0.00	147.37
4	4	0.00	-285.83	0.00	-49.43	0.00	-658.41
	5	0.00	175.86	0.00	42.55	0.00	417.09
5	4	0.00	-151.78	0.00	-36.17	0.00	-479.15
	5	0.00	58.79	0.00	32.91	0.00	259.33
6	4	0.00	-105.73	0.00	-27.07	0.00	-358.12
	5	0.00	11.01	0.00	25.62	0.00	146.03
7	4	0.00	-79.64	0.00	-19.92	0.00	-270.60
	5	0.00	-20.56	0.00	19.10	0.00	60.91
8	4	0.00	-65.02	0.00	-14.45	0.00	-207.93
	5	0.00	-41.33	0.00	13.32	0.00	-0.14
9	4	0.00	-57.36	0.00	-10.60	0.00	-163.13
	5	0.00	-53.78	0.00	8.31	0.00	-40.46
10	4	0.00	-53.19	0.00	-8.22	0.00	-129.92
	5	0.00	-59.55	0.00	4.04	0.00	-63.06
11	4	0.00	-49.60	0.00	-7.07	0.00	-102.87
	5	0.00	-59.51	0.00	0.39	0.00	-70.51
12	4	0.00	-44.01	0.00	-6.79	0.00	-77.67
	5	0.00	-53.72	0.00	-2.64	0.00	-64.95
13	4	0.00	-34.14	0.00	-6.83	0.00	-51.62
	5	0.00	-41.59	0.00	-4.87	0.00	-48.61
14	4	0.00	-18.53	0.00	-6.25	0.00	-24.88
	5	0.00	-22.49	0.00	-5.66	0.00	-25.18
15	4	0.00	-4.18	0.00	-3.19	0.00	-4.08
	5	0.00	-4.39	0.00	-3.22	0.00	-4.22
31	4	0.00	-2.59	0.00	-4.43	0.00	-3.35
	5	0.00	-2.96	0.00	-4.55	0.00	-3.35
47	4	0.00	-20.60	0.00	-26.10	0.00	-6.13
	5	0.00	-23.62	0.00	-26.20	0.00	-5.57
63	4	0.00	-38.80	0.00	-52.66	0.00	-6.32
	5	0.00	-42.98	0.00	-50.22	0.00	-5.11
79	4	0.00	-51.78	0.00	-75.82	0.00	-5.02
	5	0.00	-55.48	0.00	-68.96	0.00	-3.61
95	4	0.00	-58.14	0.00	-91.08	0.00	-2.82
	5	0.00	-61.27	0.00	-80.08	0.00	-1.81
111	4	0.00	-52.06	0.00	-95.17	0.00	-0.28
	5	0.00	-56.68	0.00	-82.43	0.00	-0.03
127	4	0.00	-24.07	0.00	-47.36	0.00	0.00
	5	0.00	-26.61	0.00	-40.91	0.00	0.00
112	4	0.00	0.00	0.00	0.00	0.00	-6.14
	5	0.00	0.00	0.00	0.00	0.00	5.32
113	4	0.00	0.00	0.00	0.00	0.00	-5.32
	5	0.00	0.00	0.00	0.00	0.00	4.69
114	4	0.00	0.00	0.00	0.00	0.00	-88.77
	5	0.00	0.00	0.00	0.00	0.00	61.21

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = FLOOR

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
115	4	0.00	0.00	0.00	0.00	0.00	-410.41
	5	0.00	0.00	0.00	0.00	0.00	289.73
116	4	0.00	0.00	0.00	0.00	0.00	-325.24
	5	0.00	0.00	0.00	0.00	0.00	209.55
117	4	0.00	0.00	0.00	0.00	0.00	-246.51
	5	0.00	0.00	0.00	0.00	0.00	136.27
118	4	0.00	0.00	0.00	0.00	0.00	-185.01
	5	0.00	0.00	0.00	0.00	0.00	80.62
119	4	0.00	0.00	0.00	0.00	0.00	-137.68
	5	0.00	0.00	0.00	0.00	0.00	40.20
120	4	0.00	0.00	0.00	0.00	0.00	-101.35
	5	0.00	0.00	0.00	0.00	0.00	12.79
121	4	0.00	0.00	0.00	0.00	0.00	-73.07
	5	0.00	0.00	0.00	0.00	0.00	-3.59
122	4	0.00	0.00	0.00	0.00	0.00	-50.35
	5	0.00	0.00	0.00	0.00	0.00	-10.89
123	4	0.00	0.00	0.00	0.00	0.00	-31.49
	5	0.00	0.00	0.00	0.00	0.00	-11.24
124	4	0.00	0.00	0.00	0.00	0.00	-15.90
	5	0.00	0.00	0.00	0.00	0.00	-7.20
125	4	0.00	0.00	0.00	0.00	0.00	-4.48
	5	0.00	0.00	0.00	0.00	0.00	-2.00
126	4	0.00	0.00	0.00	0.00	0.00	0.44
	5	0.00	0.00	0.00	0.00	0.00	0.52

********** END OF LATEST ANALYSIS RESULT **********

75. FINISH

********** END OF STAAD-III **********

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 *          S T A A D - III                       *
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 1. STAAD FLOOR ESTRIBO 1  ALZADO (APOYADO)
 2. * FICHERO (EMPA2)
 3. UNITS MET MTON
 4. JOINT COORDINATES
 5.  1  0.00 0.0 0.0 15  0.00 0.0 14.70
 6. 16  0.52 0.0 0.0 30  0.52 0.0 14.70
 7. 31  0.52 0.0 15.20
 8. 32  1.56 0.0 0.0 46  1.56 0.0 14.70
 9. 47  1.56 0.0 15.20
10. 48  2.60 0.0 0.0 62  2.60 0.0 14.70
11. 63  2.60 0.0 15.20
12. 64  3.64 0.0 0.0 78  3.64 0.0 14.70
13. 79  3.64 0.0 15.20
14. 80  4.68 0.0 0.0 94  4.68 0.0 14.70
15. 95  4.68 0.0 15.20
16. 96  5.72 0.0 0.0 110 5.72 0.0 14.70
17. 111 5.72 0.0 15.20
18. 112 6.24 0.0 0.0 126 6.24 0.0 14.70
19. 127 6.24 0.0 15.20
20. MEMBER INCIDENCES
21.  1  16  17  15
22. R 6 15 16
23. 107 16 32 112 1 16
24. R 14 7 1
25. 106 1 16
26. R 14 7 1
27. MEMBER PROPERTIES
28.   1 2 16 17 31 32          PRIS AX 0.520 IX 0.02166 IZ 0.01083
29.  46 47 61 62 76 77          PRIS AX 0.520 IX 0.02166 IZ 0.01083
30.  91 92                      PRIS AX 0.260 IX 0.01084 IZ 0.00542
31.   3 TO 15 18 TO 30 33 TO 45 PRIS AX 2.444 IX 2.24950 IZ 1.12475
32.  48 TO 60 63 TO 75 78 TO 90 PRIS AX 2.444 IX 2.24950 IZ 1.12475
33.  93 TO 105                  PRIS AX 1.222 IX 1.12474 IZ 0.56237
34. 106 TO 119                  PRIS AX 0.525 IX 0.02188 IZ 0.01094
35. 120 TO 126                  PRIS AX 1.496 IX 0.50638 IZ 0.25319
36. 127 TO 210                  PRIS AX 2.468 IX 2.27112 IZ 1.13556
37. CONSTANTS
38. E 3000000. ALL
39. POISSON 0.15 ALL
40. SUPPORTS
41.  1 TO 15        FIXED BUT MZ
42. 31 TO 127 BY 16 FIXED
43. 112 TO 126      FIXED BUT FY MX
44. LOADING  1 EMPUJE DE TIERRAS
45. MEMBER LOADS
46. 106 TO 112    UNI GY  1.320
47. 113 TO 119    UNI GY  2.013
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* FICHERO (EMPA2)
48. 120 TO 126    UNI GY  2.706
49. 127 TO 133    UNI GY  3.399
50. 134 TO 140    UNI GY  4.092
51. 141 TO 147    UNI GY  4.785
52. 148 TO 154    UNI GY  5.478
53. 155 TO 161    UNI GY  6.171
54. 162 TO 168    UNI GY  6.864
55. 169 TO 175    UNI GY  7.557
56. 176 TO 182    UNI GY  8.250
57. 183 TO 189    UNI GY  8.943
58. 190 TO 196    UNI GY  9.636
59. 197 TO 203    UNI GY 10.329
60. 204 TO 210    UNI GY 11.022
61. LOADING  2 FRENADO+ARRANQE
62. JOINT LOADS
63.  82 98        FY 93.00
64. LOADING  3 DIF.+INTE. CARRIL-TABLERO
65. JOINT LOADS
66.  82 98        FY 97.00
67. LOAD COMB 4
68. 1 1.5 2 1.5 3 1.35
69. LOAD COMB 5
70. 1 1.35 2 -1.5 3 -1.35
71. PERFORM ANALYSIS
```

P R O B L E M S T A T I S T I C S

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 NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS =   127/  210/   37
 ORIGINAL/FINAL BAND-WIDTH =   16/    9
 TOTAL PRIMARY LOAD CASES  =    3, TOTAL DEGREES OF FREEDOM =   315
 SIZE OF STIFFNESS MATRIX =    8505 DOUBLE PREC. WORDS
 TOTAL REQUIRED DISK SPACE =   12.48 MEGA-BYTES
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++ PROCESSING ELEMENT STIFFNESS MATRIX.          23: 2:27
++ PROCESSING GLOBAL STIFFNESS MATRIX.           23: 2:28
++ PROCESSING TRIANGULAR FACTORIZATION.          23: 2:28
++ CALCULATING JOINT DISPLACEMENTS.              23: 2:29
++ CALCULATING MEMBER  FORCES.                   23: 2:29
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 72. LOAD LIST 4 5
 73. PRINT MEMBER FORCES
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MEMBER END FORCES STRUCTURE TYPE = FLOOR
ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	4	16	0.00	0.35	0.00	3.41	0.00	0.24
		17	0.00	-0.35	0.00	-3.41	0.00	0.12
	5	16	0.00	0.23	0.00	-0.25	0.00	0.08
		17	0.00	-0.23	0.00	0.25	0.00	0.16
2	4	17	0.00	2.00	0.00	3.71	0.00	0.21
		18	0.00	-2.00	0.00	-3.71	0.00	1.89
	5	17	0.00	1.57	0.00	-1.06	0.00	0.06
		18	0.00	-1.57	0.00	1.06	0.00	1.59
3	4	18	0.00	2.31	0.00	175.37	0.00	-1.32
		19	0.00	-2.31	0.00	-175.37	0.00	3.74
	5	18	0.00	0.56	0.00	-128.39	0.00	-0.98
		19	0.00	-0.56	0.00	128.39	0.00	1.56
4	4	19	0.00	3.13	0.00	218.62	0.00	-1.98
		20	0.00	-3.13	0.00	-218.62	0.00	5.26
	5	19	0.00	-3.53	0.00	-163.50	0.00	-0.15
		20	0.00	3.53	0.00	163.50	0.00	-3.55
5	4	20	0.00	4.50	0.00	213.80	0.00	-3.05
		21	0.00	-4.50	0.00	-213.80	0.00	7.77
	5	20	0.00	-5.25	0.00	-158.88	0.00	3.25
		21	0.00	5.25	0.00	158.88	0.00	-8.76
6	4	21	0.00	4.81	0.00	203.16	0.00	-4.31
		22	0.00	-4.81	0.00	-203.16	0.00	9.36
	5	21	0.00	-5.43	0.00	-145.15	0.00	6.83
		22	0.00	5.43	0.00	145.15	0.00	-12.54
7	4	22	0.00	4.54	0.00	190.70	0.00	-4.91
		23	0.00	-4.54	0.00	-190.70	0.00	9.67
	5	22	0.00	-4.66	0.00	-125.99	0.00	9.60
		23	0.00	4.66	0.00	125.99	0.00	-14.49
8	4	23	0.00	4.32	0.00	178.11	0.00	-4.74
		24	0.00	-4.32	0.00	-178.11	0.00	9.27
	5	23	0.00	-3.55	0.00	-103.81	0.00	11.31
		24	0.00	3.55	0.00	103.81	0.00	-15.04
9	4	24	0.00	4.46	0.00	166.20	0.00	-4.21
		25	0.00	-4.46	0.00	-166.20	0.00	8.89
	5	24	0.00	-2.36	0.00	-80.50	0.00	12.13
		25	0.00	2.36	0.00	80.50	0.00	-14.61
10	4	25	0.00	5.10	0.00	154.70	0.00	-3.88
		26	0.00	-5.10	0.00	-154.70	0.00	9.24

MEMBER END FORCES STRUCTURE TYPE = FLOOR
ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	25	0.00	-1.12	0.00	-57.44	0.00	12.31
		26	0.00	1.12	0.00	57.44	0.00	-13.49
11	4	26	0.00	6.40	0.00	142.22	0.00	-4.32
		27	0.00	-6.40	0.00	-142.22	0.00	11.04
	5	26	0.00	0.26	0.00	-35.76	0.00	11.95
		27	0.00	-0.26	0.00	35.76	0.00	-11.68
12	4	27	0.00	8.60	0.00	126.10	0.00	-6.19
		28	0.00	-8.60	0.00	-126.10	0.00	15.22
	5	27	0.00	2.00	0.00	-16.65	0.00	11.04
		28	0.00	-2.00	0.00	16.65	0.00	-8.94
13	4	28	0.00	12.21	0.00	101.98	0.00	-10.47
		29	0.00	-12.21	0.00	-101.98	0.00	23.29
	5	28	0.00	4.51	0.00	-1.85	0.00	9.29
		29	0.00	-4.51	0.00	1.85	0.00	-4.55
14	4	29	0.00	18.91	0.00	63.91	0.00	-18.80
		30	0.00	-18.91	0.00	-63.91	0.00	38.66
	5	29	0.00	9.33	0.00	5.52	0.00	5.95
		30	0.00	-9.33	0.00	-5.52	0.00	3.85
15	4	30	0.00	32.71	0.00	25.08	0.00	-35.68
		31	0.00	-32.71	0.00	-25.08	0.00	52.03
	5	30	0.00	20.61	0.00	3.87	0.00	-2.14
		31	0.00	-20.61	0.00	-3.87	0.00	12.45
16	4	32	0.00	1.16	0.00	2.93	0.00	0.68
		33	0.00	-1.16	0.00	-2.93	0.00	0.53
	5	32	0.00	0.80	0.00	-0.47	0.00	0.16
		33	0.00	-0.80	0.00	0.47	0.00	0.69
17	4	33	0.00	4.47	0.00	3.23	0.00	0.15
		34	0.00	-4.47	0.00	-3.23	0.00	4.53
	5	33	0.00	3.22	0.00	-1.41	0.00	-0.39
		34	0.00	-3.22	0.00	1.41	0.00	3.78
18	4	34	0.00	5.81	0.00	172.46	0.00	-3.62
		35	0.00	-5.81	0.00	-172.46	0.00	9.72
	5	34	0.00	-0.18	0.00	-131.23	0.00	-2.43
		35	0.00	0.18	0.00	131.23	0.00	2.25
19	4	35	0.00	11.61	0.00	214.97	0.00	-5.28
		36	0.00	-11.61	0.00	-214.97	0.00	17.47
	5	35	0.00	-11.81	0.00	-164.55	0.00	0.84
		36	0.00	11.81	0.00	164.55	0.00	-13.24
20	4	36	0.00	15.20	0.00	208.15	0.00	-9.65
		37	0.00	-15.20	0.00	-208.15	0.00	25.61

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	36	0.00	-16.68	0.00	-156.69	0.00	11.10
		37	0.00	16.68	0.00	156.69	0.00	-28.61
21	4	37	0.00	15.11	0.00	195.21	0.00	-13.71
		38	0.00	-15.11	0.00	-195.21	0.00	29.57
	5	37	0.00	-16.24	0.00	-140.30	0.00	21.66
		38	0.00	16.24	0.00	140.30	0.00	-38.71
22	4	38	0.00	13.83	0.00	181.30	0.00	-15.15
		39	0.00	-13.83	0.00	-181.30	0.00	29.68
	5	38	0.00	-13.48	0.00	-119.92	0.00	29.35
		39	0.00	13.48	0.00	119.92	0.00	-43.51
23	4	39	0.00	13.05	0.00	168.15	0.00	-14.29
		40	0.00	-13.05	0.00	-168.15	0.00	27.99
	5	39	0.00	-10.10	0.00	-97.80	0.00	33.89
		40	0.00	10.10	0.00	97.80	0.00	-44.50
24	4	40	0.00	13.42	0.00	156.19	0.00	-12.56
		41	0.00	-13.42	0.00	-156.19	0.00	26.65
	5	40	0.00	-6.60	0.00	-75.37	0.00	35.98
		41	0.00	6.60	0.00	75.37	0.00	-42.91
25	4	41	0.00	15.30	0.00	144.83	0.00	-11.55
		42	0.00	-15.30	0.00	-144.83	0.00	27.61
	5	41	0.00	-2.98	0.00	-53.67	0.00	36.25
		42	0.00	2.98	0.00	53.67	0.00	-39.38
26	4	42	0.00	19.04	0.00	132.51	0.00	-12.95
		43	0.00	-19.04	0.00	-132.51	0.00	32.94
	5	42	0.00	1.02	0.00	-33.64	0.00	34.98
		43	0.00	-1.02	0.00	33.64	0.00	-33.90
27	4	43	0.00	25.29	0.00	116.59	0.00	-18.74
		44	0.00	-25.29	0.00	-116.59	0.00	45.29
	5	43	0.00	5.96	0.00	-16.36	0.00	31.99
		44	0.00	-5.96	0.00	16.36	0.00	-25.73
28	4	44	0.00	35.39	0.00	92.97	0.00	-31.78
		45	0.00	-35.39	0.00	-92.97	0.00	68.94
	5	44	0.00	12.95	0.00	-3.44	0.00	26.37
		45	0.00	-12.95	0.00	3.44	0.00	-12.77
29	4	45	0.00	51.93	0.00	56.68	0.00	-57.23
		46	0.00	-51.93	0.00	-56.68	0.00	111.76
	5	45	0.00	24.28	0.00	2.72	0.00	15.55
		46	0.00	-24.28	0.00	-2.72	0.00	9.94
30	4	46	0.00	74.60	0.00	21.36	0.00	-105.84
		47	0.00	-74.60	0.00	-21.36	0.00	143.14

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	46	0.00	41.37	0.00	1.87	0.00	-7.50
		47	0.00	-41.37	0.00	-1.87	0.00	28.18
31	4	48	0.00	1.58	0.00	2.16	0.00	0.90
		49	0.00	-1.58	0.00	-2.16	0.00	0.75
	5	48	0.00	1.28	0.00	-0.62	0.00	0.02
		49	0.00	-1.28	0.00	0.62	0.00	1.33
32	4	49	0.00	5.55	0.00	2.73	0.00	0.11
		50	0.00	-5.55	0.00	-2.73	0.00	5.72
	5	49	0.00	3.46	0.00	-1.61	0.00	-1.31
		50	0.00	-3.46	0.00	1.61	0.00	4.95
33	4	50	0.00	11.08	0.00	169.18	0.00	-5.40
		51	0.00	-11.08	0.00	-169.18	0.00	17.03
	5	50	0.00	-4.96	0.00	-135.69	0.00	-2.70
		51	0.00	4.96	0.00	135.69	0.00	-2.51
34	4	51	0.00	27.40	0.00	207.10	0.00	-8.57
		52	0.00	-27.40	0.00	-207.10	0.00	37.33
	5	51	0.00	-27.22	0.00	-164.68	0.00	3.98
		52	0.00	27.22	0.00	164.68	0.00	-32.57
35	4	52	0.00	29.43	0.00	194.10	0.00	-19.00
		53	0.00	-29.43	0.00	-194.10	0.00	49.90
	5	52	0.00	-30.72	0.00	-149.63	0.00	23.00
		53	0.00	30.72	0.00	149.63	0.00	-55.25
36	4	53	0.00	26.12	0.00	176.87	0.00	-25.58
		54	0.00	-26.12	0.00	-176.87	0.00	53.00
	5	53	0.00	-26.76	0.00	-128.75	0.00	39.35
		54	0.00	26.76	0.00	128.75	0.00	-67.46
37	4	54	0.00	23.00	0.00	161.07	0.00	-26.55
		55	0.00	-23.00	0.00	-161.07	0.00	50.69
	5	54	0.00	-21.26	0.00	-107.09	0.00	49.94
		55	0.00	21.26	0.00	107.09	0.00	-72.26
38	4	55	0.00	21.45	0.00	147.55	0.00	-24.08
		56	0.00	-21.45	0.00	-147.55	0.00	46.60
	5	55	0.00	-15.57	0.00	-85.81	0.00	55.81
		56	0.00	15.57	0.00	85.81	0.00	-72.15
39	4	56	0.00	21.97	0.00	135.96	0.00	-20.74
		57	0.00	-21.97	0.00	-135.96	0.00	43.81
	5	56	0.00	-9.93	0.00	-65.45	0.00	58.22
		57	0.00	9.93	0.00	65.45	0.00	-68.64
40	4	57	0.00	24.90	0.00	125.25	0.00	-19.04
		58	0.00	-24.90	0.00	-125.25	0.00	45.18

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	57	0.00	-4.22	0.00	-46.48	0.00	57.96
		58	0.00	4.22	0.00	46.48	0.00	-62.39
41	4	58	0.00	30.63	0.00	113.68	0.00	-21.61
		59	0.00	-30.63	0.00	-113.68	0.00	53.78
	5	58	0.00	1.98	0.00	-29.48	0.00	55.30
		59	0.00	-1.98	0.00	29.48	0.00	-53.22
42	4	59	0.00	39.94	0.00	98.75	0.00	-31.57
		60	0.00	-39.94	0.00	-98.75	0.00	73.51
	5	59	0.00	9.37	0.00	-15.32	0.00	49.76
		60	0.00	-9.37	0.00	15.32	0.00	-39.92
43	4	60	0.00	54.27	0.00	77.14	0.00	-53.31
		61	0.00	-54.27	0.00	-77.14	0.00	110.30
	5	60	0.00	19.08	0.00	-5.10	0.00	39.82
		61	0.00	-19.08	0.00	5.10	0.00	-19.79
44	4	61	0.00	75.30	0.00	45.71	0.00	-94.20
		62	0.00	-75.30	0.00	-45.71	0.00	173.27
	5	61	0.00	32.44	0.00	0.00	0.00	21.98
		62	0.00	-32.44	0.00	0.00	0.00	12.09
45	4	62	0.00	99.51	0.00	16.93	0.00	-166.22
		63	0.00	-99.51	0.00	-16.93	0.00	215.97
	5	62	0.00	48.97	0.00	0.49	0.00	-10.35
		63	0.00	-48.97	0.00	-0.49	0.00	34.84
46	4	64	0.00	1.32	0.00	1.27	0.00	0.81
		65	0.00	-1.32	0.00	-1.27	0.00	0.57
	5	64	0.00	1.82	0.00	-0.50	0.00	-0.08
		65	0.00	-1.82	0.00	0.50	0.00	1.99
47	4	65	0.00	5.37	0.00	2.05	0.00	0.37
		66	0.00	-5.37	0.00	-2.05	0.00	5.27
	5	65	0.00	3.85	0.00	-1.47	0.00	-2.26
		66	0.00	-3.85	0.00	1.47	0.00	6.30
48	4	66	0.00	40.56	0.00	167.14	0.00	-2.40
		67	0.00	-40.56	0.00	-167.14	0.00	44.99
	5	66	0.00	-34.80	0.00	-142.41	0.00	-6.43
		67	0.00	34.80	0.00	142.41	0.00	-30.12
49	4	67	0.00	55.71	0.00	188.07	0.00	-16.42
		68	0.00	-55.71	0.00	-188.07	0.00	74.92
	5	67	0.00	-55.26	0.00	-155.84	0.00	12.97
		68	0.00	55.26	0.00	155.84	0.00	-70.99
50	4	68	0.00	44.43	0.00	165.05	0.00	-34.69
		69	0.00	-44.43	0.00	-165.05	0.00	81.35

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	68	0.00	-45.07	0.00	-130.56	0.00	41.87
		69	0.00	45.07	0.00	130.56	0.00	-89.19
51	4	69	0.00	36.46	0.00	144.68	0.00	-40.19
		70	0.00	-36.46	0.00	-144.68	0.00	78.48
	5	69	0.00	-36.06	0.00	-106.93	0.00	59.52
		70	0.00	36.06	0.00	106.93	0.00	-97.38
52	4	70	0.00	31.21	0.00	128.67	0.00	-38.62
		71	0.00	-31.21	0.00	-128.67	0.00	71.39
	5	70	0.00	-27.65	0.00	-86.18	0.00	70.06
		71	0.00	27.65	0.00	86.18	0.00	-99.09
53	4	71	0.00	28.76	0.00	116.16	0.00	-33.60
		72	0.00	-28.76	0.00	-116.16	0.00	63.80
	5	71	0.00	-19.75	0.00	-67.65	0.00	75.56
		72	0.00	19.75	0.00	67.65	0.00	-96.29
54	4	72	0.00	29.36	0.00	106.06	0.00	-28.30
		73	0.00	-29.36	0.00	-106.06	0.00	59.13
	5	72	0.00	-12.29	0.00	-50.97	0.00	77.28
		73	0.00	12.29	0.00	50.97	0.00	-90.18
55	4	73	0.00	33.11	0.00	96.99	0.00	-25.91
		74	0.00	-33.11	0.00	-96.99	0.00	60.67
	5	73	0.00	-4.90	0.00	-36.06	0.00	75.93
		74	0.00	4.90	0.00	36.06	0.00	-81.08
56	4	74	0.00	40.26	0.00	87.24	0.00	-29.78
		75	0.00	-40.26	0.00	-87.24	0.00	72.04
	5	74	0.00	2.90	0.00	-23.16	0.00	71.50
		75	0.00	-2.90	0.00	23.16	0.00	-68.45
57	4	75	0.00	51.34	0.00	74.67	0.00	-43.83
		76	0.00	-51.34	0.00	-74.67	0.00	97.74
	5	75	0.00	11.76	0.00	-12.79	0.00	63.21
		76	0.00	-11.76	0.00	12.79	0.00	-50.86
58	4	76	0.00	67.42	0.00	56.97	0.00	-73.24
		77	0.00	-67.42	0.00	-56.97	0.00	144.03
	5	76	0.00	22.48	0.00	-5.54	0.00	49.26
		77	0.00	-22.48	0.00	5.54	0.00	-25.66
59	4	77	0.00	89.91	0.00	32.71	0.00	-125.55
		78	0.00	-89.91	0.00	-32.71	0.00	219.95
	5	77	0.00	35.89	0.00	-1.57	0.00	26.44
		78	0.00	-35.89	0.00	1.57	0.00	11.25
60	4	78	0.00	115.10	0.00	11.88	0.00	-212.23
		79	0.00	-115.10	0.00	-11.88	0.00	269.78

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	78	0.00	51.81	0.00	-0.34	0.00	-10.29
		79	0.00	-51.81	0.00	0.34	0.00	36.19
61	4	80	0.00	0.92	0.00	0.65	0.00	0.51
		81	0.00	-0.92	0.00	-0.65	0.00	0.46
	5	80	0.00	2.12	0.00	-0.42	0.00	-0.08
		81	0.00	-2.12	0.00	0.42	0.00	2.31
62	4	81	0.00	2.12	0.00	1.27	0.00	-0.08
		82	0.00	-2.12	0.00	-1.27	0.00	2.30
	5	81	0.00	6.57	0.00	-1.13	0.00	-2.27
		82	0.00	-6.57	0.00	1.13	0.00	9.17
63	4	82	0.00	145.25	0.00	120.61	0.00	22.39
		83	0.00	-145.25	0.00	-120.61	0.00	130.11
	5	82	0.00	-140.02	0.00	-105.28	0.00	-31.04
		83	0.00	140.02	0.00	105.28	0.00	-115.97
64	4	83	0.00	71.08	0.00	132.92	0.00	-44.22
		84	0.00	-71.08	0.00	-132.92	0.00	118.86
	5	83	0.00	-70.19	0.00	-112.45	0.00	42.34
		84	0.00	70.19	0.00	112.45	0.00	-116.04
65	4	84	0.00	55.99	0.00	113.29	0.00	-53.25
		85	0.00	-55.99	0.00	-113.29	0.00	112.04
	5	84	0.00	-55.95	0.00	-91.18	0.00	63.20
		85	0.00	55.95	0.00	91.18	0.00	-121.95
66	4	85	0.00	44.46	0.00	96.50	0.00	-54.58
		86	0.00	-44.46	0.00	-96.50	0.00	101.26
	5	85	0.00	-43.08	0.00	-72.18	0.00	78.20
		86	0.00	43.08	0.00	72.18	0.00	-123.44
67	4	86	0.00	36.90	0.00	84.03	0.00	-49.68
		87	0.00	-36.90	0.00	-84.03	0.00	88.43
	5	86	0.00	-31.78	0.00	-56.60	0.00	87.10
		87	0.00	31.78	0.00	56.60	0.00	-120.47
68	4	87	0.00	33.68	0.00	74.88	0.00	-41.78
		88	0.00	-33.68	0.00	-74.88	0.00	77.14
	5	87	0.00	-22.13	0.00	-43.60	0.00	91.15
		88	0.00	22.13	0.00	43.60	0.00	-114.39
69	4	88	0.00	34.39	0.00	67.85	0.00	-34.53
		89	0.00	-34.39	0.00	-67.85	0.00	70.64
	5	88	0.00	-13.41	0.00	-32.47	0.00	91.62
		89	0.00	13.41	0.00	32.47	0.00	-105.70
70	4	89	0.00	38.80	0.00	61.70	0.00	-31.48
		90	0.00	-38.80	0.00	-61.70	0.00	72.23

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	89	0.00	-4.94	0.00	-22.85	0.00	88.96
		90	0.00	4.94	0.00	22.85	0.00	-94.14
71	4	90	0.00	46.92	0.00	55.10	0.00	-36.46
		91	0.00	-46.92	0.00	-55.10	0.00	85.73
	5	90	0.00	3.83	0.00	-14.79	0.00	82.82
		91	0.00	-3.83	0.00	14.79	0.00	-78.80
72	4	91	0.00	58.86	0.00	46.53	0.00	-53.95
		92	0.00	-58.86	0.00	-46.53	0.00	115.75
	5	91	0.00	13.33	0.00	-8.53	0.00	72.11
		92	0.00	-13.33	0.00	8.53	0.00	-58.11
73	4	92	0.00	74.88	0.00	34.49	0.00	-89.37
		93	0.00	-74.88	0.00	-34.49	0.00	167.99
	5	92	0.00	23.96	0.00	-4.33	0.00	55.00
		93	0.00	-23.96	0.00	4.33	0.00	-29.84
74	4	93	0.00	95.98	0.00	18.69	0.00	-149.24
		94	0.00	-95.98	0.00	-18.69	0.00	250.02
	5	93	0.00	36.30	0.00	-1.96	0.00	29.11
		94	0.00	-36.30	0.00	1.96	0.00	9.00
75	4	94	0.00	121.20	0.00	6.47	0.00	-242.33
		95	0.00	-121.20	0.00	-6.47	0.00	302.93
	5	94	0.00	51.53	0.00	-0.70	0.00	-8.73
		95	0.00	-51.53	0.00	0.70	0.00	34.49
76	4	96	0.00	0.53	0.00	0.27	0.00	0.35
		97	0.00	-0.53	0.00	-0.27	0.00	0.21
	5	96	0.00	2.46	0.00	-0.26	0.00	-0.19
		97	0.00	-2.46	0.00	0.26	0.00	2.77
77	4	97	0.00	1.50	0.00	0.47	0.00	0.09
		98	0.00	-1.50	0.00	-0.47	0.00	1.49
	5	97	0.00	5.76	0.00	-0.59	0.00	-3.04
		98	0.00	-5.76	0.00	0.59	0.00	9.09
78	4	98	0.00	141.10	0.00	31.12	0.00	18.12
		99	0.00	-141.10	0.00	-31.12	0.00	130.04
	5	98	0.00	-136.90	0.00	-25.68	0.00	-26.38
		99	0.00	136.90	0.00	25.68	0.00	-117.37
79	4	99	0.00	75.59	0.00	44.94	0.00	-54.84
		100	0.00	-75.59	0.00	-44.94	0.00	134.21
	5	99	0.00	-77.07	0.00	-37.70	0.00	52.48
		100	0.00	77.07	0.00	37.70	0.00	-133.40
80	4	100	0.00	49.33	0.00	40.72	0.00	-72.20
		101	0.00	-49.33	0.00	-40.72	0.00	124.00

MEMBER END FORCES STRUCTURE TYPE = FLOOR
ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	100	0.00	-52.01	0.00	-32.95	0.00	82.05
		101	0.00	52.01	0.00	32.95	0.00	-136.67
81	4	101	0.00	34.57	0.00	34.36	0.00	-71.70
		102	0.00	-34.57	0.00	-34.36	0.00	107.99
	5	101	0.00	-36.08	0.00	-25.83	0.00	95.89
		102	0.00	36.08	0.00	25.83	0.00	-133.78
82	4	102	0.00	27.39	0.00	29.52	0.00	-63.18
		103	0.00	-27.39	0.00	-29.52	0.00	91.93
	5	102	0.00	-25.25	0.00	-19.90	0.00	101.82
		103	0.00	25.25	0.00	19.90	0.00	-128.33
83	4	103	0.00	25.17	0.00	26.10	0.00	-52.45
		104	0.00	-25.17	0.00	-26.10	0.00	78.88
	5	103	0.00	-16.61	0.00	-15.13	0.00	103.50
		104	0.00	16.61	0.00	15.13	0.00	-120.95
84	4	104	0.00	27.07	0.00	23.56	0.00	-43.33
		105	0.00	-27.07	0.00	-23.56	0.00	71.75
	5	104	0.00	-8.89	0.00	-11.16	0.00	102.12
		105	0.00	8.89	0.00	11.16	0.00	-111.45
85	4	105	0.00	32.84	0.00	21.38	0.00	-39.36
		106	0.00	-32.84	0.00	-21.38	0.00	73.84
	5	105	0.00	-1.29	0.00	-7.80	0.00	97.81
		106	0.00	1.29	0.00	7.80	0.00	-99.16
86	4	106	0.00	42.51	0.00	19.04	0.00	-44.46
		107	0.00	-42.51	0.00	-19.04	0.00	89.10
	5	106	0.00	6.74	0.00	-5.04	0.00	89.97
		107	0.00	-6.74	0.00	5.04	0.00	-82.89
87	4	107	0.00	56.14	0.00	15.94	0.00	-63.33
		108	0.00	-56.14	0.00	-15.94	0.00	122.28
	5	107	0.00	15.57	0.00	-2.96	0.00	77.30
		108	0.00	-15.57	0.00	2.96	0.00	-60.96
88	4	108	0.00	73.46	0.00	11.49	0.00	-101.56
		109	0.00	-73.46	0.00	-11.49	0.00	178.70
	5	108	0.00	25.27	0.00	-1.66	0.00	57.98
		109	0.00	-25.27	0.00	1.66	0.00	-31.44
89	4	109	0.00	92.93	0.00	5.57	0.00	-165.23
		110	0.00	-92.93	0.00	-5.57	0.00	262.81
	5	109	0.00	35.42	0.00	-1.03	0.00	29.97
		110	0.00	-35.42	0.00	1.03	0.00	7.23
90	4	110	0.00	110.41	0.00	1.18	0.00	-258.43
		111	0.00	-110.41	0.00	-1.18	0.00	313.63

MEMBER END FORCES STRUCTURE TYPE = FLOOR
ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	110	0.00	46.33	0.00	-0.71	0.00	-7.74
		111	0.00	-46.33	0.00	0.71	0.00	30.90
91	4	112	0.00	0.16	0.00	0.00	0.00	0.14
		113	0.00	-0.16	0.00	0.00	0.00	0.03
	5	112	0.00	1.34	0.00	0.00	0.00	-0.09
		113	0.00	-1.34	0.00	0.00	0.00	1.50
92	4	113	0.00	1.09	0.00	0.00	0.00	0.20
		114	0.00	-1.09	0.00	0.00	0.00	0.95
	5	113	0.00	2.33	0.00	0.00	0.00	-1.76
		114	0.00	-2.33	0.00	0.00	0.00	4.21
93	4	114	0.00	50.76	0.00	0.00	0.00	1.73
		115	0.00	-50.76	0.00	0.00	0.00	51.57
	5	114	0.00	-49.85	0.00	0.00	0.00	-6.23
		115	0.00	49.85	0.00	0.00	0.00	-46.10
94	4	115	0.00	34.48	0.00	0.00	0.00	-28.69
		116	0.00	-34.48	0.00	0.00	0.00	64.90
	5	115	0.00	-36.25	0.00	0.00	0.00	27.06
		116	0.00	36.25	0.00	0.00	0.00	-65.12
95	4	116	0.00	18.73	0.00	0.00	0.00	-40.34
		117	0.00	-18.73	0.00	0.00	0.00	60.01
	5	116	0.00	-21.30	0.00	0.00	0.00	44.72
		117	0.00	21.30	0.00	0.00	0.00	-67.08
96	4	117	0.00	12.08	0.00	0.00	0.00	-39.45
		118	0.00	-12.08	0.00	0.00	0.00	52.13
	5	117	0.00	-14.17	0.00	0.00	0.00	50.99
		118	0.00	14.17	0.00	0.00	0.00	-65.87
97	4	118	0.00	9.05	0.00	0.00	0.00	-34.65
		119	0.00	-9.05	0.00	0.00	0.00	44.15
	5	118	0.00	-9.47	0.00	0.00	0.00	53.38
		119	0.00	9.47	0.00	0.00	0.00	-63.33
98	4	119	0.00	8.42	0.00	0.00	0.00	-28.86
		120	0.00	-8.42	0.00	0.00	0.00	37.70
	5	119	0.00	-5.83	0.00	0.00	0.00	53.72
		120	0.00	5.83	0.00	0.00	0.00	-59.84
99	4	120	0.00	9.78	0.00	0.00	0.00	-23.99
		121	0.00	-9.78	0.00	0.00	0.00	34.25
	5	120	0.00	-2.57	0.00	0.00	0.00	52.61
		121	0.00	2.57	0.00	0.00	0.00	-55.31
100	4	121	0.00	13.04	0.00	0.00	0.00	-21.79
		122	0.00	-13.04	0.00	0.00	0.00	35.48

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	121	0.00	0.71	0.00	0.00	0.00	50.10
		122	0.00	-0.71	0.00	0.00	0.00	-49.35
101	4	122	0.00	18.28	0.00	0.00	0.00	-24.20
		123	0.00	-18.28	0.00	0.00	0.00	43.39
	5	122	0.00	4.28	0.00	0.00	0.00	45.84
		123	0.00	-4.28	0.00	0.00	0.00	-41.35
102	4	123	0.00	25.60	0.00	0.00	0.00	-33.53
		124	0.00	-25.60	0.00	0.00	0.00	60.41
	5	123	0.00	8.33	0.00	0.00	0.00	39.21
		124	0.00	-8.33	0.00	0.00	0.00	-30.46
103	4	124	0.00	34.88	0.00	0.00	0.00	-52.57
		125	0.00	-34.88	0.00	0.00	0.00	89.20
	5	124	0.00	12.91	0.00	0.00	0.00	29.28
		125	0.00	-12.91	0.00	0.00	0.00	-15.72
104	4	125	0.00	45.31	0.00	0.00	0.00	-84.25
		126	0.00	-45.31	0.00	0.00	0.00	131.83
	5	125	0.00	17.75	0.00	0.00	0.00	15.06
		126	0.00	-17.75	0.00	0.00	0.00	3.58
105	4	126	0.00	52.84	0.00	0.00	0.00	-130.56
		127	0.00	-52.84	0.00	0.00	0.00	156.98
	5	126	0.00	21.41	0.00	0.00	0.00	-4.03
		127	0.00	-21.41	0.00	0.00	0.00	14.74
107	4	16	0.00	-5.67	0.00	-3.39	0.00	-0.38
		32	0.00	3.61	0.00	3.39	0.00	-4.45
	5	16	0.00	-0.37	0.00	0.26	0.00	0.56
		32	0.00	-1.49	0.00	-0.26	0.00	0.02
108	4	32	0.00	-4.77	0.00	-2.71	0.00	1.52
		48	0.00	2.71	0.00	2.71	0.00	-5.40
	5	32	0.00	0.68	0.00	0.41	0.00	0.45
		48	0.00	-2.54	0.00	-0.41	0.00	1.22
109	4	48	0.00	-4.28	0.00	-1.81	0.00	3.25
		64	0.00	2.22	0.00	1.81	0.00	-6.63
	5	48	0.00	1.26	0.00	0.43	0.00	-0.60
		64	0.00	-3.11	0.00	-0.43	0.00	2.87
110	4	64	0.00	-3.54	0.00	-0.99	0.00	5.36
		80	0.00	1.48	0.00	0.99	0.00	-7.97
	5	64	0.00	1.29	0.00	0.35	0.00	-2.37
		80	0.00	-3.15	0.00	-0.35	0.00	4.68
111	4	80	0.00	-2.40	0.00	-0.49	0.00	7.32
		96	0.00	0.34	0.00	0.49	0.00	-8.75

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	80	0.00	1.02	0.00	0.28	0.00	-4.26
		96	0.00	-2.87	0.00	-0.28	0.00	6.28
112	4	96	0.00	-0.87	0.00	-0.14	0.00	8.48
		112	0.00	-0.16	0.00	0.14	0.00	-8.66
	5	96	0.00	0.41	0.00	0.09	0.00	-6.03
		112	0.00	-1.34	0.00	-0.09	0.00	6.48
114	4	17	0.00	-2.82	0.00	-3.40	0.00	0.72
		33	0.00	-0.32	0.00	3.40	0.00	-2.03
	5	17	0.00	-0.18	0.00	0.46	0.00	0.57
		33	0.00	-2.65	0.00	-0.46	0.00	0.72
115	4	33	0.00	-2.99	0.00	-2.71	0.00	1.72
		49	0.00	-0.15	0.00	2.71	0.00	-3.20
	5	33	0.00	0.23	0.00	0.76	0.00	0.22
		49	0.00	-3.06	0.00	-0.76	0.00	1.49
116	4	49	0.00	-3.83	0.00	-1.85	0.00	2.63
		65	0.00	0.69	0.00	1.85	0.00	-4.98
	5	49	0.00	0.87	0.00	0.77	0.00	-0.50
		65	0.00	-3.70	0.00	-0.77	0.00	2.88
117	4	65	0.00	-4.74	0.00	-0.91	0.00	4.19
		81	0.00	1.60	0.00	0.91	0.00	-7.49
	5	65	0.00	1.67	0.00	0.50	0.00	-1.90
		81	0.00	-4.50	0.00	-0.50	0.00	5.11
118	4	81	0.00	-2.80	0.00	-0.53	0.00	6.87
		97	0.00	-0.34	0.00	0.53	0.00	-8.14
	5	81	0.00	0.05	0.00	0.53	0.00	-4.40
		97	0.00	-2.88	0.00	-0.53	0.00	5.93
119	4	97	0.00	-0.63	0.00	-0.22	0.00	7.95
		113	0.00	-0.94	0.00	0.22	0.00	-7.87
	5	97	0.00	-0.42	0.00	0.26	0.00	-5.60
		113	0.00	-0.99	0.00	-0.26	0.00	5.74
121	4	18	0.00	-189.67	0.00	-51.08	0.00	-72.64
		34	0.00	185.45	0.00	51.08	0.00	-122.42
	5	18	0.00	128.11	0.00	37.73	0.00	61.74
		34	0.00	-131.91	0.00	-37.73	0.00	73.47
122	4	34	0.00	-186.79	0.00	-50.17	0.00	-46.80
		50	0.00	182.57	0.00	50.17	0.00	-145.26
	5	34	0.00	135.31	0.00	39.07	0.00	56.35
		50	0.00	-139.11	0.00	-39.07	0.00	86.35
123	4	50	0.00	-188.09	0.00	-49.85	0.00	-21.19
		66	0.00	183.87	0.00	49.85	0.00	-172.23

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	50	0.00	147.53	0.00	41.31	0.00	47.73
		66	0.00	-151.33	0.00	-41.31	0.00	107.68
124	4	66	0.00	-219.06	0.00	-46.98	0.00	7.15
		82	0.00	214.84	0.00	46.98	0.00	-232.78
	5	66	0.00	189.98	0.00	41.18	0.00	33.26
		82	0.00	-193.78	0.00	-41.18	0.00	166.30
125	4	82	0.00	-87.52	0.00	-22.28	0.00	113.44
		98	0.00	83.30	0.00	22.28	0.00	-202.27
	5	82	0.00	69.92	0.00	19.31	0.00	-62.14
		98	0.00	-73.72	0.00	-19.31	0.00	136.83
126	4	98	0.00	47.56	0.00	-2.68	0.00	171.61
		114	0.00	-49.67	0.00	2.68	0.00	-146.34
	5	98	0.00	-54.08	0.00	2.02	0.00	-111.74
		114	0.00	52.18	0.00	-2.02	0.00	84.12
128	4	19	0.00	-147.85	0.00	-225.43	0.00	33.90
		35	0.00	142.54	0.00	225.43	0.00	-184.90
	5	19	0.00	62.67	0.00	170.14	0.00	5.26
		35	0.00	-67.44	0.00	-170.14	0.00	62.40
129	4	35	0.00	-148.35	0.00	-220.99	0.00	142.39
		51	0.00	143.05	0.00	220.99	0.00	-293.92
	5	35	0.00	79.08	0.00	173.23	0.00	-29.07
		51	0.00	-83.85	0.00	-173.23	0.00	113.80
130	4	51	0.00	-159.38	0.00	-212.52	0.00	256.00
		67	0.00	154.08	0.00	212.52	0.00	-419.00
	5	51	0.00	106.12	0.00	174.71	0.00	-84.81
		67	0.00	-110.89	0.00	-174.71	0.00	197.66
131	4	67	0.00	-169.23	0.00	-183.96	0.00	398.06
		83	0.00	163.92	0.00	183.96	0.00	-571.30
	5	67	0.00	131.34	0.00	157.56	0.00	-184.22
		83	0.00	-136.11	0.00	-157.56	0.00	323.30
132	4	83	0.00	-89.74	0.00	-98.08	0.00	558.98
		99	0.00	84.44	0.00	98.08	0.00	-649.56
	5	83	0.00	66.28	0.00	83.93	0.00	-316.12
		99	0.00	-71.05	0.00	-83.93	0.00	387.54
133	4	99	0.00	-18.92	0.00	-22.88	0.00	635.74
		115	0.00	16.27	0.00	22.88	0.00	-644.91
	5	99	0.00	11.25	0.00	19.04	0.00	-375.50
		115	0.00	-13.64	0.00	-19.04	0.00	381.98
135	4	20	0.00	-97.84	0.00	-218.56	0.00	55.81
		36	0.00	91.46	0.00	218.56	0.00	-154.25

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	20	0.00	24.43	0.00	165.41	0.00	-15.69
		36	0.00	-30.18	0.00	-165.41	0.00	44.08
136	4	36	0.00	-95.04	0.00	-210.73	0.00	161.07
		52	0.00	88.66	0.00	210.73	0.00	-256.59
	5	36	0.00	35.05	0.00	163.27	0.00	-51.94
		52	0.00	-40.80	0.00	-163.27	0.00	91.39
137	4	52	0.00	-90.69	0.00	-192.39	0.00	269.60
		68	0.00	84.31	0.00	192.39	0.00	-360.60
	5	52	0.00	44.29	0.00	153.70	0.00	-106.44
		68	0.00	-50.04	0.00	-153.70	0.00	155.49
138	4	68	0.00	-73.03	0.00	-152.17	0.00	383.62
		84	0.00	66.65	0.00	152.17	0.00	-456.26
	5	68	0.00	39.85	0.00	124.58	0.00	-180.77
		84	0.00	-45.59	0.00	-124.58	0.00	225.20
139	4	84	0.00	-51.59	0.00	-86.56	0.00	475.88
		100	0.00	45.20	0.00	86.56	0.00	-526.21
	5	84	0.00	31.38	0.00	71.74	0.00	-246.48
		100	0.00	-37.12	0.00	-71.74	0.00	282.10
140	4	100	0.00	-18.95	0.00	-24.55	0.00	530.43
		116	0.00	15.75	0.00	24.55	0.00	-539.46
	5	100	0.00	12.12	0.00	20.40	0.00	-286.84
		116	0.00	-14.99	0.00	-20.40	0.00	293.89
142	4	21	0.00	-85.40	0.00	-207.72	0.00	55.85
		37	0.00	77.94	0.00	207.72	0.00	-140.79
	5	21	0.00	12.40	0.00	153.14	0.00	-19.22
		37	0.00	-19.12	0.00	-153.14	0.00	35.61
143	4	37	0.00	-77.85	0.00	-195.82	0.00	153.72
		53	0.00	70.39	0.00	195.82	0.00	-230.80
	5	37	0.00	18.68	0.00	146.19	0.00	-52.00
		53	0.00	-25.40	0.00	-146.19	0.00	74.93
144	4	53	0.00	-67.06	0.00	-171.50	0.00	248.03
		69	0.00	59.60	0.00	171.50	0.00	-313.89
	5	53	0.00	21.43	0.00	130.29	0.00	-95.80
		69	0.00	-28.15	0.00	-130.29	0.00	121.58
145	4	69	0.00	-51.63	0.00	-130.34	0.00	334.26
		85	0.00	44.16	0.00	130.34	0.00	-384.07
	5	69	0.00	19.15	0.00	100.61	0.00	-145.21
		85	0.00	-25.87	0.00	-100.61	0.00	168.62
146	4	85	0.00	-32.61	0.00	-72.87	0.00	400.86
		101	0.00	25.15	0.00	72.87	0.00	-430.90

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	85	0.00	12.98	0.00	56.86	0.00	-187.62
		101	0.00	-19.70	0.00	-56.86	0.00	204.61
147	4	101	0.00	-10.43	0.00	-20.56	0.00	437.24
		117	0.00	6.70	0.00	20.56	0.00	-441.70
	5	101	0.00	3.79	0.00	16.09	0.00	-211.72
		117	0.00	-7.15	0.00	-16.09	0.00	214.56
149	4	22	0.00	-74.43	0.00	-194.60	0.00	52.42
		38	0.00	65.88	0.00	194.60	0.00	-125.38
	5	22	0.00	1.21	0.00	134.97	0.00	-19.19
		38	0.00	-8.90	0.00	-134.97	0.00	24.44
150	4	38	0.00	-64.61	0.00	-180.18	0.00	139.29
		54	0.00	56.06	0.00	180.18	0.00	-202.04
	5	38	0.00	6.15	0.00	125.61	0.00	-44.82
		54	0.00	-13.84	0.00	-125.61	0.00	55.21
151	4	54	0.00	-52.94	0.00	-153.73	0.00	217.83
		70	0.00	44.40	0.00	153.73	0.00	-268.45
	5	54	0.00	8.35	0.00	108.10	0.00	-76.86
		70	0.00	-16.04	0.00	-108.10	0.00	89.54
152	4	70	0.00	-39.13	0.00	-113.87	0.00	284.46
		86	0.00	30.58	0.00	113.87	0.00	-320.72
	5	70	0.00	7.62	0.00	80.78	0.00	-110.30
		86	0.00	-15.31	0.00	-80.78	0.00	122.22
153	4	86	0.00	-23.04	0.00	-62.30	0.00	333.19
		102	0.00	14.49	0.00	62.30	0.00	-352.71
	5	86	0.00	4.00	0.00	44.44	0.00	-137.79
		102	0.00	-11.69	0.00	-44.44	0.00	145.95
154	4	102	0.00	-7.34	0.00	-17.48	0.00	357.53
		118	0.00	3.07	0.00	17.48	0.00	-360.24
	5	102	0.00	0.88	0.00	12.49	0.00	-151.88
		118	0.00	-4.72	0.00	-12.49	0.00	153.33
156	4	23	0.00	-63.79	0.00	-181.20	0.00	47.12
		39	0.00	54.16	0.00	181.20	0.00	-108.46
	5	23	0.00	-8.75	0.00	113.36	0.00	-17.08
		39	0.00	0.09	0.00	-113.36	0.00	12.48
157	4	39	0.00	-53.37	0.00	-165.82	0.00	121.61
		55	0.00	43.75	0.00	165.82	0.00	-172.11
	5	39	0.00	-3.47	0.00	103.74	0.00	-34.61
		55	0.00	-5.19	0.00	-103.74	0.00	35.50
158	4	55	0.00	-42.19	0.00	-139.21	0.00	185.63
		71	0.00	32.57	0.00	139.21	0.00	-224.50

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	55	0.00	-0.50	0.00	87.29	0.00	-56.78
		71	0.00	-8.16	0.00	-87.29	0.00	60.76
159	4	71	0.00	-30.12	0.00	-101.41	0.00	237.01
		87	0.00	20.49	0.00	101.41	0.00	-263.33
	5	71	0.00	0.26	0.00	63.75	0.00	-79.29
		87	0.00	-8.92	0.00	-63.75	0.00	84.06
160	4	87	0.00	-17.29	0.00	-54.76	0.00	272.47
		103	0.00	7.66	0.00	54.76	0.00	-285.44
	5	87	0.00	-0.72	0.00	34.44	0.00	-97.05
		103	0.00	-7.95	0.00	-34.44	0.00	100.81
161	4	103	0.00	-5.39	0.00	-15.29	0.00	288.88
		119	0.00	0.58	0.00	15.29	0.00	-290.43
	5	103	0.00	-0.65	0.00	9.60	0.00	-105.57
		119	0.00	-3.68	0.00	-9.60	0.00	106.37
163	4	24	0.00	-53.44	0.00	-168.66	0.00	41.02
		40	0.00	42.73	0.00	168.66	0.00	-91.02
	5	24	0.00	-16.70	0.00	90.29	0.00	-14.00
		40	0.00	7.06	0.00	-90.29	0.00	1.64
164	4	40	0.00	-43.10	0.00	-153.23	0.00	102.99
		56	0.00	32.40	0.00	153.23	0.00	-142.25
	5	40	0.00	-10.56	0.00	81.77	0.00	-24.08
		56	0.00	0.92	0.00	-81.77	0.00	18.10
165	4	56	0.00	-32.93	0.00	-127.37	0.00	153.84
		72	0.00	22.22	0.00	127.37	0.00	-182.51
	5	56	0.00	-6.56	0.00	67.84	0.00	-38.47
		72	0.00	-3.08	0.00	-67.84	0.00	36.66
166	4	72	0.00	-22.81	0.00	-91.87	0.00	192.62
		88	0.00	12.10	0.00	91.87	0.00	-210.77
	5	72	0.00	-4.38	0.00	48.82	0.00	-53.34
		88	0.00	-5.26	0.00	-48.82	0.00	53.79
167	4	88	0.00	-12.81	0.00	-49.26	0.00	217.80
		104	0.00	2.10	0.00	49.26	0.00	-225.56
	5	88	0.00	-3.47	0.00	26.05	0.00	-64.93
		104	0.00	-6.17	0.00	-26.05	0.00	66.34
168	4	104	0.00	-3.99	0.00	-13.71	0.00	228.10
		120	0.00	-1.37	0.00	13.71	0.00	-228.78
	5	104	0.00	-1.55	0.00	7.23	0.00	-70.31
		120	0.00	-3.27	0.00	-7.23	0.00	70.75
170	4	25	0.00	-42.84	0.00	-157.10	0.00	34.97
		41	0.00	31.05	0.00	157.10	0.00	-73.39

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	25	0.00	-22.30	0.00	67.18	0.00	-10.73
		41	0.00	11.69	0.00	-67.18	0.00	-6.94
171	4	41	0.00	-32.93	0.00	-142.00	0.00	84.75
		57	0.00	21.14	0.00	142.00	0.00	-112.87
	5	41	0.00	-15.30	0.00	60.52	0.00	-14.75
		57	0.00	4.69	0.00	-60.52	0.00	4.35
172	4	57	0.00	-24.07	0.00	-117.23	0.00	123.58
		73	0.00	12.28	0.00	117.23	0.00	-142.48
	5	57	0.00	-10.41	0.00	49.84	0.00	-23.33
		73	0.00	-0.20	0.00	-49.84	0.00	18.02
173	4	73	0.00	-16.03	0.00	-84.01	0.00	151.54
		89	0.00	4.24	0.00	84.01	0.00	-162.08
	5	73	0.00	-7.18	0.00	35.59	0.00	-32.93
		89	0.00	-3.43	0.00	-35.59	0.00	30.99
174	4	89	0.00	-8.65	0.00	-44.86	0.00	168.23
		105	0.00	-3.14	0.00	44.86	0.00	-171.10
	5	89	0.00	-5.04	0.00	18.85	0.00	-40.60
		105	0.00	-5.57	0.00	-18.85	0.00	40.88
175	4	105	0.00	-2.62	0.00	-12.47	0.00	173.28
		121	0.00	-3.28	0.00	12.47	0.00	-173.11
	5	105	0.00	-2.03	0.00	5.21	0.00	-44.23
		121	0.00	-3.28	0.00	-5.21	0.00	44.56
177	4	26	0.00	-31.14	0.00	-145.55	0.00	29.67
		42	0.00	18.27	0.00	145.55	0.00	-55.36
	5	26	0.00	-25.34	0.00	45.09	0.00	-7.72
		42	0.00	13.75	0.00	-45.09	0.00	-12.61
178	4	42	0.00	-22.00	0.00	-130.89	0.00	67.67
		58	0.00	9.13	0.00	130.89	0.00	-83.86
	5	42	0.00	-17.76	0.00	40.69	0.00	-7.42
		58	0.00	6.17	0.00	-40.69	0.00	-5.02
179	4	58	0.00	-14.87	0.00	-107.32	0.00	95.43
		74	0.00	2.00	0.00	107.32	0.00	-104.20
	5	58	0.00	-12.37	0.00	33.60	0.00	-11.97
		74	0.00	0.79	0.00	-33.60	0.00	5.13
180	4	74	0.00	-9.15	0.00	-76.42	0.00	113.95
		90	0.00	-3.72	0.00	76.42	0.00	-116.76
	5	74	0.00	-8.60	0.00	24.02	0.00	-18.02
		90	0.00	-2.98	0.00	-24.02	0.00	15.10
181	4	90	0.00	-4.39	0.00	-40.66	0.00	123.36
		106	0.00	-8.48	0.00	40.66	0.00	-121.24

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	90	0.00	-5.77	0.00	12.70	0.00	-23.17
		106	0.00	-5.81	0.00	-12.70	0.00	23.19
182	4	106	0.00	-1.18	0.00	-11.28	0.00	123.58
		122	0.00	-5.25	0.00	11.28	0.00	-122.52
	5	106	0.00	-2.22	0.00	3.51	0.00	-25.95
		122	0.00	-3.57	0.00	-3.51	0.00	26.30
184	4	27	0.00	-17.20	0.00	-132.02	0.00	25.73
		43	0.00	3.25	0.00	132.02	0.00	-36.36
	5	27	0.00	-25.48	0.00	25.04	0.00	-5.14
		43	0.00	12.93	0.00	-25.04	0.00	-14.84
185	4	43	0.00	-9.49	0.00	-117.82	0.00	52.28
		59	0.00	-4.46	0.00	117.82	0.00	-54.90
	5	43	0.00	-17.86	0.00	23.13	0.00	-2.44
		59	0.00	5.31	0.00	-23.13	0.00	-9.61
186	4	59	0.00	-4.85	0.00	-95.61	0.00	69.83
		75	0.00	-9.10	0.00	95.61	0.00	-67.62
	5	59	0.00	-12.70	0.00	19.67	0.00	-4.56
		75	0.00	0.14	0.00	-19.67	0.00	-2.12
187	4	75	0.00	-1.99	0.00	-67.40	0.00	80.18
		91	0.00	-11.96	0.00	67.40	0.00	-75.00
	5	75	0.00	-9.01	0.00	14.42	0.00	-8.25
		91	0.00	-3.55	0.00	-14.42	0.00	5.41
188	4	91	0.00	0.02	0.00	-35.62	0.00	83.57
		107	0.00	-13.97	0.00	35.62	0.00	-76.29
	5	91	0.00	-5.96	0.00	7.73	0.00	-11.67
		107	0.00	-6.60	0.00	-7.73	0.00	12.01
189	4	107	0.00	0.36	0.00	-9.85	0.00	79.39
		123	0.00	-7.33	0.00	9.85	0.00	-77.39
	5	107	0.00	-2.22	0.00	2.14	0.00	-14.09
		123	0.00	-4.06	0.00	-2.14	0.00	14.56
191	4	28	0.00	0.46	0.00	-113.13	0.00	23.96
		44	0.00	-15.49	0.00	113.13	0.00	-15.67
	5	28	0.00	-22.08	0.00	8.32	0.00	-2.86
		44	0.00	8.56	0.00	-8.32	0.00	-13.07
192	4	44	0.00	5.39	0.00	-99.63	0.00	39.29
		60	0.00	-20.42	0.00	99.63	0.00	-25.87
	5	44	0.00	-15.54	0.00	8.96	0.00	0.15
		60	0.00	2.02	0.00	-8.96	0.00	-9.29
193	4	60	0.00	6.09	0.00	-79.43	0.00	47.48
		76	0.00	-21.12	0.00	79.43	0.00	-33.33

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	60	0.00	-11.72	0.00	8.86	0.00	-0.93
		76	0.00	-1.81	0.00	-8.86	0.00	-4.23
194	4	76	0.00	5.05	0.00	-54.94	0.00	51.04
		92	0.00	-20.08	0.00	54.94	0.00	-37.97
	5	76	0.00	-8.90	0.00	7.26	0.00	-3.03
		92	0.00	-4.62	0.00	-7.26	0.00	0.81
195	4	92	0.00	4.06	0.00	-28.56	0.00	50.01
		108	0.00	-19.09	0.00	28.56	0.00	-37.97
	5	92	0.00	-6.01	0.00	4.16	0.00	-5.00
		108	0.00	-7.52	0.00	-4.16	0.00	5.79
196	4	108	0.00	1.77	0.00	-7.84	0.00	42.42
		124	0.00	-9.28	0.00	7.84	0.00	-39.55
	5	108	0.00	-2.19	0.00	1.18	0.00	-7.09
		124	0.00	-4.58	0.00	-1.18	0.00	7.71
198	4	29	0.00	22.45	0.00	-83.46	0.00	25.01
		45	0.00	-38.56	0.00	83.46	0.00	6.71
	5	29	0.00	-14.33	0.00	-2.90	0.00	-0.53
		45	0.00	-0.17	0.00	2.90	0.00	-6.83
199	4	45	0.00	22.01	0.00	-71.75	0.00	29.58
		61	0.00	-38.13	0.00	71.75	0.00	1.70
	5	45	0.00	-11.15	0.00	-0.11	0.00	0.66
		61	0.00	-3.35	0.00	0.11	0.00	-4.72
200	4	61	0.00	17.10	0.00	-55.65	0.00	29.74
		77	0.00	-33.21	0.00	55.65	0.00	-3.58
	5	61	0.00	-10.02	0.00	2.08	0.00	-0.38
		77	0.00	-4.48	0.00	-2.08	0.00	-2.50
201	4	77	0.00	10.72	0.00	-37.17	0.00	27.83
		93	0.00	-26.83	0.00	37.17	0.00	-8.30
	5	77	0.00	-8.93	0.00	2.86	0.00	-1.47
		93	0.00	-5.57	0.00	-2.86	0.00	-0.28
202	4	93	0.00	5.73	0.00	-18.41	0.00	24.10
		109	0.00	-21.84	0.00	18.41	0.00	-9.77
	5	93	0.00	-6.76	0.00	2.13	0.00	-2.09
		109	0.00	-7.74	0.00	-2.13	0.00	2.60
203	4	109	0.00	2.38	0.00	-4.94	0.00	15.69
		125	0.00	-10.43	0.00	4.94	0.00	-12.36
	5	109	0.00	-2.41	0.00	0.66	0.00	-3.22
		125	0.00	-4.84	0.00	-0.66	0.00	3.85
205	4	30	0.00	27.72	0.00	-34.03	0.00	19.47
		46	0.00	-44.91	0.00	34.03	0.00	18.30

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	30	0.00	-5.78	0.00	-4.45	0.00	0.80
		46	0.00	-9.70	0.00	4.45	0.00	1.24
206	4	46	0.00	22.25	0.00	-28.11	0.00	17.02
		62	0.00	-39.44	0.00	28.11	0.00	15.06
	5	46	0.00	-7.39	0.00	-2.01	0.00	-0.39
		62	0.00	-8.09	0.00	2.01	0.00	0.75
207	4	62	0.00	15.24	0.00	-21.07	0.00	13.72
		78	0.00	-32.44	0.00	21.07	0.00	11.07
	5	62	0.00	-8.44	0.00	-0.27	0.00	-1.24
		78	0.00	-7.03	0.00	0.27	0.00	0.51
208	4	78	0.00	7.24	0.00	-13.35	0.00	9.77
		94	0.00	-24.43	0.00	13.35	0.00	6.70
	5	78	0.00	-8.88	0.00	0.69	0.00	-1.74
		94	0.00	-6.59	0.00	-0.69	0.00	0.54
209	4	94	0.00	-0.79	0.00	-5.66	0.00	5.52
		110	0.00	-16.40	0.00	5.66	0.00	2.60
	5	94	0.00	-8.64	0.00	0.97	0.00	-1.80
		110	0.00	-6.84	0.00	-0.97	0.00	0.87
210	4	110	0.00	-1.07	0.00	-1.27	0.00	1.79
		126	0.00	-7.52	0.00	1.27	0.00	-0.11
	5	110	0.00	-4.07	0.00	0.46	0.00	-1.19
		126	0.00	-3.66	0.00	-0.46	0.00	1.08
106	4	1	0.00	-6.35	0.00	-3.63	0.00	0.00
		16	0.00	5.32	0.00	3.63	0.00	-3.04
	5	1	0.00	-1.07	0.00	0.18	0.00	0.00
		16	0.00	0.14	0.00	-0.18	0.00	-0.31
113	4	2	0.00	-2.74	0.00	-3.73	0.00	0.00
		17	0.00	1.17	0.00	3.73	0.00	-1.02
	5	2	0.00	-0.25	0.00	0.25	0.00	0.00
		17	0.00	-1.16	0.00	-0.25	0.00	0.24
120	4	3	0.00	-191.48	0.00	-51.66	0.00	0.00
		18	0.00	189.37	0.00	51.66	0.00	-99.02
	5	3	0.00	125.20	0.00	37.12	0.00	0.00
		18	0.00	-127.10	0.00	-37.12	0.00	65.60
127	4	4	0.00	-149.68	0.00	-227.19	0.00	0.00
		19	0.00	147.03	0.00	227.19	0.00	-77.14
	5	4	0.00	56.21	0.00	168.73	0.00	0.00
		19	0.00	-58.59	0.00	-168.73	0.00	29.85
134	4	5	0.00	-99.66	0.00	-220.77	0.00	0.00
		20	0.00	96.47	0.00	220.77	0.00	-50.99

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	5	0.00	19.83	0.00	165.72	0.00	0.00
		20	0.00	-22.71	0.00	-165.72	0.00	11.06
141	4	6	0.00	-88.82	0.00	-211.18	0.00	0.00
		21	0.00	85.09	0.00	211.18	0.00	-45.22
	5	6	0.00	8.87	0.00	155.07	0.00	0.00
		21	0.00	-12.23	0.00	-155.07	0.00	5.49
148	4	7	0.00	-78.97	0.00	-199.06	0.00	0.00
		22	0.00	74.70	0.00	199.06	0.00	-39.95
	5	7	0.00	-1.87	0.00	137.90	0.00	0.00
		22	0.00	-1.98	0.00	-137.90	0.00	0.03
155	4	8	0.00	-68.83	0.00	-186.14	0.00	0.00
		23	0.00	64.01	0.00	186.14	0.00	-34.54
	5	8	0.00	-11.97	0.00	116.54	0.00	0.00
		23	0.00	7.64	0.00	-116.54	0.00	-5.10
162	4	9	0.00	-58.65	0.00	-173.72	0.00	0.00
		24	0.00	53.30	0.00	173.72	0.00	-29.11
	5	9	0.00	-20.33	0.00	93.19	0.00	0.00
		24	0.00	15.51	0.00	-93.19	0.00	-9.32
169	4	10	0.00	-48.08	0.00	-162.11	0.00	0.00
		25	0.00	42.18	0.00	162.11	0.00	-23.47
	5	10	0.00	-26.36	0.00	69.49	0.00	0.00
		25	0.00	21.06	0.00	-69.49	0.00	-12.33
176	4	11	0.00	-36.27	0.00	-150.48	0.00	0.00
		26	0.00	29.83	0.00	150.48	0.00	-17.19
	5	11	0.00	-29.74	0.00	46.63	0.00	0.00
		26	0.00	23.95	0.00	-46.63	0.00	-13.96
183	4	12	0.00	-21.98	0.00	-136.87	0.00	0.00
		27	0.00	15.00	0.00	136.87	0.00	-9.61
	5	12	0.00	-30.03	0.00	25.68	0.00	0.00
		27	0.00	23.75	0.00	-25.68	0.00	-13.98
190	4	13	0.00	-3.45	0.00	-117.88	0.00	0.00
		28	0.00	-4.06	0.00	117.88	0.00	0.16
	5	13	0.00	-26.33	0.00	7.97	0.00	0.00
		28	0.00	19.57	0.00	-7.97	0.00	-11.93
197	4	14	0.00	21.09	0.00	-87.95	0.00	0.00
		29	0.00	-29.15	0.00	87.95	0.00	13.06
	5	14	0.00	-16.77	0.00	-4.29	0.00	0.00
		29	0.00	9.52	0.00	4.29	0.00	-6.83
204	4	15	0.00	32.92	0.00	-37.02	0.00	0.00
		30	0.00	-41.51	0.00	37.02	0.00	19.35

MEMBER END FORCES STRUCTURE TYPE = FLOOR

ALL UNITS ARE -- MTON MET

MEMB	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	5	15	0.00	-2.23	0.00	-6.16	0.00	0.00
		30	0.00	-5.51	0.00	6.16	0.00	0.85

********** END OF LATEST ANALYSIS RESULT **********

74. PRINT SUPPORT REACTIONS

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = FLOOR

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
1	4	0.00	-6.35	0.00	-3.63	0.00	0.00
	5	0.00	-1.07	0.00	0.18	0.00	0.00
2	4	0.00	-2.74	0.00	-3.73	0.00	0.00
	5	0.00	-0.25	0.00	0.25	0.00	0.00
3	4	0.00	-191.48	0.00	-51.66	0.00	0.00
	5	0.00	125.20	0.00	37.12	0.00	0.00
4	4	0.00	-149.68	0.00	-227.19	0.00	0.00
	5	0.00	56.21	0.00	168.73	0.00	0.00
5	4	0.00	-99.66	0.00	-220.77	0.00	0.00
	5	0.00	19.83	0.00	165.72	0.00	0.00
6	4	0.00	-88.82	0.00	-211.18	0.00	0.00
	5	0.00	8.87	0.00	155.07	0.00	0.00
7	4	0.00	-78.97	0.00	-199.06	0.00	0.00
	5	0.00	-1.87	0.00	137.90	0.00	0.00
8	4	0.00	-68.83	0.00	-186.14	0.00	0.00
	5	0.00	-11.97	0.00	116.54	0.00	0.00
9	4	0.00	-58.65	0.00	-173.72	0.00	0.00
	5	0.00	-20.33	0.00	93.19	0.00	0.00
10	4	0.00	-48.08	0.00	-162.11	0.00	0.00
	5	0.00	-26.36	0.00	69.49	0.00	0.00
11	4	0.00	-36.27	0.00	-150.48	0.00	0.00
	5	0.00	-29.74	0.00	46.63	0.00	0.00
12	4	0.00	-21.98	0.00	-136.87	0.00	0.00
	5	0.00	-30.03	0.00	25.68	0.00	0.00
13	4	0.00	-3.45	0.00	-117.88	0.00	0.00
	5	0.00	-26.33	0.00	7.97	0.00	0.00
14	4	0.00	21.09	0.00	-87.95	0.00	0.00
	5	0.00	-16.77	0.00	-4.29	0.00	0.00
15	4	0.00	32.92	0.00	-37.02	0.00	0.00
	5	0.00	-2.23	0.00	-6.16	0.00	0.00
31	4	0.00	-32.71	0.00	-52.03	0.00	-25.08
	5	0.00	-20.61	0.00	-12.45	0.00	-3.87
47	4	0.00	-74.60	0.00	-143.14	0.00	-21.36
	5	0.00	-41.37	0.00	-28.18	0.00	-1.87
63	4	0.00	-99.51	0.00	-215.97	0.00	-16.93
	5	0.00	-48.97	0.00	-34.84	0.00	-0.49
79	4	0.00	-115.10	0.00	-269.78	0.00	-11.88
	5	0.00	-51.81	0.00	-36.19	0.00	0.34
95	4	0.00	-121.20	0.00	-302.93	0.00	-6.47
	5	0.00	-51.53	0.00	-34.49	0.00	0.70
111	4	0.00	-110.41	0.00	-313.63	0.00	-1.18
	5	0.00	-46.33	0.00	-30.90	0.00	0.71
127	4	0.00	-52.84	0.00	-156.98	0.00	0.00
	5	0.00	-21.41	0.00	-14.74	0.00	0.00
112	4	0.00	0.00	0.00	0.00	0.00	-8.66
	5	0.00	0.00	0.00	0.00	0.00	6.48
113	4	0.00	0.00	0.00	0.00	0.00	-7.87
	5	0.00	0.00	0.00	0.00	0.00	5.74
114	4	0.00	0.00	0.00	0.00	0.00	-146.34
	5	0.00	0.00	0.00	0.00	0.00	84.12

SUPPORT REACTIONS -UNIT MTON MET STRUCTURE TYPE = FLOOR

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
115	4	0.00	0.00	0.00	0.00	0.00	-644.91
	5	0.00	0.00	0.00	0.00	0.00	381.98
116	4	0.00	0.00	0.00	0.00	0.00	-539.46
	5	0.00	0.00	0.00	0.00	0.00	293.89
117	4	0.00	0.00	0.00	0.00	0.00	-441.70
	5	0.00	0.00	0.00	0.00	0.00	214.56
118	4	0.00	0.00	0.00	0.00	0.00	-360.24
	5	0.00	0.00	0.00	0.00	0.00	153.33
119	4	0.00	0.00	0.00	0.00	0.00	-290.43
	5	0.00	0.00	0.00	0.00	0.00	106.37
120	4	0.00	0.00	0.00	0.00	0.00	-228.78
	5	0.00	0.00	0.00	0.00	0.00	70.75
121	4	0.00	0.00	0.00	0.00	0.00	-173.11
	5	0.00	0.00	0.00	0.00	0.00	44.56
122	4	0.00	0.00	0.00	0.00	0.00	-122.52
	5	0.00	0.00	0.00	0.00	0.00	26.30
123	4	0.00	0.00	0.00	0.00	0.00	-77.39
	5	0.00	0.00	0.00	0.00	0.00	14.56
124	4	0.00	0.00	0.00	0.00	0.00	-39.55
	5	0.00	0.00	0.00	0.00	0.00	7.71
125	4	0.00	0.00	0.00	0.00	0.00	-12.36
	5	0.00	0.00	0.00	0.00	0.00	3.85
126	4	0.00	0.00	0.00	0.00	0.00	-0.11
	5	0.00	0.00	0.00	0.00	0.00	1.08

********** END OF LATEST ANALYSIS RESULT **********

75. FINISH

********** END OF STAAD-III **********

SIEGRIST Y MORENO, S.L.

Proyectos de Ingeniería

Comportamiento Dinámico

Viaducto sobre el Torrente del Bó
Luces de cálculo 22-28-28-22m

L.A.V. Madrid-Barcelona-Frontera Francesa
Tramo: Costa Blanca-Conexión del Vallés

Madrid, 23 de julio de 2003

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1. Descripción del cálculo dinámico

1.1. Introducción

El procedimiento más simplicado de cálculo, basado en el cálculo estático afectado de un coeficiente de impacto, puede no resultar del lado de la seguridad para velocidades superiores a 220 km/h y tipologías singulares.

Los fenómenos dinámicos que se producen por el tráfico ferroviario se deben, fundamentalmente, a las cargas verticales móviles producidas por las ruedas de las composiciones. También contribuye la existencia de irregularidades de la vía o de las propias ruedas que causan variaciones en las cargas por eje, aunque estos efectos se tienen en cuentan mediante la formulación empírica propuesta en el borrador de la IAPF y no mediante un cálculo dinámico específico.

Generalmente las cargas de los vehículos se encuentran a unos espaciamientos determinados a lo largo de la longitud de la composición lo que, a velocidades de circulación constantes, llega a convertirse en excitaciones periódicas. De esta forma, además del efecto dinámico inherente al paso de cargas por un puente a velocidad constante, hay que añadir los posibles efectos resonantes debidos a la entrada rítmica de las cargas. La evaluación de los fenómenos asociados a la resonancia se puede realizar mediante la obtención de uno o más espaciamientos característicos, λ_k, que dependen de la distribución espacial de cargas de un tren. El riesgo de resonancia se producirá a las velocidades para las que estos espaciamientos sean múltiplos de la longitud de onda principal, v/f_o.

$$\frac{v}{f_o} = \frac{\lambda_k}{i} \quad i = 1, 2...$$

Todo lo anteriormente expuesto pone de manifiesto la necesidad de realizar cálculos dinámicos adicionales para garantizar la seguridad e idoneidad del puente proyectado para el paso de composiciones ferroviarias a gran velocidad.

1.2. Cálculo dinámico

El método elegido para abordar el análisis dinámico de los puentes ha sido la *Integración directa en el tiempo sin interacción vehículo-estructura.* Se ha optado por este método por las siguientes razones:

- Método válido para todo rango de velocidades;
- No presenta limitaciones de frecuencias y masas mínimas;
- Es aplicable tanto a puentes isostáticos como hiperestáticos;
- Incluye posibles fenómenos resonantes;
- Los cálculos dinámicos a realizar son de relativa poca complejidad.

El método utilizado se basa en la descomposición modal de la estructura y la combinación de respuestas modales frente a las cargas móviles. No se tiene en cuenta la interacción vehículo-estructura ya que generalmente esto conduce a una disminución de los esfuerzos dinámicos sólo apreciable en luces menores de los 30 m.

El puente queda definido por las siguientes variables que representan todas las características geométricas y mecánicas de la estructura necesarias para el cálculo:

- $\phi_i(x)$: i-ésima forma modal;
- $EI(x)$: rigidez dinámica a flexión $[kN\ m^2]$;
- $\rho(x)$: masa [ton/m];
- ω_i: i-ésima frecuencia propia [rad/seg] ($\omega_i = f_i 2\pi$);
- ξ_i: i-ésimo índice de amortiguamiento modal;
- $i = 1...n$: número de modos de vibración utilizados;
- L: Longitud del puente.

Si se considera la respuesta a una carga única que recorre el puente con una velocidad v, la ecuación dinámica de la elástica es:

$$\rho(x)\frac{\partial^2 u}{\partial t^2} + \frac{\partial^2}{\partial t^2}[EI(x)\frac{\partial^2 u}{\partial x^2}] = p(x,t) \tag{1}$$

Utilizando las técnicas del análisis modal[1], sólo aplicable bajo comportamiento lineal del sistema, se obtienen los modos de vibración $\phi_i(x)$ y las frecuencias correspondientes a estos modos, ω_i. Se admite entonces la descomposición de la respuesta en desplazamientos en función de las formas modales $\phi_i(x)$:

$$u(x,t) = \sum_{i=1}^{n} y_i(t)\phi_i(x) \tag{2}$$

Sustituyendo en la ecuación (1), se consigue desacoplar las ecuaciones dinámicas y obtener la ecuación para cada modo de forma separada. Esto equivale, para cada modo de vibración, a un problema de un grado de libertad:

$$M_i\ddot{y}_i + K_i y_i = P_i(t) \tag{3}$$

donde:

M_i i-ésima masa generalizada,

$$M_i = \int_0^L \rho(x)\phi_i^2(x)dx$$

K_i i-ésima rigidez generalizada,

$$K_i = \int_0^L \phi_i(x)[EI(x)\phi_i''(x)]''dx$$

$P_i(t)$ i-ésima carga generalizada. Para una carga puntual F móvil, con velocidad de circulación constante v, adopta el siguiente valor:

$$P_i(t) = \phi_i(vt)F$$

[1] A partir de la matriz de rigidez condensada del puente y de la matriz de masas concentradas se resuelve el problema generalizado de autovalores, $|K - \Omega^2 M|\Phi = 0$, que arroja como autovectores las formas modales $\phi_i(x)$ y como autovalores las frecuencias propias al cuadrado ω_i^2

y_i coordenada generalizada (amplitud del modo i).

Si se añade la consideración del amortiguamiento estructural del puente, se obtiene:

$$M_i\ddot{y}_i + C_i\dot{y}_i + K_i y_i = \phi_i(vt)F \tag{4}$$

Donde C_i es el i-ésimo amortiguamiento generalizado y está definido a partir del índice de amortiguamiento modal, ξ_i, según la relación:

$$C_i = 2\xi_i\omega_i M_i$$

La ecuación (4) puede escribirse también de la forma:

$$\ddot{y}_i + 2\xi_i\omega_i\dot{y}_i + \omega_i^2 y_i = \phi_i(vt)\frac{F}{M_i}$$

Se entiende que para $t < 0$ o $t > L/v$ y todas las i: $\phi_i = 0$.

Podemos extender el planteamiento al caso de un tren real de cargas en el que el número total de ejes que integran la composición es n_F. Cada carga está caracterizada por su valor F_k y su distancia, d_k, a la entrada del puente en el instante inicial. En este caso las ecuaciones desacopladas para cada modo i tienen la siguientes expresión:

$$\ddot{y}_i + 2\xi_i\omega_i\dot{y}_i + \omega_i^2 y_i = \sum_{k=1}^{n_F}\phi_i(vt - d_k)\frac{F_k}{M_i}$$

Análogamente al caso anterior, podemos decir que para $(vt-l_k) < 0$ o $(vt-l_k) > L$ y todas las i: $\phi_i = 0$, que corresponden a las situaciones de carga que no ha llegado aún al puente y carga que ya lo ha rebasado, respectivamente.

La respuesta en desplazamientos, velocidades y aceleraciones para un punto dado, x_f, volverá a calcularse de la siguiente manera:

$$\delta_f(t) = u(x_f, t) = \sum_{i=1}^{n} y_i(t)\phi_i(x_f)$$

$$\dot{\delta}_f(t) = \dot{u}(x_f, t) = \sum_{i=1}^{n} \dot{y}_i(t)\phi_i(x_f)$$

$$\ddot{\delta}_f(t) = \ddot{u}(x_f, t) = \sum_{i=1}^{n} \ddot{y}_i(t)\phi_i(x_f)$$

La única diferencia que presenta el tren de cargas respecto al caso de carga aislada se encuentra en la carga modal; con un tren de cargas, la carga modal asociada que se utiliza para resolver la ecuación de los factores de participación es la suma de la contribución de las cargas que, en cada instante, se encuentran sobre el puente.

1.3. Resultados

Los cálculos dinámicos deben evaluar la situación más desfavorable desde el punto de vista de la resonancia. Para ello, será necesario realizar distintos cálculos a diversas velocidades de paso del tren, efectuando un barrido desde la

velocidad mínima 5 m/s -que puede considerarse como velocidad cuasiestática- hasta la velocidad máxima previsible, V_{max}.

Se adopta un valor para V_{max} de 120 m/s. Este valor cumple que $V_{max} > 1,2V_o$, donde $V_o = 350$ km/h es la velocidad máxima de proyecto de la línea considerada. El incremento de velocidad considerado entre distintos cálculos es de 2,5 m/s, valor inferior al límite de 10 km/h propuesto por el borrador de la nueva *Instrucción de acciones a considerar en el proyecto de puentes de ferrocarril (IAPF).*

Los cálculos realizados consideran los trenes definidos en el *Anexo F del Eurocódigo 1 parte 3* pues son representativos de los trenes de alta velocidad reales susceptibles de circular por la estructura. Estos trenes son:

- Tipo 3, tren de pasajeros de alta velocidad.
- Tipo 4, tren de pasajeros de alta velocidad.

Como resultado del barrido de velocidades y composiciones ferroviarias que circulan por la línea se han obtenido los siguientes datos:

- $\delta^{real}_{din,ideal}$ flechas máximas del puente en el rango de velocidades entre 5 m/s y 120 m/s.
- v_{max} valor de la velocidad vertical máxima del puente en el rango de velocidades entre 5 m/s y 120 m/s.
- a_{max} valor de la aceleración vertical máxima del puente en el rango de velocidades entre 5 m/s y 120 m/s.

A partir de los resultados obtenidos[2] se comprueba que las aceleraciones máximas obtenidas no superan los límites establecidos. Además, estableciendo una relación directa entre el factor de amplificación dinámica en desplazamientos verticales y en esfuerzos, se compara el coeficiente de impacto obtenido para la carga real con el considerado en los modelos de carga estática. También se compara la flecha máxima obtenida según los modelos estáticos con la flecha máxima dinámica con objeto de comprobar que situación de cálculo es condicionante para los *Estados Límite de Servicio de Deformaciones.*

2. Definición de la estructura

El Viaducto sobre el Torrente del Bó del tramo Cost Blanca - COnexión del Vallés, en la Línea de Alta Velocidad Madrid-Zaragoza-Barcelona-Frontera Francesa, consta de cuatro tramos contínuos de luces iguales a 22,00 – 28,00 – 28,00 – 22,00 metros y se realiza con un tablero único que constituye una viga hiperestática de sección en doble viga artesa de canto constante igual a 2.190 metros en el eje y coronación en bombeo del 0,02. El ancho del tablero es constante de 14.00 metros.

[2]Los resultados obtenidos se multiplican previamente por un coeficiente que tiene en cuenta las irregularidades de la vía.

2.1. Hipótesis consideradas

Las hipótesis adoptadas en los cálculos de cara a simplificar los mismos sin una pérdida apreciable de precisión son:

- Se adopta un modelo de viga hiperestática con las siguientes características:
  - Sólo se tienen en cuenta los grados de libertad de desplazamiento vertical de la viga.
  - No se tiene en cuenta la torsión generada por el movimiento del tren sobre una vía.
  - Se supone la inercia bruta de la sección sin fisurar, ya que para las cargas actuantes la sección se encuentra comprimida o en todo caso por debajo de la tensión de rotura por tracción del hormigón.
  - El módulo de elasticidad del hormigón adoptado para las cargas instantáneas o rápidamente variables del paso de los trenes es:

$$E = 10000\sqrt[3]{f_{cm}} \quad \text{MPa}$$

    donde f_{cm} es la resistencia media del hormigón definida como $f_{cm} = f_{ck} + 8$ MPa y donde f_{ck} es la resistencia característica del hormigón.
- No se considera la interacción vehículo-estructura como ya se mencionó en la sección 1.2.
- Sólo se consideran los modos por debajo de los 30 Hz.
- Para cada velocidad de barrido se realiza la integración directa en el tiempo. El tiempo de cálculo es el de pasada del tren más un tiempo adicional ($\approx 6\ seg$) que coge la respuesta de la estructura cuando el tren está fuera de ella.
- Se adopta el mismo amortiguamiento para todos los modos de vibración.

2.2. Características mecánicas

El puente se ha discretizado en 10 divisiones por vano con objeto de obtener los modos de vibración con una precisión adecuada para el cálculo. En el Cuadro 1 se recogen las características mecánicas de la sección considerada en el análisis dinámico del puente.

Canto $[m]$	Área $[m^2]$	Inercia $[m^4]$
2.190	10.60	2.7500

Cuadro 1: *Características mecánicas de las secciones.*

La densidad utilizada para calcular la masa del puente es, $\rho = 2{,}5$ ton$/m^3$, siendo la masa por unidad de longitud de tablero:

$$m(x) = \rho A(x) + \text{cp}$$

donde, $A(x)$, es el área de la sección a lo largo de la directriz x del tablero y $cp = 14{,}17$ ton$/m$ es la masa de la carga permanente (balasto real, traviesas, carriles, barandillas, paseos, etc.) por unidad de longitud.

El módulo de elasticidad considerado en los cálculos para un hormigón $f_{ck} = 50$ MPa es:

$$E = 8500\sqrt[3]{f_{cm}} \quad = 8500\sqrt[3]{58} \approx 32902 \text{ MPa}$$

2.3. Parámetros dinámicos

Los parámetros dinámicos considerados en el cálculo son dos:

- El valor del amortiguamiento, ξ, para un puente de hormigón estructural en función de la longitud de vanos del puente, $L[m]$, es:

$$\xi[\%] = \begin{cases} 2{,}0 + 0{,}1(20 - L) & L < 20, \\ 2{,}0 & L \geq 20. \end{cases}$$

  El amortiguamiento adoptado para el puente es: $\xi = 0{,}02$.
- El paso de tiempo adoptado para la integración directa en el tiempo debe ser lo suficientemente pequeño como para recoger con suficiente detalle la variación de carga. Un valor que recoge con detalle estas variaciones es:

$$\Delta t = \frac{1}{10 \times f_n}$$

  siendo f_n la frecuencia máxima utilizada, que en nuestro caso es 30 Hz y da como paso de integración para el cálculo: $\Delta t = 0{,}003$ seg.

3. Definición de las composiciones

Los composiciones ferroviarias consideradas en el análisis dinámico son:

1. Tipo 3, tren de pasajeros de alta velocidad.
2. Tipo 4, tren de pasajeros de alta velocidad.

A continuación se presenta para cada composición la distribución espacial de cargas, los espaciamientos característicos, λ_k, que permiten una aproximación teórica a las velocidades de posible resonancia y la carga uniforme equivalente del tren real.

3.1. Tren 3 - Eurocódigo 1

En el Cuadro 2 se encuentra la distribución espacial de cargas de la composición, en ella se muestran por columnas los siguientes valores:

- l_k, distancia a la cabeza de la composición en metros.
- F_k, carga por eje en kilonewtons.

Se observa que una vez pasadas las locomotoras delantera y trasera de la composición las cargas presentan la misma distribución cada 4 ejes formando 13 grupos de ejes de $21{,}5m$ separados $5{,}0m$. La distribución de ejes de cada grupo es $2{,}5 - 16{,}5 - 2{,}5m$.

La presente composición consta de 60 ejes distribuidos a lo largo de una longitud total de $384{,}520m$ por tanto, la carga uniforme equivalente será:

$$q_{uniforme} = \frac{200 \times 8 + 150 \times 52}{384{,}520} \frac{[kN]}{[m]} = 24{,}38\ [kN/m]$$

l_k $[m]$	F_k $[kN]$	l_k $[m]$	F_k $[kN]$	l_k $[m]$	F_k $[kN]$
0.000	200	124.510	150	256.510	150
3.000	200	127.010	150	259.010	150
11.460	200	143.510	150	275.510	150
14.460	200	146.010	150	278.010	150
18.910	150	150.910	150	282.910	150
21.410	150	153.410	150	285.410	150
37.910	150	169.910	150	301.910	150
40.410	150	172.410	150	304.410	150
45.310	150	177.310	150	309.310	150
47.810	150	179.810	150	311.810	150
64.310	150	196.310	150	328.310	150
66.810	150	198.810	150	330.810	150
71.710	150	203.710	150	335.710	150
74.210	150	206.210	150	338.210	150
90.710	150	222.710	150	354.710	150
93.210	150	225.210	150	357.210	150
98.110	150	230.110	150	361.660	200
100.610	150	232.610	150	364.660	200
117.110	150	249.110	150	373.120	200
119.610	150	251.610	150	376.120	200

Cuadro 2: *Cargas por eje del Tren 3 Eurocódigo 1.*

3.2. Tren 4 - Eurocódigo 1

En el Cuadro 3 se encuentra la distribución espacial de cargas de la composición, en ella se muestran por columnas los siguientes valores:

- l_k, distancia a la cabeza de la composición en metros.
- F_k, carga por eje en kilonewtons.

Se observa que una vez pasadas las locomotoras delantera y trasera de la composición las cargas presentan la misma distribución cada 2 ejes formando 8 grupos de ejes de $15{,}7m$ separados $3{,}0m$.

La presente composición consta de 30 ejes distribuidos a lo largo de una longitud total de $237{,}600m$ por tanto, la carga uniforme equivalente será:

$$q_{u_{equi}} = \frac{170 \times 30}{237{,}600} \frac{[kN]}{[m]} = 21{,}46\ [kN/m]$$

l_k $[m]$	F_k $[kN]$	l_k $[m]$	F_k $[kN]$	l_k $[m]$	F_k $[kN]$
0.000	170	76.400	170	169.900	170
3.000	170	79.400	170	172.900	170
14.000	170	95.100	170	188.600	170
17.000	170	98.100	170	191.600	170
20.300	170	113.800	170	207.300	170
23.300	170	116.800	170	210.300	170
39.000	170	132.500	170	213.600	170
42.000	170	135.500	170	216.600	170
57.700	170	151.200	170	227.600	170
60.700	170	154.200	170	230.600	170

Cuadro 3: *Cargas por eje del Tren 4 Eurocódigo 1.*

4. Resultados

4.1. Formas modales consideradas

En el Cuadro 4 se recogen los modos considerados en el cálculo definidos mediante los siguientes parámetros:

- ω_i frecuencia circular en rad/s.
- f_i frecuencia en Hz obtenida como $\frac{\omega_i}{2\pi}$.
- T_i periodo en segundos $(1/f_i)$.
- r_z factor de participación de la masa del puente (peso propio y carga permanente) para cada modo.

Modo	ω_i [rad/s]	f_i [Hz]	T_i $[s]$	r_z
1	24.84	3.9541	0.2529	0.0
2	33.87	5.3903	0.1855	1.2
3	46.03	7.3255	0.1365	0.0
4	51.13	8.1376	0.1229	77.4
5	95.72	15.2337	0.0656	0.0
6	116.12	18.4813	0.0541	0.0
7	154.40	24.5736	0.0407	0.0
8	159.78	25.4304	0.0393	0.1

Cuadro 4: *Modos considerados en el cálculo.*

En las Figuras 1 a 8 se muestran las formas modales consideradas en el cálculo.

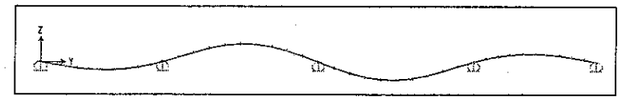

Figura 1: *Modo 1. Periodo* $T_1 = 0{,}2529$ *segundos*

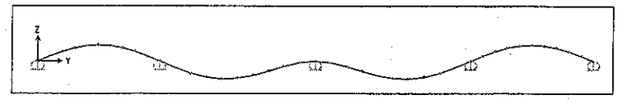

Figura 2: *Modo 2. Periodo* $T_2 = 0{,}1855$ *segundos*

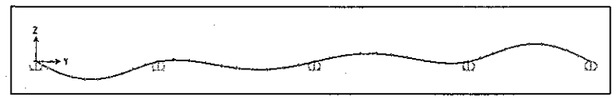

Figura 3: *Modo 3. Periodo* $T_3 = 0{,}1365$ *segundos*

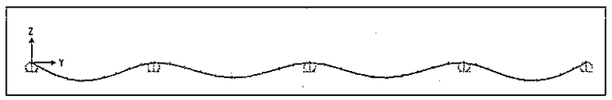

Figura 4: *Modo 4. Periodo* $T_4 = 0{,}1229$ *segundos*

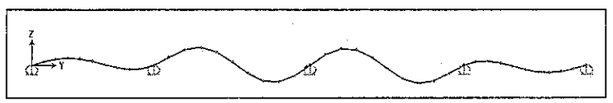

Figura 5: *Modo 5. Periodo* $T_5 = 0{,}0656$ *segundos*

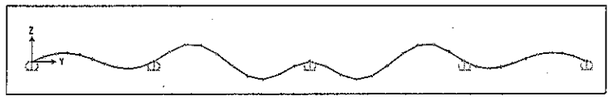

Figura 6: *Modo 6. Periodo* $T_6 = 0{,}0541$ *segundos*

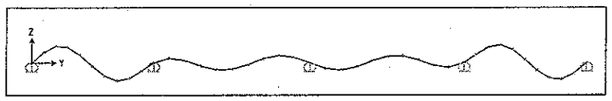

Figura 7: *Modo 7. Periodo* $T_7 = 0{,}0407$ *segundos*

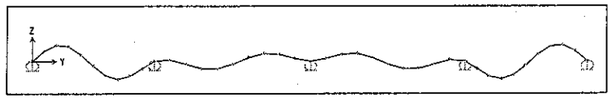

Figura 8: *Modo 8. Periodo* $T_8 = 0{,}0393$ *segundos*

4.2. Barrido de velocidades

A continuación se muestran las envolventes de desplazamientos, velocidades y aceleraciones máximas en los puntos que se detallan a continuación:

- Centro vano 1 (11,00 m): Figuras 9 a 11.
- Centro vano 2 (36,00 m): Figuras 12 a 14.
- Centro vano 3 (64,00 m): Figuras 15 a 17.
- Centro vano 3 (89,00 m): Figuras 18 a 20.

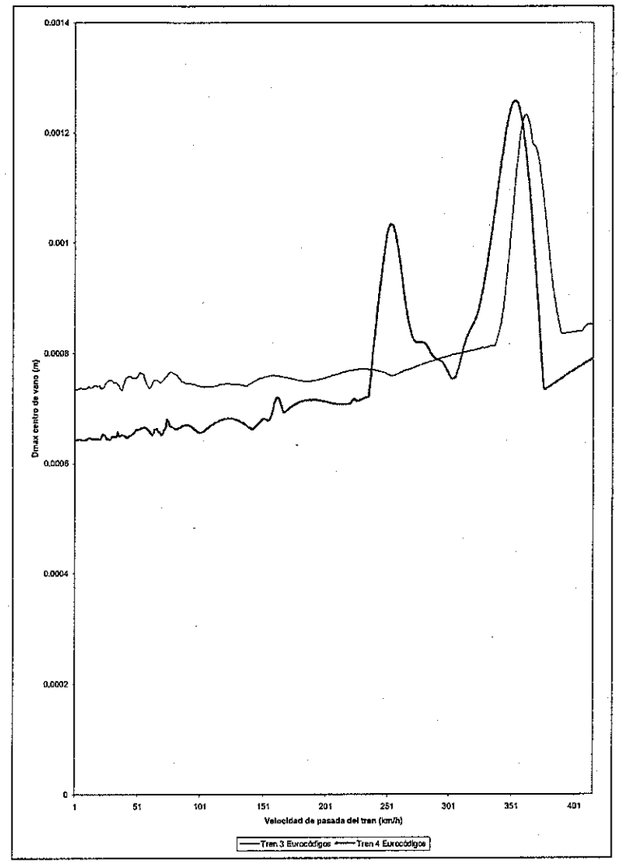

Figura 9: *Envolvente de desplazamientos máximos en el centro del vano 1.*

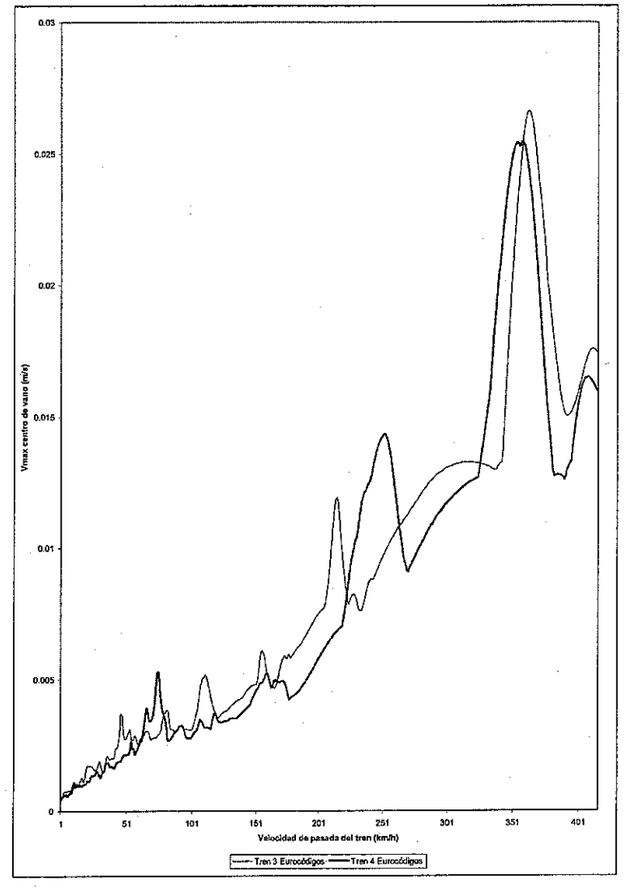

Figura 10: *Envolvente de velocidades máximas en el centro del vano 1.*

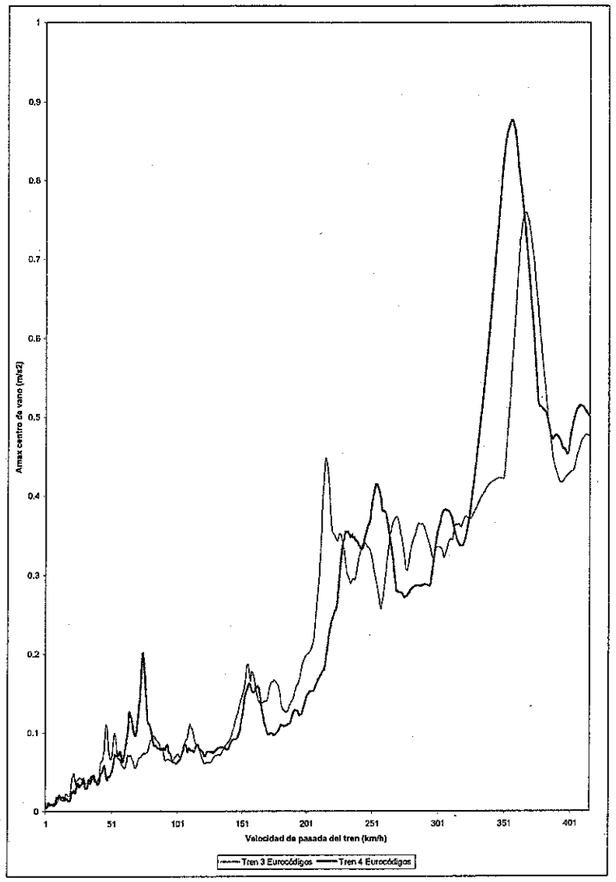

Figura 11: *Envolvente de aceleraciones máximas en el centro del vano 1.*

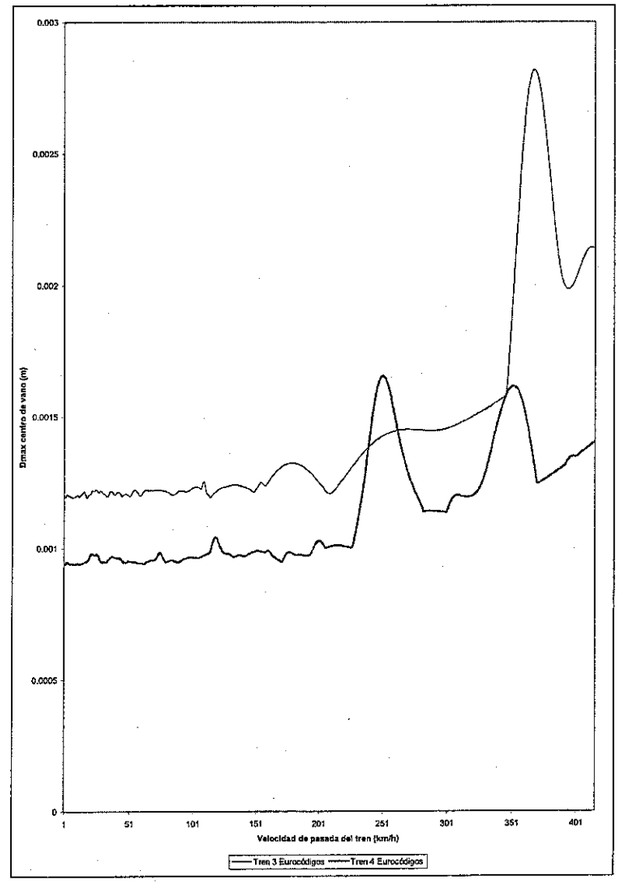

Figura 12: *Envolvente de desplazamientos máximos en el centro del vano 2.*

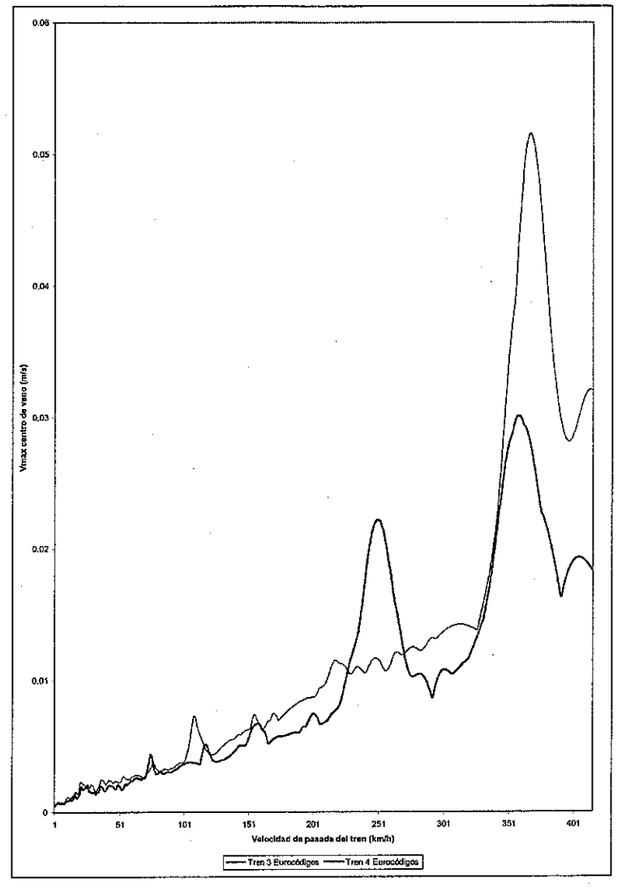

Figura 13: *Envolvente de velocidades máximas en el centro del vano 2.*

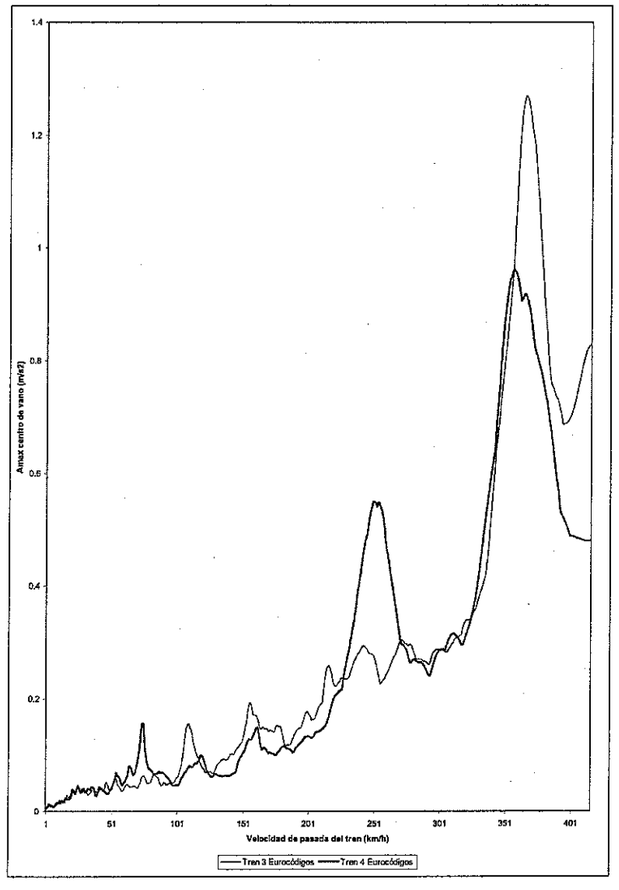

Figura 14: *Envolvente de aceleraciones máximas en el centro del vano 2.*

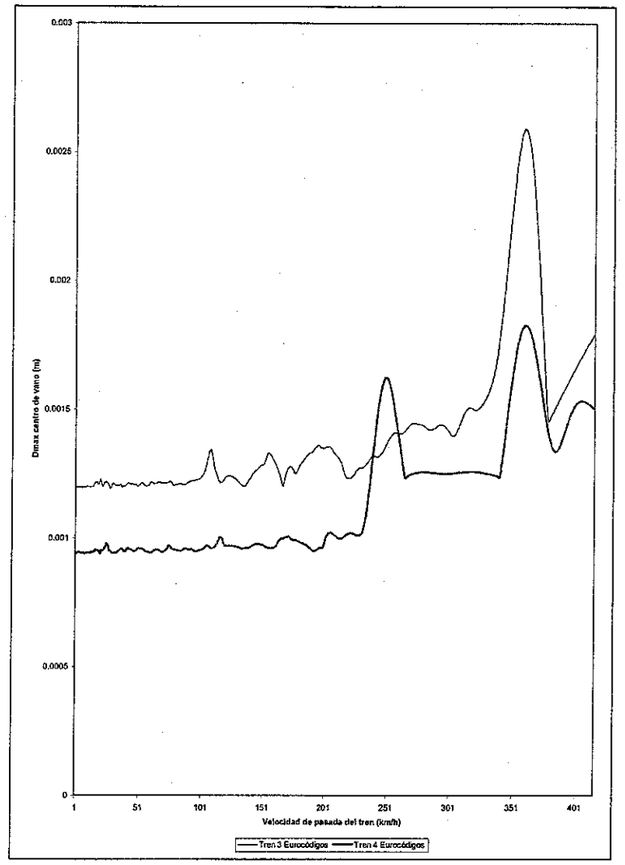

Figura 15: *Envolvente de desplazamientos máximos en el centro del vano 3.*

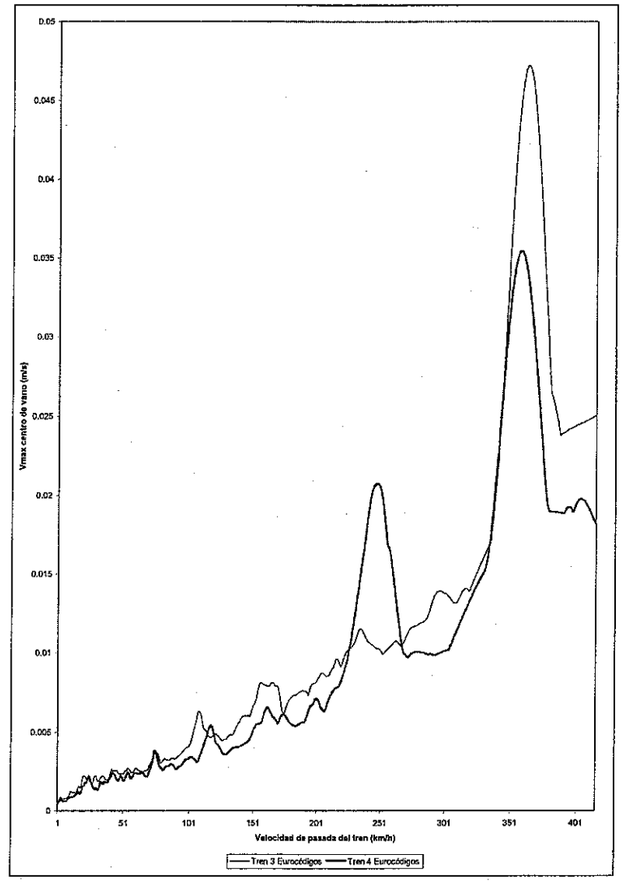

Figura 16: *Envolvente de velocidades máximas en el centro del vano 3.*

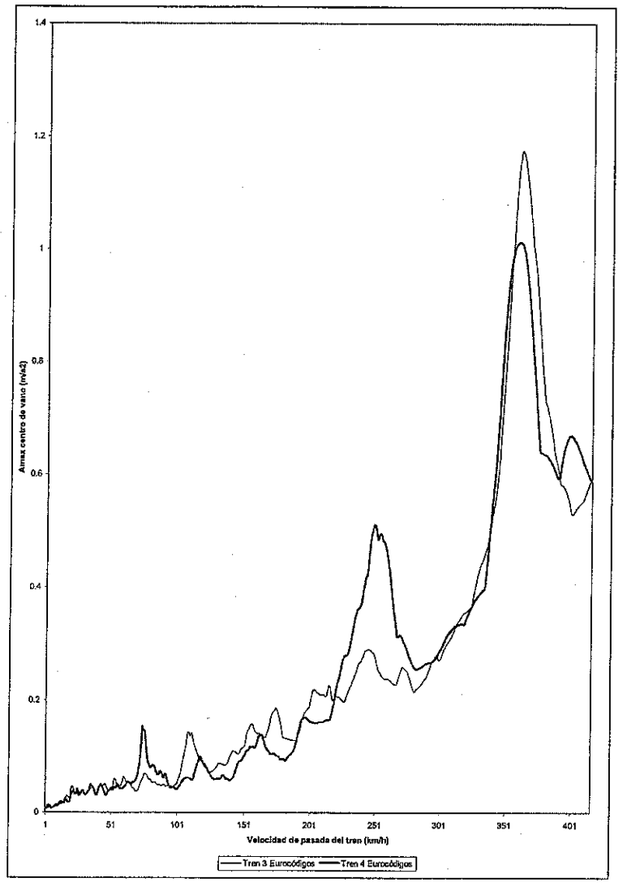

Figura 17: *Envolvente de aceleraciones máximas en el centro del vano 3.*

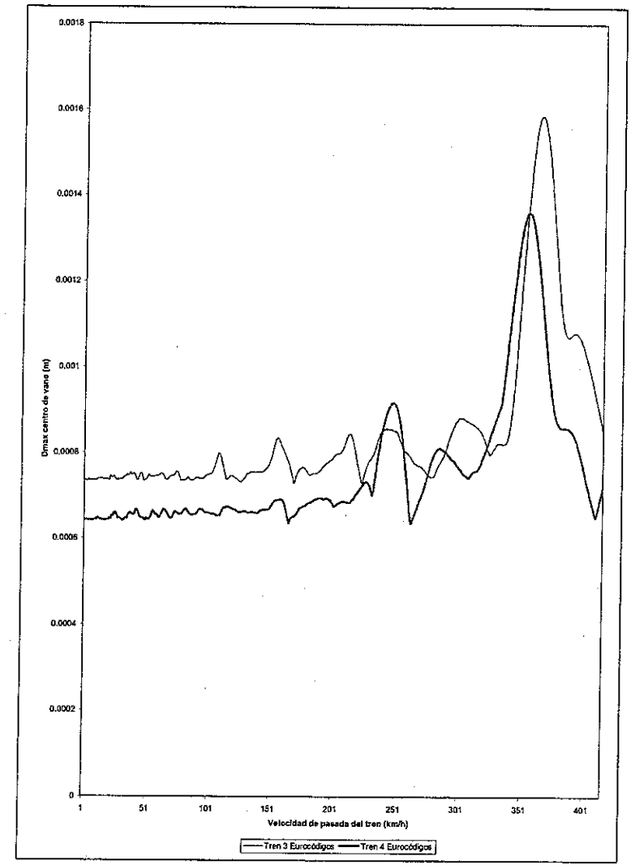

Figura 18: *Envolvente de desplazamientos máximos en el centro del vano 4.*

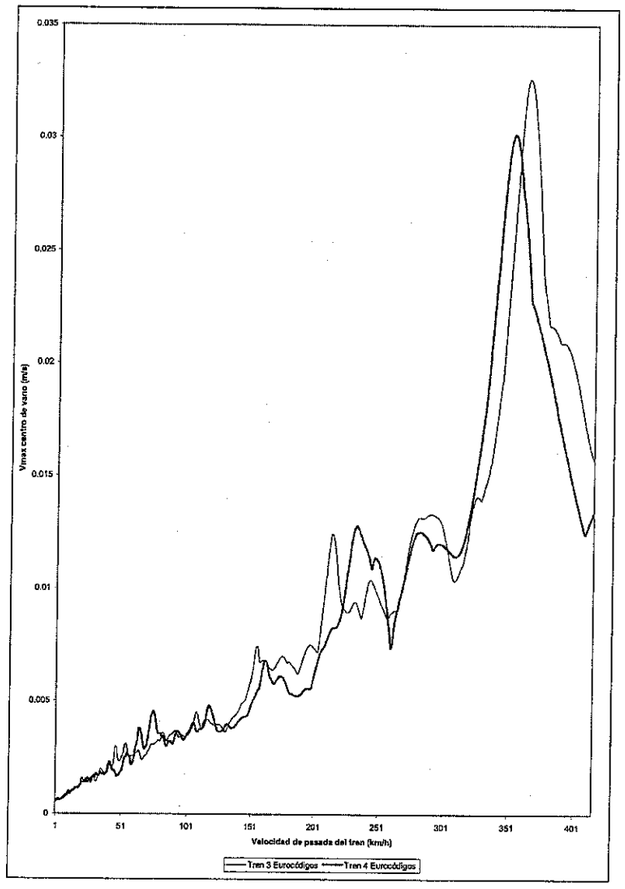

Figura 19: *Envolvente de velocidades máximas en el centro del vano 4.*

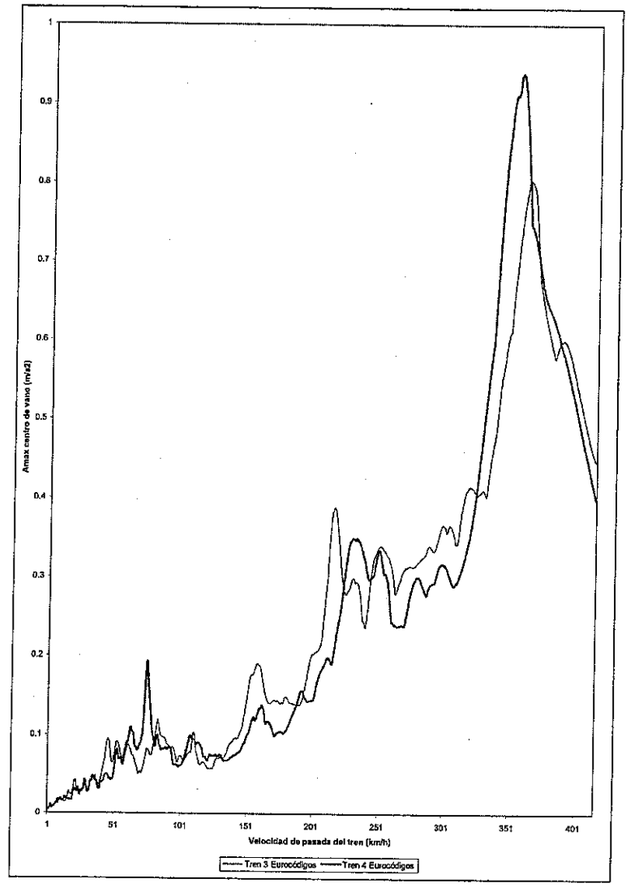

Figura 20: *Envolvente de aceleraciones máximas en el centro del vano 4.*

4.3. Consideraciones sobre las irregularidades del carril

El cálculo realizado mediante la descomposición modal y la integración directa en el tiempo de las respuestas modales frente a las cargas móviles sin interacción vehículo-estructura no tiene en cuenta el incremento de los efectos dinámicos debido a las irregularidades del carril. Para ello se calcula un coeficiente, φ'', de mayoración de los resultados dinámicos para estructura ideal (ver apartado 4.2), mediante las fórmulas empíricas recogidas en el apartado **B.3.2 Cálculo cuasi-estático y coeficiente dinámico** del *Apéndice B del borrador de la IAPF*.

Los desplazamientos máximos se verán afectados por el coeficiente de irregularidades del carril, φ'', de la siguiente forma:

$$\delta_{din,irr} = \delta^{real}_{din,ideal} + 0{,}5\varphi'' \delta^{real}_{est,ideal}$$

donde:

- $\delta_{din,irr}$ flecha dinámica en metros que incluye el efecto de las irregularidades del carril.
- $\delta^{real}_{din,ideal}$ flecha dinámica producida por el paso de los trenes reales sobre una estructura ideal sin irregularidades en los carriles.
- $\delta^{real}_{est,ideal}$ flecha dinámica producida por el paso de los trenes reales a 5 km/h sobre la estructura supuesta ideal (sin irregularidades en los carriles).

Las aceleraciones por su parte serán:

$$a_{max,irr} = (1 + 0{,}5\varphi'')a_{max}$$

donde:

- $a_{max,irr}$ aceleración máxima incluyendo el efecto de las irregularidades del carril.
- a_{max} aceleración máxima suponiendo que la estructura es ideal.

El coeficiente 0,5 que afecta a φ'' tiene en consideración el grado de mantenimiento que tendrá el puente, que en líneas de alta velocidad es bueno.

El coeficiente, φ'', se define mediante la siguiente expresión:

$$\varphi'' = \frac{\alpha}{100}\left[56e^{-(\frac{L_\phi}{10})^2} + 50(\frac{f_o L_\phi}{80} - 1)e^{-(\frac{L_\phi}{20})^2}\right] = 0{,}05970$$

donde:

- $\alpha = \min[\frac{V}{22}, 1]$, siendo V la velocidad de proyecto en m/s. En nuestro caso $\alpha = \min[\frac{97{,}22}{22}, 1] = 1$.
- f_o, frecuencia natural fundamental a flexión del puente en Hz. De la tabla 4 se obtiene que $f_o = 8{,}1164$ IIz.
- L_ϕ, longitud determinante. Según el apartado *2.3.3.2.1 del borrador de la IAPF* $L_\phi = 35{,}000\,m$.

4.4. Criterios a verificar

Para garantizar la seguridad del tráfico ferroviario al paso por los puentes, así como el adecuado confort para los pasajeros, es necesario limitar los valores tanto de aceleraciones máximas del tablero, como de desplazamientos. Además, se deben tener en cuenta los efectos dinámicos en los esfuerzos producidos por el paso del tren sobre la estructura.

4.4.1. Esfuerzos

En una primera aproximación, se puede aceptar que -teniendo en cuenta que los esfuerzos estructurales dependen de los desplazamientos- la amplificación en esfuerzos dinámicos es proporcional a la amplificación producida en desplazamientos. Por tanto, a la hora de comprobar los *Estados Límite* de las secciones estructurales, la amplificación dinámica de los esfuerzos y tensiones de estas secciones puede suponerse proporcional al incremento dinámico de los desplazamientos.

En el Cuadro 5 se muestran los siguientes resultados:

- δ^{tipo}_{est} flecha estática en metros para el modelo de carga tipo (UIC,RENFE,SW).
- $\delta^{real}_{din,ideal}$ flecha dinámica máxima en metros obtenida como resultado del barrido de velocidades para cada tren sobre la estructura supuesta ideal.
- Φ_v factor de amplificación dinámica debido al efecto dinámico de las cargas:

$$\Phi_v = \frac{\delta^{real}_{din,ideal}}{\delta^{tipo}_{est}}$$

- $\delta^{real}_{est,ideal}$ flecha estática en metros para el tren de carga real. Este valor se obtiene mediante una pasada a 5 km/h de cada tren sobre la estructura.
- Φ_i factor de amplificación dinámica debido a las irregularidades del carril:

$$\Phi_i = 0{,}5\varphi'' \frac{\delta^{real}_{est,ideal}}{\delta^{tipo}_{est}}$$

- Φ factor de amplificación dinámica total:

$$\Phi = \Phi_v + \Phi_i$$

Observando los valores de Φ obtenidos en el Cuadro 5 se observa que no se supera el valor 1 en ningún caso, lo cual implica que **los esfuerzos dinámicos son inferiores a los producidos por las cargas estáticas.**

4.4.2. Aceleraciones

En la tabla 6 se muestran las aceleraciones verticales máximas en centros de vano y las velocidades de pasada de los trenes que las originan obtenidas tras el barrido de velocidades, se observa que **se cumplen las limitaciones establecidas por la normativa vigente:**

	vano	δ_{est}^{tipo} $10^{-6} \times [m]$	$\delta_{din,ideal}^{real}$ $10^{-6} \times [m]$	Φ_v	$\delta_{est,ideal}^{real}$ $10^{-6} \times [m]$	Φ_i	Φ
Tren 3	V-1	2700	1233	0.457	734	0.008	0.465
	V-2	4333	2819	0.651	1195	0.008	0.659
	V-3	4333	2590	0.598	1198	0.008	0.606
	V-4	2700	1587	0.588	737	0.008	0.596
Tren 4	V-1	2700	1258	0.466	642	0.007	0.473
	V-2	4333	1655	0.382	940	0.006	0.388
	V-3	4333	1826	0.421	940	0.006	0.428
	V-4	2700	1360	0.504	642	0.007	0.511

Cuadro 5: *Flechas dinámicas máximas y factores de amplificación dinámica.*

- $a_{max} < 0{,}35g$ en puentes con vías sobre balasto (una o más vías). Estructura completa bajo la acción de un sólo tren. Vibraciones de frecuencia inferior a 20 Hz.
- $a_{max} < 0{,}5g$ en cualquier otro caso.

	$V_{barrido}$ $[m/s]$	a_{max} $[g]$	$a_{max,irr}$ $[g]$
Vano 1	$V_{Tren4} = 103{,}6$	0.089	0.092
Vano 2	$V_{Tren3} = 106{,}1$	0.129	0.133
Vano 3	$V_{Tren3} = 105{,}3$	0.120	0.123
Vano 4	$V_{Tren4} = 103{,}6$	0.096	0.099

Cuadro 6: *Aceleraciones verticales máximas.*

4.4.3. Desplazamientos

En el Cuadro 7 se muestran los desplazamientos verticales máximos en centros de vano y las velocidades de pasada de los trenes que los originan obtenidos tras el barrido de velocidades.

Los desplazamientos verticales máximos en centros de vano para una vía cargada originados por el modelo de carga estática de la UIC propuesto en el *borrador IAPF*, δ_{est}^{tipo}, se muestran en la última columna del Cuadro 7. Comparando con las flechas máximas dinámicas (1 vía) se observa que para el *Estado Límite de Servicio de Deformaciones* es necesario **utilizar los valores máximos obtenidos en el cálculo mediante modelos de carga estática.**

	$V_{barrido}$ $[m/s]$	$\delta_{din,irr}$ $[m]$	δ_{est}^{tipo} $[m]$
Vano 1	$V_{Tren4} = 102{,}8$	0.001296	0.002700
Vano 2	$V_{Tren3} = 106{,}9$	0.002904	0.004333
Vano 3	$V_{Tren3} = 104{,}7$	0.002668	0.004333
Vano 4	$V_{Tren3} = 106{,}1$	0.001635	0.002700

Cuadro 7: *Desplazamientos verticales máximos.*

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